NUREG/CR-4551 SAND86-1309 Vol. 2, Rev. 1, Part 7

# Evaluation of Severe Accident Risks: Quantification of Major Input Parameters

**MACCS** Input

Prepared by J. L. Sprung, J. A. Rollstin, J. C. Helton, H-N Jow

Sandia National Laboratories Operated by Sandia Corporation

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Manuscript Completed: November 1990 Date Published: December 1990

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Estimation of offsite accident consequences is the customary final step in a probabilistic assessment of the risks of severe nuclear reactor accidents. Recently, the Nuclear Regulatory Commission reassessed the risks of severe accidents at five U.S. power reactors (NUREG-1150). Offsite accident consequences for NUREG-1150 source terms were estimated using the MELCOR Accident Consequence Code System (MACCS). Before these calculations were performed, most MACCS input parameters were reviewed, and for each parameter reviewed, a best-estimate value was recommended. This report presents the results of these reviews. Specifically, recommended values and the basis for their selection are presented for MACCS atmospheric and biospheric transport, emergency response, food pathway, and economic input parameters. Dose conversion factors and health effect parameters are not reviewed in this report.

#### ABSTRACT

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#### 1. INTRODUCTION

Estimation of offsite accident consequences is the customary final step in a probabilistic assessment of the risks of severe nuclear reactor accidents. For NUREG-1150 source terms [1,2], offsite accident consequences were estimated using the MELCOR Accident Consequence Code System (MACCS) [3-5]. In preparing for the performance of those calculations, most input parameters for the MACCS offsite consequences analysis code were reviewed, and for each parameter reviewed, a best estimate value and an uncertainty range were estimated. The following chapters summarize these reviews. Sample MACCS input files for the NUREG-1150 calculations are presented in Appendix A. The remainder of this chapter provides a brief overview of offsite consequence modeling.

#### 1.1 Offsite Accident Progression

Should a severe reactor accident culminate in containment failure, winds would transport the radioactive gases and aerosols in the plume released to the atmosphere away from the reactor site. Downwind populations would be exposed to radiation, and land, buildings, and crops would be contaminated by radioactive materials deposited from the plume. Estimation of the range and probability of the health effects induced by the radiation exposures, and of the economic costs and losses that would result from the contamination of land, buildings, and crops is the object of an ex-plant consequence analysis [6,7].

#### 1.2 Input Data and Quantities Calculated

MACCS calculations require the following data:

- The *inventory* at accident initiation (reactor scram) of those radioactive isotopes important for the calculation of ex-plant consequences (e.g., an end-of-cycle reactor core contains about 10<sup>8</sup> Ci of 131<sub>1</sub>).
- The atmospheric source term produced by the accident (number of plume segments released, sensible heat content of each plume segment, time and duration of release, time when offsite officials are warned that an emergency response should be initiated, and the fraction of each important nuclide's scram inventory released with each plume segment).
- Meteorological data characteristic of the site region--usually one year of hourly windspeed, atmospheric stability, and rainfall readings recorded at the site or at a nearby National Weather Service station. Although one year of hourly readings contains 8760 weather sequences, most consequence calculations examine only a representative subset of these sequences (typically about 150 sequences). The representative subset is selected by stratified sampling of the 8760 sequences after sorting of the sequences into categories defined by windspeed, atmospheric stability, and the location (downwind distance) of rain.

- The *population distribution* about the reactor site (the distribution is usually constructed from census data on a polar coordinate grid having 16 angular sectors aligned with the 16 compass directions and some number of radial intervals that extend outward to 500 miles).
- Emergency response assumptions (evacuation time and average speed, effectiveness and occurrence of sheltering, criteria and timing for post-accident relocation of people, decontamination criteria and effectiveness, temporary interdiction criteria for land and buildings, and disposal criteria for contaminated crops).
- Land usage (habitable land fractions, farmland fractions), and economic data (worth of crops, land, and buildings) for the region about the reactor site.

Given these data, MACCS predicts

- Downwind *transport*, *dispersion*, and *deposition* of the radioactive materials released to the atmosphere from the failed containment.
- Short-term and long-term *radiation doses* received by exposed populations via direct (cloudshine, inhalation, groundshine, resuspension) and indirect (ingestion) pathways.
- Mitigation of those doses by *emergency response actions* (evacuation, sheltering, and relocation of people; disposal of milk, meat, and crops; decontamination, temporary interdiction, and condemnation of land and buildings).
- Fatalities and injuries expected within one year of the accident (early health effects) and the latent cancer deaths expected over the lifetime of the exposed individuals.
- Offsite costs of emergency response actions, and of the decontamination, temporary interdiction, and condemnation of milk, crops, land, and buildings.

#### 1.3 <u>Phenomena Modeled</u>

1.3.1 Atmospheric Transport [8,9]

As in most consequence codes [10-14], MACCS neglects wind trajectories. The 16 compass sector population distributions are assumed to constitute a representative set of downwind exposed populations. The exposure probability of each of the 16 compass sector population distributions is assumed to be given by the frequency with which wind blows from the site into the sector (i.e., compass sector site wind rose frequencies). Windspeed determines the rate of downwind transport. Release duration and windspeed determine plume length. Dispersion of the plume in the downwind direction is neglected. Dispersion in the vertical and crosswind directions is estimated using a Gaussian plume model and therefore varies with windspeed and atmospheric stability. Vertical plume expansion is capped by the mixing depth (seasonal mixing layer height).

#### 1.3.2 Deposition

Aerosols are removed from the plume by washout, which varies with rainfall rate, and by diffusion to, impaction on, and gravitational settling onto surfaces. The combined removal rate because of diffusion, impaction, and settling is modeled using an empirical, particle-size-dependent, dry deposition velocity. Runoff of rain and weathering decrease surface concentrations of radioactive aerosols deposited on the ground. Decrease of radioactivity because of radioactive decay is also modeled (only parent and daughter nuclides are followed, since doses from second generation daughters are insignificant).

#### 1.3.3 Emergency Response

Population doses are mitigated by user-specified emergency response actions (evacuation, sheltering, and post-accident relocation of people; decontamination, temporary interdiction, and condemnation of land and buildings; disposal of contaminated meat, milk, and crops).

#### 1.3.4 Dosimetry and Health Effects

Populations located on the MACCS computational grid receive doses from the passing plume (cloudshine), by exposure to materials deposited on the ground (groundshine), by inhalation of airborne radioactive materials (from the plume or from mechanical or wind driven resuspension of materials deposited on the ground), and by ingestion of contaminated water and foods. Contaminated water and foods may also be consumed by populations off of the computational grid.

Health effects are calculated from doses to specific organs [15]. Doses to specific organs are calculated using dose conversion factors [16]. Early injuries and fatalities (those that occur within one year of the accident) are estimated using nonlinear dose-response models. A recent expert review of radiation induced health effects [17] recommended the use of Hazard functions  $(H_i)$  when calculating early injuries or fatalities due to damage to organ i. Thus, the risk (r) per person of contracting a given early health effect is given by

 $r = 1 - \exp \{\sum_{i} -H_{i}\}$   $H_{i} = \ln 2 (D_{i}/D_{50,i})^{\beta}$   $H_{i} = 0 \text{ if } D_{i} \leq D_{th,i}$ 

where  $D_i$  is the dose received by the impaired organ,  $D_{th,i}$  is the damage threshold (dose threshold values are poorly known and variable over any population cohort),  $D_{50,i}$  is the dose that induces the specified health effect in half of the exposed population (LD<sub>50</sub> value for deaths), and  $\beta$  is a parameter that determines the slope of the dose-response curve. Sums of Hazard functions are used (1) to model any health effect that has D<sub>50</sub> values that vary significantly with exposure period, and (2) to model early fatalities where death may be caused by the impaired functioning of several organs. Linear-quadratic, zero-threshold, dose-response models are recommended by several recent reviews of mortality caused by radiation-induced cancers [18-20]. However, the quadratic portion of the model is not important, when long-term individual exposures are limited to 25 rems in 30 years, as is done in most consequence calculations. Accordingly, cancer fatality predictions are linear with dose. Cancer fatality predictions are not always linear with source term magnitude because dose is avoided by crop disposal and by decontamination and interdiction of land and buildings.

#### 1.3.5 Economic Effects

Economic consequences [21] are estimated by summing the following costs: evacuation costs, temporary relocation costs (food, lodging, lost income), costs of decontaminating land and buildings, the value of crops destroyed because they were contaminated by direct deposition or root uptake, the value of farmland and of nonfarm commercial, public, and individual property that is condemned. Costs for damage to the reactor, the purchase of replacement power, medical care, life-shortening, and litigation are not calculated by MACCS.

#### 1.4 Computational Framework

Figure 1-1 depicts the progression of a consequence calculation for one source term, one weather sequence, and one exposed population distribution. However, severe accidents can lead to source terms of quite different magnitudes (e.g., negligible at TMI, substantial at Chernobyl), and the weather conditions at the time of the release can greatly alter consequence magnitudes (e.g., intense rain at the time of the release or plume transport out to sea would largely eliminate health effects, while rainout of the plume onto a downwind city would greatly increase early fatalities).

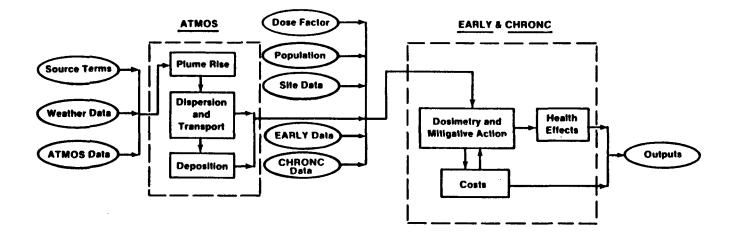


Figure 1-1. Progression of a Consequence Calculation.

Because consequences vary with source term magnitude, weather, and population density, to develop statistical distributions of consequence measures (doses, health effects, costs) that depict the range and probability of consequences for the reactor being examined, consequence assessments must examine all possible combinations of representative sets of source terms, weather sequences, and exposed populations. Usually distributions that display the variation of consequences with weather and population density are first developed for each representative source term. Then an integral depiction of consequences may be constructed by weighted summation of these source term dependent distributions, with each distribution weighted by the estimated absolute probability of occurrence of its underlying source term.

#### REFERENCES

- [1] U.S. Nuclear Regulatory Commission, <u>Severe Accident Risks: An</u> <u>Assessment for Five U.S. Nuclear Power Plants</u>, NUREG-1150, June 1989.
- [2] E. Gorham-Bergeron et al., <u>Evaluation of Severe Accident Risks</u>, Vol. 1, <u>Part I: Methodology for the Accident Progression</u>, <u>Source Term</u>, <u>Consequence</u>, <u>Risk Integration and Uncertainty Analyses</u>, NUREG/CR-4451, SAND86-1309, Sandia National Laboratories, Albuquerque, NM, in preparation.
- [3] D. I. Chanin et al., <u>MELCOR Accident Code System (MACCS)</u>, Vol. I: <u>User's Guide</u>, NUREG/CR-4691, SAND86-1562, Sandia National Laboratories, Albuquerque, NM, 1990.
- [4] H. N. Jow et al., <u>MELCOR Accident Code System (MACCS)</u>, Vol. II: <u>Model</u> <u>Description</u>, NUREG/CR-4691, SAND86-1562, Sandia National Laboratories, Albuquerque, NM, 1990.
- [5] J. A. Rollstin et al., <u>MELCOR Accident Code System (MACCS)</u>, Vol. III: <u>Programmer's Reference Manual</u>, NUREG/CR-4691, SAND86-1562, Sandia National Laboratories, Albuquerque, NM, 1990.
- [6] U.S. Nuclear Regulatory Commission, <u>PRA Procedures Guide</u>, Vol. II, Chapter 9, "Environmental Transport and Consequence Analysis," NUREG/CR-2300, Washington, DC, 1983.
- [7] CEC, <u>Radiation Protection: Methods for Assessing the Off-Site</u> <u>Radiological Consequences of Nuclear Accidents</u>, EUR 10243 en, Commission of the European Communities, Luxemburg, 1986.
- [8] D. Randerson, ed., <u>Atmospheric Science and Power Production</u>, DOE/TIC-27601, U.S. Department of Energy, Washington, DC, 1984.
- [9] S. R. Hanna, <u>Handbook on Atmospheric Diffusion</u>, DOE/TIC-27601, U.S. Department of Energy, Washington, DC, 1982.
- [10] U.S. Nuclear Regulatory Commission, <u>Reactor Safety Study</u>, Appendix VI, "Calculation of Reactor Accident Consequences," WASH-1400, Washington, DC, 1975.

- [11] L. T. Ritchie et al., <u>Calculation of Reactor Accident Consequences</u>, Version 2, NUREG/CR-2324, Sandia National Laboratories, Albuquerque, NM 1981.
- [12] K. Woodard and T. E. Potter, "Modification of the Reactor Safety Study Consequence Computer Program (CRAC) to Incorporate Plume Trajectories," <u>Trans. Am. Nucl. Soc.</u>, Vol. 33, No. 193 (1979).
- [13] A. Bayer et al., "The German Risk Study: Accident Consequence Model and Results of the Study," <u>Nucl. Technol.</u>, Vol. 59, No. 20 (1982).
- [14] R. H. Clarke and G. N. Kelly, <u>The NRPB Methodology for Assessing</u> <u>Radiological Consequences of Accidental Releases of Activity</u>, " NRPB-R127, National Radiological Protection Board, Chilton, England, 1981.
- [15] G. E. Runkle and R. M. Ostmeyer, <u>An Assessment of Dosimetry Data for</u> <u>Accidental Radionuclide Release from Nuclear Reactors</u>, NUREG/CR+4185, Sandia National Laboratories, Albuquerque, NM, 1985.
- [16] D. C. Kocher, "Dose Rate Conversion Factors for External Exposure to Photons and Electron Radiation from Radionuclides Occuring in Routine Releases from Nuclear Fuel Cycle Facilities," <u>Health Phys.</u>, Vol. 38, p. 543 (1980).
- [17] J. S. Evans et al., <u>Health Effects Model for Nuclear Power Plant</u> <u>Accident Consequence Analysis</u>, NUREG/CR-4214, Sandia National Laboratories, Albuquerque NM (1985).
- [18] United Nations Scientific Committee of Atomic Radiation, <u>Sources and</u> <u>Effects on Ionizing Radiation</u>, United Nations, NY, 1977.
- [19] Advisory Committee on the Biological Effects of Ionizing Radiation, <u>The Effects on Populations of Exposure to Low Levels of Ionizing Radiation</u>, National Academy of Sciences, Washington, DC, 1980.
- [20] National Council on Radiation Protection and Measurements, <u>Influence of</u> <u>Dose and Its Distribution in Time on Dose-Response Relationships for</u> <u>Low-LET Radiations</u>, NCRP Rept. No. 64, Washington, DC, 1980.
- [21] R. P. Burke et al., <u>Economic Risks of Nuclear Power Reactor Accidents</u>, NUREG/CR-3673, Sandia National Laboratories, Albuquerque, NM, 1984.

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MACCS allows a release of radioactive materials to the atmosphere to be divided into plume segments, which can have different compositions, release durations, and energies (amounts of sensible heat). Plume segment lengths are determined by the product of the segment's release duration and the average windspeed during release. The initial vertical and horizontal dimensions of each plume segment are user specified. If release occurs into a building wake, then wake dimensions can be used to set the initial crosswind dimensions of the plume. If not, a point source can be specified.

A liftoff criterion (a critical windspeed that increases as plume buoyancy increases [1]) determines whether buoyant plumes are subject to plume rise. When the windspeed at release equals or exceeds the critical windspeed, plume rise is prevented. When the windspeed at release is less than the critical windspeed, plume rise is allowed, and the height to which a buoyant plume rises is determined using equations recommended by Briggs [2,3].

After release, windspeed determines the rates at which plume segments transport in the downwind direction, and wind direction at the time of release determines the direction of travel. As is done by most consequence codes [4,5], MACCS neglects wind trajectories. The sixteen compass sector population distributions are assumed to constitute a representative set of downwind exposed populations. The exposure probability of each of the 16 compass sector population distributions is assumed to be given by the frequency with which wind blows from the site into the sector (i.e., compass sector site wind rose frequencies).

During transport, dispersion in the vertical and horizontal (crosswind) directions is estimated using a Gaussian plume model [6]. Thus, dispersion rates depend on windspeed and on atmospheric stability. The crosswind Gaussian distribution of each plume segment is approximated by a multistep histogram. Although horizontal dispersion of plume segments is unconstrained, vertical dispersion is bounded by the ground and by the depth of the mixing layer (as specified by annual or seasonal mixing layer heights [7]), which are modeled as totally reflecting layers using mirror image sources [6]. Since the number of reflections increases as travel times lengthen, the vertical distribution of each plume segment eventually becomes uniform and is so modeled thereafter [8].

In MACCS, aerosols are removed from the plume by washout, which varies with rainfall rate [9], and by diffusion to, impaction on, and gravitational settling onto surfaces. The combined removal rate due to diffusion, impaction, and settling is modeled using an empirical, dry deposition velocity [10]. Because dry deposition velocity varies with particle size, if the aerosol size distribution is divided into ranges, a dry deposition velocity must be specified for each range.

Water bodies (rivers, great lakes, oceans) are contaminated by direct deposition of radioactive materials onto their surfaces, by runoff of contaminated rain that falls on land, and by washoff from land by uncontaminated rain of previously deposited contamination. Weathering, resuspension, runoff, washoff, and radioactive decay decrease surface concentrations of radioactive materials deposited on the ground. Weathering is modeled using Gale's equation [11]. Resuspension is modeled using resuspension factors [10] that attempt to represent the average effect of resuspension by many processes at very different rates throughout large regions. Runoff is modeled by assuming that some fixed fraction of all materials initially deposited onto land is rapidly transferred to water bodies either during the initial rain event or by rain events that occur very soon after the initial deposition [12]. Washoff is modeled as a first order removal process that is integrated over all time after the initial deposition [12]. Decrease of radioactivity due to radioactive decay treats only first generation daughter products, since doses from second generation daughters are insignificant.

#### 2.1 <u>Reactor Dimensions</u>

#### 2.1.1 Recommendation.

Table 2.1 gives the values recommended for initial plume (reactor wake) dimensions for the MACCS NUREG-1150 calculations.

		BUI	LDHa		BUIL	'DMp
<u>Reactor</u>	Value	<u>Range</u>	Distribution	Value	<u>Range</u>	Distribution
Surry	50	10-50	Uniform	40	10-?	Uniform
Sequoyah	40	10-40	Uniform	40	10-225	Uniform
Peach Bottom	50	10-50	Uniform	50	10-200	Uniform
Grand Gulf	60	10-60	Uniform	40	10-175	Uniform
a BUILDH - B b BUILDW - B		<u> </u>				

Table 2.1.	Values	for	Initial	Plume	Dimensions

#### 2.1.2 <u>Discussion</u>

In MACCS, the values specified for BUILDH and BUILDW determine the initial size of the plume upon escape from the wake of the reactor. Specifically, initial values for  $\sigma_z$  and  $\sigma_y$ , the vertical and crosswind standard deviations of the Gaussian plume, are calculated using the following relations [13a]:

BUILDH = 2.15  $\sigma_z$ BUILDW = 4.3  $\sigma_y$ 

These equations allow mixing of the plume into the reactor wake to be modeled by first setting crosswind plume dimensions upon escape from the wake equal to the crosswind dimensions of the wake and then backcalculating an upwind virtual point source for a plume with these dimensions. Both theory [13b] and experiments [1] suggest that a plume released from a building under turbulent conditions will be entrained by the building's wake and before escaping from that wake will become well mixed throughout its volume. As long as windspeeds are significant, entrainment and thorough mixing occur not only when the release occurs from the lee face of the building, but also from its side, top, or upwind face. However, when conditions are not turbulent, the plume is observed to escape from the wake before becoming well mixed throughout its full volume.

These observations suggest that selecting values for BUILDH and BUILDW may not be straightforward. For example, for release from a rectangular building under turbulent conditions, the crosswind dimensions of the wake will depend on the orientation of the wind relative to the building. Moreover, when turbulence is minimal, initial plume dimensions upon escape from the building wake may be much smaller than the crosswind dimensions of the wake itself. Indeed, if windspeeds are very low, initial plume dimensions may be much closer to the dimensions of the hole in the building from which the plume issues, than to the dimensions of the building's wake.

Experiments also indicate that when prevailing conditions are turbulent, plume growth is so rapid that downwind size soon becomes independant of size upon escape from the building wake. Therefore, use of initial plume dimensions appropriate for release under nonturbulent conditions will not lead to significant errors if applied to releases under turbulent conditions. But failure dimensions are not known for NUREG-1150 source terms and no simple model for mixing into a portion of a building wake is available. Therefore, the specification of plume dimensions upon escape from the building wake when conditions are nonturbulent must be largely a guess.

Since some mixing into the building wake will occur whenever the prevailing wind is not stagnant, use of dimensions significantly larger than the dimensions of the containment failure seems appropriate. This will also be correct for blowdown plumes where dissipation of the energy of the jet produces substantial expansion of the plume (e.g., a jet that issues from a 1 m<sup>2</sup> hole will produce a plume with a cross-sectional area of about 100 m<sup>2</sup> after expansion dissipates the initial energy of the jet [14]). Therefore, somewhat arbitrarily, after rounding to the nearest multiple of 10 m, the dimensions of the reactor containment as read from FSAR drawings [15-18] are given above for BUILDH and BUILDW.

#### 2.1.3 Correlations

BUILDH and BUILDW will be strongly correlated with prevailing atmospheric stability. Specifically, when unstable (Classes A-C) or neutral (Class D) atmospheric conditions prevail, the plume will become well mixed throughout the wake cavity before it escapes from the building wake. Therefore, when unstable or neutral conditions prevail, values at the upper end of the ranges specified above for BUILDH and BUILDW should be used. Conversely, when stable atmospheric conditions prevail (Classes E and F), the plume may either not be completely entrained into the building wake or, if completely entrained, may not become well mixed throughout its volume before escaping. Therefore, when stable atmospheric conditions prevail, values at the lower end of the ranges specified above for BUILDH and BUILDW should be used. Because BUILDH and BUILDW are both correlated in the same way with atmospheric stability, they are also positively correlated with each other. For blowdown plumes, BUILDH and BUILDW will also be strongly and positively correlated with the energy of the blowdown jet. Finally, for plumes not initialized by blowdown, the nature of the correlation of BUILDH and BUILDW with atmospheric stability may cause the distributions of these variables to be bimodal, having small values when stable conditions prevail and large values when neutral or unstable conditions prevail.

#### 2.2 Plume Rise

2.2.1 Recommendation

The values in Table 2.2 are recommended for plume rise scaling factors.

/ariable	Summary
· · · · · · · · · · · · · · · · · · ·	
CLCRW	Linear scaling factor on the critical wind speed $(U_c)$ used in MACCS to determine whether buoyant plumes will be trapped in the turbulent wake of the reactor building complex. For any release, if the wind speed is greater than $U_c$ , the plume is assumed to be trapped in the building wake, thereby preventing plume rise. By scaling the value of $U_c$ , the MACCS user can examine the effect of the critical windspeed for escape from the building wake on the occurrence of plume rise.
, ,	Base value: 1.0 Range: 0.5 to 2.0
CLADP	Linear scaling factor on the amount of plume rise that will occur when the prevailing atmospheric conditions are characterized by stability class A, B, C, or D.
CLADP	Linear scaling factor on the amount of plume rise that will occur when the prevailing atmospheric conditions are
CLADP	Linear scaling factor on the amount of plume rise that will occur when the prevailing atmospheric conditions are characterized by stability class A, B, C, or D.
	Linear scaling factor on the amount of plume rise that will occur when the prevailing atmospheric conditions are characterized by stability class A, B, C, or D.

#### 2.2.2 Discussion

The parameter values that determine plume rise are all hardwired in MACCS. The user can modify them only by using the scaling factors, SCLCRW, SCLADP, or SCLEFP. A short overview of the plume rise formula that these scaling factors modify is presented below.

SCLCRW is a factor that linearly scales the critical wind speed;  $U_c$ ; that MACCS uses to determine if buoyant plumes escape from the turbulent wake of a reactor complex before they dissipate all of their buoyancy. The critical wind speed is defined by [1]:

$$U_c = (9.09 \text{ F/L})^{1/3}$$

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where

F = buoyancy flux from the source =  $8.8 \times 10^{-6}Q$ , Q = energy release rate (Joules/s), and

L = suitable length scale for the reactor building (m).

This expression was first suggested by Briggs [19] and later experimentally confirmed by Hall and Waters during wind tunnel experiments with 1/300 scale models [1]. However, it should be noted that the critical wind speed does not mark a sudden change in the plume position as ground level concentrations change relatively slowly with the buoyancy parameter,  $F/U^3L$ . Since the coefficient 9.09 is uncertain by something like an order of magnitude, Uc must be uncertain by about a factor of two.

SCLADP is a factor that linearly scales the amount of plume rise predicted by MACCS when the prevailing atmospheric stability class is A through D. The plume rise formula for stability classes A through D used in MACCS is Equation 2.15 in Hanna et al. [3]:

$$\Delta h = \frac{1.6 \ F^{1/3} \ X^{2/3}}{U}$$

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where

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The above expression is the so-called "2/3 law," which agrees well with field studies and laboratory data. In Reference [3], the authors pointed out that the coefficient 1.6 can be expected to be accurate to  $\pm 40$ %. Therefore, the value of  $\Delta h$  must be uncertain by at least a factor of 1.5.

2-5.

SCLEFP is a factor that linearly scales the amount of plume rise predicted by MACCS when the prevailing atmospheric stability class is E or F. The plume rise formula for stability classes E and F is Equation 3.19 in Hanna et al. [3]:

 $\Delta h = 2.6 [F/(US)]^{1/3}$ 

where

 $\Delta h = plume rise above release height (m),$ 

F = buoyancy flux parameter  $(m^4/s^3) = 8.8 \times 10^{-6} Q$ ,

Q = energy release rate (Joules/s),

U = wind speed (m/s), and

S = stability parameter (see discussion for details)

= (g/T) (dT/dZ + 0.01 K/m).

where

 $g = gravitational constant = 9.8 m/s^2$ , T = ambient temperature (K), and dT/dZ = vertical temperature gradient for stability class E or F.

In NRC Regulatory Guide 1.23 [20], dT/dZ is expressed by

dT/dZ = -0.5 to 1.5 K/100 m, for class E dT/dZ = 1.5 to 4.0 K/100 m, for class F

By taking the midpoints of these ranges, we have

dT/dZ = 0.5 K/100 m = 0.005 K/m, for class E dT/dZ = 2.75 K/100 m = 0.0275 K/m, for class F

After substituting the above values for dT/dZ and 288 K (the reference temperature for the standard atmosphere) for T, we have

 $S = 5.1 \times 10^{-4}$ , for stability class E S = 1.27 \times 10^{-3}, for stability class F

These values are currently hardwired in MACCS. Note that S is a function of ambient temperature T, which could vary from 270 K to 308 K for a site with a temperate climate.

#### 2.3 Plume Meander

#### 2.3.1 Recommendation

Table 2.3 lists the values recommended for the parameters used in MACCS to correct Pasquill-Gifford  $\sigma_y$  values for the effects of horizontal meandering of plume segments:

	Definition	
-	Delimition	<del>_</del>

Table 2.3. MACCS Correction Paramet	cers	
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<u>Variable</u>	Definition	Value
TIMBAS	Release time for the Prairie Grass experiments (s)	180
XPFAC1	Release time exponent for releases shorter than BRKPNT	0.2
XPFAC2	Release time exponent for releases greater than or equal to BRKPNT	0.25
BRKPNT	Release time break point for changing from XPFAC1 to XPFAC2 (s)	3600

#### 2.3.2 Discussion

MACCS uses the following equation to correct Pasquill-Gifford  $\sigma_{\rm y}$  values for the effect of horizontal meandering of plume segments [21]:

$$\sigma_{y,MACCS}(x) = \sigma_{y,P-G}(x) [\Delta t_{seg}/\Delta t_{P-G}]^{m}$$

where x is the downwind distance of the plume segment from its point of release,  $\sigma_{y,MACCS}(x)$  is the  $\sigma_{y}$  value used in MACCS,  $\sigma_{y,P-G}(x)$  is the Pasquill-Gifford value for  $\sigma_{y}$  at the distance x,  $\Delta t_{seg}$  is the release duration of the plume segment, and  $\Delta t_{P-G} = 10$  minutes [22,23,3b] is the release duration of the Prairie Grass Project [24] plumes, which are the experimental basis for the Pasquill-Gifford curves that express the increase of  $\sigma_y$  with downwind distance [25]. Parameter values for this equation have been reviewed by Gifford [26], who suggests that m = 0.2 when  $\Delta t$  is greater than 3 minutes but less than 1 hour, that m = 0.25 when t = 1 hour, and that m = 0.3 when  $\Delta t =$ 100 hours. Since in MACCS plume segment durations may not exceed 10 hours, m = 0.25 is recommended for plume segments having release durations between 1 and 10 hours.

#### 2.4 <u>Plume Dispersion</u>

The power-law parameter values recommended in Table 2.4 for use in MACCS to estimate stability-class dependent values for  $\sigma_y$  and  $\sigma_z$  are the values developed by Tadmor and Gur [27]:

<u>Variable</u>		• `	Defini	tion	4	
DPCYSIGA	coeffici	lent in	the powe	r-law ex	xponenti pression ility Cl	for $\sigma_{\rm s}$
	A	<u></u> B	C	D	E	F
- 14 - 15 - 17 	0.3658	0.2751	0.2089	0.1474	0.1046	0.072
DPCYSIGB		•	depende ssion fo	-	ent in t	he
.:	Values b	oy Pasqu	ill-Giff	ord Stab	ility Cl	ass
	<u> </u>	<u> </u>	C	D	E	F
	0.9031	0.9031	0.9031	0.9031	0.9031	0.903
·	<i>ь</i> .					
DPCZSIGA					xponenti pression	
DPCZSIGA	coeffici	ient in	the powe	er-law ex		for $\sigma$
DPCZSIGA	coeffici	ient in	the powe	er-law ex	pression	for $\sigma$
DPCZSIGA	coeffici	ient in by Pasqu	the powe	er-law ex	pression bility Cl	ass
DPCZSIGA	coeffic: Values b A	ient in by Pasqu <u>B</u> 0.9031	the powe iill-Giff  0.9031	er-law ex	pression	ass
DPCZSIGA DPCZSIGB	coeffici Values b A 0.9031 0.00025 Stabilin	ient in by Pasqu <u>B</u> 0.9031 0.0019 ty class	the powe iill-Giff  0.9031 0.2	or-law ex ford Stab  0.9031 0.3 ent expor	pression ility Cl <u>E</u> 0.9031	a for <i>o</i> .ass <u>F</u> 0.903 0.2
· .	coeffici Values b A 0.9031 0.00025 Stabilit power-la	ient in by Pasqu <u>B</u> 0.9031 0.0019 ty class aw expre	the powe ill-Giff  0.9031 0.2 depende ssion fo	er-law ex Ford Stab D 0.9031 0.3 ent export or $\sigma_y$	Epression Mility Cl E 0.9031 0.4	for $\sigma_1$ ass F 0.903 0.2 the
· .	coeffici Values b A 0.9031 0.00025 Stabilit power-la	ient in by Pasqu <u>B</u> 0.9031 0.0019 ty class aw expre	the powe ill-Giff  0.9031 0.2 depende ssion fo	er-law ex Ford Stab D 0.9031 0.3 ent export or $\sigma_y$	pression ility Cl <u>E</u> 0.9031 0.4 ent in t	for $\sigma_1$ ass F 0.903 0.2 the

#### 2.4.1 Discussion

In MACCS, horizontal and vertical dispersion of plume segments about their centerlines are calculated using Gaussian plume models [21]. These models assume that dispersion of plume materials produces normal distributions in the horizontal (y) and vertical (z) directions. Thus, the standard deviations ( $\sigma_y$  and  $\sigma_z$ ) of these distributions determine the horizontal and vertical extent of each plume segment, and are calculated using the following:

$$\sigma_y = ax^b$$
  $\sigma_z = cx^d$  (2.1)

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where a = DPCYSIGA, b = DPCYSIGB, c = DPCZSIGA, d = DPCZSIGB, and x is the distance from the segment's release point to its present location. The values of the coefficients a, b, c, and d depend on atmospheric stability and thus vary with the six stability classes (Pasquill-Gifford classes A-F) used in MACCS. So whenever stability class changes, the apparent upwind location of the release (virtual source distance) must be recalulated by solving Equation 2.1 for x using the current value of  $\sigma_y$  or  $\sigma_z$  and the values of the parameters a, b, c, and d that correspond to the new atmospheric stability class.

Analytical fits of Equation 2.1 to experimental diffusion data measured in the field have been developed for all of the six Pasquill-Gifford stability classes by Tadmor and Gur [27], by Klug [28], and by Geiss [28]. The fits of Tadmur and Gur and of Klug are based on data gathered during the Prairie Grass Project [24]. The fits of Geiss are based on field studies of diffusion performed near the Julich Nuclear Research Center in Germany. The Prairie Grass (low surface roughness). The releases were cold, of short duration (10 min.), and made at ground level. Downwind measurements were made to a distance of 0.8 km. The Julich experiments were conducted over farmland (medium surface roughness) and woodland (high surface roughness). The releases were cold, not a farmland (medium surface roughness) and woodland (high surface roughness). The releases were cold, had one hour durations, and were made at three heights (50, 100, and 180 m).

Table 2.5 presents the values of a, b, c, and d developed by Tadmor and Gur, by Klug, and by Geiss:

		Pasquill-Gifford Diffusion Class					
<u>Study</u>	<u>Constant</u>	A	<u>B</u>	C	D	E	F
Tadmor	а	0.3658	0.2751	0.2089	0.1474	0.1046	0.0722
& Gur	Ъ	0.9031	0.9031	0.9031	0.9031	0.9031	0.9031
	с	0.00025	0.0019	0.2000	0.3000	0.4000	0.2000
	d	2.125	1.6021	0.8543	0.6532	0.6021	0.6020
Klug	а	0.4690	0.3060	0.2300	0.2190	0.2370	0.2730
	b	0.9030	0.8850	0.8550	0.7640	0.6910	0.5940
	с	0.0170	0.0720	0.0760	0.1400	0.2170	0.2620
	d	1.3800	1.0210	0.8790	0.7270	0.6100	0.5000
Geiss	50m a	1.503	0.876	0.659	0,640	0.801	1.294
	b	0.833	0.823	0.807	0.784	0.754	0.718
	c	0.151	0.127	0.165	0.215	0.264	0.241
	d	1.219	1.108	0.996	0.885	0.774	0.662
Geiss	100m a	0.170	0.324	0.446	0.504	0.411	0.253
00133	b	1.296	1.025	0.866	0.818	0.882	1.057
	c	0.051	0.070	0.137	0.265	0.487	0.717
	d	1.317	1.151	0.985	0.818	0.652	0.486
Geiss	180m a	0.671	0.415	0.232	0.208	0.345	0.671
Gerss	b	0.903	0.903	0.903	0.903	0.903	0.903
	c	0.2045	0.0330	0.104	0.307	0,546	0.484
	d	1.500	1.320	0.997	0.734	0.557	0.500

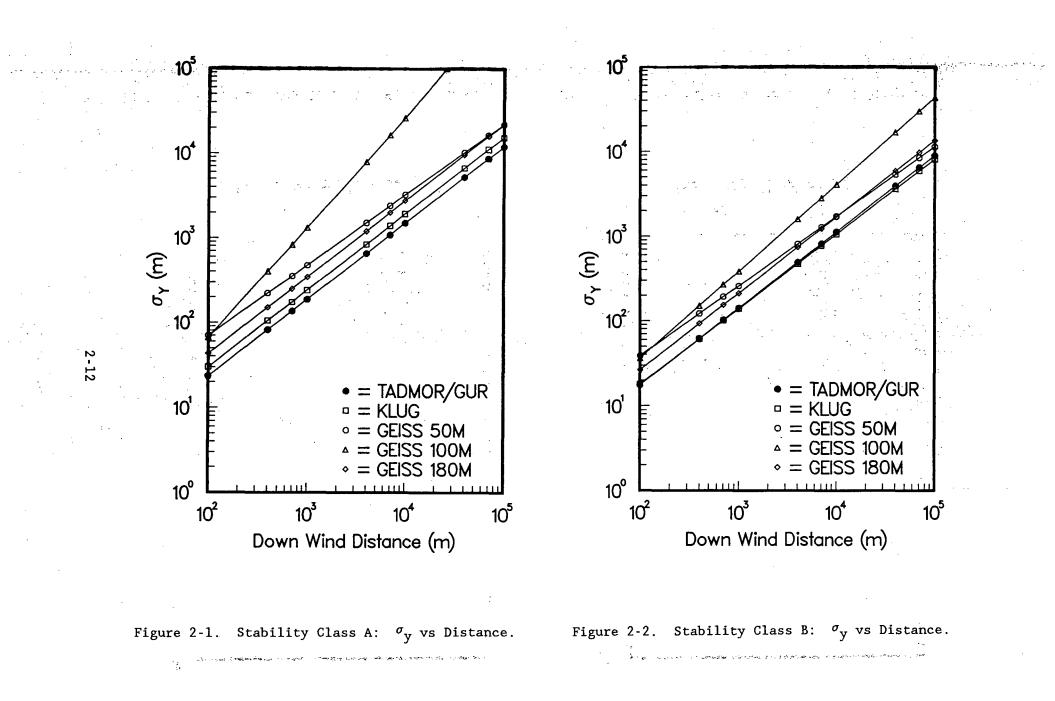
Table 2.5. Values for Constants in Equation 2.1

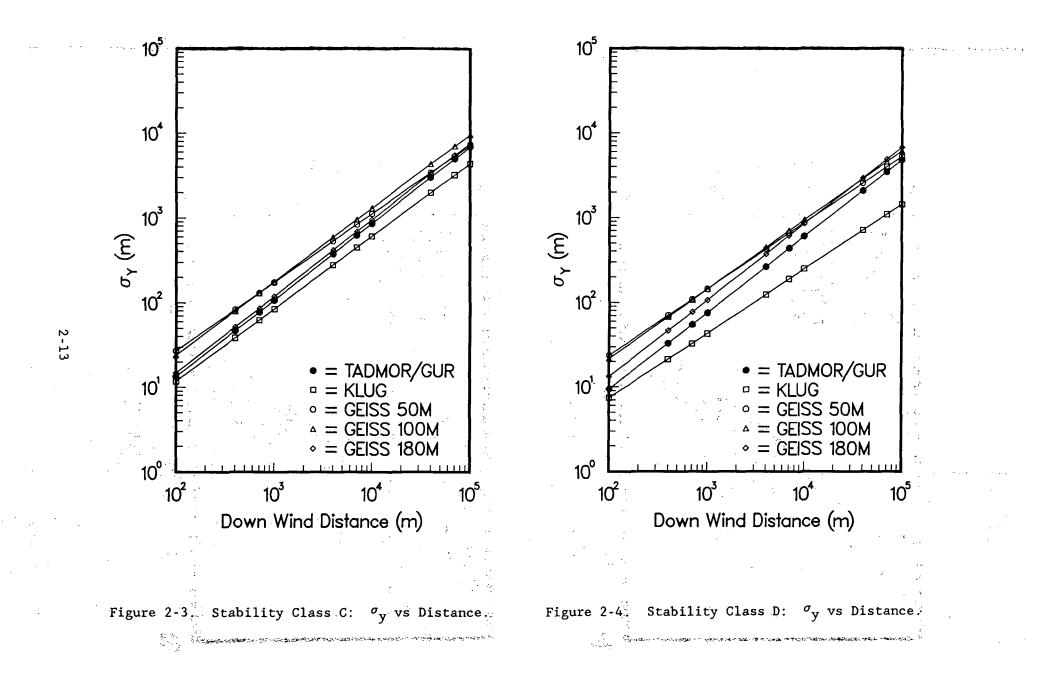
Figures 2.1 through 2.12 compare the effect of these five sets of parameter values on the increase of  $\sigma_y$  and  $\sigma_z$  with downwind distance. Figures 2.1 through 2.6 present the fits for  $\sigma_y$ . The fits for  $\sigma_z$  are presented in Figures 2.7 through 2.12.

Because in MACCS reactor building dimensions determine the initial size (initial  $\sigma_y$  and  $\sigma_z$  values) of plume segments, the slope of the fits displayed in Figures 2.1 through 2.12 is important, but the magnitude of  $\sigma_y$  or  $\sigma_z$  (size of the plume) at a given distance is not. For example, if the width of the reactor building specified in MACCS input corresponds to an initial  $\sigma_y$  value of 250 m and the atmospheric stability at plume release is Class E, then Figure 2.5 shows that MACCS will calculate an initial upwind virtual source distance of 100 m if the Geiss 100 m  $\sigma_y$  fit is used, and an initial upwind virtual source this initialization step is completed, plume growth with downwind transport

distance will be about the same using either  $\sigma_y$  fit, since both fits have about the same slope.

Figures 2.1 through 2.12 show that for any stability class, all the fits have similar slopes with but two exceptions: for stability classes A and B, the Geiss  $\sigma_y$  fits to 100 m releases and the Tadmor and Gur  $\sigma_z$  fits have significantly larger slopes than the other fits to those stability classes. The figures also show that the fits of Geiss to 180 m releases and the fits of Klug have slopes that are qualitatively representative of the envelope of slopes for the fits to any single stability class. Since buoyant plumes typically rise 180 m or so after release and most U.S. reactors are situated in regions having surface roughnesses greater than that of prairie grass, use of the Geiss 100 m fits seems indicated. Nevertheless, for the NUREG-1150 calculations, use of the Tadmur and Gur fits is recommended because relative to their uncertainties all of the fits are more or less equivalent and because the Tadmur and Gur fits have been used in most previous NRC consequence modeling studies.





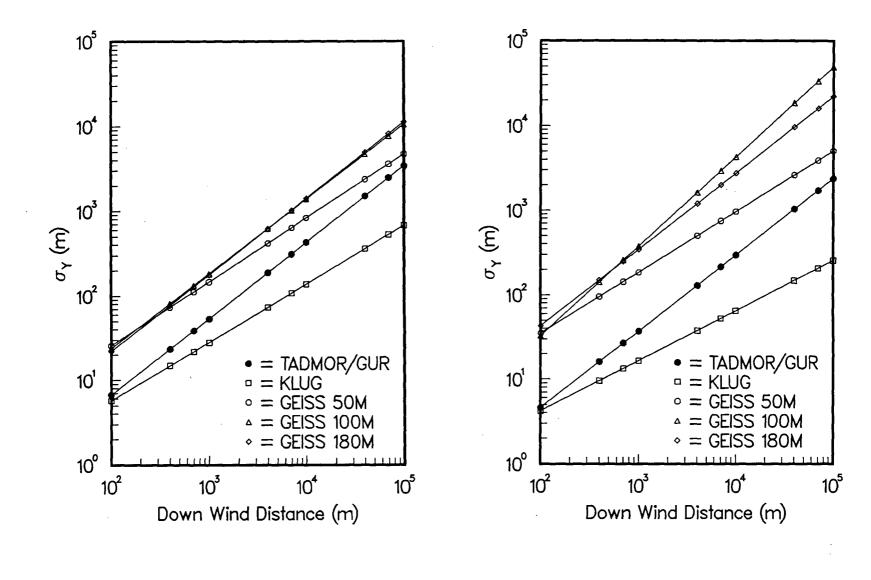
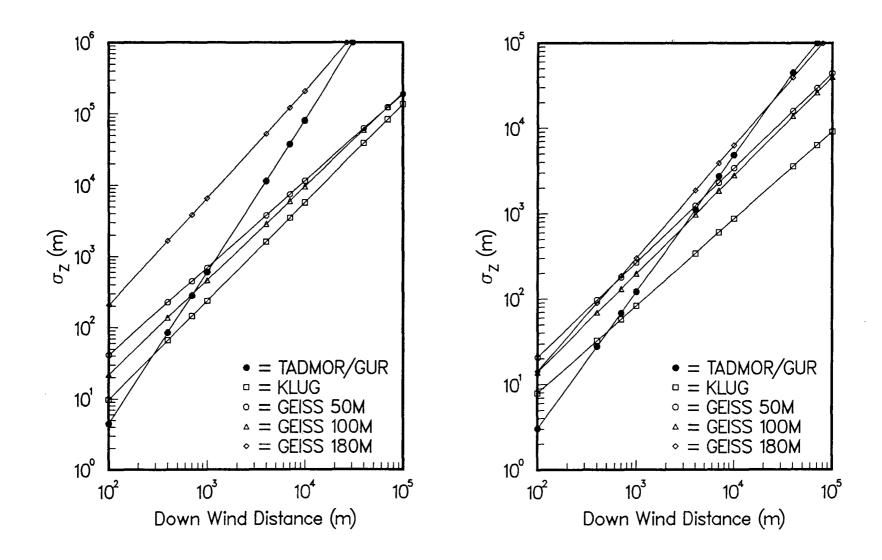


Figure 2-5. Stability Class E:  $\sigma_y$  vs Distance.

Figure 2-6. Stability Class F:  $\sigma_y$  vs Distance.



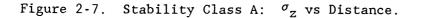


Figure 2-8. Stability Class B:  $\sigma_z$  vs Distance.

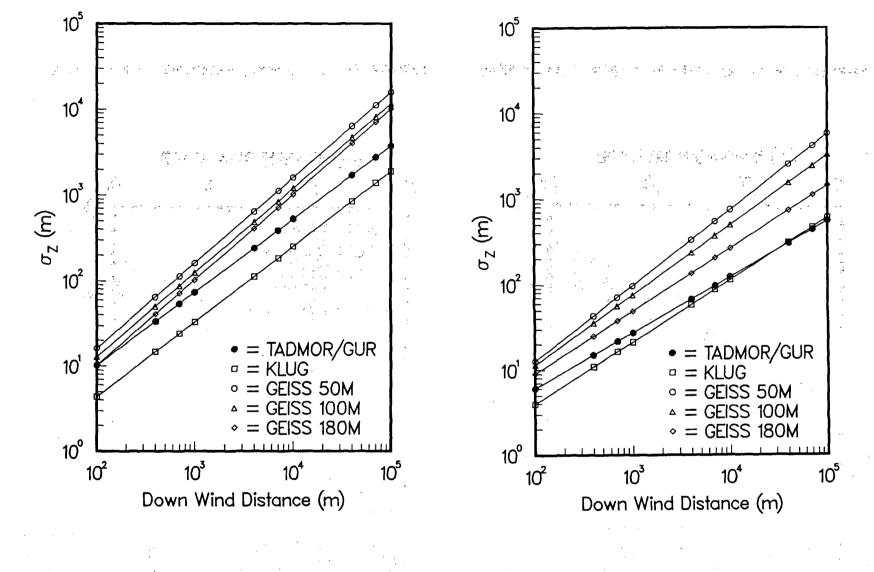
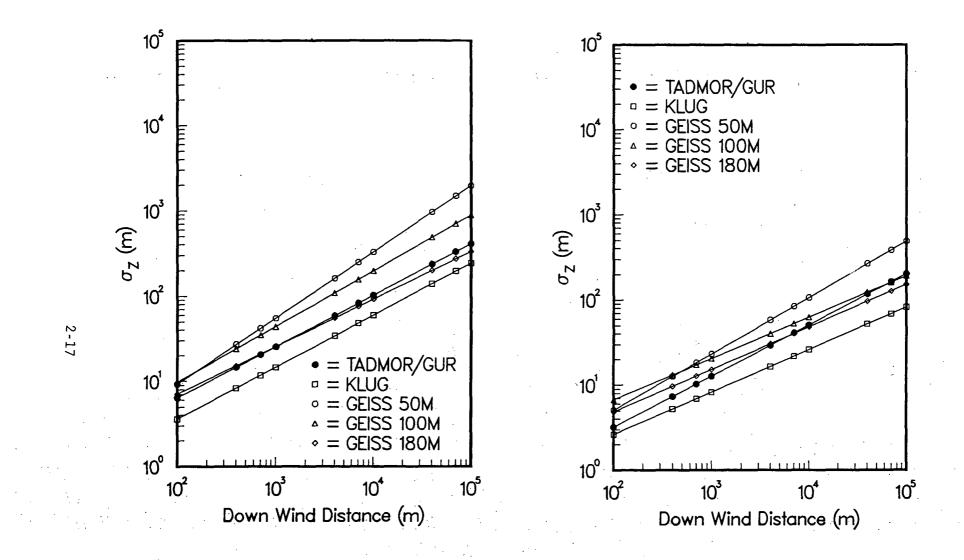


Figure 2-9. Stability Class C:  $\sigma_z$  vs Distance.

Figure 2-10. Stability Class D:  $\sigma_z$  vs Distance.



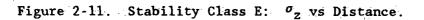


Figure 2-12. Stability Class F:  $\sigma_{\rm v}$  vs Distance.

#### 2.5 Dry Deposition Velocity

#### 2.5.1 Recommendation

The values in Table 2.6 are recommended for the dry deposition velocity (VDEPOS).

<u>Variable</u>	Definition	Value	Range
VDEPOS	Dry deposition velosity (cm/s)	0.3	0.03 - 3.0

Table 2.6. Dry Deposition Velocity

#### 2.5.1 Discussion

In MACCS, particulate matter is removed from plumes during downwind transport by washout and by dry deposition. Dry deposition is modeled using a mass transfer approach. Thus, the flux ( $\omega$ ) of particles to the ground due to dry deposition is calculated as the product of the ground level air concentration of the particles (X) and their dry deposition velocity ( $v_d = VDEPOS$ ), where the dry deposition velocity is an empirical, particle-size-dependent parameter that represents the combined effects of diffusion to, impaction on, and settling onto surfaces:

 $\omega = v_d \chi$ 

The magnitude of  $v_d$  depends on particle size, shape, and density, on atmospheric turbulence (wind speed, stability class), and on surface roughness  $(z_0)$  and friction velocity  $(u_*)$ . Because aerosol size distributions were not developed for NUREG-1150 source terms, a single value for  $v_d$  had to be selected for the NUREG-1150 MACCS calculations and the value selected needed to reasonably represent the mean of the range of values that might actually occur.

This discussion of  $v_d$  is based on the following assumptions:

Rapid agglomeration of small particles before plume release from containment will largely eliminate particles smaller than 0.5  $\mu$ m.

Gravitational settling will deplete the distribution of particles larger than 5  $\mu$ m.

Fission product aerosols will have densities of a few grams per cubic centimeter  $(1 - 4 \text{ g/cm}^2)$ .

The value selected for  $v_d$  should well represent deposition to suburban areas because most population exposures will occur in suburban areas.

Both theoretical [10,29,30] and experimental [28,31,32,3] estimates of the magnitude of  $v_d$  are available. A theoretical model that gives  $v_d$  as a function of particle diameter, particle density, surface roughness, and

friction velocity has been developed by Sehmel and Hodgson [29]. Hobert et al. [30] found that  $v_d = 0.0036$  u\* with little dependence on particle size. The prevailing windspeed (u), its measurement height (z), surface roughness ( $z_0$ ), and friction velocity (u\*) are related as follows [10]:

$$u = (u_{\star}/k) \ln \{(z+z_0)/z_0\}$$
 (2.5.1)

where k = 0.4 is von Karman's constant.

1 10

Table 2.7 presents values of  $z_0$  and  $u_*$  for various surfaces

Surface	Zo	<u>u*</u>	
Lawns	1	40	
Tall Grass, Crops	10 - 15	70	
Countryside	30		
Suburbs	100		
Trees, Forests	20 - 200	90	
Cities	100 - 300		

Table 2.7. Values of  $z_0$  and  $u_*$ 

If  $z_0 = 100$  for suburbs and 5 m/s is a typical windspeed at a measurement height of 10 m, then from Equation 2.5.1  $u_* = 87$  cm/s and  $v_d = 0.0036$   $u_* = 0.0036$  (87 cm/s) = 0.3 cm/s.

Figure 2.13 presents typical results for the Sehmel and Hodgson model for  $v_d$  for  $u_* = 50$  cm/s. The figure shows that if  $z_0 = 10$  cm, an aerosol distribution with a mean size (particle diameter) of 2  $\mu$ m and a mean density of 2 g/cm<sup>2</sup> will have  $v_d = 0.4$  cm/s. Figures from Sehmel [1] similar to this figure give  $v_d = 3.0$  cm/s when  $u_* = 100$  cm/s,  $z_0 = 100$  cm, r = 5  $\mu$ m, and  $\rho = 4$  g/cm<sup>3</sup>; and  $v_d = 0.03$  cm/s when  $u_* = 30$  cm/s,  $z_0 = 3$  cm, r = 0.5  $\mu$ m, and  $\rho = 1$  g/cm<sup>3</sup>.

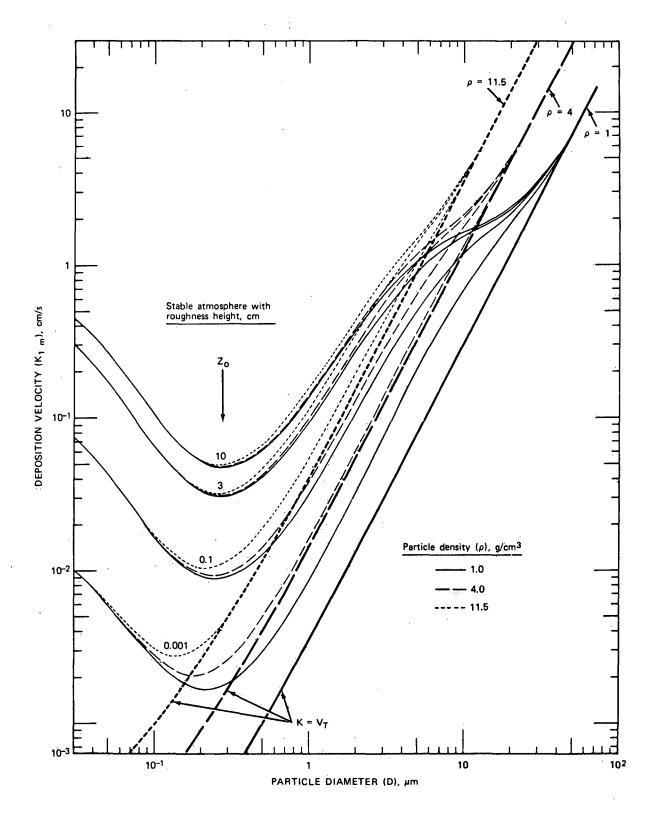


Figure 2.13. Predicted Deposition Velocities at 1 m for  $u^* = 50$  cm/s and Particle Densities of 1.4 and 11.5 g/cm<sup>3</sup>.

Aerosol <u>Composition</u>	Aerosol <u>Size</u> (um)	Deposition Surface	Depositio Range (cm/s)	on Velocity Arithmatic Mean <sup>a</sup> (cm/s)	Reference	
Variousb	1	Grass Asphalt Concrete Flagstones Roofs Bare Soils Trees	0.1 -1 0.01-0.3 0.005-0.2 0.03-0.6 0.1-0.6 0.05-1	0.1 0.5 0.15 0.1 0.3 0.3 0.5	[28] [31] [32]	
Various <sup>c</sup>  	0.1-10 0.003-100	Forest Grass Tall Grass	0.07-0.9 0.03-0.8 0.5-2 0.001-180	0.5 0.4 1.0 0.4 <sup>d</sup>	[3] [10]	
<ul> <li> 0.003-100 0.001-180 0.4<sup>a</sup> [10]</li> <li><sup>a</sup> Arithmatic mean because for any aerosol size distribution mass will be concentrated amoung the larger particles that will have larger dry deposition velocities.</li> <li><sup>b</sup> Aerosols containing Cs-134, Cs-137, I-131, La-140, La-141, Ce-141, Ce-144, Ru-106, Zr-95, and Nb-95.</li> </ul>						

Table 2.8.	Experimental	Values	for	٧d
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d Geometric mean because of the large size range.

Examination of the table suggests that deposition to roads, lawns, and trees will occur with velocities of about 0.1, 0.3, and 0.5 cm/s. Therefore, if a typical residential suburb has roughly equal amounts of surface area provided by roads, lawns, and canopy (leaves on trees and shrubs), then  $v_d = 0.3$ . Therefore, since both theory and experiment suggest that  $v_d =$  about 0.3 cm/s with a range of 0.03 to 3 cm/s, these values are recommended for use in the MACCS NUREG-1150 calculations.

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<sup>&</sup>lt;sup>c</sup> Aerosols containing Cs-137 and I-131.

### 2.6 <u>Wet Deposition Parameters</u>

### 2.6.1 Recommendation

The values in Table 2.9 are recommended for use in characterizing plume washout from rainfall.

Variable	Summary				
CWASH1	Liner coefficient $(s^{-1})$ in expression defining rate constant for plume washout from rainfall (see Eq. 2.3). <u>Base value</u> : 9.5 x $10^{-5}$ . <u>Range</u> : 3 x $10^{-5}$ - 3 x $10^{-4}$ . <u>Sampling Distribution</u> : Log uniform.				
CWASH2	Exponential term in expression defining rate constant for plume washout due to rainfall (see Eq. 2.3). <u>Base value</u> : 0.8. <u>Range</u> : 0.7-0.9. <u>Sampling Distribution</u> : Uniform.				

# Table 2.9. Plume Washout from Rainfall

#### 2.6.2 Rationale

The rain washout model in MACCS is of the form

$$dA/dt = -\lambda A, A(0) = A_0$$
(2.2)

where

- $A(t) = amount (Bq/m^2)$  of a radionuclide in the atmosphere above a region after a period of rainfall of length t (s),
  - $\lambda$  = rate constant (s<sup>-1</sup>) for radionuclide scavenging due to rainfall, and
  - $A_0$  = amount (Bq/m<sup>2</sup>) of a radionuclide in the atmosphere above a region at the start of a period of rainfall (i.e., at t = 0 s).

In turn,  $\lambda$  is assumed to be a function of rainfall intensity. Specifically,  $\lambda$  is defined by

$$\lambda = aR^{b}$$
(2.3)

where R is the rainfall rate (mm/h) and a = CWASH1 and b = CWASH2 are empirically derived constants.

Additional background on this and other characterizations for rainfall scavenging is available elsewhere [9,33-36].

In MACCS, the constants a and b appearing in Equation 2.3 are used to characterize washout from rainfall. Brenk and Vogt [9] gave the following values for a and b,

$$a = 1.2 \times 10^{-4}, b = 0.5$$
 (2.4)

which have been used in past analyses with MACCS. In the NRPB review [33,31], it is concluded that the following ranges characterize values for a and b that are appropriate for use in a reactor accident code that must calculate washout under a variety of conditions:

$$3 \times 10^{-5} \le a \le 3 \times 10^{-4}, \quad 0.7 \le b \le 0.9$$
 (2.5)

For uncertainty studies, the above ranges will be used. Further, the following values at the center of the indicated ranges will be used as base values in the NUREG-1150 consequence analyses:

$$a = 9.5 \times 10^{-5}, b = 0.8$$
 (2.6)

## 2.7 <u>Weathering</u>

### 2.7.1 Recommendation

The values in Table 2.10 are recommended for characterizing the "weathering" of external exposure in MACCS.

Table 2.10. Weathering of Radionuclides on Ground

Variable	Summary
NGWTRM	Number of different weathering processes selected for consideration. <u>Base Value</u> : 2.
GWCOEF1	Fraction of the deposition undergoing weathering process 1. <u>Base</u> <u>Value</u> : 0.5. <u>Range</u> : 0.25 to 0.75. <u>Sampling Distribution</u> : Uniform.
TGWHLF1	Weathering half-life (sec) for fraction of the deposition undergoing weathering process 1. <u>Base Value</u> : $1.6 \times 10^7$ s. <u>Range</u> : 7.8 x 10 <sup>6</sup> to 2.3 x 10 <sup>7</sup> . <u>Sampling Distribution</u> : Uniform.
GWCOEF2	Fraction of the deposition undergoing weathering process 2. <u>Value</u> : 1-A <sub>1</sub> .
TGWHLF2	Weathering half-life (sec) for fraction of the deposition undergoing weathering process 2. <u>Base Value</u> : 2.8 x $10^9$ s. <u>Range</u> : 1.4 x $10^9$ to 4.2 x $10^9$ . <u>Sampling Distribution</u> : Uniform.

# 2.7.2 Rationale

The "weathering" model in MACCS for external exposure to deposited radionuclides is of the form

$$D(t) = D_0 e^{-\lambda t} \sum_{i=1}^{n} \begin{pmatrix} -\lambda_i t \\ A_i e \end{pmatrix}$$
(2.7)

where

- D(t) = dose rate (Sv/s) from a ground-deposited radionuclide at time t (s) after its initial deposition,
  - $D_0$  = dose rate (Sv/s) at the time of initial deposition (i.e., at t = 0 s),
  - $\lambda$  = decay constant (s<sup>-1</sup>) for the radionuclide under consideration,
  - n = number of different weathering processes selected for consideration
     (e.g., short term and long term),

- $A_i$  = fraction of the deposition undergoing weathering process i (subject to the constraint that  $A_1$  + ... +  $A_n$  = 1), and
- $\lambda_i$  = decay constant (s<sup>-1</sup>) for the portion of the external dose subject to weathering process i.

In turn, the  $\lambda_i$  are defined by

$$\lambda_{i} = \ln(2)/\tau_{i} \tag{2.8}$$

where

 $r_i$  = weathering half-life (s), i.e., the time period over which the dose rate subject to weathering process i will decrease by 50%.

When only weathering processes are specified (i.e., NGWTRM = 2), then  $T_1 = TGWHLF1$  and  $T_2 = TGNHLF2$ .

The use of weathering expressions of the form shown in Equation 2.7 for the assessment of time-dependent external exposure in reactor accident consequence assessments derives from a study by Gale et al. [37]. This study was performed in England and used experimental plots involving five different soil types to estimate the time-dependent external exposure from a deposition of 137Cs. The results of this study lead to the following form of the expression in Equation 2.7:

$$D(t) = D_0 e^{-\lambda t} \begin{pmatrix} -\lambda_1 t & -\lambda_2 t \\ A_1 e & +A_2 e \end{pmatrix}$$
(2.9)

where

A<sub>1</sub> = 0.63,  $\lambda_1 = \ln(2)/\tau_1 = \ln(2)/0.61 \text{ yr} = 1.13 \text{ yr}^{-1} = 3.65 \text{ x} 10^{-8} \text{ s},$ A<sub>2</sub> = 0.37, and  $\lambda_2 = \ln(2)/\tau_2 = \ln(2)/92 \text{ yr} = 0.075 \text{ yr}^{-1} = 2.42 \text{ x} 10^{-9} \text{ s}.$ 

The relationship in Equation 2.9 was used to estimate dose reduction in WASH-1400 and has also been used in many other reactor accident consequence assessments.

Until recently, the study by Gale et al. [37] appears to have been the only study providing any direct information of the time-dependent change in external exposure. However, several additional studies have recently been completed and will be briefly discussed. It is likely that more information on time-dependent weathering will become available in the future as the results of the Chernobyl accident are analyzed.

Warming [38,39] has performed several weathering experiments on impermeable surfaces in Denmark. The 1984 study involved the behavior of  $^{86}$ Rb (an analogue for cesium) on concrete and asphalt surfaces. The following results were obtained. For one-year-old concrete, a maximum of 60% of the contamination (i.e.,  $A_1 = 0.6$ ) was weathered away with a half-life of 100 days

(i.e.,  $\tau_1 = 0.27 \text{ yr}$ ). For "young" asphalt, 60% of the contamination (i.e., A<sub>1</sub> = 0.6) is removed with a half-life of 60 days (i.e.,  $\tau_1 = 0.16 \text{ yr}$ ). An "old" concrete surface lost 40% (i.e., A<sub>1</sub> = 0.4) with a half-life of 100 days (i.e.,  $\tau_1 = 0.27 \text{ yr}$ ). An "old" asphalt surface showed no signs of weathering (i.e, A<sub>1</sub> = 0). The 1982 study involved the behavior of  $^{86}$ Rb,  $^{130}$ Ru, and  $^{44}$ Ba on asphalt surfaces. The combined results of this studied estimated A<sub>1</sub> to be 0.29 ± 0.18 and  $\tau_1$  to be 79 ± 55 days = 0.22 ± 0.15 yr.

Karlberg [40] studied the behavior of post-Chernobyl depositions on impermeable surfaces in Sweden. He provides the following summary for his results:

In general, the different nuclides seem to act in a similar way. The average remaining fraction after 12 months is around 0.4 except for paving stones, where the fraction is 0.8. For  $10^{3}$ Ru and  $11^{0}$ Agm on asphalt, the removal also seems to be less than for the other nuclides. A rough estimate of the remaining fraction and half-life times for 'short' weathering gives 0.3 and 104 days, 0.6 and 105 days, and 0.70 and 100 days for paving stones, asphalt, and concrete, respectively.

Thus, for various impermeable surfaces, Karlberg is observing values for A<sub>1</sub> that range from 0.2 to 0.7 and values for  $r_1$  that range from 0.27 yr to 0.38 yr. Further, Figure 2 in Karlberg's paper suggests that the corresponding values above a grass-covered area might be in the area of A<sub>1</sub> = 0.15 and  $r_1 < 60$  days = 0.16 yr. The depositions considered by Karlberg involved rain during and after the passage of the plume and before the first measurements were made.

Jacob et al. [41] studied the behavior of post-Chernobyl depositions in southern Bavaria. They provide the following summary of their results:

Surface activities on paved areas have been determined by in situ measurements in Munich after a deposition of radionuclides from Chernobyl by heavy rain. No significant differences were found between asphalt, concrete, and granite pavements. In the first few days, about 50-70% of the caesium was removed by run-off with the depositing rain and by street cleaning. Barium behaved as cesium, about 80% of the ruthenium and about 90% of the iodine were removed. About 70% of the cesium initially retained disappears from the streets and squares with a half-life of about 80 days due to weathering and street cleaning. Cobbled pavement turned out to retain the radionuclides more effectively. In situ measurements on lawns supported the suggestion that the analytical approximation of Gale et al. under-estimates the external exposures from deposited cesium.

Thus, for impermeable surfaces, their results support a value of  $A_1$  in the area of 0.9 and an effective value of  $\tau_1$ , which is considerably less than 80 days = 0.22 yr when the effects of early runoff are included. Their statement

with respect to Gale's equation is not entirely correct. In their comparison, they reduced the initial ground concentration by 30% because of infiltration effects. Such a reduction is not generally done when Gale's equation is used, and if this reduction had been omitted, use of Gale's equation would have provided an upper, rather than lower, bound on the external exposure rates observed by the authors.

Additional discussion of the time-dependent decrease in external exposure is given in Appendix C of Ostmeyer and Helton [42].

As can be seen from the studies just discussed, there exists considerable variation in the parameters associated with the Equation 2.7. This variation is due to many factors, including type of deposition surface, method of deposition, and the action of weather and other processes subsequent to deposition. Further, the uncertainty in these parameters for use in MACCS is compounded by the fact that consequence calculations involve both wet and dry deposition, weathering over a long time period, and environments that are a mixture of many different types of surfaces. With the preceding in mind, it was decided to pick values and ranges for use in MACCS that are representative of the observed values but do not allow any sort of rigorous statistical interpretation. Specifically, the following values are selected:

Parameter	Value	Range	Distribution
n	2		
Al	0.5	0.25-0.75	uniform
τ	0.5 yr	0.25-0.75	uniform
A2	1-A1		
<i>τ</i> 2	90 yr	45-135	uniform

Table 2.11. MACCS Weathering Values

In picking the preceding values, observed results for permeable surfaces (i.e., grass) were weighted more heavily than those for impermeable surfaces, since permeable surface area typically exceeds impermeable surface area (including in most urban and suburban areas). Because the half-lives of the radionuclides involved in external exposure calculations are relatively short (i.e.,  $\leq 30$  yr), the parameter  $\tau_2$  is not very important.

# 2.8 Runoff and Washoff

# 2.8.1 Summary

Table 2.12 summarizes the base values and ranges for the variables for surface-water contamination.

Table 2.12. Base Value and Range for Variables Associated with Surface-Water Contamination

Variable	Summary			
NUMWP	Number of radionuclides to be considered in the drinking- water pathway. <u>Base Value</u> : 4.			
NAMWPI	Names of radionuclides to be considered in the drinking- water pathway. <u>Selected Radionuclides</u> : <sup>89</sup> Sr, <sup>90</sup> Sr, <sup>134</sup> Cs, 137 <sub>Cs.</sub>			
WSHFR11	Initial radionuclide wash-off fraction for <sup>89</sup> Sr. <u>Base</u> <u>Value</u> : 0.01. <u>Range</u> : 0.002 to 0.02. <u>Sampling Distribution</u> : Log Uniform.			
WSHFR12	Same variable as WSHFRI1 (but for <sup>90</sup> Sr).			
WSHFRI3	Initial radionuclide wash-off fraction for <sup>134</sup> Cs. <u>Base</u> <u>Value</u> : 0.005. <u>Range</u> : 0.001 to 0.01. <u>Sampling</u> <u>Distribution</u> : Log Uniform.			
WSHFRI4	Same variable as WSHFRI3 (but for $137$ Cs).			
WSHRTA1	Rate constant (yr <sup>-1</sup> ) for long-term wash-off for <sup>89</sup> Sr. <u>Base</u> <u>Value</u> : 0.004. <u>Range</u> : 0.0008 to 0.008. <u>Sampling</u> <u>Distribution</u> : Log Uniform.			
WSHRTA2	Same variable as WSHRTAl (but for <sup>90</sup> Sr).			
WSHRTA3	Rate constant (yr <sup>-1</sup> ) for long-term wash-off for <sup>134</sup> Cs. <u>Base Value</u> : 0.001. <u>Range</u> : 0.0002 to 0.002. <u>Sampling</u> <u>Distribution</u> : Log Uniform.			
WSHRTA4	Same variable as WSHRTA3 (but for $137_{Cs}$ ).			

Variable	Summary
WINGF1	Water ingestion factor for <sup>89</sup> Sr. <u>For Rivers</u> : Base value: 5 x 10 <sup>-6</sup> . Range: 1 x 10 <sup>-6</sup> to 1 x 10 <sup>-5</sup> . Sampling Distribution: Log Uniform. <u>For Large Lakes</u> : Base Value: 2 x 10 <sup>-7</sup> . Range: 1 x 10 <sup>-7</sup> to 1 x 10 <sup>-6</sup> . Sampling Distribution: Log Uniform.
WINGF2	Water ingestion factor for <sup>90</sup> Sr. <u>For Rivers</u> : Same variable as WINGF1. <u>For Large Lakes</u> : Base Value: 2 x 10 <sup>-5</sup> . Range: 1 x 10 <sup>-5</sup> to 1 x 10 <sup>-4</sup> . Sampling Distribution: Log Uniform.
WINGF3	Water ingestion factor $134$ Cs. For Rivers: Base Value: 5 x 10 <sup>-6</sup> . Range: 1 x 10 <sup>-6</sup> to 1 x 10 <sup>-5</sup> . Sampling Distribution: Log Uniform. For Large Lakes: Base value: 2 x 10 <sup>-6</sup> . Range: 1 x 10 <sup>-6</sup> to 1 x 10 <sup>-5</sup> . Sampling Distribution: Log Uniform.
WINGF4	Water ingestion factor for <sup>137</sup> Cs. <u>For Rivers</u> : Same variable as WINGF3. <u>For Large Lakes</u> : Base Value: 4 x 10 <sup>-6</sup> Range: 2 x 10 <sup>-6</sup> to 2 x 10 <sup>-5</sup> . Take as twice WINGF3 for lakes.

# 2.8.2 Rationale

The radionuclide wash-off model in MACCS is based on the relationship

$$dx/dt = -(\lambda + \lambda_{\rm b}) x, x(0) = (1 - \lambda_{\rm a}) x_0$$
 (2.10)

where

- x(t) = amount (bq) of a radionuclide on land surfaces at time t (yr) after an initial deposition at time t = 0,
  - $\lambda = \text{decay constant (yr}^{-1})$  for radionuclide,
  - $\lambda_a$  = fraction of initial radionuclide deposition that moves from land surfaces to surface-water bodies in a short time period after deposition,
  - $\lambda_b$  = rate constant (yr<sup>-1</sup>) for the long-term movement of the radionuclide from land surfaces to surface-water bodies, and
  - $x_0$  = initial radionuclide deposition (bq) on land surfaces.

The quantities  $\lambda_a$  and  $\lambda_b$  are the MACCS input variables WSHFRI and WSHRTA. The quantity  $x_0$  is defined by

$$x_0 = \text{TOTDEP} * \text{FRACLD}$$
 (2.11)

where

- TOTDEP = total deposition (bq) predicted by MACCS for the radionuclide in the region under consideration and
- FRACLD = fraction of region under consideration that is land; the remaining fraction l-FRACLD is assumed to be covered by surface-water bodies.

A single value can be used for FRACLD in a MACCS analysis or FRACLD can be specified for individual grid elements through the use of a Site Data File.

The amount of radionuclide moving from land surfaces to surface-water bodies is given by

$$D_1 = \lambda_a x_0 + \int_0^\infty \lambda_b x(t) dt$$

$$= (\lambda_a \ \lambda + \lambda_b) \ x_0 / (\lambda + \lambda_b)$$
(2.12)

Further, the total deposition directly onto surface-water bodies is given by

$$D_2 = TOTDEP (1 - FRACLD)$$
(2.13)

Thus, the total amount of a radionuclide entering a surface-water system is given by

$$DTOT = D_1 + D_2$$
 (2.14)

The quantity in Equation 2.14 is then used to determine radionuclide consumption due to water ingestion.

For a given surface-water system, it is assumed that a constant fraction of a radionuclide entering the system will be ultimately consumed via the drinking-water pathway. This fraction is defined by the ratio

$$WINGF = PTOT/DTOT$$
(2.15)

where PTOT is the total amount (bq) of radionuclide consumed by the population via the surface-water pathway and DTOT is the total amount of radionuclide entering the surface-water system under consideration (see Equation 2.14).

Some type of analysis/modeling is required to define WINGF. This effort could range from the use of empirical data or simple compartment models to the development/application of quite sophisticated models for surface-water systems and their associated public water supply systems. However, in deciding on the amount of effort to invest in determining WINGF, it should be kept in mind that the surface-water pathway is probably a small contributor to the total cancer risk from chronic exposure pathways [12,43].

We are interested in values for  $\lambda_a = \text{WSHFRI}$ ,  $\lambda_b = \text{WSHRTA}$ , and WINGF. The quantities  $\lambda_a$  and  $\lambda_b$  are considered first. Table 2.13, which is taken from Helton et al. [12], provides a number of observed values for these quantities. Additional values are given in Table 2.14.

Helton et al. [12] concluded that only four radionuclides,  $^{89}$ Sr,  $^{90}$ Sr,  $^{134}$ Cs, and  $^{137}$ Cs, are needed to treat contamination of surface-water bodies. Based on the values for WSHFRI ( $\lambda_a$ ) and WSHRTA ( $\lambda_b$ ) in Tables 2.14 and 2.15 the following values are recommended for these variables and those nuclides:

<u>Isotope</u>	WSHFRI (Range)	WSHRTA (Range)
<sup>89</sup> Sr	0.01 (0.002 to 0.02)	0.004 (0.0008 to 0.008)
90 <sub>Sr</sub>	0.01 (0.002 to 0.02)	0.004 (0.0008 to 0.008)
134 <sub>Cs</sub>	0.005 (0.001 to 0.01)	0.001 (0.0002 to 0.002)
137 <sub>Cs</sub>	0.005 (0.001 to 0.01)	0.001 (0.0002 to 0.002)

Table 2.13. Values for WSHFRI ( $\lambda_a$ ) and WSRTH ( $\lambda_b$ )

\* Considerable subjective judgment was used in selecting these values and ranges.

The development of values for WINGF is now considered. Helton et al. [12] present an exploratory study of the health effects of radionuclide wash-off into surface-water bodies. In that study of wash-off into river systems, WINGF is in effect defined by

(2.16)

where

- WC = individual water consumption (l/yr-ind),
- POP = number of individuals obtaining drinking water from the river under consideration (ind), and
  - D = river discharge (l/yr)

Two river systems were considered in Reference [12]: the lower Mississippi and Rhein-Meuse. Values for WINGF are now calculated using Equation 2.16 and parameter values taken from Reference [12].

Table 2.14.	Removal Rates	for Fallout	: Radionuclides	Determined	on a	Regional
•	Basis (Refere	nce[12], Tab	ole 1).			

Ref.	Nuclide	<u>100 λa</u>	<u>100 λb</u>	Location	Comment
Straub et al. [44]	<sup>90</sup> Sr B-emitters <sup>90</sup> Sr	1.7* 1.6 3.9-12.2		Continental United States Continental United States Five watersheds in Ohio Valley	Three month period Nine month period Three month period
	deposition,				l D are the removal in suface credit is taken for removal of
Miyake and Tsubota [45]	90 <sub>Sr</sub> 137 <sub>Cs</sub>	1.7	0.7-3.3	Ten watersheds in Japan	Mean value for $90_{Sr}$ is 1.5. Value for $137_{CS}$ is estimated as that due to direct deposition on water bodies.
Yamagata et al. [46]	90 <sub>Sr</sub> 137 <sub>Cs</sub>	7.2 1.3	0.31 0.06	Japan	1 month period for $\lambda_a$
Jacobi et al. [47]	B~emitters	0.20-1.05	0.12-0.97	Twenty watersheds in West Germany	1 month period for $\lambda_a$ . Extensive Study.
Jordan et al. [48,49]	90 <sub>Sr</sub>		0.036	Tropical rain forest, Puerto Rico	Derives $\lambda_b$ for stable Sr and uses to predict behavior of 90 <sub>Sr</sub> .
[50]	<sup>90</sup> Sr	roportimatod	0.2-2*	Three watersheds in Japan	D and the entrol mediaturalide
*The values for	λ <sub>b</sub> may be ov ace water and		as $\lambda_b$ is de	Japan	D are the annual radionuclide
<pre>[50] *The values for removal to surf</pre>	$\lambda_{b}$ may be ov		as $\lambda_b$ is de	Japan fined by $\lambda_{b}^{=} \mathbb{R}/\mathbb{D},$ where R and	D are the annual radionuclide
<pre>[50] *The values for removal to surf Miyake et al. [51] Kamada et al.</pre>	λ <sub>b</sub> may be ov ace water and		as λ <sub>b</sub> is de mulated depo	Japan fined by λ <sub>b</sub> =R/D, where R and sition, respectively.	D are the annual radionuclide
<pre>[50] *The values for removal to surf Miyake et al. [51] Kamada et al. [52] Menzel</pre>	λ <sub>b</sub> may be ov ace water and 239 <sub>Pu</sub>		as λ <sub>b</sub> is de mulated depo 0.12	Japan fined by $\lambda_b = R/D$ , where R and sition, respectively. Japan Four watersheds in	Two month period for
<pre>[50] *The values for removal to surf Miyake et al. [51] Kamada et al. [52] Menzel [53] Simpson et al.</pre>	$\lambda_{\rm b}$ may be ov ace water and $239_{\rm Pu}$ $90_{\rm Sr}$	l total accu	as λ <sub>b</sub> is de mulated depo 0.12 0.2-2	Japan fined by λ <sub>b</sub> =R/D, where R and sition, respectively. Japan Four watersheds in Japan Eight regions in	Two month period for
<pre>(50) *The values for removal to surf Miyake et al. [51] Kamada et al. [52] Menzel [53] Simpson et al. [54] Carlsson</pre>	$\lambda_{\rm b}$ may be ov ace water and $239_{\rm Pu}$ $90_{\rm Sr}$ $90_{\rm Sr}$	l total accu	as λ <sub>b</sub> is de mulated depo 0.12 0.2-2 0.17-0.75	Japan fined by λ <sub>b</sub> =R/D, where R and sition, respectively. Japan Four watersheds in Japan Eight regions in United States Hudson River	Two month period for
<pre>[50] *The values for removal to surf Miyake et al. [51] Kamada et al. [52] Menzel [53] Simpson et al. [54] Carlsson [55] Sprugel and Bartelt</pre>	$\lambda_{\rm b}$ may be ov ace water and $239_{\rm Pu}$ $90_{\rm Sr}$ $90_{\rm Sr}$ $137_{\rm Cs}$	1 total accu	as $\lambda_b$ is demulated depo 0.12 0.2-2 0.17-0.75 0.1	Japan fined by λ <sub>b</sub> =R/D, where R and sition, respectively. Japan Four watersheds in Japan Eight regions in United States Hudson River watershed Small watershed in	Two month period for
<pre>(50) *The values for removal to surf Miyake et al. [51] Kamada et al. [52] Menzel [53] Simpson et al. [54] Carlsson [55] Sprugel and Bartelt [56] Aarkrog</pre>	$\lambda_{\rm b}$ may be ov ace water and $239_{\rm Pu}$ $90_{\rm Sr}$ $90_{\rm Sr}$ $137_{\rm Cs}$ $137_{\rm Cs}$	1 total accu	as λ <sub>b</sub> is de mulated depo 0.12 0.2-2 0.17-0.75 0.1	Japan fined by λ <sub>b</sub> =R/D, where R and sition, respectively. Japan Four watersheds in Japan Eight regions in United States Hudson River watershed Small watershed in Sweden	Two month period for
[50] *The values for	$λ_b$ may be ov ace water and $239_{Pu}$ $90_{Sr}$ $90_{Sr}$ $137_{Cs}$ $137_{Cs}$ $239,240_{Pu}$	1 total accu 0.59-2.17 1.9	as λ <sub>b</sub> is de mulated depo 0.12 0.2-2 0.17-0.75 0.1 0.56	Japan ofined by $\lambda_b=R/D$ , where R and osition, respectively. Japan Four watersheds in Japan Eight regions in United States Hudson River watershed Small watershed in Sweden Ohio	Two month period for $\lambda_a$ . Extensive investigation

Ref.	Nuclide	100 λa	100 λb	Comment
[59,60]	137 <sub>Cs</sub> 131 <sub>I,</sub> 132 <sub>Te,</sub> 103 <sub>Ru</sub>	1 4-10	• •	Northern Switzerland and southern Germany in first few weeks following depositions from the Chernobyl accident
[61]	137 <sub>Cs</sub> 239 <sub>Pu,</sub> 240 <sub>Pu</sub> 241 <sub>Am</sub>		0.02 0.02 0.02	Fallout in the Columbia River basin
[62]	7 Be 137 <sub>Cs</sub> 210 <sub>Pb</sub>	0.6-2.3	0.1 0.1	Alpine Rhone watershed in Switzerland. Suggests that value of $\lambda_a$ for <sup>7</sup> Be may also be appropriate for Cs and Pb.
[63]	239 <sub>Pu</sub> , 240 <sub>Pu</sub>		0.4	Mississippi drainage basin
[64]	210 <sub>Pb</sub>	<u> </u>	0.05	Susquehanna river system
[65]	Pu		0.002-0.08	Modeling study for the continental United States based on the universal soil loss equations

Table 2.15. Additional Removal Rates for Radionuclides Determined on a Regional Basis

## Mississippi for Sr

WINGF = (0.87) (370 
$$\ell/yr$$
-ind) (2.9E6 ind)/(5.7 x 10<sup>14</sup>  $\ell/yr$ )  
= 1.6 x 10<sup>-6</sup> (2.17)

### <u>Mississippi for Cs</u>

WINGF = 
$$(0.53)$$
 (370 *l*/yr-ind) (2.9E6 ind)/(5.7 x 10<sup>14</sup> *l*/yr)  
= 1.0 x 10<sup>-6</sup> (2.18)

Rhein-Meuse for Sr

WINGF = (1.0) (440 
$$l/yr$$
-ind) (1.3E7 ind)/(8.5 x 10<sup>13</sup>  $l/yr$ )  
= 6.7 x 10<sup>-5</sup> (2.19)

Rhein-Meuse for Cs

WINGF = (0.1) (440 
$$l/yr$$
-ind) (1.3 x 10<sup>7</sup> ind)/(8.5 x 10<sup>13</sup>  $l/yr$ )  
= 6.7 x 10<sup>-6</sup> (2.20)

Helton et al. [12] also considered the effects of a deposition onto Lake Michigan. The model used in this part of the analysis is equivalent to defining WINGF by

WINGF = 
$$(\int_{0}^{\infty} e^{-\lambda t} dt/V) * WT * WC * POP$$
  
=  $\frac{WT * WC * POP}{\lambda * V}$  (2.21)

where V is the volume (l) of the lake,  $\lambda$  is the rate constant (yr<sup>-1</sup>) for removal from the lake (including radioactive decay, sedimentation, and outflow), and WT, WC, and POP are the same as in Equation 2.16. In turn,  $\lambda$  is defined by

$$\lambda = \ln(2) / \text{HL} \tag{2.22}$$

where HL is the effective half-life (yr) for the radionuclide under consideration. When Equation 2.21 and Equation 2.23 are combined, the following relationship is obtained:

$$WINGF = \frac{HL * WT * WC * POP}{ln(2) * V}$$
(2.23)

Equation 2.14 and the data in Helton et al. [12] can now be used to estimate WINGF for a release to Lake Michigan.

Lake Michigan for <sup>89</sup>Sr

WINGF = 
$$\frac{(0.14 \text{ yr}) (1.0) (370 \ \ell/\text{yr-ind}) (1.0 \text{ x } 107 \text{ ind})}{\ln(2) * (4.87 \text{ x } 10^{15} \ \ell)}$$
  
= 1.7 x 10<sup>-7</sup> (2.24)

:

Lake Michigan for <sup>90</sup>Sr

WINGF = 
$$\frac{(15.4 \text{ yr}) (1.0) (370 \ l/\text{yr-ind}) (1.1 \times 107 \text{ ind})}{\ln(2) \times (4.8 \times 10^{15} \ l)}$$
  
= 1.9 x 10<sup>-5</sup> (2.25)

Lake Michigan for 134Cs

WINGF = 
$$\frac{(0.13 \text{ yr}) (1.0) (370 \ l/\text{yr-ind}) (1.1 \text{ x } 107 \text{ ind})}{\ln(2) * (4.87 \text{ x } 10^{-15} \ l)}$$
  
= 1.6 x 10<sup>-6</sup> (2.26)

Lake Michigan for 137Cs

WINGF = 
$$\frac{(3.5 \text{ yr}) (1.0) (370 \ l/\text{yr-ind}) (1.1 \text{ x } 107 \text{ ind})}{\ln(2) * (4.87 \text{ x } 10^{15} \ l)}$$
  
= 4.2 x 10<sup>-5</sup> (2.27)

Two additional, very crude calculations are now given for WINGF. The first uses Equation 2.16 and data for the entire United States. Specifically, the following data are used:

WT = 0.87 for Sr, 0.53 for Cs (same as used in Helton et al.[12],

WC =  $370 \ l/yr$ -ind,

- POP =  $2.4 \times 10^8$  ind  $* 0.718 = 1.7 \times 10^8$  ind, where  $2.4 \times 10^8$  ind is the population of the United States (<u>Statistical Abstract of the</u> <u>United States 1988</u>) and 0.718 is an approximation of the fraction of the total United States population that receives its water from surface-water bodies (Ref. [66], Table 6-39, p. 345), and
  - D =  $(1,500 \times 10^{6} \text{ acre ft/yr})$   $(1.234 \times 10^{6} \text{ l/acre ft}) = 1.9 \times 10^{15}$ l/yr, where 1,500 x 10<sup>6</sup> is the annual discharge of rivers in the conterminous United States (Ref. [66], Table 2-2, p. 61).

Then the following approximations to WINGF are obtained:

. .

WINGF = (0.87) (370 
$$l/yr$$
-ind) (1.7 x 10<sup>8</sup> ind)/(1.9 x 10<sup>15</sup>  $l/yr$ )  
= 2.9 x 10<sup>-5</sup> (2.28)

<u>Rivers in Conterminous United States for Cs</u>

WINGF = 
$$(0.53)$$
 (370 *l*/yr-ind) (1.7 x 10<sup>8</sup> ind)/(1.9 x 10<sup>15</sup> *l*/yr)  
= 1.8 x 10<sup>-5</sup> (2.29)

The second calculation uses Equation 2.2 and the data for the entire United States. Specifically, the following variable values are assumed:

- WT = 1 for Sr and Cs, WC =  $370 \ \ell/\text{yr-ind}$ , POP =  $1.7 \ x \ 10^8 \text{ ind}$ , V =  $4,500 \ \text{mi}^3 \ x \ 3.38 \ x \ 10^6 \ \text{acre ft/mi}^{-3} \ x \ 1.234 \ x \ 10^6 \ \ell/\text{acre ft}$ =  $1.9 \ x \ 10^{16} \ \ell$ , where  $4500 \ \text{mi}^3$  is the volume of freshwater lakes in the conterminous United States (Ref. [66], Table 2-2, p. 61), and
  - HL = 0.14 yr for <sup>89</sup>Sr, 15.4 yr for <sup>90</sup>Sr, 1.3 yr for <sup>134</sup>Cs, 3.5 yr for <sup>137</sup>Cs, where these are the values obtained in Helton et al. [12] for Lake Michigan (values for smaller and/or other lakes could be quite different; e.g., see Santschi et al. [59].

Then, the following approximations to WINGF are obtained:

Lakes in Conterminous United States for <sup>89</sup>Sr

WINGF = 
$$\frac{(0.14 \text{ yr}) (1.0) (370 \ell/\text{yr-ind}) (1.7 \times 108) \text{ ind})}{\ell n(2) (1.9 \times 10^{16} \ell)}$$
  
= 6.7 x 10<sup>-7</sup> (2.30)

Lakes in Conterminous United States for 90Sr

WINGF = 
$$\frac{(15.4 \text{ yr}) (1.0) (370 \ l/\text{yr-ind}) (1.7 \text{ x } 108 \text{ ind})}{ln(2) (1.9 \text{ x } 10^{16} \ l)}$$
  
= 7.4 x 10<sup>-5</sup> (2.31)

Lakes in Conterminous United States for 134Cs

WINGF = 
$$\frac{(1.3 \text{ yr}) (1.0) (370 \ \ell/\text{yr-ind}) (1.7 \text{ x } 108 \text{ ind})}{\ln(2) (1.9 \text{ x } 10^{16} \ \ell)}$$
  
= 6.2 x 10<sup>-6</sup> (2.32)

Lakes in Conterminous United States for 137Cs

WINGF = 
$$\frac{(3.5 \text{ yr}) (1.0) (370 \ l/\text{yr-ind}) (1.1 \times 107 \text{ ind})}{ln(2) (1.9 \times 10^{16} \ l)}$$
  
= 1.7 x 10<sup>-5</sup> (2.33)

Several simplistic calculations for WINGF have been given. These calculations are intended to provide only a ballpark estimate of the value of WINGF. The recommendations in Table 2.16 for WINGF are suggested for preliminary assessments of the drinking water pathway:

<u>Isotope</u>	River (Range)	Lake (Range)
89 <sub>Sr</sub>	$5 \times 10^{-6}$ (1 x 10 <sup>-6</sup> - 1 x 10 <sup>-5</sup> )	$2 \times 10^{-7}$ (1 x 10 <sup>-7</sup> - 1 x 10 <sup>-6</sup> )
90 <sub>Sr</sub>	$5 \times 10^{-6}$ (1 x $10^{-6}$ - 1 x $10^{-5}$ )	$2 \times 10^{-5}$ (1 x $10^{-5}$ - 1 x $10^{-4}$ )
134 <sub>Cs</sub>	$5 \times 10^{-6}$ (1 x 10 <sup>-6</sup> - 1 x 10 <sup>-5</sup> )	$2 \times 10^{-6}$ (1 x 10 <sup>-6</sup> - 1 x 10 <sup>-5</sup> )
137 <sub>Cs</sub>	$5 \times 10^{-6} (1 \times 10^{-6} - 1 \times 10^{-5})$	$4 \times 10^{-6} (2 \times 10^{-6} - 2 \times 10^{-5})$

The values recommended here for "River" systems are somewhat lower than the screening estimates for WINGF because those calculations probably underestimated effects due to binding to sediments. The values for "Lake" are those obtained for Lake Michigan and they should be used only for a very large lake. The ranges are subjective estimates and are intended to be sampled with a log-uniform distribution.

<u>Note</u>: Although it was obtained too late to use in the development of the parameters presented here, a useful source of information on water use in the United States is <u>Estimated Use of Water in the United States in</u> <u>1985</u> by W. B. Solley, C. F. Merk, and R. R. Pierce (USGS Circular 1004, 1988).

# 2.9 <u>Resuspension</u>

# 2.9.1 Summary

Table 2.17 summarizes the base values and ranges for the variables for resuspension.

Table 2.17 Base Values and Ranges for Resuspension Variables

Variable	Summary
NRWTRM	Number of resuspension processes under consideration. <u>Base</u> <u>Value</u> : 3.
RWCOEF1	Resuspension coefficient for short term resuspension (m <sup>-1</sup> ). <u>Base</u> <u>Value</u> : 10 <sup>-5</sup> . <u>Range</u> : 10 <sup>-6</sup> -10 <sup>-4</sup> . <u>Sampling Distribution</u> : Log Uniform. Rank correlation of 1 with RWCOEF2 and RWCOEF3; rank correlation of -0.75 with TRWHLH1, TRWHLH2 and TRWHLH3.
RWCOEF2	Resuspension coefficient for intermediate term resuspension (m <sup>-1</sup> ). <u>Base Value</u> : 10 <sup>-7</sup> . <u>Range</u> : 10 <sup>-8</sup> -10 <sup>-6</sup> . <u>Sampling</u> <u>Distribution</u> : Log uniform. Correlation same as for RWCOEF1.
RWCOEF3	Resuspension coefficient for long term resuspension (m <sup>-1</sup> ). <u>Base</u> <u>Value</u> : 10 <sup>-9</sup> . <u>Range</u> : 10 <sup>-8</sup> -10 <sup>-10</sup> . <u>Sampling Distribution</u> : Log uniform. Correlations same as for RWCOEF1.
TRWHLF1	Half-life (s) for resuspension coefficient RWCOEF1. <u>Base Value</u> : 1.6x10 <sup>7</sup> (~6 mn). <u>Range</u> : 2.6x10 <sup>6</sup> -3.1x10 <sup>7</sup> (~ 1-12 mn). <u>Sampling</u> <u>Distribution</u> : Log uniform. Rank correlation of 1 with TRWHLF2 and TRWHLF3; rank correlation of -0.75 with RWCOEF1, RWCOEF2 and RWCOEF3.
TRWHLF2	Half-life (s) for resuspension coefficient RWCOEF2. <u>Base Value</u> : 1.6x10 <sup>8</sup> (~ 5 yr). <u>Range</u> : 3.1x10 <sup>7</sup> -3.1x10 <sup>8</sup> (~ 1-10 yr). <u>Sampling</u> <u>Distribution</u> : Log uniform. Correlations same as for TRWHLF1.
TRWHLF3	Half-life (s) for resuspension coefficient RWCOEF3. <u>Base Value</u> : 1.6x10 <sup>9</sup> (~50 yr). <u>Range</u> : 3.1x10 <sup>8</sup> -3.1x10 <sup>9</sup> (~10-100 yr). <u>Sampling Distribution</u> : Log uniform. Correlations same as for TRWHLF1.
	Comment: Since RWCOEF1, RWCOEF2, and RWCOEF3 are assumed to have a rank correlation of 1, a single variable can be sampled as a surrogate for all three. The same applies to TRWHLF1, TRWHLF2, and TRWHLF3. Thus, it is necessary to sample only two variables to implement these six variables.

# 2.9.2 Rationale

The resuspension model in MACCS is based on the resuspension factor approach. The resuspension factor  $K(t)(m^{-1})$  is defined by

$$K(t) = a(t)/s(t)$$
 (2.34)

where

- a(t) = air concentration (Bq/m<sup>3</sup>) of resuspended activity at time t after an initial deposition and
- s(t) = initial surface deposition (Bq/m<sup>2</sup>) corrected for radioactive decay.

Additional discussion is available in a number of reviews [10,42,67,68,69].

In MACCS, K(t) is defined by

$$K(t) = \sum_{i=1}^{n} K_i \exp(-\lambda_i t)$$
(2.35)

where

- n = NRWTRM = number of resuspension processes under consideration (e.g., short-term, intermediate-term, and long-term resuspension),
- $K_i = RWCOEF(i) = resuspension factor (m<sup>-1</sup>) for the i<sup>th</sup> resuspension process,$ and
- $\lambda_i = ln(2)/r_i$  = rate constant (s<sup>-1</sup>) for the time-dependent reduction in resuspension factor K<sub>i</sub>

where

 $r_i$  = TRWHLF(i) = resuspension half-life (s) (i.e., the time period over which the observed air concentration will decrease by 50%).

An excellent review of the data on resuspension is given by Sehmel [10]. As indicated by both the data in this review and statements by the author, there is great uncertainty in characterizing resuspension. For the resuspension model in MACCS, the data in Tables 12.7 and 12.9 of Sehmel will be used to characterize resuspension factors (i.e., the K<sub>i</sub> in Equation 2.35). Further, the data in Table 12.8 of Sehmel will be used for guidance with respect to the rate constant  $\lambda_i$ .

Three time periods (i.e., n=3) will be considered in the definition of the resuspension factors: short term (i.e.,  $K_1$ ), intermediate term (i.e.,  $K_2$ ), and long term (i.e.,  $K_3$ ). The short-term and intermediate-term resuspension is assumed to correspond to the larger and intermediate sized factors in Sehmel, Table 12.9. The long-term resuspension corresponds to the values in Sehmel, Table 12.7 and the smaller to values in Sehmel, Table 12.9. Short-,

intermediate-, and long-term resuspension is intended to correspond respectively to resuspension which takes place over a few months, a few years, and a few tens of years after deposition.

Table 2.18 shows the values selected for the K<sub>i</sub> and the  $\tau_i$ .

<u>Variable</u>	Base Value	Range	Comment
к1	10-5	10-6 - 10-4	
$r_1$	6 mon	1 - 12 mn	$1 \text{ mon} = 2.6 \text{ x} 10^6 \text{ s}$
к2	10-7	10-8 - 10-6	
τ2	5 yr	1-10 yr	$1 \text{ yr} = 3.1 \text{ x} 10^7 \text{ s}$
K <sub>3</sub>	10-9	10-10 - 10-8	
<i>t</i> 3	50 yr	10-100 yr	$1 \text{ yr} = 3.1 \text{ x} 10^7 \text{ s}$

Table 2.18. Values for Ki and	Table	2.18.	Values	for	Ki	and	τi
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Although the values in Table 2.18 are not inconsistent with the available data, it must be recognized that these quantities are very uncertain.

Changes in environmental conditions are expected to have inverse effects on corresponding values of  $K_i$  and i, but very similar effects on the set of  $K_i$  values, and also on the set of i values. Thus, for sampling purposes, all values of  $K_i$  should be assumed to be strongly correlated (e.g., rank correlation of 1), all values of i should be assumed to be assumed to be strongly correlated (e.g., rank correlation of 1), and corresponding values of  $K_i$  and  $r_i$  should be assumed to have a moderately strong, negative rank correlation (e.g., -0.75).

For comparison, values for  $K_i$  and  $\tau_i$  used in the Reactor Safety Study (i.e., WASH-1400) and suggested in the review by Lassey [67] are listed in Tables 2.19 and 2.20.

	Values in Reactor Safety Study [11]	Table 2.20.	Values in Lassey [67]
<u>Variable</u>	Value	<u>Variable</u>	Value
Κ <sub>1</sub> τ1 Κ2 τ2	10-5 1 yr 10-9 no decrease with time	K1 71 K2 72 K3 73	9x10-5 1.4 mn 1x10-5 1 yr 10-9 no decrease with time

#### REFERENCES

- [1] D. J. Hall, and R. A. Waters, <u>Further Experiments on a Buoyant Emission</u> <u>from a Building</u>, Warren Spring Laboratory, Stevenage, England, LR 567 (PA), 1986.
- [2] G. A. Briggs, <u>Plume Rise Predictions</u>, Environmental Research Laboratories, U.S. Department of Commerce, National Oceanic and Atmospheric Administration, 1975.
- S. R. Hanna, G. A. Briggs, and R. P. Hozkers, <u>Handbook on Atmospheric</u> <u>Diffusion</u>, DOE/TIC-27601, U.S. Department of Energy, Washington, DC, 1982. (a.) p. 33, (b) p. 375.
- [4] U.S. Nuclear Regulatory Commission, <u>PRA Procedures Guide</u>, Vol. II, Chapter 9, "Environmental Transport and Consequence Analysis," NUREG/CR-2300, U.S. Nuclear Regulatory Commission, Washington, DC, 1983.
- [5] CEC, <u>Radiation Protection: Methods for Assessing the Off-Site</u> <u>Radiological Consequences of Nuclear Accidents</u>, EUR 10243 en, Commission of the European Communities, Luxemburg, 1986.
- [6] S. K. Koa, "Theories of Atmospheric Transport and Diffusion," <u>Atmospheric Sciences and Power Production</u>, ed. D. Randerson, U.S. Department of Energy, Washington, DC, DOE/TIC-27601, 1984.
- [7] G. C. Holzworth, <u>Mixing Heights, Wind Speeds, and Potential for Urban</u> <u>Air Pollution Throughout the Contiguous United States</u>, AP-101, U.S. Environmental Protection Agency, Research Triangle Park, NC, 1972.
- [8] D. B. Turner, <u>Workbook of Atmospheric Dispersion Estimates</u>, PSH-999-AP-26, U. S. Department of Health, Education, and Welfare, Washington, DC, 1969.
- [9] H. D. Brenk and K. J. Vogt, "The Calculation of Wet Deposition from Radioactive Plumes," <u>Nuclear Safety</u>, Vol. 22, pp. 362-371 (1981).
- [10] G. A. Sehmel, "Deposition and Resuspension," <u>Atmospheric Science and</u> <u>Power Production</u>, ed. D. Randerson, U.S. Department of Energy, Washington, DC, DOE/TIC-27601, 1984.
- U.S. Nuclear Regulatory Commission, <u>Reactor Safety Study</u>, Appendix VI, "Calculation of Reactor Accident Consequences," WASH-1400, Washington, DC, 1975.
- [12] J. C. Helton, A. B. Muller, and A. Bayer, "Contamination of Surfacewater Bodies after Reactor Accidents by the Erosion of Atmospherically Deposited Radionuclides," <u>Health Physics</u>, Vol. 48, pp. 757-771 (1985).
- [13] R. P. Hosker, "Flow and Diffusion Near Obstacles," in <u>Atmospheric Science and Power Production</u>, ed. D. Randerson, DOE/TIC-27601, U. S. Department of Energy, Washington, DC, 1984, pp. 302, 241-326. (a.) p. 302, (b.) pp. 241-326.

- [14] C. D. Leigh et al., <u>Analyses of Plume Formation</u>, <u>Aerosol Agglomeration</u> <u>and Rainout Following Containment Failure</u>, NUREG/CR-4222, SAND84-2581, Sandia National Laboratories, Albuquerque, NM.
- [15] Virginia Electric and Power Co., <u>Final Safety Analysis Report:</u> Surry <u>Nuclear Station</u>.
- [16] Tennessee Valley Authority, <u>Final Safety Analysis Report, Sequoyah</u> <u>Nuclear Plant</u>.
- [17] Philadelphia Electric Co., <u>Final Safety Analysis Report: Peach Bottom</u> <u>Atomic Power Station, Units 2 & 3</u>.
- [18] Mississippi Power and Light Co., <u>Final Safety Analysis Report: Grand</u> <u>Gulf Nuclear Station, Units 1 and 2</u>.
- [19] Briggs, G. "Lift Off of Buoyant Gas Initially on the Ground," ADTL Contribution File No. 87, Air Resources Atmospheric Turbulence and Diffusion Laboratory NOAA, Oak Ridge, TN, Nov. 1973.
- [20] U.S. Nuclear Regulatory Commission, <u>Onsite Meteorological Programs</u> <u>Safety Guide 23</u>, <u>Regulatory Guide 1.23</u>; Washington, DC, 1972.
- [21] H. N. Jow, <u>MELCOR Accident Consequence Code System (MACCS)</u>, Volume II, <u>Model Description</u>, NUREG/CR-4691, SAND86-1562, Sandia National Laboratories, Albuquerque NM, 1989, pp. 2-16.
- [22] D. H. Slade, <u>Meteorology and Atomic Energy</u>, U.S. Atomic Energy Commission, Washington, DC, 1968, p. 119.
- [23] D. Randerson, <u>Atmospheric Science and Power Production</u>, Office of Scientific and Technical Information, U.S. Department of Energy, DOE/TIC-27601, Washington, DC, 1984, p. 375.
- [24] M. L. Barad and D. A. Haugen, <u>Project Prairie Grass</u>, Geophysical Research Paper No. 59, Vols. I-III, AFCRC-TR-58-235, Air Force Cambridge Research Center, Bedford, MA, 1958.
- [25] F. A. Gifford, "A Review of Turbulent Diffusion Typing Schemes," <u>Nuclear</u> <u>Safety</u>, Vol. 17, p. 68 (1976).
- [26] F. A. Gifford, "Atmospheric Dispersion Models for Environmental Pollution Applications," in <u>Lectures on Air Pollution and Environmental</u> <u>Impact Analyses</u>, American Meteorological Society, Boston, MA, 1975, p. 35.
- [27] J. Tadmor and Y. Gur, "Analytical Expressions for the Vertical and Lateral Dispersion Coefficients in Atmospheric Diffusion," <u>Atmos.</u> <u>Envir</u>., Vol. 3, p. 688 (1969).

- [28] H. D. Brenk et al., "Transport of Radionuclides in the Atmosphere," <u>Radiological Assessment</u>, ed. J. E. Till and H. R. Myer, NUREG/CR-3332, U.S. Nuclear Regulatory Commission, Washington, DC, September 1983.
- [29] G. A. Sehmel and W. H. Hodgson, <u>A Model for Predicting Dry Deposition of Particles and Gases to Environmental Surfaces</u>, DOE Rept. PNL-SA-6721, Pacific Northwest Laboratory, NTIS, 1975.
- [30] M. Hobert et al., <u>Studies of the Deposition of Aerosols on Vegetation</u> <u>and Other Surfaces</u>, ORNL-tr-4314, Oak Ridge National Laboratory, Oak Ridge, TN, 1976.
- [31] J. A. Jones, "The Uncertainty in Dispersion Estimates Obtained from the Working Group Models," <u>The Seventh Report of the Working Group on</u> <u>Atmospheric Dispersion</u>, NRPB-R199, England, 1986.
- [32] J. Roed, "Dry Deposition in Rural and in Urban Areas," Presented at the Workshop on the Consequences of an Accidental Contamination of the Urban Environment, Roskilde, Denmark, June 1987.
- [33] J. A. Jones, <u>Modelling Wet Deposition from a Short Release</u>, NRPB-R198, National Radiological Protection Board, Chilton, Didcot, Oxon, United Kingdom, 1986.
- [34] T. A. McMahon and P. J. Denison, "Empirical Atmospheric Deposition Parameters--A Survey," <u>Atmospheric Environment</u>, Vol. 13, pp. 577-585 (1979).
- [35] W. G. N. Slinn, "Precipitation Scavenging," in D. Randerson (ed.), <u>Atmospheric Science and Power Production</u>, U.S. Department of Energy, Office of Scientific and Technical Information, DOE/TIC-27601, pp. 466-532, Washington, DC, 1984.
- [36] B. Y Underwood, "Wet Deposition," in B. Y. Underwood, P. J. Cooper, N. J. Holloway, G. D. Kaiser, and W. Nixon, <u>Review of Specific Effects</u> <u>in Atmospheric Dispersion Calculations</u>, Vol. I, EUR8935EN, Commission of the European Communities, Luxembourg, 1984, pp. 3-1 to 3-232.
- [37] H. J. Gale, D. L. O. Humphreys, and E. M. R. Fisher, "Weathering of Caesium-137 in Soil," <u>Nature</u>, Vol. 201, pp. 257-261 (1964).
- [38] L. Warming, <u>Weathering and Decontamination of Radioactivity Deposited on</u> <u>Asphalt Surfaces</u>, RISO-M-2273, Riso National Laboratory, DK-4000 Roskilde, Denmark, 1982.
- [39] L. Warming, <u>Weathering and Decontamination of Radioactivity Deposited on</u> <u>Concrete Surfaces</u>, RISO-M-2473, Riso National Laboratory, DK-4000 Roskilde, Denmark, 1984.
- [40] O. Karlberg, "Weathering and Migration of Chernobyl Fall-Out in Sweden," <u>Radiation Protection Dosimetry</u>, Vol. 21, pp. 75-78 (1987).

- [41] P. Jacob, R. Meckbach, and H. M. Mueller, "Reduction of External Exposure from Deposited Chernobyl Activity by Run-Off, Weathering, Street Cleaning, and Migration in the Soil," <u>Radiation Protection</u> <u>Dosimetry</u>, Vol. 21, pp. 51-57 (1987).
- [42] R. M. Ostmeyer and J. C. Helton, <u>Exposure Pathways Models for Accidental</u> <u>Radionuclide Releases</u>, NUREG/CR-4184, SAND85-0520, Sandia National Laboratories, Albuquerque, NM (draft available).
- [43] R. B. Codell, "Potential Contamination of Surface Water Supplies by Atmospheric Releases from Nuclear Plants," <u>Health Phys</u>., Vol. 48, pp. 713-730, (1985).
- [44] C. P. Straub, L. R. Setter, A. S. Goldin, and P. E. Hallbach, "Strontium-90 in Surface Water in the United States," <u>J. Amer. Water</u> <u>Works Assoc.</u>, Vol. 59, pp. 756-768 (1960).
- [45] Y. Miyake and H. Tsubota, "Estimation of Direct Contribution of Meteoric Water to River Water by Means of Fallout Radiocaesium and Radiostrontium," in <u>Radioisotopes in Hydrology</u>, pp. 425-431 (Vienna: IAEA) (1963).
- [46] N. Yamagata, S. Matsuda, and K. Kodaira, "Run-off of Caesium-137 and Strontium-90 from Rivers," <u>Nature</u>, Vol. 200, pp. 668-669 (1963).
- [47] W. Jacobi, J. Eichler, and N. Stolterfoht, <u>Korrelation zwischen dem</u> <u>Fallout aus Kernwaffenversuchen und der Spaltproduktaktivitaet in</u> <u>Flusswasser</u>, Hahn-Meitner-Institue fur Kernforschung, Berlin, HMI-B82 (1969).
- [48] C. F. Jordan, J. R. Kline, and D. C. Sasscer, "A Simple Model of Strontium and Manganese Dynamics in a Tropical Rain Forest," <u>Health</u> <u>Phys.</u>, Vol. 24, pp. 477-489 (1973).
- [49] C. F. Jordan and J. R. Kline, "Strontium-90 in a Tropical Rain Forest: 12th-yr Validation of a 32-yr Prediction," <u>Health Phys.</u>, Vol. 30, pp. 199-201 (1976).
- [50] H. Kamada, M. Yukawa, and M. Saiki, "Studies on Removal of <sup>90</sup>Sr in Fallout from Land to River" (in Japanese), <u>Radioisotopes</u>, Vol. 22, pp. 279-285 (1973).
- [51] Y. Miyake, Y. Sugimura, and K. Saruhashi, "Content of Plutonium in River Water in Japan," <u>Pap. Met. Geophys.</u>, Vol. 24, pp. 75-78 (1973).
- [52] H. Kamada, M. Yukawa, and M. Saiki, "Studies on Removal of Strontium-90, Ruthenium-106, Caesium-137, and Cerium-144 in Land and Fresh Water," in <u>Environmental Surveillance Around Nuclear Installations</u>, Vol. II, pp. 137-146, IAEA, Vienna, 1974.
- [53] R. D. Menzel, "Land Surface Erosion and Rainfall as Sources of Strontium-90 in Streams," <u>J. Environ. Quality</u>, Vol. 3, pp. 219-223, (1974).

- [54] H. J. Simpson, C. R. Olsen, R. M. Trier, and S. C. Williams, "Man-made Radionuclides and Sedimentation in the Hudson River Estuary," <u>Science</u>, Vol. 194, pp. 179-193 (1976).
- [55] S. Carlsson, "A Model for the Movement and Loss of <sup>137</sup>Cs in a Small Watershed," <u>Health Phys.</u>, Vol. 34, pp. 33-37 (1978).
- [56] D. G. Sprugel and G. E. Bartelt, "Erosional Removal of Fallout Plutonium from a Large Midwestern Watershed," <u>J. Environ. Qual</u>., Vol. 7, pp. 175-177 (1978).
- [57] A. Aarkrog, <u>Environmental Studies on Radiological Sensitivity and</u> <u>Variability with Special Emphasis on the Fallout Radionuclides <sup>90</sup>Sr and</u> <u>137<sub>Cs</sub></u>, Risoe-R-437, Risoe National Laboratory, Roskilde, Denmark, 1979.
- [58] G. S. Linsley, S. M. Haywood, and J. Dionian, "The Use of Fallout Data in the Development of Models for the Transfer of Nuclides in Terrestrial and Freshwater Systems," in <u>Migration in the Terrestrial Environment of</u> <u>Long-Lived Radionuclides from the Nuclear Fuel Cycle</u>, pp. 615-634 IAEA, Vienna, 1982.
- [59] P. H. Santschi, S. Bollhalder, K. Farrenkothen, A. Lueck, S. Zingg, and M. Sturm, "Chernobyl Radionuclides in the Environment: Tracers for the Tight Coupling of Atmospheric Terrestrial and Aquatic Geochemical Processes," <u>Environmental Science and Technology</u>, Vol. 22, pp. 510-516 (1988).
- [60] P. H. Santschi, S. Bollhalder, S. Zingg, A. Lueck, and K. Farrenkothen, "The Self-Cleaning Capacity of Surface Water after Radioactive Fallout. Evidence from European Waters after Chernobyl, 1986-1988," <u>Environmental</u> <u>Science and Technology</u>, Vol. 24, pp. 519-527 (1990).
- [61] T. M. Beasley and C. D. Jennings, "Inventories of 239,240Pu, 241Am, 137Cs, and 60Co in Columbia River Sediments from Hanford to the Columbia River Estuary," <u>Environ. Sci. Technol.</u>, Vol. 18, pp. 207-212 (1984).
- [62] J. Dominik, D. Burrus, and J. P. Vernet, "Transport of the Environmental Radionuclides in an Alpine Watershed," <u>Earth and Planetary Science</u> <u>Letters</u>, Vol. 84, pp. 165-180 (1987).
- [63] M. R. Scott, R. J. Rotter, and P. F. Salter, "Transport of Fallout Plutonium to the Ocean by the Mississippi River," <u>Earth and Planetary</u> <u>Science Letters</u>, Vol. 75, pp. 321-326 (1985).
- [64] D. M. Lewis, "The Use of <sup>210</sup>Pb as a Heavy Metal Tracer in the Susquehanna River System," <u>Geochimica et Cosmochimica Acta</u>, Vol. 41, pp. 1557-1564) (1977).
- [65] G. R. Foster and T. E. Hakonson, "Predicted Erosion and Sediment Delivery of Fallout Plutonium," <u>J. Environ. Qual</u>., Vol. 13, pp. 595-602 (1984).
- [66] D. K. Todd, <u>The Water Encyclopedia</u>, Water Information Center, Port Washington, NY (1970).

- [67] K. R. Lassey, "The Possible Importance of Short-Term Exposure to Resuspended Radionuclides," <u>Health Physics</u>, Vol. 38, pp. 749-761 (1980).
- [68] National Council on Radiation Protection, <u>Radiological Assessment:</u> <u>Predicting the Transport, Bioaccumulation, and Uptake by Man of</u> <u>Radionuclides Released to the Environment</u>, NCRP Report No. 76, National Council on Radiation Protection and Measurements, Bethesda, MD 1984.
- [69] W. J. Smith, F. W. Whicker, and H. R. Myer, "Review and Categorization of Saltation, Suspension, and Resuspension Models," <u>Nuclear Safety</u>, Vol. 23, pp. 685-699 (1982).

### 3.1 Evacuation Parameters

### 3.1.1 Recommendation

The values in Table 3.1 for evacuation parameters are recommended for the MACCS NUREG-1150 calculations.

<u>Variable</u>	<u>(Units)</u>	Definition	<u>Site</u>	<u>Value</u>	<u>Range<sup>a</sup></u>
EDELAY	(h)	Evacuation Delay Time	Sur GG PB Seq	1.5 0.75 1.0 1.8	1.25 - 3.25 0.25 - 1.25 0.7 - 1.7 0.5 - 2.0
ESPEED	(m s <sup>-1</sup> )	Radial Evacuation Speed	Sur GG PB Seq	1.8 3.7 4.8 1.8	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$

Table 3.1. Recommended Evacuation Parameter Values

#### <sup>a</sup> All sampling distributions should be uniform over the stated ranges.

### 3.1.2 Data Sources

During 1985, NUS conducted a review for SNL of emergency response plans and estimates of evacuation times prepared for the utilities that run the five NUREG-1150 reactors (Surry, Grand Gulf, Sequoyah, Peach Bottom, and Zion) and, as was appropriate, discussed emergency response assumptions (e.g., evacuation delay period and average evacuation speed) with utility emergency response personnel. NUS submitted the results of this study to SNL in letter reports to which were appended copies of pertinent documentation (e.g., the utility studies of estimated Emergency Protection Zone [EPZ] clearance times) from which the data in the letter reports had been taken. The data presented here were drawn from the NUS reports and supporting documentation.

### 3.1.3 Surry

The Surry reactor is located on the south side of the James River. On the south side of the river within ten miles of the reactor (i.e., within the EPZ), population densities are low. However, on the north side of the river on the peninsula defined by the James and York rivers, population densities are high because of the presence of three cities: Williamsburg, Newport News, and Hampton. Should a severe accident ever occur at the Surry reactor, evacuation of this peninsula could be difficult because of the high population densities and because only two arteries (I64 and US60) are available to support the evacuation.

Table 3.2 presents EPZ populations for the five counties that neighbor the Surry site and estimates of preevacuation delay periods and average evacuation speeds for a Summer Sunday, a Winter Weekday, and Adverse Weather (winter ice storms).

	EPZ	Summer	Sunday	Winter	Weekday	Adverse	<u>Weather</u>
	Pop	Delay	Speed	Delay	Speed	Delay	Speed
<u>County/Location</u>	<u>(x10-3)</u>	<u>(h)</u>	<u>(mph)</u>	<u>(h)</u>	(mph)	<u>(h)</u>	<u>(mph)</u>
James City	16.5	3.25	4.0			1.25	1.6
Williamsburgh	11.6	2.25	5.7			1.25	2.2
York	8.6	1.25	4.4			1.25	2.5
Newport News Surry/Isle of	45.3	2.25	3.0			1.25	1.7
Wight	4.5	1.25	8.0			1.25	8.0
Total (Population weighted)	86.5	2.3	4.0			1.25	2.2
N of River S of River	82.0 4.5	1.25 1.25	2.4 8.0	1.25 1.25	2.7 8.0	1.25 1.25	1.8 8.0
Total (Population weighted)	86.5	1.25	2.7	1.25	3.0	1.25	2.1

Table 3.2. Surry Emergency Response Data

The population-weighted results for the five counties are probably superior to the population-weighted results for the data for North and South of the river. However, if the county data are used, estimates of the preevacuation delay period and average speed for a Winter Weekday must be developed that are consistent with the county data for a Summer Sunday and Adverse Weather.

The NUS study states that delays in excess of 1.25 h are expected only during the tourist season (summer months). Thus, a preevacuation delay period of 1.25 h should apply to Winter Weekdays, which agrees with the NUS estimates for delays N and S of the river on Winter Weekdays.

The NUS average speed of 3.0 mph estimated from the data for N and S of the river is inconsistent with the population weighted aggregate county data, since the average evacuation speed for the Winter Weekday (3.0 mph) estimated from the data for N and S of the river is lower than the average speed for a Summer Sunday (4.0 mph) estimated from the county data. If the Summer Sunday 4.0 mph speed derived from county data is scaled by the ratio of the Winter Weekday speed (3.0 mph) to the Summer Sunday speed (2.7 mph) developed from the N and S of the river data, then an average evacuation speed of 4.4 mph results.

Two-sevenths of the year are weekend days, and the summer tourist season is about four months long. Therefore, assume that Summer Sunday values apply 30 percent of the time.

$$0.3 = 0.5(2/7 + 4/12)$$

On the coast of Virginia, during the winter (December 21 through March 21) precipitation occurs about 8 percent of the time. If precipitation during the winter is assumed to mean that a severe ice storm has occurred, then during a full year at Surry, adverse weather will occur about 2 percent of the time. Finally, by difference, Winter Weekday values will apply 68 percent of the time.

Yearly average values for the preevacuation delay time and the average evacuation speed at the Surry site may now be estimated using the following equation:

 $0.3 \text{ S} + 0.68 \text{ W} + 0.02 \text{ A} = \overline{X}$  (3.1)

Table 3.3 presents the yearly average values obtained using this equation.

Table 3.3. Surry Evacuation Parameter Values Estimated from the Seasons and Time of Week

Parameter	Summer	Winter	Adverse	Yearly
	<u>Sunday</u>	<u>Weekday</u>	<u>Weather</u>	<u>Average</u>
Delay (h)	2.3	1.25	1.25	1.57
Speed (mph)	4.0	4.4	2.2	4.24

Average evacuation speeds for the Surry EPZ can be estimated in at least two other ways. From a map of the peninsula near Williamsburg, one can estimate the following maximum travel distances within the EPZ for population located on the peninsula: maximum travel distance to I64 = 7 mi; and the maximum travel distance on I64 = 5 mi. Therefore, the average evacuation distance within the EPZ is about 6.0 mi = (1/2)(7 + 5). The Surry "Estimation of Evacuation Times" report prepared by PRC Voorhees gives clear time distributions for a Summer Sunday and a Winter Weekday. The distributions show that 50% of the population in the EPZ will be ready to evacuate in 1.0 h and will have cleared the EPZ in 2.6 h. Their average evacuation time is therefore 1.6 h, and their average speed is 3.75 mph = 6.0 mi/1.6 h.

The PRC Voorhees report also presents vehicle capacities (vehicles per hour) for the roads that will be used to exit the EPZ for the counties that neighbor the Surry site, and for the number of vehicles available to support the evacuation in each county. From the number of vehicles available and the total EPZ population of each county, one can estimate that the average evacuating vehicle will be occupied by three people. Thus, from the county EPZ populations and vehicle capacities, one can estimate average evacuation times. Table 3.4 presents these estimates:

	EPZ	Vehicle	Evacuation
	Рор	Capacity	Time
County	<u>(x10-3)</u>	<u>(x10-3)</u>	<u>(h)</u>
Surry/Wight	4.5	6.0	0.25
James/Williamsburgh	28.1	7.2	1.3
York	8.6	3.6	0.8
Newport News	<u>45,3</u>	9.6	<u>1.6</u>
Population weighted to	al 86.5	-	1.4

Table 3.4. Estimation of Surry Evacuation Times from Vehicle Capacities and Populations

Since evacuation of the peninsula will determine average evacuation speeds within the EPZ, that speed can be estimated to be 4.29 mph = 6.0 mi/1.4 h, where 6.0 is the maximum travel distance within the EPZ on the peninsula.

Given the preceding results, a pre-evacuation delay period of 1.5 hours and an average evacuation speed of 4.0 mph (1.8 m s<sup>-1</sup>) are recommended for NUREG-1150 calculations for the Surry site.

Table 3.5 presents the evacuation delay time and evacuation speed recommended for use at the Surry site and compares the recommended values to those specified by the NRC for use in the first pass NUREG-1150 calculations:

Table 3.5. Values Recommended for Surry Evacuation Parameters

· · ·	Recommended	
	<u>Value</u>	NRC
Delay (h)	1.5	1.0
Delay (h) Speed (m s <sup>-1</sup> )	1.8	1.2

### 3.1.4 Grand Gulf

Evacuation time estimates for the Grand Gulf site are based on a state-of-theart road network analysis. Data for pre-evacuation delay times and EPZ clearance times (delay time plus evacuation time) were developed for Weekdays, Weekend Days/Nights, and Adverse Weather (severe thunderstorms). Table 3.6 presents the evacuation data.

Table 3.6. Evacuation Data	for	Grand	Gulf
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	Average <sup>a</sup> Delay Time	Clear Time	Evacu. 		Maximum Travel Distance	Speed
<u> </u>	(min)45	<u>(min)</u> 160	<u>(min)</u> 115	<u>(h)</u> 1,92	<u>(min)</u> 10	Speed <u>(mph)</u> 5.21
Weekend/Night (WE/N) Adverse Weather (A)	45 45	105 205	60 160	1.0 2.67	10 10	10.0 3.75

<sup>a</sup>Delay times ranged from 15 to 75 minutes, so the average delay time is 45 minutes.

At the Grand Gulf site, precipitation at rates in excess of 0.1 in/h occurs about 2 percent of the time. If rain at rates that exceed 0.1 in/h is assumed to mean that a severe thunderstorm is occurring, then adverse weather will also occur at the Grand Gulf site about 2 percent of the time.

Yearly average pre-evacuation times and average evacuation speeds can be calculated from these data using the following equation:

$$0.02 \text{ A} + 0.98 [0.5 \text{ N} + 0.5(0.71 \text{ WD} + 0.29 \text{ WE})] = X$$
 (3.2)

where 0.71 = 2/7, and 0.29 = 5/7. Substitution of the evacuation delay times and speeds listed in the preceding table into this equation yields a yearly average evacuation delay time of 45 min = 0.75 h and a yearly average evacuation speed of 8.2 mph = 3.7 m s<sup>-1</sup>. Table 3.7 presents the evacuation delay time and evacuation speed recommended for use at the Grand Gulf site and compares the recommended values to those specified by the NRC for use in the first pass NUREG-1150 calculations:

Table 3.7. Values Recommended for Grand Gulf and Evacuation Parameters

Parameter	Recommended Value	NRC
Delay (h) Speed (m s <sup>-1</sup> )	0.75 3.7	1.25 <sup>a</sup> 2.0
<sup>a</sup> where 1.25 h = 75 min, delay time.	, the maximum	pre-evacuation

### 3.1.4 Peach Bottom

Estimates of total EPZ clearance times and pre-evacuation delay times (expressed in minutes after offsite warning) have been reported by the Philadelphia Electric Company for the five counties (Lancaster, York, Chester, Cecil, and Harford) that neighbor the Peach Bottom site. Values are reported for two types of weather (normal and adverse), two seasons of the year (winter and summer), and two times of day (daytime and nighttime). The estimates were developed using a state-of-the-art road network analysis. Table 3.8 presents estimates of the preevacuation delay time and the evacuation time, where

Evacuation Time = Total EPZ Clearance Time - Pre-evacuation Delay Time

for each county and set of conditions (prevailing weather, season, time of day). Also presented for each county are the distance to the EPZ boundary and the population within the EPZ.

	County					Population
	Lancaster	<u>York</u>	<u>Chester</u>	<u>Cecil</u>	<u>Harford</u>	Weighted <u>Average</u>
Population						
(0-12 mi x 10 <sup>-3</sup> )	19.2	7.9	2.8	4.2	12.9	47.0
Evacuation						
<u>Distance</u> (mi)	13	12	15	12	12	12.6
<u>Daytime</u>						
Normal Weather						
Delay Time	85	80	88	75	80	82
Evacuation Time						
Winter	95	80	75	75	90	88
Summer	95	80	75	75	90	88
Adverse Weather	100	0.5	~~	0.5	0.5	
Delay Time	100	95	98	85	95	96
Evacuation Time	100	105	75	76	0.5	0.0
Winter	100	105	75	75 75	95 105	96
Summer	120	105	75	75	105	107
Nighttime						
Normal Weather						
Delay Time	40	40	53	40	40	41
Evacuation Time						-
Winter	50	50	40	40	50	49
Summer	60	50	40	40	60	55
Adverse Weather						
Delay Time	40	40	53	40	40	41
Evacuation Time						
Winter	70	70	50	50	80	70
Summer	90	70	50	50	90	81

Table 3.8. Peach Bottom Evacuation Data

Yearly average values of pre-evacuation delay times and evacuation times can be calculated from this data using the following equation:

 $0.05[0.25(SDA + WDA + SNA + WNA)] + 0.95[0.25(SDN + WDN + SNN + WNN)] = \overline{X}$ 

where

SDA = summer, daytime, adverse weather WDA = winter, daytime, adverse weather SNA = summer, nighttime, adverse weather WNA = winter, nighttime, adverse weather SDN = summer, daytime, normal weather WDN = winter, daytime, normal weather SNN = summer, nighttime, normal weather WNN = winter, nighttime, normal weather

and adverse weather (weather that reduces road capacities by 30%, e.g., snow, ice, rain, fog) is assumed to occur 5% of the time (precipitation occurs during about 8.5% of the hours in the year at the Peach Bottom site).

Substitution of the pre-evacuation delay times and evacuation times listed in the preceding table into this equation yields a yearly average preevacuation delay time of 62 min = 1.0 h and a yearly average evacuation time of 71 min = 1.18 h. Since the population weighted straight-line evacuation distance is 12.6 mi, this average evacuation time corresponds to an average evacuation speed of 10.7 mph =  $4.8 \text{ m s}^{-1}$ .

Table 3.9 presents the evacuation delay time and evacuation speed recommended for the Peach Bottom site and compares the recommended values to those specified by the NRC for use in the first pass NUREG-1150 calculations:

Parameter	Recommended Value	· NRC
Delay (h)	1.0	1.25
Speed (m s <sup>-1</sup> )	4.8	2.0

Table 3.9. Values Recommended for Peach Bottom Evacuation Parameters

### 3.1.5 Sequoyah

Estimates of clear times for the Sequoyah site are presented in the Multijurisdictional Emergency Response Plan prepared for that site by the State of Tennessee. That plan divides population into two groups, residents and transients, where transients are primarily people who visit the river to swim or picnic during summer months (June through September). For each of these population groups, and for both together, the plan esimates clear times for each of 28 sectors within the 10-m EPZ. These clear time estimates are presented in Table 3.10.

Sector	Рор	ulation				Clear T	ime (h)	
- <u>-</u>		Transients	Resid	dents	Transients		Both	
			<u>Normal</u>	<u>Adverse</u>	<u>Normal</u>	<u>Adverse</u>	<u>Normal</u>	<u>Adverse</u>
_								
A-1	1210	1500	5.25	6.00	2.50	3.25	6.00	6.75
A-2	490	600	5.25	6.00	2.50	3.25	6.00	6.75
A-3	3575		5.25	6.00			6.00	6.75
A-4	660		2.25	3.00			3.00	3.75
A-5	1100		4.25	5.00			5.00	5.75
A-6	1085	1350	3.88	4.63	2.50	3.25	4.63	5.38
B-1	850	2000	2.94	3.69	1.50	2.25	3.69	4.44
<b>B-2</b>	600	1050	2.67	3.42	1.50	2.25	3.42	4.17
B-3	845		2.83	3.58			3.58	4.33
B-4	410	900	2.50	3.25	1.50	2.25	3.25	4.00
<b>B-</b> 5	1195		3.17	3.92			3.92	4.67
B-6	160		3.50	4.25			4.25	5.00
B-7	250		2.25	3.00			3.00	3.75
<b>B - 8</b>	645		3.50	4.25			4.25	5.00
C-1	1040	750	3.50	4.25	1.50	2.25	4.25	5.00
C-2	1945	3700	3.50	4.25	2.50	3.25	4.25	5.00
C-3	1810		3.00	3.75			3.75	4.25
C-4	750		3.50	4.25			4.25	5.00
C-5	445		2.50	3.25			3.25	4.00
C-6	1670		3.13	3.88			3.88	4.63
C-7	1880	235	3.08	3.83	2.50	3.25	3.83	4.58
C-8	2440	4000	3.50	4.25	2.50	3.25	4.25	5.00
D-1	300	1250	5.25	6.00	2.50	3.25	6.00	6.75
D-2	3585	1500	5.25	6.00	3.88	4.63	6.00	6.75
D-3	3450		4.75	5.50		•	5.50	6.25
D-4	1650		4.00	4.75			4.75	5.50
D-5	10340		4.50	5.25			5.25	6.00
D-6	2880	5200	5.25	6.00	5.25	6.00	6.00	6.75
Sum	47260	24035						
Popula								
<u>Weight</u>	<u>ed Sum</u>		4.17	4.92			4.90	5.65

The clear time estimates presented in Table 3.10 rest on the following four assumptions:

- Whenever the residential population of the full EPZ is evacuated, the delay between notification to evacuate and the actual start of evacuation is 1.75 h.
- (2) When the full EPZ is evacuated, adverse weather (snow or flooding) lengthens evacuation times by 45 min.
- (3) Clear times for residents are lengthened by 45 m in. whenever the recreational transient population evacuates with the residential population.

(4) Delay times are not lengthened by adverse weather.

At Knoxville, TN, total yearly precipitation averages 47.29 inches and snow (as snow) averages 12.3 inches. Since the density of water is  $1.0 \text{ g/cm}^3$  and the density of snow is about  $0.1 \text{ g/cm}^3$ , the Knoxville data suggest that about 2.6 percent

$$2.6 = 100[12.3(0.1)/47.49(1.0)]$$

of all precipitation at the Sequoyah site will be snow. At the Sequoyah site, rain occurs during 7 percent of the hours of the year, and intense rain (rain rate greater than 6 mm/h for one h) occurs less than 0.15 percent of the time (during only 13 of 8760 h). If rain at a rate of 6 mm/h is assumed to indicate flooding, then adverse weather (flooding or snowfall) will occur at the Sequoyah site less than 3 percent of the time. Finally, if significant transient population is assumed to be present within the EPZ only on weekend days during the months of June through September, then the fraction of time when both the residential and the transient populations will evacuate together will be 0.1 = (4/12)(2/7).

The following equation can now be used to estimate a yearly average clear time for the entire Sequoyah EPZ:

$$f_A(f_R t_{RA} + f_B t_{BA}) + f_N(f_R t_{RN} + f_B t_{BN}) = \overline{X}$$
(3.3)

where

- $f_A$  = fraction time adverse weather prevails = 0.03,
- $f_{\rm N}$  = fraction time normal weather prevails = 0.97,
- $f_R$  = fraction time only residential population evacuates = 0.9,
- $f_B$  = fraction time both residential and transient population evacuates = 0.1,
- $t_{RA}$  = clear time during adverse weather when only the residential population evacuates = 4.90 h,
- $t_{BA}$  = clear time during adverse weather when both the residential and the transient population evacuate = 5.65 h,
- $t_{RA}$  = clear time during normal weather when only the residential population evacuates = 4.17 h, and
- $t_{BA}$  = clear time during normal weather when both the residential and the transient population evacuates = 4.92 h.

Substitution of the parameter values given above now yields an average clear time of 4.27 hours and thus an average evacuation time of 2.52 h = 4.27 h - 1.75 h where 1.75 h is the delay time before evacuation commences. Accordingly,  $3.97 \text{ mph} = 10 \text{ mi}/2.52 \text{ h} = 1.8 \text{ m s}^{-1}$  is a reasonable estimate of average evacuation speeds within the Sequoyah EPZ when the average is taken over all weather conditions and all evacuating populations. Table 3.11

presents the evacuation delay time and evacuation speed recommended for use at the Sequoyah site and compares the recommended values to those specified by the NRC for use in the first pass NUREG-1150 calculations:

Table 3.11. Values Recommended for Sequoyah Evacuation Parameters

	Recommended	
Parameter	Value	NRC
Delay (h)	1.75	1.7
Delay (h) Speed (m s <sup>-1</sup> )	1.8	1.2

## 3.2 Shielding Factors and Breathing Rate

### 3.2.1 Recommendation

The shielding factor values and breathing rate in Table 3.12 are recommended for use in MACCS NUREG-1150 calculations. In Table 3.12, BRRATE = breathing rate, CSFACT = cloudshine shielding factor, GSFACT = groundshine shielding factor, PROTIN = inhalation protection factor, and SKPFAC = skin protection factor.

Table 3.12.	Recommended	Shielding	Factor	Values
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<u>Variable</u>	<u>(Units)</u>	Activity	<u>Site</u>	Value	Range*
BRRATE	(liters/day)	A11	A11 2	$.3 \times 10^4$	$(0.9-2.6) \times 10^4$
CSFACT	(unitless)	Evacuation	A11	1.0	n/a
		Normal Activity	A11	0.75	0.6-0.95
		Active Sheltering	Zion	0.5	0.4-0.6
			GG	0.7	0.6-0.8
			PB	0.5	0.4-0.6
			Sur	0.6	0.5-0.7
			Seq	0.65	0.55-0.75
GSFACT	(unitless)	Evacuation	A11	0.5	0.3-0.7
		Normal Activity	A11	0.4	0.2-0.75
		Active Sheltering	Zion	0.1	0.03-0.2
		-	GG	0.25	0.1-0.4
			PB	0.1	0.02-0.2
			Sur	0.2	0.1-0.3
			Seq	0.2	0.1-0.35
PROTIN	(unitless)	Evacuation	A11	1.0	n/a
		Normal Activity	A11	0.5	0.15-1.0
		Active Sheltering	A11	0.2	0.1-0.4
SKPFAC	(unitless)	Evacuation	A11	1.0	n/a
		Normal Activity	A11	0.5	0.15-1.0
		Active Sheltering	A11	0.2	0.1-0.4

\* All sampling distributions should be uniform over the stated ranges.

#### 3.2.2 Discussion

MACCS requires that shielding factors be specified for people evacuating in vehicles (cars, buses), taking shelter in structures (houses, offices, schools), and continuing normal activities either outdoors, in vehicles, or indoors. Because inhalation doses depend on breathing rate, breathing rates must be specified for people who are continuing normal activities, taking shelter, and evacuating. Since indoor concentrations of gas-borne radioactive materials are usually substantially less than outdoor concentrations, MACCS also requires that inhalation and skin protection shielding factors (i.e., indoor/outdoor concentration ratios) be provided.

## 3.2.2.1 Breathing Rate

Breathing rates depend on activity, sex, and age. Adult men, women, and children, who sleep 8 hours per day and engage in light activity when awake, breathe respectively about  $2.3 \times 10^4$ ,  $2.1 \times 10^4$ , and  $1.5 \times 10^4$  liters of air per day [1]. Breathing rates for infants are substantially lower. Heavy activity increases breathing rates by about 50 percent. If fear is assumed not to increase the breathing rates of persons taking shelter or evacuating in vehicles, then the age and sex weighted breathing rate for light activity should be a reasonable number to use for persons responding to an accident. If 80 percent [2] of the population is assumed to be teenagers and adults (light activity breathing rate =  $2.8 \times 10^4$  liters/day), 17 percent [2] is preteen children (light activity breathing rate =  $1.8 \times 10^4$  liters/day), and 3 percent [2] is babies (waking breathing rate =  $0.6 \times 10^4$  liters/day), the average light activity breathing rate is 2.6x10<sup>4</sup> liters/day. Since this value differs little from the daily breathing rate of an adult man  $(2.3 \times 10^4)$ liters/day =  $2.66 \times 10^{-4} \text{ m}^3/\text{s}$ ) typically used in ex-plant consequence calculations, the value for an adult man is selected for use in the NUREG-1150 calculations. For sensitivity studies, this parameter should be varied over the range  $0.9 \times 10^4$  liters/day (sleeping population) to  $2.6 \times 10^4$  liters/day (light activity).

# 3.2.2.2 Inhalation and Skin Protection Factors

Penetration of particulate matter into buildings is usually expressed as the ratio of the indoor particulate concentration to the outdoor concentration. Incomplete penetration lowers indoor inhalation and skin doses. Specifically, the Indoor Dose = (Outdoor Dose) (Indoor/Outdoor Ratio). Thus, the Indoor/Outdoor ratio gives the shielding factor provided by buildings for inhalation and skin exposures.

Indoor/Outdoor ratios of particulate matter in houses and buildings have been determined during several experimental studies [3-7]. These studies show that indoor/outdoor ratios depend strongly on particle size. Table 3.13 summarizes the results of these studies.

Range (µm)	<u>Indoor/Outdoor Ratio</u>	Reference
0.05 - 0.2	0.5	[7]
0.1 - 0.65	0.4	[3]
< 1	0.4	[4]
0.1 - 2	0.6	[6]
0.65 - 20	0.2	[3]
> 1	0.2	[4]
?	0.1 - 0.5	[5]

Table 3.13. Building Inhalation and Skin Shielding Factors (Indoor/Outdoor Ratios)

These data suggest that small particles  $(0.1 - 1 \ \mu\text{m})$  will have an indoor/outdoor ratio of about 0.5, while large particles  $(1 - 20 \ \mu\text{m})$  will have indoor/outdoor ratios of about 0.2. Since mass and therefore radioactivity will be concentrated in a distribution's large particles, use of a value smaller than 0.5 is indicated.

Indoor/Outdoor inhalation dose ratios have been calculated by Aldrich for a single compartment subject both to infiltration and ventilation [8]. As derived by Aldrich, this ratio is directly proportional to the fraction of the plume that penetrates the compartment (indoor/outdoor concentration ratio). Using best estimate values for model parameters (including a penetration fraction, indoor/outdoor concentration ratio, of 0.85), Aldrich found this dose ratio to have a value of about 0.6. Use of a penetration fraction of 0.3 would lower Aldrich's indoor/outdoor dose ratio to about 0.2.

Opening windows is observed rapidly to increase indoor/outdoor ratios. If windows are assumed to be open during the summer, then a time weighted summation of an indoor/outdoor ratio of 1.0 for the summer (3 months) and 0.2 for the rest of the year (9 months) yields an average indoor/outdoor ratio of 0.4.

Accordingly, for people in buildings, skin and inhalation protection factors of 0.2 (range 0.1 to 0.4) if actively taking shelter and 0.4 (range 0.1 to 1.0) if continuing normal activity are recommended. For people outdoors and evacuating in vehicles, skin and inhalation protection factors of 1.0 (no significant protection) should be assumed.

# 3.2.2.3 Reference Doses

External radiation doses to individuals are reduced by materials (e.g., hills, buildings, building walls if indoors) that are between the individual and the radiation source. The reduction, which is usually called the "shielding factor," is defined by the following equation:

$$S = D/D_{ref}$$
(3.4)

where S is the shielding factor, D is the dose received, and  $D_{ref}$  is the reference dose, which is the groundshine dose that would be received by an individual standing on a contaminated, completely smooth, infinite plane or

the cloudshine dose that would be received by an individual immersed in a contaminated infinite cloud (the effects of finite cloud dimensions and off-centerline locations on cloudshine doses are treated in MACCS using the semi-infinite cloud correction factor).

## 3.2.2.4 Outdoor Shielding Factors

People outdoors may be partially shielded from a contaminated cloud by buildings and hills. Since this shielding is likely to be pronounced only for people located in urban street canyons, a cloudshine shielding factor of 1.0 for people outdoors is recommended for use in best estimate MACCS calculations.

People who are outdoors are shielded from contaminated ground not only by buildings and hills but also by the roughness of the contaminated ground surfaces (e.g., dirt, lawns, pavement). The average shielding provided by suburban land will depend on how much of that land is typically devoted to houses, lawns, and pavement. Consider a 2000 ft<sup>2</sup> house (45 ft<sup>2</sup>) on a quarter acre ( $10^4$  ft<sup>2</sup>) lot fronted by a 3-ft-wide sidewalk and half of a 32-ft-wide road. If the roof of the house has a surface roughness like that of pavement, then the fraction of suburban land devoted to lawns is about 0.67, and the fraction devoted to pavement is about 0.33.

$$0.67 = \frac{(100)^2 - (45)^2}{100(100 + 3 + 16)}$$
(3.5)

Accordingly, using surface roughness shielding factors [9] of 0.8 for lawn and of 0.93 for pavement yields an average surface roughness shielding factor for suburban surfaces of 0.84.

The shielding from groundshine provided by buildings to people located outdoors can be estimated by a view factor calculation. For example, a square house, 45 ft on a side, located at the center of a square quarter acre lot will screen about 36 degrees of the horizon from the view of a person, who is standing at the intersection of the lot sideline with the centerline of the street that fronts the lot. Thus, assuming obstruction of view principally by the four nearest houses, groundshine reduction due to screening by buildings will be about 0.6 = 1 - 4(36/360).

Table 3.14 presents estimates for overall urban and suburban shielding factors for people located outdoors

Location	<u>Shielding Factor</u>	<u>Reference</u>
Urban Copenhagen	0.06	[10]
Street canyon	0.1	[11]
Suburban Copenhagen	0.6	[10]
Urban areas	0.3 - 0.7	[12]
Lawns, trees, and streets (after dry deposition)	0.5 - 2.0	[11]
Lawns and streets (deposition during heavy rain, little	0.2 - 0.5	[11]

Table 3.14. Urban and Suburban Skidding Factors for People Located Outdoors

deposition to tree leaves)

If the following three assumptions are made,

- (1) the amount of material deposited on tree leaves is about the half the amount deposited on the ground,
- (2) the shielding factor for material deposited on tree leaves is 2.0 (this number is larger than 1.0 because the leaves of a tree are a smooth vertical planar source) and the roughness shielding factor for material deposited on suburban surfaces is 0.84, and
- (3) buildings and hills reduce exposures to materials deposited on tree leaves and on the ground by a factor of 0.6,

then, in agreement with Ostmeyer and Helton [la], an overall shielding factor of 0.73 can be calculated for people located oudoors in suburban areas as follows:

$$0.73 = 0.6[0.33(2.0) + 0.67(0.84)]$$
(3.6)

Increasing the fraction of material deposited on tree leaves to 0.5 from 0.33 increases the overall shielding factor to 0.85. Decreasing the fraction deposited on tree leaves to 0.25, lowers the overall shielding factor to 0.68. Accordingly, an overall groundshine shielding factor of 0.7 for people located outdoors is suggested for use in best estimate MACCS calculations. For sensitivity studies a range of 0.2 - 1.0 should be assumed for this factor.

#### 3.2.2.5 Mass Thickness

The shielding provided by a material is directly proportional to its mass thickness, which is the product of the density of the material and its thickness. Densities for typical building materials [13] are presented in Table 3.15.

	Density
<u>Material</u>	<u>(g/cm<sup>3</sup>)</u>
aluminum	2.6
asphaltum, tar	1.2
brick	1.8
concrete block '	2.3
glass	2.6
gypsum (wallboard)	0.93
insulation	0.65
steel	7.8
Portland cement	3.1
wood (pine)	0.5

Table 3.15.	Densities	of	Building	Materials
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From these data, approximate mass thicknesses may be calculated for several types of wall construction typical of U.S. houses.

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WOOD FRAME HOUSES FACED WITH WOOD, ALUMINUM, OR STUCCO 0.125" aluminum + 0.5" wood + 3.0" insulation + 0.5" wallboard  $2.54[0.125(2.6) + 0.5(0.5) + 3.0(0.65) + 0.5(0.93)] = 7.6 \text{ g/cm}^2$ 

0.5" wood siding + 0.5" wood + 3" insulation + 0.5" wallboard  $2.54[0.5(0.5) + 0.5(0.5) + 3.0(0.65) + 0.5(0.93)] = 7.4 \text{ g/cm}^2$ 

0.75" stucco + 0.5" wallboard + 3.0" insulation + 0.5" wallboard 2.54  $[0.75(3.1) + 0.5(0.93) + 3.0(0.65) + 0.5(0.93)] = 13.2 \text{ g/cm}^2$ 

# BRICK AND CONCRETE BLOCK HOUSES

2.5" brick + 0.5" wallboard + 3.0" insulation + 0.5" wallboard 2.54[2.5(1.8) + 0.5(0.93) + 3.0(0.65) + 0.5(0.93)] = 18.7 g/cm<sup>2</sup>

0.75" stucco + 3.0" cement + 0.5" wallboard 2.54[0.75(3.1) + 3.0(2.3) + 0.5(0.93)] = 24.6 g/cm<sup>2</sup>

#### ROOFS

0.25" asphalt shingles + 0.5" wood + 0.5" wallboard 2.54[0.25(1.2) + 0.5(0.5) + 0.5(0.93)] = 2.6 g/cm<sup>2</sup>

#### FLOORS

0.5" wood + 0.5" wallboard

 $2.54[0.5(0.5) + 0.5(0.93)] = 1.8 \text{ g/cm}^2$ 

In agreement with Ostmeyer and Helton [1b], these qualitative calculations suggest that 10 g/cm<sup>2</sup> is a typical mass thickness for wood frame houses faced with wood siding, aluminum siding, or stucco, and that 20 g/cm<sup>2</sup> is a typical mass thickness for brick or concrete block houses.

#### 3.2.2.6 Vehicular Shielding Factors

An eighth of an inch of steel corresponds to a mass thickness of 2.5 g/cm<sup>2</sup> and an eighth of an inch of glass to a mass thickness of 0.8 g/cm<sup>2</sup>, neither of which is sufficient to provide significant shielding from a radioactive plume. Therefore, since the interior space of cars and buses will not exclude a significant fraction of the plume, the value of the cloudshine shielding factor for vehicles should be assumed to be 1.0.

The shielding afforded by vehicles from exposure to contaminated ground has been examined experimentally by comparing the dose rate in the vehicle to the dose rate outside the vehicle [15,16]. Data for cars and buses are presented in Table 3.16.

<u>Vehicle</u>	<u>Indoor/Outdoor Ratio</u>	<u>Reference</u>
Cars	0.6 - 0.7 0.3 - 0.6	[16] [17]
Buses	0.5 - 0.7 0.3 - 0.4	[16] [17]

Table 3.16. Vehicle Groundshine Shielding Factors

A shielding factor referenced to a contaminated infinite smooth plane may be calculated from these numbers by multiplying by the surface roughness shielding factor for the land surrounding the roadway. Both for countryside and suburbia, the surface roughness shielding factor for grass should be used. Thus, assuming that (1) inside/outside vehicular dose ratios are respectively 0.5 and 0.6 for buses and cars, and that (b) 10 percent of the people in vehicles are in buses and the balance in cars, in agreement with Ostmeyer and Helton [1c], a groundshine shielding factor of 0.5 for vehicles can be calculated as follows:

$$0.5 = 0.8[0.1(0.5) + 0.9(0.6)] \tag{3.7}$$

## 3.2.2.7 Structure Shielding

The degree of shielding afforded to persons within a structure depends strongly on the nature (construction type) of the structure, the location within the structure of the shielded person, and the amount of radioactive material that infiltrates the structure. Accordingly, the shielding afforded to persons, who actively take shelter in basements or interior rooms with building windows and doors closed, can be significantly greater than that afforded persons who continue normal activities.

Structures shield people from cloudshine because their walls attenuate radiation and because indoor gas-borne concentrations of plume materials are usually substantially less than those in the outdoor plume. Indoor concentrations are lower because infiltration is not complete and deposition to interior surfaces further reduces the gas-borne amounts of those materials that do infiltrate the structure. But the indoor volumes of typical houses will usually be small compared to the volume of the outdoor plume. Therefore, complete plume exclusion from typical houses will produce a reduction in dose of only about 0.95 [1d]. Since complete plume exclusion is unlikely, dose reduction due to plume exclusion can be neglected. Shielding due to dose attenuation is calculated as the sum of the attenuation factors for the structural elements (walls, roofs, ground if in a basement) that lie between the shielded person and the plume with each attenuation factor weighted by the fraction of the plume shielded by that element. Consider a person standing in the middle of a single story square 2000 ft<sup>2</sup> house enveloped by a hemispherical plume. If approximated by a circle, the house will have a radius of 25 ft. Mensuration formuli for spheres [20] show that the fraction of the hemispherical plume subtended by the walls of the house is given by the ratio of the wall height to the distance from the center of the house to the top of its walls. That distance is about 26 ft, where 26 is the hypotenuse of the right triangle having sides 8 and 25 ft long. Therefore, the walls of the single story square 2000 sq ft house will screen about 0.3 = 8/26 of the hemispherical cloud from a person standing in the middle of the house. The remaining 0.7 of the hemisphere will be screened by the roof of the house. If this single story house has a full basement, then the ground, walls, and roof plus floor of the house will respectively screen the following fractions of the hemispherical cloud: 0.3, 0.23, and 0.47.

If the house has two 1000  $ft^2$  stories and thus an effective radius of 18 ft, for a person standing in the middle of the first floor, the fractions of the hemispherical plume screened by the walls and the roof will be 0.67 and 0.33. For a person standing in the middle of the second floor, the wall and roof screening fractions are 0.4 and 0.6. If the person is standing in the middle of the basement of the house, the fractions of the hemispherical plume screened by the ground, walls, and roof are 0.4, 0.4, and 0.2. Assuming complete screening by the ground and attenuation factors [1e] of 0.74 for wood frame walls, 0.52 for masonry walls, 0.92 for a roof, 0.87 for a roof plus one floor, and 0.81 for a roof plus two floors, now allows the following cloudshine shielding factors to be estimated for houses as in Table 3.17.

House	<u>Construction</u>	<u>Location</u>	<u>Factor</u>
1-story	wood frame masonary	lst floor basement lst floor	0.87 0.58 0.80
2-story	wood frame masonry	basement 2nd floor 1st floor basement 2nd floor 1st floor basement	0.53 0.85 0.78 0.46 0.76 0.64 0.37

Table 3.17. Cloudshine Shielding Factors

Assuming that most people are downstairs during waking hours and upstairs when sleeping yields overall normal activity cloudshine attenuation factors of 0.80 = 0.67(0.78) + 0.33(0.85) for two story wood frame houses and 0.68 = 0.67(0.64) + 0.33(0.76) for two story masonry houses.

Now consider a two story school or office building with an effective radius of 25 ft. If walls, floors, and roofs all have mass thicknesses of about 20

 $g/cm^2$ , then the value of the cloudshine attenuation factor will be 0.52 for people on the second floor and 0.39 for people on the first floor, where

0.39 = 0.53(0.52) + 0.47(0.24)

The fraction of the cloud subtended by walls is 0.53, and 0.24 is the shielding provided by a roof plus a floor (total mass thickness of 40 g/cm<sup>2</sup>). Now if people in the building are evenly distributed between the first and second floors, an overall cloudshine attenuation factor of 0.46 can be calculated for schools and small office buildings. Larger effective building radii and poured concrete (rather than concrete block) walls will reduce this value. Therefore, a cloudshine shielding factor of 0.4 for schools and small office buildings is recommended for use in MACCS. For sensitivity studies, a range of 0.2 (cloudshine shielding factor for large office buildings [18]) to 0.5 (cloudshine shielding factor for single story school or office building) should be assumed.

Structure shielding to cloudshine has been examined by Burson and Profio [18] who assumed different building dimensions and mass thicknesses in their calculations then were assumed above. Table 3.18 presents the shielding factor recommendations of Burson and Profio both as originally developed by those authors (the number not in parentheses) and as obtained using the same mass thicknesses assumed above (the number in parentheses).

Structure	Location	Factor
House		
Wood Frame	Ground Floor	0.9 (0.8)
	Basement	0.6 (0.5)
Masonry	Ground Floor	0.6 (0.7)
	Basement	0.4 (0.45)
0.C.C	<b>-</b>	
Office Building	Interior	0.2 (0.4)

Table 3.18. Cloudshine Shielding Factors Recommended by Burson and Profio [18] for People Located in Buildings

Since cloudshine structure shielding factors are certainly not precise to two significant figures, values in Table 3.19 are recommended for use in MACCS.

<u>Activity</u>	Structure	<u>Stories</u>	Factor
Normal	Wood Frame House	2	0.8
		1	0.9
	Masonry House	2	0.7
		1	0.8
	School or Office	2	0.4
Sheltering	Wood Frame House	2	0.5
		1	0.6
	Masonry House	2	0.4
		1	0.5
	School or Office	2	0.4

# Table 3.19. Recommended Cloudshine Shielding Factor for People Located in Buildings

In contrast to cloudshine, where the dose from gas-borne materials that have infiltrated a structure is usually small compared to the dose received from the plume that envelopes the structure, for the groundshine dose received from indoor deposits of infiltrated materials can be important when compared to the groundshine dose received from materials deposited outdoors. The contribution of indoor deposits to total groudshine doses (the dose from all deposited materials whether deposited outdoors or indoors) has been examined by Ostmeyer and Helton [1f] and by Jacob and Meckbach [11]. Jacob and Meckbach note that as structure shielding increases, the dose from indoor deposits becomes increasingly important. For example, in a structure that has a groundshine shielding factor of 0.015, indoor exposures are increased by about a factor of two, if the indoor deposit is 2 percent of the outdoor deposit [11]. In agreement with Ostmeyer and Helton [1g], Jacob and Meckbach [11] also estimate that an indoor deposit that is 10 percent of that outdoors will double the indoor dose if the structure's groundshine shielding factor is 0.07.

The dose from indoor deposits can be indirectly modeled by increasing the value of the groundshine shielding factor as required to produce a total dose equal to that which would result from all deposited materials (both those deposited on outdoor surfaces and those deposited on indoor surfaces). For wood frame houses (mass thickness =  $10 \text{ g/cm}^2$ ) and masonry houses (mass thickness =  $20 \text{ g/cm}^2$ ), Ostmeyer and Helton estimate [1h] that if indoor deposite are half those outdoors, the total indoor dose from all deposited materials (both indoors and outdoors) is well approximated by increasing the structure's groundshine shielding factor 0.1 unit.

Groundshine shielding has been reviewed by Burson and Profio [18] and by Ostmeyer and Helton [1f] and recent European studies of groundshine shielding factors have been summarized by Roed [19]. Table 3.20 presents pertinent results from these studies.

		Houses	<u>.</u>			Sch	<u>001/0f</u>	fice	B	asemen	<u>it</u>
	Wood Fra	ame	<u>M</u>	asonry							
<u>Ref</u>	<u> </u>	<u> </u>	L	<u> </u>	<u> </u>	<u>L</u> _	<u> </u>	<u>U_</u>	<u>    L</u>	<u> </u>	<u>U</u>
0	0.4 0.5	0.6	0.3	0.35	0.4	0.15	0.4	0.5	0.02	0.08	0.08
В	0.2 0.4	0.5	0.04	0.2	0.4	0.01	0.05	0.08	0.02	0.04	0.07
B+d	0.3 0.4	0.6	0.14	0.3	0.5	0.11	0.15	0.18	0.12	0.14	0.17
R	0.44			0.19			0.1				
R+d	0.54			0.29			0.2				

Table 3.20. Groundshine Shielding Factors for Buildings

In the table, the shielding factor value in the C column is the central (best) estimate value and the L (lower) and U (upper) values define the estimated range of the factor. In the column labeled Ref, O denotes Ostmeyer and Helton [1a], B Burson and Profio [18], and R Roed [19]. Since the values of Ostmeyer and Helton reflect correction for indoor deposits (i.e., groundshine shielding factor imcremented 0.1 unit to correct for 50 percent infiltration) while those of Burson and Profio and of Roed do not, the table also presents the values of Burson and Profio and of Roed incremented by 0.1 unit (B+d and R+d on the table) to permit comparison to the values of Ostmeyer and Helton. Finally, the values in the table attributed to Roed were calculated assuming mass thicknesses of 10 g/cm<sup>2</sup> (wood frame houses), 20 g/cm<sup>2</sup> (masonry houses), and 35 g/cm<sup>2</sup> (office building with solid concrete walls, i.e., not concrete block) using the following dependence of groundshine shielding factor (S<sub>gd</sub>) on exterior wall thickness (m<sub>t</sub>)

$$S_{gd} = \exp(-0.083 m_t)$$
 (3.8)

which was developed from data taken from Roed [19].

Inspection of the preceding table suggests that reasonable values for groundshine shielding factors for normal activity (indoor deposits half those outside) are 0.5 for wood frame houses, 0.3 for masonry houses, 0.3 for schools and small office buildings, and 0.1 for basements. For sheltering, the following values are recommended: 0.4 for wood frame houses, 0.2 for masonry houses, 0.2 for schools and small office buildings, and 0.05 for basements.

<u>Normal Activity</u>. Because people continuing normal activities may be in more than one location, the shielding factor for normal activity,  $S_N$ , must be constructed as a weighted sum of the shielding factors for people outdoors,  $S_O$ , in vehicles,  $S_V$ , and indoors in schools and office buildings,  $S_B$ , and in houses,  $S_H$ . Thus,

$$S_{N} = F_{0}S_{0} + F_{B}S_{B} + F_{B}S_{B} + F_{H}S_{H}$$

$$(3.9)$$

where  $F_0$ ,  $F_V$ ,  $F_B$ , and  $F_H$  are the fractions of the population that continue normal activities outdoors, in vehicles, indoors in schools and office buildings, and indoors in houses.

Because differences in dimensions and building materials cause individual house shielding factors to vary significantly, the shielding factor for houses,  $S_{\rm H}$ , must be constructed as a weighted sum over types of houses. Here, for simplicity, only two types of houses will be considered:

- (1) Wood frame houses faced with wood, aluminum, or stucco,
- (2) Concrete block houses, and wood frame houses faced with masonry (e.g., brick).

Because the shielding afforded by a structure changes as a person moves about within the structure (walls afford more shielding than windows, basements more than attics), location within structures will affect the value of structure shielding factors. Only two locations, in basements and not in basements, will be considered here. Lastly, because the shielding afforded by structures does not decrease exposures to radioactive materials that penetrate the structure, ventilation and infiltration will increase the values of structure shielding factors. Accordingly,

$$S_{\rm H} = f_{\rm W}S_{\rm W} + f_{\rm Wb}S_{\rm Wb} + f_{\rm M}S_{\rm M} + f_{\rm Mb}S_{\rm Mb} \tag{3.10}$$

where f is the fraction of all houses that provide the degree of shielding S, the subscript b indicates a basement, and the subscripts W and M respectively denote wood frame houses not faced by masonry and concrete block and masonry faced houses, respectively.

Since most people performing normal activities in houses are not located in basements,  $f_{Wb}$  and  $f_{Mb}$  should be set to zero when Equation 3.10 is used to calculate structure shielding factors for normal activity. Since all houses do not have basements, when this equation is used to calculate house shielding factors for people who have taken shelter, nonzero values should be used for  $f_{Wb}$  and  $f_{Mb}$  that reflect the degree of utilization of available basements.

Values for the fractions  $F_0$ ,  $F_V$ ,  $F_B$ , and  $F_H$  are developed by considering how much time different groups of people spend in different locations. At least three groups of people need to be considered: workers, school age children, and people who spend most of their time at home (i.e., preschool children, homemakers, retired persons, the unemployed). Table 3.21 presents census data for 1986 [2] from which population fractions for these three population groups may be constructed.

Crown	Ago Bongo	Number
<u>Group</u>	<u>Age Range</u>	<u>(millions)</u>
Preschool	< 5	18.1
School	5 - 17	45.1
Adult	18 - 64	148.6
<u>Retired</u>	> 64	29.2
		0/1 0
A11		241.0

Table 3.21. Census Data for Population Groups

In 1986, 109.6 million Americans were employed [2]. Therefore, about 39.0 million Americans (39.0 = 148.6 - 109.6) between the ages of 18 and 64 must either be homemakers or unemployed, which means that about 86.3 million Americans spend most of their time at home (86.3 = 18.1 + 39.0 + 29.2). Thus, workers constitute 45.5% = 100 (109.6/241.0) of the total 1986 population, school age children 18.7% = 100 (45.1/241.0), and homebodies 35.8% = 100 = (86.3/241.0).

Table 3.22 presents plausible estimates of the number of hours in a day on weekdays and weekends during winter and during the rest of the year that individuals in each of the three population groups defined above spend sleeping (N), indoors in houses (I), indoors in schools and office buildings (B), in vehicles (V), and outdoors (O).

Group	Season	N	<u>Wee</u> <u>I</u>	<u>kda</u> <u>B</u>	<u>ys</u> V	<u>0</u>	<u>N</u>	<u>Wee</u> I	<u>ken</u> <u>B</u>	<u>ids</u>	<u>0</u>
Workers	(R) Not Winter	8	6	8	1	1	8	9	0	2	5
	(W) Winter	8	6	8	1	1	8	13	0	1	2
School Children	(R) Not Winter	8	5	4	1	6	8	7	0	2	7
	(W) Winter	8	7	6	1	2	8	12	0	1	3
Homebodies	(R) Not Winter	8	12	0	2	2	8	9	0	2	5
	(W) Winter	8	13	0	2	1	8	13	0	1	2

Table 3.22. Estimates of Time Spent in Different Locations by Population Groups

The fraction of the time that the general population spends in houses, in schools or office buildings, in vehicles, or outdoors is now given by

$$F_{t} = \frac{1}{24} \{ 0.75[(F_{1})(h_{1R}) + (F_{2})(h_{2R}) + (F_{3})(h_{3R})] + 0.25[(F_{1})(h_{1W}) + (F_{2})(h_{2W}) + (F_{3})(h_{3W})] \}$$
(3.8)

where  $F_1 = 0.455$ ,  $F_2 = 0.187$ , and  $F_3 = 0.358$ ; the subscripts 1, 2, and 3 denote workers, school children, and homebodies; and the subscripts R and W denote "not winter" (that is spring, summer, and fall) and "winter." Substitution of numbers from Table 3.22 yields the values in Table 3.23 for the fractions of time spent by the general population in houses, in schools and offices, in vehicles, and outdoors.

Table 3.23. Time Fractions by Locations for the General Population

<u>Population</u>	<u>Location</u>	<u>Weekday</u>	<u>Weekend</u>	<u>Total</u>
A11	Houses	0.67	0.74	0.69
	Buildings	0.19	0.0	0.14
	Vehicles	0.057	0.073	0.06
	Outdoors	0.084	0.19	0.11

Robinson and Converse [20] have developed values for fractions of the time spent in houses, buildings, vehicles, and outdoors by adults less than 65 years old. Since adults less than 65 years old are comprised of 109.6 million workers plus the 39.0 million adult homebodies, the following equation can be used to develop values for time fractions for these adults to compare to the results of Robinson and Converse,

$$F_{t} = \frac{1}{24} \{ 0.75[(F_{1A})(h_{1R}) + (F_{3A})(h_{3R})] + 0.25[(F_{1A})(h_{1W}) + (F_{3A})(h_{3W})] \}$$
(3.9)

where  $F_{1A} = 0.74 = 109.6/148.6$  and  $F_{3A} = 0.26 = 39.0/148.6$  are the fractions of the adult population that are workers less than 65 years old and homebodies less than 65 years old. Table 3.24 presents time fractions for adults less than 65 years old and compares the values for total time to those of Ref. [20].

Table 3.24. Time Fractions by Location for Working Adults

<u>Population</u>	<u>Location</u>	<u>Weekday</u>	Weekend	<u>Total</u>	<u>Total R&amp;C</u>
Adults < 65	Houses	0.65	0.75	0.68	0.69
	Buildings	0.247	0.0	0.18	0.20
	Vehicles	0.053	0.073	0.06	0.05
	Outdoors	0.05	0.177	0.09	0.06

The good agreement in this table between the calculated results and those of Robinson and Converse suggests that the estimates of hours spent in different locations that were presented in Table 3.22 are reasonable. Thus, the following time fractions for the general population are recommended for use in MACCS: Houses = 0.7, Schools and Office Buildings = 0.15, Vehicles = 0.05, and Outdoors = 0.1.

1983 data on new detached housing (i.e., not apartments) has been published by the FHA [21] and 1980 data on existing housing (single and multiunit structures) have been published by the Department of Commerce [22]. If, as was done by Aldrich [8], it is assumed that the characteristics of new detached housing in a state or metropolitan area applies to all detached houses in that state or area and that most multiunit structures have basements and masonry walls (brick faced or concrete block), then the following formula can be used to estimate the percentage of housing units in a state or metropolitan area that have basements or are constructed with masonry walls:

X = ( houses)(fraction new with X) + ( apartments) (3.10)

where X is either basements or masonry walls. Table 3.25 presents the FHA [21] and Department of Commerce [22] data needed by Equation 3.10 and the percent masonry housing and percent basements at the five NUREG-1150 sites as calculated using Equation 3.10 and as developed using 1970 and 1971 data either by the Reactor Safety Study [23] or by Aldrich [8].

		<u>% Units at</u>	t Address	<u> </u>	<u>sonry</u>			&	Base	ement	<u>s</u>
		one		FHA		RSS		FHA		A1	d
<u>Site</u>	<u>State/City</u>	[22]	<u>&gt; one</u>	[21]	<u>Calc</u>	[23]	<u>Ch</u>	[21	] <u>Ca</u> ]	<u>Lc [8</u>	<u>] Ch</u>
	WI	76	24	16	36	<20		81	86	90	
Zion	Chicago	46	54		61		50				85
	IL	64	36	15	46	40-60		43	64	77	
GG	MI	82	18	56	64	40-60	60	0	18	5	5
PB	PA	77	23	41	55	60-80	55	87	90	89	90
Surry	VA	79	21	14	32	40-60	35	41	53	42	45
Seq	TN	80	20	50	60	40-60	55	12	30	28	30
Stud	- Grand Gulf, Hy [23], Calc Lee (recommen	= as calc	ulated wit								

Table 3.25. Regional Building Data

Shielding Factors for Normal Activity and for Sheltering. Values for all of the parameters in Equations 3 and 4 have now been selected. Therefore, parameter values can be calculated for persons who contine normal activity (N) and for persons who actively take shelter (S). Values for three shielding factors, cloudshine (C), groundshine (G), and inhalation/skin (I), are calculated for each activity (normal activity and sheltering). For each shielding factor, three values, an upper bound (H), a best estimate (B), and a lower bound (L), are calculated. Because housing stock varies by location, values are calculated for each NUREG-1150 reactor site (Zion, Grand Gulf, Peach Bottom, Surry, and Sequoyah).

Upper and lower bounds are estimated by assuming that the accident occurs at an unfavorable time (after school during the rush hours on a summer weekday) and at a favorable time (during school hours on a winter weekday). For the summer weekday after school during the rush period (the unfavorable upper bound situation), it is assumed that that school children are now outdoors and most office workers are in vehicles commuting to their homes. For the winter weekday with school in session (the favorable lower bound situation), it is assumed that about two-thirds of the population that on average would be outdoors or in vehicles is now indoors in schools or office buildings. These assumptions yield the upper and lower bound values listed in Table 3.26 for the fractions of the general population that are outdoors  $(F_0)$ , in vehicles  $(F_V)$ , in buildings  $(F_B)$ , and in houses  $(F_H)$ .

Τέ	able 3.	26.	Upper an Populat:			s for
Sce	enario_		<u></u>	<u></u> V	<u></u>	<u></u> H
	Bound Bound	• •	0.4 0.03	0.15 0.02	0.05 0.3	0.4 0.65

The parameter values used to calculate shielding factors for normal activity and for active sheltering are now presented in Table 3.27 and the resulting site specific average shielding values for normal activity and for active sheltering are presented in Table 3.27. In Table 3.27, the column headers are the parameters defined for Equations 3.9 and 3.10. In Table 3.28, <u>Average</u> indicates the average of the site specific values and is given only when the site specific values were quite similar; <u>NRC</u> indicates the value of the indicated shielding factor used in the first pass NUREG-1150 calculations; and <u>Choice</u> indicates the value recommended on the basis of these calculations. In both tables, the line headers are defined as follows: C = cloudshine, G =groundshine, I = inhalation/skin, N = normal activity, S = active sheltering, H = upper bound, B = control estimate, and L = lower bound. Thus, CNH = cloudshine, normal activity, upper bound and the B that comes next = cloudshine, normal activity, central estimate, and so forth. Table 3.27. Input Data for Calculation of Shielding Factors Using Equations 3.9 and 3.10

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							<u>Peacl</u>	n Boti	<u>tom</u>						
	Fo	s <sub>o</sub>	<sup>г</sup> v	s <sub>v</sub> .	F <sub>B</sub>	s <sub>B</sub>	ғ <sub>н</sub>	f <sub>W</sub>	s <sub>w</sub>	f <sub>Wb</sub>	s <sub>wb</sub>	f <sub>M</sub>	s <sub>m</sub>	f <sub>Mb</sub>	S <sub>Mb</sub>
B L SH B	0.4 0.1 0.03 0.0 0.0 0.0	1.0 1.0 0.0 0.0 0.0	0.15 0.05 0.02 0.0 0.0 0.0		0.05 0.15 0.3 0.2 0.2 0.2		0.4 0.7 0.65 0.8 0.8 0.8	0.45 0.45 0.04 0.04	0.85	0.0 0.0 0.41 0.41	0.0 0.0 0.65 0.55	0.55 0.55 0.05 0.05	0.85 0.75 0.65 0.85 0.75 0.65	0.0 0.0 0.5 0.5	0.0 0.0 0.55 0.45 0.35
L SH B	0.4 0.1 0.03 0.0 0.0 0.0	1.0 0.7 0.2 0.0 0.0 0.0	0.15 0.05 0.02 0.0 0.0 0.0	0.5	0.05 0.15 0.3 0.2 0.2 0.2	0.3 0.1 0.4 0.2	0.4 0.7 0.65 0.8 0.8 0.8	0.45 0.45 0.45 0.04 0.04 0.04	0.5 0.3 0.5 0.4	0.41	0.05	0.55 0.55 0.55 0.05 0.05 0.05	0.3 0.15 0.4 0.2	0.0 0.0 0.5 0.5 0.5	0.0 0.0 0.08 0.05 0.02
L SH B	0.4 0.1 0.03 0.0 0.0 0.0	1.0 1.0 0.0 0.0 0.0	0.15 0.05 0.02 0.0 0.0 0.0	1.0	0.05 0.15 0.3 0.2 0.2 0.2		0.4 0.7 0.65 0.8 0.8 0.8	0.45 0.45 0.04 0.04 0.04	0.4 0.1 0.4 0.2	0.0 0.0 0.41 0.41 0.41	0.2	0.55 0.55 0.55 0.05 0.05 0.05	0.4 0.1 0.4 0.2	0.0 0.0 0.5 0.5 0.5	0.0 0.0 0.4 0.2 0.1

#### Surry

	Fo	s <sub>o</sub>	г <sub>v</sub>	.s <sub>v</sub> .	FB	s <sub>b</sub>	<sup>F</sup> н	fw	s <sub>w</sub>	f <sub>Wb</sub>	s <sub>wb</sub>	f <sub>M</sub>	s <sub>m</sub>	f <sub>Mb</sub>	s <sub>Mb</sub>
CNH	0.4	1.0	0.15	1.0	0.05	0.5	0.4	0.65	0.95	0.0	0.0	0.35	0.85	0.0	0.0
В	0.1	1.0	0.05	1.0	0.15	0.4	0.7	0.65	0.85	0.0	0.0	0.35	0.75	0.0	0.0
$\mathbf{L}$	0.03	1.0	0.02	1.0	0.3	0.3	0.65	0.65	0.75	0.0	0.0	0.35	0.65	0.0	0.0
SH	0.0	0.0	0.0	0.0	0.2	0.5	0.8	0.36	0.95	0.29	0.65	0.19	0.85	0.16	0.55
В	0.0	0.0	0.0	0.0	0.2	0.4	0.8	0.36	0.85	0.29	0.55	0.19	0.75	0.16	0.45
L	0.0	0.0	0.0	0.0	0.2	0.3	0.8	0.36	0.75	0.29	0.45	0.19	0.65	0.16	0.35
GNH	0.4	1.0	0.15	0.7	0.05	0.5	0.4	0.65	0.6	0.0	0.0	0.35	0.5	0.0	0.0
В	0.1	0.7	0.05	0.5	0.15	0.3	0.7	0.65	0.5	0.0	0.0	0.35	0.3	0.0	0.0
L	0.03	0.2	0.02	0.2	0.3	0.1	0.65	0.65	0.3	0.0	0.0	0.35	0.15	0.0	0.0
SH	0.0	0.0	0.0	0.0	0.2	0.4	0.8	0.36	0.5	0.29	0.08	0.19	0.4	0.16	0.08
В	0.0	0.0	0.0	0.0	0.2	0.2	0.8	0.36	0.4	0.29	0.05	0.19	0.2	0.16	0.05
L	0.0	0.0	0.0	0.0	0.2	0.01	0.8	0.36	0.2	0.29	0.02	0.19	0.05	0.16	0.02
INH	0.4	1.0	0.15	1.0	0.05	1.0	0.4	0.65	1.0	0.0	0.0	0.35	1.0	0.0	0.0
В	0.1	1.0	0.05	1.0	0.15	0.4	0.7	0.65	0.4	0.0	0.0	0.35	0.4	0.0	0.0
L	0.03	1.0	0.02	0.9	0.3	0.1	0.65	0.65	0.1	0.0	0.0	0.35	0.1	0.0	0.0
SH	0.0	0.0	0.0	0.0	0.2	0.4	0.8	0.36	0.4	0.29	0.4	0.19	0.4	0.16	0.4
В	0.0	0.0	0.0	0.0	0.2	0.2	0.8	0.36	0.2	0.29	0.2	0.19	0.2	0.16	0.2
$\mathbf{L}$	0.0	0.0	0.0	0.0	0.2	0.1	0.8	0.36	0.1	0.29	0.1	0.19	0.1	0.16	0.1

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Table 3.27. (Continued)

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	Fo	s <sub>o</sub>	<sup>F</sup> v	s <sub>v</sub>	<sup>г</sup> в	s <sub>B</sub>	F <sub>H</sub>	f <sub>W</sub>	s <sub>w</sub>	f <sub>Wb</sub>	s <sub>wb</sub>	f <sub>M</sub>	s <sub>m</sub>	f <sub>Mb</sub>	s <sub>Mb</sub>
CNH	0.4	1.0	0.15												
В	0.1	1.0	0.05	1.0	0.15	0.4	0.7	0.5	0.85	0.0	0.0	0.5	0.75	0.0	0.0
L	0.03	1.0	0.02	1.0	0.3	0.3	0.65	0.5	0.75	0.0	0.0	0.5	0.65	0.0	0.0
SH	0.0	0.0	0.0								0.65				
В	0.0	0.0	0.0	0.0							0.55				
	0.0		0.0								0.45				
_			-		·										
GNH	0.4	1.0	0.15	0.7	0.05	0.5	0.4	0.5	0.6	0.0	0.0	0.5	0.5	0.0	0.0
В	0.1	0.7	0.05	0.5	0.15	0.3	0.7	0.5	0.5	0.0	0.0	0.5 ;	0.3	0.0	0.0
L	0.03	0.2	0.02	0.2	0.3	0.1	0.65	0.5	0.3	0.0	0.0	0.5	0.15	0.0	0.0
SH	0.0	0.0	0.0								0.08				
В	0.0	0.0	0.0	0.0							0.05				
$\mathbf{L}$	0.0	0.0	0.0								0.02				
										-		•			
INH	0.4	1.0	0.15	1.0	0.05	1.0	0.4	0.5	1.0	0.0	0.0	0.5	1.0	0.0	0.0
В	0.1	1.0	0.05	1.0	0.15	0.4	0.7	0.5	0.4	0.0	0.0	0.5	0.4	0.0	0.0
$\mathbf{L}$	0.03	1.0	0.02												
	0.0										0.4				
		0.0	0.0	0.0	0.2	0.2	0.8	0.08	0.2	0.42	0.2	0.08	0.2	0.42	0.2
		0.0	0.0	0.0	0.2	0.1	0.8	0.08	0.1	0.42	0.1	0.08	0.1	0.42	0.1
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<u>Zion</u>

# Grand Gulf

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		Fo	s <sub>o</sub>	Fv	s <sub>v</sub>	F <sub>B</sub>	s <sub>B</sub>	<sup>F</sup> н	f <sub>W</sub>	S <sub>W</sub>	f <sub>Wb</sub>	s <sub>wb.</sub>	f <sub>M</sub>	s <sub>M</sub>	f <sub>Mb</sub>	s <sub>Mb</sub>
(	CNH	0.4	1.0	0.15	1.0	0.05	0.5	0.4	0.4	0.95	0.0	0.0	0.6	0.85	0.0	0.0
	В	0.1	1.0	0.05	1.0	0.15	0.4	0.7	0.4	0.85	0.0	0.0	0.6	0.75	0.0	0.0
	$\mathbf{L}$	0.03	1.0	0.02	1.0	0.3	0.3	0.65	0.4	0.75	0.0	0.0	0.6	0.65	0.0	0.0
	SH	0.0	0.0	0.0	0.0	0.2	0.5	0.8	0.38	0.95	0.02	0.65	0.57	0.85	0.03	0.55
	В	0.0	0.0	0.0	0.0	0.2	0.4	0.8	0.38	0.85	0.02	0.55	0.57	0.75	0.03	0.45
	L	0.0	0.0	0.0	0.0	0.2	0.3	0.8	0.38	0.75	0.02	0.45	0.57	0.65	0.03	0.35
(	GNH	0.4	1.0	0.15	0.7	0.05	0.5	0.4	0.4	.0.6	0.0	0.0	0.6	0.5	0.0	0.0
	В	0.1	0.7	0.05	0.5	0.15	0.3	0.7	0.4	0.5	0.0	0.0	0.6	0.3	0.0	0.0
			0.2	0.02	0.2	0.3	0.1	0.65	0.4	0.3	0.0	0.0	0.6	0.15	0.0	0.0
	SH	0.0	0.0	0.0	0.0	0.2	0.4	.0.8	0.38	0.5	0.02	0.08	0.57	0.4	0.03	0.08
	В	0.0	0.0	0.0	0.0	0.2	0.2	0.8	0.38	0.4	0.02	0.05	0.57	0.2	0.03	0.05
	L	0.0	0.0	0.0	0.0	0.2	0.01	0.8	0.38	0.2	0.02	0.02	0.57	0.05	0.03	0.02
	INH	0.4	1.0	0.15	1.0	0.05	1.0	0.4	0.4	1.0	0.0	0.0	0.6	1.0	0.0	0.0
•	В	0.1	1.0	0.05	1.0	0.15	0.4	0.7	0.4	0.4	0.0	0.0	0.6	0.4	0.0	0.0
	L	0.03	1.0	0.02	0.9	0.3	0.1	0.65	0.4	0.1	0.0	0.0	0.6	0.1	0.0	0.0
	SH	0.0	0.0	0.0	0.0	0.2	0.4	0.8	0.38	0.4	0.02	0.4	0.57	0.4	0.03	0.4
			0.0	0.0	0.0	0.2	0.2	0.8	0.38	0.2	0.02	0.2	0.57	0.2	0.03	0.2
	L	0.0			0.0											

# <u>Sequoyah</u>

	Fo	s <sub>o</sub>	Fv	s <sub>v</sub>	<sup>г</sup> в	s <sub>B</sub>	<sup>F</sup> Н	f <sub>W</sub>	s <sub>w</sub>	$f_{Wb}$	s <sub>wb</sub>	f <sub>M</sub>	s <sub>m</sub>	f <sub>Mb</sub>	s <sub>Mb</sub>
CNH	0.4	1.0	0.15	1.0	0.05	0.5	0.4	0.45	0.95	0.0	0.0	0.55	0.85	0.0	0.0
В	0.1	1.0	0.05	1.0	0.15	0.4	0.7	0.45	0.85	0.0	0.0	0.55	0.75	0.0	0.0
$\mathbf{L}$	0.03	1.0	0.02	1.0	0.3	0.3	0.65	0.45	0.75	0.0	0.0	0.55	0.65	0.0	0.0
SH	0.0	0.0	0.0	0.0	0.2	0.5	0.8	0.31	0.95	0.14	0.65	0.38	0.85	0.17	0.55
В	0.0	0.0	0.0	0.0	0.2	0.4	0.8	0.31	0.85	0.14	0.55	0.38	0.75	0.17	0.45
L	0.0	0.0	0.0	0.0	0.2	0.3	0.8	0.31	0.75	0.14	0.45	0.38	0.65	0.17	0.35
GNH	0.4	1.0	0.15	0.7	0.05	0.5	0.4	0.45	0.6	0.0	0.0	0.55	0.5	0.0	0.0
В	0.1	0.7	0.05	0.5	0.15	0.3	0.7	0.45	0.5	0.0	0.0	0.55	0.3	0.0	0.0
$\mathbf{L}$	0.03	0.2	0.02	0.2	0.3	0.1	0.65	0.45	0.3	0.0	0.0	0.55	0.15	0.0	0.0
SH	0.0	0.0	0.0	0.0	0.2	0.4	0.8	0.31	0.5	0.14	0.08	0.38	0.4	0.17	0.08
В	0.0	0.0	0.0	0.0	0.2	0.2	0.8	0.31	0.4	0.14	0.05	0.38	0.2	0.17	0.05
L	0.0	0.0	0.0	0.0	0.2	0.01	0.8	0.31	0.2	0.14	0.02	0.38	0.05	0.17	0.02
				•											
INH	0.4	1.0	0.15	1.0	0.05	1.0	0.4	0.45	1.0	0.0	0.0	0.55	1.0	0.0	0.0
В	0.1	1.0	0.05	1.0	0.15	0.4	0.7	0.45	0.4	0.0	0.0	0.55	0.4	0.0	0.0
L	0.03	1.0	0.02	0.9	0.3	0.1	0.65	0.45	0.1	0.0	0.0	0.55	0.1	0.0	0.0
SH	0.0	0.0	0.0	0.0	0.2	0.4	0.8	0.31	0.4	0.14	0.4	0.38	0.4	0.17	0.4
В	0.0	0.0	0.0	0.0	0.2	0.2	0.8	0.31	0.2	0.14	0.2	0.38	0.2	0.17	0.2
L	0.0	0.0	0.0	0.0	0.2	0.1	0.8	0.31	0.1	0.14	0.1	0.38	0.1	0.17	0.1

# Table 3.28. Recommended Shielding Factor Values

	Zion	Grand Gulf	Peach Bottom	Surry	Sequoyah	Average	NRC	Choice
CNH	0.94	0.93	0.93	0.94	0.93	0.93		0.95
B	0.77	0.76	0.77	0.78	0.77	0.77	0.75	0.75
L	0.59	0.59	0.59	0.60	0.59	0.59		0.60
SH	0.62	0.80	0.60	0.72	0.74			0.80
B	0.52	0.70	0.50	0.62	0.64			
L	0.42	0.60	0.40	0.52	0.54			0.40
GNH	0.75	0.75	0.75	0.76	0.75	0.75		0.75
В	0.42	0.41	0.41	0.44	0.41	0.42	0.33	0.40
L	0.19	0.18	0.18	0.20	0.18	0.19		0.20
SH	0.19	0.42	0.17	0.31	0.35			0.35
B	0.11	0.25	0.10	0.20	0.21			
Ĺ	0.03	0.09	0.02	0.07	0.07			0.02
INH	1.00	1.00	1.00	1.00	1.00	1.00		1.00
В	0.49	0.49	0.49	0.49	0.49	0.49	0.75	0.50
L	0.14	0.14	0.14	0.14	0.14	0.14		0.15
SH	0.40	0.40	0.40	0.40	0.40	0.40		0.40
В	0.20	0.20	0.20	0.20	0.20	0.20		0.20
Ĺ	0.10	0.10	0.10	0.10	0.10	0.10		0.10

#### REFERENCES

- [1] R. M. Ostmeyer and J. C. Helton, <u>Exposure Pathways Models for Accidental Radionuclide Releases</u>, NUREG/CR-4184, Sandia National Laboratories, Albuquerque, NM, p. 33, draft available. (a) p. B-17, (b) p. B-13, (c) p. B-23, (d) p. B-22, (e) p. B-21, (f) p. B-10, (g) p. B-16, (h) p. B-11.
- [2] <u>Statistical Abstract of the United States</u>, 108th Edition, 1988, summary insert.
- [3] J. Alzona et al., Atmos. Environment, Vol. 13, No. 55 (1979).
- [4] A. F. Cohen and B. L. Cohen, <u>Infiltration of Particulate Matter into</u> <u>Buildings</u>, NUREG/CR-1151, Sandia National Laboratories, Albuquerque, NM, November 1979.
- [5] J. Roed and R. J. Cannell, <u>Radiation Protection Dosimetry</u>, Vol. 21, No. 107 (1987).

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- [6] H. D. Brenk and H. de Witt, <u>Radiation Protection Dosimetry</u>, Vol. 21, No. 117 (1987).
- [7] G. C. Christensen and R. Mustonen, <u>Radiation Protection Dosimetry</u>, Vol. 21, No. 125 (1987).
- [8] D. C. Aldrich and D. M. Ericson, <u>Public Protection Strategies in the</u> <u>Event of a Nuclear Reactor Accident: Multicompartment Ventilation Model</u> <u>for Shelters</u>, SAND77-1555, Sandia National Laboratories, Albuquerque, NM, January 1978.
- [9] Office of Civil Defense, Shelter Design and Analysis, Vol. 1, Fallout Radiation Shielding, TR-20-(Vol. 1), Department of Defense, 1968.
- [10] P. H. Jensen, <u>Shielding Factors for Gamma Radiation from Activity</u> <u>Deposited on Structures and Ground Surfaces</u>, Riso National Laboratory, Riso-M-2270, DK-4000 Roskilde, Denmark, 1982.
- [11] P. Jacob and R. Meckbach, <u>Radiation Protection Dosimetry</u>, Vol. 21, No. 79 (1987).
- [12] M. O. Cohen, <u>Calculations of Dose Rates Arising from Radioactive Fallout</u> <u>Upon an Urban Environment</u>, MR-7027, Mathematical Applications Group, Inc., 1975.
- [13] T. Baumeister, ed., <u>Marks' Handbook for Mechanical Engineers</u>, McGraw-Hill, New York, 1978, pp. 6-7.
- [15] Z. G. Burson, <u>Health Physics</u>, Vol. 16, No. 42 (1974).
- [16] B. Lauridsen and P. H. Jensen, <u>Shielding Factors for Vehicles to Gamma</u> <u>Radiation Deposited on Structures and Ground Surfaces</u>, Riso-M-2339, Riso National Laboratory, DK-4000 Roskilde, Denmark, 1982.

- [17] R. H. Perry and C. H. Chilton, <u>Chemical Engineers' Handbook</u>, Fifth Edition, McGraw-Hill, New York, 1973, pp. 2-7.
- [18] Z. G. Burson and A. E. Profio, <u>Structure Shielding from Cloud and</u> <u>Fallout Gamma Ray Sources for Assessing the Consequences of Reactor</u> <u>Accidents</u>, EG&G, EGG-1183-1670, 1975.
- [19] J. Roed, "Parameters Used in Consequence Calculations for an Urban Area," <u>Recent Advances in Reactor Accident Consequence Assessment</u>, CSNI Rpt. 145, OECD, Paris, February 1988, p. 103.
- [20] J. P. Robinson and P. E. Converse, <u>Summary of U.S. Time Use Survey</u>, Institute for Social Relations, University of Michigan, Ann Arbor, MI, 1966.
- [21] U.S. Department of Housing and Urban Development, <u>1983 FHA Homes, Data</u> for States and Selected Areas, 1983.
- [22] U.S. Department of Commerce, <u>1980 Census of Housing</u>, <u>General Housing</u> <u>Characteristics</u>, 1982.
- [23] U.S. Nuclear Regulatory Commission, <u>Reactor Safety Study</u>, <u>Appendix VI</u>, <u>Calculation of Reactor Accident Consequences</u>, WASH-1400, October 1975, pp. 11-26.

 $(1,1,2,\dots,n_{n-1}) = \sum_{i=1}^{n-1} (1,1,2,\dots,n_{n-1}) = \sum_{i=1}^{n-1} (1,1$ 

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#### 4. MACCS FOOD PATHWAY INPUT PARAMETERS

## 4.1 Introduction

Within the MACCS code, of the consequences from the ingestion of food contaminated by radionuclides deposited onto farmland following an accidental release are measured. These consequences can be divided into two general categories:

- (1) societal dose received from the ingestion of contaminated food and the health effects from that dose, and
- (2) economic costs from the mitigative actions to limit the dose to some user-defined level of acceptability.

In addition, a further distinction is made within the MACCS code between the dose received via the food pathway from crops being grown at the time of the release (i.e., the growing season submodel) and the dose received subsequent to the current growing season from food grown on land contaminated by the release (i.e., the long-term submodel). This distinction becomes evident in the preparation of the food pathway input parameters. Doses are calculated and mitigative actions determined for each of these submodels.

In general, the following model is used to determine the dose received via the food pathway. The dose received by organ k from the ingestion of nuclide i found in food arising from crop j,  $D_{i,j,k}$ , can be expressed as

$$D_{i,j,k} = GC_i \cdot A \cdot FA_j \cdot TF_{i,j} \cdot DF_{i,k}$$

where

GCi	= ground concentration of nuclide i $(Bq/m^2)$ ,
А	= farmland area $(m^2)$ ,
FAj	= fraction of farmland used to grow crop j (unitless),
<sup>TF</sup> i,j	= transfer factor, i.e., the fraction of deposited material incorporated onto or into the edible portion of crop j and ultimately eaten by man (unitless), and
DF <sub>i,k</sub>	= dose received by organ k from ingested nuclide i $(Sv/Bq)$ .

The resulting dose to organ k from ingested nuclide i becomes

4-1

$$D_{i,k} = GC_i \cdot DF_{i,k} \cdot \sum_j (A \cdot FA_j \cdot TF_{i,j})$$
 (4.1)

Equation 4.1 is used both to project the potential dose for the determination of necessary mitigative actions and to determine the societal health effects resulting from the actual dose received.

The food pathway parameters will be discussed in three major groups. Section 4.1 describes the general parameters to define the food pathway model, i.e., information about the nuclides to be considered and the crop categories to be used. Section 4.2 discusses the components of the transfer factor,  $TF_{i,j}$ , in Equation 4.1. In Section 4.3, the input parameters specifically required in determining the necessary mitigative actions are discussed. The input parameters within each section are presented in alphabetical order for ease of location. Each parameter is described as well as its recommended values. Because there is uncertainty inherent in the derivation of the input parameters will also contain a range of possible parameter values. This range for the input parameters will be enclosed in parentheses or, in some cases, indicated explicitly. The recommended values for each parameter are followed by a discussion of the methodology used and the assumptions made in deriving the values currently recommended.

## 4.2 Food Pathway Definition Input Parameters

Several input parameters are required for the definition of the MACCS food pathway model. The values selected for some of these parameters will determine the dimensions for all subsequent food pathway input parameters.

#### 4.2.1 NFICRP

NFICRP = number of crop categories to be used

The recommended value for NFICRP is 7.

#### Discussion

The recommended crop categories are listed in Table 4.1 with the major crops included within each category.

Pasture	Stored <u>Forage</u>	Grain	Legumes & Nuts	Leafy <u>Green Veg</u>	Roots <u>&amp; Tubers</u>	Other Food
Tascule	rorage	_OIAIII_	<u>a nucs</u>	Gleen veg	<u>a iubers</u>	_ Other Food
Various grasses	Alfalfa Clover Sorghum	Wheat Oats Barley Corn (incl. sweet corn) Sorghum	Soybeans Peanuts Snap beans Dried beans Peas Nuts	Lettuce Cabbage Broccoli Spinach Celery Cauliflower Greens	Potatoes Carrots Beets Sugar Onion	Fruits: Apples Grapes Citrus Fruits: Oranges Grapefruits Lemons Vegetables: Tomatoes Cucumbers Peppers

Several factors were considered in dividing the crops into the seven distinct categories in Table 4.1. The evaluation of the input parameters for the food pathway in the MACCS code tends to be somewhat labor intensive, so the intent was to keep the derivation of input parameters as simple and straightforward as possible.

The first factor considered was the harvesting pattern for the various crop categories. Pasture is the only crop for which harvesting is considered continuous. It is also assumed that all radioactive material deposited onto pastureland during a given growing season will be consumed by grazing animals before the end of that growing season. In addition, it is assumed that the rate at which the pasture is harvested is constant over the entire season. In contrast, harvest is assumed to be a discrete process for all nonpasture crops. This significant difference in harvesting patterns served as the basis for the first major subdivision into crop categories, that is,

- (1) Pasture, and
- (2) Nonpasture crops.

To make an additional distinction between the nonpasture crops, consideration was given to how the edible portion of the nonpasture crops becomes contaminated during deposition. In certain crops, the edible portion is not exposed to the environment, and contamination occurs only by the translocation of the radioactive material deposited onto plant surfaces into the edible portion of the plant. Examples of this type of crop are grains, legumes, nuts, roots, and tubers. For all other nonpasture crops, the edible portion of the plant is directly exposed to the radioactive material during deposition. These crops include stored forage and all fruits and vegetables. By differentiating between nonpasture crops in which the edible portion is directly contaminated and those in which the edible portion is not subject to direct contamination, the crops were then further subdivided into the following categories:

- (1) Pasture
- (2) Nonpasture

Indirect contamination of the edible portion
 (grains, legumes, nuts, roots, and tubers)
Direct contamination of the edible portion
 (stored forage, fruits, and vegetables)

Within each of these broad groups of nonpasture crops, a further distinction can be made when consideration is given to the plant surface characteristics. For all crops, an increased roughness of the plant surfaces directly affects the efficiency with which the plant retains the radioactive material until the time of harvest.

For crops in which the edible portion is not exposed to the environment, an increase in the amount of material retained on the plant surfaces increases the translocation that can occur. The beard structure of grains further enhances the efficiency of the translocation process. The plant surfaces of legumes, nuts, roots, and tubers are similar and characteristically have less surface roughness than the plant surfaces of grains.

For crops in which the edible portion is exposed to the outside environment, an increased roughness in the plant surfaces will increase the amount of material physically retained on those surfaces until the crop is harvested. A distinction was thus made between green leafy vegetables and stored forage, in which the edible portion has significant surface roughness, and all other fruits and vegetables for which the edible portion has a relatively smooth surface or a "rind" that will be removed during preparation.

By considering the differences in the surface roughness of both plants and their edible portions, the crops categories were further refined as follows:

(1)	Pasture
(2)	Nonpasture
	Indirect contamination of the edible portion
	High plant surface roughness
	(grains)
	Low plant surface roughness
	(legumes, nuts, roots, tubers)
	Direct contamination of the edible portion
	High surface roughness of the edible portion
	(stored forage, green leafy vegetables)
	Low surface roughness of the edible portion
	(fruits and vegetables)

Finally, two additional factors were given consideration in arriving at the crop categories currently being used. The first, biological dissimilarity of the edible portion of the plant, led to a distinction between seeds (legumes

and nuts) and roots (roots and tubers). The second factor, crop utilization, gave rise to the distinction being made between stored forage (consumed only by animals) and green leafy vegetables (consumed only by man).

By giving consideration to these distinctions between crop types, the following crop categories evolved:

- (1) Pasture
- (2) Nonpasture Indirect contamination of the edible portion High plant surface roughness (grains) Low plant surface roughness Reproductive plant part (legumes and nuts) Absorptive or energy storing plant part (roots and tubers) Direct contamination of the edible portion High plant surface roughness Consumed only by animals (stored forage) Consumed only by man (green leafy vegetables) Low plant surface roughness (other food)

Of the crop categories, pasture crops and stored forage are eaten by animals that in turn are food for man, but they are not eaten by man directly. On the other hand, green leafy vegetables, roots, tubers, and "other" crops are not consumed by animals, but are consumed directly by man. Grains and legumes and nuts are consumed by both man and animals, which is important in evaluating the input parameters for the food pathway.

- 4.2.2 NFIISO
- NFIISO = number of nuclides for which data will be specified for the food pathway

The recommended value for NFIISO is 6.

#### <u>Discussion</u>

When NFIISO = 6, the recommended food pathway nuclides are Sr-89, Sr-90, Cs-134, Cs-137, I-131, and I-133. It is expected that these radionuclides will dominate the food pathway doses across the entire spectrum of potential reactor accident scenarios [1:40].

#### 4.2.3 NTTRM

The recommended value for NTTRM is 2.

#### **Discussion**

The growing season crop retention model calculates the fraction of the radioactive material deposited onto the surface of growing plants that will be retained following an exponential weathering loss resulting from exposure of the plant to the environment. By using two terms in the growing crop retention model, it is possible to separate the deposited material into the portion that will weather rapidly with a relatively short half-life and the remaining material that will adhere more stubbornly to the plant surfaces and weather more slowly.

The fractions of the material weathering with each pattern and the half-lives associated with each weathering pattern are supplied by the input parameters CTCOEF and CTHALF as described in Section 4.3.

## 4.2.4 TGSBEG and TGSEND

 $TGSBEG_j = day$  of the year marking the start of the growing season for crop j  $TGSEND_j = day$  of the year marking the end of the growing season for crop j

Table 4.10 gives recommended values for TGSBEG; and TGSEND;.

## **Discussion**

Since the fraction of radioactive material deposited directly onto growing crops that remains on the crop at the time of harvest is time dependent, it must be determined when during the growing season the deposition occurred. The elapsed time before harvest,  $T_e$ , is then the difference between the day on which the crop is harvested, TGSEND, and the day on which deposition,  $T_a$ , (i.e., the day on which the accidental release occured). Therefore,

 $T_e = TGSEND - T_a$ 

This elapsed time is used within the MACCS code to determine the amount of radioactive material deposited onto plant surfaces that will be weathered away before the crop is harvested.

The values recommended for TGSBEG and TGSEND are summarized in Table 4.2.

4-6

Crop	<u>TGSBEG</u> j	<u>TGSEND</u> j	(Dates)
Pasture	90	270	(3/31-9/27)
Stored Forage	150	240	(5/30-8/28)
Grains	150	240	
Legumes & Nuts	150	240	
Leafy Green Vegetables	150	240	
Root Vegetables	150	240	
Other Food	150	240	

Table 4.2. Values for TGSBEG and TGSEND

## 4.3 <u>Transfer Factor Component Input Parameters</u>

Calculation of the dose to organ k from nuclide i,  $D_{i,k}$  in Equation 4.1, requires the determination of the transfer factors,  $TF_{i,j}$ , which define the fraction of nuclide i deposited onto cropland used to grow crop j that is incorporated into the edible portion of the crop and ultimately consumed by man.

Figure 4.1 depicts the overall transfer of deposited radionuclides to man as modeled by MACCS. Each transfer path is labeled using the MACCS input parameters that either define the transfer along the path or, as in the case of CTCOEF and CTHALF, calculate within the MACCS code the fraction of the available material transferred at that segment of the pathway. Tables 4.3 to 4.6 give the recommended values.

Two submodels within the MACCS food pathway model describe the transfer of deposited radioactive material to the edible portion of the crop. The first of these, the growing season submodel, describes the transfer of radionuclides deposited directly onto the surfaces of crops growing at the time of the release. The second, the long-term submodel, describes the transfer of radionuclides deposited onto soil that will subsequently enter the food chain via root uptake by plants or by direct ingestion of the contaminated soil by grazing animals. Within each of these submodels, crops are considered to enter the food chain in one of three ways: (1) the crop may be consumed directly by man, (2) it may be consumed by meat-producing animals with the meat in turn being consumed by man, or (3) it may be consumed by milkproducing animals with the milk in turn being consumed by man.

The derivation of values for each of the input parameters depicted in Figure 4.1 is discussed fully in the remainder of this section. These input parameters are considered in alphabetical order.

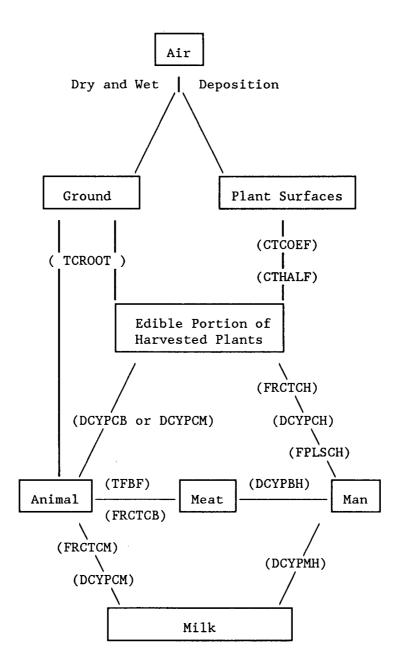


Figure 4.1 Transfer of Released Radionuclides to Man Via the Food Pathway as Depicted in the MACCS Code.

4.3.1 CTCOEF and CTHALF

 $CTCOEF_n = fraction of material weathering with a half-life CTHALF_n$  $CTHALF_n = half-life for the nth exponential term of the weathering model$ 

Crop	Strontium	Cesium	<u>Iodine</u>
Pasture	0.30	0.30	0.30
	(0.23-0.38)	(0.23-0.38)	(0.23-0.38)
Stored Forage	0.20	0.20	0.20
	(0.15-0.24)	(0.15-0.24)	(0.15-0.24)
Grain	0.010	0.050	0.0
	(0.0075-0.013)	(0.038-0.063)	
Legumes	0.0050	0.010	0.0
J	(0.0038-0.0063) (	(0.0075-0.013)	
Green Leafy	0.24	0.24	0.24
Vegetables	(0.18-0.30)	(0.18-0.30)	(0.18-0.30)
Roots & Tubers	0.0006	0.025	0.0
	(0.00045-0.00075)	(0.019-0.031)	
Other Food	0.020	0.020	0.020
	(0.15-0.24)	(0.15-0.24)	(0.15-0.24)

Table 4.3. Recommended Values for CTCOEF1

Table 4.4. Recommended Values for CTHALF1\*

			- <u></u>
<u> </u>	<u>Strontium</u>	Cesium	Iodine
Pasture	1.2096x106	1.2096x106	1.2096x10 <sup>6</sup>
Stored Forage	1.2096x10 <sup>6</sup>	1.2096x106	1.2096x10 <sup>6</sup>
Grain	3.1536x1013	3.1536x1013	1.0
Legumes	3.1536x1013	3.1536x1013	1.0
Green Leafy	$1.2096 \times 10^{6}$	1.2096x10 <sup>6</sup>	1.2096x10 <sup>6</sup>
Vegetables			
Roots & Tubers	$3.1536 \times 10^{13}$	3.1536x10 <sup>13</sup>	1.0
Other Food	1.2096x10 <sup>6</sup>	1.2096x106	1.2096x10 <sup>6</sup>
* Half-lives in seconds: 14 days = $1.2096 \times 10^{6}$ 1 million years = $3.153 \times 10^{13}$ .			

Crop	<u>Strontium</u>	Cesium	Iodine
Pasture	0.076 (0.058-0.096)	0.076 (0.058-0.096)	0.076 (0.058-0.096)
Stored Forage	0.050 (0.038-0.063)	0.050 (0.038-0.063)	0.050 (0.038-0.063)
Grain	0.0	0.0	0.0
Legumes	0.0	0.0	0.0
Green Leafy Vegetables	0.060 (0.046-0.076)	0.060 (0.046-0.076)	0.060 (0.046-0.076)
Roots & Tubers	0.0	0.0	0.0
Other Food	0.050 (0.038-0.063)	0.050 (0.038-0.063)	0.050 (0.038-0.063)

Table 4.5. Recommended Values for  $CTCOEF_2$ 

Table 4.6. Recommended Values for  $\text{CTHALF}_{2}*$ 

Crop	<u>Strontium</u>	<u>Cesium</u>	<u>Iodine</u>
Pasture Stored Forage	4.3200x106 4.3200x106	4.3200x106 4.3200x106	4.3200x106 4.3200x1066
Grain	1.0	1.0	1.0
Legumes	1.0	1.0	1.0
Green Leafy	4.3200x10 <sup>6</sup>	4.3200x10 <sup>6</sup>	4.3200x10 <sup>6</sup>
Vegetables			
Roots & Tubers	1.0	1.0	1.0
Other Food	4.3200x10 <sup>6</sup>	4.3200x10 <sup>6</sup>	4.3200x106

\* Half-lives in seconds: 50 days =  $4.3200 \times 10^6$ .

A uniform sampling distribution is recommended for all CTCOEF and CTHALF. Recall that the numbers within the parentheses represent the possible range of values for each parameter value.

#### **Discussion**

Between the time of deposition of radioactive material onto plant surfaces and the time when the plants are harvested, part of the radioactive material will be lost from the plant surfaces by the following processes (1) weathering, (2) radioactive decay, (3) translocation to interior portions of the plant, and (4) harvesting.

The fraction of the radioactive material initially deposited onto plant surfaces that remains in or on the edible portions of the harvested plant is called the direct deposition transfer factor.

The magnitude of the direct deposition transfer factor depends on the time during the growing season when the accident (deposition) occurs. For crops in which the edible portion is exposed to the outside environment, the losses from weathering and decay will increase with time. Therefore, decreasing the time between deposition and harvest will result in an increase in the direct deposition transfer factor.

It is assumed that pasture undergoes continuous harvesting throughout the growing season. Deposition early in the pasturing season will increase both the time available for nuclide loss from weathering and decay and will also increase the time available for the consumption of contaminated pasture by grazing animals. Since consumption of nuclides by grazing is faster than the removal by either weathering or radioactive decay, the size of the direct deposition transfer factor will increase as the time available for grazing increases.

Weathering has been observed to cause a loss of radioactive material on plant surfaces due to the simultaneous occurrence of several exponential processes. Therefore, the removal of radioactivity from plant surfaces by weathering can be treated as a sum of terms that have the following form:

$$\sum_{n} \{CTCOEF_{n} \cdot EXP[-(ln2/CTHALF_{n})]\}$$

(4.2)

where

 $CTCOEF_n$  = fraction of material deposited per unit area of cultivated field that is removed by weathering with a half-life CTHALF<sub>n</sub>

• • • • • •

In addition,

 $CTCOEF_n = IF \cdot AF_n$ 

where

- IF = interception fraction, i.e., the fraction of the material
   deposited onto the field that is intercepted by crop surfaces
- $AF_n =$  availability fraction, i.e., the fraction of the material deposited onto crop surfaces from which the material is removed by weathering with the half-life CTHALF<sub>n</sub>

and

$$\sum_{n} AF_{n} = 1$$

The edible portion of some crops is not exposed to the outside environment. For these crops, the retention of radioactivity in the edible portions will be determined by translocation of the material from plant surfaces to the edible portion. When this is the case, the weathering model as described above will not be applicable. Instead, an empirical transfer factor is used that has been derived from fallout studies. The empirical transfer factor represents the combined effects of interception, weathering, and translocation to the edible portion of the plant. For convenience, this empirical factor can be input as a value of  $CTCOEF_n$ . Since this empirical value includes the effects of weathering, the exponential part of weathering decay expression associated with this empirical value for  $CTCOEF_n$  is reduced to a value of unity by setting CTHALF<sub>n</sub>, in Equation 4.2, equal to one million years (i.e., 3.1536 x $10^{13}$  seconds). In addition, all but the first term of the weathering equation are set to zero by setting  $CTCOEF_n$  for n > 1 equal to 0.0 and letting the associated value of CTHALF for n > 1 be 1 second. In effect, this transforms the exponential equation into a constant (i.e., CTCOEF1) for those crops in which the edible portion is not exposed to the outside environment.

Finally, the removal of radioactivity is treated explicitly for all crops. It is currently assumed that there are two exponential weathering terms for all crop categories with appropriate adjustments made for the crops in which the edible portion is not exposed to the outside environment. When using a two exponential term weathering model, it becomes necessary to derive two values for each crop/nuclide combination that indicates the CTCOEF<sub>n</sub> for each exponential expression. In addition, each of these terms will also require a value of CTHALF<sub>n</sub> that describes the weathering half-life for that nuclide/crop combination for that component of the weathering process.

The following crops have edible portions that are exposed to the outside environment: pasture, stored forage, green leafy vegetables, and "other food." Given that the "other food" crop category consists primarily of fruits and vegetables in the light of per capita consumption data [2], the entire category will be treated as though the edible portion is exposed to the outside environment. As previously stated,  $CTCOEF_n$  is the product of the interception fraction and the availability fraction. In addition, a half-life will be needed for each of the two exponential terms in the weathering equation. Based on studies by Simmonds and Linsley [3,4], the following values and associated ranges recommended for the interception fraction, availability fraction, and weathering half-lives are as summarized in Table 4.7. The higher interception fractions for pasture and spinach seems to be justified by Vuori's [5] study of fallout data following the Chernobyl accident.

Variable	<u>Value</u>	Range <u>of Values</u>
Interception fraction		
Pasture	0.38	0.29-0.48
Stored Forage	0.25	0.20-0.28
Green Leafy Vegetables	0.30	0.23-0.38
Other Food	0.25	0.20-0.28
Availability fraction	0.80	0.75-0.85
for short-term weathering Availability fraction for long-term weathering	0.20	0.15-0.25
Half-life for short- term weathering (day) Half-life for long-	14.0	13.0-19.0
term weathering (day)	50.0	13.0-19.0

Table 4.7.Interception Fraction, AvailabilityFraction, and Half-Lives

These data lead to the values in Table 4.8 for the variables CTCOEF and CTHALF for all nuclides being treated in the MACCS code. The remaining crop categories (i.e., grains, legumes, and roots and tubers) have edible portions not exposed to the environment, and the values for CTCOEF1 will therefore represent empirical transfer factors as derived from fallout data. To ensure that MACCS will treat these factors as constants, the other related

	<u>Pasture</u>		Green Leafy <u>Vegetables</u>	y Other <u>Food</u>
CTCOEF1 CTCOEF2 CTHALF1 CTHALF2	0.30 0.076 14 d. 50 d.	0.20 0.05 14 d. 50 d.	0.24 0.060 14 d. 50 d.	0.20 0.05 14 d. 14 d.
* These va MACCS co		onverted	to seconds i	for use in the

Table 4.8. Values for CTCOEF and CTHALF\*

input variables take on the following values:

 $CTHALF_1 = 1$  million years (i.e., 3.154 x 10<sup>13</sup> s),  $CTCOEF_2 = 0.0$  $CTHALF_2 = 1$  s

Since the iodine isotopes considered have very short half-lives, it has been assumed that these isotopes will not be found in the edible portion of the plant at the time of harvest. Therefore, the value for CTCOEF1 for both I-131 and I-133 will be 0.0.

In a review of the available data on direct deposition transfer factors to be used for CTCOEF1, Ostmeyer and Helton [1] arrived at empirical direct deposition transfer factors for grain and legumes. Coughtrey and Thorne [6] discussed the analogous empirical direct deposition transfer factor for roots and tubers. For each of these transfer factors, a range of possible values for each element/crop combination was chosen by assuming a 25% uncertainty range.

A summary of these empirical transfer factors and the associated range of possible values is given in Table 4.9.

	Empirical_Transfer Factors		
Crop	Strontium	Cesium	
Grain	0.010 (0.0075-0.013)	0.050 (0.038-0.063)	
Legumes	0.005 (0.0038-0.0063)	0.010 (0.0075-0.013)	
Roots & Tubers	0.00060 (0.00045-0.00075)	0.025 (0.019-0.031)	

Table 4.9. Summary of Empirical Transfer Factors

#### 4.3.2 DCYPBH

 $DCYPBH_i$  = Fraction of radionuclide i present in meat at the time of slaughter that is retained and consumed by man (accounts for losses from both decay and processing).

Table 4.10 shows the recommended values for DCYPBHi.

· · · ·

Table 4.10.	Recommended Values for DCYPBH <sub>1</sub>
Nuclide	DCYPBH
Sr-89	0.77 (0.58-0.96)
Sr-90	1.0
Cs-134	1.0
Cs-137	1.0
I-131	0.18 (0.14-0.23)
I-133	0.0

A uniform sampling distribution is recommended for  $DCYPBH_i$ .

# **Discussion**

DCYPBH<sub>i</sub> can be expressed as

		FINALi
DCYPBHi	=	,
		INITIAL

## where

A value for DCYPBH is obtained for each nuclide i by evaluating the following expression:

$$DCYPBH_{i} = EXP \left\{ -\left[ (1n2/THALF_{i}) \cdot TDELAY \right] \right\}$$

$$(4.3)$$

where

 $THALF_i = radiological half-life of isotope i$ 

TDELAY = delay time between the production and consumption of the food product

The values for DCYPBH<sub>i</sub> were obtained using Equation 4.3 with two assumptions. The first assumption is that 20 days elapse between the time of production and the consumption of meat and meat products as recommended in the Regulatory Guide 1.109 [7: Table E-15]. That delay time seems reasonable for all meat products purchased fresh by the consumer. The second assumption is that there is no significant difference in the delay time between production and consumption of beef, pork, and poultry; therefore, the loss from decay will be basically the same for all meat products.

In finding the range of values for this variable, it was assumed that the estimated value would most probably be accurate to 25%.

#### 4.3.3 DCYPCB and DCYPCM

 $DCYPCB_{i,j}$  and  $DCYPCM_{i,j}$  give the fraction of radionuclide i present in crop j at the time of harvest that is ingested respectively by meat-producing or milk-producing animals.

DCYPCB<sub>i,j</sub> = Transfer factor for meat-producing animals

 $DCYPCM_{i,i} = Transfer factor for milk-producing animals$ 

Because dairy and beef cattle have similar consumption patterns for different crop types, DCYPCB<sub>i,j</sub> and DCYPCM<sub>i,j</sub> have the same values. The recommended values are presented in Tables 4.11 and 4.12. Since there are no processing losses between harvest and consumption by cattle, DCYPCB<sub>i,j</sub> and DCYPCM<sub>i,j</sub> treat only losses resulting from radioactive decay.

A uniform sampling distribution is recommended for DCYPCB<sub>i,j</sub> and DCYPCM<sub>i,j</sub>.

#### **Discussion**

Because  $DCYPCB_{i,j}$  and  $DCYPCM_{i,j}$  have the same values for any nuclide/crop pair, they are both denoted in the following discussion by  $DCYPCA_{i,j}$ .

		Stored		Legumes
<u>luclide</u>	<u>Pasture</u>	<u> </u>	Grains	and Nuts
Sr-89	1.0	0.37	0.20	0.20
		(0.28-0.46)	(0.15-0.25)	(0.15-0.25)
Sr-90	1.0	0.99	0.99	0.99
Cs-134	1.0	0.92	0.85	0.85
		(0.69-1.0)	(0.64-1.0)	(0.64-1.0)
Cs-137	1.0	0.99	0.99	0.99
I-131	1.0	0.063	0.032	0.032
		(0.047-0.079)	(0.024-0.040)	(0.024-0.040)
I-133	1.0	0.0068	0.0034	0.0034
		(0.0051-0.0085)	(0.0025-0.0043)	(0.0025-0.0043)

Table 4.11. Recommended Values for  $\text{DCYPCB}_{i,j}$  and  $\text{DCYPCM}_{i,j}$  for Crops Consumed by Cattle

Table 4.12. Recommended Values for All Nuclides for Crops Not Consumed by Cattle

Nuclide	Leafy Green	Roots	Other
	<u>Vegetables</u>	<u>&amp; Tubers</u>	<u>Food</u>
A11	0.0	0.0	0.0

Thus,

$$DCYPCA_{i,j} = \frac{CONSUMED_{i,j}}{HARVEST_{i,j}}$$

where

- HARVEST<sub>i,j</sub> = concentration (Ci/kg) of radionuclide i in crop j at harvest.

Crops used to feed livestock will generally follow the same storage pattern regardless of whether the animal that consumes the crop is a milk- or beefproducing animal. For this reason, these two variables will have the same value for any nuclide/crop pair.

The values derived are based on the assumption that the consumption patterns for the crops in each crop category are similar from year to year. Three the crop categories have no significant consumption by animals, Leafy Green Vegetables, Roots and Tubers, and Other Food, and therefore are assigned a transfer factor of 0.0.

For pasture, grazing is the method of harvesting, and there is therefore no delay time between harvesting and consumption. Since herds are usually sized to the fields on which they graze, all radionuclides deposited onto the pasture grass are assumed to be consumed by the end of the pasturing season. For this reason, for pasture the value for the ratio of the amount of the nuclide consumed to the amount of the nuclide present at the time of harvest is 1.0 for all nuclides.

It is assumed that stored forage will be used on a continuous basis during the time when the animals are not grazing on pasture. The length of time over which this continuous feeding takes place is the difference between 365 days and the length of the pasturing season (growing season) for pasture. If  $FT_s$  is the time period over which the feeding of stored forage takes place, then letting the length of the growing season for pasture be 180 days (see TGSBEG and TGSEND),  $FT_s = 365 - 180 = 185$  days.

For both grains and legumes, it is assumed that harvest occurs once a year, and the crops will be fed to animals in a continuous manner throughout the year until their next harvest. Accordingly, if the time over which grain and legumes are fed is denoted by  $FT_g$ , then  $FT_g = 365$  days.

For a crop that is not harvested continuously (single harvest time), if an exact delay time (TDELAY) between harvest and consumption can be assigned the transfer factor,  $TF_{i,j}$ , for a given crop j for nuclide i is evaluated as follows:

 $TF_{i,j} = EXP \left\{ -\left[ (1n2/THALF_i) \cdot TDELAY_j \right] \right\}$ (4.4)

where

 $THALF_i$  = radiological decay half-life for nuclide i and

and the second second

 $TDELAY_{j}$  = time delay between harvest and consumption of crop j by animals.

 $TF_{i,j}$  represents the fraction of the radioactive material present in the crop at the time of harvest that remains when the crop is consumed. The losses of radioactive material over that period of time is the result of radioactive decay.

For a crop that is continuously consumed, the transfer factor,  $TF_{i,j}$ , is calculated as the product of the consumption rate for the crop and the integral of the rate of transfer over the entire period of time the crop is being consumed. The transfer factor for a given crop category for a specific nuclide is then calculated using the following expression:

$$TF_{i,j} = CR_j \cdot \int_{0}^{T_j} EXP\{-[(ln2/THALF_i) \cdot t]\} dt$$

where

 $CR_j = consumption rate for crop j (day<sup>-1</sup>)$ THALF<sub>1</sub> = radiological decay half-life for nuclide i T<sub>j</sub> = length of overall period during which crop j is consumed

If it is assumed that consumption takes place at a constant rate over the designated period,  $T_j$ , then  $CR_j = 1/T_j$ , and the expression for the transfer factor becomes

$$TF_{i,j} = DCYPCA_{i,j}$$

$$= \frac{1}{T_j} \cdot \int_{0}^{T_j} EXP \left\{ -\left[ (\ln 2/THALF_i) \cdot t \right] \right\} dt$$

$$= \frac{1 - EXP \left\{ -\left[ (\ln 2/THALF_i) \cdot T_j \right] \right\}}{T_j \cdot (\ln 2/THALF_i)}$$
(4.5)

For the period of consumption,  $T_j$ , the values  $FT_s$  and  $FT_g$  were used. That is,

 $T_{j}$  =  $FT_{s}$  = 185 days for Stored Forage  $= FT_{g} = 365 \text{ days for Grains, Legumes, and Seeds}$ 

The range of possible values in each case was arrived at by assuming that the best estimate values are probably accurate to 25%.

#### 4.3.4 DCYPCH

 $DCYPCH_{i,j}$  = fraction of radionuclide i present in crop j at the time of harvest remains in food at the time of consumption by man (accounts for losses from radioactive decay)

The transfer factor, DCYPCH<sub>i,j</sub>, accounts only for losses of radioactive material attributable to radioactive decay. Losses of material which occurs during the processing of food before it is eaten is accounted for by the transfer factor FPLSCH<sub>i,j</sub>. Table 4.13 summarizes the recommended values of DCYPCH<sub>i,j</sub> for crops consumed by man, and Table 4.14 summarizes the values for crops not consumed by man.

<u> </u>				<u> </u>	
		Legumes	Green Leafy	y Roots	Other
<u>Nuclides</u>	Grains	and Nuts	Vegetables	<u>s &amp; Tubers</u>	Food
Sr-89	0.18	0.18	0.67	0.18	0.21
	(0.14-0.22)	(0.14-0.22)	(0.50-0.84)	) (0.14-0.22)	(0.16-0.26)
Sr-90	0.99	0.99	1.0	0.99	0.99
	(0.97-1.0)	(0.97-1.0)		(0.97-1.0)	(0.97-1.0)
Cs-134	0.84	0.84	0.96	0.84	0.85
		(0.63-1.0)			
Cs-137	0.99	0.99	1.0	0.99	0.99
	(0.77-1.0)	(0.77-1.0)			(0.77-1.0)
I-131	0.0099	0.0099	0.21	0.0099	0.024
		(0.0074-0.012)			
I-133	0.0	0.0	0.0	0.0	0.0

Table 4.13. Recommended Values of DCYPCH<sub>i,j</sub> for Crops Consumed by Man

Table 4.14.		Values for DCYPCH <sub>i,j</sub> ot Consumed by Man
Nuclide	<u>Pasture</u>	Stored Forage
A11	0.0	0.0

The uniform sampling sampling distribution is recommended for DCYPCHi, j.

## **Discussion**

 $DCYPCH_{i,j}$  can be defined as

 $DCYPCH_{i,j} = \frac{INTAKE_{i,j}}{HARVEST_{i,j}}$ 

where

HARVEST<sub>i,j</sub> = concentration (Ci/kg) of radionuclide i in crop j at harvest

For the variable  $DCYPCH_{i,j}$ , it is necessary to determine a value for each crop category and radionuclides considered.

Since neither Pasture nor Stored Forage is consumed directly by man, a value of 0.0 is assigned to the variable DCYPCH for these crop categories over all the nuclides considered.

The values derived by Ostmeyer and Helton [1] were based on the assumption that there was a 14-day delay between harvest and consumption of all crops except grain. Grain was assumed to be put into storage upon harvest and then continuously released for consumption over the course of the year prior to the next harvest.

The revised values were derived by taking a more comprehensive look at the current marketing practices for each crop category. It is acknowledged that processing (canning and freezing) as well as storage will considerably change the delay time from harvest to consumption. A brief discussion follows of the observed practices and the assumptions made for each crop category.

Grains are harvested once a year and placed in storage to be released continuously to produce the edible products. It was assumed that the harvest of any given year would be completely depleted by the time of harvest the following year. This is considered a conservative model for grain usage, since the current stores would indicate that the actual delay time before consumption may well be considerably longer than the assumed delay time. Sweet corn has been included in the grain category to allow using similar transfer factors for the concentration of radionuclides found in the edible portion. This does not disrupt the model for crop usage, since sweet corn represents only 1.5% of the total grains consumed by man. In addition, only 30% of the sweet corn is consumed fresh, and the remaining 70% is processed [2:Table 213]. In effect, processing allows for the same continuous consumption over the year that is used in the model for all grain. It has been further assumed that there is a minimum processing and delivery time of 14 days before the grain products would be available for consumption. The model used for grains was also used for two other categories of crops: (1) Legumes and Nuts and (2) Roots and Tubers. Continuous consumption for crops in these categories is assumed to begin 14 days after the crop is harvested and extends until the next year's harvest is ready for consumption, that is, until 14 days after the next harvest. The total time over which consumption of these crops occurs is therefore 365 days.

Storage and consumption patterns for the crop categories Green Leafy Vegetables and Other Food fall into three broad categories. Some produce is delivered fresh to market and consumed within 14 days. Some produce is placed in refrigerated storage for up to 6 months. Finally, some produce is undergoes additional processing (i.e., freezing, canning, or drying), which significantly increases its shelf life. For the processed produce, it has been assumed that the processing and delivery to the consumer will require 14 days and that the supply of processed products will be consumed continuously over the course of the next year.

By surveying agricultural data, it can be shown that 70% of the Green Leafy Vegetables will be consumed fresh after approximately a 14-day delay to the consumer. Another 25% of the crop will be placed in refrigerated storage and used over the course of six months. The final 5% will undergo additional processing and be used continuously until the time of the next harvest a year later. This information can be found in Ref. [2]: Table 161, p. 218; Table 244, p. 178; Table 205, p. 152; Table 209, p. 154; Table 246, p. 180.

For the Other Food crop category, a review of agricultural data [2: Tables 246, 258, 277, and 295] shows that 5% will be consumed fresh (after 14 days), while 95% undergoes additional processing that allows continuous utilization over the course of the year prior to the next harvest. This information is taken from Ref. [2]: Table 258, p. 189; Table 295, p. 211; Table 277, p. 199; Table 246, p. 180.

The information on consumption patterns for the various crop categories is summarized in Table 4.15. These percentages are used to evaluate a weighted average for the fraction of radionuclide i present in crop j at harvest that will be consumed by man,  $DCYPCH_{i,j}$ . Therefore,  $DCYPCH_{i,j}$  will be derived as follows:

 $DCYPCH_{i,j} = FF_{j} \cdot TFF_{i} + FR_{j} \cdot TFR_{i} + FP_{j} \cdot TFP_{i}, \qquad (4.6)$ 

where

 $FF_j$  = fraction of crop j consumed fresh within 14 days of harvest

- FR<sub>j</sub> = fraction of crop j refrigerated and consumed continuously over a
   6-month time period beginning 14 days after harvest,
- FPj = fraction of crop j processed and continuously consumed over a 1-year time period beginning 14 days after harvest,
- $\text{TFF}_i$  = transfer factor that represents the fraction of radionuclide i present at harvest that would ultimately be consumed by man if the entire crop is consumed as fresh produce
- TFR<sub>i</sub> = transfer factor that represents the fraction of radionuclide i
   present at harvest that would ultimately be consumed by man if the
   entire crop has been refrigerated and then is consumed continuously
   over 6 months
- TFP<sub>i</sub> = transfer factor that represents the fraction of radionuclide i
   present at harvest that would ultimately be consumed by man if the
   entire crop undergoes further processing and then is consumed
   continuously over a period of 1 year

	Fresh (% eaten	Refrigerated (% eaten	Processed (% eaten
Crop	<u>after 14-day delay)</u>	over 6 mo)	<u>over l yr)</u>
Grains	0	0	100
Legumes & Nuts	0	0	100
Green Leafy Vegetables	70	25	5
Roots & Tubers	0	0	100
Other Food	5	0	95

Table 4.15. Consumption Patterns

All transfer factors that are part of Equation 4.5 are used to describe the fraction of radioactive material present in the edible portion of the crop at the time of harvest and retained following radioactive decay. As was noted earlier, the losses from the processing of food are handled by the parameter FPLSCH.

If an exact delay time between harvest and consumption can be assigned, as has been done for  $\text{TFF}_i$ , the fraction of radionuclide i present at harvest that is consumed by man would be calculated as follows:

$$TFF_{i} = EXP \left\{ -\left[ \left( \frac{\ln 2}{THALF_{i}} \right) \cdot TDELAY \right] \right\}$$

$$(4.7)$$

where

THALF<sub>i</sub> = radiological decay half-life for the nuclide i 
$$(day^{-1})$$

TDELAY = time delay between harvest and consumption (day)

If a portion of the crop is stored or preserved for utilization over an extended period, the consumption is considered to be continuous. The transfer factors, TFR and TRP, will be the product of the daily consumption rate of the food and the integral of the rate of transfer over the entire period of time the crop is being consumed. If it is assumed that consumption of the crop occurs at a constant rate over a given time period,  $T_j$ , then the consumption rate for crop j,  $CR_j$ , is

$$CR_i = 1 / T_i (day^{-1})$$

Then the transfer factors TFR and TFP can be calculated using the following equation.

$$TRF_{i,j} = TRP_{i,j} = CR_j \int_{T_1}^{T_2} EXP\{-[(ln2/THALF_i \cdot t]) dt \}$$

$$= \frac{1}{T_i} \cdot \int_{T_1}^{T_2} EXP\{-[(ln2/THALF_i) \cdot t]\} dt$$

$$= \frac{\text{THALF}_{i}}{\text{T}_{j} \cdot \text{In2}} \cdot \left[ \text{EXP} \left( -\frac{\ln 2}{\text{THALF}_{i}} \cdot \text{T}_{2} \right) - \text{EXP} \left( -\frac{\ln 2}{\text{THALF}_{i}} \cdot \text{T}_{1} \right) \right] (4.8)$$

where

$$\Gamma_i$$
 = length of the consumption period (day)

CR<sub>j</sub> = consumption rate for crop j (day<sup>-1</sup>) = 
$$\frac{1}{T_j} = \frac{1}{T_2 - T_1}$$

 $THALF_i$  = radiological decay half-life for nuclide i (day)

T<sub>1</sub> = the shortest time after harvest that crop j will be consumed (days)

 $T_2$  = the longest time after harvest that the crop will be consumed (days)

The values of  $T_j$ ,  $T_1$ , and  $T_2$  used for the various consumption patterns are given in Table 4.16.

Time	Foods Consumed Fresh	Foods Refrigerated and Consumed Over 6 Months	Foods Processed and Consumed Over 1 Year
T <sub>1</sub>	0	14	14
T <sub>2</sub>	14	197	379
Tj	14	183	365

Table 4.16. Values for Time Variables

The range of possible values in each case was arrived at by assuming that the best estimate values being used are most probably accurate to within 25% of their actual value.

- 4.3.5 DCYPMH
- $DCYPMH_i$  = fraction of radionuclide i present in milk at the time of production that is retained in the milk until the time of consumption by man (accounts for losses from both radioactive decay and processing)

The recommended values for DCYPMH<sub>i</sub> are as in Table 4.17.

Table 4.17. Recommended Values for DCYPMH<sub>i</sub> <u>Nuclide</u> **DCYPMH** Range of Values Sr-89 0.66 0.50-0.83 Sr-90 1.0 Cs-134 1.0 Cs-137 1.0 I-131 0.28 0.21-0.35 I-133 0.002 0.0015-0.0025

The uniform sampling distribution is recommended for DCYPMH.

## **Discussion**

 $DCYPMH_i$  can be defined as

$$DCYPMH_{i} = \frac{FINAL_{i}}{INITIAL_{i}}$$

where

Values for this variable are found for each nuclide treated by the food pathways model by evaluating the following expression

 $DCYPMH_i = EXP \{-[(1n2/THALF_i) \cdot TDELAY]\}$ 

where

 $THALF_i$  = radiological half-life of nuclide i (days)

TDELAY = delay time between the production and consumption of the dairy product (days)

The values first used for this variable were obtained by the assuming that all milk produced was consumed as fluid. Furthermore, a delay time (TDELAY) of four days was used as recommended in the Regulatory Guide 1.109 [7:Table E-15].

An investigation of the utilization of milk in the United States [2:Table 480] showed that milk products could by divided into three groups according to their shelf-life. These groups, the milk products included in each group, and the percentage of the total amount of milk that is accounted for by each group are shown in Table 4.18.

Since the products with the long shelf-life represent such a small percentage of the total milk produced, it was decided to combine it with those products having an intermediate shelf-life and to consider the entire group as having an intermediate shelf-life.

The derivation of the values for DCYPMH; now takes the form:

$$DCYPMH_{i} = FR_{s} \cdot EXP \left( -\frac{\ln 2}{THALF_{i}} \cdot T_{s} \right) + FR_{1} \cdot EXP \left( -\frac{\ln 2}{THALF_{i}} \cdot T_{1} \right) \quad (4.9)$$

where

- FR<sub>s</sub> = fraction of milk production used in products with a short shelflife
- FR1 = fraction milk production used in products with an intermediate shelf-life (including long shelf-life products)
- $T_s$  = delay time between production of milk and consumption of those products with a short shelf-life (days)
- T<sub>1</sub> = delay between production of milk and consumption of those products with an intermediate shelf-life (days)
- $THALF_i$  = as defined previously (days)

Delay times needed to be established for the two groups. Milk consumed as a fluid accounts for nearly 80% of those products with a short shelf-life. Therefore, milk was assumed to be representative of short-shelf life products. It was found through the Associated Milk Producers that 2 or 3 days are required to get the milk to the shelf, and that a freshness date of at least 2 weeks is applied at the time of packaging, 1 or 2 days following production. Based on this information, the 4-day delay time originally used to calculate DCYPMH seemed somewhat short for this product group. A modified delay time of 7 days was, therefore, used to derive the current values of DCYPMH. Still, it seems likely that even the revised delay time may be too short.

Cheese and butter dominate the product group with intermediate shelf-life (which now also includes canned and dehydrated products). Cheese accounts for

Group	Products	Total <u>Production (%</u> )
Short Shelf-Life	Fluid Milk	
Short Sherr-Life	Cottage Cheese	
	Bulk Condensed Milk	
	Ice Cream	49
Intermediate Shelf-Life	Cheese American	
	Other	
	Butter	49
Long Shelf-Life	Canned Milk	
-	Dry Milk	
	Other Dehydrated Products	2

59% of the milk used for these products, and butter accounts for 37%. After curing for at least 60 days, cheese is given a freshness date of 60 days at the time of packaging. Butter, on the other hand, takes 5 or 6 days to produce, is readily frozen, which greatly enhances its shelf-life, and is given a freshness date of 60 days at the time of packaging. Using this information, it was decided to use value for the delay time for these products of 65 days.

In summary, the data in Table 4.19 were used to determine the value of the variable  $DCYPMH_i$  for each nuclide i using Equation 4.9.

Product Group	Milk Production (%)	<u>Delay Time (Days)*</u>
Short Shelf-Life	50	7
Intermediate Shelf-Life	50	65
* Time from production to	consumption.	

Table 4.19. Consumption Intervals for Milk Products

It has been assumed for the nuclides with relatively long half-lives that the entire amount of radioactivity present at the time of production will in fact be consumed.

The range of possible values for DCYPMH was derived based on the estimate that the actual value would probably lie within 25% of the calculated value.

# 4.3.6 FPLSCH

FPLSCH<sub>i,j</sub> = fraction of radionuclide i present in crop j at harvest that is retained until consumption by man (does not account for losses from radioactive decay, which are handled separately by the parameter DCYPCH)

The recommended values for FPLSCH are summarized in Tables 4.20 and 4.21. A uniform sampling distribution is recommended for FPLSCH.

## **Discussion**

The variable FPLSCH<sub>i,j</sub> can be defined as follows:

$$FPLSCH_{i,j} = \frac{FINAL_{i,j}}{INITIAL_{i,i}}$$

FINAL <sub>i,j</sub> =	concentration (Ci/kg) of radionuclide i in the edible portion of crop j at consumption by man when there are no losses caused by radioactive decay
INITIAL <sub>i,j</sub> =	concentration (Ci/kg) of radionuclide i in the edible portion of crop j at harvest

where

Since neither pasture nor stored forage is consumed by man, each of these crops are assigned a processing retention factor of 0.0 over all nuclides. Processing loss factors for crops consumed by man were developed using data compiled by Boone et al. [8].

Nuclide	Grains	•	Green Leafy <u>Vegetables</u>	Other Food
Sr-89			0.5 (0.38-0.63)	
Sr-90			0.5 (0.38-0.63)	
Cs-134			0.5 (0.38-0.63)	
Cs-137			0.5 (0.38-0.63)	
I-131			0.5 (0.38-0.63)	
I-133			0.5 (0.38-0.63)	

Table 4.20. Recommended Values for  $FPLSCH_{i,j}$  for Crops Consumed by Man

Table 4.21. Recommended Value of FPLSCH<sub>i,j</sub> for Crops Not Consumed by Man

	<u>Pasture</u>	<u>Stored Forage</u>
All nuclides	0.0	0.0

The retention factor for grain is quite low because of the high degree of refinement of grains during the production of the refined products that dominate the per capita consumption of grain. This retention factor may be expected to increase as eating patterns change toward whole grain products as witnessed recently.

On the other hand, in the processing of legumes and nuts, the edible portion is consumed without such refinement. Therefore, all crops in this category except snap beans have a retention factor of 1.0. The edible pod of the snap bean is exposed to the environment during the growing season and will therefore be contaminated directly, and the bean itself will be contaminated by translocation. According to Boone et al. [10], only 50% of the radioactive material present at harvest will be retained in the bean after processing. Snap bean consumption accounts for approximately 40% of the human intake from this crop category. A weighted averaging approach was used in arriving at the overall retention factor for the legume and nut crops. That is, FPLSCH = (0.60)(1.0) + (0.40)(0.50) = 0.80

For green leafy vegetables, translocation is not an important factor in the contamination resulting from direct deposition. Furthermore, half the radioactive material present on the edible portions of green leafy vegetables will be removed during washing and cooking.

Part of the contamination of the roots and tubers is from direct contact with contaminated soil, but translocation transfers an even greater amount of radioactive material from above-ground plant parts into the roots. Washing and peeling will remove the material in the skin of these vegetables, but processing will not decrease the amount of translocated material.

The Other Food category consists primarily of a wide variety of fruits and vegetables that can be grouped into three broad subcategories, each of which has a characteristic retention factor for radioactivity after processing:

- Foods that have a rind or peel not considered to be edible and therefore removed before consumption. Examples are citrus fruits and melons. The contamination in the edible portion of the plant consists of material translocated to the flesh of the fruit. Retention fraction = 0.80
- (2) Fruits and vegetables that are contaminated by direct deposition and also contain radioactive material translocated to the interior portion of the fruit. The entire harvested portion of the crop is edible (for example, apples, pears, etc.). Since the skin is smooth and the fruit will be washed before consumption, much of the radioactive material present at the time of harvest will be removed. Retention fraction = 0.50
- (3) Tomatoes are especially susceptible to translocation to all edible portions, including the seeds. Therefore, even though their skin is smooth and easily washed, the retention fraction is greater than for the fruits and vegetables in subgroup 2. Retention fraction = 0.80

Approximately 70% of the crops in this category have a retention factor of 0.80, while the other 30% have a retention factor of 0.50. By weighting these two groups appropriately, an overall retention factor can be calculated as FPLSCH = 0.70 (0.80) + 0.30 (0.50) = 0.7.

The ranges of values were found by assuming that the calculated value is most probably correct to 25%.

4.3.7 FRCTCB, FRCTCH, FRCTCM

 $FRCTCB_{i}$  = fraction of crop j consumed by meat-producing animals,

 $FRCTCH_{j}$  = fraction of crop j consumed by man,

 $FRCTCM_{j}$  = fraction of crop j consumed by milk-producing animals.

The recommended values for FRCTCH, FRCTCM, and FRCTCB are as given in Table 4.22. When sampling is to be done over the range of possible values, it is recommended that a uniform sampling distribution be assumed.

Crop	FRCTCH	FRCTCM	FRCTCB
Pasture	0.0	0.10 (0.075-0.125)	0.90 (0.875-0.925)
Stored Forage	0.0	0.13 (0.098-0.16)	0.87 (0.84-0.902)
Grain	0.35 (0.26-0.44)	0.040 (0.030-0.050)	0.61 (0.51-0.71)
Legumes and Nuts	0.24 (0.18-0.30)	0.046 (0.035-0.058)	0.714 (0.642-0.785)
Green Leafy Veg.	1.0	0.0	0.0
Roots & Tubers	1.0	0.0	0.0
Other Food	1.0	0.0	0.0

Table 4.22. Values for FRCTCH, FRCTCM, and FRCTCB

The recommended values were derived by analyzing current agricultural statistics [2] and using the summary of livestock ingestion rates as summarized by Boone et al. [8] as adapted from Ng [9]. A partial list of the reference tables [1] used to compile the data for the various crops and animals is given in Table 4.23. Since the health effects in MACCS are considered in the societal sense, the products exported are also included in defining the amounts of each crop category consumed by man and by animals. With the exception of soybeans, it has been assumed that utilization of the part of the crop exported follows the same pattern as domestic utilization. On the other hand, the utilization pattern for domestic use versus the

	Domes	tic	Exp	ort		
Crop	Food (1bs)	Feed (1bs)	Food (1bs)	Feed (1bs)	<u>Ref</u> Table	<u> </u>
Wheat	3.75x1010	2.70x10 <sup>10</sup>	4.87x10 <sup>10</sup>	3.53x10 <sup>10</sup>	5	4
Rye	1.96x10 <sup>8</sup>	8.40x10 <sup>8</sup>	1.06x10 <sup>7</sup>	4.54x10 <sup>7</sup>	19	16
Barley	8.35x10 <sup>9</sup>	1.33x1010	1.70x10 <sup>9</sup>	2.66x10 <sup>9</sup>	58	44
Sorghum	5.60x10 <sup>8</sup>	2.18x1010	3.50x10 <sup>8</sup>	1.37x1010	67	51
Oats	2.50x10 <sup>9</sup>	1.49x1010	8.96x10 <sup>6</sup>	5.50x10 <sup>7</sup>	50	39
Rice	5.58x10 <sup>9</sup>	0.0	6.50x10 <sup>9</sup>	0.0	28	20
Corn	2.73x1010	1.09x10 <sup>11</sup>	1.04x1010	4.14x1010	41	31
Sweet Corn	2.89x10 <sup>9</sup>	0.0	0.0	0.0	213	157
Soybeans	7.18x10 <sup>9</sup>	6.46x1010	1.89x10 <sup>10</sup>	3.52x1010	170	127
Peanuts	1.52x10 <sup>9</sup>	5.81x10 <sup>8</sup>	7.26x10 <sup>7</sup>	2.82x10 <sup>7</sup>	160	121
Snap beans	1.27x10 <sup>9</sup>	0.0	0.0	0.0	204	151
Peas	3.65x10 <sup>8</sup>	0.0	0.0	0.0	223	163
Dried beans	1.55x10 <sup>9</sup>	0.0	0.0	0.0	376	255
Nuts	5.19x10 <sup>8</sup>	0.0	0.0	0.0	343	237
					345	237
					348	238
					351	240

Table 4.23. Crop Utilization Patterns

utilization pattern for exported soybeans is significantly different. According to the American Soybean Association the patterns of soybean utilization are as indicated in Table 4.24.

Table	4.24.	Crop	Utilization	
-------	-------	------	-------------	--

Market	<u>Food (%)</u>	<u>Feed (%)</u>
Domestic	10	90
Export	35	65

These utilization patterns for soybeans have been incorporated into Table 4.22, the summary table of crop utilization.

Using the summary data for crop utilization within the general categories of Grains and Legumes & Nuts, overall utilization can be summarized as in Table 4.25.

Table 4.25.	Utilization of Grains,
	Legumes, and Nuts

	1
<u>Food (%)</u>	<u>Feed (%)</u>
35	65
24	76
	35

Boone et al. [8] compiled a summary of the daily consumption rates of various animals for a variety of crops. The rates for cattle, hogs, chickens, and dairy cattle from this summary are given below. In addition, a consumption rate for turkeys has been added, since they are being considered as part of the crop-meat-man pathway. To obtain a daily consumption rate for turkeys, the following assumptions were made:

- (1) Turkeys and chickens have similar biological and metabolic characteristics.
- (2) Similar amounts of feed will produce a similar weight-gain in both types of poultry.
- (3) The diet of both chickens and turkeys are similar in content.

As a result of these assumptions and the use of weight-at-slaughter statistics, it was determined that the daily consumption of a turkey is 2.6 times the daily consumption of a chicken. This factor was then used to determine the daily consumption rate for turkeys of the various crops based on the daily consumption by chickens. An overall summary of the daily consumption rates (lbs/day) is summarized in Table 4.26.

	Cattl	e			
<u> </u>	<u>Dairy</u> 8.55	<u>Beef</u> 8.55	<u>Hogs</u> 0.0	<u>Chickens</u> 0.0	<u>Turkeys</u> 0.0
Нау	14.90	10.80	0.0	0.0	0.0
Corn Silage	5.84	4.54	0.0	0.0	0.0
Sorghum Silage	1.33	0,966	0.0	0.0	0.0
Wheat	0.0509	0.0375	0.0675	0.00126	0.00328
Oats	0.131	0.0970	0.175	0.00328	0.00854
Rye	0.0888	0.0653	0.118	0.00232	0.00603
Barley	0.0372	0.0274	0.492	0.000922	0.00240
Sorghum	0.0599	0.0441	0.0794	0.00149	0.00387
Corn	4.48	3.30	5.92	0.111	0.289
Soybeans	1.06	0.783	1.41	0.0265	0.688
Peanuts	0.00992	0.00729	0.00131	0.000246	0.000640

Table 4.26. Daily Consumption Rates of Feeds by Animals in Pounds per Day

Since the consumption rates for the different types of animals are given on a daily basis, it is necessary to determine how many of each type of animal there are on any given day to determine the total daily consumption by all such animals. For dairy cows and beef cattle, statistical data [2] provide those numbers. However, in the case of hogs and poultry, the age of the animal at the time of slaughter is less than one year. Therefore, for hogs and poultry, the "standing crop" (i.e., the number extant) on any given day is less than the total number produced during the year and is found by dividing the total number produced annually by the "number of crops per year", where

12 months

Number of crops per year =

Age at time of slaughter (mo)

A summary of the "standing crop" for each type of food-producing animal is given in Table 4.27.

By multiplying the daily consumption rate for a particular species of animal by the "standing crop" of that species, the total daily consumption of that crop by that type of animal can be found. With this total daily consumption for each crop category, it is then possible to determine the percentage of each crop category consumed by each species of food-producing animal. The percentages obtained are given in Table 4.28. Finally, by using Table 4.25 in conjuction with Table 4.28, it is possible to arrive at the fraction of the crop which is consumed by man, dairy animals, and meat-producing animals.

The range of possible values was derived by assuming that the smallest fraction would most probably not vary by more than 25% of its calculated value. The variation for the larger fractions was then calculated such that

Animal	Total No. <u>During Year</u>	Age at <u>Slaughter (mo)</u>	Number of <u>"Crops"</u>	Standing Crop	<u>Table</u>	Page
Cattle						
Dairy	$1.114 \times 10^{7}$	24	1.0	$1.114 \times 10^{7}$	388	261
Beef	$1.029 \times 10^{8}$	96	1.0	$1.029 \times 10^{8}$	388	261
Hogs	9.847x10 <sup>7</sup>	6	2.4	$4.103 \times 10^{7}$	407	276
Chickens	4.415x10 <sup>9</sup>	3	4.0	1.104x10 <sup>9</sup>	508	358
					511	360
Turkeys	1.698x10 <sup>8</sup>	6 .	2.0	8.490x10 <sup>7</sup>	524	367

Table 4.27. "Standing Crops" (Animials)

Table 4.28.	Crop	Consumption by	y Animal
-------------	------	----------------	----------

airy (%)	<u>Beef (%)</u>			
	DEET (9)	<u>Hogs (%)</u>	<u>Chickens (%)</u>	<u>Turkeys (%)</u>
10	0.0	<b>A</b>	<u>^</u>	<b>A</b>
10	90	0	. 0	0
13	87	0	0	0
6	42	30	15	6
6	43	31	16	4
0	0	0	0	0
0	0	0	0	0
0	0	0	0	0
	6 6 0 0	13     87       6     42       6     43       0     0       0     0	13     87     0       6     42     30       6     43     31       0     0     0       0     0     0	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$

. . . .

the ranges would be proportional to their sizes, but would not allow the total consumption of any crop to exceed 100%.

## 4.3.8 TCROOT

TCROOT<sub>i,j</sub> = fraction of the nuclide i deposited onto soil used to grow crop j
that will ultimately be consumed by man as a result of the longterm uptake by plant roots or by direct consumption of the soil by
grazing animals.

Table 4.29 shows the recommended values for  $TCROOT_{i,j}$  for the Sr and Cs nuclides and Table 4.30 shows the recommended values for  $TCROOT_{i,j}$  for the I nuclides.

Crop	<u>Sr-89</u>	Sr-90	<u>Cs-134</u>	<u>Cs-137</u>
Pasture	0.00041	0.026	0.0013	0.0069
	(0.00030-	(0.014-	(0.0010-	(0.0047-
	0.00051)	0.049)	0.0016)	0.0102)
Stored Forage	0.0013 (0.00095- 0.0016)	0.090 (0.05- 0.17)	0.00071 (0.00048- 0.0010)	0.0015 (0.00092- 0.0027)
Grain	0.000043	0.0033	0.000035	0.000076
	(0.000033-	(0.0019-	(0.000024-	(0.000046-
	0.000053)	0.0063)	0.000051)	0.00013)
Legumes	0.00037	0.028	0.000093	0.00020
	(0.00028-	(0.016-	(0.000062	(0.00012-
	0.00047)	0.054)	0.00014)	0.00035)
Green Leafy Vegetables	0.00017 (0.00013- 0.00021)	0.013 (0.0071- 0.024)	0.000014 (0.0000094- 0.000020)	0.000030 (0.000018- 0.000051
Roots & Tubers	0.00011 (0.000083- 0.00014)	0.0084 (0.0047- 0.0016)	0.000056 (0.000038- 0.000080)	0.00012 (0.000072- 0.00021)
Other Food	0.000008	0.00066	0.00011	0.00023
	(0.0000063-	(0.00036-	(0.000071-	(0.00014-
	0.00041)	0.0013)	0.00015)	0.00041)

Table 4.29. Recommended Values for TCROOTi, j for Sr and Cs Nuclides

±,j	
<u> </u>	<u> </u>
0.000016	0.0000017
0.0	0.0
	0.000016

Table 4.30. Recommended Values for

TCROOT; ; for I Nuclides

A uniform sampling distribution is recommended for  $TCROOT_{i,j}$ .

**Discussion** 

 $TCROOT_{i,j} = IRU_{i,j} + ISI_{i,j}$ 

where

The principal mechanism by which nuclides are transferred from soil to plants is via root uptake. Transfer to plant surfaces may also occur by rainsplash and by the deposition of materials resuspended from surface soil. A rate at which nuclides are transferred from the soil to plants via each of these mechanisms can be established. The overall transfer rate is then just the weighted sum of these individual rates.

For the pasture, an additional term is used in deriving the data for TCROOT. To account for the fact that grazing cattle will ingest a certain amount of soil along with the plant material they consume, a time-integrated soil ingestion factor is added to the time-integrated root uptake rate. It is assumed that pasture undergoes continuous harvest (grazing by animals) and that all nuclides deposited onto pasture will be consumed by the end of the growing season. Therefore, the transfer factors (DCYPCB and DCYPCM) for nuclides deposited onto pasture and consumed by meat- or milk-producing animals is unity. The overall transfer factor for soil ingestion by grazing animals can be obtained by treating the ingestion of soil by grazing animals as though the ingested soil was first transferred to the surface of pasture grass then and consumed. The soil ingestion component, ISI, of the transfer factor TCROOT will be 0.0 for all crops except pasture.

According to Ostmeyer and Helton [1], the rate of transfer from soil to plants by either rainsplash or resuspension is negligible compared the rate of transfer via root uptake. The values for TCROOT were thus derived using only root uptake transfer factors.

(4.10)

If the nuclides deposited onto the soil were to remain at a constant level over time, the long-term transfer factor would simply be the product of the annual uptake rate and the length of time being considered. However, in actuality, the availability of the deposited material decreases over time. This decrease is a reflection of the following physical and chemical processes: (1) radioactive decay, (2) percolation of material to the region below the root zone, (3) irreversible chemical binding of the nuclides to components of the soil, (4) previous root uptake of nuclides, and (5) soil ingestion by grazing animals.

Because the availability of the material does not remain constant, it is necessary to integrate the uptake rate over time. If an exponential depletion rate is assumed, then the time-integrated root uptake transfer factor, IRU, can be expressed as

$$IRU_{i,j} = RU_{i,j} \cdot \int_{0}^{T} EXP\{-[(RU_{i,j} + RD_i + RP_i + RB_i + RSI_{i,j}) \cdot t]\} dt (4.11)$$

#### where

- RU<sub>i,j</sub> = rate at which nuclide i is corporated into the edible portion of crop j via root uptake from the soil (yr<sup>-1</sup>)
- $RD_i$  = radiological decay rate for nuclide i (yr<sup>-1</sup>)
- $RP_i$  = rate at which nuclide i percolates to a region below the root zone  $(yr^{-1})$
- $RSI_{i,j}$  rate at which nuclide i is removed via soil ingestion from the soil used to grow crop j (yr<sup>-1</sup>)
- T = the time period of interest for the transfer of deposited nuclides via root uptake from the soil to the edible portion of the plant (yr)

The time-integrated soil ingestion factor is obtained in an analogous manner with several differences. Soil ingestion occurs only from the surface soil, and therefore, the unavailability of material for ingestion by grazing cattle relates to the "loss" of the material from surface soil. Several factors contribute to the unavailability of material for ingestion. They are radiological decay, percolation of the nuclides out of the surface soil, removal of material via root uptake, and removal of material via ingestion by grazing animals. Even though irreversible chemical binding may occur to the soil in the surface soil compartment (the top 1 cm), this irreversibly bound material is still available to be ingested. Therefore, the rate at which chemical binding occurs does not appear in the derivation of the transfer factor, ISI. ISI can be derived as follows:

$$ISI_{i,j} = RSI_{i,j} \cdot \int_{0}^{T} EXP\{-[(SRU_{i,j} + RD_i + SRP_i + RSI_{i,j}) \cdot t]\} dt \quad (4.12)$$

where

- RSI<sub>i,j</sub> = rate at which nuclide i is removed via soil ingestion from the surface soil compartment on land used to grow crop j (yr<sup>-1</sup>)
- $SRU_{i,j}$  = rate at which nuclide i is corporated into the edible portion of crop j via root uptake from the surface soil compartment (yr<sup>-1</sup>)

 $RD_i$  = radiological decay rate for nuclide i (yr<sup>-1</sup>)

- SRPi = rate at which nuclide i percolates to a region below the surface soil compartment (yr<sup>-1</sup>)
- T = the time period of interest for the transfer of deposited nuclides via soil ingestion of soil on which pasture is grown (yr)

When the time period of concern for the long-term doses arising from the food pathway is taken to be all time following the accident (i.e., letting  $T = \infty$ ), TCROOT<sub>i.i</sub> will be evaluated as follows:

$$TCROOT_{i,j} = IRU_{i,j} + ISI_{i,j}$$

and

$$TCROOT_{i,j} = \frac{RU_{i,j}}{RU_{i,j} + RD_i + RP_i + RB_i + RSI_{i,j}}$$

$$+ \frac{RSI_{i,j}}{SRU_{i,j} + RD_i + SRP_i + RSI_{i,j}}$$
(4.13)

The values for  $RU_{i,j}$  are derived from fallout data. Root uptake by plants is usually described using an empirical concentration ratio (CR) defined as

Radionuclide activity per unit mass (dry) of plant (bq/kg)

Radionuclide activity per unit mass (dry) of soil (bq/kg)

The root uptake rate, RU, is then defined as

$$RU_{i,j} = CR_{i,j} \cdot \frac{CM_j}{SM}$$

CR ≕

where

 $CM_j$  = annual yield of crop j (kg yr<sup>-1</sup>/m<sup>2</sup>)

SM = soil mass in root uptake compartment  $(kg/m^2)$ 

The soil mass (SM) is taken to be an average value of 240  $\rm kg/m^2$ .

A summary of concentration ratios can be found in Till and Meyer [10:Table 5.17], and a summary of crop yield values can be found in Boone et al. [8]. A value for CM for each crop category is obtained by a weighted average over the predominant crops in each category. The values used for CR and CM for Sr and Cs nuclides are given in Table 4.31. The CR values for the short-lived I nuclides are assumed to be 0.0, which in turn implies that the IRU values for the I nuclides is 0.0 for all crops.

	CR	CM	
Crop	Strontium	Cesium	(kg/yr•m <sup>2</sup> )
Pasture	2.0	0.01	0.175
Stored Forage	3.0	0.2	0.50
Grains	0.2	0.02	0.25
Legumes	2.0	0.06	0.22
Green Leafy Ve	g. 2.0	0.02	0.10
Roots & Tubers	0.5	0.03	0.26
Other Foods	0.2	0.03	0.05

Table 4.31. Values for Concentration Ratios (CR) and Crop Yield Values (CM)

By using these values for CR and CM, the corresponding values for RU were established. These RU values are summarized in Table 4.32. The range of

values derived by assuming that the correct value would lie within 25% of the value estimated for RU.

		RU	
Crop	<u>Strontium</u>	Cesium	<u>Iodine</u>
Pasture	0.0015 (0.0011-0.0019)	0.0000073 (0.0000054-0.0000091)	0.0
Stored Forage	e 0.0063 (0.0047-0.0079)	0.00042 (0.00032-0.00053)	0.0
Grain	0.00021 (0.00016-0.00026)	0.000021 (0.000016-0.000026)	0.0
Legumes	0.0018 (0.0014-0.0023)	0.000055 (0.000041-0.000069)	0.0
Green Leafy Vegetables	0.00083 (0.00062-0.0010)	0.0000083 (0.0000062-0.000010)	0.0
Roots & Tubers	0.00054 (0.00041-0.00068)	0.000033 (0.000025-0.000041)	0.0
Other Foods	0.000042 (0.000031-0.000053)	0.000063 (0.000047-0.000079)	0.0

Table 4.32. Values for Root Uptake (RU	Table	4.32.	Values	for	Root	Uptake	(RU)
--	-------	-------	--------	-----	------	--------	------

The rate at which nuclide i becomes unavailable for root uptake from radioactive decay,  $RD_i$ , can be defined as

 $RD_i = 1n2 / THALF_i$ 

where

 $THALF_i = radiological half-life of nuclide i (yr)$ 

Because radioactive half-lives are precisely known, no range of values has been established for  $RD_i$ . The values of  $RD_i$  are summarized in Table 4.33.

The percolation rate is strongly dependent on soil characteristics; therefore, these values are quite uncertain. The range of possible values was established by assuming that the actual value would most likely lie within 25% of the predicted value. The half-lives of the iodine isotopes considered are so short that radioactive decay is the primary mechanism by which these nuclides become unavailable for root uptake. Thus, no percolation rate has been established for iodine nuclides.

Table 4.33.	Values for Radioactive Decay
Nuclide	RD
Sr-89	4.860
Sr-90	0.024
Cs-134	0.340
Cs-137	0.023
I-131	31.500
I-133	292.000

The percolation rates, RP, for strontium and cesium established by Hoffman and Baes [11] are summarized in Table 4.34.

Table 4.34.	Percolation Rate for Sr and Cs
Element	<u></u>
Strontium	0.0021
Cesium	0.0096

In addition, the derived values for RP apply to the entire root zone (the top 15 cm of soil compartment). Since the surface soil compartment is assumed to reach a depth of 1 cm, the value of SRP, the percolation rate for the surface soil compartment, could be assumed to be one-fifteenth of the value RP established for the root zone. This does not seem too unreasonable, since the percolation distance would be one critical factor in the percolation rate. Still, this approximation may be somewhat conservative, since the surface soil compartment is much more susceptible to weathering than is the root uptake soil compartment.

Table 4.35 gives a summary of the values for RP, the percolation rate from the root uptake zone, and SRP, the percolation rate from the surface soil compartment.

	ITF	ISI
_Element_	RP	SRP
Strontium	0.0096 (0.0072-0.012)	0.14 (0.11-0.18)
Cesium	0.0021 (0.0016-0.0026)	0.032 (0.024-0.040)

Table 4.35. Values for ITF and ISI

Ostmeyer and Helton [1] established the rate of soil ingestion, RSI, for all nuclides for pasture. Since no soil ingestion occurs during the harvest of the nonpasture crops, the corresponding values of RSI is 0.0  $yr^{-1}$ . Table 4.36 shows the values for RSI for all nuclides.

Table 4.36.	Values for RSI for All Nuclides		
Crop	RSI		
Pasture	0.0005 (0.0004-0.0006)		
Nonpasture	0.0		

The range of possible values for the soil ingestion rate was established by assuming the actual value would most probably lie within 25% of the estimated value.

4.3.9 TFBF

 $TFBF_i$  = fraction of the daily consumption of nuclide i by meat-producing animals that remains in the meat at the time of slaughter

Table 4.37 shows the recommended values for  $\text{TFBF}_i$ . A uniform sampling distribution is recommended for  $\text{TFBF}_i$ .

<u>Discussion</u>

$$TFBF_{i} = \frac{OUTPUT_{i}}{EATEN_{i}}$$

Nuclide	<u>TFBF</u>	Range of Values
Sr-89	0.00022	0.000094 - 0.00038
Sr-90	0.00022	0.000094 - 0.00038
Cs-134	0.023	0.020 - 0.035
Cs-137	0.024	0.020 - 0.035
I-131	0.0024	0.00082 - 0.0037
I-133	0.0011	0.00041 - 0.0013

Table 4.37. Recommended Values for TFBF<sub>1</sub>

where

 $OUTPUT_i$  = amount of radionuclide i in meat produced by meat animals (Ci)

 $EATEN_i$  = amount of radionuclide i in feed consumed by meat animals (Ci)

The value of this transfer factor is derived by evaluating the following expression:

 $TFBF_i = TR \cdot M \cdot ETF_i$ ,

where

TR = fraction of animals slaughtered per day  $(day^{-1})$ 

M = quantity of meat produced by those animals at slaughter (kg)

 $ETF_i$  = equilibrium transfer factor to meat for the radionuclide i (day/kg)

Previously, TFBF<sub>i</sub> was calculated using only beef in the calculations. By using recent agricultural data [2:Tables 455 and 516], it can be shown that beef accounts for only 42% of the meat produced, pork an additional 29%, and poultry the final 29%. The amount of poultry produced is composed of 84% chicken and 16% turkey. In light of these data, it was decided to consider all three meat sources (beef, pork, and poultry) in deriving a value for TFBF.

A transfer factor is obtained for each of these meat sources and an overall transfer is developed by taking a weighted average of these animal-specific transfer factors. That is,

 $TFBF_i = FB \cdot TFB_i + FPK \cdot TFPK_i + FC \cdot TFC_i + FT \cdot TFT_i$ 

where

FB = fraction of meat produced that is beef (i.e., 0.42)
FPK = fraction of meat produced that is pork (i.e., $0.29$ )
FC = fraction of meat produced that is chicken (i.e., $0.24$ )
FT = fraction of meat produced that is turkey (i.e., 0.05)
$TFB_i$ = transfer factor for nuclide i by beef
$TFPK_i = transfer factor for nuclide i by pork$
$\text{TFC}_{i}$ = transfer factor for nuclide i by chicken
$TFT_i$ = transfer factor for nuclide i by turkey

Equilibrium transfer factors (ETF<sub>i</sub>) for Sr, Cs, and I were derived by Ng et al. [12] and are presented in Table 4.38.

<u>Element</u>	Product	<u> </u>	<u>Range of Values*</u>
Sr	Beef	0.00030	0.000064 - 0.00057
	Pork	0.0029	0.0012 - 0.0040
	Poultry	0.032	0.018 - 0.080
Cs	Beef	0.020	0.0072 - 0.093
	Pork	0.30	0.26 - 0.38
	Poultry	4.4	4.3 - 4.5
	Beef	0.0072	0.0072 - 0.020
	Pork	0.027	0.0010 - 0.027
	Poultry	0.20	0.0080 - 0.20

Table 4.38. Equilibrium Transfer Factors (ETFs)

Due to the physiological similarity between different poultry types, the  $\text{ETF}_{i}$  values established by Ng for chicken have been used for both chicken and turkey.

These  $\text{ETF}_i$  values were derived for stable strontium and cesium and for I-131, and therefore represent biological losses for strontium and cesium but not radioactive decay losses. For iodine, the radioactive decay constant for I-131 has been included. For I-133, it is therefore necessary to adjust value of TF to reflect the significantly shorter half-life of this isotope.

To find an adjusted ETF value to incorporate specific radioactive decay rates, it is possible to begin with the assumption that

$$\frac{dQ_{i}(t)}{dt} = \frac{R_{i}}{M} - \lambda_{i} \cdot Q_{i}(t)$$
(4.14)

where

- $Q_i(t)$  = concentration of the nuclide i in the meat at time t (Ci/kg)
- $R_i$  = ingestion rate for nuclide i (Ci/day)
- M = the total weight of the meat in an animal at the time of slaughter (kg)
- $\lambda_i$  = decay constant reflecting both radiological decay and biological losses of nuclide i (day<sup>-1</sup>)

Therefore,

$$\frac{dQ_{i}(t)}{\lambda_{i}Q_{i}(t) - \frac{R_{i}}{M}} = -dt$$
(4.15)

By letting 
$$u = \frac{R_i}{M} - \lambda_i Q_i(t)$$
 then  $\frac{du}{dQ_i(t)} = -\lambda_i$  and  $\frac{du}{dQ_i(t)} = dQ_i(t)$ 

Therefore, by subsitution into Equation 4.15

then  $\lambda_{i}u = e^{-\lambda t} + C = e^{C}e^{-\lambda t}$  and  $u = \frac{e^{C}}{\lambda_{i}}e^{-\lambda t}$ 

Therefore,

$$\frac{R_{i}}{M} - \lambda_{i}Q_{i}(t) = \frac{e^{C}}{\lambda_{i}} e^{-\lambda t} \text{ and } Q_{i}(t) = \frac{R_{i}}{\lambda_{i}M} + \frac{e^{C}}{\lambda_{i}^{2}} e^{-\lambda t}$$

and in the equilibrium state

$$ETF_{i} = \lim_{t \to \infty} Q_{i}(t) = \frac{R_{i}}{\lambda_{i}M}$$
(4.16)

Since

$$ETF_{i} = \frac{Q_{i}(t)}{R_{i}} = \frac{Concentration of nuclide i in meat (Ci/kg)}{Daily ingestion rate of nuclide i by the animal (Ci/day)}$$

in the equilibrium state, it follows from Equation 4.16 that

$$ETF_{i} = \frac{Q_{i}(t)}{R_{i}} = \frac{\frac{R_{i}}{\lambda_{i}M}}{R_{i}} = \frac{1}{\lambda_{i}M}$$
(4.17)

For ETF<sub>1</sub> as derived by Ng et al. [12],  $\lambda_i$  represents the biological decay constant for both strontium and cesium and represents the sum of the biological decay constant and the I-131 radiological decay constant for the iodine ETF<sub>1</sub>. The revised RETF<sub>1</sub> can be defined as

$$RETF_{i} = \frac{1}{M (\lambda_{b,i} + \lambda_{d,i})} (day/kg)$$
(4.18)

 $\lambda_{b,i}$  = biological decay constant for nuclide i for the animal being considered (day<sup>-1</sup>)

$$\lambda_{d,i}$$
 = radiological decay constant for nuclide i (day<sup>-1</sup>)

To derive the revised  $\text{RETF}_i$  for a specific nuclide i, it will be assumed that the the Ng value,  $\text{ETF}_i$ , is based on nuclide with the radiological decay rate,  $\lambda_1$ . Therefore,

$$ETF_{i} = \frac{1}{M (\lambda_{1} + \lambda_{b,i})}$$
(4.19)

To establish the RETF<sub>i</sub>, the biological decay rate will be needed. By solving Equation 4.19 for  $\lambda_{b,i}$ , we find

$$\lambda_{b,i} = \frac{1}{M \cdot ETF_i} - \lambda_1$$

Therefore, by Equation 4.17,

$$RETF_{i} = \frac{1}{M (\lambda_{b,i} + \lambda_{d,i})}$$

$$= \frac{1}{M\left[\left(\begin{array}{c} \frac{1}{M \cdot ETF_{i}} - \lambda_{1} \end{array}\right) + \lambda_{d,i}\right]}$$

$$= \frac{1}{M\left(\frac{1 - \lambda_1 \cdot M \cdot ETF_i + \lambda_{d,i} \cdot M \cdot ETF_i}{M \cdot ETF_i}\right)}$$

$$= \frac{\text{ETF}_{i}}{1 + [M \cdot \text{ETF}_{i} \cdot (\lambda_{d,i} - \lambda_{1})]}$$

where

- $ETF_i$  = original equilibrium transfer factor as established by Ng (day/kg)
- M = amount of meat produced by animals at time of slaughter (kg)
- $\lambda_1$  = radioactive decay constant of used to establish the original ETF<sub>1</sub> (day<sup>-1</sup>)
- $\lambda_{d,i}$  = radioactive decay constant for nuclide i (day<sup>-1</sup>)

It has been noted that the ETF for strontium and cesium were established using the stable elements. This implies that  $\lambda_1$  for both these cases would be nearly zero, and the expression for RETF<sub>1</sub> would simplify for strontium and cesium isotopes and becomes

$$\operatorname{RETF}_{i} = \frac{\operatorname{ETF}_{i}}{1 + (\lambda_{d,i} * M * \operatorname{ETF}_{i})}$$
(4.20)

The ETF for iodine was established using data for I-131, and therefore, in Equation 4.19,

$$\lambda_1 = \frac{\ln 2}{8.04}$$

Therefore, for any other isotope of iodine

$$\operatorname{RETF}_{i} = \frac{\operatorname{ETF}_{i}}{1 + \left[ M \cdot \operatorname{ETF}_{i} \cdot \left( \lambda_{d,i} - \frac{\ln 2}{8.04} \right) \right]}$$
(4.21)

Using Equations 4.20 and 4.21 and the values and ranges of  $\text{ETF}_i$  established by Ng et al. [12], the values and associated ranges for the revised equilibrium factors,  $\text{RETF}_i$ , were established and are summarized in Table 4.39. These values for  $\text{RETF}_i$  were in turn used in deriving the transfer factor  $\text{TFBF}_i$  for each nuclide i.

The variable M, the amount of meat produced by the animal at the time of slaughter, is needed both in the calculation of  $\text{RETF}_i$  and the calculation of  $\text{TFBF}_i$ . Based on agricultural data [2:Tables 444 and 516], the values for M summarized in Table 4.40 were used.

Nuclide	Cattle	Hog	Chicken	Turkey
Sr-89	0.00030 (0.000064-0.00057)			0.032 (0.018-0.079)
Sr-90	0.00030 (0.000064-0.00057)			
Cs-134	0.020 (0.0072-0.091)	0.29 (0.26-0.37)		
Cs-137	0.20 (0.0072-0.093)	0.30 (0.26-0.38)		
I-131	0.0072 (0.0072-0.020)	0.027 (0.0010-0.027)		0.20 (0.0080-0.20)
I-133	0.0033 (0.0033-0.0047)			

Table 4.39. Values for Revised Equilibrium Transfer Factors

Animal	Dressed <u>Weight (kg)</u>	Cutting Losses (%)	Edible Products Weight (kg) *
Cattle	269.0	15	229.0
Hogs	84.02	10	70.62
Chickens	1.34	10	1.188
Turkeys	6.96	10	6.183

Table 4.40. Meat Produced at Slaughter

Also needed for the calculation of  $\text{TFBF}_i$  are values for the variable TR, the fraction of animals slaughtered per day. By using agricultural data on meat production [2:Tables 388, 398, 406, 407, 415, 502, 511, 516, 521, and 523], the values for TR in Table 4.41 were derived.

Recently there has been fallout data being made available following the Chernobyl accident. These data were reviewed by Nair and Iijima [13] and estimates were made for several  $\text{ETF}_i$ . For Cs-137, they found an ETF of 0.02 day/kg for beef and a factor of 0.3 day/kg for pork, both of which closely agree with the ETFs as established by Ng [12].

A range of values for the equilibrium transfer factors was given by Ng. These ranges were used to determine the possible ranges for the variable  $TFBF_i$ .

<u> </u>				
			Poult	ry
	<u>Beef</u>	<u>Pork</u>	Chicken	Turkey

0.0024

0.0026

0.0026

TR  $(day^{-1})$  0.0011

Table 4.41. Values for the Fraction of Animals Slaughtered per Day (TR)

#### 4.3.10 TFMLK

TFMLK<sub>i</sub> = fraction of the amount of radionuclide i present in the feed consumed by milk-producing animals that is present in the milk produced

Table 4.42 gives the recommended values for  $\text{TFMLK}_i$ . A uniform sampling distribution is recommended for  $\text{TFMLK}_i$ .

Nuclide	<u>TFMLK</u> i	Range of Values
Sr-89	0.022	(0.0072-0.061)
Sr-90	0.022	(0.0072-0.061)
Cs-134	0.11	(0.040-0.26)
Cs-137	0.11	(0.040-0.26)
I-131	0.13	(0.036-0.46)
I-133	0.062	(0.018-0.22)

Table 4.42. Recommended Values for TFMLK;

**Discussion** 

 $TFMLK_{i} = \frac{OUTPUT_{i}}{EATEN_{i}}$ 

where

 $OUTPUT_i$  = amount of nuclide i in milk produced

 $EATEN_i$  = amount of nuclide i in feed consumed

This variable is evaluated in the following manner for each nuclide i:

$$TFMLK_i = ETF_i \cdot MP$$

where

 $ETF_i$  = equilibrium transfer coefficient for nuclide i into milk (day/L)

MP = average daily total milk production (L/day)

Using recent agricultural data it was found the the average daily production is 16.01 L/day/cow [2:Table 471]. Therefore a value of MP = 16 was used for these calculations.

The equilibrium transfer factor,  $\text{ETF}_i$ , for the nuclide i is given below as summarized by Ng [12]. It is expected that there will be considerable variation in all ETF values. A summary of the possible range of values for the ETF for each of the elements is given below as adapted from Hoffman and Baes [11] by Ng [12].

<u>Element</u>	<u>ETF (L/day)</u>	<u>Range of Values</u>
Strontium	0.0014	(0.00045-0.0038)
Cesium	0.0071	(0.0025-0.016)
Iodine	0.0099	(0.0027-0.035)
•		

Table 4.43. ETF for Nuclides

These values for ETF are based on stable element concentrations in associated milk and feed. Radioactive decay within the animal has an important impact on the ETF values for the short-lived radionuclides. The ETF values to be used for the I-131 and I-133 were adjusted to reflect these losses. The transfer coefficient can be thought of as the time-integrated transfer fraction for a unit nuclide intake by an animal [12]. In a development of the model used to describe the crop-animal-milk pathway, Ostmeyer and Helton [1] conclude that when intake is considered to be constant with time the intake-to-milk equilibrium transfer coefficient can be derived as follows:

$$ETF_{i} = \sum_{k=1}^{n} \frac{A_{k}}{\lambda_{b,k} + \lambda_{i}}$$
(4.22)

where

ъ. н. <u>-</u>

- $A_k$  = concentration coefficient associated with a single acute exposure  $(L^{-1})$
- $\lambda_{b,k}$  = biological decay constant for the associated concentration coefficient  $A_k$  (day<sup>-1</sup>)
- $\lambda_i$  = radiological decay constant for the nuclide i (day<sup>-1</sup>)

This formulation accounts for the decrease in elemental concentration patterns over time from radioactive decay. Ng et al. [12] gave the values for stable iodine in Table 4.44.

Table	4.44. Values Iodine	for Stable
k	≜k	BDCk
1 2	0.0055 0.00017	0.69 0.088

Using the  $\lambda_i$  values of 0.086 and 0.80 for I-131 and I-133 respectively, the adjusted ETF<sub>i</sub> values for these two nuclides are then as shown in Table 4.45.

Table 4.45	Adjusted ETF Values
Nuclide	Adjusted ETF Value
I-131	0.0081 (0.0022-0.029)
I-133	0.0039 (0.0011-0.014)

The range of possible values for ETF as noted above served as the basis for determining the adjusted range of values for ETF. This was accomplished by using similar ratios between the ETF values for stable iodine and the adjusted ETF value for each nuclide.

The values and ranges used in determining the values of the variable  $\text{TFMLK}_i$  for each nuclide i are summarized in Table 4.46.

<u>Nuclide</u>	ETF Value (L/d)	Range of Value
Sr-89	0.0014	(0.00045-0.0038)
Sr-90	0.0014	(0.00045-0.0038)
Cs-134	0.0071	(0.0025-0.016)
Cs-137	0.0071	(0.0025-0.016)
I-131	0.0081	(0.0022-0.029)
I-133	0.0039	(0.0011-0.014)

Table 4.46. ETF Values for TFMLKi

In a review of fallout data following the Chernobyl accident by Nair and Iijima [13], an equilibrium transfer factor of 0.002 d/L was suggested for I-131, which is somewhat less than the transfer factor derived here. This may be a notable development, since milk is the primary means within the food pathway by which iodine may be ingested. If this value is correct, the value of TFMLK for I-131 would then become 0.032.

### 4.4 <u>Mitigative Action Input Parameters</u>

Within the MACCS code, the dose received by society is restricted by userestablished dose criteria. For the food pathway model, two distinct criteria can be established: one for the growing season submodel and one for the longterm submodel. Various mitigative action options are available within the code for each of these submodels within the code. Each of the mitigative actions are designed to attenuate the societal dose received following an accidental release.

Several input parameters are required by the MACCS code to assure that the dose to be received via the food pathway will remain below the criteria. These input parameters are discussed in this section.

- $GCMAXR_i$  = maximum allowable concentration for ground on which crops are grown that assures the lifetime dose criteria will be met (Bq/m<sup>2</sup>)
- $PSCMLK_i$  = maximum allowable concentration for ground on which crops are grown that assures the emergency dose criteria will be met without milk disposal (Bq/m<sup>2</sup>)
- $PSCOTH_i$  = maximum allowable concentration for ground on which crops are grown that assures the emergency dose criteria will be met without crop disposal (Bq/m<sup>2</sup>)

Table 4.47 gives the recommended values for GCMAXR;, PSCMLK;, and PSCOTH;.

<u>Nuclide</u>	GCMAXR	PSCMLK	PSCOTH
Sr-89	1.79x108	2.16x10 <sup>7</sup>	2.16x10 <sup>7</sup>
Sr-90	3.67x104	2.41x10 <sup>5</sup>	2.41x10 <sup>5</sup>
Cs-134	4.07x10 <sup>6</sup>	2.18x10 <sup>5</sup>	2.18x10 <sup>6</sup>
Cs-137	1.76x106	2.66x10 <sup>5</sup>	2.66x1010
I-131	$1.00 \times 10^{20}$	$1.34 \times 10^{6}$	7.9510x <sup>6</sup>
I-137	$1.00 \times 10^{20}$	$1.05 \times 10^{10}$	$1.02 \times 10^{11}$

Table 4.47. Recommended Values for  $GCMAXR_i$ , PSCMLK<sub>i</sub>, and PSCOTH<sub>i</sub>

It can be assumed the actual value for these variables will most probably lie within 25% of the calculated value. This assumption served as the basis for deriving a possible range of values for each nuclide/parameter pair.

#### Discussion

To assure that the dose received by individual remains below the user-defined dose criterion, the dose equation (i.e., Equation 4.1) is solved to find a maximum allowable ground concentration that would ensure the dose limit would not be exceeded. That is,

 $GCMAXR_{i} = \frac{DL_{i,k}}{DF_{i,k} \cdot \sum_{j} (A \cdot FA_{j} \cdot TF_{i,j})}$ 

To determine these maximum allowable ground concentrations, a dose limit for a maximally exposed individual was used. That is, the ground concentration was calculated for an individual whose entire intake of food was assumed to originate on contaminated ground. The maximally exposed individual can be either an infant whose food intake consists entirely of milk or an adult whose intake of food is based on a "typical" market basket.

Since the dose is being limited for an individual, parameters in Equation 4.23 assume the following definitions:

 $DL_{i,k}$  = dose limit for the maximally exposed individual (Sv)

- A = total cropland area required to grow crops to provide the food for the annual market basket for a maximally exposed individual (m<sup>2</sup>)
- FA; = fraction of area A needed to grow crop j (unitless)
- TF<sub>i,j</sub> = fraction of the amount of nuclide i deposited following the release that will ultimately be consumed by man (unitless)

Separate maximum allowable ground concentrations are derived for the long-term and growing season food pathway submodels. Associated with each of these submodels is an allowable dose (user input dose criterion).

 $GCMAXR_i$  is the maximum allowable ground concentration established for nuclide i to meet the lifetime exposure criteria. It is applied to the long-term food pathway submodel.

For the growing season food pathway submodel, two maximum allowable ground concentrations are established.  $PSCMLK_i$  is applied to the crop-milk-man pathway and assures that a maximally exposed infant (i.e., an infant drinking milk only from animals raised and fed on contaminated ground).  $PSCOTH_i$  assures that the maximally exposed individual would not exceed the allowable dose when the nonmilk portion of his annual intake is added to the milk consumed when the ground concentration for milk production is  $PSCMLK_i$ .

Each of these allowable ground concentrations is determined for each nuclide is considered in the food pathway model. They are used within the MACCS code to determine mitigative action to assure the individual dose received as a result of the release of radioactive material will remain within the preestablished exposure criteria.  $PSCMLK_i$  is used to determine the necessity of disposing of the milk being produced on contaminated ground. No disposal of milk is deemed to be necessary if the following condition is met:

$$\sum_{i} \frac{\text{PSCMLK}_{i}}{\text{GC}_{i}} \leq 1$$
(4.24)

where

 $GC_i$  = the actual ground concentration of nuclide i following the release  $(Bq/m^2)$ 

Analogously,  $PSCOTH_i$  is used to determine the necessity of disposing of crops contaminated by direct deposition of radioactive material onto the plant surfaces following the release. No crop disposal is deemed necessary if the following condition is met:

$$\sum_{i} \frac{PSCOTH_{i}}{GC_{i}} \leq 1$$
(4.25)

The parameter GCMAXR<sub>i</sub> is used to ensure that the lifetime exposure from radionuclides ingested via the food pathway will meet the established criteria. No mitigative actions will be required if the following condition is met:

$$\sum_{i} \frac{\text{GCMAXR}_{i}}{\text{GC}_{i}} \leq 1 \qquad (4.26)$$

If the ground concentration following the release is too high for this criteria to be met, several mitigative actions are evaluated for effectiveness in reducing the projected dose to within allowable standards. The first of the mitigative actions evaluated is decontamination of the cropland. If decontamination alone is insufficient to produce the required results, it is determined whether restricting crop production to allow natural depletion of the radioactive material would bring the dose received to within the lifetime criteria. Currently a maximum of eight years is permitted for interdiction of crop growth. To calculate the effectiveness of an interdiction of crops for t years, the ground concentration following decontamination is attenuated by an overall annual depletion rate,  $QROOT_i$ , and the dose is again projected to determine whether the lifetime criteria have been fulfilled. That is,

 $GCI_{i,t} = GCD_i \cdot EXP (-QROOT_i \cdot t)$ 

where

- $GCI_{i,t}$  = ground concentration of nuclide i following t years of interdiction  $(Bq/m^2)$
- $GCD_i$  = ground concentration of nuclide i following decontamination (Bq/m<sup>2</sup>)
- $QROOT_i$  = annual natural depletion rate for nuclide i (i.e., the depletion resulting from radioactive decay, percolation from the root zone, irreversible chemical binding with the soil, previous loss from the root zone from root uptake, and the loss from soil ingestion by grazing animals) (yr<sup>-1</sup>)

Following the calculation of the ground concentration following each additional year of interdiction (up to a maximum of eight years), a check is made to see whether the lifetime dose criteria are met, that is,

$$\sum_{k=1}^{n} \frac{\text{GCMAXR}_{i}}{\text{GCI}_{i,k}} \leq 1 \qquad n \leq 8$$

If eight years proves to be insufficient for natural depletion to bring ground concentrations to within acceptable levels, the farmland will be condemned. That is, it will be purchased and restricted from production.

A complete discussion of the derivation of the values used for the input parameters  $\text{GCMAXR}_i$ ,  $\text{PSCOTH}_i$ , and  $\text{PSCMLK}_i$  is given in Appendix C of the MACCS Model Description [14]. Because of the lengthy discussion needed to describe these calculations adequately, that discussion will not be repeated in this document.

# 4.4.2 QROOT

 $QROOT_i$  = annual depletion rate of nuclide i from the root zone

Table 4.48 gives the recommended values for QROOT for each nuclide i. A uniform sampling distribution is recommended for  $QROOT_i$ .

	QROOT	
Nuclide	QROOT	Range of <u>Possible Values</u>
Sr-89	4.9	
Sr-90	0.065	(0.041-0.090)
Cs-134	0.59	(0.51-0.69)
Cs-137	0.28	(0.19-0.38)
I-131	32.0	
I-133	290.0	

Table 4.48. Recommended Values for

**Discussion** 

$$QROOT_{j} = RRU_{j} + RD_{j} + RP_{j} + RB_{j}$$

$$(4.27)$$

#### where

QROOT <sub>i</sub> =	-	annual rate of depletion of nuclide i from the root zone $(yr^{-1})$
RRU <sub>i</sub> =	=	annual rate of depletion from root uptake of the nuclide from the root zone $(yr^{-1})$
RDi =	-	annual rate of depletion from radioactive decay $(yr^{-1})$
RPi =	=	annual rate of depletion from percolation into soil below root zone $(yr^{-1})$
RB <sub>i</sub> =	=	annual rate of depletion from irreversible chemical binding of the nuclide with soil components $(yr^{-1})$

A single value of this variable is derived for each nuclide considered in the food pathway.

The annual rate at which plants remove strontium and cesium from the root zone via root uptake for the various crop categories is discussed and summarized by Ostmeyer and Helton [1] whose recommended values are presented in Table 4.49.

	<u>Rate of Root Uptake</u>			
Crop	<u>    Sr    </u>	<u> </u>		
Pasture	0.0017	0.000083		
Stored Forage	0.0042	0.00021		
Grains	0.00021	0.000021		
Leafy Vegetables	0.0013	0.000013		
Other Foods	0.00083	0.000042		

Table 4.49. Root Uptake (RU) by Crop and Element

Even though not all the crop categories considered were included in this summary, the cross section is wide enough that a weighted average of these values was used to determine the annual rate of depletion from soil via root uptake. As a result, the following values given for RU in Table 4.50 were obtained.

Table 4.50. Values for Root Uptake (RU	Table	4.50.	Values	for	Root	Uptake	(RU)
--	-------	-------	--------	-----	------	--------	------

Element	RU	Range of Values
Strontium	0.0016	(0.00021-0.0042)
Cesium	0.000074	(0.000013-0.00021)

No value for RU was derived for iodine isotopes because their short half-lives mean that these isotopes do not contribute significantly to the root uptake dose.

The annual rate at which a nuclide i disappears from the root zone due to radioactive decay  $(RD_i)$  is dependent on its radiological half-life.  $RD_i$  can be defined as follows:

$$RD_{i} = \frac{ln2}{THALF_{i}}$$

where

#### $THALF_i = radiological half-life of nuclide i (yr)$

Values for  $RD_i$  are given in Table 4.51.

	Decay, RD <sub>1</sub> (yr <sup>-1</sup> )
Nuclide	RD
Sr-89	4.86
Sr-90	0.024
Cs-134	0.34
Cs-137	0.023
I-131	31.5
I-133	292.0

Table 4.51. Values for Radioactive

Because radioactive half-lives are precisely known, no ranges are given for the values of  $RD_i$ .

The percolation rate for strontium and cesium have been established by Hoffman and Baes [11]. For strontium, this rate is given as 0.0021 yr<sup>-1</sup>, and for cesium, it is given as  $0.0096 \text{ yr}^{-1}$ . The percolation rate is strongly dependent on soil characteristics; therefore, these values represent an approximate rate and are quite uncertain. A range of possible values was established by assuming that the actual value would most likely lie within 25% of the estimated value. No value for RP was derived for the iodine isotopes being considered since their depletion rate is dominated almost totally by radioactive decay. The values and possible ranges of values used for RP are summarized as in Table 4.52.

_Element_	DRP	<u>Range of Values</u>
Strontium	0.0096	(0.0072-0.012)
Cesium	0.0021	(0.0016-0.0026)

Table 4.52. Values for Rate of Percolation (R)	Table	4.52.	Values	for	Rate	of	Percolation	(RP;	)	
--	-------	-------	--------	-----	------	----	-------------	------	---	--

When attempting to establish the rate of depletion from the root zone because of irreversible chemical binding with the soil, it becomes apparent that the binding rates for both strontium and cesium are strongly dependent on soil

characteristics. Based on investigations by Squire [15], Squire and Middleton [16], and Lassey [17], and a discussion by Coughtrey and Thorne [8], it seems reasonable to assume that 10-20% of the strontium in the soil will become chemically bound to the soil particles at a rate of about 1-5% per year. Cesium reacts even more dramatically with clay, and approximately 85-95% will become chemically bound to the clay particles and this binding will essentially be complete in three years. Chemical binding is not an important consideration for the iodine isotopes being considered, since radioactive decay is the primary mechanism by which they are depleted from the environment.

Based on this information, the values and ranges in Table 4.53 were established for the annual rate at which the nuclides become unavailable for root uptake because of irreversible binding with the soil.

Element	RB	Range of Values
Strontium	0.030	(0.01-0.05)
Cesium	0.25	(0.17-0.32)

Table 4.53. Values for Binding Rate, RB

Using the indicated derived values and ranges for the depletion rates from root uptake, radioactive decay, percolation out of the root zone, and chemical binding with the soil, the recommended values for the total depletion rates were found as the sum of the component parts as indicated in Equation 4.23.

#### REFERENCES

- [1] R. M. Ostmeyer and J. C. Helton, <u>Exposure Pathways Models for</u> <u>Accidental Radionuclide Releases</u>, NUREG/CR-4148, SAND85-0520, Sandia National Laboratories, Albuquerque, NM (unpublished but available upon request).
- [2] <u>Agricultural Statistics 1984</u>, United States Department of Agriculture, Washington, DC, 1984.
- [3] J. R. Simmonds and G. S. Linsley, "A Dynamic System for Transfer of Radioactivity in Terrestrial Food Chains," <u>Nuclear Safety</u>, pp. 766-777, 1981.
- [4] J. R. Simmonds and G.S. Linsley, "Parameters for Modelling the Interception and Retention of Deposits from the Atmosphere by Grain and Green Leafy Vegetables," <u>Health Physics</u>, pp. 679-691, 1982.
- [5] S. Vuori, <u>Radionuclide Transfer to Foodstuffs Via Plant in View of the</u> <u>Data Available After the Chrenobyl Accident</u>, Technical Report, OECD/NEA Group of Experts on Accident Consequences (GRECA), Helsinki, Finland, 1988.
- [6] P. J. Coughtrey and M. C. Thorne, <u>Radionuclide Distribution and</u> <u>Transport in Terrestrial and Aquatic Ecosystems: A Critical Review of</u> <u>Data</u>, A. A. Balkema, Rotterdam, Netherlands, 1983.
- [7] USNRC, <u>Regulatory Guide 1.109</u>; <u>Calculation of Annual Dose from Routine</u> <u>Releases of Reactor Effluents for the Purpose of Evaluating Compliance</u> <u>with 10 CFR Part 50 Appendix I</u>. U.S. Nuclear Regulatory Commission, Washington, DC, 1977.
- [8] F. W. Boone, Y. C. Ng, and J. M. Palms, "Terrestrial Pathways of Radionuclide Particulates," <u>Health Physics</u>, Vol. 41, pp. 735-747, 1981.
- [9] Y. C. Ng, <u>Methodology for Assessing Dose Commitment to Individuals and</u> to the Population from Ingestion of Terrestrial Foods Contaminated by <u>Emissions from a Nuclear Fuel Reprocessing Plant at the Savannah River</u> <u>Plant</u>, Report UCID-17743, University of California, 1978.
- [10] J. E. Till, and H. R. Meyer, eds. <u>Radiological Assessment: A Textbook</u> <u>On Environmental Dose Analysis</u>. U.S. Nuclear Regulatory Commission, Washington, DC, 1983.
- [11] F. O. Hoffman and C. F. Baes III, <u>A Statistical Analysis of Selected</u> <u>Parameters for Predicting Food Chain Transport and Internal Dose of</u> <u>Radionuclides</u>, NUREG/CR-1004, July 1979.
- [12] Y. C. Ng, C. S. Colsher, D. J. Quinn, and S. E. Thompson, <u>Transfer</u> <u>Coefficients for the Prediction of the Dose to Man via the Forage-Cow-</u> <u>Milk Pathway from Radionuclides Released to the Biosphere</u>, UCRL-51939, Lawrence Livermore National Laboratory, Livermore, California, 1977.

- [13] S. Nair and T. Iijima "GRECA Review of Chernobyl Data on Transfer to Animal Products" in <u>Proceedings of Joint OECD (NEA)/CEC Workshop on</u> <u>Recent Advances in Reactor Accident Consequence Assessments</u>, vol. I, Rome, January 25-29, 1988, pp. 169-99, OECD Nuclear Energy Agency, Paris, 1988.
- [14] H-N Jow, J. L. Sprung, J. A. Rollstin, L. T. Ritchie, D. I. Chanin, <u>MELCOR Accident Consequence Code System (MACCS): Model Description</u>. NUREG/CR-4691, SAND86-1562, Sandia National Laboratories, 1990.
- [15] H. M. Squire, "Long Term Studies of Sr-90 in Soils and Pastures," <u>Radiation Botany</u>, pp. 49-67, 1966.
- [16] H. M. Squire and L. J. Middleton, "Behaviour of Cs-137 in Soils and Pastures, A Long Term Experiment," <u>Radiation Botany</u>, pp. 413-423, 1966.
- [17] K. Lassey, "The Transfer of Radiostrontium and Radiocesium from Soil to Diet: Models Consistent with Fallout Analysis, <u>Health Physics</u>, pp. 557-573, 1979.

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# 5.1 <u>Nonfarm Parameters: Recommended Values</u>

Table 5.1 lists the values of nonfarm economic parameters recommended for use in MACCS.

<u>Variable</u>	<u>(Units)</u>	Site	<u>Value</u>	Range*	Definition
DPRATE	(per yr)	A11	0.2	0.1 - 0.3	Property depreciation rate
DSRATE	(per yr)	A11	0.12	0.7 - 0.17	Investment rate of return
EVACST	(\$/day)	A11	\$27	\$25 - \$30	Per diem living expenses for evacuees
FRNFIM		A11	0.8	0.7 - 0.9	Nonfarm
POPCST	(\$)	A11	\$5000	\$3500 - \$7500	Relocation costs for owners of interdicted property
RELCST	(\$/day)	A11	\$27	\$25 - \$30	Per diem living expenses for relocated population
VALWNR	(\$)	Grand Gulf	\$53K	\$43K - \$63K	Per capita value of nonfarm wealth
		Peach Bottom	\$79K	\$69K - \$89K	
		Surry	\$84K	\$74K - \$94K	
		Sequoyah	\$66K	\$56K - \$76K	
		Zion	\$76K	\$66K - \$86K	
		US	\$80K	\$60K - \$100K	

Table 5.1. Economic Parameter Values for MACCS

\* All sampling distributions should be uniform over the stated ranges.

#### 5.2 Nonfarm Parameters: Discussion

Most of the data presented in the following discussion were taken from Statistical Abstract of the United States for 1988. A few figures were taken from <u>Fortune</u> (April 25, 1988) and <u>Forbes</u> (January 11, 1989; June 27, 1988) magazines.

The economic model in the MACCS code treats following costs:

 Daily food and lodging costs per person for short-term relocation of people who evacuate or relocate during the emergency phase of the accident (e.g., the first seven days after the accident),

- (2) Decontamination costs for property that can be returned to use,
- (3) Economic losses incurred while property is temporarily interdicted so that a period of decay following maximum decontamination can reduce yearly doses to acceptable levels (e.g., 5.5 rem in eight years), and
- (4) Economic losses from the permanent interdiction of property.

The model divides economic costs into two groups, farm costs and nonfarm costs. Farm costs are always calculated per hectare of farmland (worth of farmland and improvements per hectare, crop worth per hectare). Nonfarm costs are always calculated per person (temporary and permanent relocation costs per person, tangible worth of nonfarm property per person, decontamination costs of nonfarm property per person), where nonfarm property includes residential, commercial, and public land, improvements, equipment, and possessions.

#### 5.2.1 Relocation Costs

Burke [1] estimated per diem relocation costs (housing, food, transportation) per person to be \$23.70 in 1982 dollars. Correction to 1986 (1986 CPI = 328; 1982 CPI = 289; ratio = 1.13) gives \$26.90 per day per person. Fifty dollars per night for a four-person motel room, and \$3.50, \$4.50, and \$7.00 per person for breakfast, lunch, and dinner plus \$1.50 per day for public transportation, gives \$29.00 per day per person. Burke estimated that mass care per diem costs would be about half the cost of commercial care (hotels and restaurants) and that about one fifth of all relocated persons would be accommodated in mass care facilities. If per diem costs are \$29 per person for the remaining 20 per cent, an average per diem relocation cost of \$26 per person results, which agrees well with Burke's result after correction to 1986 dollars. Therefore, a per diem relocation cost of \$27 per person is recommended for use in the final NUREG-1150 calculations.

#### 5.2.2 Decontamination Costs

The MACCS decontamination model assumes that for both farm and nonfarm property several (no more than three) decontamination methods will be available. For each decontamination method, the model requires a cost (per hectare for farm property and per person for nonfarm property) and a decontamination factor,  $F_D$ , where

#### $F_D = C_i/C_f$

and  $C_i$  and  $C_f$  are the surface contamination levels before and after the decontamination step. Although the costs of the decontamination methods for farm and nonfarm property need not be the same, the set of decontamination factors used for farm property must be the same as the set used for nonfarm property.

#### 5.2.3 Temporary Interdiction Losses

When property is temporarily interdicted, three costs are incurred for nonfarm property and two for farm property. For nonfarm property, the three costs are lost wages per person moved, lost return on investment on the interdicted property, and the cost of the repairs required to return the property to use once the interdiction period ends. For farm property, the second and third costs apply but the first does not (because only the nonfarm economic model treats people).

Burke [1] examined the relocation costs that would be incurred by a person forced to relocate because his home had been interdicted. Since most of his possessions have been contaminated, Burke concluded that moving costs would be small when compared to lost wages, which he estimated to total about \$4000 based on the assumption that each worker relocated would be out of work for 100 to 180 days. Since per capita income in 1986 was \$14,600, if 140 days of lost wages are assumed (the average duration of unemployment from 1972 through 1986 was 15 weeks or 105 days, <u>Reactor Safety Study</u> [2] assumed that interdicted businesses would require about six months to reopen in a new location) and lost wages per person relocated would be \$5600. Correction of Burke's estimate of \$4000 based on 1982 data to 1986 yields \$4500. Accordingly, a moving cost of \$5000 is recommended for use in the final NUREG-1150 calculations.

Assume that all property (land, buildings, equipment, etc.) can be viewed as an investment that yields a rate of return, r, and depreciates at a rate, p, if left untended for some length of time, t. If, for example, the property is interdicted for t years, then two costs are incurred: (1) lost return on investment and (2) repair costs.

Consider a property composed of land (present value L) and improvements (present value I). The total present value of the property is L + I = V, and the fraction of the total present value that is improvements is I/V = f. If this property is now interdicted for t years, the lost return on investment is  $V_t - V$ , where  $V_t = V e^{rt}$  and the repair costs that will be incurred at the end of the interdiction period are I -  $I_t$ , where  $I_t = I e^{-pt}$ . Therefore,

Loss on Investment =  $V_t - V = V e^{rt} - V = V (e^{rt} - 1)$ 

Repair Costs = I - I<sub>+</sub> = I - I 
$$e^{-pt}$$
 = I (1 -  $e^{-pt}$ )

Let the present values of the lost return on investment and the repair costs be V' and I'. Then

V' 
$$e^{rt} = V_t - V = V (e^{rt} - 1)$$
  
V' = V (1 - e^{-rt})  
I'  $e^{rt} = I - I_t = I (1 - e^{-pt})$   
I' = I  $e^{-rt} (1 - e^{-pt})$ 

and C', the present value of the total losses incurred during the interdiction period (t), is

$$C' = V' + I' = V (1 - e^{-rt}) + I e^{-rt} (1 - e^{-pt})$$
$$= V - e^{rt} [V (1 - f + f e^{-pt})]$$

which agrees with Burke et al. [1] and with the Reactor Safety Study [2].

To apply the preceding model, values for V, f, r, and p are needed. Since MACCS calculates farm costs on a per hectare basis and nonfarm costs on a per person basis, the values of V needed are the value of farm property per hectare (per acre) and of nonfarm property per person. State and national data for farm property are available from <u>Statistical Abstract of the United</u> <u>States</u> [3] and are discussed in other data packages. A value for the per person worth of nonfarm residential, commercial, and public property can be estimated from the following data, which were taken from Ref. [3]:

Reproducible Tangible Wealth	=	\$1.98	х	1013
Urban and Built-Up Land	-	4.64	х	10 <sup>4</sup> acres
Total Farm Assets	<b>813</b>	\$7.89	x	1011
Farm Land		\$5.54		
Farm Household Possessions		\$3.05		
1987 U.S. Population	=	2.44	x	10 <sup>8</sup>

Now assuming that nonfarm land costs about 90,000 per acre (typical suburban residential lots are 0.2 acre, land usually constitutes about one fifth of the cost of a house, and the 1986 median value of houses was 92,000, the per person worth of nonfarm residential, commercial, and public property, that is V, is given by

V = [reproducible tangible wealth + value of suburban land - value of farm assets + value of farm household possessions]/[U.S. population] = [\$1.98 x 10<sup>13</sup> + (4.64 x 10<sup>4</sup> acres)(\$9 x 10<sup>4</sup> acre<sup>-1</sup>)

- \$7.89 x 10<sup>11</sup> + \$3.05 x 10<sup>10</sup>]/[2.44 x 10<sup>8</sup> people] = \$7.8 x 10<sup>4</sup>

Therefore, V is about \$80,000 per person.

The value of V is likely to vary significantly by state. This variation can be approximated by multiplying the \$80,000 value by the ratio of a state's per capita income to the national per capita income. The pertinent data are given in Table 5.2.

<u>Reactor</u>	<u>Region</u>	<u>(\$1000) Per Capita Income</u>	<u>V (\$1000)</u>	
•	US	\$14.6	\$80	
Seq	TN	12.0	66	
-	AL	11.3	62	
Zion	WI	13.9	76	
	Chicago	13.2	72	
	IL	15.6	85	
GG	MI	9.7	53	
	LA	11.2	61	
PB	PA	14.2	79	
	MD	16.9	93	
Sur	VA	15.4	84	

Table 5.2. Value to Region

Since investment property is usually purchased by borrowing money (mortgages, equipment loans), r, the total rate of return on any property must be calculated as the dollar weighted sum of the property owner's rate of return on equity ( $r_E$ ) and the debt holder's rate of return on debt ( $r_D$ ). Specifically,

$$r = fr_{E} + (1-f)r_{D},$$

where f = E/V, E is the owner's equity in the property, V is the total value of the property, and V - E = D is the debt on the property (for all manufacturing companies, D/E = 1.8 and thus f = 0.36; for the Fortune 500 companies, D/E = 1.2 and f = 0.45).

Several measures of the rate of return on debt or equity are given in Table 5.3:

Table 5.3. Rates of Return

Measure	<u>Percent</u>
Conventional Mortagage Rate (1970 - 1986)	11.9
Return on Equity	
Forbes Stock Fund Composite (1977 - 1987)	16.4
Standard and Poors 500 (1977 - 1987)	16.9
Fortune 500 (1977 - 1987)	17.2
Fortune 500 (1983 - 1987)	12.8
Fortune 500 (1986)	11.6
Fortune 500 (1987)	13.2
All Manufacturing (1985)	11.6
All Manufacturing (1986)	11.6

These data suggest that 12% is a representative rate of return on both mortagages and equity. Therefore, r equals 12%, which is the value of r used in <u>Reactor Safety Study</u> [2], where r was viewed as the carrying cost (expressed as a percent of value) for interdicted residential property (mortgage rate of 9% plus real estate tax rate of 3%).

Finally, no data on depreciation rates (p) for untended property are available. <u>Reactor Safety Study</u> assumed a value of 20% per year for p after noting that depreciation rates for property that is maintained are typically 3% to 5% per year.

Table 5.4. Recommended Values for VALWF and FRFIM

#### 5.3 Farm Parameters: Recommended Values

Table 5.4 gives the recommended values for VALUE and FRFIM.

Site >	<u>VALWF (\$/ha)</u>	<u>FRFIM (\$/ha)</u>
Grand Gulf (Mississippi)	1824	0.30
Peach Bottom (Pennsylvania)	4469	0.25
Sequoyah (Tennessee)	2708	0.27
Surry (Virginia)	2952	0.25
Zion (Wisconsin)	1754	0.49

VALWF - Value of farm wealth in region (includes all improvements belonging to both public and private sector)

FRFIM - Fraction of farm wealth in region from improvements (includes buildings, equipment, infrastructure (such as roads, utilities, etc.)

#### 5.3.1 Discussion

The total value of farm machinery and implements in 1988 is 84.5 billion dollars according to the U.S. Department of Commerce [4:Table 1086]. Since there are 1002 million acres of farmland in the U.S. [4:Table 1057], the value of machinery and implements per acre is \$84.3 or \$208.2 per/hectare.

The value of farm land and buildings in 1988 [4:Table 1066] in the states being considered can be summarized as in Table 5.5.

Table 5.5.	Value of Farm Land and Buildings (1988)
	Value of Land &
State	<u>Buildings (\$/ha)</u>
Mississippi	654
Pennsylvania	a 1725
Tennessee	1012
Virginia	1111
Wisconsin	626

The data in Table 5.5 were used to determine the value of the variable VALWF for each of the states considered in Table 5.6.

State	Value of Land	
State	<u>&amp; Buildings (\$/ha)</u>	<u>VALWF(\$/ha)</u>
Mississippi (Grand Gulf)	1615	1824
Pennsylvania (Peach Bottom)	4261	4469
Tennessee (Sequoyah)	2500	2708
Virginia (Surry)	2744	2952
Wisconsin (Zion)	1546	1754

Table 5.6. Values for VALWF by State

Based on information from the USDA for 1984 [4:Table 543], Table 5.7 shows the value that was determined for the percentage of the total value of the farm that is accounted for by the buildings for each state being considered.

State	Value of Land and Buildings*	.Value of <u>Buildings</u>	Total Value Represented by Buildings (%)
Mississippi	13814	1975	14.3
Pennsylvania	12015	3196	26.6
Tennessee	12743	2829	22.0
Virginia	10192	2140	21.0
Wisconsin	17436	4830	27.7
* in millions	s of dollars		

Table 5.7. Value of Buildings

This percentage was then used with the values derived for VALWF to determine the current value of buildings/acre, as well as the total value of buildings and equipment/hectare as in Table 5.8.

State	Value of Buildings (\$/ac)	Value of Buildings (\$/ha)	Value of Buildings & Equipment (\$/ha)
Mississippi	138	341	549
Pennsylvania	367	906	1114
Tennessee	211	521	729
Virginia	218	538	746
Wisconsin	265	655	863

Table 5.8. Value of Buildings per Acre

The values of FRFIM in Table 5.9 were derived as the fraction of VALWF that is represented by improvements (buildings and equipment).

Table 5.9. Values of FRFIM

State	FRFIM
Mississippi	0.30
(Grand Gulf) Pennsylvania	0.25
(Peach Bottom) Tennessee	0.27
(Sequoyah) Virginia	0.25
(Surry)	0 40
Wisconsin (Zion)	0.49

#### REFERENCES

- [1] R. P. Burke et al., <u>Economic Risks of Nuclear Power Reactor Accidents</u>, NUREG/CR-3673, Sandia National Laboratories, Albuquerque, NM 1984.
- U.S. Nuclear Regulatory Commission, <u>Reactor Safety Study</u>, Appendix VI, "Calculation of Reactor Accident Consequences," WASH-1400, Washington, DC, 1975.
- [3] <u>Statistical Abstract of the United States</u>, 1988, U.S. Department of Commerce.
- [4] <u>Agricultural Statistics 1984</u>, United States Department of Agriculture, Washington, DC, 1984.

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# APPENDIX A: Sample NUREG-1150 MACCS Input Files

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A.1	ATMOS	A-2
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	Sequoyah	A-48
	Peach Bottom	A-52
	Grand Gulf	A-56

A.1 ATMOS

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\* FILE NAME: 1150AT.INP \* GENERAL DESCRIPTIVE TITLE DESCRIBING THIS "ATMOS" INPUT RIATNAM1001 'ATMOS INPUT FOR FINAL NUREG-1150 CALCULATIONS' \* FLAG TO INDICATE THAT THIS IS THE LAST PROGRAM IN THE SERIES TO BE RUN OCENDAT1001 .FALSE. (SET THIS VALUE TO .TRUE. TO SKIP EARLY AND CHRONC) \* GEOMETRY DATA BLOCK, LOADED BY INPGEO, STORED IN /GEOM/ \* \* NUMBER OF RADIAL SPATIAL ELEMENTS \* GENUMRAD001 26 \* SPATIAL ENDPOINT DISTANCES IN MILES 1.0 \* 0.25 0.5 0.75 END001 3.5 1.5 2.0 7.0 \* 2.5 5.0 END002 3.0 \* END003 10 13 16 20 25 \* END004 30 40 70 50 \* END005 100 150 200 350 500 END006 1000 \* \* \* SPATIAL ENDPOINT DISTANCES IN KILOMETERS \* 
 SITE
 GG
 LS
 PB
 SEQ
 SUR
 ZION

 EXCLUSION ZONE DISTANCE (MI)
 0.432
 0.320
 0.510
 0.364
 0.323
 0.249

 EXCLUSION ZONE DISTANCE (KM)
 0.696
 0.515
 0.820
 0.585
 0.520
 0.400

 EXCLUSION ZONE + 1.0 MI (KM)
 2.305
 2.124
 2.429
 2.194
 2.129
 2.009
 \* \* \* J. 2. 1.61 1.61 1.21 1.61 1.21 1.61 1.21 1.6' 1.21 1 1.21 1 . 50 1.21 .70 1.21 .52 1.21 .82 .40 \*GESPAEND001 2.41 \* STANDARD GRID .40 \*GESPAEND001 2.31 \* GRAND GULF 2.13 \* LA SALLE 2.43 \* PEACH BOTTOM 2.20 \* SEQUOYAH .16 \*GESPAEND001 .82 .59 .52 .80 .40 \*GESPAEND001 \*GESPAEND001 .16 \*GESPAEND001 .16 2.13 \* SURRY .40 \*GESPAEND001 2.01 \* ZION \* PEACH BOTTOM .40 .82 1.21 3.22 4.02 4.83 11.27 16.09 20.92 1.612.435.638.05 GESPAEND001 GESPAEND002 25.75 32.19 GESPAEND003 11.27 GESPAEND004 40.23 48.28 64.37 80.47 112.65 GESPAEND005 160.93 241.14 321.87 563.27 804.67 GESPAEND006 1609.34 \* NUCLIDE DATA BLOCK, LOADED BY INPISO, STORED IN /ISOGRP/, /ISONAM/ \* NUMBER OF NUCLIDES \* ISNUMISO001 60 \* NUMBER OF NUCLIDE GROUPS ISMAXGRP001 9 \* WET AND DRY DEPOSITION FLAGS FOR EACH NUCLIDE GROUP \* \* WETDEP DRYDEP ISDEPFLA001 .FALSE. .FALSE. ISDEPFLA002 .TRUE. .TRUE.

ISDEPFLA003 ISDEPFLA004 ISDEPFLA005 ISDEPFLA006 ISDEPFLA007 ISDEPFLA008 ISDEPFLA009 * * NUCLIDE GROUP * * NUCLIDE GROUP * * ISOTPGRP001 ISOTPGRP003 ISOTPGRP004 ISOTPGRP005 ISOTPGRP005 ISOTPGRP005 ISOTPGRP005 ISOTPGRP008 ISOTPGRP009 ISOTPGRP010 ISOTPGRP011 ISOTPGRP013 ISOTPGRP015 ISOTPGRP016	NUCNAM CO-58 CO-60 KR-85 KR-85M KR-87 KR-88 RB-86 SR-89 SR-90 SR-91 SR-92 Y-90 Y-91 Y-92 Y-93	PARENT NONE NONE NONE NONE NONE NONE NONE N	IGROUP 6 1 1 1 3 5 5 5 5 5 7 7	HAFLIF 6.160E+06 1.660E+08 3.386E+08 1.613E+04 4.560E+03 1.008E+04 1.611E+06 4.493E+06 8.865E+08 3.413E+04 9.756E+03 2.307E+05 5.080E+06	NEW
ISDEPFLA005 ISDEPFLA006 ISDEPFLA007 ISDEPFLA008 ISDEPFLA009 * * NUCLIDE GROUP * * ISOTPGRP001 ISOTPGRP002 ISOTPGRP003 ISOTPGRP003 ISOTPGRP004 ISOTPGRP005 ISOTPGRP005 ISOTPGRP007 ISOTPGRP008 ISOTPGRP009 ISOTPGRP010 ISOTPGRP011 ISOTPGRP013 ISOTPGRP014 ISOTPGRP015	. TRUE. . TRUE. . TRUE. . TRUE. . TRUE. . TRUE. . TRUE. . DATA FOR NUCNAM CO-58 CO-60 KR-85 KR-85M KR-87 KR-88 RB-86 SR-89 SR-90 SR-91 SR-92 Y-90 Y-91 Y-92 Y-93	. TRUE. . TRUE. . TRUE. . TRUE. . TRUE. 9 NUCLIDE PARENT NONE NO	IGROUP 6 1 1 1 3 5 5 5 5 5 7 7	6.160E+06 1.660E+08 3.386E+08 1.613E+04 4.560E+03 1.008E+04 1.611E+06 4.493E+06 8.865E+08 3.413E+04 9.756E+03 2.307E+05	NEW
ISDEPFLA006 ISDEPFLA007 ISDEPFLA008 ISDEPFLA009 * * NUCLIDE GROUP * * ISOTPGRP001 ISOTPGRP002 ISOTPGRP003 ISOTPGRP003 ISOTPGRP004 ISOTPGRP005 ISOTPGRP005 ISOTPGRP005 ISOTPGRP008 ISOTPGRP009 ISOTPGRP010 ISOTPGRP011 ISOTPGRP013 ISOTPGRP014 ISOTPGRP015	. TRUE. . TRUE. . TRUE. . TRUE. . TRUE. . TRUE. DATA FOR NUCNAM CO-58 CO-60 KR-85 KR-85M KR-87 KR-88 RB-86 SR-89 SR-90 SR-91 SR-92 Y-90 Y-91 Y-92 Y-93	. TRUE. . TRUE. . TRUE. . TRUE. 9 NUCLIDE 9 NUCLIDE PARENT NONE	IGROUP 6 1 1 1 3 5 5 5 5 5 7 7	6.160E+06 1.660E+08 3.386E+08 1.613E+04 4.560E+03 1.008E+04 1.611E+06 4.493E+06 8.865E+08 3.413E+04 9.756E+03 2.307E+05	NEW
ISDEPFLA007 ISDEPFLA008 ISDEPFLA009 * * NUCLIDE GROUP * * ISOTPGRP001 ISOTPGRP002 ISOTPGRP003 ISOTPGRP004 ISOTPGRP004 ISOTPGRP005 ISOTPGRP007 ISOTPGRP008 ISOTPGRP008 ISOTPGRP010 ISOTPGRP011 ISOTPGRP012 ISOTPGRP013 ISOTPGRP014 ISOTPGRP015	. TRUE. . TRUE. . TRUE. . TRUE. DATA FOR NUCNAM CO-58 CO-60 KR-85 KR-85M KR-87 KR-88 RB-86 SR-89 SR-90 SR-91 SR-92 Y-90 Y-91 Y-92 Y-93	. TRUE. . TRUE. . TRUE. 9 NUCLIDE 9 NUCLIDE PARENT NONE	IGROUP 6 1 1 1 3 5 5 5 5 5 7 7	6.160E+06 1.660E+08 3.386E+08 1.613E+04 4.560E+03 1.008E+04 1.611E+06 4.493E+06 8.865E+08 3.413E+04 9.756E+03 2.307E+05	NEW
ISDEPFLA008 ISDEPFLA009 * * NUCLIDE GROUP * * * ISOTPGRP001 ISOTPGRP002 ISOTPGRP003 ISOTPGRP004 ISOTPGRP005 ISOTPGRP005 ISOTPGRP005 ISOTPGRP008 ISOTPGRP008 ISOTPGRP009 ISOTPGRP010 ISOTPGRP011 ISOTPGRP013 ISOTPGRP014 ISOTPGRP015	. TRUE. . TRUE. . TRUE. DATA FOR NUCNAM CO-58 CO-60 KR-85 KR-85M KR-87 KR-88 RB-86 SR-89 SR-90 SR-91 SR-92 Y-90 Y-91 Y-92 Y-93	. TRUE. . TRUE. 9 NUCLIDE PARENT NONE SR-90 SR-91 SR-92	IGROUP 6 1 1 1 3 5 5 5 5 5 7 7	6.160E+06 1.660E+08 3.386E+08 1.613E+04 4.560E+03 1.008E+04 1.611E+06 4.493E+06 8.865E+08 3.413E+04 9.756E+03 2.307E+05	NEW
ISDEPFLA009 * * NUCLIDE GROUP * * ISOTPGRP001 ISOTPGRP002 ISOTPGRP003 ISOTPGRP003 ISOTPGRP004 ISOTPGRP005 ISOTPGRP005 ISOTPGRP007 ISOTPGRP008 ISOTPGRP009 ISOTPGRP010 ISOTPGRP011 ISOTPGRP013 ISOTPGRP014 ISOTPGRP015	.TRUE. DATA FOR NUCNAM CO-58 CO-60 KR-85 KR-85M KR-87 KR-88 RB-86 SR-89 SR-90 SR-91 SR-92 Y-90 Y-91 Y-92 Y-93	.TRUE. 9 NUCLIDE PARENT NONE NONE NONE NONE NONE NONE NONE NONE NONE NONE NONE NONE NONE NONE NONE NONE NONE NONE NONE	IGROUP 6 1 1 1 3 5 5 5 5 5 7 7	6.160E+06 1.660E+08 3.386E+08 1.613E+04 4.560E+03 1.008E+04 1.611E+06 4.493E+06 8.865E+08 3.413E+04 9.756E+03 2.307E+05	NEW
ISDEPFLA009 * * NUCLIDE GROUP * * ISOTPGRP001 ISOTPGRP002 ISOTPGRP003 ISOTPGRP003 ISOTPGRP004 ISOTPGRP005 ISOTPGRP005 ISOTPGRP007 ISOTPGRP008 ISOTPGRP009 ISOTPGRP010 ISOTPGRP011 ISOTPGRP013 ISOTPGRP014 ISOTPGRP015	.TRUE. DATA FOR NUCNAM CO-58 CO-60 KR-85 KR-85M KR-87 KR-88 RB-86 SR-89 SR-90 SR-91 SR-92 Y-90 Y-91 Y-92 Y-93	.TRUE. 9 NUCLIDE PARENT NONE NONE NONE NONE NONE NONE NONE NONE NONE NONE NONE NONE NONE NONE NONE NONE NONE NONE NONE	IGROUP 6 1 1 1 3 5 5 5 5 5 7 7	6.160E+06 1.660E+08 3.386E+08 1.613E+04 4.560E+03 1.008E+04 1.611E+06 4.493E+06 8.865E+08 3.413E+04 9.756E+03 2.307E+05	NEW
* NUCLIDE GROUP * NUCLIDE GROUP * * ISOTPGRP001 ISOTPGRP002 ISOTPGRP003 ISOTPGRP004 ISOTPGRP005 ISOTPGRP006 ISOTPGRP007 ISOTPGRP008 ISOTPGRP009 ISOTPGRP010 ISOTPGRP011 ISOTPGRP013 ISOTPGRP014 ISOTPGRP015	DATA FOR NUCNAM CO-58 CO-60 KR-85 KR-85M KR-87 KR-88 RB-86 SR-89 SR-90 SR-91 SR-92 Y-90 Y-91 Y-92 Y-93	9 NUCLIDE PARENT NONE NONE NONE NONE NONE NONE NONE N	IGROUP 6 1 1 1 3 5 5 5 5 5 7 7	6.160E+06 1.660E+08 3.386E+08 1.613E+04 4.560E+03 1.008E+04 1.611E+06 4.493E+06 8.865E+08 3.413E+04 9.756E+03 2.307E+05	NEW
* * ISOTPGRP001 ISOTPGRP002 ISOTPGRP003 ISOTPGRP004 ISOTPGRP005 ISOTPGRP006 ISOTPGRP007 ISOTPGRP009 ISOTPGRP010 ISOTPGRP010 ISOTPGRP012 ISOTPGRP013 ISOTPGRP014 ISOTPGRP015	NUCNAM CO-58 CO-60 KR-85 KR-85M KR-87 KR-88 RB-86 SR-89 SR-90 SR-91 SR-92 Y-90 Y-91 Y-92 Y-93	PARENT NONE NONE NONE NONE NONE NONE NONE N	IGROUP 6 1 1 1 3 5 5 5 5 5 7 7	6.160E+06 1.660E+08 3.386E+08 1.613E+04 4.560E+03 1.008E+04 1.611E+06 4.493E+06 8.865E+08 3.413E+04 9.756E+03 2.307E+05	NEW
* ISOTPGRP001 ISOTPGRP002 ISOTPGRP003 ISOTPGRP004 ISOTPGRP005 ISOTPGRP006 ISOTPGRP007 ISOTPGRP008 ISOTPGRP009 ISOTPGRP010 ISOTPGRP010 ISOTPGRP012 ISOTPGRP013 ISOTPGRP014 ISOTPGRP015	CO-58 CO-60 KR-85 KR-85M KR-87 KR-88 RB-86 SR-89 SR-90 SR-91 SR-92 Y-90 Y-91 Y-92 Y-93	NONE NONE NONE NONE NONE NONE NONE NONE	6 6 1 1 1 3 5 5 5 5 7 7 7	6.160E+06 1.660E+08 3.386E+08 1.613E+04 4.560E+03 1.008E+04 1.611E+06 4.493E+06 8.865E+08 3.413E+04 9.756E+03 2.307E+05	NEW
ISOTPGRP002 ISOTPGRP003 ISOTPGRP004 ISOTPGRP005 ISOTPGRP006 ISOTPGRP007 ISOTPGRP008 ISOTPGRP009 ISOTPGRP010 ISOTPGRP010 ISOTPGRP012 ISOTPGRP013 ISOTPGRP014 ISOTPGRP015	CO-60 KR-85 KR-85M KR-87 KR-88 RB-86 SR-89 SR-90 SR-91 SR-92 Y-90 Y-91 Y-92 Y-93	NONE NONE NONE NONE NONE NONE NONE SR-90 SR-91 SR-92	6 1 1 3 5 5 5 5 7 7 7	1.660E+08 3.386E+08 1.613E+04 4.560E+03 1.008E+04 1.611E+06 4.493E+06 8.865E+08 3.413E+04 9.756E+03 2.307E+05	NEW
ISOTPGRP003 ISOTPGRP004 ISOTPGRP005 ISOTPGRP006 ISOTPGRP007 ISOTPGRP009 ISOTPGRP009 ISOTPGRP010 ISOTPGRP011 ISOTPGRP012 ISOTPGRP013 ISOTPGRP014 ISOTPGRP015	KR-85 KR-85M KR-87 KR-88 RB-86 SR-89 SR-90 SR-91 SR-92 Y-90 Y-91 Y-92 Y-93	NONE NONE NONE NONE NONE NONE SR-90 SR-91 SR-92	1 1 3 5 5 5 5 7 7	3.386E+08 1.613E+04 4.560E+03 1.008E+04 1.611E+06 4.493E+06 8.865E+08 3.413E+04 9.756E+03 2.307E+05	NEW
ISOTPGRP004 ISOTPGRP005 ISOTPGRP007 ISOTPGRP008 ISOTPGRP009 ISOTPGRP010 ISOTPGRP011 ISOTPGRP012 ISOTPGRP013 ISOTPGRP014 ISOTPGRP015	KR-85M KR-87 KR-88 RB-86 SR-89 SR-90 SR-91 SR-92 Y-90 Y-91 Y-92 Y-93	NONE NONE NONE NONE NONE NONE SR-90 SR-91 SR-92	1 1 3 5 5 5 5 7 7 7	1.613E+04 4.560E+03 1.008E+04 1.611E+06 4.493E+06 8.865E+08 3.413E+04 9.756E+03 2.307E+05	NEW
ISOTPGRP005 ISOTPGRP006 ISOTPGRP007 ISOTPGRP008 ISOTPGRP009 ISOTPGRP010 ISOTPGRP011 ISOTPGRP012 ISOTPGRP013 ISOTPGRP014 ISOTPGRP015	KR-87 KR-88 RB-86 SR-89 SR-90 SR-91 SR-92 Y-90 Y-91 Y-92 Y-93	NONE NONE NONE NONE NONE SR-90 SR-91 SR-92	1 3 5 5 5 5 7 7 7	4.560E+03 1.008E+04 1.611E+06 4.493E+06 8.865E+08 3.413E+04 9.756E+03 2.307E+05	NEW
ISOTPGRP006 ISOTPGRP007 ISOTPGRP008 ISOTPGRP009 ISOTPGRP010 ISOTPGRP011 ISOTPGRP012 ISOTPGRP013 ISOTPGRP014 ISOTPGRP015	KR-88 RB-86 SR-89 SR-90 SR-91 SR-92 Y-90 Y-91 Y-92 Y-93	NONE NONE NONE NONE SR-90 SR-91 SR-92	1 3 5 5 5 5 7 7 7	1.008E+04 1.611E+06 4.493E+06 8.865E+08 3.413E+04 9.756E+03 2.307E+05	NEW
ISOTPGRP006 ISOTPGRP007 ISOTPGRP008 ISOTPGRP009 ISOTPGRP010 ISOTPGRP011 ISOTPGRP012 ISOTPGRP013 ISOTPGRP014 ISOTPGRP015	KR-88 RB-86 SR-89 SR-90 SR-91 SR-92 Y-90 Y-91 Y-92 Y-93	NONE NONE NONE NONE SR-90 SR-91 SR-92	1 3 5 5 5 5 7 7 7	1.611E+06 4.493E+06 8.865E+08 3.413E+04 9.756E+03 2.307E+05	NEW
ISOTPGRP007 ISOTPGRP008 ISOTPGRP009 ISOTPGRP010 ISOTPGRP011 ISOTPGRP012 ISOTPGRP013 ISOTPGRP014 ISOTPGRP015	RB-86 SR-89 SR-90 SR-91 SR-92 Y-90 Y-91 Y-92 Y-93	NONE NONE NONE NONE SR-90 SR-91 SR-92	3 5 5 5 7 7 7	1.611E+06 4.493E+06 8.865E+08 3.413E+04 9.756E+03 2.307E+05	NEW
ISOTPGRP008 ISOTPGRP009 ISOTPGRP010 ISOTPGRP011 ISOTPGRP012 ISOTPGRP013 ISOTPGRP014 ISOTPGRP015	SR-89 SR-90 SR-91 SR-92 Y-90 Y-91 Y-92 Y-93	NONE NONE NONE SR-90 SR-91 SR-92	5 5 5 7 7 7	4.493E+06 8.865E+08 3.413E+04 9.756E+03 2.307E+05	NEW
ISOTPGRP009 ISOTPGRP010 ISOTPGRP011 ISOTPGRP012 ISOTPGRP013 ISOTPGRP014 ISOTPGRP015	SR-90 SR-91 SR-92 Y-90 Y-91 Y-92 Y-93	NONE NONE SR-90 SR-91 SR-92	5 5 7 7	8.865E+08 3.413E+04 9.756E+03 2.307E+05	NEW
ISOTPGRP010 ISOTPGRP011 ISOTPGRP012 ISOTPGRP013 ISOTPGRP014 ISOTPGRP015	SR-91 SR-92 Y-90 Y-91 Y-92 Y-93	NONE NONE SR-90 SR-91 SR-92	5 5 7 7	3.413E+04 9.756E+03 2.307E+05	NEW
ISOTPGRP011 ISOTPGRP012 ISOTPGRP013 ISOTPGRP014 ISOTPGRP015	SR-92 Y-90 Y-91 Y-92 Y-93	NONE SR-90 SR-91 SR-92	5 7 7	9.756E+03 2.307E+05	NEW
ISOTPGRP012 ISOTPGRP013 ISOTPGRP014 ISOTPGRP015	Y-90 Y-91 Y-92 Y-93	SR-90 SR-91 SR-92	7 7	2.307E+05	NEW
ISOTPGRP013 ISOTPGRP014 ISOTPGRP015	Y-91 Y-92 Y-93	SR-91 SR-92	7		
ISOTPGRP014 ISOTPGRP015	Y-92 Y-93	SR-92	7	5 በደበፑ∔በፉ	
ISOTPGRP015	Y-93			2.000000000	
ISOTPGRP015			7	1.274E+04	NEW
		NONE	7	3.636E+04	NEW
	ZR-95	NONE	7	5.659E+06	
ISOTPGRP017	ZR-97	NONE	7	6.048E+04	
		ZR-95	7	3.033E+06	
ISOTPGRP018	NB-95				
ISOTPGRP019	MO-99	NONE	6	2.377E+05	
ISOTPGRP020	TC-99M	MO-99	6	2.167E+04	
ISOTPGRP021	RU-103	NONE	6	3.421E+06	
ISOTPGRP022	RU-105	NONE	6	1.598E+04	
ISOTPGRP023	RU-106	NONE	6	3.188E+07	
ISOTPGRP024	RH-105	RU-105	6	1.278E+05	
ISOTPGRP025	SB-127	NONE	4	3.283E+05	
ISOTPGRP026	SB-129	NONE	4	1.562E+04	
ISOTPGRP027	TE-127	SB-127	4	3.366E+04	
			4	9.418E+06	
ISOTPGRP028	TE-127M	NONE			
ISOTPGRP029	TE-129	SB-129	4	4.200E+03	
ISOTPGRP030	TE-129M	NONE	4	2.886E+06	
ISOTPGRP031	TE-131M	NONE	4	1.080E+05	
ISOTPGRP032	TE-132	NONE	4	2.808E+05	
ISOTPGRP033	I-131	TE-131M	2	6.947E+05	
ISOTPGRP034	I-132	TE-132	2	8.226E+03	
ISOTPGRP035	I-133	NONE	2	7.488E+04	
ISOTPGRP036	I-134	NONE	2	3.156E+03	
ISOTPGRP037	I-135	NONE	2	2.371E+04	
	XE-133		ĺ	4.571E+05	
ISOTPGRP038		I-133	4		
ISOTPGRP039	XE-135	I-135	1	3.301E+04	
ISOTPGRP040	CS-134	NONE	3 3	6.501E+07	
ISOTPGRP041	CS-136	NONE	3	1.123E+06	
ISOTPGRP042	CS-137	NONE	3	9.495E+08	
ISOTPGRP043	BA-139	NONE	9	4.986E+03	NEW
ISOTPGRP044	BA-140	NONE	9	1.105E+06	
ISOTPGRP045	LA-140	BA-140	7	1.448E+05	
			7	1.418E+04	NIEW.I
ISOTPGRP046	LA-141	NONE	/		NEW
ISOTPGRP047	LA-142	NONE	7	5.724E+03	NEW
ISOTPGRP048	CE-141	LA-141	8	2.811E+06	PARENT ADDEI
ISOTPGRP049	CE-143	NONE	8	1.188E+05	
ISOTPGRP050	CE-144	NONE	8	2.457E+07	
ISOTPGRP051	PR-143	CE-143	. 7	1.173E+06	
ISOTPGRP052	ND-147	NONE	7	9.495E+05	
ISOTPGRP053	NP-239	NONE	8	2.030E+05	
ISOTPGRP054	PU-238	CM-242	8	2.809E+09	

A-4

7.700E+11 ISOTPGRP055 PU-239 NP-239 8 PU-240 CM-244 8 2.133E+11 ISOTPGRP056 PU-241 NONE ISOTPGRP057 8 4.608E+08 PU-241 AM-241 7 1.366E+10 ISOTPGRP058 ISOTPGRP059 CM-242 NONE 7 1.408E+07 NONE 7 ISOTPGRP060 CM-244 5.712E+08 \*\*\*\*\* \*\*\*\*\*\* \* \* WET DEPOSITION DATA BLOCK, LOADED BY INPWET, STORED IN /WETCON/ \* WASHOUT COEFFICIENT NUMBER ONE, LINEAR FACTOR WDCWASH1001 9.5E-5 (HELTON AFTER JONES, 1986) \* WASHOUT COEFFICIENT NUMBER TWO, EXPONENTIAL FACTOR WDCWASH2001 0.8 (HELTON AFTER JONES, 1986) \* DRY DEPOSITION DATA BLOCK, LOADED BY INPDRY, STORED IN /DRYCON/ \* NUMBER OF PARTICLE SIZE GROUPS <sup>#</sup>See letter from M.A. Cunningham (NRC) to F.T. Harper (SNL) dated Aug. 7, 1990 filed in NRC Public DDNPSGRP001 1 \* DEPOSITION VELOCITY OF EACH PARTICLE SIZE GROUP (M/S) Document Room. DDVDEPOS001 0.01 (VALUE SELECTED BY S. ACHARYA, NRC) # \* DISPERSION PARAMETER DATA BLOCK, LOADED BY INPDIS, STORED IN /DISPY/, /DISPZ/ \* SIGMA = A X \*\* B WHERE A AND B VALUES ARE FROM TADMOR AND GUR (1969) \* LINEAR TERM OF THE EXPRESSION FOR SIGMA-Y, 6 STABILITY CLASSES STABILITY CLASS: A В С D Е F DPCYSIGA001 0.3658 0.2751 0.2089 0.1046 0.1474 0.0722 \* EXPONENTIAL TERM OF THE EXPRESSION FOR SIGMA-Y, 6 STABILITY CLASSES STABILITY CLASS: A В С D  $\mathbf{E}$ F .9031 .9031 .9031 DPCYSIGB001 .9031 .9031 . 9031 \* LINEAR TERM OF THE EXPRESSION FOR SIGMA-Z, 6 STABILITY CLASSES STABILITY CLASS: A в С D  $\mathbf{E}$ F .2 DPCZSIGA001 2.5E-4 1.9E-3 .3 .4 .2 \* EXPONENTIAL TERM OF THE EXPRESSION FOR SIGMA-Z, 6 STABILITY CLASSES \* STABILITY CLASS; A С B D E F 2.125 DPC2SIGB001 1.6021 .8543 .6532 .6021 .6020 \* LINEAR SCALING FACTOR FOR SIGMA-Y FUNCTION, NORMALLY 1 DPYSCALE001 1. LINEAR SCALING FACTOR FOR SIGMA-Z FUNCTION, \* NORMALLY USED FOR SURFACE ROUGHNESS LENGTH CORRECTION. \* (Z1 / Z0) \*\* 0.2, FROM CRAC2 WE HAVE (10 CM / 3 CM) \*\* 0.2 = 1.27 DPZSCALE001 1.27 \* EXPANSION FACTOR DATA BLOCK, LOADED BY INPEXP, STORED IN / EXPAND/

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* TIME BASE FOR EXPANSION FACTOR (SECONDS)
            600. (10 MINUTES)
PMTIMBAS001
* BREAK POINT FOR FORMULA CHANGE (SECONDS)
PMBRKPNT001 3600. (1 hour)
* EXPONENTIAL EXPANSION FACTOR NUMBER 1
             0.2
PMXPFAC1001
* EXPONENTIAL EXPANSION FACTOR NUMBER 2
              0.25
PMXPFAC2001
* PLUME RISE DATA BLOCK, LOADED BY INPLRS, STORED IN /PLUMRS/
* SCALING FACTOR FOR THE CRITICAL WIND SPEED FOR ENTRAINMENT OF A BOUYANT PLUME
 (USED BY FUNCTION CAUGHT)
*
PRSCLCRW001 1.
* SCALING FACTOR FOR THE A-D STABILITY PLUME RISE FORMULA
* (USED BY FUNCTION PLMRIS)
PRSCLADP001
            1.
* SCALING FACTOR FOR THE E-F STABILITY PLUME RISE FORMULA
* (USED BY FUNCTION PLMRIS)
PRSCLEFP001 1.
WAKE EFFECTS DATA BLOCK, LOADED BY INPWAK, STORED IN /BILWAK/
*
*
    SITE
              GG
                  ΡB
                      SEQ SUR
*
                   50
    WIDTH (M) 40
                      40
                           40
    HEIGHT (M) 60
*
                   50
                       40
                           50
*
* BUILDING WIDTH (METERS)
WEBUILDW001 50. * PEACH BOTTOM
* BUILDING HEIGHT (METERS)
WEBUILDH001 50. * PEACH BOTTOM
                    * RELEASE DATA BLOCK, LOADED BY INPREL, STORED IN /RELEAS/
* SPECIFIC DESCRIPTIVE TEXT DESCRIBING THIS PARTICULAR SOURCE TERM
RDATNAM2001 'NUREG-1150 PEACH BOTTOM SOURCE TERM PB-15-1'
* TIME (SECONDS) AFTER ACCIDENT INITIATION WHEN THE ACCIDENT REACHES GENERAL
* EMERGENCY CONDITIONS (AS DEFINED IN NUREG-0654), OR WHEN PLANT PERSONNEL
* CAN RELIABLY PREDICT THAT GENERAL EMERGENCY CONDITIONS WILL BE ATTAINED.
RDOALARMOO1 1.40E4
* SELECTION OF RISK DOMINANT PLUME
RDMAXRIS001 1
* NUMBER OF PLUME SEGMENTS THAT ARE RELEASED
```

RDNUMREL001 2 \* REPRESENTATIVE TIME POINT FOR DISPERSION AND RADIOACTIVE DECAY RDREFTIM001 0.0 0.5 (CORRESPONDING TO HEAD AND MIDPOINT WEATHER) \* \* HEAT CONTENT OF THE RELEASE SEGMENTS (WATTS) \* A VALUE SPECIFIED FOR EACH OF THE RELEASE SEGMENTS 8.0E8 CAL/240 SEC, 5.0E9 CAL/1.4E4 SEC RDPLHEAT001 1.40E7 1.49E6 \* 4.184 CAL/SEC = 1.0 WATT \* \* \* HEIGHT OF THE PLUME SEGMENTS AT RELEASE (METERS) \* A VALUE SPECIFIED FOR EACH OF THE RELEASE SEGMENTS RDPLHITE001 30. 30. \* DURATION OF THE PLUME SEGMENTS (SECONDS) \* A VALUE SPECIFIED FOR EACH OF THE RELEASE SEGMENTS RDPLUDUR001 240. 1.40E4 \* TIME OF RELEASE FOR EACH PLUME (SECS FROM SCRAM) \* A VALUE SPECIFIED FOR EACH OF THE RELEASE SEGMENTS RDPDELAY001 2.51E4 2.58E4 \* RELEASE FRACTIONS FOR NUCLIDE GROUPS IN RELEASE \* GENERIC SOURCE TERM A \* \* GROUP: XE/KR Т CS TESR RU LA CE BA RDRELFRC001 8.5E-3 9.4E-3 0.019 0.026 3.5E-3 0.66 2.8E-3 5.4E-3 0.026 RDRELFRC002 0.34 0.49 0.54 0.72 9.3E-3 0.062 0.61 0.12 0.62 \* 3578 MWTH BWR CORE INVENTORY, 80 0/0 CAPACITY, 3/3 SHUTDOWN INVENTORY SUPPLIED BY D.E. BENNETT, 6/17/86 NUCNAM CORINV(BQ) RDCORINV001 CO-58 2.024E+16 RDCORINV002 CO-60 2.423E+16 RDCORINV003 KR-85 3.317E+16 RDCORINV004 KR-85M 1.206E+18 RDCORINV005 KR-87 2.193E+18 RDCORINV006 2.960E+18 KR-88 RDCORINV007 RB-86 1.856E+15 RDCORINV008 SR-89 3.673E+18 RDCORINV009 SR-90 2.599E+17 RDCORINV010 SR-91 4.771E+18 RDCORINV011 SR-92 4.984E+18 RDCORINV012 Y-90 2.783E+17 RDCORINV013 Y-91 4.482E+18 RDCORINV014 Y-92 5.004E+18 RDCORINV015 Y-93 5.690E+18 RDCORINV016 ZR-95 5.899E+18 RDCORINV017 ZR-97 6.073E+18 RDCORINV018 NB-95 5.581E+18 RDCORINV019 MO-99 6.436E+18 RDCORINV020 TC-99M 5.554E+18 RDCORINV021 RU-103 4.877E+18 3.254E+18 RDCORINV022 RU-105 RDCORINV023 RU-106 1.327E+18 RDCORINV024 RH-105 2.429E+18 RDCORINV025 SB-127 3.077E+17

A-7

RDCORINVO RDCORINVO	26	00-100		1.068E-	L10						
RIA LINUS	-	SB-129 TE-127		2.979E							
				4.010E-							
RDCORINVO		TE-127M									
RDCORINVO	-	TE-129		1.002E-							
RDCORINVO		TE-129M		2.634E-							
RDCORINVO		TE-131M		5.058E-							
RDCORINVO		TE-132		4.944E-							
RDCORINVO	-	I-131		3.417E-							
RDCORINVO	-	I-132		5.020E-							
RDCORINV0	35	I-133		7.172E-	+18						
RDCORINV0	36	I-134		7.850E-	+18						
RDCORINV0	37	I-135		6.751E-	+18						
RDCORINV0	38	XE-133		7.182E-	+18						
RDCORINV0	39	XE-135		1.707E-	+18						
RDCORINV0	40	CS-134		5.596E-	⊦17						
RDCORINV0	41	CS-136		1.501E-	+17						
RDCORINV0	42	CS-137		3.350E-	+17						
RDCORINV0	43	BA-139		6.612E+	+18						
RDCORINV0	44	BA-140		6.522E+							
RDCORINVO		LA-140		6.655E							
RDCORINV0		LA-141		6.145E							
RDCORINVO		LA-142		5.912E-							
RDCORINV0		CE-141		5.922E+							
RDCORINVO		CE-143		5.765E							
RDCORINVO		CE = 144		3.841E							
RDCORINV0		PR-143		5.643E							
RDCORINVO		ND-147		2.522E							
RDCORINVO		ND-147 NP-239		7.516E							
RDCORINVO		PU-238		5.226E							
RDCORINVO	-	PU-239		1.325E							
RDCORINVO		PU-240		1.659E+							
RDCORINVO	-	PU-241		2.856E							
RDCORINVO		AM-241		2.903E							
RDCORINVO		CM-241		7.667E							
RDCORINVO	-			4.137E							
	60										
RDCORINV0	60	CM-244		1.10/10	1.7						
RDCORINVO	-	CM-244 OR TO ADJ	UST TH			ORY					
RDCORINVO * * SCALIN *	G FACTO			IE CORE	INVENT						
RDCORINVO * SCALIN * `REA	G FACTO		UST TH PWR		INVENT	ORY LS	PB	SEQ	SUR	ZION	
RDCORINVO * SCALIN * REA * REA * TYP	G FACTO CTOR E	OR TO ADJ	PWR	IE CORE BWR	INVENT GG : B	LS B	В	P	Р	Р	
RDCORINVO * SCALIN * REA * REA * TYP * POW	G FACTO CTOR E ER LEVI	OR TO ADJ EL (MWTH)	PWR	IE CORE	INVENT GG B 3833	LS B 3292	В 3293	Р 3423	Р 2441	Р 3250	
RDCORINVO * SCALIN * REA * REA * TYP * POW	G FACTO CTOR E	OR TO ADJ EL (MWTH)	PWR	IE CORE BWR	INVENT GG : B	LS B 3292	В 3293	Р 3423	Р 2441	Р 3250	
RDCORINVO * SCALIN * REA * TYP * POW * SCA	G FACTO CTOR E ER LEVI LING FA	OR TO ADJ EL (MWTH) ACTOR	PWR 3412 1.0	HE CORE BWR 3578 1.0	INVENT GG B 3833	LS B 3292	В 3293	Р 3423	Р 2441	Р 3250	
RDCORINVO * SCALIN * REA * TYP * POW * SCA RDCORSCAO	G FACTO CTOR E ER LEVI LING FA	OR TO ADJ EL (MWTH)	PWR 3412 1.0	HE CORE BWR 3578 1.0	INVENT GG B 3833	LS B 3292	В 3293	Р 3423	Р 2441	Р 3250	
RDCORINVO * SCALIN * REA * TYP * POW * SCA RDCORSCAO *	G FACTO CTOR E ER LEVI LING FA	OR TO ADJ EL (MWTH) ACTOR .920 *	PWR 3412 1.0 PEACH	HE CORE BWR 3578 1.0 BOTTOM	INVENT GG 3 8 3833 1.071	LS B 3292 0.920	B 3293 0.920	Р 3423	Р 2441	Р 3250	
RDCORINVO * SCALIN * REA * TYP * POW * SCA RDCORSCAO	G FACTO CTOR E ER LEVI LING FA 01 0 E SIZE	OR TO ADJ EL (MWTH) ACTOR .920 * DISTRIBU	PWR 3412 1.0 PEACH TION C	HE CORE BWR 3578 1.0 BOTTOM DF EACH	INVENT GG 3 3833 1.071 NUCLID	LS B 3292 0.920 E GRO	B 3293 0.920 UP	р 3423 1.003	P 2441 0.715	P 3250 0.953	
RDCORINVO * SCALIN * REA * TYP * POW * SCA * RDCORSCAO * * PARTICL * YOU MUS *	G FACTO CTOR E ER LEVI LING FA 01 0 E SIZE T SPEC:	OR TO ADJ EL (MWTH) ACTOR .920 * DISTRIBU	PWR 3412 1.0 PEACH TION C	HE CORE BWR 3578 1.0 BOTTOM DF EACH	INVENT GG 3 3833 1.071 NUCLID	LS B 3292 0.920 E GRO	B 3293 0.920 UP	р 3423 1.003	P 2441 0.715	P 3250 0.953	
RDCORINVO * SCALIN * REA * TYP * POW * SCA * RDCORSCAO * * PARTICL * YOU MUS * RDPSDISTO	G FACTO CTOR E ER LEVI LING FA 01 0 E SIZE T SPEC: 01	OR TO ADJ EL (MWTH) ACTOR .920 * DISTRIBU IFY A COL 1.	PWR 3412 1.0 PEACH TION C	HE CORE BWR 3578 1.0 BOTTOM DF EACH	INVENT GG 3 3833 1.071 NUCLID	LS B 3292 0.920 E GRO	B 3293 0.920 UP	р 3423 1.003	P 2441 0.715	P 3250 0.953	
RDCORINVO * SCALIN * REA * TYP * POW * SCA * PARTICL * YOU MUS * RDPSDISTO RDPSDISTO	G FACTO CTOR E ER LEVI LING F2 01 0 E SIZE T SPEC: 01 02	OR TO ADJ EL (MWTH) ACTOR .920 * DISTRIBU IFY A COL 1. 1.	PWR 3412 1.0 PEACH TION C	HE CORE BWR 3578 1.0 BOTTOM DF EACH	INVENT GG 3 3833 1.071 NUCLID	LS B 3292 0.920 E GRO	B 3293 0.920 UP	р 3423 1.003	P 2441 0.715	P 3250 0.953	
RDCORINVO * SCALIN * REA * TYP * POW * SCA * RDCORSCAO * * PARTICL * YOU MUS * RDPSDISTO	G FACTO CTOR E ER LEVI LING F2 01 0 E SIZE T SPEC: 01 02	OR TO ADJ EL (MWTH) ACTOR .920 * DISTRIBU IFY A COL 1.	PWR 3412 1.0 PEACH TION C	HE CORE BWR 3578 1.0 BOTTOM DF EACH	INVENT GG 3 3833 1.071 NUCLID	LS B 3292 0.920 E GRO	B 3293 0.920 UP	р 3423 1.003	P 2441 0.715	P 3250 0.953	
RDCORINVO * SCALIN * REA * TYP * POW * SCA * PARTICL * YOU MUS * RDPSDISTO RDPSDISTO RDPSDISTO RDPSDISTO	G FACTO CTOR E ER LEVI LING FZ 01 0 E SIZE T SPEC: 01 02 03 04	OR TO ADJ EL (MWTH) ACTOR .920 * DISTRIBU IFY A COL 1. 1.	PWR 3412 1.0 PEACH TION C	HE CORE BWR 3578 1.0 BOTTOM DF EACH	INVENT GG 3 3833 1.071 NUCLID	LS B 3292 0.920 E GRO	B 3293 0.920 UP	р 3423 1.003	P 2441 0.715	P 3250 0.953	
RDCORINVO * SCALIN * REA * REA * TYP * POW * SCA * RDCORSCAO * * PARTICL * YOU MUS * RDPSDISTO RDPSDISTO RDPSDISTO	G FACTO CTOR E ER LEVI LING FZ 01 0 E SIZE T SPEC: 01 02 03 04	OR TO ADJ EL (MWTH) ACTOR .920 * DISTRIBU IFY A COL 1. 1. 1.	PWR 3412 1.0 PEACH TION C	HE CORE BWR 3578 1.0 BOTTOM DF EACH	INVENT GG 3 3833 1.071 NUCLID	LS B 3292 0.920 E GRO	B 3293 0.920 UP	р 3423 1.003	P 2441 0.715	P 3250 0.953	
RDCORINVO * SCALIN * REA * TYP * POW * SCA * PARTICL * YOU MUS * RDPSDISTO RDPSDISTO RDPSDISTO RDPSDISTO	G FACTO CTOR E ER LEVI LING F2 01 0 E SIZE T SPEC: 01 02 03 04 05	OR TO ADJ EL (MWTH) ACTOR .920 * DISTRIBU IFY A COL 1. 1. 1. 1.	PWR 3412 1.0 PEACH TION C	HE CORE BWR 3578 1.0 BOTTOM DF EACH	INVENT GG 3 3833 1.071 NUCLID	LS B 3292 0.920 E GRO	B 3293 0.920 UP	р 3423 1.003	P 2441 0.715	P 3250 0.953	
RDCORINVO * SCALIN * REA * REA * TYP * POW * SCA * RDCORSCAO * * PARTICL * YOU MUS * RDPSDISTO RDPSDISTO RDPSDISTO RDPSDISTO	G FACTO CTOR E ER LEVI LING FZ 01 0 E SIZE T SPEC: 01 02 03 04 05 06	OR TO ADJ EL (MWTH) ACTOR .920 * DISTRIBU IFY A COL 1. 1. 1. 1. 1.	PWR 3412 1.0 PEACH TION C	HE CORE BWR 3578 1.0 BOTTOM DF EACH	INVENT GG 3 3833 1.071 NUCLID	LS B 3292 0.920 E GRO	B 3293 0.920 UP	р 3423 1.003	P 2441 0.715	P 3250 0.953	
RDCORINVO * SCALIN * REA * TYP * POW * SCA * PARTICL * YOU MUS * RDPSDISTO RDPSDISTO RDPSDISTO RDPSDISTO RDPSDISTO RDPSDISTO	G FACTO CTOR E ER LEVI LING FZ 01 0 E SIZE T SPEC: 01 02 03 04 05 06 07	OR TO ADJ EL (MWTH) ACTOR .920 * DISTRIBU IFY A COL 1. 1. 1. 1. 1. 1.	PWR 3412 1.0 PEACH TION C	HE CORE BWR 3578 1.0 BOTTOM DF EACH	INVENT GG 3 3833 1.071 NUCLID	LS B 3292 0.920 E GRO	B 3293 0.920 UP	р 3423 1.003	P 2441 0.715	P 3250 0.953	
RDCORINVO * SCALIN * REA * TYP * POW * SCA * PARTICL * YOU MUS * RDPSDISTO RDPSDISTO RDPSDISTO RDPSDISTO RDPSDISTO RDPSDISTO RDPSDISTO	G FACTO CTOR E ER LEVE LING F2 01 0 E SIZE T SPEC: 01 02 03 04 05 06 07 08	OR TO ADJ EL (MWTH) ACTOR .920 * DISTRIBU IFY A COL 1. 1. 1. 1. 1. 1. 1.	PWR 3412 1.0 PEACH TION C	HE CORE BWR 3578 1.0 BOTTOM DF EACH	INVENT GG 3 3833 1.071 NUCLID	LS B 3292 0.920 E GRO	B 3293 0.920 UP	р 3423 1.003	P 2441 0.715	P 3250 0.953	
RDCORINVO * SCALIN * REA * TYP * POW * SCA * PARTICL * YOU MUS * RDPSDISTO RDPSDISTO RDPSDISTO RDPSDISTO RDPSDISTO RDPSDISTO RDPSDISTO RDPSDISTO	G FACTO CTOR E ER LEVE LING F2 01 0 E SIZE T SPEC: 01 02 03 04 05 06 07 08 09	OR TO ADJ EL (MWTH) ACTOR .920 * DISTRIBU IFY A COL 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	PWR 3412 1.0 PEACH TION C UMN OF	HE CORE BWR 3578 1.0 BOTTOM OF EACH 7 DATA H	INVENT GG 3 3833 1.071 NUCLID FOR EAC	LS B 3292 0.920 E GROI H OF	В 3293 0.920 UP THE PA	P 3423 1.003 RTICLE	P 2441 0.715 SIZE	P 3250 0.953 GROUPS	
RDCORINVO * SCALIN * REA * TYP * POW * SCA * PARTICL * YOU MUS * RDPSDISTO RDPSDISTO RDPSDISTO RDPSDISTO RDPSDISTO RDPSDISTO RDPSDISTO RDPSDISTO RDPSDISTO RDPSDISTO	G FACTO CTOR E ER LEVI LING F2 01 0 E SIZE T SPEC: 01 02 03 04 05 06 07 08 09	OR TO ADJ EL (MWTH) ACTOR .920 * DISTRIBU IFY A COL 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	PWR 3412 1.0 PEACH TION C UMN OF	HE CORE BWR 3578 1.0 BOTTOM OF EACH 7 DATA H	INVENT GG 3 3833 1.071 NUCLID FOR EAC	LS B 3292 0.920 E GROI H OF 1	B 3293 0.920 UP THE PA	P 3423 1.003 RTICLE	P 2441 0.715 SIZE	P 3250 0.953 GROUPS	
RDCORINVO * SCALIN * REA * TYP * POW * SCA * RDCORSCAO * * PARTICL * YOU MUS * RDPSDISTO RDPSDIST	G FACTO CTOR E ER LEVE LING F2 01 0 E SIZE T SPEC: 01 02 03 04 05 06 07 08 09 ******	OR TO ADJ EL (MWTH) ACTOR .920 * DISTRIBU IFY A COL 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	PWR 3412 1.0 PEACH TION C UMN OF	HE CORE BWR 3578 1.0 BOTTOM OF EACH 7 DATA H	INVENT GG 3 3833 1.071 NUCLID FOR EAC	LS B 3292 0.920 E GROI H OF 1	B 3293 0.920 UP THE PA	P 3423 1.003 RTICLE	P 2441 0.715 SIZE	P 3250 0.953 GROUPS	
RDCORINVO * SCALIN * REA * TYP * POW * SCA * RDCORSCAO * * PARTICL * YOU MUS * RDPSDISTO RDPSDI	G FACTO CTOR E ER LEVE LING F2 01 0 E SIZE T SPEC: 01 02 03 04 05 06 07 08 09 ******	OR TO ADJ EL (MWTH) ACTOR .920 * DISTRIBU IFY A COL 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	PWR 3412 1.0 PEACH TION C UMN OF	HE CORE BWR 3578 1.0 BOTTOM OF EACH 7 DATA H	INVENT GG 3 3833 1.071 NUCLID FOR EAC	LS B 3292 0.920 E GROI H OF 1	B 3293 0.920 UP THE PA	P 3423 1.003 RTICLE	P 2441 0.715 SIZE	P 3250 0.953 GROUPS	
RDCORINVO * SCALIN * REA * TYP * POW * SCA * PARTICL * YOU MUS * RDPSDISTO R	G FACTO CTOR E ER LEVI LING F2 01 0 E SIZE T SPEC: 01 02 03 04 05 06 07 08 09 ****** CONTROI 01 0	OR TO ADJ EL (MWTH) ACTOR .920 * DISTRIBU IFY A COL 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	PWR 3412 1.0 PEACH TION C UMN OF	HE CORE BWR 3578 1.0 BOTTOM DF EACH F DATA H	INVENT GG 3833 1.071 NUCLID FOR EAC	LS B 3292 0.920 E GROU H OF 7	B 3293 0.920 UP THE PA	P 3423 1.003 RTICLE	P 2441 0.715 SIZE ******	P 3250 0.953 GROUPS	
RDCORINVO * SCALIN * REA * TYP * POW * SCA * RDCORSCAO * * PARTICL * YOU MUS * RDPSDISTO RDPSDI	G FACTO CTOR E ER LEVI LING F2 01 0 E SIZE T SPEC: 01 02 03 04 05 06 07 08 09 ****** CONTROI 01 0	OR TO ADJ EL (MWTH) ACTOR .920 * DISTRIBU IFY A COL 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	PWR 3412 1.0 PEACH TION C UMN OF	HE CORE BWR 3578 1.0 BOTTOM DF EACH F DATA H	INVENT GG 3833 1.071 NUCLID FOR EAC	LS B 3292 0.920 E GROU H OF 7	B 3293 0.920 UP THE PA	P 3423 1.003 RTICLE	P 2441 0.715 SIZE ******	P 3250 0.953 GROUPS	
RDCORINVO * SCALIN * REA * POW * SCA * OUTPUT * OUTPUT * OUTPUT * OUTPUT * NAME OF	G FACTO CTOR E ER LEVI LING F2 01 0 E SIZE T SPEC: 01 02 03 04 05 06 07 08 09 ****** CONTROI 01 0 THE NU	OR TO ADJ EL (MWTH) ACTOR .920 * DISTRIBU IFY A COL 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	PWR 3412 1.0 PEACH TION C UMN OF	HE CORE BWR 3578 1.0 BOTTOM DF EACH F DATA H	INVENT GG 3833 1.071 NUCLID FOR EAC	LS B 3292 0.920 E GROU H OF 7	B 3293 0.920 UP THE PA	P 3423 1.003 RTICLE	P 2441 0.715 SIZE ******	P 3250 0.953 GROUPS	

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* METEOROLOGICAL SAMPLING DATA BLOCK
 METEOROLOGICAL SAMPLING OPTION CODE:
*
 METCOD = 1, USER SPECIFIED DAY AND HOUR IN THE YEAR (FROM MET FILE),
*
           2, WEATHER CATEGORY BIN SAMPLING,
           3, 120 HOURS OF WEATHER SPECIFIED ON THE ATMOS USER INPUT FILE,
           4, CONSTANT MET (BOUNDARY WEATHER USED FROM THE START),
           5, STRATIFIED RANDOM SAMPLES FOR EACH DAY OF THE YEAR.
M1METCOD001 2
* LAST SPATIAL INTERVAL FOR MEASURED WEATHER
M2LIMSPA001 25
      BOUNDARY WEATHER, NO RAIN, WIND SPEED = 0.5 M/S, A-STABILITY,
     MIXING HEIGHT = 1000 M, APPLIES TO THE LAST SPATIAL INTERVAL
*
      (500 - 1000 MILES)
*
* BOUNDARY WEATHER MIXING LAYER HEIGHT
M2BNDMXH001 1000. (METERS)
* BOUNDARY WEATHER STABILITY CLASS INDEX
M2IBDSTB001 1
                  (A-STABILITY)
* BOUNDARY WEATHER RAIN RATE
M2BNDRAN001 0.
                  (0 MM / HOUR = NO RAIN)
* BOUNDARY WEATHER WIND SPEED
M2BNDWND001 0.5
                   (M / S)
* NUMBER OF SAMPLES PER BIN
M4NSMPLS001 4 (THIS NUMBER SHOULD BE SET TO 4 FOR RISK ASSESSMENT)
* NUMBER OF BINS TO BE SAMPLED (WHEN NSMPLS = 0)
*M4NSBINS001 6
*
         BIN NUMBER
                        SAMPLE SIZE
           INDXBN
                          INWGHT
*M4SMPLDF001 3
                            8
*M4SMPLDF002 4
                            16
             5
*M4SMPLDF003
                            12
*M4SMPLDF004
             6
                             4
*M4SMPLDF005
              7
                             4
*M4SMPLDF006
             - 8
                             4
* NUMBER OF RAIN DISTANCE INTERVALS FOR BINNING
M4NRNINT001 6
* ENDPOINTS OF THE RAIN DISTANCE INTERVALS (KILOMETERS)
* NOTE: THESE MUST BE CHOSEN TO MATCH THE SPATIAL ENDPOINT DISTANCES
*
        SPECIFIED FOR THE ARRAY SPAEND (10 % ERROR IS ALLOWED).
             2.0
                   3.5
                         7.0
                                13.0
                                       25.0
                                              50.0
                                                     MILES
M4RNDSTS001 3.22 5.63 11.27 20.92 40.23 80.47 KM
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* NUMBER OF RAIN INTENSITIY BREAKPOINTS
*
M4NRINTN001 3
*
* RAIN INTENSITY BREAKPOINTS FOR WEATHER BINNING (MILLIMETERS PER HOUR)
*
M4RNRATE001 1. 2. 3.
*
* INITIAL SEED FOR RANDOM NUMBER GENERATOR
*
M4IRSEED001 1
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A.2 EARLY

\*\*\*\*\*\* \* FILE NAME: 1150ER.INP \* GENERAL DESCRIPTIVE TITLE DESCRIBING THIS "EARLY" INPUT FILE MIEANAM1001 'EARLY INPUT FOR FINAL NUREG-1150 CALCULATIONS' \* FLAG TO INDICATE THAT THIS IS THE LAST PROGRAM IN THE SERIES TO BE RUN (SET THIS VALUE TO .TRUE. TO SKIP CHRONC) MIENDAT2001 .FALSE. 1 \* \* DISPERSION MODEL OPTION CODE: STRAIGHT LINE 2 \* WIND-SHIFT WITH ROTATION 3 WIND-SHIFT WITHOUT ROTATION \* MIIPLUME001 2 \* NUMBER OF FINE GRID SUBDIVISIONS USED BY THE MODEL MINUMFIN001 7 (3, 5 OR 7 ALLOWED) \* LEVEL OF DEBUG OUTPUT REQUIRED, NORMAL RUNS SHOULD SPECIFY ZERO MIIPRINT001 0 \* FLAG INDICATING IF WIND-ROSES FROM ATMOS ARE TO BE OVERRIDDEN MIOVRRID001 .FALSE. (USE THE WIND ROSE CALCULATED FOR EACH WEATHER BIN) \* LOGICAL FLAG SIGNIFYING THAT THE BREAKDOWN OF RISK BY WEATHER CATEGORY \* BIN ARE TO BE PRESENTED TO SHOW THEIR RELATIVE CONTRIBUTION TO THE MEAN RISBIN MIRISCAT001 .FALSE. \* POPULATION DISTRIBUTION DATA BLOCK, LOADED BY INPOPU, STORED IN /POPDAT/ PDPOPFLG001 FILE \*PDPOPFLG001 UNIFORM \*PDIBEGIN001 1 (SPATIAL INTERVAL AT WHICH POPULATION BEGINS) \*PDPOPDEN001 50. (POPULATION DENSITY (PEOPLE PER SQUARE KILOMETER)) \* ORGAN DEFINITION DATA BLOCK, LOADED BY INORGA, STORED IN /EARDIM/ AND /ORGNAM/ \* NUMBER OF ORGANS DEFINED FOR HEALTH EFFECTS ODNUMORG001 9 \* NAMES OF THE ORGANS DEFINED FOR HEALTH EFFECTS ODORGNAM001 'SKIN', 'EDEWBODY', 'LUNGS', 'RED MARR', 'LOWER LI', 'STOMACH', ODORGNAM002 'THYROIDH', 'BONE SUR', 'BREAST' \*ODORGNAM003 'EMBRYO', 'FETAL BONE', 'FETAL OTHR', 'GONADS', \*\*\*\*\*\*\* \* SHIELDING AND EXPOSURE FACTORS, LOADED BY INDFAC, STORED IN /EADFAC/ \* THREE VALUES OF EACH PROTECTION FACTOR ARE SUPPLIED, \* ONE FOR EACH TYPE OF ACTIVTY: \* ACTIVITY TYPE: 1 - EVACUEES WHILE MOVING \* 2 - NORMAL ACTIVITY IN SHELTERING AND EVACUATION ZONE 3 - SHELTERED ACTIVITY

\*

```
* CLOUD SHIELDING FACTOR
    SITE GG PB SEQ SUR ZION
SHELTERING 0.7 0.5 0.65 0.6 0.5
*
*
            EVACUEES NORMAL SHELTER
                      0.75
                               0.5
                                         PEACH BOTTOM SHELTERING VALUE
SECSFACT001
                1.
                                     *
* PROTECTION FACTOR FOR INHALATION
                                           VALUES FOR NORMAL ACTIVITY
              1.
                     0.41
                               0.33
                                      *
SEPROTIN001
                                           AND SHELTERING SELECTED
                                           BY S. ACHARYA, NRC.
* BREATHING RATE (CUBIC METERS PER SECOND)
SEBRRATE001 2.66E-4 2.66E-4 2.66E-4
* SKIN PROTECTION FACTOR
SESKPFAC001
                                           VALUES FOR NORMAL ACTIVITY
                1. 0.41
                               0.33
                                      *
                                           AND SHELTERING SELECTED
                                           BY S. ACHARYA, NRC.
* GROUND SHIELDING FACTOR
                GG
                      PB
                          SEQ SUR ZION
    SITE
    SHELTERING 0.25 0.1 0.2 0.2
                                    0.1
SEGSHFAC001
                0.5
                       0.33
                               0.1
                                      *
                                           VALUE FOR NORMAL ACTIVITY
                                           SELECTED BY S. ACHARYA, NRC;
                                           PEACH BOTTOM SHELTERING VALUE.
 RESUSPENSION INHALATION MODEL CONCENTRATION COEFFICIENT (/METER)
*
*
   RESCON = 1.E-4 IS APPROPRIATE FOR MECHANICAL RESUSPENSION BY VEHICLES.
   RESHAF = 2.11 DAYS CAUSES 1.E-4 TO DECAY IN ONE WEEK TO 1.E-5, THE VALUE
*
*
   OF RESCON USED IN THE FIRST TERM OF THE LONG-TERM RESUSPENSION EQUATION
   USED IN CHRONC.
SERESCON001
             1.E-4
                       (RESUSPENSION IS TURNED ON)
* RESUSPENSION CONCENTRATION COEFFICIENT HALF-LIFE (SEC)
SERESHAF001
             1.82E5
                       (2.11 DAYS)
* EVACUATION ZONE DATA BLOCK, LOADED BY EVNETW, STORED IN /NETWOR/, /EOPTIO/
* SPECIFIC DESCRIPTION OF THE EMERGENCY RESPONSE STRATEGY BEING USED
EZEANAM2001 'EVACUATION TO 10 MILES WITH HOT SPOT AND NORMAL RELOCATION'
*
 THE TYPE OF WEIGHTING TO BE APPLIED TO THE EMERGENCY RESPONSE SCENARIOS
*
   YOU MUST SUPPLY A VALUE OF 'TIME' OR 'PEOPLE'
EZWTNAME001 'PEOPLE'
* WEIGHTING FRACTION APPLICABLE TO THIS SCENARIO
EZWTFRAC001
              1.0
                        (100% OF THE PEOPLE WITHIN 10 MILES EVACUATE)
* LAST RING IN THE MOVEMENT ZONE
                        (EVACUEES ARE DIRECTED AWAY FROM THE PATH OF
EZLASMOV001
             15
                         THE RELEASE AFTER TRAVELLING TO 20 MILES)
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\* FIRST SPATIAL INTERVAL IN THE EVACUATION ZONE (NO INNER SHELTER ZONE) EZINIEVA001 1 \* OUTER BOUNDS OF THE 3 EVACUATION ZONES (0 MEANS THE ZONE IS NOT DEFINED) EZLASEVA001 0 0 12 (EVACUATION FROM A SINGLE ZONE OUT TO 10 MILES) SITE GG PB SEQ SUR EDELAY (HR) 1.25 1.5 2.3 2.0 ESPEED (M/S) 3.7 4.8 1.8 1.8 \* EDELAY = CLDELAY + 0.5 HRCLDELAY = DELAY BETWEEN WARNING OF PUBLIC TO BEGIN EVACUATION AND TIME EVACUATION ACTUALLY BEGINS, VALUES USED ARE DEVELOPED FROM SITE SPECIFIC CLEAR TIME STUDIES 0.5 HR = MEAN (EXPECTED) TIME FROM OCCURENCE GENERAL EMERGENCY CONDITIONS TO WARNING OF PUBLIC (SYRENS, BROADCAST) \* EVAUATION DELAY TIMES (SECONDS) FOR THE 3 EVACUATION ZONES EZEDELAY001 0. 0. 5400. \* PEACH BOTTOM \* RADIAL EVACUATION SPEED (METERS / SECOND) EZESPEED001 4.8 \* PEACH BOTTOM \* EMERGENCY RESPONSE DEFINITION, LOADED BY INPENR, STORED IN /SRZONE/,/PHASE2/ \* TIME TO TAKE SHELTER IN THE INNER SHELTER ZONE (SECONDS FROM ALARM) SRTTOSH1001 0. (THIS ZONE IS NULL BECAUSE INIEVA=0) \* SHELTER TIME IN THE INNER SHELTER ZONE (SECONDS) SRSHELT1001 0. (THIS ZONE IS NULL BECAUSE INIEVA=0) \* LAST RING OF THE OUTER SHELTER ZONE SRLASHE2001 0 (THIS ZONE IS NULL) \* TIME TO TAKE SHELTER IN THE OUTER SHELTER ZONE (SECONDS FROM ALARM) SRTTOSH2001 0. (THIS ZONE IS NULL) \* SHELTER TIME IN THE OUTER SHELTER ZONE (SECONDS) SRSHELT2001 0. (THIS ZONE IS NULL) DURATION OF THE EMERGENCY PHASE (SECONDS FROM PLUME ARRIVAL) SRENDEMP001 604800. (ONE WEEK) \* CRITICAL ORGAN FOR RELOCATION DECISIONS SRCRIORG001 'EDEWBODY' \* HOT SPOT RELOCATION TIME (SECONDS FROM PLUME ARRIVAL) SRTIMHOT001 43200. (ONE-HALF DAY)

\* NORMAL RELOCATION TIME (SECONDS FROM PLUME ARRIVAL) SRTIMNRM001 86400. (ONE DAY) \* HOT SPOT RELOCATION DOSE CRITERION THRESHOLD (SIEVERTS) (PROJECTED WHOLE BODY DOSE OF 50 IN 1 WEEK TRIGGERS SRDOSHOT001 0.5 RELOCATION AT ONE-HALF DAY) \* NORMAL RELOCATION DOSE CRITERION THRESHOLD (SIEVERTS) SRDOSNRM001 0.25 (PROJECTED WHOLE BODY DOSE OF 25 IN 1 WEEK TRIGGERS RELOCATION AT ONE DAY) \* EARLY FATALITY MODEL PARAMETERS, LOADED BY INEFAT, STORED IN /EFATAL/ \* NUMBER OF EARLY FATALITY EFFECTS EFNUMEFA001 3 LD50 by t \* EFFACA EFFACB EFFTHR 1 7 14 30 200 365 \* ORGNAM EFATAGRP001 'RED MARR' EFATAGRP002 'LUNGS' 8 16 1.5 4. 6. 4 10.0 7. 10 160 5.0 370 920 EFATAGRP003 'LOWER LI' 15. 10. 7.5 15 35 \* NOTE: LUNG PARAMETERS TAKEN FROM LETTER FROM B. SCOTT TO N. WALD DATED 3/7/87; SHAPE FACTOR OF 7 IS APPROPRIATE FOR EXTERNAL AND INTERNAL \* \* DOSE DELIVERED AT THE SAME TIME. \* EARLY INJURY MODEL PARAMETERS, LOADED BY INEINJ, STORED IN /EINJUR/ \* NUMBER OF EARLY INJURY EFFECTS EINUMEINO01 7 D50 vs t ORGNAM EISUSC EITHRE EIFACA EIFACB 1 7 10 21 EINAME EINJUGRP001 'PRODROMAL VOMIT' 'STOMACH' 1. .5 2. 3. 2 5 'STOMACH' 1. 1. 3. 'LUNGS' 1. 5. 10. 'SKIN' 1. 3. 6 EINJUGRP002 'DIARRHEA' 2.5 36 EINJUGRP003 'PNEUMONITIS' 7. = DEATH 'SKIN' 1. 3. 6. 'SKIN' 1. 10. 20. 'THYROIDH' 1. 40. 240. 'THYROIDH' 1. 2. 60. EINJUGRP004 'SKIN ERYTHEMA' 5. 6 20 EINJUGRP005 'TRANSEPIDERMAL' 'SKIN' 5. 20 80 EINJUGRP006 'THYROIDITIS' 2. 240 EINJUGRP007 'HYPOTHYROIDISM' 1.3 2.2 TO 270d 1. TO 1757 60 0.012 0.1 2. 2.2 TO 270d 0.0048 0. 2.5 1. TO 175d 0.0053 0.05 0.7 0.4 TO 119d \*EINJUGRP008 'FETAL DEATH' 'EMBRYO' \*EINJUGRP009 'MENTAL RETARD' 'EMBRYO' \*EINJUGRP010 'MICROCEPHALY' 'EMBRYO' NOTE: THYROIDH ACUTE DOSE CONVERSION FACTORS ARE USED TO CALCULATE THYROID INJURIES. WHEN THESE DOSE FACTORS WERE CALCULATED, INHALATION DOSE FACTORS FOR IODINE ISOTOPES WERE REDUCED BY A FACTOR OF FIVE TO ACCOUNT FOR THE REDUCED EFFECTIVENESS OF DOSE FROM IODINE ISOTOPES.  $0.0048 = 0.012 \times 0.4$ ;  $0.0053 = 0.012 \times (17X7)/270$ . \* ACUTE EXPOSURE CANCER PARAMETERS, LOADED BY INACAN STORED IN /ACANCR/. \* NUMBER OF ACUTE EXPOSURE CANCER EFFECTS LCNUMACA001 7 \* DOSE THRESHOLD FOR LINEAR DOSE RESPONSE (SV) LCACTHRE001 1.5 ACNAME ORGNAM ACSUSC DOSEFA DOSEFB CFRISK CIRISK

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<b>n</b> -	τu

	ANCER IS ASSUMED TO BE LINEAR		
* GENETT	C EFFECTS ARE INTEGRATED OVER		THE GENERATIONS (SEE
	D REPORT FOR FRACTIONS IN EACH		
****	****	*******	****
	ONS BLOCK, LOADED BY INOUT1, S		
	OF A GIVEN EFFECT (LATENT CANC		
*	· · · · · · · · · · · · · · · · · · ·	,	
* NUMBER OF DES *	IRED RESULTS OF THIS TYPE		
TYPE1NUMBER *	35		
TYPE1OUT001	'ERL FAT/TOTAL'	1 26	(0 TO 1000 MILES)
TYPE1OUT002	'ERL INJ/PRODROMAL VOMIT'	1 26	
TYPE1OUT003	'ERL INJ/DIARRHEA'	1 26	
TYPE1OUT004	'ERL INJ/PNEUMONITIS'	1 26	
TYPE1OUT005	'ERL INJ/THYROIDITIS'	1 26	• .
TYPE1OUT006	'ERL INJ/HYPOTHYROIDISM'	1 26	
TYPE1OUT007	'ERL INJ/SKIN ERYTHEMA'	1 26	
TYPE1OUT008	'ERL INJ/TRANSEPIDERMAL'	1 26	
TYPE1OUT009	'CAN FAT/TOTAL'	1 26	
TYPE1OUT010	'CAN FAT/LUNG'	1 26	
TYPE1OUT011	'CAN FAT/THYROID'	1 26	
TYPE1OUT012	'CAN FAT/BREAST'	1 26	
TYPE1OUT013	'CAN FAT/GI'	1 26	
TYPE1OUT014	'CAN FAT/LEUKEMIA'	1 26	
TYPE1OUT015	'CAN FAT/BONE'	1 26     1 26	
TYPE1OUT016 TYPE1OUT017	'CAN FAT/OTHER'	1 26     1 26	
TYPE1OUT018	'CAN INJ/TOTAL' 'ERL FAT/TOTAL'	1 20 1 19	(0 TO 50 MILES)
TYPE1OUT019	'ERL INJ/PRODROMAL VOMIT'	1 19 1 19	(0 10 50 MILES)
TYPE1OUT020	'ERL INJ/DIARRHEA'	1 19	
TYPE1OUT021	'ERL INJ/PNEUMONITIS'	1 19	
TYPE1OUT022	'ERL INJ/THYROIDITIS'	1 19	
TYPE1OUT023	'ERL INJ/HYPOTHYROIDISM'	1 19	
TYPE1OUT024	'ERL INJ/SKIN ERYTHEMA'	1 19	
TYPE1OUT025	'ERL INJ/TRANSEPIDERMAL'	1 19	
TYPE1OUT026	'CAN FAT/TOTAL'	1 19	
TYPE1OUT027	'ERL FAT/TOTAL'	1 12	(0 TO 10 MILES)
TYPE1OUT028	'ERL INJ/PRODROMAL VOMIT'	1 12	· · ·
TYPE1OUT029	'ERL INJ/DIARRHEA'	1 12	
TYPE1OUT030	'ERL INJ/PNEUMONITIS'	1 12	· · ·
TYPE1OUT031	'ERL INJ/THYROIDITIS'	1 12	

DCUUCTU	DOTO MUTOLIOIDI	GONADO	±.	<b>.</b> .	0.0	0.0	5.00 1
*LCANCER	S014 'TRANSLOCAT'	'GONADS'		0.5	0.5	0.0	2.0E-3
*LCANCER	S015 'M-FACTOR'	'GONADS '	1.	0.5	0.5	0.0	1.4E-2
*LCANCER	S016 'PREG LOSS'	'GONADS '	1.	0.74	0.26	0.0	3.5E-2
*							
* NOTE:	THYROIDH LIFETIME	DOSE CONVERSION 1	FACTORS	ARE USED	TO CA	LCULATE	
*	THYROID CANCERS.	WHEN THESE DOSE 1	FACTORS	WERE CAL	CULATE	D, INHA	LATION
*	AND INGESTION DOSI	E FACTORS FOR IOD	INE ISOT	OPES WER	E REDU	CED BY	А
*	FACTOR OF THREE TO	ACCOUNT FOR THE	REDUCED	EFFECTI	VENESS	OF DOS	E FROM
*	IODINE ISOTOPES.	0.74 = (17 + 9)/	(17 + 9	+ 9) AND	0.26	= 1.0 -	0.74.
*	GONADS DOSE FACTOR						
*	SKIN CANCER IS ASS	SUMED TO BE LINEAD	R (SEE N	UREG/CR-	4214 P.	AGE II-	122).
*	GENETIC EFFECTS AN						
*	HARVARD REPORT FOR					•	
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*							
LCANCERS001 'I	LEUKEMIA '	'RED MARR'	1.	.39	.61	3.7E-3	3.7E-3
LCANCERS002 'E	BONE '	'BONE SUR'	1.	.39	.61	1.5E-4	1.5E-4
LCANCERS003 'E	BREAST'	'BREAST'	1.	·1.	0.	6.0E-3	1.7E-2
LCANCERS004 'I	LUNG '	'LUNGS'	1.	.39	.61	5.1E-3	5.7E-3
LCANCERS005 '7	THYROID'	'THYROIDH'	1.	1.	Ο.	7.2E-4	7.2E-3
LCANCERSOO6 'G	GI'	'LOWER LI'	1.	.39	.61	1.5E-2	2.5E-2
LCANCERS007 'C	OTHER '	'LOWER LI'	1.	.39	.61	7.5E-3	1.3E-2
*LCANCERS008 '	'SKIN'	'SKIN'	1.	1.0	0.0	0.0	6.7E-3
*LCANCERS009 '	'LEUK UTERO'	'FETAL BONE'	0.012	0.4	0.0	3.0E-2	3.0E-2
*LCANCERS010 '	'OTHR UTERO'	'FETAL OTHR'	0.012	0.4	0.0	3.0E-2	3.0E-2
*LCANCERS011 '	'DOMINANT'	'GONADS '	1.	0.5	0.5	0.0	1.4E-2
*LCANCERS012 '	'X-LINKED'	'GONADS'	1.	0.5	0.5	0.0	4.4E-2
*LCANCERS013 '	'ANEUPLOIDY'	'GONADS'	1.	1.	0.0	0.0	5.0E-4
*LCANCERS014 '	'TRANSLOCAT'	'GONADS'	1.	0.5	0.5	0.0	2.0E-3
*LCANCERS015 '	'M-FACTOR '	'GONADS'	1.	0.5	0.5	0.0	1.4E-2
*LCANCERSOIG '	PREG LOSS!	'CONADS'	1	0 74	0.26	0 0	3 5E-2

TYPE10IT032 'ERL INJ/HYPOTHYROIDISM' 12 1 'ERL INJ/SKIN ERYTHEMA' TYPE1OUT033 1 12 'ERL INJ/TRANSEPIDERMAL' 1 12 TYPE1OUT034 'CAN FAT/TOTAL' TYPE10UT035 1 12 \*\*\*\*\* \* RESULT 2 OPTIONS BLOCK, LOADED BY INOUT2, STORED IN /INOUT2/ \* FURTHEST DISTANCE AT WHICH A GIVEN RISK OF EARLY DEATH IS EXCEEDED. \* NUMBER OF DESIRED RESULTS OF THIS TYPE TYPE2NUMBER 1 FATALITY RISK THRESHOLD \* TYPE2OUT001 0.\* RESULT 3 OPTIONS BLOCK, LOADED BY INOUT3, STORED IN /INOUT3/ \* NUMBER OF PEOPLE WHOSE ACUTE DOSE TO A GIVEN ORGAN EXCEEDS A GIVEN THRESHOLD. \* NUMBER OF DESIRED RESULTS OF THIS TYPE TYPE3NUMBER 2 \* ORGAN NAME DOSE THRESHOLD (SV) \* 'RED MARR' TYPE30UT001 1.5 5.0 TYPE3OUT002 'LUNGS' \* RESULT 4 OPTIONS BLOCK, LOADED BY INOUT4, STORED IN /INOUT4/ \* 360 DEGREE AVERAGE RISK OF A GIVEN EFFECT AT A GIVEN DISTANCE. \* POSSIBLE TYPES OF EFFECTS ARE: \* 'ERL FAT/TOTAL' 'ERL INJ/INJURY NAME' \* 'CAN FAT/CANCER NAME' 'CAN FAT/TOTAL' \* NUMBER OF DESIRED RESULTS OF THIS TYPE TYPE4 NUMBER 5 RADIAL INDEX TYPE OF EFFECT 'ERL FAT/TOTAL' TYPE4OUT001 1 TYPE4OUT002 2 'ERL FAT/TOTAL' TYPE4OUT003 'ERL FAT/TOTAL' 3 TYPE4OUT004 4 'ERL FAT/TOTAL' TYPE4OUT005 5 'ERL FAT/TOTAL' \* RESULT 5 OPTIONS BLOCK, LOADED BY INOUT5, STORED IN /INOUT5/ \* TOTAL POPULATION DOSE TO A GIVEN ORGAN BETWEEN TWO DISTANCES. \* NUMBER OF DESIRED RESULTS OF THIS TYPE TYPE5NUMBER 3 \* I1DIS5 ORGAN I2DIS5 TYPE5OUT001 'EDEWBODY' (0-10 MILES) 1 12 TYPE5OUT002 'EDEWBODY' 1 19 (0-50 MILES) TYPE5OUT003 'EDEWBODY' 1 26 (0-1000 MILES) \* RESULT 6 OPTIONS BLOCK, LOADED BY INOUT6, STORED IN /INOUT6/

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\* CENTERLINE DOSE TO AN ORGAN VS DIST BY PATHWAY, PATHWAY NAMES ARE AS FOLLOWS: \* PATHWAY NAME: \* - CLOUDSHINE 'CLD' - GROUNDSHINE \* 'GRD' 'INH ACU' - "ACUTE DOSE EQUIVALENT" FROM DIRECT INHALATION OF THE CLOUD \* 'INH LIF' - "LIFETIME DOSE COMMITMENT" FROM DIRECT INHALATION OF THE CLOUD \* 'RES ACU' - "ACUTE DOSE EQUIVALENT" FROM RESUSPENSION INHALATION \* 'RES LIF' - "LIFETIME DOSE COMMITMENT" FROM RESUSPENSION INHALATION 'TOT ACU' - "ACUTE DOSE EQUIVALENT" FROM ALL PATHWAYS 'TOT LIF' - "LIFETIME DOSE COMMITMENT" FROM ALL PATHWAYS \* NUMBER OF DESIRED RESULTS OF THIS TYPE TYPE6NUMBER 0 \* ORGNAM PATHNM I1DIS6 I2DIS6 \* \*TYPE6OUT001 'RED MARR' 'LUNGS' 'TOT ACU' 19 (0-50 MILES) 1 'TOT ACU' 19 (0-50 MILES)\*TYPE60UT002 1 \*TYPE6OUT003 'EDEWBODY' 'TOT LIF' 26 1 (0-1000 MILES) \*\*\*\*\* \* RESULT 7 OPTIONS BLOCK, LOADED BY INOUT7, STORED IN /INOUT7/ \* \* CENTERLINE RISK OF A GIVEN EFFECT VS DISTANCE \* NUMBER OF DESIRED RESULTS OF THIS TYPE TYPE7NUMBER 0 \* I1DIS7 I2DIS7 NAME \*TYPE7OUT001 'ERL FAT/TOTAL' 1 19 (0-50 MILES) 'CAN FAT/TOTAL' (0-1000 MILES) \*TYPE7OUT002 26 1 \* RESULT 8 OPTIONS BLOCK, LOADED BY INOUT8, STORED IN /INOUT8/ \* \* POPULATION WEIGHTED FATALITY RISK BETWEEN 2 DISTANCES \* \* NUMBER OF DESIRED RESULTS OF THIS TYPE TYPE8NUMBER 2 \* \* NAME I1DIS8 T2DTS8 TYPE8OUT001 'ERL FAT/TOTAL' 5 (0-EXCL ZONE + 1 MI)1 'CAN FAT/TOTAL' TYPE8OUT002 12 1 (0-10 MILES)

## A.3 CHRONC

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\* FILE NAME: 1150CH.INP \* GENERAL DESCRIPTIVE TITLE DESCRIBING THIS "CHRONC" INPUT FILE CHCHNAME001 'CHRONC INPUT FOR FINAL NUREG-1150 CALCULATIONS' \*\*\* \*\*\*\*\* \* EMERGENCY RESPONSE COST DATA BLOCK \* EVACUATION COST (DOLLARS/PERSON-DAY) CHEVACST001 27.00 \* RELOCATION DOST (DOLLARS/PERSON-DAY) CHRELCST001 27.00 \* LONG TERM PROTECTIVE ACTION DATA BLOCK \* END OF THE INTERMEDIATE PHASE PERIOD (SECONDS FROM ACCIDENT INITIATION) CHTMIPND001 604800. (7 DAYS, NO INTERMEDIATE PHASE) \* ACTION PERIOD (PROJECTION PERIOD) FROM THE START OF THE LONG TERM PHASE, \* THE POINT AT WHICH THE LONG TERM DOSE CRITERION IS EVALUATED (SECONDS) CHTMPACT001 1.58E8 (5 YEARS) \* DOSE CRITERION FOR INTERMEDIATE PHASE RELOCATION (SV) CHDSCRTI001 1.0E5 (NO INTERMEDIATE PHASE RELOCATION) \* DOSE CRITERION FOR LONG TERM PHASE RELOCATION (SV) (2 REM IN FIRST YEAR, 0.5 REM PER YEAR FOR YRS 2 - 5) CHDSCRLT001 0.04 \* CRITICAL ORGAN NAME FOR LONG-TERM ACTIONS CHCRTOCR001 'EDEWBODY' \*\*\*\*\* \* DECONTAMINATION PLAN DATA BLOCK \* NUMBER OF LEVELS OF DECONTAMINATION \* CHLVLDEC001 2 \* DECONTAMINATION TIMES (SECONDS) CORRESPONDING TO THE LVLDEC LEVELS \* OF DECONTAMINATION 5.184E6 1.0368E7 CHTIMDEC001 (60, 120 DAYS) \* DOSE REDUCTION FACTORS CORRESPONDING TO THE LVLDEC LEVELS OF DECONTAMINATION \* CHDSRFCT001 3. 15. \* COST OF FARM DECONTAMINATION PER UNIT AREA (DOLLARS/HECTARE) \* FOR THE VARIOUS LEVELS OF DECONTAMINATION CHCDFRM0001 562.5 1250. \* COST OF NONFARM DECONTAMINATION PER PERSON (DOLLARS/PERSON) \* FOR THE VARIOUS LEVELS OF DECONTAMINATION CHCDNFRM001 3000. 8000.

\* \* FRACTION OF FARMLAND DECONTAMINATION COST DUE TO LABOR FOR THE VARIOUS DECONTAMINATION LEVELS \* CHFRFDL0001 0.3 0 35 \* FRACTION OF NON-FARM DECONTAMINATION COST DUE TO LABOR \* FOR THE VARIOUS DECONTAMINATION LEVELS CHFRNFDL001 0.7 0.5 \* FRACTION OF TIME WORKERS IN FARM AREAS SPEND IN DECONTAMINATION WORK \* FOR THE VARIOUS DECONTAMINATION LEVELS CHTFWKF0001 0.10 0.33 \* FRACTION OF TIME WORKERS IN NON-FARM AREAS SPEND IN DECONTAMINATION WORK \* FOR THE VARIOUS DECONTAMINATION LEVELS CHTFWKNF001 0.33 0.33 \* AVERAGE COST OF DECONTAMINATION LABOR (DOLLARS/MAN-YEAR) CHDLBCST001 35000. \* INTERDICTION COST DATA BLOCK \* DEPRECIATION RATE DURING INTERDICTION PERIOD (PER YEAR) CHDPRATE001 0.20 \* SOCIETAL DISCOUNT RATE DURING INTERDICTION PERIOD (PER YEAR) \* CHDSRATE001 0.12 \* URBAN POPULATION REMOVAL COST (DOLLARS/PERSON) CHPOPCST001 5000. \* GROUNDSHINE WEATHERING DEFINITION DATA BLOCK \* NUMBER OF TERMS IN THE GROUNDSHINE WEATHERING RELATIONSHIP (EITHER 1 OR 2) CHNGWTRM001 2 \* GROUNDSHINE WEATHERING COEFFICIENTS CHGWCOEF001 0.5 0.5 (GAYLE'S EQUATION) HALF LIVES CORRESPONDING TO THE GROUNDSHINE WEATHERING COEFFICIENTS (S) \* CHTGWHLF001 1.6E7 2.8E9 (GAYLE'S EQUATION) \* RESUSPENSION WEATHERING DEFINITION DATA BLOCK \* \* NUMBER OF TERMS IN THE RESUSPENSION WEATHERING RELATIONSHIP + CHNRWTRM001 3 \* RESUSPENSION CONCENTRATION COEFFICIENTS (/ METER) \* RELATIONSHIP BETWEEN GROUND CONCENTRATION AND INSTANTANEOUS AIR CONC. CHRWCOEF001 1.0E-5 1.0E-7 1.0E-9 \* HALF-LIVES CORRESPONDING TO THE RESUSPENSION CONCENTRATION COEFFICIENTS (S)

CHTRWHLF001 1.6E7 1.6E8 1.6E9 (6 MONTHS, 5 YEARS, 50 YEARS) \*\*\*\*\* \* SITE REGION DESCRIPTION DATA BLOCK \* FRACTION OF AREA THAT IS LAND IN THE REGION (VALUE NOT USED SINCE SITE FILE PROVIDED) CHFRACLD001 1.0E-35 \* FRACTION OF LAND DEVOTED TO FARMING IN THE REGION CHFRCFRM001 1.0E-35 (VALUE NOT USED SINCE SITE FILE PROVIDED) \* AVERAGE VALUE OF ANNUAL FARM PRODUCTION IN THE REGION (DOLLARS/HECTARE) (CASH RECEIPTS FROM FARMING PLUS VALUE OF HOME CONSUMPTION)/(LAND IN FARMS) (VALUE NOT USED SINCE SITE FILE PROVIDED) CHFRMPRD001 0. \* FRACTION OF FARM PRODUCTION RESULTING FROM DAIRY PRODUCTION IN THE REGION (VALUE OF MILK PRODUCED)/(CASH RECEIPTS FROM FARMING PLUS VALUE OF HOME...) \* (VALUE NOT USED SINCE SITE FILE PROVIDED) CHDPFRCT001 0. \* VALUE OF FARM WEALTH (DOLLARS/HECTARE): AVERAGE VALUE OF FARM LAND \* AND BUILDINGS PER HECTARE TO 100 MILES SUR ZION \* SITE GG LS PB SEO VALWF (\$/HECTARE) 2561 3305 3421 1855 2613 2897 \* CHVALWF0001 3421. \* PEACH BOTTOM \* FRACTION OF FARM WEALTH IN IMPROVEMENTS FOR THE REGION LS PB SEQ SUR ZION 0.19 0.25 0.27 0.25 0.49 \* SITE GG FRFIM 0.3 0.25 \* PEACH BOTTOM CHFRFIM0001 \* NON-FARM WEALTH, PROPERTY AND IMPROVEMENTS FOR THE REGION (DOLLARS/PERSON) \* THE VALUE OF ALL RESIDENTIAL, BUSINESS, AND PUBLIC ASSETS WHICH WOULD BE \* LOST IN THE EVENT OF PERMANENT INTERDICTION OF THE AREA SITE GG PB SUR SEQ ZION \* VALWNF (\$K) 53 78 84 66 76 CHVALWNF001 78000. \* PEACH BOTTOM \* FRACTION OF NON-FARM WEALTH IN IMPROVEMENTS FOR THE REGION CHFRNFIM001 0.8 \* SPECIAL OPTIONS DATA BLOCK \* DETAILED PRINT OPTION CONTROL SWITCHES, LOOK AT THE CODE BEFORE TURNING ON !! (KCEPNT, KDFPNT, KDTPNT, KGCPNT, KLTPNT, KWTPNT, KSWRSK, KSWDSC) \* WATER PATHWAY NUCLIDE DEFINITIONS FOR CHRONC \* NUMBER OF NUCLIDES IN THE WATER INGESTION PATHWAY MODEL CHNUMWPI001 \* TABLE OF NUCLIDE DEFINITIONS IN THE WATER INGESTION PATHWAY MODEL \* WATER PATHWAY NUCLIDES MUST BE A SUBSET OF THE INGESTION MODEL NUCLIDES

\* IF A SITE DATA FILE IS DEFINED, THE DATA DEFINING THE WATERSHED INGESTION FACTOR IS SUPERSEDED BY THE CORRESPONDING DATA IN THE SITE DATA FILE WINGF VALUES BY DRAINAGE SYSTEM SR-89 SR-90 CS-134 CS-137 \* NUCLIDE \* RIVER 5.0E-6 5.0E-6 5.0E-6 5.0E-6 \* GREAT LAKE 2.0E-7 2.0E-7 2.0E-6 4.0E-6 0.0 0.0 0.0 0.0 \* OCEAN ALL NUREG-1150 SITES HAVE RIVER DRAINAGE SYSTEMS EXCEPT LASALLE AND ZION \* INITIAL ANNUAL INGESTION FACTOR \* WATER WASHOFF WASHOFF ((BQ INGESTED)/ NUCLIDE FRACTION RATE \* (BQ IN WATER)) \* NAMWPI WSHFRI WSHRTA WINGF SR-89 CHWTRIS0001 0.01 0.004 5.0E-6 SR-90 0.004 CHWTRIS0002 0.01 5.0E-6 CHWTRIS0003 CS-134 0.005 0.001 5.0E-6 0.005 CHWTRISO004 CS-137 0.001 5.0E-6 \*\*\*\*\*\*\*\* \*\*\*\*\*\*\* \* CROP PATHWAY DEFINITIONS FOR CHRONC \* MODIFIED 14 OCT 88, BY JLS, VALUES CHANGED TO THOSE DEVELOPED BY J. ROLLSTIN \* \* NUMBER OF DEFINED CROPS IN THE CHRONC FOOD INGESTION MODEL (UP TO 10 ALLOWED) CHNFICRP001 7 \* NOTE TO USER: THE CODE MAKES SPECIAL TREATMENT OF CROP NAMES BEGINNING WITH \* 'PASTURE' DUE TO THE CONTINUOUS NATURE OF THE HARVESTING PROCESS. \* \* IF THE USER WISHES TO DEFINE A NEW CROP CATEGORY FOR RANGELAND PASTURE, IT SHOULD BE CALLED 'PASTURE-RANGE' OR 'PASTURE-DRY' \* \* TABLE OF CROP DEFINITIONS FOR THE CHRONC FOOD INGESTION MODEL \* \* FRACTION OF CROP CONSUMED BY \* \* MEAT DATRY \* CROP NAME MAN ANIMALS ANIMALS \* FRCTCH FRCTCM NAMCRP FRCTCB CHCRPTBL001 'PASTURE ' 0.0 0.1 0.9 CHCRPTBL002 'STORED FORAGE ' 0.0 0.13 0.87 CHCRPTBL003 'GRAINS 0.35 0.040 0.61 CHCRPTBL004 'GRN LEAFY VEGETABLES' 1.0 0.0 0.0 + CHCRPTBL005 'OTHER FOOD CROPS 1.0 0.0 0.0 CHCRPTBL006 'LEGUMES AND SEEDS ' 0.24 0.046 0.714 ' 1.0 CHCRPTBL007 'ROOTS AND TUBERS 0.0 0.0 \*\*\*\*\* \* CHRONC INGESTION PATHWAY NUCLIDE DEFINITIONS \* \* NUMBER OF NUCLIDES IN THE CHRONC FOOD INGESTION MODEL CHNFIISO001 6 (UP TO 10 ALLOWED, BEWARE THAT DAUGHTER BUILDUP IS NOT TREATED) \* TABLE OF NUCLIDE DEFINITIONS IN THE CHRONC INGESTION PATHWAY MODEL \* NUCLIDES THAT WERE DEFINED IN THE WATER PATHWAY DATA ABOVE MUST BE \* A SUBSET OF THE CHRONC INGESTION FOOD PATHWAY NUCLIDES. THE WATER \* PATHWAY NUCLIDES MUST BE LISTED FIRST IN THIS DATA BLOCK AND IN THE \* SAME ORDER AS THEY WERE LISTED IN THE WATER PATHWAY DATA BLOCK \* \* TRANSFER FACTORS \* RETENTION FACTORS [(BQ TRANSFERED)/

* .	INGESTION NUCLIDE		ING AND AN MEAT		(BQ IN MILK	GESTED)] MEAT		
* CHISODEF001 CHISODEF002 CHISODEF003 CHISODEF004 CHISODEF005 CHISODEF006 **********	SR-90 CS-134 CS-137 I-131 I-133 ********		0. 1. 1. 0. 2 0. *******	0 0 18 0 *******		0.00 0.02 0.02 0.02 0.00 0.00	022 022 3 4 24 11 ********	
* TRANSFER 1 * GRAZING OI *								
* * *	NUCLIDE	PASTURE	STORED FORAGE	GRAINS	GREEN LEAFY VEG	OTHER FOOD CROPS	LEGUMES AND SEEDS	ROOTS AND TUBERS
* CHTCROOT001 CHTCROOT002 CHTCROOT003 CHTCROOT004 CHTCROOT005 CHTCROOT006 *********** * RADIOACT	SR-90 CS-134 CS-137 I-131 I-133 ********* IVE DECAY IVITY LOS	2.6E-2 1.3E-3 6.9E-3 1.6E-4 1.7E-6 ********* RETENTIO	1.3E-3 9.0E-2 7.1E-4 1.5E-3 0.0 0.0 ******* N FACTOR Y) FOR N	4.3E-5 3.3E-3 3.5E-5 7.6E-5 0.0 0.0 ******* S (I.E., UCLIDES	1 - F W IN CROPS	8.6E-6 6.6E-4 1.1E-4 2.3E-4 0.0 0.0 ******** HERE F = FROM TI	2.8E-2 9.3E-5 2.0E-4 0.0 0.0	1.1E-4 8.4E-3 5.6E-5 1.2E-4 0.0 0.0 **********
* * *	NUCLIDE		STORED FORAGE		GREEN LEAFY VEG	OTHER FOOD CROPS	LEGUMES AND SEEDS	ROOTS AND TUBERS
* CHDCYPCH001 CHDCYPCH002 CHDCYPCH003 CHDCYPCH004 CHDCYPCH005 CHDCYPCH006	SR-90 CS-134 CS-137 I-131 I-133	0.0 0.0	DCYPCH 0.0 0.0 0.0 0.0 0.0 0.0	0.18 0.99 0.84 0.99 0.009 0.0	9 0.21 0.0	0.21 0.99 0.85 0.99 0.024 0.0	0.0099 0.0	0.0
<ul> <li>* CROP PROCESSING AND PREPARATION RETENTION FACTORS FOR NUCLIDES IN FOOD</li> <li>* CROPS CONSUMED BY HUMANS (FRACTION RETAINED). FACTORS REFLECT LOSS OF</li> <li>* NUCLIDES FROM FOODS DUE TO PROCESSING (E.G., WASHING OF FRUIT, PEELING</li> <li>* OF POTATOES, LOSSES DURING CANNING) AND FOOD PREPARATION (COOKING) FROM</li> <li>* THE TIME OF PROCESSING OF THE HARVESTED CROP TO THE TIME OF CONSUMPTION</li> <li>* BY HUMANS. FACTORS DO NOT REFLECT LOSSES DUE TO RADIOACTIVE DECAY.</li> </ul>								
* - * - *	NUCLIDE	PASTURE	STORED FORAGE	GRAINS	GREEN LEAFY VEG	OTHER FOOD CROPS	LEGUMES AND SEEDS	ROOTS AND TUBERS
* CHFPLSCH001 CHFPLSCH002	SR-90 CS-134 CS-137 I-131 I-133	FPLSCH 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0	FPLSCH 0.25 0.25 0.25 0.25 0.33 0.33	FPLSCH 0.5 0.5 0.5 0.5 0.5 0.5	0.71 0.71 0.71 0.71 0.71 0.71	0.8 0.8 0.8 0.8 0.8 0.8 0.8	FPLSCH 0.8 0.8 0.8 0.8 0.8 0.8 0.8
* RETENTION * CONSUMPT * LOSSES D	N FACTORS	FOR NUCL	IDES IN ING ANIM	CROPS FR	OM TIME	OF HARVE	ST TO TIM FACTOR	E OF
*					GREEN	OTHER	LEGUMES	ROOTS

FOOD STORED LEAFY AND \* AND NUCLIDE PASTURE FORAGE GRAINS VEG CROPS SEEDS TUBERS \* DCYPCM DCYPCM DCYPCM DCYPCM DCYPCM DCYPCM DCYPCM NAMISO CHDCYPCM001 SR-89 1.0 0.37 0.20 0.0 0.0 0.20 0.0 SR-90 1.0 0.99 0.99 0.0 0.0 0.99 CHDCYPCM002 0.0 CS-134 1.0 0.92 0.85 0.0 0.0 CHDCYPCM003 0.85 0.0 CS-137 0.99 0.99 0.0 0.0 CHDCYPCM004 1.0 0.99 0.0 CHDCYPCM005 I-131 0.063 0.032 0.0 0.0 1.0 0.032 0.0 0.0068 0.0034 0.0 CHDCYPCM006 I-133 1.0 0.0 0.0034 0.0 RETENTION FACTORS FOR NUCLIDES IN CROPS FROM TIME OF HARVEST TO TIME OF CONSUMPTION BY MEAT-PRODUCING ANIMALS (FRACTION RETAINED). FACTOR REFLECTS \* LOSSES DUE TO RADIOACTIVE DECAY. \* LEGUMES ROOTS GREEN OTHER \* STORED LEAFY FOOD AND AND NUCLIDE PASTURE FORAGE GRAINS VEG \* CROPS SEEDS TUBERS DCYPCB DCYPCB DCYPCB DCYPCB DCYPCB DCYPCB NAMISO DCYPCB CHDCYPCB001 SR-89 0.37 0.20 0.0 0.0 1.0 0.20 0.0 0.99 CHDCYPCB002 SR-90 0.99 0.0 1.0 0.0 0.99 0.0 . CHDCYPCB003 CS-134 CHDCYPCB004 CS-137 0.92 0.85 1.0 0:0 0.0 0.85 0.0 1.0 0.99 0.99 0.0 0.0 0.99 0.0 CHDCYPCB005 I-131 0.063 0.032 1.0 0.0 0.0 0.032 0.0 CHDCYPCB006 I-133 1.0 0.0068 0.0034 0.0 0.0 0.0034 0 0 \* DEFINE THE DIRECT DEPOSITION TO CROPS TRANSFER FUNCTION \* NUMBER OF TERMS IN THE DIRECT DEPOSITION TO CROPS TRANSFER FUNCTION CHNTRTRM001 2 \* LOSSES DUE TO WEATHERING FROM PLANT SURFACES AND DURING TRANSLOCATION FROM PLANT SURFACES TO INTERIOR EDIBLE PORTIONS OF PLANTS ARE MODELLED \* \* USING THE FOLLOWING EOUATION: \* FRACTION RETAINED = CTCOEF1\*EXP(-LN2/CTHALF1) + CTCOEF2\*EXP(-LN2/CTHALF2) \* FOR PASTURE, STORED FORAGE, GREEN LEAFY VEGETABLES, AND OTHER FOOD CROPS, THIS EQUATION IS USED AS A TWO TERM WEATHERING EQUATION. FOR GRAINS, \* \* LEGUMES AND SEEDS, AND ROOTS AND TUBERS WHERE RADIOACTIVITY IS CONSUMED ONLY IF TRANSLOCATED TO EDIBLE PORTIONS OF THE PLANT, THIS EQUATION IS REDUCED TO A TRANSLOCATION TRANSFER FACTOR BY SETTING CTCOEF2 TO ZERO, CTHALF2 TO ONE SECOND, AND CTHALF1 TO ABOUT ONE MILLION YEARS (1E13 \* SECONDS). WHEN USED TO MODEL TRANSLOCATION, THE VALUE OF THE TRANSLOCATION TRANSFER FACTOR IS DEVELOPED FROM FALLOUT DATA AND IS INPUT AS THE VALUE \* OF CTCOEF1. \* TWO TIME PERIODS ARE USED FOR WEATHERING, THE FIRST IS 14 DAYS LONG (1.21E6 SECONDS) AND THE SECOND IS 50 DAYS LONG (4.32E6 SECONDS). \* DIRECT DEPOSITION TRANSFER COEFFICIENTS [(BQ TRANSFERED)/(BQ DEPOSITED)] \* \* BY CHRONC INGESTION MODEL NUCLIDE GREEN OTHER LEGUMES ROOTS \* STORED LEAFY FOOD AND AND TUBERS NUCLIDE PASTURE FORAGE GRAINS TERM 1 VEG CROPS SEEDS CHCTCOEF101 SR-89 0.3 0.2 0.01 0.2 0.005 0.0006 0.24 SR-90 CHCTCOEF102 0.3 0.2 0.01 0.24 0.2 0.005 0.0006 CS-134 CHCTCOEF103 0.3 0.2 0.05 0.24 0.2 0.01 0.025 CHCTCOEF104 CS-137 0.3 0.2 0.05 0.24 0.2 0.01 0.025 CHCTCOEF105 I-131 0.3 0.2 0.0 0.24 0.2 0.0 0.0 CHCTCOEF106 I-133 0.3 0.2 0.0 0.24 0.2 0.0 0.0 TERM 2 CHCTCOEF201 SR-89 0.05 0.076 0.05 0.0 0.06 0.0 0.0

CHCTCOEF202 SR-90 0.076 0.05 0.06 0.05 0.0 0.0 0.0 0.0 CHCTCOEF203 CS-134 0.076 0.05 0.0 0.06 0.05 0.0 0.05 CHCTCOEF204 CS-137 0.076 0.05 0.0 0.06 0.0 0.0 0.05 0.0 CHCTCOEF205 I-131 0.076 0.05 0.0 0.06 0.0 0.05 CHCTCOEF206 I-133 0.076 0.05 0.0 0.06 0.0 0.0 CROP TRANSFER HALF-LIVES BY CHRONC INGESTION MODEL NUCLIDE (SECONDS) GREEN OTHER LEGUMES ROOTS AND STORED LEAFY FOOD AND NUCLIDE PASTURE FORAGE GRAINS VEG SEEDS CROPS TUBERS \* TERM 1 1.21E6 CHCTHALF101 SR-89 1.21E6 1.21E6 1E13 1.21E6 1E13 1E13 1.21E6 1E13 1.21E6 1.21E6 1E13 CHCTHALF102 SR-90 1E13 1.21E6CHCTHALF103 CS-134 1.21E6 1.21E6 1E13 1.21E6 1.21E6 1E13 1E13 CHCTHALF104 CS-137 1.21E6 1.21E6 1E13 1.21E6 1.21E6 1E13 1E131.0 1.21E6 1.21E6 1.0 1.21E6 1.21E6 1.0 1.0 CHCTHALF105 I-131 1.21E6 1.21E6 CHCTHALF106 I-133 1.21E6 1.21E6 1.0 1.0 \* TERM2 CHCTHALF201 SR-89 4.32E6 4.32E6 1.0 4.32E6 4.32E0 CHCTHALF202 SR-90 4.32E6 4.32E6 1.0 4.32E6 4.32E6 4.32E6 4.32E6 1.0 1.0 1.0 1.0 1.0 1.0 CHCTHALF204 CS-137 4.32E6 4.32E6 1.0 4.32E6 4.32E6 1.0 1.0 CHCTHALF205 I-131 CHCTHALF206 I-133 4.32E6 4.32E6 4.32E6 4.32E6 1.0 4.32E6 4.32E6 1.0 4.32E6 4.32E6 1.0 1.0 1.0 1.0 \* TABLE OF CROP DATA (GROWING SEASON AND FARMLAND SHARE) IN THE REGION. \* IF A SITE DATA FILE IS BEING USED (AS SPECIFIED ON THE EARLY USER INPUT FILE), \* THEN DATA FROM THE SITE FILE (AND NOT THE DATA BELOW) IS USED FOR THE \* CALCULATION OF DOSES AND COSTS FROM THE AGRICULTURE MODEL AND THE NUMBERS \* BELOW ARE IGNORED. \* IF A SITE DATA FILE IS NOT BEING USED, THE DATA BELOW IS USED IN ITS STEAD. \* FARMLAND SHARE VALUES (FRCTFL) BY SITE AND CROP CATEGORY \* SITE GG LS PB SEO SUR ZION \* 0.70 0.47 0.38 0.69 0.41 PASTURE 0.45 STORED FORAGE 0.05 0.10 0.13 0.006 0.13 0.11 \* 0.18 0.26 0.23 0.16 0.21 0.26 GRATNS GRN LEAFY VEGETABLES 0.0005 0.0003 0.002 0.0007 0.002 0.0004 \* OTHER FOOD CROPS 0.004 0.001 0.004 0.005 0.004 0.001 \* LEGUMES AND SEEDS 0.13 0.13 0.16 0.15 0.15 0.13 0.0008 0.002 0.004 0.001 0.003 0.002 ROOTS AND TUBERS GROWING SEASON (DAYS) FARMLAND \* CROP NAME START END SHARE \* NAMCRP TGSBEG TGSEND FRCTFL CHCRPRGN001 'PASTURE ' 90. 270. 0.38 ' 150. 240. CHCRPRGN002 'STORED FORAGE 0.13 ' 150. 240. CHCRPRGN003 'GRAINS 0.23 CHCRPRGN004 'GRN LEAFY VEGETABLES' 150. 240. CHCRPRGN005 'OTHER FOOD CROPS ' 150. 240. CHCRPRGN006 'LEGUMES AND SEEDS ' 150. 240. 0.002 0.004 0.16 CHCRPRGN007 'ROOTS AND TUBERS ' 150. 240 0.004 \* PROTECTIVE ACTION GUIDES FOR THE DIRECT DEPOSITION PATHWAY TO \* MILK AND ITS PRODUCTS AND TO OTHER CROPS AND THEIR PRODUCTS \* BY FOOD INGESTION MODEL NUCLIDE (PERMISSIBLE SURFACE \* CONCENTRATION IN BECQUERELS PER SQUARE METER) \* PERMISSIBLE SURFACE CONCENTRATIONS WERE DERIVED BY INVERTING

\* THE FOOD PATHWAY MODEL THEREBY MAKING THE DOSE TO AN ORGAN THE

\* INDEPENDENT VARIABLE AND GROUND CONCENTRATION THE DEPENDENT VARIABLE. PERMISSIBLE GROUND CONCENTRATIONS WERE CALCULATED \* ASSUMING (1) ALLOWABLE FIRST YEAR (I.E., DIRECT DEPOSITION) \* ORGAN DOSES OF 15 REM PER YEAR TO THYROID AND 5 REM PER YEAR \* TO ANY OTHER ORGAN; AND (2) ALLOWABLE DOSES IN SUBSEQUENT YEARS \* (I.E., ROOT UPTAKE PATH) OF 1.5 REM TO THYROID AND 0.5 REM TO \* ANY OTHER ORGAN. MILK AND OTHER CROPS NUCLIDE PRODUCTS AND PRODUCTS NAMIPI PSCMLK PSCOTH 2.1E06 CHPAGMCP001 SR-89 2.2E06 CHPAGMCP002 SR-90 4.6E04 5.1E04 CHPAGMCP003 CS-134 1.4E05 9.6E04 CS-137 CHPAGMCP004 1.9E05 1.3E05 I-131 CHPAGMCP005 1.0E05 9.2E06 CHPAGMCP006 I-133 1.2E09 1.0E20 = NO LIMIT1.0E20 \* PROTECTIVE ACTION GUIDES FOR LONG-TERM TRANSFER TO FARM CROPS FROM ROOT AND OTHER SOIL UPTAKE FROM SURFACE CONTAMINATION \* BY CHRONC INGESTION MODEL NUCLIDE (PERMISSIBLE SURFACE CONCENTRATION IN BEQUERELS PER SQUARE METER) AND THE ASSOCIATED ANNUAL DEPLETION RATE FOR THE NUCLIDE IN THE SOIL. PERMISSIBLE ANNUAL SURFACE DEPLETION NUCLIDE CONCENTRATION RATE \* NAMIPI GCMAXR QROOT CHPAGLTS001 SR-89 8.3E05 4.9 CHPAGLTS002 SR-90 4.0E03 0.065 CHPAGLTS003 CS-134 1.1E05 0.59 CHPAGLTS004 CS-137 1.2E05 0.28 CHPAGLTS005 I-131 2.1E07 32.0 CHPAGLTS006 I-133 1.6E12 290.0 \* DEFINE THE TYPE 9 RESULTS \* LONG-TERM POPULATION DOSE IN A GIVEN REGION BROKEN DOWN BY THE 12 PATHWAYS \* NUMBER OF RESULTS OF THIS TYPE THAT ARE BEING REQUESTED \* FOR EACH RESULT YOU REQUEST, THE CODE WILL PRODUCE A SET OF 12 TYPE9NUMBER (UP TO 10 ALLOWED) 2 ORGNAM INNER OUTER (0-1000 MILES) TYPE90UT001 'EDEWBODY' 26 1 'EDEWBODY' TYPE90UT002 1 19 (0-50 MILES) \* ECONOMIC COST RESULTS IN A REGION BROKEN DOWN BY 12 TYPES OF COSTS \* NUMBER OF RESULTS OF THIS TYPE THAT ARE BEING REQUESTED \* FOR EACH RESULT YOU REQUEST, THE CODE WILL PRODUCE A SET OF 12 TYP10NUMBER (UP TO 10 ALLOWED) 2 \* INNER OUTER TYP100UT001 (0-1000 MILES) 1 26 TYP100UT002 1 19 (0-50 MILES)\* DEFINE A FLAG THAT CONTROLS THE PRODUCTION OF THE ACTION DISTANCE RESULTS \* SPECIFYING A VALUE OF .TRUE. TURNS ON ALL 8 OF THE ACTION DISTANCE RESULTS,

\* A VALUE OF .FALSE. WILL ELIMINATE THE ACTION DISTANCE RESULTS FROM THE OUTPUT. \* TYP11FLAG11 .TRUE. \* IMPACTED AREA/POPULATION RESULTS IN A REGION BROKEN DOWN BY 6 TYPES OF IMPACTS \* \* NUMBER OF RESULTS OF THIS TYPE THAT ARE BEING REQUESTED \* FOR EACH RESULT YOU REQUEST, THE CODE WILL PRODUCE A SET OF 8 \* TYP12NUMBER (UP TO 10 ALLOWED) 2 \* INNER \* OUTER 26 (0-1000 MILES) TYP12OUT001 1 TYP12OUT002 19 (0-50 MILES) 1

## A.4 DOSDATA

MACCS DOSE SANDIA NATI 12		DRATORIES	3	J. JO	10:20:02
STOMACH SMALL IN LUNGS RED MARR THYROID LOWER LI BONE SUR BREAST TESTES OVARIES EDEWBODY THYROIDH					
60 CO-58 CO-60 KR-85 KR-85M KR-87 KR-88 RB-86 SR-89 SR-90 SR-91 SR-92 Y-90 Y-91 Y-92 Y-93 ZR-95 ZR-97 NB-95 MO-99 TC-99M RU-103 RU-105	NUCLIDES	DEFINED	IN THIS	FILE:	
RU-106 RH-105 SB-127 SB-129			( F	2 3	
TE-127 TE-127M TE-129 TE-129M TE-131M		•		÷	
TE-132 I-131 I-132 I-133 I-134 I-135 XE-133					
XE-133 XE-135 CS-134 CS-136 CS-137 BA-139 BA-140 LA-140 LA-140 LA-141 LA-142 CE-141 CE-143 CE-144					

PR-143 ND-147		ч					
NP-239 PU-238 PU-239							
PU-240 PU-241							
AM-241 CM-242 CM-244							
	CLOUDSHINE		GROUND SHINE 7DA	GROUND Y SHINE RA	INHALED TE ACUTE	INHALED CHRONIC	INGESTION
CO-58 STOMACH SMALL IN					1.558E-10 3.307E-10		
LUNGS	3.805E-14	2.143E-11	4.356E-10	7.452E-16	1.039E-09	1.601E-08	8.510E-11
RED MARR THYROID					1.577E-10 -1.000E+00		
LOWER LI					9.144E-10		
BONE SUR					-1.000E+00 -1.000E+00		
BREAST TESTES			+ +		-1.000E+00		
OVARIES	3.456E-14	1.942E-11	3.948E-10	6.754E-16	-1.000E+00	6.166E-10	1.041E-09
EDEWBODY THYROIDH					-1.000E+00 6.142E-11		
CO-60	4.7005 14	2.00011	5.4096 10	9.554E 10	0.1425 11	0.7046 10	0.5005 11
STOMACH					3.840E-10		
SMALL IN LUNGS					8.077E-10 5.186E-09		
RED MARR	9.957E-14	5.032E-11	1.055E-09	1.747E-15	3.986E-10	1.718E-08	1.311E-09
THYROID LOWER LI					-1.000E+00 2.386E-09		
BONE SUR					-1.000E+00		
BREAST	1.164E-13	5.872E-11	1.232E-09	2.039E-15	-1.000E+00	1.843E-08	1.100E-09
TESTES OVARIES					-1.000E+00 -1.000E+00		
EDEWBODY	1.125E-13	5.666E-11	1.189E-09	1.968E-15	-1.000E+00	5.948E-08	2.839E-09
THYROIDH KR-85			· .		1.465E-10		
STOMACH SMALL IN					6.757E-14 6.781E-14		
LUNGS					4.672E-13		
RED MARR	8.562E-17	0.000E+00	0.000E+00	0.000E+00	6.808E-14	7.007E-14	0.000E+00
THYROID LOWER LI					-1.000E+00 6.781E-14		
BONE SUR							0.000E+00
BREAST	1.037E-16	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	7.007E-14	0.000E+00
TESTES OVARIES					-1.000E+00 -1.000E+00		
EDEWBODY	2.315E-16	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	1.180E-13	0.000E+00
THYROIDH	1.037E-16	0.000E+00	0.000E+00	0.000E+00	6.689E-14	7.007E-14	0.000E+00
KR-85M STOMACH	5 232E-15	0 000E+00	0 000E+00	0 000E+00	6.098E-14	6 101E-14	0 000E+00
SMALL IN					6.101E-14		
LUNGS					4.804E-13		
RED MARR THYROID					6.369E-14 -1.000E+00		
LOWER LI	5.105E-15	0.000E+00	0.000E+00	0.000E+00	5.912E-14	5.915E-14	0.000E+00
BONE SUR BREAST					-1.000E+00		
TESTES					-1.000E+00 -1.000E+00		
OVARIES	4.630E-15	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	5.995E-14	0.000E+00
EDEWBODY THYROIDH					-1.000E+00 5.529E-14		
KR-87							
STOMACH	3.161E-14	0.000E+00	0.000E+00	0.000E+00	2.218E-13	2.218E-13	0.000E+00

SMALL IN	2.946E-14	0.000E+00	0.000E+00	0.000E+00 2.2	10E-13	2.210E-13	0.000E+00
LUNGS				0.000E+00 2.3			
RED MARR	3.456E-14	0.000E+00	0.000E+00	0.000E+00 2.1	79E-13	2.179E-13	0.000E+00
THYROID				0.000E+00-1.0			
LOWER LI				0.000E+00 2.2			
BONE SUR				0.000E+00~1.0			
BREAST				0.000E+00-1.0			
TESTES	4.439E-14	0.000E+00	0.000E+00	0.000E+00-1.0	00E+00	2.140E-13	0.000E+00
OVARIES				0.000E+00-1.0			
EDEWBODY				0.000E+00-1.0			
THYROIDH	4.091E-14	0.000E+00	0.000E+00	0.000E+00 2.1	49E-13	2.149E-13	0.000E+00
KR-88							
STOMACH				0.000E+00 3.7			
SMALL IN				0.000E+00 3.7			
LUNGS				0.000E+00 4.2			
RED MARR				0.000E+00 3.6			
THYROID				0.000E+00-1.0			
LOWER LI				0.000E+00 3.9			
BONE SUR				0.000E+00-1.0			
BREAST				0.000E+00-1.0			
TESTES				0.000E+00-1.0			
OVARIES				0.000E+00-1.0			
EDEWBODY				0.000E+00-1.0			
THYROIDH	1.30/E-13	0.000£+00	0.000E+00	0.000E+00 3.5	3/E-13	3.338E-13	0.0002+00
RB-86 STOMACH	2 4000-15	1 0065-10	2 2618-11	6.310E-17 3.0	205-10	1 4525-00	2 0125-00
SMALL IN				5.835E-17 2.0			
LUNGS	3.203E = 15 3.742E = 15	1.070E 12	3 631F-11	6.818E-17 1.5	95E-09	3 2985-09	2.100E 09 2 137E-09
RED MARR				6.913E-17 8.0			
THYROID				8.593E-17-1.0			
LOWER LI	3 425E-15	1.788E-12	3.327E-11	6.247E-17 2.0	41E-10	1.349E-09	2.167E-09
BONE SUR				7.388E-17-1.0			
BREAST				8.054E-17-1.0			
TESTES				9.006E-17-1.0			
OVARIES				6.183E-17-1.0			
EDEWBODY				1.366E-16-1.0			
THYROIDH				8.593E-17 2.4			
SR-89							
STOMACH				9.545E-20 1.9			
SMALL IN				8.689E-20 2.7			
LUNGS				1.027E-19 1.3			
RED MARR				1.043E-19.9.3			
THYROID				1.297E-19-1.0			
LOWER LI	4.947E-18	2.697E-15	5.413E-14	9.386E-20 1.9	80E-09	3.586E-09	2.063E-08
BONE SUR				1.126E-19-1.0			
BREAST				1.221E-19-1.0			
TESTES				1.360E-19-1.0			
OVARIES	4.94/E-18	2.688E-13	3.395E - 14	9.354E-20-1.0 5.069E-17-1.0	005+00	4.4/0E-10 1 797E-00	2.5846-10
EDEWBODY THYROIDH	5.790E-10 6.940E-19	$1.45/E^{-12}$	$2.924E^{-11}$	1.297E-19 8.8	785-11	1.767E-09	2.503E-09 2.584E-10
SR-90	0.0475 10	5.7275 15	7.4001 14	1.27/11 17 0.0	100 11	1.1/51 10	2.5041 10
STOMACH	0 0005+00	0 0005+00	0 000E+00	0.000E+00 1.2	19E-10	2 365E-09	1 570E-09
SMALL IN				0.000E+00 1.6			
LUNGS				0.000E+00 7.4			
RED MARR				0.000E+00 1.7			
THYROID				0.000E+00-1.0			
LOWER LI				0.000E+00 1.6			
BONE SUR				0.000E+00-1.0			
BREAST				0.000E+00-1.0			
TESTES				0.000E+00-1.0			
OVARIES				0.000E+00-1.0			
EDEWBODY				5.000E-18-1.0			
THYROIDH	0.000E+00	0.000E+00	0.000E+00	0.000E+00 1.1	38E-10	2.328E-09	1.333E-09
SR-91							
STOMACH				6.938E-16 1.6			
SMALL IN	3.254E-14	1.324E-11	3.112E-11	6.305E-16 2.3	33E-10	2.419E-10	1.353E-09

LUNGS RED MARR THYROID LOWER LI BONE SUR BREAST TESTES OVARIES EDEWBODY THYROIDH SR-92	3.873E-14 1.575E-11 3.702E-11 7.501E-16 8.695E-10 9.243E-10 3.289E-11 3.936E-14 1.599E-11 3.760E-11 7.620E-16 7.944E-11 1.446E-10 1.233E-10 4.869E-14 1.971E-11 4.633E-11 9.388E-16-1.000E+00 4.434E-11 2.641E-11 3.516E-14 1.425E-11 3.350E-11 6.787E-16 5.220E-10 6.234E-10 3.929E-09 4.322E-14 1.756E-11 4.133E-11 8.375E-16-1.000E+00 1.424E-10 9.812E-11 4.662E-14 1.895E-11 4.458E-11 9.034E-16-1.000E+00 4.814E-11 5.224E-11 5.136E-14 2.089E-11 4.914E-11 9.957E-16-1.000E+00 4.335E-11 4.141E-11 3.507E-14 1.425E-11 3.350E-11 6.787E-16-1.000E+00 4.335E-11 4.141E-11 3.507E-14 1.425E-11 3.184E-11 6.435E-16-1.000E+00 2.615E-10 6.790E-10 4.869E-14 1.971E-11 4.633E-11 9.388E-16 3.583E-11 4.434E-11 2.641E-11
STOMACH SMALL IN LUNGS RED MARR THYROID LOWER LI BONE SUR BREAST TESTES OVARIES EDEWBODY THYROIDH Y-90	$\begin{array}{c} 4.883E-14 & 1.157E-11 & 1.422E-11 & 8.403E-16 & 1.104E-10 & 1.108E-10 & 5.294E-10 \\ 4.566E-14 & 1.081E-11 & 1.327E-11 & 7.864E-16 & 1.857E-10 & 1.861E-10 & 1.081E-09 \\ 5.264E-14 & 1.253E-11 & 1.539E-11 & 9.101E-16 & 7.106E-10 & 7.173E-10 & 1.948E-11 \\ 5.327E-14 & 1.266E-11 & 1.556E-11 & 9.196E-16 & 4.114E-11 & 4.213E-11 & 4.225E-11 \\ 6.532E-14 & 1.556E-11 & 1.913E-11 & 1.129E-15-1.000E+00 & 2.288E-11 & 1.418E-11 \\ 4.852E-14 & 1.352E-11 & 1.415E-11 & 8.371E-16 & 3.252E-10 & 3.369E-10 & 2.179E-09 \\ 5.644E-14 & 1.343E-11 & 1.653E-11 & 9.735E-16-1.000E+00 & 5.591E-11 & 3.874E-11 \\ 6.247E-14 & 1.481E-11 & 1.821E-11 & 1.075E-15-1.000E+00 & 2.549E-11 & 2.743E-11 \\ 6.913E-14 & 1.643E-11 & 2.020E-11 & 1.192E-15-1.000E+00 & 3.134E-11 & 8.079E-11 \\ 4.725E-14 & 1.123E-11 & 1.381E-11 & 8.149E-16-1.000E+00 & 3.134E-11 & 8.079E-11 \\ 6.019E-14 & 1.536E-11 & 1.953E-11 & 1.043E-15-1.000E+00 & 1.741E-10 & 4.451E-10 \\ 6.532E-14 & 1.556E-11 & 1.913E-11 & 1.129E-15 & 2.241E-11 & 2.288E-11 & 1.418E-11 \\ \end{array}$
STOMACH SMALL IN LUNGS RED MARR THYROID LOWER LI BONE SUR BREAST TESTES OVARIES EDEWBODY THYROIDH	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
Y-91 STOMACH SMALL IN LUNGS RED MARR THYROID LOWER LI BONE SUR BREAST TESTES OVARIES EDEWBODY THYROIDH Y-92	1.316E-16 6.690E-14 1.351E-12 2.328E-18 2.740E-10 3.431E-10 6.914E-10 1.224E-16 6.234E-14 1.259E-12 2.169E-18 6.656E-10 8.421E-10 1.737E-09 1.424E-16 7.246E-14 1.463E-12 2.521E-18 6.923E-09 9.836E-08 2.017E-13 1.436E-16 7.310E-14 1.476E-12 2.543E-18 2.798E-11 3.174E-10 6.562E-12 1.782E-16 9.060E-14 1.830E-12 3.152E-18-1.000E+00 8.479E-12 1.288E-13 1.306E-16 6.644E-14 1.342E-12 2.312E-18 6.908E-09 1.455E-08 3.027E-08 1.528E-16 7.765E-14 1.568E-12 2.702E-18-1.000E+00 3.166E-10 6.108E-12 1.677E-16 8.540E-14 1.725E-12 2.971E-18-1.000E+00 8.908E-12 5.545E-13 1.874E-16 9.570E-14 1.933E-12 3.330E-18-1.000E+00 6.404E-12 4.137E-13 1.284E-16 6.535E-14 1.320E-12 2.274E-18-1.000E+00 8.190E-12 3.532E-12 5.509E-16 1.594E-12 3.218E-11 5.544E-17-1.000E+00 1.312E-08 2.571E-09 1.782E-16 9.060E-14 1.830E-12 3.152E-18 6.243E-13 8.479E-12 1.288E-13
Y-92 STOMACH SMALL IN LUNGS RED MARR THYROID LOWER LI BONE SUR BREAST TESTES OVARIES EDEWBODY THYROIDH Y-93	9.228E-15 2.473E-12 3.125E-12 1.700E-16 1.703E-10 1.705E-10 1.420E-09 8.498E-15 2.274E-12 2.875E-12 1.563E-16 2.382E-10 2.390E-10 2.000E-09 9.989E-15 2.671E-12 3.376E-12 1.836E-16 1.242E-09 1.249E-09 1.393E-12 1.012E-14 2.708E-12 3.423E-12 1.861E-16 2.061E-12 2.079E-12 4.930E-12 1.249E-14 3.344E-12 4.227E-12 2.299E-16-1.000E+00 1.054E-12 1.776E-13 9.132E-15 2.440E-12 3.084E-12 1.677E-16 1.959E-10 2.090E-10 1.749E-09 1.088E-14 2.920E-12 3.691E-12 2.007E-16-1.000E+00 1.512E-12 1.754E-12 1.186E-14 3.178E-12 4.017E-12 2.185E-16-1.000E+00 1.503E-12 3.564E-12 1.316E-14 3.529E-12 4.460E-12 2.426E-16-1.000E+00 3.494E-13 1.399E-12 9.006E-15 2.413E-12 3.049E-12 1.658E-16-1.000E+00 2.628E-12 1.971E-11 1.238E-14 5.018E-12 6.342E-12 3.449E-16-1.000E+00 2.125E-10 5.153E-10 1.249E-14 3.344E-12 4.227E-12 2.299E-16 1.049E-12 1.054E-12 1.776E-13
Y-93 STOMACH SMALL IN LUNGS	3.361E-15 1.321E-12 3.127E-12 5.961E-17 2.810E-10 2.896E-10 1.280E-09 3.127E-15 1.223E-12 2.895E-12 5.518E-17 5.455E-10 5.711E-10 2.524E-09 3.647E-15 1.427E-12 3.377E-12 6.437E-17 2.190E-09 2.524E-09 8.661E-13

RED MARR 3.710				
	E-15 1.448E-12	3.427E-12	6.532E-17 3.495E	-12 4.018E-12 4.936E-12
THYROID 4.503	E-15 1.771E-12	4.192E-12	7.991E-17-1.000E	+00 9.250E-13 1.259E-13
	E-15 1.307E-12	3.094E-12	5.898E-17 1.398F	-09 1.997E-09 8.844E-09
				+00 3.134E-12 1.726E-12
				+00 1.742E-12 3.121E-12
				+00 6.650E-13 1.777E-12
				+00 5.307E-12 2.194E-11
				+00 5.829E-10 1.232E-09
THYROIDH 4.503	E-15 1.771E-12	4.192E-12	7.991E-17 8.313E	-13 9.250E-13 1.259E-13
ZR-95				
STOMACH 2.660	E-14 1.509E-11	3.258E-10	5.232E-16 1.541E	-10 1.085E-09 3.568E-10
				-10 9.802E-10 1.119E-09
				-09 1.843E-08 2.342E-11
				-10 3.207E-09 2.135E-10
				+00 7.790E-10 8.238E-12
				-09 4.164E-09 7.778E-09
				+00 2.172E-08 4.860E-10
				+00 9.280E-10 1.047E~10
				+00 3.023E-10 8.032E-11
OVARIES 2.616	E-14 1.482E-11	3.199E-10	5.137E-16-1.000E	+00 8.361E-10 8.153E-10
EDEWBODY 3.299	E-14 1.873E-11	4.043E-10	6.493E-16-1.000E	+00 4.327E-09 1.027E-09
	E - 14 2.049E - 11	4.425E-10	7.103E-16 6.141E	-11 7.790E-10 8.238E-12
ZR-97				
	F-14 2 431F-11	9 4985-11	1 0838-15 3 7728	-10 4.175E-10 1.213E-09
				~10 8.857E-10 3.389E-09
				-09 3.957E-09 1.759E-11
				-10 1.396E-10 1.297E-10
				+00 3.744E-11 2.662E-12
				-09 4.271E-09 1.795E-08
BONE SUR 6.691	E-14 2.949E-11	1.153E-10	1.315E-15-1.000E	+00 1.217E-10 4.538E-11
BREAST 7.210	E-14 3.172E-11	1.240E-10	1.414E-15-1.000E	+00 5.790E-11 8.094E-11
TESTES 7.937	E-14 3.496E-11	1.366E-10	1.558E-15-1.000E	+00 2.986E-11 5.200E-11
OVARIES 5.415	E-14 2.380E-11	9.302E-11	1.061E-15-1.000E	+00 1.696E-10 6.219E-10
				+00 1.067E-09 2.288E-09
		1.7906-10		
		1.290E-10	1.4/16-15 2./006	-11 3.744E-11 2.662E-12
NB-95				
NB-95 STOMACH 2.778	E-14 1.557E-11	3.063E-10	5.422E-16 1.287E	-10 6.362E-10 2.796E-10
NB-95 STOMACH 2.778 SMALL IN 2.515	E-14 1.557E-11 E-14 1.411E-11	3.063E-10 2.776E-10	5.422E-16 1.287E 4.915E-16 2.838E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000	E-14 1.557E-11 E-14 1.411E-11 E-14 1.684E-11	3.063E-10 2.776E-10 3.314E-10	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051	E-14 1.557E-11 E-14 1.411E-11 E-14 1.684E-11 E-14 1.684E-11 E-14 1.711E-11	3.063E-10 2.776E-10 3.314E-10 3.367E-10	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773	E-14 1.557E-11 E-14 1.411E-11 E-14 1.684E-11 E-14 1.711E-11 E-14 2.121E-11	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724	E-14 1.557E-11 E-14 1.411E-11 E-14 1.684E-11 E-14 1.711E-11 E-14 2.121E-11 E-14 1.529E-11	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E 5.327E-16 9.234E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11 -10 1.928E-09 4.009E-09
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724           BONE SUR         3.330	E-14 1.557E-11 E-14 1.411E-11 E-14 1.684E-11 E-14 1.711E-11 E-14 2.121E-11 E-14 1.529E-11	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E 5.327E-16 9.234E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724           BONE SUR         3.330	E-14 1.557E-11 E-14 1.411E-11 E-14 1.684E-11 E-14 1.711E-11 E-14 2.121E-11 E-14 1.529E-11 E-14 1.866E-11	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10 3.672E-10	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E 5.327E-16 9.234E 6.501E-16-1.000E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11 -10 1.928E-09 4.009E-09
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724           BONE SUR         3.330           BREAST         3.583	E-14 1.557E-11 E-14 1.411E-11 E-14 1.684E-11 E-14 1.711E-11 E-14 2.121E-11 E-14 1.529E-11 E-14 1.866E-11 E-14 2.012E-11	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10 3.672E-10 3.959E-10	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E 5.327E-16 9.234E 6.501E-16-1.000E 7.008E-16-1.000E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11 -10 1.928E-09 4.009E-09 +00 5.161E-10 2.965E-10 +00 4.062E-10 1.074E-10
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724           BONE SUR         3.330           BREAST         3.583           TESTES         3.995	$\begin{array}{l} E-14 & 1.557E-11 \\ E-14 & 1.411E-11 \\ E-14 & 1.684E-11 \\ E-14 & 1.711E-11 \\ E-14 & 2.121E-11 \\ E-14 & 1.529E-11 \\ E-14 & 1.866E-11 \\ E-14 & 2.012E-11 \\ E-14 & 2.230E-11 \end{array}$	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10 3.672E-10 3.959E-10 4.388E-10	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E 5.327E-16 9.234E 6.501E-16-1.000E 7.008E-16-1.000E 7.769E-16-1.000E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11 -10 1.928E-09 4.009E-09 +00 5.161E-10 2.965E-10 +00 4.062E-10 1.074E-10 +00 6.507E-11 9.664E-11
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724           BONE SUR         3.330           BREAST         3.583           TESTES         3.995           OVARIES         2.730	$\begin{array}{l} E-14 & 1.557E-11\\ E-14 & 1.411E-11\\ E-14 & 1.684E-11\\ E-14 & 1.711E-11\\ E-14 & 2.121E-11\\ E-14 & 1.529E-11\\ E-14 & 1.866E-11\\ E-14 & 2.012E-11\\ E-14 & 2.230E-11\\ E-14 & 1.529E-11\\ \end{array}$	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10 3.672E-10 3.959E-10 4.388E-10 3.009E-10	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E 5.327E-16 9.234E 6.501E-16-1.000E 7.008E-16-1.000E 7.769E-16-1.000E 5.327E-16-1.000E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11 -10 1.928E-09 4.009E-09 +00 5.161E-10 2.965E-10 +00 4.062E-10 1.074E-10 +00 6.507E-11 9.664E-11 +00 4.310E-10 8.030E-10
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724           BONE SUR         3.330           BREAST         3.583           TESTES         3.995           OVARIES         2.730           EDEWBODY         3.449	$\begin{array}{l} E-14 & 1.557E-11 \\ E-14 & 1.411E-11 \\ E-14 & 1.684E-11 \\ E-14 & 1.711E-11 \\ E-14 & 2.121E-11 \\ E-14 & 1.529E-11 \\ E-14 & 1.866E-11 \\ E-14 & 2.012E-11 \\ E-14 & 2.230E-11 \\ E-14 & 1.529E-11 \\ E-14 & 1.937E-11 \end{array}$	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10 3.672E-10 3.959E-10 4.388E-10 3.009E-10 3.812E-10	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E 5.327E-16 9.234E 6.501E-16-1.000E 7.008E-16-1.000E 7.769E-16-1.000E 5.327E-16-1.000E 6.748E-16-1.000E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11 -10 1.928E-09 4.009E-09 +00 5.161E-10 2.965E-10 +00 4.062E-10 1.074E-10 +00 6.507E-11 9.664E-11 +00 4.310E-10 8.030E-10 +00 1.652E-09 7.029E-10
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724           BONE SUR         3.330           BREAST         3.583           TESTES         3.995           OVARIES         2.730           EDEWBODY         3.449           THYROIDH         3.773	$\begin{array}{l} E-14 & 1.557E-11 \\ E-14 & 1.411E-11 \\ E-14 & 1.684E-11 \\ E-14 & 1.711E-11 \\ E-14 & 2.121E-11 \\ E-14 & 1.529E-11 \\ E-14 & 1.866E-11 \\ E-14 & 2.012E-11 \\ E-14 & 2.230E-11 \\ E-14 & 1.529E-11 \\ E-14 & 1.937E-11 \end{array}$	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10 3.672E-10 3.959E-10 4.388E-10 3.009E-10 3.812E-10	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E 5.327E-16 9.234E 6.501E-16-1.000E 7.008E-16-1.000E 7.769E-16-1.000E 5.327E-16-1.000E 6.748E-16-1.000E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11 -10 1.928E-09 4.009E-09 +00 5.161E-10 2.965E-10 +00 4.062E-10 1.074E-10 +00 6.507E-11 9.664E-11 +00 4.310E-10 8.030E-10
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724           BONE SUR         3.330           BREAST         3.583           TESTES         3.995           OVARIES         2.730           EDEWBODY         3.449           THYROIDH         3.773           MO-99         3.449	$\begin{array}{l} E-14 & 1.557E-11\\ E-14 & 1.411E-11\\ E-14 & 1.684E-11\\ E-14 & 1.711E-11\\ E-14 & 2.121E-11\\ E-14 & 1.529E-11\\ E-14 & 1.866E-11\\ E-14 & 2.012E-11\\ E-14 & 2.230E-11\\ E-14 & 1.529E-11\\ E-14 & 1.937E-11\\ E-14 & 2.121E-11\\ \end{array}$	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10 3.672E-10 3.959E-10 4.388E-10 3.009E-10 3.812E-10 4.173E-10	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E 5.327E-16 9.234E 6.501E-16-1.000E 7.008E-16-1.000E 7.769E-16-1.000E 5.327E-16-1.000E 6.748E-16-1.000E 7.388E-16 4.278E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11 -10 1.928E-09 4.009E-09 +00 5.161E-10 2.965E-10 +00 4.062E-10 1.074E-10 +00 6.507E-11 9.664E-11 +00 4.310E-10 8.030E-10 +00 1.652E-09 7.029E-10 -11 3.582E-10 1.184E-11
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724           BONE SUR         3.330           BREAST         3.583           TESTES         3.995           OVARIES         2.730           EDEWBODY         3.449           THYROIDH         3.773           MO-99         STOMACH	$\begin{array}{l} E-14 & 1.557E-11\\ E-14 & 1.411E-11\\ E-14 & 1.684E-11\\ E-14 & 1.711E-11\\ E-14 & 2.121E-11\\ E-14 & 1.529E-11\\ E-14 & 1.866E-11\\ E-14 & 2.012E-11\\ E-14 & 2.230E-11\\ E-14 & 2.230E-11\\ E-14 & 1.529E-11\\ E-14 & 1.937E-11\\ E-14 & 2.121E-11\\ E-15 & 3.820E-12\\ \end{array}$	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10 3.672E-10 3.959E-10 4.388E-10 3.009E-10 3.812E-10 4.173E-10 5.368E-11	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E 5.327E-16 9.234E 6.501E-16-1.000E 7.008E-16-1.000E 7.769E-16-1.000E 5.327E-16-1.000E 6.748E-16-1.000E 7.388E-16 4.278E 1.100E-16 1.894E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11 -10 1.928E-09 4.009E-09 +00 5.161E-10 2.965E-10 +00 4.062E-10 1.074E-10 +00 6.507E-11 9.664E-11 +00 4.310E-10 8.030E-10 +00 1.652E-09 7.029E-10 -11 3.582E-10 1.184E-11 -10 2.325E-10 5.135E-10
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724           BONE SUR         3.330           BREAST         3.583           TESTES         3.995           OVARIES         2.730           EDEWBODY         3.449           THYROIDH         3.773           MO-99         STOMACH           SMALL IN         4.978	$\begin{array}{l} E-14 & 1.557E-11\\ E-14 & 1.411E-11\\ E-14 & 1.684E-11\\ E-14 & 1.711E-11\\ E-14 & 2.121E-11\\ E-14 & 1.529E-11\\ E-14 & 1.866E-11\\ E-14 & 2.012E-11\\ E-14 & 2.230E-11\\ E-14 & 2.230E-11\\ E-14 & 1.529E-11\\ E-14 & 1.937E-11\\ E-14 & 2.121E-11\\ E-15 & 3.820E-12\\ E-15 & 3.408E-12\\ \end{array}$	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10 3.672E-10 3.959E-10 4.388E-10 3.009E-10 3.812E-10 4.173E-10 5.368E-11 4.751E-11	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E 5.327E-16 9.234E 6.501E-16-1.000E 7.008E-16-1.000E 7.769E-16-1.000E 6.748E-16-1.000E 7.388E-16 4.278E 1.100E-16 1.894E 9.894E-17 4.221E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11 -10 1.928E-09 4.009E-09 +00 5.161E-10 2.965E-10 +00 4.062E-10 1.074E-10 +00 6.507E-11 9.664E-11 +00 4.310E-10 8.030E-10 +00 1.652E-09 7.029E-10 -11 3.582E-10 1.184E-11 -10 2.325E-10 5.135E-10 -10 5.189E-10 1.249E-09
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724           BONE SUR         3.330           BREAST         3.583           TESTES         3.995           OVARIES         2.730           EDEWBODY         3.449           THYROIDH         3.773           MO-99         STOMACH         5.518           SMALL IN         4.978           LUNGS         5.993	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10 3.672E-10 3.959E-10 4.388E-10 3.009E-10 3.812E-10 4.173E-10 5.368E-11 4.751E-11 5.884E-11	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E 5.327E-16 9.234E 6.501E-16-1.000E 7.769E-16-1.000E 5.327E-16-1.000E 6.748E-16-1.000E 7.388E-16 4.278E 1.100E-16 1.894E 9.894E-17 4.221E 1.192E-16 1.592E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11 -10 1.928E-09 4.009E-09 +00 5.161E-10 2.965E-10 +00 4.062E-10 1.074E-10 +00 6.507E-11 9.664E-11 +00 4.310E-10 8.030E-10 +00 1.652E-09 7.029E-10 -11 3.582E-10 1.184E-11 -10 2.325E-10 5.135E-10 -10 5.189E-10 1.249E-09 -09 4.292E-09 1.506E-11
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724           BONE SUR         3.330           BREAST         3.583           TESTES         3.995           OVARIES         2.730           EDEWBODY         3.449           THYROIDH         3.773           MO-99         3.703           STOMACH         5.518           SMALL IN         4.978           LUNGS         5.993           RED MARR         6.057	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10 3.959E-10 4.388E-10 3.009E-10 3.812E-10 4.173E-10 5.368E-11 4.751E-11 5.884E-11 5.687E-11	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E 5.327E-16 9.234E 6.501E-16-1.000E 7.008E-16-1.000E 7.769E-16-1.000E 6.748E-16-1.000E 7.388E-16 4.278E 1.100E-16 1.894E 9.894E-17 4.221E 1.192E-16 1.592E 1.202E-16 3.096E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11 -10 1.928E-09 4.009E-09 +00 5.161E-10 2.965E-10 +00 4.062E-10 1.074E-10 +00 6.507E-11 9.664E-11 +00 4.310E-10 8.030E-10 +00 1.652E-09 7.029E-10 -11 3.582E-10 1.184E-11 -10 2.325E-10 5.135E-10 -10 5.189E-10 1.249E-09 -09 4.292E-09 1.506E-11 -11 5.074E-11 7.972E-11
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724           BONE SUR         3.330           BREAST         3.583           TESTES         3.995           OVARIES         2.730           EDEWBODY         3.449           THYROIDH         3.773           MO-99         3700           STOMACH         5.518           SMALL IN         4.978           LUNGS         5.993           RED MARR         6.057           THYROID         7.579	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10 3.672E-10 3.959E-10 4.388E-10 3.009E-10 3.812E-10 4.173E-10 5.368E-11 4.751E-11 5.884E-11 5.687E-11 7.737E-11	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E 5.327E-16 9.234E 6.501E-16-1.000E 7.769E-16-1.000E 5.327E-16-1.000E 6.748E-16-1.000E 7.388E-16 4.278E 1.100E-16 1.894E 9.894E-17 4.221E 1.192E-16 1.592E 1.202E-16 3.096E 1.513E-16-1.000E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11 -10 1.928E-09 4.009E-09 +00 5.161E-10 2.965E-10 +00 4.062E-10 1.074E-10 +00 6.507E-11 9.664E-11 +00 4.310E-10 8.030E-10 +00 1.652E-09 7.029E-10 -11 3.582E-10 1.184E-11 -10 2.325E-10 5.135E-10 -10 5.189E-10 1.249E-09 -09 4.292E-09 1.506E-11 -11 5.074E-11 7.972E-11 +00 1.516E-11 1.034E-11
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724           BONE SUR         3.330           BREAST         3.583           TESTES         3.995           OVARIES         2.730           EDEWBODY         3.449           THYROIDH         3.773           MO-99         3.743           STOMACH         5.518           SMALL IN         4.978           LUNGS         5.993           RED MARR         6.057           THYROID         7.579           LOWER LI         5.422	$\begin{array}{l} E-14 & 1.557E-11\\ E-14 & 1.411E-11\\ E-14 & 1.684E-11\\ E-14 & 1.711E-11\\ E-14 & 1.711E-11\\ E-14 & 1.529E-11\\ E-14 & 1.866E-11\\ E-14 & 2.012E-11\\ E-14 & 2.230E-11\\ E-14 & 1.529E-11\\ E-14 & 1.529E-11\\ E-14 & 1.937E-11\\ E-14 & 2.121E-11\\ E-15 & 3.820E-12\\ E-15 & 3.408E-12\\ E-15 & 4.163E-12\\ E-15 & 4.163E-12\\ E-15 & 5.376E-12\\ E-15 & 3.740E-12\\ \end{array}$	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10 3.959E-10 4.388E-10 3.009E-10 3.812E-10 4.173E-10 5.368E-11 4.751E-11 5.884E-11 5.687E-11 7.737E-11 5.251E-11	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E 5.327E-16 9.234E 6.501E-16-1.000E 7.008E-16-1.000E 7.769E-16-1.000E 6.748E-16-1.000E 7.388E-16 4.278E 1.100E-16 1.894E 9.894E-17 4.221E 1.192E-16 1.592E 1.202E-16 3.096E 1.513E-16-1.000E 1.078E-16 2.860E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11 -10 1.928E-09 4.009E-09 +00 5.161E-10 2.965E-10 +00 4.062E-10 1.074E-10 +00 6.507E-11 9.664E-11 +00 4.310E-10 8.030E-10 +00 1.652E-09 7.029E-10 -11 3.582E-10 1.184E-11 -10 2.325E-10 5.135E-10 -10 5.189E-10 1.249E-09 -09 4.292E-09 1.506E-11 -11 5.074E-11 7.972E-11 +00 1.516E-11 1.034E-11 -09 5.516E-09 1.367E-08
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724           BONE SUR         3.330           BREAST         3.583           TESTES         3.995           OVARIES         2.730           EDEWBODY         3.449           THYROIDH         3.773           MO-99         3           STOMACH         5.518           SMALL IN         4.978           LUNGS         5.993           RED MARR         6.057           THYROID         7.579           LOWER LI         5.4222           BONE SUR         6.913	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10 3.959E-10 4.388E-10 3.009E-10 3.812E-10 4.173E-10 5.368E-11 4.751E-11 5.884E-11 5.687E-11 7.737E-11 5.251E-11 7.849E-11	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E 5.327E-16 9.234E 6.501E-16-1.000E 7.008E-16-1.000E 7.769E-16-1.000E 6.748E-16-1.000E 7.388E-16 4.278E 1.100E-16 1.894E 9.894E-17 4.221E 1.192E-16 1.592E 1.202E-16 3.096E 1.513E-16-1.000E 1.078E-16 2.860E 1.386E-16-1.000E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11 -10 1.928E-09 4.009E-09 +00 5.161E-10 2.965E-10 +00 4.062E-10 1.074E-10 +00 6.507E-11 9.664E-11 +00 4.310E-10 8.030E-10 +00 1.652E-09 7.029E-10 -11 3.582E-10 1.184E-11 -10 2.325E-10 5.135E-10 -10 5.189E-10 1.249E-09 -09 4.292E-09 1.506E-11 -11 5.074E-11 7.972E-11 +00 1.516E-11 1.034E-11 -09 5.516E-09 1.367E-08 +00 4.290E-11 6.669E-11
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724           BONE SUR         3.330           BREAST         3.583           TESTES         3.995           OVARIES         2.730           EDEWBODY         3.449           THYROIDH         3.773           MO-99         3           STOMACH         5.518           SMALL IN         4.978           LUNGS         5.993           RED MARR         6.057           THYROID         7.579           LOWER LI         5.4222           BONE SUR         6.913	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10 3.959E-10 4.388E-10 3.009E-10 3.812E-10 4.173E-10 5.368E-11 4.751E-11 5.884E-11 5.687E-11 7.737E-11 5.251E-11 7.849E-11	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E 5.327E-16 9.234E 6.501E-16-1.000E 7.008E-16-1.000E 7.769E-16-1.000E 6.748E-16-1.000E 7.388E-16 4.278E 1.100E-16 1.894E 9.894E-17 4.221E 1.192E-16 1.592E 1.202E-16 3.096E 1.513E-16-1.000E 1.078E-16 2.860E 1.386E-16-1.000E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11 -10 1.928E-09 4.009E-09 +00 5.161E-10 2.965E-10 +00 4.062E-10 1.074E-10 +00 6.507E-11 9.664E-11 +00 4.310E-10 8.030E-10 +00 1.652E-09 7.029E-10 -11 3.582E-10 1.184E-11 -10 2.325E-10 5.135E-10 -10 5.189E-10 1.249E-09 -09 4.292E-09 1.506E-11 -11 5.074E-11 7.972E-11 +00 1.516E-11 1.034E-11 -09 5.516E-09 1.367E-08
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724           BONE SUR         3.330           BREAST         3.583           TESTES         3.995           OVARIES         2.730           EDEWBODY         3.449           THYROIDH         3.773           MO-99         3.743           STOMACH         5.518           SMALL IN         4.978           LUNGS         5.993           RED MARR         6.0577           THYROID         7.5791           LOWER LI         5.4222           BONE SUR         6.9133           BREAST         7.388	$\begin{array}{l} \text{E-14} & 1.557\text{E-11} \\ \text{E-14} & 1.411\text{E-11} \\ \text{E-14} & 1.684\text{E-11} \\ \text{E-14} & 1.711\text{E-11} \\ \text{E-14} & 2.121\text{E-11} \\ \text{E-14} & 1.529\text{E-11} \\ \text{E-14} & 1.529\text{E-11} \\ \text{E-14} & 2.012\text{E-11} \\ \text{E-14} & 2.230\text{E-11} \\ \text{E-14} & 1.529\text{E-11} \\ \text{E-14} & 1.529\text{E-11} \\ \text{E-14} & 1.529\text{E-11} \\ \text{E-15} & 3.820\text{E-12} \\ \text{E-15} & 3.408\text{E-12} \\ \text{E-15} & 4.163\text{E-12} \\ \text{E-15} & 4.111\text{E-12} \\ \text{E-15} & 3.740\text{E-12} \\ \text{E-15} & 5.376\text{E-12} \\ \text{E-15} & 5.189\text{E-12} \\ \text{E-15} & 5.483\text{E-12} \\ \end{array}$	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10 3.959E-10 4.388E-10 3.009E-10 3.812E-10 4.173E-10 5.368E-11 4.751E-11 5.884E-11 5.687E-11 7.737E-11 5.251E-11 7.849E-11 8.176E-11	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E 5.327E-16 9.234E 6.501E-16-1.000E 7.008E-16-1.000E 7.769E-16-1.000E 6.748E-16-1.000E 7.388E-16 4.278E 1.100E-16 1.894E 9.894E-17 4.221E 1.192E-16 1.592E 1.202E-16 3.096E 1.513E-16-1.000E 1.386E-16-1.000E 1.386E-16-1.000E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11 -10 1.928E-09 4.009E-09 +00 5.161E-10 2.965E-10 +00 4.062E-10 1.074E-10 +00 6.507E-11 9.664E-11 +00 4.310E-10 8.030E-10 +00 1.652E-09 7.029E-10 -11 3.582E-10 1.184E-11 -10 2.325E-10 5.135E-10 -10 5.189E-10 1.249E-09 -09 4.292E-09 1.506E-11 -11 5.074E-11 7.972E-11 +00 1.516E-11 1.034E-11 -09 5.516E-09 1.367E-08 +00 4.290E-11 6.669E-11 +00 2.748E-11 3.422E-11
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724           BONE SUR         3.330           BREAST         3.583           TESTES         3.995           OVARIES         2.730           EDEWBODY         3.449           THYROIDH         3.773           MO-99         3           STOMACH         5.518           SMALL IN         4.978           LUNGS         5.993           RED MARR         6.057           THYROID         7.579           LOWER LI         5.422           BONE SUR         6.913           BREAST         7.388           TESTES         7.991	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10 3.672E-10 3.959E-10 4.388E-10 3.009E-10 3.812E-10 4.173E-10 5.368E-11 4.751E-11 5.884E-11 5.687E-11 7.37E-11 5.251E-11 7.849E-11 8.176E-11 8.026E-11	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E 5.327E-16 9.234E 6.501E-16-1.000E 7.008E-16-1.000E 7.769E-16-1.000E 6.748E-16-1.000E 7.388E-16 4.278E 1.100E-16 1.894E 9.894E-17 4.221E 1.92E-16 1.592E 1.202E-16 3.096E 1.513E-16-1.000E 1.386E-16-1.000E 1.487E-16-1.000E 1.487E-16-1.000E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11 -10 1.928E-09 4.009E-09 +00 5.161E-10 2.965E-10 +00 4.062E-10 1.074E-10 +00 6.507E-11 9.664E-11 +00 4.310E-10 8.030E-10 +00 1.652E-09 7.029E-10 -11 3.582E-10 1.184E-11 -10 2.325E-10 5.135E-10 -10 5.189E-10 1.249E-09 -09 4.292E-09 1.506E-11 -11 5.074E-11 7.972E-11 +00 1.516E-11 1.034E-11 -09 5.516E-09 1.367E-08 +00 4.290E-11 6.669E-11 +00 2.748E-11 3.422E-11 +00 1.220E-11 2.719E-11
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724           BONE SUR         3.330           BREAST         3.583           TESTES         3.995           OVARIES         2.730           EDEWBODY         3.449           THYROIDH         3.773           MO-99         3.70MACH           STOMACH         5.518           SMALL IN         4.978           LUNGS         5.993           RED MARR         6.057           THYROID         7.579           LOWER LI         5.422           BONE SUR         6.913           BREAST         7.389           TESTES         7.991           OVARIES         5.359	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10 3.959E-10 4.388E-10 3.009E-10 3.812E-10 4.173E-10 5.368E-11 4.751E-11 5.884E-11 5.687E-11 7.737E-11 7.737E-11 7.37E-11 7.849E-11 8.176E-11 8.026E-11 4.983E-11	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E 5.327E-16 9.234E 6.501E-16-1.000E 7.008E-16-1.000E 7.769E-16-1.000E 6.748E-16-1.000E 7.388E-16 4.278E 1.100E-16 1.894E 9.894E-17 4.221E 1.92E-16 1.592E 1.202E-16 3.096E 1.513E-16-1.000E 1.386E-16-1.000E 1.386E-16-1.000E 1.487E-16-1.000E 1.595E-16-1.000E 1.595E-16-1.000E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11 -10 1.928E-09 4.009E-09 +00 5.161E-10 2.965E-10 +00 4.062E-10 1.074E-10 +00 6.507E-11 9.664E-11 +00 4.310E-10 8.030E-10 +00 1.652E-09 7.029E-10 -11 3.582E-10 1.184E-11 -10 2.325E-10 5.135E-10 -10 5.189E-10 1.249E-09 -09 4.292E-09 1.506E-11 -11 5.074E-11 7.972E-11 +00 1.516E-11 1.034E-11 -09 5.516E-09 1.367E-08 +00 4.290E-11 6.669E-11 +00 2.748E-11 3.422E-11 +00 1.220E-11 2.719E-11 +00 9.503E-11 2.174E-10
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724           BONE SUR         3.330           BREAST         3.583           TESTES         3.995           OVARIES         2.730           EDEWBODY         3.449           THYROIDH         3.773           MO-99         3.749           STOMACH         5.518           SMALL IN         4.978           LUNGS         5.993           RED MARR         6.057           THYROID         7.579           LOWER LI         5.422           BONE SUR         6.913           BREAST         7.388           TESTES         7.991           OVARIES         5.359           EDEWBODY         7.164	$\begin{array}{l} E-14 & 1.557E-11\\ E-14 & 1.411E-11\\ E-14 & 1.684E-11\\ E-14 & 1.711E-11\\ E-14 & 2.121E-11\\ E-14 & 1.529E-11\\ E-14 & 1.866E-11\\ E-14 & 2.012E-11\\ E-14 & 2.012E-11\\ E-14 & 1.529E-11\\ E-14 & 1.529E-11\\ E-14 & 1.937E-11\\ E-14 & 1.937E-11\\ E-15 & 3.820E-12\\ E-15 & 3.408E-12\\ E-15 & 3.408E-12\\ E-15 & 3.740E-12\\ E-15 & 5.76E-12\\ E-15 & 5.189E-12\\ E-15 & 5.622E-12\\ E-15 & 3.624E-12\\ E-15 & 5.694E-12\\ E-15 &$	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10 3.672E-10 3.959E-10 4.388E-10 3.009E-10 3.812E-10 4.173E-10 5.368E-11 4.751E-11 5.884E-11 5.687E-11 7.737E-11 5.251E-11 7.849E-11 8.026E-11 4.983E-11 7.867E-11	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E 5.327E-16 9.234E 6.501E-16-1.000E 7.008E-16-1.000E 7.769E-16-1.000E 6.748E-16-1.000E 7.388E-16 4.278E 1.100E-16 1.894E 9.894E-17 4.221E 1.92E-16 1.592E 1.202E-16 3.096E 1.513E-16-1.000E 1.386E-16-1.000E 1.386E-16-1.000E 1.487E-16-1.000E 1.595E-16-1.000E 1.667E-16-1.000E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11 -10 1.928E-09 4.009E-09 +00 5.161E-10 2.965E-10 +00 4.062E-10 1.074E-10 +00 6.507E-11 9.664E-11 +00 4.310E-10 8.030E-10 +00 1.652E-09 7.029E-10 -11 3.582E-10 1.184E-11 -10 2.325E-10 5.135E-10 -10 5.189E-10 1.249E-09 -09 4.292E-09 1.506E-11 -11 5.074E-11 7.972E-11 +00 1.516E-11 1.034E-11 -09 5.516E-09 1.367E-08 +00 4.290E-11 6.669E-11 +00 2.748E-11 3.422E-11 +00 1.220E-11 2.719E-11 +00 1.075E-09 1.362E-09
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724           BONE SUR         3.330           BREAST         3.583           TESTES         3.995           OVARIES         2.730           EDEWBODY         3.449           THYROIDH         3.773           MO-99         3.749           STOMACH         5.518           SMALL IN         4.978           LUNGS         5.993           RED MARR         6.057           THYROID         7.579           LOWER LI         5.422           BONE SUR         6.913           BREAST         7.388           TESTES         7.991           OVARIES         5.359           EDEWBODY         7.164           THYROIDH         7.579	$\begin{array}{l} E-14 & 1.557E-11\\ E-14 & 1.411E-11\\ E-14 & 1.684E-11\\ E-14 & 1.711E-11\\ E-14 & 2.121E-11\\ E-14 & 1.529E-11\\ E-14 & 1.866E-11\\ E-14 & 2.012E-11\\ E-14 & 2.012E-11\\ E-14 & 1.529E-11\\ E-14 & 1.529E-11\\ E-14 & 1.937E-11\\ E-14 & 1.937E-11\\ E-15 & 3.820E-12\\ E-15 & 3.408E-12\\ E-15 & 3.408E-12\\ E-15 & 3.740E-12\\ E-15 & 5.76E-12\\ E-15 & 5.189E-12\\ E-15 & 5.622E-12\\ E-15 & 3.624E-12\\ E-15 & 5.694E-12\\ E-15 &$	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10 3.672E-10 3.959E-10 4.388E-10 3.009E-10 3.812E-10 4.173E-10 5.368E-11 4.751E-11 5.884E-11 5.687E-11 7.737E-11 5.251E-11 7.849E-11 8.026E-11 4.983E-11 7.867E-11	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E 5.327E-16 9.234E 6.501E-16-1.000E 7.008E-16-1.000E 7.769E-16-1.000E 6.748E-16-1.000E 7.388E-16 4.278E 1.100E-16 1.894E 9.894E-17 4.221E 1.92E-16 1.592E 1.202E-16 3.096E 1.513E-16-1.000E 1.386E-16-1.000E 1.386E-16-1.000E 1.487E-16-1.000E 1.595E-16-1.000E 1.667E-16-1.000E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11 -10 1.928E-09 4.009E-09 +00 5.161E-10 2.965E-10 +00 4.062E-10 1.074E-10 +00 6.507E-11 9.664E-11 +00 4.310E-10 8.030E-10 +00 1.652E-09 7.029E-10 -11 3.582E-10 1.184E-11 -10 2.325E-10 5.135E-10 -10 5.189E-10 1.249E-09 -09 4.292E-09 1.506E-11 -11 5.074E-11 7.972E-11 +00 1.516E-11 1.034E-11 -09 5.516E-09 1.367E-08 +00 4.290E-11 6.669E-11 +00 2.748E-11 3.422E-11 +00 1.220E-11 2.719E-11 +00 9.503E-11 2.174E-10
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724           BONE SUR         3.330           BREAST         3.583           TESTES         3.995           OVARIES         2.730           EDEWBODY         3.449           THYROIDH         3.773           MO-99         3.749           STOMACH         5.518           SMALL IN         4.978           LUNGS         5.993           RED MARR         6.057           THYROID         7.579           LOWER LI         5.422           BONE SUR         6.913           BREAST         7.388           TESTES         7.991           OVARIES         5.359           EDEWBODY         7.164           THYROIDH         7.579           TC-99M         7.164	$\begin{array}{l} E-14 & 1.557E-11\\ E-14 & 1.411E-11\\ E-14 & 1.684E-11\\ E-14 & 1.711E-11\\ E-14 & 2.121E-11\\ E-14 & 1.529E-11\\ E-14 & 1.866E-11\\ E-14 & 2.012E-11\\ E-14 & 2.230E-11\\ E-14 & 1.529E-11\\ E-14 & 1.529E-11\\ E-14 & 1.937E-11\\ E-14 & 2.121E-11\\ E-15 & 3.820E-12\\ E-15 & 3.408E-12\\ E-15 & 3.408E-12\\ E-15 & 5.376E-12\\ E-15 & 5.189E-12\\ E-15 & 5.483E-12\\ E-15 & 5.622E-12\\ E-15 & 5.624E-12\\ E-15 & 5.376E-12\\ E-15 & 5.694E-12\\ E-15 & 5.376E-12\\ E-15 & 5.376E-12\\ E-15 & 5.694E-12\\ E-15 & 5.376E-12\\ E-15 $	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10 3.672E-10 3.959E-10 4.388E-10 3.009E-10 3.812E-10 4.173E-10 5.368E-11 4.751E-11 5.884E-11 5.687E-11 7.737E-11 8.176E-11 8.026E-11 4.983E-11 7.37E-11 7.737E-11	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E 5.327E-16 9.234E 6.501E-16-1.000E 7.769E-16-1.000E 7.769E-16-1.000E 7.388E-16 4.278E 1.100E-16 1.894E 9.894E-17 4.221E 1.92E-16 1.592E 1.202E-16 3.096E 1.513E-16-1.000E 1.386E-16-1.000E 1.386E-16-1.000E 1.386E-16-1.000E 1.595E-16-1.000E 1.595E-16-1.000E 1.667E-16-1.000E 1.513E-16 5.884E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11 -10 1.928E-09 4.009E-09 +00 5.161E-10 2.965E-10 +00 4.062E-10 1.074E-10 +00 6.507E-11 9.664E-11 +00 4.310E-10 8.030E-10 +00 1.652E-09 7.029E-10 -11 3.582E-10 1.184E-11 -10 2.325E-10 5.135E-10 -10 5.189E-10 1.249E-09 -09 4.292E-09 1.506E-11 -11 5.074E-11 7.972E-11 +00 1.516E-11 1.034E-11 -09 5.516E-09 1.367E-08 +00 4.290E-11 6.669E-11 +00 2.748E-11 3.422E-11 +00 1.220E-11 2.719E-11 +00 1.075E-09 1.362E-09 -12 1.516E-11 1.034E-11
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724           BONE SUR         3.330           BREAST         3.583           TESTES         3.995           OVARIES         2.730           EDEWBODY         3.449           THYROIDH         3.773           MO-99         3.749           STOMACH         5.518           SMALL IN         4.978           LUNGS         5.993           RED MARR         6.057           HYROID         7.579           LOWER LI         5.422           BONE SUR         6.913           BREAST         7.388           TESTES         7.991           OVARIES         5.359           EDEWBODY         7.164           THYROIDH         7.579           TC-99M         3.50           STOMACH         4.154	$\begin{array}{l} \text{E-14} & 1.557\text{E-11} \\ \text{E-14} & 1.411\text{E-11} \\ \text{E-14} & 1.684\text{E-11} \\ \text{E-14} & 1.711\text{E-11} \\ \text{E-14} & 2.121\text{E-11} \\ \text{E-14} & 1.529\text{E-11} \\ \text{E-14} & 1.529\text{E-11} \\ \text{E-14} & 2.30\text{E-11} \\ \text{E-14} & 2.30\text{E-11} \\ \text{E-14} & 1.529\text{E-11} \\ \text{E-14} & 1.529\text{E-11} \\ \text{E-14} & 1.937\text{E-11} \\ \text{E-14} & 2.121\text{E-11} \\ \text{E-15} & 3.820\text{E-12} \\ \text{E-15} & 3.408\text{E-12} \\ \text{E-15} & 3.740\text{E-12} \\ \text{E-15} & 5.376\text{E-12} \\ \text{E-15} & 5.189\text{E-12} \\ \text{E-15} & 5.622\text{E-12} \\ \text{E-15} & 5.624\text{E-12} \\ \text{E-15} & 5.376\text{E-12} \\ \text{E-15} & 5.694\text{E-12} \\ \text{E-15} & 5.376\text{E-12} \\ \text{E-15} & 5.376\text{E-12} \\ \text{E-15} & 5.776\text{E-12} \\ \end{array}$	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10 3.672E-10 3.959E-10 4.388E-10 3.009E-10 3.812E-10 4.173E-10 5.368E-11 4.751E-11 5.884E-11 5.687E-11 7.737E-11 5.251E-11 7.849E-11 8.026E-11 4.983E-11 7.37E-11 2.875E-12	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E 5.327E-16 9.234E 6.501E-16-1.000E 7.008E-16-1.000E 7.769E-16-1.000E 6.748E-16-1.000E 7.388E-16 4.278E 1.100E-16 1.894E 9.894E-17 4.221E 1.92E-16 1.592E 1.202E-16 3.096E 1.513E-16-1.000E 1.386E-16-1.000E 1.386E-16-1.000E 1.595E-16-1.000E 1.595E-16-1.000E 1.667E-16-1.000E 1.667E-16-1.000E 1.513E-16 5.884E 9.196E-17 1.437E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11 -10 1.928E-09 4.009E-09 +00 5.161E-10 2.965E-10 +00 4.062E-10 1.074E-10 +00 6.507E-11 9.664E-11 +00 4.310E-10 8.030E-10 +00 1.652E-09 7.029E-10 -11 3.582E-10 1.184E-11 -10 2.325E-10 5.135E-10 -10 5.189E-10 1.249E-09 -09 4.292E-09 1.506E-11 -11 5.074E-11 7.972E-11 +00 1.516E-11 1.034E-11 -09 5.516E-09 1.367E-08 +00 4.290E-11 6.669E-11 +00 2.748E-11 3.422E-11 +00 1.075E-09 1.362E-09 -12 1.516E-11 1.034E-11 -11 1.519E-11 7.169E-11
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724           BONE SUR         3.330           BREAST         3.583           TESTES         3.995           OVARIES         2.730           EDEWBODY         3.449           THYROIDH         3.773           MO-99         3.773           STOMACH         5.518           SMALL IN         4.978           LUNGS         5.993           RED MARR         6.057           THYROID         7.579           LOWER LI         5.422           BONE SUR         6.913           BREAST         7.388           TESTES         7.991           OVARIES         5.3591           OVARIES         5.3591           EDEWBODY         7.1641           THYROIDH         7.5791           OVARIES         5.3591           EDEWBODY         7.1642           THYROIDH         7.5791           OVARIES         3.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10 3.672E-10 3.959E-10 4.388E-10 3.009E-10 3.812E-10 4.173E-10 5.368E-11 4.751E-11 5.884E-11 5.687E-11 7.37E-11 5.251E-11 7.849E-11 8.176E-11 8.026E-11 4.983E-11 7.737E-11 2.875E-12 2.489E-12	5.422E-16 1.287E 4.915E-16 2.838E 5.866E-16 7.399E 5.961E-16 1.212E 7.388E-16-1.000E 5.327E-16 9.234E 6.501E-16-1.000E 7.769E-16-1.000E 7.769E-16-1.000E 7.769E-16-1.000E 7.388E-16 4.278E 1.100E-16 1.894E 9.894E-17 4.221E 1.192E-16 1.592E 1.202E-16 3.096E 1.513E-16-1.000E 1.386E-16-1.000E 1.487E-16-1.000E 1.487E-16-1.000E 1.487E-16-1.000E 1.595E-16-1.000E 1.667E-16-1.000E 1.513E-16 5.884E 9.196E-17 1.437E 7.959E-17 3.397E	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11 -10 1.928E-09 4.009E-09 +00 5.161E-10 2.965E-10 +00 4.062E-10 1.074E-10 +00 6.507E-11 9.664E-11 +00 4.310E-10 8.030E-10 +00 1.652E-09 7.029E-10 -11 3.582E-10 1.184E-11 -10 2.325E-10 5.135E-10 -10 5.189E-10 1.249E-09 -09 4.292E-09 1.506E-11 -11 5.074E-11 7.972E-11 +00 1.516E-11 1.034E-11 -09 5.516E-09 1.367E-08 +00 4.290E-11 6.669E-11 +00 2.748E-11 3.422E-11 +00 1.220E-11 2.719E-11 +00 1.075E-09 1.362E-09 -12 1.516E-11 1.034E-11 -11 1.519E-11 7.169E-11 -12 3.520E-12 2.227E-11
NB-95           STOMACH         2.778           SMALL IN         2.515           LUNGS         3.000           RED MARR         3.051           THYROID         3.773           LOWER LI         2.724           BONE SUR         3.330           BREAST         3.583           TESTES         3.995           OVARIES         2.730           EDEWBODY         3.449           THYROIDH         3.773           MO-99         3.773           STOMACH         5.518           SMALL IN         4.978           LUNGS         5.993           RED MARR         6.057           THYROID         7.579           LOWER LI         5.422           BONE SUR         6.913           BREAST         7.388           TESTES         7.991           OVARIES         5.3592           EDEWBODY         7.164           THYROIDH         7.5792           OVARIES         5.3592           EDEWBODY         7.164           THYROIDH         7.5792           OVARIES         5.3592           EDEWBODY         7.1	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.063E-10 2.776E-10 3.314E-10 3.367E-10 4.173E-10 3.009E-10 3.672E-10 3.959E-10 4.388E-10 3.009E-10 3.812E-10 4.173E-10 5.368E-11 4.751E-11 5.884E-11 5.687E-11 7.37E-11 5.251E-11 7.849E-11 8.176E-11 8.026E-11 4.983E-11 7.37E-11 2.875E-12 2.489E-12 3.203E-12	5.422E-16 $1.287E4.915E-16$ $2.838E5.866E-16$ $7.399E5.961E-16$ $1.212E7.388E-16-1.000E5.327E-16$ $9.234E6.501E-16-1.000E7.769E-16-1.000E7.769E-16-1.000E7.78E-16-1.000E7.388E-16$ $4.278E1.100E-16$ $1.894E9.894E-17$ $4.221E1.192E-16$ $1.592E1.202E-16$ $3.096E1.513E-16-1.000E1.386E-16-1.000E1.386E-16-1.000E1.487E-16-1.000E1.487E-16-1.000E1.65E-16-1.000E1.65E-16-1.000E1.67E-16-1.000E1.513E-16$ $5.884E9.196E-17$ $1.437E7.959E-17$ $3.397E1.024E-16$ $2.924E$	-10 6.362E-10 2.796E-10 -10 5.201E-10 9.116E-10 -10 8.319E-09 2.743E-11 -10 4.425E-10 1.993E-10 +00 3.582E-10 1.184E-11 -10 1.928E-09 4.009E-09 +00 5.161E-10 2.965E-10 +00 4.062E-10 1.074E-10 +00 6.507E-11 9.664E-11 +00 4.310E-10 8.030E-10 +00 1.652E-09 7.029E-10 -11 3.582E-10 1.184E-11 -10 2.325E-10 5.135E-10 -10 5.189E-10 1.249E-09 -09 4.292E-09 1.506E-11 -11 5.074E-11 7.972E-11 +00 1.516E-11 1.034E-11 -09 5.516E-09 1.367E-08 +00 4.290E-11 6.669E-11 +00 2.748E-11 3.422E-11 +00 1.075E-09 1.362E-09 -12 1.516E-11 1.034E-11 -11 1.519E-11 7.169E-11

THYROID LOWER LI BONE SUR BREAST TESTES OVARIES EDEWBODY THYROIDH RU-103	6.342E-15 2.656E-12 4.412E-12 1.411E-16-1.000E+00 2.088E-11 8.449E-11 4.027E-15 1.689E-12 2.806E-12 8.974E-17 3.371E-12 3.834E-12 2.545E-11 7.230E-15 3.020E-12 5.017E-12 1.605E-16-1.000E+00 1.784E-12 4.064E-12 7.230E-15 3.050E-12 5.067E-12 1.620E-16-1.000E+00 1.520E-12 3.563E-12 6.437E-15 2.698E-12 4.482E-12 1.433E-16-1.000E+00 5.222E-13 2.294E-12 3.615E-15 1.510E-12 2.509E-12 8.023E-17-1.000E+00 1.703E-12 9.738E-12 5.729E-15 2.418E-12 4.017E-12 1.285E-16-1.000E+00 7.451E-12 1.673E-11 6.342E-15 2.656E-12 4.412E-12 1.411E-16 1.968E-11 2.088E-11 8.449E-11
STOMACH SMALL IN LUNGS RED MARR THYROID LOWER LI BONE SUR BREAST TESTES OVARIES EDEWBODY THYROIDH RU-105	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
STOMACH SMALL IN LUNGS RED MARR THYROID LOWER LI BONE SUR BREAST TESTES OVARIES EDEWBODY THYROIDH RU-106	$\begin{array}{llllllllllllllllllllllllllllllllllll$
RU-106 STOMACH SMALL IN LUNGS RED MARR THYROID LOWER LI BONE SUR BREAST TESTES OVARIES EDEWBODY THYROIDH RH-105	7.293E-15 4.175E-12 8.726E-11 1.452E-16 6.984E-10 2.938E-09 3.119E-09 6.564E-15 3.765E-12 7.869E-11 1.310E-16 1.589E-09 3.397E-09 5.548E-09 7.896E-15 4.531E-12 9.469E-11 1.576E-16 3.044E-08 1.037E-06 1.435E-09 8.054E-15 4.622E-12 9.660E-11 1.608E-16 8.744E-11 1.770E-09 1.483E-09 9.862E-15 5.652E-12 1.181E-10 1.966E-16-1.000E+00 1.733E-09 1.432E-09 7.135E-15 4.093E-12 8.555E-11 1.424E-16 1.604E-08 3.713E-08 7.087E-08 9.037E-15 5.187E-12 1.084E-10 1.804E-16-1.000E+00 1.620E-09 1.445E-09 9.672E-15 5.552E-12 1.160E-10 1.931E-16-1.000E+00 1.798E-09 1.457E-09 1.056E-14 6.053E-12 1.265E-10 2.106E-16-1.000E+00 1.154E-09 1.474E-09 7.103E-15 4.075E-12 8.517E-11 1.417E-16-1.000E+00 1.308E-09 1.656E-09 1.010E-14 9.017E-12 1.885E-10 3.137E-16-1.000E+00 1.289E-07 7.419E-09 9.862E-15 5.652E-12 1.181E-10 1.966E-16 4.022E-11 1.733E-09 1.432E-09
RH-105 STOMACH SMALL IN LUNGS RED MARR THYROID LOWER LI BONE SUR BREAST TESTES OVARIES EDEWBODY THYROIDH SB-127	2.600E-15 1.488E-12 9.870E-12 5.581E-17 6.353E-11 7.262E-11 1.946E-10 2.315E-15 1.327E-12 8.804E-12 4.978E-17 1.353E-10 1.578E-10 4.427E-10 2.841E-15 1.631E-12 1.082E-11 6.120E-17 4.985E-10 9.509E-10 3.847E-12 2.936E-15 1.682E-12 1.116E-11 6.310E-17 5.385E-12 7.746E-12 1.463E-11 3.615E-15 2.071E-12 1.374E-11 7.769E-17-1.000E+00 2.878E-12 2.894E-12 2.556E-15 1.462E-12 9.701E-12 5.486E-17 7.389E-10 1.347E-09 3.781E-09 3.647E-15 2.088E-12 1.385E-11 7.832E-17-1.000E+00 4.441E-12 6.731E-12 3.805E-15 2.189E-12 1.452E-11 8.213E-17-1.000E+00 5.592E-12 8.959E-12 3.837E-15 2.206E-12 1.464E-11 8.276E-17-1.000E+00 2.827E-12 7.209E-12 2.416E-15 1.386E-12 9.197E-12 5.200E-17-1.000E+00 2.105E-11 5.798E-11 3.449E-15 2.012E-12 1.335E-11 7.546E-17-1.000E+00 2.573E-10 3.980E-10
SB-127 STOMACH SMALL IN LUNGS RED MARR THYROID	2.337E-14 1.314E-11 1.623E-10 4.693E-16 2.278E-10 3.267E-10 5.597E-10 2.106E-14 1.181E-11 1.459E-10 4.217E-16 5.199E-10 7.090E-10 1.630E-09 2.534E-14 1.420E-11 1.755E-10 5.074E-16 1.907E-09 6.915E-09 1.574E-11 2.584E-14 1.456E-11 1.799E-10 5.200E-16 9.334E-11 1.547E-10 1.317E-10 3.171E-14 1.784E-11 2.205E-10 6.374E-16-1.000E+00 6.144E-11 4.642E-12

LOWER LI	2.289E-14	1.287E-11	1.590E-10	4.598E-16 3.663E-09 7.432E-09 1.959E-08
BONE SUR				5.835E-16-1.000E+00 1.331E-10 5.225E-11
BREAST				6.247E-16-1.000E+00 9.102E-11 7.574E-11
		· · · · · <b>·</b> - <b>-</b>		6.818E-16-1.000E+00 4.588E-11 5.894E-11
TESTES				
OVARIES				4.566E-16-1.000E+00 2.521E-10 6.148E-10
EDEWBODY				6.088E-16-1.000E+00 1.633E-09 1.948E-09
THYROIDH	3.171E-14	1.784E-11	2.205E-10	6.374E-16 2.443E-11 6.144E-11 4.642E-12
SB-129				
STOMACH	5.264E - 14	1 651E-11	2 316E-11	9.830E-16 1.226E-10 1.235E-10 7.245E-10
SMALL IN				9.006E-16 1.888E-10 1.912E-10 1.473E-09
LUNGS				1.062E-15 8.374E-10 8.954E-10 9.379E-12
RED MARR				1.078E-15 1.608E-11 1.654E-11 3.661E-11
THYROID				1.329E-15-1.000E+00 9.720E-12 1.464E-12
LOWER LI				9.672E-16 2.014E-10 2.321E-10 1.929E-09
BONE SUR	6.247E-14	1.970E-11	2.764E-11	1.170E-15-1.000E+00 1.481E-11 1.332E-11
BREAST	6.786E-14	2.143E-11	3.008E-11	1.272E-15-1.000E+00 1.281E-11 2.560E-11
TESTES	7.515E-14	2.363E-11	3.315E-11	1.405E-15-1.000E+00 5.415E-12 1.105E-11
OVARIES				9.576E-16-1.000E+00 2.148E-11 1.514E-10
EDEWBODY				1.238E-15-1.000E+00 1.740E-10 4.830E-10
				1.329E-15 9.521E-12 9.720E-12 1.464E-12
THYROIDH	7.1036-14	2.2336-11	2.1226-11	1.3296-13 9.3216-12 9.7206-12 1.4046-12
TE-127				
STOMACH				3.456E-18 4.321E-11 4.465E-11 2.425E-10
SMALL IN	1.462E-16	6.717E-14	1.502E-13	3.092E-18 6.822E-11 7.117E-11 3.896E-10
LUNGS	1.788E-16	8.198E-14	1.833E-13	3.773E-18 3.748E-10 4.258E-10 2.885E-12
RED MARR	1.836E-16	8.405E-14	1.879E-13	3.869E-18 3.342E-12 3.986E-12 6.413E-12
THYROID				4.756E-18-1.000E+00 1.844E-12 2.855E-12
LOWER LI				3.393E-18 1.640E-10 2.275E-10 1.265E-09
BONE SUR				4.630E-18-1.000E+00 4.063E-12 6.424E-12
BREAST				4.883E-18-1.000E+00 1.878E-12 2.998E-12
TESTES				5.105E-18-1.000E+00 1.828E-12 2.940E-12
OVARIES				3.298E-18-1.000E+00 2.029E-12 4.040E-12
EDEWBODY				0.000E+00-1.000E+00 8.597E-11 1.874E-10
THYROIDH	2.245E-16	1.033E-13	2.310E-13	4.756E-18 1.590E-12 1.844E-12 2.855E-12
TE-127M				
STOMACH	4.566E-17	7.804E-14	2.953E-12	1.884E-18 8.892E-11 2.302E-10 2.115E-10
SMALL IN				1.287E-18 1.832E-10 3.690E-10 4.338E-10
LUNGS				2.616E-18 2.476E-09 3.337E-08 9.597E-11
RED MARR				1.034E-18 2.769E-10 5.309E-09 5.373E-09
THYROID				5.296E-18-1.000E+00 9.635E-11 9.411E-11
LOWER LI				1.662E-18 2.309E-09 5.719E-09 1.109E-08
BONE SUR				4.503E-18-1.000E+00 2.055E-08 2.086E-08
BREAST				1.322E-17-1.000E+00 1.097E-10 9.733E-11
TESTES	1.877E-16	2.688E-13	7.518E-12	8.118E-18-1.000E+00 9.225E-11 9.303E-11
OVARIES	<b>4.</b> 503E-17	7.676E-14	2.865E-12	1.877E-18-1.000E+00 1.100E-10 1.248E-10
EDEWBODY	1.412E-16	1.758E-13	3.615E-12	6.111E-18-1.000E+00 5.801E-09 2.224E-09
THYROIDH	1.237E-16	1.852E-13	5.663E-12	5.296E-18 1.337E-11 9.635E-11 9.411E-11
TE-129				
STOMACH	1 842E-15	2 273E-13	2 2938-13	3.805E-17 1.553E-11 1.553E-11 3.970E-10
SMALL IN				3.393E-17 1.083E-11 1.083E-11 2.730E-10
LUNGS				4.154E~17 1.526E-10 1.526E~10 4.910E-13
RED MARR				4.186E-17 6.131E-13 6.131E-13 7.610E-13
THYROID				5.264E-17-1.000E+00 5.088E-13 3.350E-13
LOWER LI				3.710E-17 1.838E-12 1.839E-12 3.700E-11
BONE SUR	2.375E-15	2.956E-13	2.981E-13	4.947E-17-1.000E+00 7.058E-13 5.990E-13
BREAST	2.610E-15	3.334E-13	3.363E-13	5.581E-17-1.000E+00 5.381E-13 6.050E-13
TESTES				5.740E-17-1.000E+00 4.522E-13 3.750E-13
OVARIES				3.678E-17-1.000E+00 5.052E-13 1.580E-12
EDEWBODY				9.248E-17-1.000E+00 2.085E-11 5.430E-11
THYROIDH				5.264E-17 5.088E-13 5.088E-13 3.350E-13
	2.32/6-13	2.1400-13	2.1/2E-13	J.204E I/ J.000E-IS D.000E-IS 3.3DUE-IS
TE-129M	1 1575 15	1 0400 10	0 700- 1-	
STOMACH				2.359E-17 2.603E-10 4.813E-10 6.262E-10
SMALL IN				2.099E-17 5.055E-10 7.966E-10 1.470E-09
LUNGS				2.591E-17 4.429E-09 4.028E-08 1.588E-10
RED MARR				2.524E-17 4.854E-10 3.038E-09 3.432E-09
THYROID	1.617E-15	1.753E-12	3.820E-11	3.393E-17-1.000E+00 1.555E-10 1.566E-10
LOWER LI	1.132E-15	1.208E-12	2.639E-11	2.296E-17 4.897E-09 1.100E-08 2.464E-08

BONE SUR BREAST TESTES OVARIES	1.687E-15 1.754E-15	1.936E-12 1.932E-12	4.203E-11 4.207E-11	3.022E+17+1.000E+00 7.149E-09 8.103E-09 3.869E+17-1.000E+00 1.684E-10 1.657E-10 3.773E+17+1.000E+00 1.390E+10 1.604E+10 2.318E+17+1.000E+00 1.783E+10 2.405E+10
EDEWBODY THYROIDH TE-131M	1.644E-15	2.813E-12	6.190E-11	5.035E-17-1.000E+00 6.466E-09 2.885E-09 3.393E-17 3.040E-11 1.555E-10 1.566E-10
STOMACH SMALL IN LUNGS	5.016E-14 5.966E-14	2.504E-11 2.979E-11	1.589E-10 1.895E-10	1.048E-15 2.208E-10 2.758E-10 6.627E-10 9.528E-16 3.920E-10 4.928E-10 1.600E-09 1.133E-15 1.244E-09 2.231E-09 6.208E-11
RED MARR THYROID LOWER LI	7.492E-14	3.757E-11	2.390E-10	1.145E-15 9.441E-11 1.386E-10 2.393E-10 1.430E-15-1.000E+00 3.280E-08 3.908E-08 1.031E-15 1.333E-09 2.367E-09 8.102E-09
BONE SUR BREAST	6.713E-14	3.366E-11	2.159E-10	1.281E-15-1.000E+00 2.608E-10 3.698E-10 1.387E-15-1.000E+00 9.204E-11 1.342E-10
TESTES	7.928E-14	3.970E-11	2.529E-10	1.511E-15-1.000E+00 4.542E-11 9.816E-11
OVARIES				1.016E-15-1.000E+00 2.335E-10 7.370E-10
EDEWBODY THYROIDH TE-132	7.492E-14	3.757E-11	2.390E-10	1.227E-15-1.000E+00 1.634E-09 2.355E-09 1.430E-15 6.429E-09 3.280E-08 3.908E-08
STOMACH				1.551E-16 2.302E-10 4.076E-10 4.855E-10
SMALL IN LUNGS				1.364E-16 3.127E-10 5.081E-10 7.662E-10 1.722E-16 5.740E-10 1.641E-09 2.937E-10
RED MARR				1.681E-16 2.500E-10 3.951E-10 4.064E-10
THYROID				2.308E-16-1.000E+00 5.284E-08 4.695E-08
LOWER LI				1.519E-16 8.207E-10 1.574E-09 3.764E-09
BONE SUR BREAST				2.419E-16-1.000E+00 7.249E-10 8.537E-10 2.686E-16-1.000E+00 3.312E-10 3.126E-10
TESTES	1.078E - 14	4.683E-11	7.922E-10	2.461E-16-1.000E+00 3.374E-10 3.256E-10
OVARIES				1.395E-16-1.000E+00 3.866E-10 5.058E-10
EDEWBODY				2.153E-16-1.000E+00 2.229E-09 2.132E-09
THYROIDH I-131				2.308E-16 2.263E-08 5.284E-08 4.695E-08
STOMACH SMALL IN				2.727E-16 5.997E-11 7.516E-11 3.059E-10 2.435E-16 1.572E-11 2.742E-11 4.471E-11
LUNGS				2.974E-16 4.616E-10 6.565E-10 1.016E-10
RED MARR	1.449E-14	8.678E-12	1.388E-10	3.057E-16 3.518E-11 6.260E-11 9.444E-11
THYROID				3.742E-16-1.000E+00 2.911E-07 4.753E-07
LOWER LI BONE SUR				2.673E-16 1.465E-11 2.593E-11 4.239E-11 3.678E-16-1.000E+00 5.718E-11 8.699E-11
BREAST				3.869E-16-1.000E+00 7.861E-11 1.209E-10
TESTES	1.899E-14	1.143E-11	1.829E-10	4.027E-16-1.000E+00 2.322E-11 3.777E-11
OVARIES				2.584E-16-1.000E+00 2.533E-11 4.067E-11
EDEWBODY THYROIDH				3.553E-16-1.000E+00 8.872E-09 1.434E-08 3.742E-16 1.279E-08 9.694E-08 1.583E-07
I-132	1.7700 11	1.0020 11	1.000 10	J.742E 10 1.275E 00 J.054E 00 1.505E 07
STOMACH				1.598E-15 9.896E-11 9.896E-11 6.320E-10
SMALL IN				1.452E-15 1.245E-11 1.245E-11 3.160E-11
LUNGS RED MARR				1.728E-15 2.702E-10 2.703E-10 2.640E-11 1.757E-15 1.401E-11 1.401E-11 2.450E-11
THYROID	1.126E-13	2.352E-11	2.584E-11	2.163E-15-1.000E+00 1.726E-09 3.842E-09
LOWER LI	8.149E-14	1.703E-11	1.871E-11	1.566E-15 1.126E-11 1.127E-11 2.750E-11
BONE SUR				1.922E-15-1.000E+00 1.242E-11 2.190E-11
BREAST TESTES				2.077E-15-1.000E+00 1.412E-11 2.511E-11 2.293E-15-1.000E+00 9.901E-12 2.220E-11
OVARIES				1.563E-15-1.000E+00 9.960E-12 2.340E-11
EDEWBODY				2.025E-15-1.000E+00 1.026E-10 1.814E-10
THYROIDH I-133	1.126E-13	2.352E-11	2.584E-11	2.163E-15 3.442E-10 5.748E-10 1.279E-09
STOMACH	2.121E-14	1.076E-11	4.720E-11	4.249E-16 1.023E-10 1.046E-10 5.533E-10
SMALL IN				3.837E-16 2.006E-11 2.150E-11 4.041E-11
LUNGS RED MARR	2.305E-14 2 350E-14	1.1/2E-11	5.158E-11	4.630E-16 7.128E-10 8.162E-10 4.518E-11 4.725E-16 2.454E-11 2.717E-11 4.313E-11
THYROID				5.771E-16-1.000E+00 4.855E-08 9.102E-08
LOWER LI	2.077E-14	1.052E-11	4.605E-11	4.154E-16 1.910E-11 2.049E-11 3.883E-11
BONE SUR	2.645E-14	1.350E-11	6.041E-11	5.327E-16-1.000E+00 2.518E-11 4.080E-11

BREAST	2.829E-14 1.439E-11 6.509E-11 5.676E-16-1.000E+00 2.931E-11 4.688E-11
TESTES	3.079E-14 1.566E-11 6.965E-11 6.183E-16-1.000E+00 1.947E-11 3.632E-11
OVARIES	2.071E-14 1.052E-11 4.602E-11 4.154E-16-1.000E+00 1.934E-11 3.573E-11
EDEWBODY	2.685E-14 1.427E-11 6.312E-11 5.637E-16-1.000E+00 1.583E-09 2.800E-09
THYROIDH	2.873E-14 1.462E-11 6.491E-11 5.771E-16 4.778E-09 1.617E-08 3.031E-08
I-134	
STOMACH	9.672E-14 8.230E-12 8.245E-12 1.811E-15 7.081E-11 7.081E-11 5.480E-10
SMALL IN	8.847E-14 7.524E-12 7.537E-12 1.655E-15 5.521E-12 5.521E-12 1.600E-11
LUNGS	1.043E-13 8.893E-12 8.909E-12 1.957E-15 1.429E-10 1.429E-10 1.260E-11
RED MARR	1.059E-13 9.008E-12 9.025E-12 1.982E-15 6.067E-12 6.067E-12 1.090E-11 1.306E-13 1.114E-11 1.116E-11 2.451E-15-1.000E+00 2.848E-10 6.160E-10
THYROID	9.513E-14 8.100E-12 8.115E-12 1.782E-15 4.800E-12 4.800E-12 1.290E-11
LOWER LI BONE SUR	1.148E-13 9.787E-12 9.804E-12 2.153E-15-1.000E+00 5.296E-12 9.290E-12
BREAST	1.246E-13 1.061E-11 1.063E-11 2.334E-15-1.000E+00 6.153E-12 1.160E-11
TESTES	1.379E-13 1.175E-11 1.177E-11 2.584E-15-1.000E+00 4.001E-12 8.860E-12
OVARIES	9.418E-14 8.028E-12 8.043E-12 1.766E-15-1.000E+00 4.235E-12 1.100E-11
EDEWBODY	1.204E-13 1.042E-11 1.044E-11 2.292E-15-1.000E+00 3.548E-11 6.630E-11
THYROIDH	1.306E-13 1.114E-11 1.116E-11 2.451E-15 5.697E-11 9.485E-11 2.051E-10
I-135	
STOMACH	6.093E-14 2.170E-11 4.265E-11 1.065E-15 9.819E-11 9.855E-11 5.403E-10
SMALL IN	5.689E-14 2.020E-11 3.951E-11 9.932E-16 1.878E-11 1.899E-11 4.108E-11
LUNGS	6.589E-14 2.354E-11 4.632E-11 1.154E-15 4.295E-10 4.396E-10 3.737E-11
RED MARR	6.658E-14 2.377E-11 4.682E-11 1.165E-15 2.194E-11 2.231E-11 3.638E-11
THYROID	8.172E-14 2.917E-11 5.765E-11 1.427E-15-1.000E+00 8.435E-09 1.778E-08
LOWER LI	6.056E-14 2.154E-11 4.231E-11 1.057E-15 1.765E-11 1.784E-11 3.937E-11
BONE SUR	7.106E-14 2.561E-11 5.157E-11 1.242E-15-1.000E+00 1.997E-11 3.342E-11
BREAST	7.823E-14 2.817E-11 5.639E-11 1.370E-15-1.000E+00 2.334E-11 3.844E-11
TESTES	8.672E-14 3.094E-11 6.113E-11 1.514E-15-1.000E+00 1.521E-11 3.213E-11
OVARIES	5.897E-14 2.091E-11 4.088E-11 1.029E-15-1.000E+00 1.699E-11 3.616E-11
EDEWBODY	7.257E-14 2.643E-11 5.277E-11 1.285E-15-1.000E+00 3.308E-10 6.041E-10
THYROIDH	8.172E-14 2.917E-11 5.765E-11 1.427E-15 1.434E-09 2.809E-09 5.920E-09
XE-133	
STOMACH	9.450E-16 0.000E+00 0.000E+00 0.000E+00 1.312E-13 1.451E-13 0.000E+00
SMALL IN	7.991E-16 0.000E+00 0.000E+00 0.000E+00 1.368E-13 1.498E-13 0.000E+00
LUNGS	1.113E-15 0.000E+00 0.000E+00 0.000E+00 3.516E-13 3.716E-13 0.000E+00.
RED MARR	7.293E-16 0.000E+00 0.000E+00 0.000E+00 1.558E-13 1.686E-13 0.000E+00
THYROID	1.719E-15 0.000E+00 0.000E+00 0.000E+00-1.000E+00 1.381E-13 0.000E+00
LOWER LI	8.689E-16 0.000E+00 0.000E+00 0.000E+00 1.357E-13 1.486E-13 0.000E+00
BONE SUR	1.976E-15 0.000E+00 0.000E+00 0.000E+00-1.000E+00 1.616E-13 0.000E+00
BREAST TESTES	2.255E-15 0.000E+00 0.000E+00 0.000E+00-1.000E+00 1.415E-13 0.000E+00 1.814E-15 0.000E+00 0.000E+00 0.000E+00-1.000E+00 1.392E-13 0.000E+00
OVARIES	8.340E-16 0.000E+00 0.000E+00 0.000E+00-1.000E+00 1.392E-13 0.000E+00 8.340E-16 0.000E+00 0.000E+00 0.000E+00-1.000E+00 1.464E-13 0.000E+00
EDEWBODY	1.551E-15 0.000E+00 0.000E+00 0.000E+00 1.000E+00 1.762E-13 0.000E+00
THYROIDH	1.719E-15 0.000E+00 0.000E+00 0.000E+00 1.212E-13 1.381E-13 0.000E+00
XE-135	
STOMACH	8.213E-15 0.000E+00 0.000E+00 0.000E+00 2.546E-13 2.575E-13 0.000E+00
SMALL IN	7.293E-15 0.000E+00 0.000E+00 0.000E+00 2.560E-13 2.586E-13 0.000E+00
LUNGS	9.006E-15 0.000E+00 0.000E+00 0.000E+00 7.646E-13 7.685E-13 0.000E+00
RED MARR	9.228E-15 0.000E+00 0.000E+00 0.000E+00 2.532E-13 2.554E-13 0.000E+00
THYROID	1.167E-14 0.000E+00 0.000E+00 0.000E+00-1.000E+00 2.341E-13 0.000E+00
LOWER LI	8.118E-15 0.000E+00 0.000E+00 0.000E+00 2.479E-13 2.504E-13 0.000E+00
BONE SUR	1.202E-14 0.000E+00 0.000E+00 0.000E+00-1.000E+00 2.473E-13 0.000E+00
BREAST	1.253E-14 0.000E+00 0.000E+00 0.000E+00-1.000E+00 2.392E-13 0.000E+00
TESTES	1.227E-14 0.000E+00 0.000E+00 0.000E+00-1.000E+00 2.321E-13 0.000E+00
OVARIES	7.515E-15 0.000E+00 0.000E+00 0.000E+00-1.000E+00 2.525E-13 0.000E+00
EDEWBODY	1.103E-14 0.000E+00 0.000E+00 0.000E+00-1.000E+00 3.151E-13 0.000E+00
THYROIDH	1.167E-14 0.000E+00 0.000E+00 0.000E+00 2.308E-13 2.341E-13 0.000E+00
CS-134	
STOMACH	5.581E-14 3.159E-11 6.615E-10 1.097E-15 3.462E-10 1.251E-08 2.009E-08
SMALL IN	5.042E-14 2.858E-11 5.984E-10 9.925E-16 3.382E-10 1.372E-08 2.178E-08
LUNGS RED MARR	6.025E-14 3.424E-11 7.169E-10 1.189E-15 1.036E-09 1.173E-08 1.746E-08 6.152E-14 3.488E-11 7.303E-10 1.211E-15 9.057E-10 1.178E-08 1.868E-08
THYROID	7.579E-14 4.292E-11 8.986E-10 1.490E-15-1.000E+00 1.113E-08 1.764E-08
LOWER LI	5.454E-14 3.095E-11 6.481E-10 1.075E-15 3.349E-10 1.372E-08 2.177E-08
BONE SUR	6.786E-14 3.844E-11 8.049E-10 1.335E-15-1.000E+00 1.091E-08 1.731E-08
BREAST	7.293E-14 4.136E-11 8.661E-10 1.436E-15-1.000E+00 1.082E-08 1.714E-08

TESTES	8 023E-14	4 556E-11	9 540E-10	1.582E-15-1.000E+00	1.296E-08 2.058E-08
OVARIES	5.454E-14	3.105E-11	6.500E-10	1.078E-15-1.000E+00	1.133E-08 1.798E-08
EDEWBODY					1.253E-08 1.975E-08
THYROIDH CS-136	/.5/9E-14	4.292E-11	8.986E-10	1.490E-15 4./36E-10	1.113E-08 1.764E-08
STOMACH					1.965E-09 3.384E-09
SMALL IN					2.114E-09 3.408E-09
LUNGS RED MARR					2.311E-09 2.617E-09 1.855E-09 2.952E-09
THYROID					1.723E-09 2.736E-09
LOWER LI					2.108E-09 3.404E-09
BONE SUR					1.691E-09 2.697E-09
BREAST TESTES					1.658E-09 2.636E-09 1.881E-09 3.034E-09
OVARIES					1.673E-09 2.699E-09
EDEWBODY	9.792E-14	5.320E-11	9.427E-10	1.863E-15-1.000E+00	1.990E-09 3.062E-09
THYROIDH	1.072E-13	5.830E-11	1.033E-09	2.042E-15 3.585E-10	1.723E-09 2.736E-09
CS-137 STOMACH	2 0105-14	1 1/05-11	2 4205-10	4 0205-16 2 2515-10	8.606E-09 1.390E-08
SMALL IN					9.043E-09 1.436E-08
LUNGS					8.799E-09 1.266E-08
RED MARR					8.295E-09 1.316E-08
THYROID LOWER LI					7.919E-09 1.257E-08 9.063E-09 1.439E-08
BONE SUR					7.933E-09 1.258E-08
BREAST	2.643E-14	1.509E-11	3.192E-10	5.280E-16-1.000E+00	7.823E-09 1.240E-08
TESTES					8.758E-09 1.390E-08
OVARIES EDEWBODY					8.107E-09 1.286E-08 8.628E-09 1.355E-08
THYROIDH					7.919E~09 1.257E-08
BA-139					
STOMACH					9.184E-11 6.880E-10
SMALL IN					7.425E-11 5.560E-10
LUNGS RED MARR					2.529E-10 4.450E-13 4.351E-12 9.610E-13
THYROID					2.905E-12 3.210E-13
LOWER LI	1.138E-15	1.711E-13	1.743E-13	2.423E-17 1.573E-11	1.573E-11 1.000E-10
BONE SUR					4.354E-12 6.400E-13
BREAST TESTES					2.947E-12 5.700E-13 2.870E-12 3.620E-13
OVARIES	1.034E-15	1.554E-13	1.583E-13	2.201E-17-1.000E+00	3.054E-12 1.610E-12
EDEWBODY					4.686E-11 1.080E-10
THYROIDH	1.709E-15	2.598E-13	2.646E-13	3.678E-17 2.905E-12	2.905E-12 3.210E-13
BA-140 STOMACH	6.405E-15	6.623E-12	5.941E-10	1.332E-16 1.416E-10	3.561E-10 5.836E-10
SMALL IN					5.526E-10 1.691E-09
LUNGS					1.678E-09 6.920E-11
RED MARR THYROID					1.221E-09 4.219E-10 2.721E-10 5.583E-11
LOWER LI					4.364E-09 2.630E-08
BONE SUR					2.317E-09 5.331E-10
BREAST					3.023E-10 1.609E-10
TESTES OVARIES					2.908E-10 1.467E-10 4.480E-10 9.877E-10
EDEWBODY					1.020E-09 2.545E-09
THYROIDH					2.721E-10 5.583E-11
LA-140	0 6575 14		0 0545 10	1 4078 15 2 5705 10	
STOMACH SMALL IN					4.664E-10 1.086E-09 9.753E-10 2.968E-09
LUNGS					4.213E-09 4.000E-11
RED MARR	9.481E-14	4.419E-11	3.242E-10	1.643E-15 1.440E-10	2.124E-10 2.816E-10
THYROID					6.865E-11 6.386E-12
LOWER LI BONE SUR					5.498E-09 1.750E-08 1.406E-10 9.757E-11
BREAST					1.453E-10 1.800E-10
TESTES					5.875E-11 1.217E-10

OVARIES	8.276E-14 3.864E-11 2.835E-10 1.436E-15-1.000E+00 4.534E-10 1.334E-09	
EDEWBODY	1.071E-13 5.107E-11 3.746E-10 1.898E-15-1.000E+00 1.315E-09 2.290E-09	
THYROIDH	1.148E-13 5.366E-11 3.936E-10 1.995E-15 3.768E-11 6.865E-11 6.386E-12	
LA-141		
STOMACH	1.566E-15 4.158E-13 6.939E-13 2.667E-17 9.818E-11 9.900E-11 9.310E-10	
SMALL IN	1.475E-15 3.913E-13 6.421E-13 2.511E-17 1.430E-10 1.445E-10 1.370E-09	
LUNGS	1.700E-15 4.510E-13 7.574E-13 2.892E-17 8.319E-10 8.904E-10 2.715E-13	
RED MARR	1.712E-15 4.545E-13 7.461E-13 2.917E-17 5.104E-12 6.845E-12 1.073E-12	
THYROID	2.099E-15 5.594E-13 9.643E-13 3.583E-17-1.000E+00 2.447E-12 5.284E-14	
-		
LOWER LI	1.563E-15 4.152E-13 6.889E-13 2.664E-17 1.440E-10 1.672E-10 1.448E-09	
BONE SUR	1.804E-15 4.812E-13 8.877E-13 3.073E-17-1.000E+00 2.502E-11 6.220E-13	
BREAST	2.001E-15 5.310E-13 9.646E-13 3.393E-17-1.000E+00 2.669E-12 7.068E-13	
TESTES	2.223E-15 5.890E-13 1.010E-12 3.773E-17-1.000E+00 2.300E-12 3.183E-13	
OVARIES	1.516E-15 4.021E-13 6.581E-13 2.581E-17-1.000E+00 2.896E-12 3.757E-12	
	2.569E-15 1.848E-12 2.653E-12 1.192E-16-1.000E+00 1.529E-10 3.750E-10	
EDEWBODY		
THYROIDH	2.099E-15 5.594E-13 9.643E-13 3.583E-17 2.195E-12 2.447E-12 5.284E-14	
LA-142		
STOMACH	1.123E-13 1.396E-11 1.440E-11 1.744E-15 4.911E-11 4.911E-11 8.530E-10	
SMALL IN	1.053E-13 1.307E-11 1.349E-11 1.633E-15 4.066E-11 4.066E-11 7.750E-10	
	1.195E-13 1.490E-11 1.537E-11 1.861E-15 3.508E-10 3.508E-10 8.370E-12	
LUNGS		
RED MARR	1.221E-13 1.521E-11 1.569E-11 1.899E-15 6.799E-12 6.799E-12 1.930E-11	
THYROID	1.433E-13 1.792E-11 1.849E-11 2.239E-15-1.000E+00 4.904E-12 1.160E-12	
LOWER LI	1.113E-13 1.384E-11 1.427E-11 1.728E-15 1.143E-11 1.144E-11 1.901E-10	
BONE SUR	1.262E-13 1.579E-11 1.629E-11 1.972E-15-1.000E+00 5.372E-12 7.400E-12	
BREAST	1.427E-13 1.780E-11 1.836E-11 2.223E-15-1.000E+00 6.257E-12 1.540E-11	
	1.427E-13 1.945E-11 1.036E-11 2.429E-15-1.000E+00 2.103E-12 5.290E-12	
TESTES		
OVARIES	1.037E-13 1.297E-11 1.338E-11 1.620E-15-1.000E+00 5.887E-12 6.970E-11	
EDEWBODY	1.366E-13 1.761E-11 1.816E-11 2.199E-15-1.000E+00 5.587E-11 1.790E-10	
THYROIDH	1.433E-13 1.792E-11 1.849E-11 2.239E-15 4.904E-12 4.904E-12 1.160E-12	
CE-141		
STOMACH	2.388E-15 1.547E-12 3.029E-11 5.391E-17 9.040E-11 1.603E-10 2.240E-10	
SMALL IN	2.074E-15 1.338E-12 2.619E-11 4.661E-17 2.167E-10 2.866E-10 5.893E-10	
LUNGS	2.664E-15 1.729E-12 3.385E-11 6.025E-17 1.538E-09 1.669E-08 1.429E-12	
RED MARR	2.419E-15 1.556E-12 3.047E-11 5.422E-17 2.434E-11 8.891E-11 3.396E-11	
THYROID	3.678E-15 2.412E-12 4.721E-11 8.403E-17-1.000E+00 2.543E-11 1.800E-13	
LOWER LI	2.328E-15 1.502E-12 2.940E-11 5.232E-17 1.972E-09 4.100E-09 8.641E-09	
BONE SUR	4.154E-15 2.703E-12 5.292E-11 9.418E-17-1.000E+00 2.657E-10 2.375E-11	
BREAST	4.249E-15 2.821E-12 5.523E-11 9.830E-17-1.000E+00 4.456E-11 1.105E-11	
TESTES	3.773E-15 2.484E-12 4.864E-11 8.657E-17-1.000E+00 5.369E-12 7.580E-12	
OVARIES	2.093E-15 1.356E-12 2.655E-11 4.725E-17-1.000E+00 5.544E-11 1.076E-10	
EDEWBODY	3.426E-15 2.229E-12 4.364E-11 7.766E-17-1.000E+00 2.436E-09 7.850E-10	
THYROIDH	3.678E-15 2.412E-12 4.721E-11 8.403E-17 3.186E-12 2.543E-11 1.800E-13	
CE-143	5.0701 15 2.4121 12 4.7211 11 0.1051 17 5.1001 12 2.5151 11 1.0001 15	
STOMACH	8.720E-15 4.926E-12 3.092E-11 1.858E-16 1.854E-10 2.121E-10 5.608E-10	
SMALL IN	7.769E-15 4.380E-12 2.749E-11 1.652E-16 4.174E-10 4.914E-10 1.365E-09	
LUNGS	9.545E-15 5.422E-12 3.403E-11 2.045E-16 1.512E-09 3.884E-09 3.829E-12	
RED MARR	9.545E-15 5.330E-12 3.345E-11 2.010E-16 2.039E-11 2.953E-11 5.074E-11	
THYROID	1.234E-14 7.087E-12 4.448E-11 2.673E-16-1.000E+00 6.239E-12 4.351E-13	
LOWER LI	8.498E-15 4.792E-12 3.007E-11 1.807E-16 2.311E-09 4.281E-09 1.167E-08	
BONE SUR	1.195E-14 6.893E-12 4.326E-11 2.600E-16-1.000E+00 1.647E-11 1.610E-11	
BREAST	1.303E-14 7.675E-12 4.817E-11 2.895E-16-1.000E+00 1.661E-11 2.327E-11	
TESTES	1.319E-14 7.616E-12 4.780E-11 2.873E-16-1.000E+00 5.816E-12 1.531E-11	
OVARIES	8.245E-15 4.657E-12 2.923E-11 1.757E-16-1.000E+00 7.556E-11 2.131E-10	
EDEWBODY	1.169E-14 7.369E-12 4.697E-11 2.778E-16-1.000E+00 9.190E-10 1.228E-09	
THYROIDH	1.234E-14 7.087E-12 4.448E-11 2.673E-16 3.686E-12 6.239E-12 4.351E-13	
CE-144		
STOMACH	1.793E-15 9.314E-13 2.002E-11 3.343E-17 6.003E-10 1.185E-09 1.110E-09	
SMALL IN	1.636E-15 8.416E-13 1.811E-11 3.024E-17 1.461E-09 2.166E-09 3.711E-09	
LUNGS	1.960E-15 1.025E-12 2.201E-11 3.675E-17 2.631E-08 7.896E-07 6.514E-12	
RED MARR	1.882E-15 9.613E-13 2.070E-11 3.457E-17 4.025E-11 2.786E-09 8.660E-11	
THYROID	2.505E-15 1.344E-12 2.880E-11 4.810E-17-1.000E+00 2.908E-10 5.137E-12	
LOWER LI	1.761E-15 9.113E-13 1.960E-11 3.272E-17 1.526E-08 3.410E-08 6.638E-08	
BONE SUR	2.426E-15 1.328E-12 2.838E-11 4.738E-17-1.000E+00 4.819E-09 1.304E-10	
	2.649E-15 1.467E-12 3.136E-11 5.235E-17-1.000E+00 3.478E-10 1.215E-11	
BREAST	$2^{\circ}0^{\circ}0^{\circ}0^{\circ}0^{\circ}0^{\circ}0^{\circ}0^{\circ}0$	
TESTES	2.660E-15 1.426E-12 3.057E-11 5.105E-17-1.000E+00 1.922E-10 1.013E-11	

EDEWBODY	8.079E-16 5.398E-13 1.124E-11 1.875E-17-1.000E+00 1.012E-07 5.710E-09
THYROIDH	2.505E-15 1.344E-12 2.880E-11 4.810E-17 3.907E-12 2.908E-10 5.137E-12
PR-143	
STOMACH	3.234E-22 1.802E-19 3.209E-18 6.310E-24 1.398E-10 1.661E-10 3.620E-10
SMALL IN	2.917E-22 1.630E-19 2.902E-18 5.708E-24 3.371E-10 4.126E-10 8.939E-10
LUNGS	3.488E-22 1.947E-19 3.467E-18 6.818E-24 1.960E-09 1.332E-08 6.518E-15
RED MARR	3.552E-22 1.983E-19 3.531E-18 6.944E-24 4.864E-12 1.497E-11 1.039E-12
THYROID	<b>4.376E-22 2.454E-19 4.370E-18 8.593E-24-1.000E+00 9.391E-14 6.518E-15</b>
LOWER LI	3.158E-22 1.766E-19 3.144E-18 6.183E-24 3.304E-09 6.763E-09 1.466E-08
BONE SUR	3.900E-22 2.173E-19 3.870E-18 7.610E-24-1.000E+00 1.495E-11 1.037E-12
BREAST	4.186E-22 2.345E-19 4.176E-18 8.213E-24-1.000E+00 9.391E-14 6.519E-15
TESTES	<b>4.630E-22 2.590E-19 4.611E-18 9.069E-24-1.000E+00 9.390E-14 6.519E-15</b>
OVARIES	3.168E-22 1.775E-19 3.160E-18 6.215E-24-1.000E+00 9.390E-14 6.523E-15
EDEWBODY	1.771E-16 5.553E-13 9.887E-12 1.944E-17-1.000E+00 2.190E-09 1.264E-09
THYROIDH	4.376E-22 2.454E-19 4.370E-18 8.593E-24 8.229E-14 9.391E-14 6.518E-15
ND-147	
STOMACH	<b>4.313E-15 2.675E-12 4.589E-11 9.386E-17 1.419E-10 1.977E-10 3.571E-10</b>
SMALL IN	3.805E-15 2.359E-12 4.046E-11 8.276E-17 3.388E-10 4.346E-10 9.403E-10
LUNGS	4.756E-15 2.982E-12 5.116E-11 1.046E-16 1.634E-09 1.060E-08 2.446E-12
RED MARR	4.471E-15 2.729E-12 4.682E-11 9.576E-17 3.426E-11 9.219E-11 5.042E-11
THYROID	6.279E-15 4.003E-12 6.868E-11 1.405E-16-1.000E+00 1.825E-11 2.699E-13
LOWER LI	4.154E-15 2.567E-12 4.403E-11 9.006E-17 2.868E-09 5.843E-09 1.279E-08
BONE SUR	6.247E-15 4.003E-12 6.868E-11 1.405E-16-1.000E+00 3.258E-10 2.219E-11
BREAST	6.818E-15 4.473E-12 7.674E-11 1.570E-16-1.000E+00 3.465E-11 1.872E-11
TESTES	6.723E-15 4.302E-12 7.379E-11 1.509E-16-1.000E+00 6.749E-12 1.364E-11
OVARIES	4.091E-15 2.539E-12 4.356E-11 8.911E-17-1.000E+00 8.412E-11 1.790E-10
EDEWBODY	5.891E-15 3.991E-12 6.847E-11 1.400E-16-1.000E+00 1.849E-09 1.184E-09
THYROIDH	6.279E-15 4.003E-12 6.868E-11 1.405E-16 4.598E-12 1.825E-11 2.699E-13
NP-239	E 2007 15 2 2207 12 2 2020 11 1 1000 10 1 0000 10 1 2010 10 2 4575 10
STOMACH	5.296E-15 3.236E-12 3.022E-11 1.180E-16 1.059E-10 1.291E-10 3.457E-10
SMALL IN	4.630E-15 2.818E-12 2.632E-11 1.027E-16 2.413E-10 2.988E-10 8.735E-10
LUNGS RED MARR	5.898E-15 3.610E-12 3.371E-11 1.316E-16 9.586E-10 2.348E-09 2.402E-12 5.454E-15 3.314E-12 3.095E-11 1.208E-16 7.943E-11 2.075E-10 4.660E-11
THYROID	7.991E-15 4.915E-12 4.590E-11 1.792E-16-1.000E+00 7.599E-12 2.063E-13
LOWER LI	5.137E-15 3.149E-12 2.941E-11 1.148E-16 1.509E-09 2.916E-09 8.684E-09
BONE SUR	8.815E-15 5.437E-12 5.077E-11 1.982E-16-1.000E+00 2.027E-09 3.609E-11
BREAST	9.037E-15 6.028E-12 5.629E-11 2.198E-16-1.000E+00 2.027E 09 5.009E 11 9.037E-15 6.028E-12 5.629E-11 2.198E-16-1.000E+00 1.623E-11 1.714E-11
TESTES	8.245E-15 5.141E-12 4.801E-11 1.874E-16-1.000E+00 2.296E-11 1.144E-11
OVARIES	4.725E-15 2.897E-12 2.705E-11 1.056E-16-1.000E+00 7.449E-11 1.621E-10
EDEWBODY	7.350E-15 4.572E-12 4.270E-11 1.667E-16-1.000E+00 6.760E-10 8.807E-10
THYROIDH	7.991E-15 4.915E-12 4.590E-11 1.792E-16 4.130E-12 7.599E-12 2.063E-13
PU-238	
STOMACH	6.723E-19 1.396E-15 2.935E-14 4.852E-20 2.725E-10 1.134E-09 1.277E-09
SMALL IN	4.566E-19 4.249E-16 8.939E-15 1.478E-20 6.381E-10 2.222E-09 3.186E-09
LUNGS	1.008E-18 3.021E-15 6.348E-14 1.050E-19 1.436E-06 3.186E-04 8.643E-14
RED MARR	4.535E-19 1.113E-15 2.340E-14 3.869E-20 2.552E-09 5.785E-05 1.266E-08
THYROID	1.465E-18 3.724E-15 7.825E-14 1.294E-19-1.000E+00 3.852E-10 7.993E-14
LOWER LI	6.659E-19 1.780E-15 3.740E-14 6.183E-20 6.605E-09 3.294E-08 5.656E-08
BONE SUR	1.792E-18 5.057E-15 1.063E-13 1.757E-19-1.000E+00 7.211E-04 1.576E-07
BREAST	1.547E-17 1.004E-13 2.110E-12 3.488E-18-1.000E+00 4.394E-10 1.804E-13
TESTES	3.615E-18 1.862E-14 3.913E-13 6.469E-19-1.000E+00 1.038E-05 2.318E-09
OVARIES	6.659E-19 1.716E-15 3.606E-14 5.961E-20-1.000E+00 1.041E-05 2.325E-09
EDEWBODY	4.028E-18 2.290E-14 4.809E-13 7.951E-19-1.000E+00 7.759E-05 1.337E-08
THYROIDH	1.465E-18 3.724E-15 7.825E-14 1.294E-19 1.480E-11 3.852E-10 7.993E-14
PU-239	
STOMACH	1.776E-18 1.489E-15 2.909E-14 5.169E-20 2.533E-10 1.069E-09 1.196E-09
SMALL IN	1.481E-18 9.863E-16 1.881E-14 3.425E-20 5.952E-10 2.097E-09 2.991E-09
LUNGS	2.074E-18 2.210E-15 4.401E-14 7.674E-20 1.352E-06 3.213E-04 7.881E-14
RED MARR	1.671E-18 1.379E-15 2.665E-14 4.788E-20 2.400E-09 6.568E-05 1.405E-08
THYROID	2.901E-18 2.877E-15 5.717E-14 9.989E-20-1.000E+00 3.757E-10 7.495E-14
LOWER LI	1.735E-18 1.616E-15 3.182E-14 5.613E-20 6.175E-09 3.099E-08 5.316E-08
BONE SUR	3.425E-18 3.635E-15 7.276E-14 1.262E-19-1.000E+00 8.167E-04 1.748E-07
BREAST	8.562E-18 3.991E-14 8.344E-13 1.386E-18-1.000E+00 3.990E-10 1.207E-13
TESTES	3.710E-18 8.548E-15 1.762E-13 2.968E-19-1.000E+00 1.197E-05 2.631E-09
OVARIES	1.573E-18 1.479E-15 2.915E-14 5.137E-20-1.000E+00 1.194E-05 2.624E-09
EDEWBODY	3.646E-18 1.003E-14 2.107E-13 3.484E-19-1.000E+00 8.299E-05 1.396E-08

THYROIDH PU-240	2.901E-18	2.877E-15	5.717E-14	9.989E-20 1.38	1E-11 3.757	7E-10 7.495E-14
	C 07CD 10	1 2075 15	2 0145 14	4 820B 20 2 FE		
STOMACH						9E-09 1.201E-09
SMALL IN						3E-09 3.005E-09
LUNGS						BE-04 8.206E-14
RED MARR						2E-05 1.405E-08
THYROID						BE-10 7.499E-14
LOWER LI						2E-08 5.337E-08
BONE SUR	1.842E-18	4.948E-15	1.039E-13	1.719E-19-1.00	0E+00 8.145	5E-04 1.746E-07
BREAST	1.490E-17	9.586E-14	2.013E-12	3.330E-18-1.00	0E+00 4.333	BE-10 1.734E-13
TESTES	3.583E-18	1.789E-14	3.758E-13	6.215E-19-1.00	0E+00 1.197	7E-05 2.631E-09
OVARIES	6.881E-19	1.689E-15	3.547E-14	5.866E-20-1.00	0E+00 1.197	7E-05 2.632E-09
EDEWBODY						LE-05 1.397E-08
THYROIDH						BE-10 7.499E-14
PU-241	1.5555 10	0.0012 10		1.0,00 19 1.00	10 11 01/01	
STOMACH	0 0005+00	8 975-19	3 2805-16	0 0005+00 2 41	5	5E-11 6.080E-12
SMALL IN						$5E-11 \ 1.513E-11$
LUNGS						2E-06 4.468E-15
RED MARR						5E-06 2.780E-10
THYROID						DE-12 1.011E-15
LOWER LI						5E-10 2.694E-10
BONE SUR	••••					5E-05 3.467E-09
BREAST						LE-11 2.780E-15
TESTES						BE-07 5.636E-11
OVARIES	0.000E+00	7.912E-19	2.915E-16	0.000E+00-1.00	0E+00 2.755	5E-07 5.650E-11
EDEWBODY	7.153E-20	6.100E-17	1.281E-15	2.118E-21-1.00	0E+00 1.334	E-06 2.069E-10
THYROIDH	0.000E+00	1.430E-18	5.268E-16	0.000E+00 1.87	2E-15 9.130	)E-12 1.011E-15
AM-241						
STOMACH	4.883E-16	4.036E-13	8.475E-12	1.402E-17 5.09	1E-10 3.253	LE-09 1.345E-09
SMALL IN						LE-09 3.330E-09
LUNGS						7E-05 3.364E-11
RED MARR						3E-04 1.448E-06
THYROID						5E-09 1.321E-11
LOWER LI						LE-08 5.810E-08
						5E-03 1.802E-05
BONE SUR						
BREAST						5E-09 2.625E-11
TESTEŠ						3E-05 2.693E-07
OVARIES						LE-05 2.706E-07
EDEWBODY						E-04 9.819E-07
THYROIDH	9.418E-16	7.834E-13	1.645E-11	2./21E-1/ 2./6	1E-10 1.596	SE-09 1.321E-11
CM-242						
STOMACH						7E-09 1.423E-09
SMALL IN						5E-09 3.545E-09
LUNGS						5E-05 8.833E-12
RED MARR						BE-06 3.581E-08
THYROID	1.560E-18	4.581E-15	9.487E-14	1.592E-19-1.00	0E+00 9.384	E-10 8.805E-12
LOWER LI	7.135E-19	2.090E-15	4.328E-14	7.262E-20 6.54	6E-09 3.118	BE-08 6.234E-08
BONE SUR	1.899E-18	5.886E-15	1.219E-13	2.045E-19-1.00	0E+00 4.862	2E-05 4.463E-07
BREAST	1.719E-17	1.059E-13	2.192E-12	3.678E-18-1.00	0E+00 9.415	5E-10 8.935E-12
TESTES						5E-07 5.190E-09
OVARIES						E-07 5.198E-09
EDEWBODY						BE-06 3.102E-08
THYROIDH						E-10 8.805E-12
CM-244	1.5000 10	4.3010 13	J.40/L 14	1.5526 15 5.04	01 10 2.504	10 0.005E 12
STOMACH	5 1058-10	1 2005-15	2 0145-14	4 9205-20 5 10	18-10 1 712	2E-09 1.356E-09
SMALL IN						7E-09 3.362E-09
LUNGS						SE-05 8.846E-12
RED MARR THYROID						DE-05 7.766E-07
						5E-09 8.467E-12
LOWER LI				6.215E-20 6.28		
BONE SUR				1.760E-19-1.00		
BREAST						2E-09 8.920E-12
TESTES				6.659E-19-1.00		
OVARIES						E-05 1.324E-07
EDEWBODY						E-05 5.429E-07
THYROIDH	1.186E-18	3.929E-15	8.244E-14	1.364E-19 2.90	9E-10 1.015	5E-09 8.467E-12

## A.3 SITE

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Surry Sequoyah Peach Bottom Grand Gulf

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MACCS SITE DATA FILE FOR SURRY (JLS, 11/10/88) SECPOP POP DISTRIBUTION FROM 1980 CENSUS DATA ALTERED USING 0-10 MI NRC DATA 26 SPATIAL INTERVALS 16 WIND DIRECTIONS								
7 CROP	CATEGORIES PATHWAY IS	OTOPES						
2 WATER								
SPATIAL D 0.16	TSTANCES	1.21	1.61	2.13	3.22	4.02	4.83	
5.63 48.28	0.52 8.05 64.37	11.27 80.47	16.09 112.65	20.92 160.93	25.75 241.14	32.19 321.87	40.23 563.27	
804.67 POPULATIO	1609.34 N							
6.	0. 25.	0. 3341. 5403.	0. 7107.	0. 2173.	0. 0.	4. 1305.	5. 474.	
2252. 2487346.	2945. 104331.	5403.	20169.	112004.	3431358.	1355700.	2742710.	
0. 15.	0. 63.	0. 1667. 5317.	0. 3550.	1. 1330.	2. 1072.	9. 3198.	13. 2425.	
515. 3290082.	9469. 830354.	5317.	7120.	13586.	198785.	1058744.	20508438.	
8.	0. 31.	0. 822. 0.	0. 1752.	0. 4543.	0. 1713.	5. 1597.	6. 2296.	
6535. 7620063.	1775. 1169436.	0.	8555.	48596.	119411.	233382.	3003954.	
0. 2.	1169436. 0. 11. 129.	543.	0. 1157.	3820.	1621.	3364.	1. 0. 0.	
0. 0.	0.	0079.	0	0.	0.	0.	0.	
0	0. 0. 2317.	0. 4798. 1756.	10202.	10348.	10480.	9570.	0.	
0. 0.	0.	0.	0.	0.	0.	1.	1.	
1. 24195.	2317. 0. 0. 7. 80412.	8316. 57477.	17684. 0.	16340. 0.	30419. 0.	39474. 0.	74998. 0.	
0. 0.	0. 0.	0.	0.	0.	0.	0.	0.	
0. 12620 <b>3</b> .	0. 0. 0. 372471.	0. 68327.	0. 8599.	1722. 6339.	6433. 1057.	36763. 0.	20632. 0.	
0. 0. 3.	0. 0.	0. 127. 3360.	0.	0.	0.	2.	2.	
	20020	3360.	273. 36387.	10447.	4571. 12402.	3441. 0.	7838. 0.	
0. 23.	0. 0. 93.	5.	4.	8.	23.	14.	20. 4065. 0.	
1106.	14665.							
0. 29.	0. 0. 117. 17636.	0. 45.	0. 105.	0. 0.	0. 510.	19. 951.	25. 1521.	
1223. 280809.	17636. 8801784.							
23.	0. 93.	0. 155.	0. 338.	1. 125.	2. 1079.	14. 0.	20. 1355. 1538059.	
2765. 1526840.	154. 3099458.	5296.	21409.	62228.	523803.	479588.	1538059.	
	0. 93.	0. 110. 4132.	0. 240.	1. 1056.	2. 0.	14. 50.	20. 1396.	
915. 3957581.	3153. 10560254.	4132.	16295.	35596.	239712.	/09522.	2845970.	
0. 38. 155.	10560254. 0. 154. 66531.	0. 30. 40902	0. 70. 9557	0. 450. 44818	U. 0. 194801	25. 980. 376828	33. 517. 1492286	
2250273.	12145932.	10306,	2001.	<b>44010</b> .	T)4001.	570020.	1792200.	

0. 12. 1986. 5086913	0. 47. 32459. 19537940.	0. 31. 183133.	0. 69. 193630.	"0. 0. 30369.		. 281.	445.
0. 0. 2794. 7535605.	0. 0. 6593.	0. 223. 96857.	0. 477. 107328.	0. 0. 47585.			4175263.
0. 23. 3965. 1969210.			0. 5326. 10765.		0. 1826. 970659.	1884.	20. 275. 1396088.
1.00 0.85 1.00 1.00 0.90 0.45	0.00 0.00 0.70 0.75 1.00 1.00 0.60 0.20	0.55 0.70 0.90 0.70 0.50 0.50	$\begin{array}{c} 0.60 \ 1.00 \\ 0.40 \ 0.00 \\ 0.30 \ 0.25 \end{array}$	1.00 0.95 0.00 0.45 0.50 0.60	1.00 0.95	0.40 0.60	1.00 1.00
0.85 0.20 1.00 1.00 0.15 0.00	1.00 1.00 0.00 0.20 1.00 1.00 0.45 0.30 1.00 1.00	$\begin{array}{c} 0.00 & 0.00 \\ 1.00 & 0.80 \\ 0.00 & 0.00 \end{array}$	$\begin{array}{cccc} 0.00 & 0.00 \\ 0.10 & 0.00 \\ 0.00 & 0.00 \end{array}$	$\begin{array}{cccc} 0.00 & 0.00 \\ 0.00 & 0.00 \\ 0.00 & 0.00 \end{array}$	1.00 1.00	0.75 0.30	0.40 0.00
1.00 1.00 0.15 0.25 1.00 1.00	0.00 0.00 1.00 1.00 0.25 0.00 1.00 1.00	1.00 0.70 0.00 0.00 1.00 1.00	$\begin{array}{cccc} 0.00 & 0.00 \\ 0.00 & 0.00 \\ 0.55 & 0.50 \end{array}$	0.00 0.80 0.00 0.00 0.25 0.15			
1.00 1.00 1.00 1.00 1.00 1.00	$\begin{array}{c} 1.00 & 0.40 \\ 1.00 & 1.00 \\ 1.00 & 1.00 \\ 1.00 & 1.00 \\ 1.00 & 1.00 \end{array}$	1.00 1.00 0.95 0.20 1.00 1.00	$\begin{array}{c} 1.00 & 1.00 \\ 0.00 & 0.00 \\ 1.00 & 1.00 \end{array}$	1.00 0.90 0.00 0.00 1.00 1.00			
1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 0.70 0.40 1.00 1.00	1.00 1.00 1.00 1.00 0.20 0.75 0.95 1.00	1.00 1.00 1.00 0.75 0.95 1.00 1.00 1.00	1.00 1.00 0.50 0.40 1.00 1.00 1.00 0.80	1.00 1.00	1.00 1.00	1.00 1.00
1.00 1.00 1.00 1.00 1.00 1.00	$\begin{array}{c} 0.00 & 0.00 \\ 1.00 & 1.00 \\ 0.00 & 0.00 \\ 1.00 & 1.00 \\ 0.00 & 0.00 \end{array}$	0.95 0.90 0.00 0.00 1.00 1.00	1.00 1.00 0.00 0.15 1.00 1.00	1.00 1.00 0.70 0.90 1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00
0.85 0.95 1.00 1.00 1.00 1.00 1.00 1.00	$\begin{array}{c} 1.00 \ 1.00 \\ 0.00 \ 0.00 \\ 1.00 \ 1.00 \\ 0.00 \ 0.00 \end{array}$	1.00 1.00 0.00 0.00 1.00 1.00 0.00 0.00	$\begin{array}{c} 1.00 & 1.00 \\ 0.00 & 0.15 \\ 1.00 & 1.00 \\ 0.00 & 0.00 \end{array}$	0.90 0.85 0.80 0.75 0.50 0.45 0.00 0.90	0.80 0.85	0.95 1.00	1.00 1.00
REGION IN 4444505050 444444444 444444444 44444444	5050505044 444450505044 44505050504 4450505050	444444444444444444444444444444444444	1444444444 1444444444 1444444444 1450445050 1444444450 144444444 1444444431 144444443131 144444443131 144444444	1818 72830 18 7283019 18505050505 505050505050 505050505050 3131505050 3131505050 3131315050 31313138 9 31313138 9 31313138 9 44444451 444444615 444444653 444443653	54 17 50 50 50 50 50 50 50 8 8 1 40 11 47 20		
$\begin{array}{c}1&1&2&2&2\\1&1&1&1&1&1\end{array}$	$\begin{array}{c} 1 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\$	11211	1 1 1 1 2	2 2 2 2 2 2	1		

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TENN	.509	.153	360.	1850.	66000.
TEX	.816	.064	164.	1492.	74000.
UTAH	.225	.259	123.	1286.	60000.
VT	.286	.789	628.	1472.	73000.
VA	.382	.198	371.	2075.	84000.
WASH	.377	.154	476.	1948.	82000.
W.VA	.246	.224	150.	1728.	58000.
WIS	.517	.591	723.	1751.	76000.
WYO	.561	.028	43.	- 380.	70000.
BRIT COL	.377	.154	476.	1948.	60000.
OCEAN	.000	.000	0.	0.	0.
SASKAT	.657	.030	61.	563.	60000.
MANITOBA	.924	.048	164.	948.	60000.
ONTARIO	.597		516.	2111.	60000.
QUEBEC			711.	1378.	60000.
		• = • •			60000.
BAJA CAL			1022.	4394.	10000.
		-			10000.
				473.	10000.
COAHUILA	.816	.064	164.	1492.	10000.
	TEX UTAH VT VA WASH W.VA WIS WYO BRIT COL OCEAN SASKAT MANITOBA ONTARIO QUEBEC NOVA SCOT BAJA CAL SONORA CHIHUAHUA	TEX       .816         UTAH       .225         VT       .286         VA       .382         WASH       .377         W.VA       .246         WIS       .517         WYO       .561         BRIT COL       .377         OCEAN       .000         SASKAT       .657         MANITOBA       .924         ONTARIO       .597         QUEBEC       .310         NOVA SCOT       .079         BAJA CAL       .330         SONORA       .516         CHIHUAHUA       .590	TEX.816.064UTAH.225.259VT.286.789VA.382.198WASH.377.154W.VA.246.224WIS.517.591WYO.561.028BRIT COL.377.154OCEAN.000.000SASKAT.657.030MANITOBA.924.048ONTARIO.597.223QUEBEC.310.589NOVA SCOT.079.260BAJA CAL.330.144SONORA.516.104CHIHUAHUA.590.144	TEX.816.064164.UTAH.225.259123.VT.286.789628.VA.382.198371.WASH.377.154476.W.VA.246.224150.WIS.517.591723.WYO.561.02843.BRIT COL.377.154476.OCEAN.000.0000.SASKAT.657.03061.MANITOBA.924.048164.ONTARIO.597.223.516.QUEBEC.310.589.711.NOVA SCOT.079.260662.BAJA CAL.330.1441022.SONORA.516.104.110.CHIHUAHUA.590.144.53.	TEX.816.064164.1492.UTAH.225.259123.1286.VT.286.789628.1472.VA.382.198371.2075.WASH.377.154476.1948.W.VA.246.224150.1728.WIS.517.591723.1751.WYO.561.02843.380.BRIT COL.377.154476.1948.OCEAN.000.000.0.SASKAT.657.03061.563.MANITOBA.924.048164.948.ONTARIO.597.223516.2111.QUEBEC.310.589711.1378.NOVA SCOT.079.260662.1133.BAJA CAL.330.1441022.4394.SONORA.516.104110.682.CHIHUAHUA.590.14453.473.

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SECPOP PO 26 SPATI 16 WIND 7 CROP	E DATA FILE P DISTRIBUT AL INTERVAL DIRECTIONS CATEGORIES PATHWAY ISO SHEDS	ION FROM 19 S	YAH (JLS, 3 980 CENSUS	11/10/88) DATA ALTE	RED USING	NRC 0-10 M	II DATA
	MIC REGIONS						
SPATIAL D	ISTANCES						
0.16		1.21	1.61	2.20	3.22	4.02	4.83
5.63	8.05 64.37	11.2/	10.09	20.92	25.75	32.19	40.23
48.28 804.67	1609.34	80.47	112.05	100.93	241.14	521.07	503.27
POPULATIO	N 1009.34						
0.	N 0. 108. 3480. 4488368	1.	2.	3.	9.	17.	23.
27.	108.	94.	205.	1723.	2650.	2143.	3115.
0.	3480.	11182.	17930.	28763.	115019.	418223.	5029591.
4226619.	4488368. 0. 123. 7260.			•			
0.	122	0.	0.	120	0.	5200	26.
2201.	7260	7325	32422	30166	160847	199147	1890643
6355716	4462791.	1525.	JZ722.	50100.	100047.	1))147.	1090043.
0.00007101	4462791. 0. 62. 8158. 16777882.	0.	. 0.	0.	0.	10.	13.
15.	62.	100.	219.	1268.	0.	842.	1545.
4148.	8158.	13530.	64005.	402619.	182881.	264818.	1337697.
1010000.	16777882.	_	_				
0.	0.	2. 137. 14663.	2.	4.	12.	21.	29.
34.	139.	137.	303.	1/91.	84.	2410.	1700710
3279.	25166. 33429318.	14003.	20036.	90922.	T00200.	42/081.	1/08/18.
2/01907.		4	٦	6	17	19.	26
21	125.	109.	241.	8099.	4329.	4865.	3644.
1631.	4373.	5694.	10190.	40504.	307949.	679113.	2706447.
1836035.							
0.	0. 185. 1342.	10. 284. 11514.	8.	15.	42.	30.	39.
46.	185.	284.	616.	14472.	17775.	2090.	0.
2584.	1342.	11514.	18499.	39805.	264994.	248066.	1611099.
158953. 0.	0.	28. 221. 5016.	21	13	108	10	26
31.	124	20.	479	1696	3491	3673	573
2284.	1781.	5016	12098.	124573.	247313.	116761.	926895.
20508.	0.						
Ο.	0.	10. 317. 8113.	8.	15.	42.	30.	39.
46.	185.	317.	683.	4433.	1428.	1116.	4812.
8921.	35672.	8113.	18140.	440744.	1509163.	332123.	724766.
1849557.	7058200.	13.	11.				
0. 51.	0. 201.	13.	11.	21.	12002	34.	42. 10102
5243.		9798	83659	74015	13902. 179136.	445749	722824
88247.	0.		05055.				
0.	0.	10.	8.	15.	42. 16715. 219844.	24.	33.
38.	155.	1388.	2964.	18490.	16715.	47757.	20708.
13611.	14501.	10374.	25951.	87033.	219844.	165903.	817257.
727568.	0.	_	_				
0.	0.	0. 1035. 8404.	0.	0.	0.	20.	26.
31.	123.	1035.	2207.	11021.	32871.	58191. 710000	25162.
5119. 2030755	10063. 2621959.	8404.	43649.	85130.	330313.	/18998.	539129.
0	2021232.	6	6	10	28. 8121. 203432.	187	229
0. 270.	0. 1064.	1598.	3402.	25316.	8121.	4311.	247.
2740.	13641.	9228.	7319.	198972.	203432.	153718.	737715.
		-					
0.	0.	6.	6.	10.	28.	63.	78.
93.	366.	928.	1979.	0.	996.	0.	4192.
	5408.	6. 928. 6558.	45279.	45072.	142776.	147560.	1566084.
1144300.	4699268.						

0. 148. 1346. 952215.	0. 582. 6102. 4577283.	4. 1596. 1913.	3. 3404. 27190.	6. 0. 109653.	17. 148. 372482.	100. 1389. 105699.	124. 2780. 775542.
932213. 0. 90. 438. 3299217.	4377283. 0. 355. 977. 5212747.	9. 1437. 10997.	8. 3063. 34763.	15. 170. 56460.	38. 549. 458043.	61. 806. 255865.	76. 1180. 988566.
0. 38. 3963. 8653033.	0. 154. 3087. 9372618.	13. 317. 4143.		21. 165. 42869.	55. 0. 162004.	25. 1108. 191306.	33. 1298. 1389826.
	0.75 0.90			0.30 0.80	0.90 0.95	0.95 1.00	1.00 1.00
1.00 0.50		0.00 0.40	0.75 0.75	0.95 0.50	0.50 0.55	0.60 0.50	0.70 0.80
1.00 0.20		0.00 0.40	0.90 1.00	1.00 1.00	1.00 1.00	0.95 0.50	1.00 1.00
1.00 0.50		0.10 0.90	1.00 1.00	1.00 1.00	1.00 1.00	1.00 0.80	0.70 1.00
	1.00 1.00 0.00 0.00			0.95 0.00 1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00
	1.00 0.95 0.00 0.00			0.40 0.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00
0.90 1.00	1.00 0.95	0.95 1.00	0.95 0.90				
1.00 1.00	1.00 1.00	1.00 1.00	1.00 0.95				
1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00				
1.00 1.00	1.00 0.80	1.00 1.00	0.95 0.85				
1.00 1.00	1.00 1.00	1.00 0.95	1.00 1.00	0.75 0.00			
1.00 1.00	1.00 0.95	0.90 0.90	1.00 1.00				
0.90 0.95	1.00 1.00	1.00 0.95	1.00 1.00				
1.00 1.00	1.00 0.80	1.00 1.00	0.95 1.00				
1.00 1.00	1.00 1.00	1.00 1.00	0.75 1.00				
	1.00 1.00 1.00 0.95				1.00 1.00	1.00 1.00	1.00 1.00
1.00 1.00	1.00 1.00 1.00 1.00	1.00 1.00	1.00 1.00	0.60 0.50	0.80 1.00	1.00 1.00	1.00 1.00
REGION IN 40404040404	DEX				20		
40	4040404040	4040404040	4040404040	4015151533	30		
40404040404	4040404040	4040404040	4040404040	40313131313	50		
40404040404 4040404040404	4040404040	4040404040	404040 9 9	9 9 93850	50		
4040404040 4040404040					-		
4040404040 404040404040	404040404040	40404040 9	99999	1 1 1 1 150	50		
4040404040	4040404040	4040404040	409911	1 1 122164	11		
40							
4040404040	4040404040	4040404040	4040404040	4040402323	14		
4040404040 4040404040	4040404040 4040404040	4040404040 4040404040	4040404040 4040404040	40401511111 40151512114	L3 17		
WATERSHED	INDEX			1 1 1 1 1			
11111	11111	11111	11111	11111 11111 11111	1		
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$\begin{array}{c}1&1&1&1&1&1&1&1&1&1\\1&1&1&1&1&1&1&1&1&1$		$\begin{array}{cccccccccccccccccccccccccccccccccccc$	
1 PASTURE 2 STORED FORAGE 3 GRAINS 4 GRN LEAFY VEGETAE 5 OTHER FOOD CROPS 6 LEGUMES AND SEEDS 7 ROOTS AND TUBERS WATERSHED DEFINITION 1 SR-89 2 SR-90 3 CS-134 4 CS-137 BEGLONAL ECONOMIC DAT	150. 240. 150. 240. BLES 150. 240. 150. 240. 5 150. 240. 150. 240. 150. 240. INITIAL AND	0.69 0.006 0.16 0.007 0.005 0.15 0.001 ANNUAL WASHOFF AN 5.0E-6 0.0 5.0E-6 0.0 5.0E-6 0.0 5.0E-6 0.0	D INGESTION FACTORS
REGIONAL ECONOMIC DAT         1 ALA         2 ARIZ         3 ARK         4 CALIF         5 COLO         6 CONN         7 DEL         8 FLA         9 GA         10 IDAHO         11 ILL         12 IND         13 IOWA         14 KANS         15 KY         16 LA         17 MAINE         18 MD         19 MASS         20 MICH         21 MINN         22 MISS         23 MO         24 MONT         25 NEBR         26 NEV         27 N.H.         28 N.J.         30 N.Y.         31 N.C.         32 N.DAK         33 OHIO         34 OKLA         35 OREG         36 PA         37 R.I.         38 S.C.		9. $1824.$ $624$ 0. $682.$ $74.$ 6. $2049.$ $61.$ 2. $4394.$ $93.$ 1. $971.$ $83.$ 5. $4980.$ $107.$ 3. $3428.$ $82.$ 2. $3341.$ $80.$ 3. $1885.$ $73.$ 3. $1562.$ $61.$ 9. $3900.$ $86.$ 1. $3283.$ $72.$ 5. $3133.$ $73.$ 1. $1204.$ $81.$ 2. $1838.$ $61.$ 2. $1838.$ $61.$ 2. $1838.$ $61.$ 9. $3284.$ $61.$ 9. $3284.$ $61.$ 9. $2563.$ $97.$ 8. $2187.$ $81.$ 6. $2111.$ $82.$ 3. $2084.$ $53.$ 2. $1647.$ $76.$ 1. $563.$ $65.$ 8. $1148.$ $75.$ 3. $601.$ $84.$ 9. $2658.$ $68.$ 1. $1378.$ $94.$ 0. $2658.$ $68.$ 4. $948.$ $69.$ 0. $2658.$ $68.$ 4. $1508.$ $67.6$ 4. $1508.$ $67.6$ 5. $1203.$ $73.6$ 6. $2534.$ $78.6$ 2. $6438.$ $80.6$ 2. $1843.$ $62.6$	000. 000.

41 TEX       .         42 UTAH       .         43 VT       .         44 VA       .         45 WASH       .         46 W.VA       .         47 WIS       .         48 WYO       .         49 BRIT COL       .         50 OCEAN       .         51 SASKAT       .         53 ONTARIO       .         54 QUEBEC       .         55 NOVA SCOT       .         56 BAJA CAL       .         57 SONORA       .         58 CHIHUAHUA       .	377 .154 000 .000 657 .030 924 .048 597 .223 310 .589 079 .260 330 .144 1 516 .104	164. 123. 628. 371. 476. 150. 723. 43. 476. 0. 61. 164. 516. 711. 662. 022. 110.	1492. 1286. 1472. 2075. 1948. 1728. 1751. 380. 1948. 0. 563. 948. 2111. 1378. 1133. 4394.	66000. 74000. 60000. 73000. 84000. 82000. 58000. 76000. 60000. 60000. 60000. 60000. 60000. 10000. 10000. 10000.
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MACCS SITE I SECPOP POP I 26 SPATIAL 16 WIND DII 7 CROP CA	DISTRIBUT INTERVAL RECTIONS FEGORIES	ION FROM 1 S	I BOTTOM (J 980 CENSUS	JLS, 11/10, S DATA ALT	/88) ERED USING	NRC 0-10 M	4I DATA
4 WATER PA 2 WATERSHI	EDS						
59 ECONOMIC SPATIAL DIST	DANCEC						
0.40 5.63 48.28	0.82	1.21	1.61	2.43	3.22	4.02	4.83
5.63	8.05	11.27	16.09	20.92	25.75	32.19	40.23
48.28	64.37	80.47	112.65	160.93	241.14	321.87	563.27
804.67 POPULATION							
0.	0.	0.	0.	0.	0. 5557. 215849.	20.	26.
31.	122.	406.	867.	2212.	5557.	68185.	42610.
36746.	25232.	43251.	88038.	210634.	215849.	547385.	1124293.
25550.	0.	1.	1.	3.	7. 1870. 430572.	19	26
30.	123.	455.	977.	5385.	1870.	9336.	12012.
13500.	29877.	188747.	79915.	174604.	430572.	162914.	1349066.
393839. 0.	0.	-	2		8. 2235.	24	22
37.	151	413	∠. 889	1602	2235	24. 3231	32. 10573
14456.	22521.	91474.	220858.	495439.	1870811.	1387490.	5663616
1201796.	326019.	_		_			
0.	0.	0.	1.	2.	4. 1710. 10635304.	31.	39.
40. 26164	90241	323. 164108	700. 2425058	2912. 987201	10635304	3207. 3591517	3038. 4107688
32847.	0.	104100.	2423030.	<i>JU1201</i> .	10033304.	3391317.	410/000.
0.	0.	6.	5.	14.	21. 4260. 268826.	32.	41.
49.	195.	323.	698.	1871.	4260.	5207.	9780.
37964. 0.	241423.	21//33.	/45025.	219373.	208820.	0.	0.
0.	0.	0.	0.	0.	0. 760. 49837.	32.	39.
46.	183.	354.	755.	4439.	760.	4691.	11312.
40619. 0.	35254.	18393.	113077.	188361.	49837.	0.	0.
0.	0.	0	0	0	0. 3109. 9233.	28	36
43.	169.	406.	870.	3309.	3109.	5776.	1130
3899	10750.	14771.	72422.	79583.	9233.	0.	0,
0.	0.	-	-		<u>^</u>		
0. 56	219	1. 702	2.	4.	8. 1019	3/.	46. 5722
856.	8539.	9246	26850	83286	8. 4019. 119486.	24424. 708	J/22. 0
0.	0.	4.	4.	11.	17. 5262.	14.	20.
23. 5216.	93. 3830.	1048.	2238.	4653.	5262. 79486.	9826.	24736.
91529	0						
0.	0.	8.	6.	20.	28. 11148. 142725.	16.	23.
27.	109.	476.	1024.	2497.	11148.	9730.	20245.
77714. 1818021. 9	765820.	262612.	524192.	713496.	142725.	773884.	1665003.
	0.	5	5. 1090.	13	19	178	219
	1019.	510.	1090.	2522.	19. 2254. 135990 <i>.</i>	7890	10533.
48267.	370900.	155161.	804528.	1197119.	135990.	265587.	2040215.
3539979.10	361091.	-					
0. 46.		4.	4.	11.	16.	30.	39.
<b>TU.</b>	0. 185	217				1911	5 / K I
	0. 185. 26679.	317. 45421	683. 93784	130701	137330	106204	1206559
4610. 2351412. 10		4. 317. 45421.					
4610. 2351412. 10 0.							
4610. 2351412. 10					137332. 30. 0. 198565.		

0. 46. 83510. 7781776		6. 322. 21768.	6. 691. 73783.	16. 1940. 45512.	22. 1080. 395828.	31. 6848. 1156228.	38. 31792. 5822832.
0. 40. 23371. 349209.	0. 162. 47987.	10. 277. 222390.	8. 601. 93214.	23. 0. 73488.	34. 1973. 171388.	25. 2991. 178662.	34. 15791. 598201.
0. 17. 19668. 0.	0. 69. 33274. 0.	6. 344. 82407.	6. 741. 38728.	16. 925. 153958.	22. 3322. 173734.	10. 15194. 178396.	14. 35881. 2242777.
	TION 0.00 0.00 1.00 1.00				0.95 1.00	1.00 1.00	1.00 1.00
1.00 1.00	0.00 0.00 1.00 1.00 0.00 0.05	1.00 1.00	1.00 1.00	0.95 0.70			
1.00 1.00	1.00 1.00	1.00 0.75	0.65 0.45	0.00 0.15			
1.00 1.00	0.00 0.40 1.00 1.00	1.00 0.15	0.00 0.00	0.00 0.00			
	0.00 0.20 0.80 0.90				1.00 1.00	1.00 1.00	1.00 1.00
0.00 0.00	0.00 0.00 0.40 0.80	0.00 0.25	0.60 1.00	1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00
0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.25	0.75 1.00	0.95 0.95	0.90 0.90	0.75 0.50
1.00 1.00	1.00 0.70 1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00	0.80 1.00	1.00 1.00	0.90 0.40
1.00 1.00	1.00 1.00 1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00	1.00 0.80
1.00 1.00	0.15 0.20 1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00
	0.75 0.95 1.00 1.00				1.00 1.00	1.00 1.00	1.00 1.00
0.80 1.00	1.00 1.00 1.00 1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00			
0.90 1.00	1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00			
1.00 1.00	$1.00 \ 1.00$ $1.00 \ 1.00$	1.00 1.00	1.00 0.90	0.95 0.90			
1.00 1.00	1.00 1.00 1.00 1.00	1.00 1.00	1.00 0.50	0.60 0.50			
1.00 1.00	1.00 1.00 1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00	0.75 0.80	1.00 0.95	0.95 0.90
0.00 0.00	0.00 0.00 1.00 1.00	0.00 0.00	0.00 0.25	0.25 0.40	1.00 1.00	0.80 0.95	1.00 1.00
REGION IN	DEX						
3636363636	3636363636363 3636363636363	363636363636	363636363636	3628302717	17		
	3636363636363 3636363636363						
3636363636	36363636363	363636363636	36 7 72828	2850505050	50		
	3636363636363 3636363618:						
	3636361818 3636181818						
3636363636	3636361818	1818181818	18181818184	444443138	9		
	3636363618 363636363636						
3636363636	3636363636	3636363636	363636363636	36363633333	11		
	3636363636363 3636363636363						
	363636363636						
11111	1 1 1 1 1						
	$ \begin{array}{c} 1 & 1 & 1 & 1 & 1 \\ 1 & 1 & 1 & 1 & 1 \end{array} $				-		

$\begin{array}{c}1&1&1&1&1&1&1&1&1\\1&1&1&1&1&1&1&1&1\\1&1&1&1&1&1&1&1&1\\1&1&1&1&1&1&1&1&1\end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$		
1 PASTURE 2 STORED FORAGE 3 GRAINS 4 GRN LEAFY VEGET 5 OTHER FOOD CROP 6 LEGUMES AND SEE 7 ROOTS AND TUBER WATERSHED DEFINITIC 1 SR-89 2 SR-90 3 CS-134 4 CS-137 REGIONAL ECONOMIC D	90. 27 150. 24 150. 24 ABLES 150. 24 S 150. 24 DS 150. 24 S 150. 24 N INITIZ	40.       0.13         40.       0.23         40.       0.002         40.       0.004         40.       0.16         40.       0.004	6 0.0 6 0.0 6 0.0	F AND INGESTION	FACTORS
1 ALA 2 ARIZ 3 ARK 4 CALIF 5 COLO 6 CONN 7 DEL 8 FLA	.354 .040 .516 .104 .483 .041 .330 .144 .522 .048 .160 .294 .534 .042 .375 .080	459. 110. 466. 1022. 211. 1605. 1723. 832.	1824. 682. 2049. 4394. 971. 4980. 3428. 3341.	62000. 74000. 61000. 93000. 83000. 107000. 82000. 80000.	
9 GA 10.IDAHO 11 ILL 12 IND 13 IOWA 14 KANS 15 KY 16 LA 17 MAINE	.363 .060 .279 .144 .806 .044 .713 .079 .938 .060 .917 .035 .571 .112 .354 .074 .079 .260	613. 343. 709. 611. 695. 281. 482. 459. 662.	1885. 1562. 3900. 3283. 3133. 1204. 1838. 3284. 1133.	73000. 61000. 86000. 72000. 73000. 81000. 61000. 61000. 70000.	
18 MD 19 MASS 20 MICH 21 MINN 22 MISS 23 MO 24 MONT 25 NEBR 26 NEV	.429 .216 .136 .249 .313 .247 .597 .223 .470 .054 .703 .102 .657 .030 .962 .031	956. 1349. 658. 516. 403. 322. 61. 318.	4489. 2563. 2187. 2111. 2084. 1647. 563. 1148.	93000. 97000. 81000. 82000. 53000. 76000. 65000. 75000.	
20 NEV 27 N.H. 28 N.J. 29 N.MEX 30 N.Y. 31 N.C. 32 N.DAK 33 OHIO 34 OKLA 35 OREG	.127 .139 .096 .482 .203 .129 .590 .144 .310 .589 .352 .065 .924 .048 .602 .175 .751 .060	63. 518. 1399. 53. 711. 860. 164. 581. 204.	601. 2018. 6477. 1378. 2658. 948. 2686. 1508.	84000. 87000. 102000. 63000. 94000. 68000. 69000. 76000. 67000.	
36 PA 37 R.I. 38 S.C. 39 S.DAK	.292 .111 .303 .447 .108 .213 .290 .084 .915 .091	236. 855. 1062. 472. 145.	1203. 2534. 6438. 1843. 587.	73000. 78000. 80000. 62000. 65000.	

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SECPOP PO 26 SPATI 16 WIND 7 CROP 4 WATER 2 WATER 59 ECONO SPATIAL D	MIC REGIONS	ION FROM 19 S OTOPES	980 CENSUS	DATA ALTEI	RED USING			
0.40		1.21	1.61	2.31	3.22	4.02	4.83	
5.63	8.05	11.27	16.09	20.92	25.75	32.19	40.23	
48.28	64.37	80.47	112.65	160.93	241.14	321.87	563.27	
	1609.34						•	
0.	0. 12. 74.	4.	3.	7.	16.	0.	1.	
2.	12.	30.	70.	0.	0.	67.	1304.	
0.	74.	743.	15484.	83209.	72162.	120923.	541090.	
3057152	9822912.		~	2	0	-	2	
0.	0. 17.	⊥. 45	2. 105	3.	9. 4637	1.	3.	
21111.	2866.	604.	10875.	31683.	110002.	126487.	1603453.	
	24970756.						2000.000	
0.	24970756. 0. 31. 3527.	0.	0.	0.	Ο.	5.	6.	
_ 8.	31.	95.	205.	713.	0.	1658.	4373.	
757.	3527. 21211502.	3814.	12032.	35282.	62550.	1/53/9.	1020222.	
2240248.	21211502. 0. 79. 3387.	0.	0.	1.	4.	11.	16.	
19.	79.	85.	190.	ō.	413.	<u> </u>	853.	
2232.	3387.	49094.	247241.	33956.	99583.	73501.	1699378.	
3029730.	18370806.	_	-					
0. 22.	0. 87.	1. 61. 10673.	120	3.	207	13.	18.	
42. 893	5713.	0⊥. 10673	16982	401. 31249	327. 133852	75589	U. 888587	
1460466.	1943140.	10075.	10902.	54245.	10002.	/5509.	000507.	
0.	1943140. 0.	1. 109. 7940.	Ο.	3.	б.	51.	65.	
77.	307.	109.	241.	0.	751.	63.	0.	
1185.	5028.	7940.	15118.	33308.	130847.	390071.	714008.	
368763. 0.	8028641. 0	1. 1149. 21095.	0	з	6	201	249	
293.	0. 1157.	1149.	2451.	0.	851.	0.	222.	
858.	1203.	21095.	19956.	49172.	94458.	284438.	656.	
0.	754387.			_				
0.	0.	0.	0.	1.	4.	14.	20.	
23. 13.	3396	1567	22369	42828	544166	1430. 811964	11629	
- <u>-</u>	0.	1007.	22305.	12020.	511100.	011904.	11027.	
0.	0.	1.	2.	3.	9.	6.	9.	
12.	48.	128.	282.	0.	0.	1492.	3370.	
0.	1858. 0. 33. 28282. 0.	2341.	9365.	67097.	515206.	208032.	0.	
0.	0.	0	0.	1	. 4	٦	. 6	
8.	33.	101.	224.	ō.	927.	0.	1091.	
65.	28282.	3770.	5243.	35077.	369254.	56437.	0.	
0.	28282. 0. 0. 23126. 639306.	_	-					
• 0.	0.	1.	0.	2.	2.	0.	0.	
0. 0.	23126	79. 3047	4072	U. 41214	100210	217276	1339. 879780	
399582.	639306.	5047.	4072.	11211.	100210.	21/2/0.	079700.	
0.	0.	0.	0.	0.	0.	0.	0.	
0.	0.	63.	137.	1716.	465.	0.	525.	
663.	639306. 0. 1298. 284505	2246.	16476.	123117.	79084.	75399.	2976832.	
2001/41.	284505.	0	0	0	0	0	0	
0.	0.	25	55. 55	0.	0	U. 117	ט. גוג	
<i>0</i> .	0. 0. 5945.	0. 25. 2397.	10843.	28920.	64335.	236712.	2130706.	
1744285.	1801823.							

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0. 2. 0. 1506956.	0. 12. 4689. 2162785.	0. 22. 14121.	0. 53. 53864.	1. 1473. 93558.	4. 87. 102537.	0. 0. 291271.	1. 855. 781001.
0. 0. 0. 1452393.	2102783. 0. 0. 2793. 3444556.	1. 32. 6767.	2. 68. 20193.	3. 0. 50650.	4. 0. 73872.	0. 107. 97972.	0. 0. 481302.
0. 0. 11703. 989294.	0. 0. 2097. 5604039.	7. 24. 2389.	5. 51. 12027.	14. 0. 17138.		0. 0. 248012.	0. 515. 811364.
0.85 0.90	1.00 1.00 0.90 0.95	1.00 1.00 0.95 0.95	1.00 1.00	1.00 0.75			
0.95 0.95 1.00 1.00	1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00	1.00 0.85 1.00 1.00			
1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 0.90	1.00 1.00 1.00 1.00 0.95 1.00	1.00 1.00 1.00 1.00	1.00 1.00 1.00 0.55			
1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00	0.90 0.20 1.00 1.00			
1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 0.20 0.05	1.00 1.00 0.00			
1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00	1.00 1.00 1.00 0.70 1.00 1.00	$0.95 0.00 \\ 1.00 1.00$	0.00 0.00 1.00 1.00			
1.00 1.00 1.00 1.00	1.00 1.00 0.95 0.95	$\begin{array}{c} 1.00 \ 1.00 \\ 1.00 \ 1.00 \\ 1.00 \ 1.00 \\ 1.00 \ 1.00 \end{array}$	1.00 1.00 1.00 0.75	1.00 1.00 0.00 0.10			
0.85 0.85 1.00 1.00	0.95 1.00 1.00 1.00	$\begin{array}{c} 1.00 & 1.00 \\ 1.00 & 1.00 \\ 1.00 & 1.00 \\ 1.00 & 1.00 \end{array}$	$\begin{array}{c} 0.60 & 0.50 \\ 0.85 & 0.60 \end{array}$	0.30 0.85 0.50 0.70			
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NRC FORM 335 (2-89)	U.S. NUCLEAR REGUL	ATORY COMMISSION 1. REPORT NUMBER (Assigned by NRC. Add Vol., Supp., Rev.,
NRCM 1102, 3201, 3202 BIBLIC	OGRAPHIC DATA SHEET See instructions on the reverse)	NUREG/CR-4551
2. TITLE AND SUBTITLE		SAND86-1309
Evaluation of Severe Ac	cident Risks:	Vol. 2, Rev. 1, Part 7
Quantification of Major	Input Parameters	3. DATE REPORT PUBLISHED
"MACCO Incut		December 1990
MACCS Input		4. FIN OR GRANT NUMBER
		A1853
5. AUTHOR(S)		6. TYPE OF REPORT
J.L. Sprung, J.A. Rolls	tin,* J.C. Helton**, H-N Jow	Technical
* GRAM, Inc.		7. PERIOD COVERED (Inclusive Dates)
** Arizona State Univers	ity	
3. PERFORMING ORGANIZATION – NAME A name and mailing address.)	ND ADDRESS (II NRC, provide Division, Office or Region, L	I.S. Nuclear Regulatory Commission, and mailing address; if contractor, provide
Sandia National Laborat	orios	
Albuquerque, NM 87185	JITES	
9. SPONSORING ORGANIZATION - NAME A	ND ADDRESS (If NRC, type "Same as above"; if contractor,	provide NRC Division, Office or Region, U.S. Nuclear Regulatory Commission,
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