

William J. Cahill, Jr.  
Vice President

Consolidated Edison Company of New York, Inc.  
4 Irving Place, New York, N Y 10003  
Telephone (212) 460-3819

November 27, 1979

Re: Indian Point Unit No. 2  
Docket No. 50-247

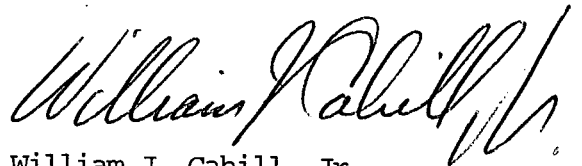
Director of Nuclear Reactor Regulation  
ATTN: Mr. A. Schwencer, Chief  
Operating Reactors Branch No. 1  
Division of Operating Reactors  
U. S. Nuclear Regulatory Commission  
Washington, D. C. 20555

Dear Mr. Schwencer:

Transmitted herewith, as Attachment A to this letter, is a supplemental response to IE Bulletins 79-02 and 79-07.

Should you or your staff have any additional questions, please contact us.

Very truly yours,



William J. Cahill, Jr.  
Vice President

attach.

cc: U. S. Nuclear Regulatory Commission  
Office of Inspection and Enforcement  
Division of Reactor Operations Inspection  
Washington, D. C. 20555

Mr. Boyce H. Grier, Director  
Office of Inspection and Enforcement  
Region I  
U. S. Nuclear Regulatory Commission  
631 Park Avenue  
King of Prussia, Pa 19406

Mr. T. Rebelowski, Resident Inspector  
U. S. Nuclear Regulatory Commission  
P. O. Box 38  
Buchanan, N.Y. 10511

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ATTACHMENT A

Supplemental Response to  
IE Bulletins 79-02 and 79-07

Consolidated Edison Company of New York, Inc.  
Indian Point Unit No. 2  
Docket No. 50-247  
November, 1979

In accordance with IE Bulletin No. 79-07, eight (8) Indian Point Unit No. 2 safety-related pipe lines (i.e., lines nos. 1,2,3,4,63,70,80 and 96) were seismically reanalyzed with the UE&C-ADLPIPE-2 dynamic computer stress analysis code. The results of the reanalyses performed for these lines were provided in the pipe stress summaries forwarded with our previous letters of May 22, 1979, May 25, 1979 and October 23, 1979. Those summaries provided results for the upset stress condition (i.e., deadweight + pressure + OBE) based on the FSAR load combination criteria. This condition was controlling in every case.

Two types of response spectra were developed by Westinghouse for Indian Point Station, one for the OBE (operating basis earthquake) and one for the DBE (design basis earthquake). For the containment structure and inner containment structures, separate response spectra were developed for both the DBE (0.15g normalized Housner type earthquake) and the OBE (0.10g normalized Housner type earthquake). For other structures, response spectra were developed for the DBE. The OBE response spectra values for these other structures are two-thirds of the DBE response spectra values.

The results of the reanalyses performed in response to IE Bulletin No. 79-07 have been considered in evaluating the adequacy of pipe supports using expansion anchor bolts pursuant to IE Bulletin No. 79-02 (as supplemented and revised). As per our previous discussions with the Regulatory Staff, the support loads obtained from the reanalyses were multiplied by a factor of 1.3. Based on these newly calculated support loads, the bolt design loads for the supports affected by the 79-07 reanalyses meet the minimum factor of safety of 5 (for shell type expansion anchors) as required by IE Bulletin No. 79-02 (as supplemented and revised). These results are included in the support load factor of safety distribution provided in our September 17, 1979 response to 79-02.