William J. Cahill, Jr.
Vice President

CENTRAL FILES

Consolidated Edison Company of New York, Inc.
4 Irving Place, New York, N Y 10003
Telephone (212) 460-3819

October 23, 1979

Re: Indian Point Unit No. 2
Docket No. 50-247

Mr. Boyce H. Grier, Director
Office of Inspection and Enforcement
Region I
U. S. Nuclear Regulatory Commission
631 Park Avenue
King of Prussia, PA 19406

Dear Mr. Grier:

Attachment A to this letter provides our supplemental response to IE Bulletin No. 79-07.

Should you or your staff have any questions, please contact us.

Very truly yours,

William J. Cahill, Jr.
Vice President

attach.

cc: Mr. Victor Stello, Jr., Director
Office of Inspection and Enforcement
U. S. Nuclear Regulatory Commission
Washington, D. C. 20555

Mr. Darrell G. Eisenhut, Acting Director
Division of Operating Reactors
U. S. Nuclear Regulatory Commission
Washington, D. C. 20555

Mr. T. Rebelowski, Resident Inspector
U. S. Nuclear Regulatory Commission
P. O. Box 38
Buchanan, N. Y. 10511

A0/I
2

7911270486 CCP

ATTACHMENT A

Supplemental Response to
IE Bulletin No. 79-07

Consolidated Edison Company of New York, Inc.
Indian Point Unit No. 2
Docket No. 50-247
October, 1979

As discussed in our earlier May 22 and 25, 1979 responses to IE Bulletin No. 79-07, eight (8) Indian Point Unit No. 2 lines (i.e., lines nos. 1,2,3,4,63,70,80 and 96) were supported based on dynamic seismic analyses utilizing algebraic summation options for intramodal response combinations. As documented in the above referenced submittals, lines nos. 63,70,80 and 96 were reanalyzed using the UE&C-ADLPIPE-2 dynamic seismic computer code. This code utilizes the worst-case two-dimensional (2-D) evaluation technique and uses the square root of the sum of the squares (SRSS) option for combining both intramodal and intermodal responses.

In accordance with our May 25, 1979 submittal, reanalysis of the remaining four lines (i.e., lines nos. 1,2,3 and 4) utilizing the UE&C-ADLPIPE-2 code was completed prior to the end of the recently completed third refueling/maintenance outage. A pipe stress summary for these reanalyzed lines is presented in Table 1. The summary includes the stress values for the original dynamic analysis and the new analysis. In addition, as requested by the NRC Staff, the new maximum seismic stress calculated from the 2-D SRSS model for these lines has been multiplied by 1.3 and the "adjusted" maximum seismic and total stresses have also been presented in Table 1.

A review of the data contained in Table 1 confirms that the difference between the newly calculated total pipe stress and the originally calculated total pipe stress is not significant. Even after applying the 1.3 "adjustment" factor to the calculated seismic stress component, the total pipe stress remains below the allowable stress limit.

Furthermore, the loads on the pipe supports and equipment nozzles have been re-evaluated on the basis of the confirmatory reanalysis and found to be acceptable.

Also, as committed in our May 25, 1979 submittal, a "walk-through" of all eight (8) lines to re-verify their as-built configurations was conducted during the recently completed third refueling/maintenance outage. This effort was performed as part of the overall safety-related line verification program conducted in response to IE Bulletin No. 79-14 (including revisions and supplements thereto). A complete report of the results of the entire IE Bulletin 79-14 line verification program was provided in our September 28, 1979 submittal. Appendix A of that submittal contains the results of line verification for the eight (8) specific lines addressed above. The new analytical computer models are consistent with the actual field configurations for these eight (8) lines.

This submittal completes our response to IE Bulletin No. 79-07.

Table 1

Indian Point Unit No. 2

Main Steam Atmospheric Relief Lines From
Steam Generators 21, 22, 23, & 24
(Lines Nos. 1, 2, 3, 4)

Pipe Stress (psi) Results Summary
for Upset Condition (OBE)

Analysis	Seismic Stress	Total Stress[1]	Allowable Stress
1. Original (UE&C-ADLPIPE-1)	5,970	11,354	18,000
2. New (UE&C-ADLPIPE-2)	8,688	14,072	18,000
3. New "Adjusted" (1.3 Seismic Adjustment Factor)	11,295	16,679	18,000

Note:
(1) The total combined loading stresses shown are conservatively determined by adding the maximum stress values calculated for each of the loading conditions.