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Russell J. Bell DIRECTOR NEW PLANT LICENSING NUCLEAR GENERATION DIVISION

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Mr. Michael T. Lesar Chief, Rulemaking and Directives Branch (RDB) **Division of Administrative Services** Office of Administration U.S. Nuclear Regulatory Commission Washington, DC 20555-0001

Subject: Industry Comments on Draft Interim Staff Guidance on Ensuring Hazard-Consistent Seismic Input for Site Response and Soil Structure Interaction Analyses (ISG-17), Docket ID NRC-2009-0380

Project Number: 689

The Nuclear Energy Institute (NEI)¹ is pleased to provide the enclosed industry comments on the subject draft Interim Staff Guidance (ISG-17).

As a result of the of the September 25-26, 2008 meeting between the NRC staff and the NEI Seismic Issues Task Force, the industry developed a white paper describing an approach for obtaining siteconsistent seismic input for soil-structure interaction analyses. The draft ISG-17 identifies the industry white paper as one of two acceptable approaches that can be used for this purpose.

We agree with the technical content of the draft ISG-17, and offer the enclosed comments as suggested clarifications for the staff's consideration.

¹ The Nuclear Energy Institute (NEI) is the organization responsible for establishing unified industry policy on matters affecting the nuclear energy industry, including the regulatory aspects of generic operational and technical issues. NEI's members include all entities licensed to operate commercial nuclear power plants in the United States, nuclear plant designers, major architect/engineering firms, fuel fabrication facilities, nuclear materials licensees, and other organizations

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If you have any questions about the industry comments, please contact me or Kimberly Keithline (202-739-8121; kak@nei.org).

Sincerely,

RASSE

Russell J. Bell

Enclosure

c: Dr. Nilesh Chocksi, U.S. Nuclear Regulatory Commission Mr. William Burton, U.S. Nuclear Regulatory Commission NRC Document Control Desk

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Industry Comments on ISG-17, Ensuring Hazard-Consistent Seismic Input for Site Response and Soil Structure Interaction Analyses (September 24, 2009)

ISG Section/ Paragraph/Sentence	Comment +	Proposed Resolution
Page 3, soil column, 2 nd	This section states that soil column properties,	The best estimate soil property should be
sentence	best estimate, and upper bound and lower	obtained from the interpolation of the median
	bound values of each layer are obtained from	strain-compatible soil properties corresponding
	the soil response motion at the MAPE of 10 ⁻¹ .	to the soil column analyses using 10 ⁻¹ and 10 ⁻⁵
	In the previous section under Site Response	MAPES rock motions. The upper bound and
	using the soil column responses at 10 ⁻⁴ and 10 ⁻⁵	from the variation of the strain-compatible soil
	are described. To be consistent with the design	properties from the median profile Typically
	motion, the soil column properties should also be	one standard deviation is used to define the
	obtained from interpolation of strain-compatible	upper and lower bound values.
	soil properties corresponding to 10 ⁻⁴ and 10 ⁻⁵	
	MAPEs.	
Section 1, page 1, middle of	"Section 3.3" should be changed to "Section	Change "Section 3.3" to "Section 5.0."
paragraph	5.0."	
Section 3, page 4, item 1	Hard rock and 9200 ft/sec is applicable to CEUS	Change to "Rock UHS is calculated at the rock
	sites only and not for all sites. In addition this	horizon under the geologic outcrop condition."
	definition is likely to change for CEUS sites when	
	NGA East is completed.	
Section 5.2.1, fist sentence, page 7	Same as the item above	Change "hard rock" to "rock."

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Industry Comments on ISG-17, Ensuring Hazard-Consistent Seismic Input for Site Response and Soil Structure Interaction Analyses (September 24, 2009)

ISG Section/ Paragraph/Septence	Comment	Proposed Resolution
Section 5.2.1, footnote 2	The PSHA analysis provides various statistical measures of the annual probability of exceedance as a function of rock spectral accelerations. Regulatory Guide 1.208 specifies that the mean annual probability of exceedance [MAPE] be used in developing the rock motions. In site response analysis, it is assumed that the soil amplification and soil response motions in terms of acceleration response spectra are log-normally distributed, consistent with the definition of the rock ground motion attenuation relations used in the PSHA commonly being defined as median ground motions. With this assumption, the mean of the logarithmic values are used, which amounts to median values of the soil response motion.	Remove foot note number 2.
Paragraph 3 on page 2, Effect of Overburden in the Soil Profile Properties.	Paragraph 3 on page 2 requires that, in computing the GMRS at the uppermost in situ competent layer, one needs to capture the effect of soil overburden on confining pressures. The paragraph does not specifically state that the "dynamic" effect of the soil overburden should also be captured in computing the GMRS. In Section 3.1.2 of the NEI paper (ISG-17 Reference 3), an approach is proposed to include the effects of the overburden soil both in terms of the confining pressure and the dynamic effect in computing the response of the truncated soil columns.	In paragraph 3 of page 2, change the statement "However, the calculation needs to capture the effect of the weight of the soil overburden in producing confinement" to: "However, the calculation needs to capture the effect of the weight of the soil overburden in producing confinement and includes the effects of the soil column frequency of the overburden soil."