### 2.3 METEOROLOGY

This section of the U.S. EPR FSAR is incorporated by reference with the following departures and supplements.

The U.S. EPR FSAR includes the following COL Item in Section 2.3.1:
If a COL applicant that references the U.S. EPR design certification identifies site-specific meteorology values outside the range of the design parameters in Table 2.1-1, then the COL applicant will demonstrate the acceptability of the site-specific values in the appropriate sections of the Combined License application.

This COL Item is addressed as follows:
\{The CCNPP Unit 3 site-specific meteorology values have been reviewed and compared to determine if they are within the bounds of the assumed meteorology values for a U.S. EPR. This comparison is provided in Table 2.0-1. The CCNPP Unit 3 site-specific meteorology parameters are within the bounds of the conservative limiting meteorology values presented in Table 2.0-1.\}

### 2.3.1 REGIONAL CLIMATOLOGY

No departures or supplements.

### 2.3.1.1 Basis for Meteorological Parameters

The U.S. EPR FSAR includes the following COL Item in Section 2.3.1.1:
A COL applicant that references the U.S. EPR design certification will provide site-specific characteristics for regional climatology.

This COL Item is addressed as follows:
\{Calvert Cliffs Nuclear Power Plant (CCNPP) is located in Calvert County, Maryland. According to information from the Office of the Maryland State Climatologist (OMSC, 2007), Calvert County is in that portion of Maryland commonly referred to as Southern Maryland, and is located on the Coastal Plain. The weather data periods used to create this narrative is identified in each subsection. The CCNPP site is located in the 18-03 state climatic division where 18 stands for the State of Maryland and 03 indicates the third division in the state.

Seasons are well defined. Winter is the dormant season for plant growth due to low temperatures rather than drought. Spring and fall are characterized by a rapid succession of warm and cold fronts associated with storm systems that generally move from a westerly direction. Summers are warm to hot. The higher humidity along the Atlantic coast causes the summer heat to feel more oppressive and the winter cold to feel more penetrating than for drier climates.

At times the Appalachian Mountains provide some protection from arctic air outbreaks in the winter. The mountain barrier may cause warming of the air descending the eastern slopes by as much as $10^{\circ} \mathrm{F}\left(5.6^{\circ} \mathrm{C}\right)$. In situations when high pressure is located over New England and a low pressure system is over the Ohio Valley, cold low-level winds may travel southwestward and be held east of the mountains.

## Winds

The prevailing winds at the surface are determined by the frequency and intensity of anticyclones and cyclones that persist or move over the area. The majority of anticyclonic circulation over the northern portion of North America in winter brings a high percentage of cold northwesterly winds to Maryland. Therefore, the prevailing winds are from the northwesterly quadrant from October through June. In the summer this pattern changes as the semi-permanent Atlantic High moves northwestward and dominates the circulation of air over the eastern U.S. A flow of warm, moist air spreads over the area with winds from the southwesterly quadrant most of the time. During the summer the northern portion of North America is dominated by low pressure and the mean storm track is displaced north of Maryland.

Surface mean wind speeds range from 9 to $10 \mathrm{mph}(4.1$ to $4.5 \mathrm{~m} / \mathrm{sec}$ ) in summer to 10 to 12 $\mathrm{mph}(4.5$ to $5.4 \mathrm{~m} / \mathrm{sec}$ ) in winter and early spring. The highest mean wind speeds are associated with the frequent passages of well-developed cyclones and anticyclones in the early spring.

## Storm Tracks

Almost all migrating cyclones and anticyclones cross the U.S. from west to east. The greater numbers of cyclones travel in a northeastward direction in a path about 300 to 500 mi ( 483 to 805 km ) north of Maryland. Storms that originate in the Gulf of Mexico, the southeastern U.S. or adjacent Atlantic coastal regions, frequently move northeastward or northward along the Atlantic Coast and can bring violent, destructive weather to the Maryland region. As these storms, commonly referred to as Nor'easters, approach from the south, strong easterly to northeasterly winds bring widespread rains and cause higher than normal tides along the Atlantic Coast and on the west side of the Chesapeake Bay. Tropical cyclones or hurricanes that develop in the West Indies, the Caribbean, or the Gulf of Mexico sometimes move into, but rarely pass entirely over the State. These systems also cause cloudy weather, heavy rains, and high tides.

## Temperatures

Mean annual temperatures range from $48^{\circ} \mathrm{F}\left(8.9^{\circ} \mathrm{C}\right)$ in Northern Maryland to $58^{\circ} \mathrm{F}\left(14.4^{\circ} \mathrm{C}\right)$ in the lower Chesapeake Bay area. The winter climate on the Coastal Plain of Maryland is intermediate between the cold of the northeast and the mild weather of the South. The average frost penetration is about 5 in ( 13 mm ) in extreme Southern Maryland; in extremely cold winters, maximum frost penetration may be double the average depth. Summer is characterized by considerable warm weather with at least several hot, humid periods. Nights are usually comfortable.

On average, temperatures of $90^{\circ} \mathrm{F}\left(32.2^{\circ} \mathrm{C}\right)$ or higher occur 15 to 25 days per year along the shores of the Chesapeake Bay. The average number of days per year with minimum temperature of $32^{\circ} \mathrm{F}\left(0^{\circ} \mathrm{C}\right)$ or lower is about 80 along the shores of the southern Chesapeake Bay area. Average relative humidity is lower in the winter and early spring, from February through April, and highest in the late summer and early fall, from August to October.

## Precipitation

The most favorable situation for rain is when there is a well-developed high pressure system over New England or the St. Lawrence Valley and a well-developed low pressure system over Georgia, Tennessee or the Ohio Valley. The reverse of this situation usually produces clear, dry weather.

Annual average precipitation is about 40 to 46 in ( 1,016 to $1,168 \mathrm{~mm}$ ). Distribution is generally uniform throughout the year. Although, for example, the heaviest precipitation occurs in the summer, this is the season when severe droughts are most frequent. Summer precipitation is less dependable and more variable than in winter. Annual precipitation deficits of over 16 inches ( 406 mm ) occurred during extreme droughts of the 1930s, 1960s, and in the 1998 to 2002 period.

Annual average snowfall along the coast ranges from 8 to 10 in ( 203 to 254 mm ). Annual snowfall totals vary considerably from one year to another. Ice and hail are infrequent; five ice storms were reported between January 14, 1999, and December 31, 2006 and twenty hail events were reported in Calvert County, Maryland, between October 9, 1962, and December 31, 2006 (NOAA, 2007a). $\}$

### 2.3.1.2 Meteorological Data for Evaluating the Ultimate Heat Sink

The U.S. EPR FSAR includes the following COL Item in Section 2.3.1.2:
A COL applicant that references the U.S. EPR design certification will describe the means for providing UHS makeup sufficient to meet the maximum evaporative and drift water loss after 72 hours through the remainder of the 30 day period consistent with RG 1.27.

This COL Item is addressed as follows:
\{This COL item is addressed in Section 2.3.1.2.2.13.
Sections 2.3.1.2.1 and 2.3.1.2.2 are added as a supplement to the U.S. EPR FSAR.

### 2.3.1.2.1 Regional Air Quality

## Background

The Clean Air Act (PL, 1977) which was last amended in 1990, requires the U.S. Environmental Protection Agency (EPA) to set National Ambient Air Quality Standards (CFR , 2007a) for pollutants considered harmful to public health and the environment. The Clean Air Act established two types of national air quality standards. Primary standards set limits to protect public health, including the health of "sensitive" populations such as asthmatics, children, and the elderly. Secondary standards set limits to protect public welfare, including protection against decreased visibility, damage to animals, crops, vegetation, and buildings.

The EPA Office of Air Quality Planning and Standards (OAQPS) has set National Ambient Air Quality Standards for six principal pollutants, which are called "criteria" pollutants. Units of measure for the standards are parts per million (ppm) by volume, milligrams per cubic meter of air $\left(\mathrm{mg} / \mathrm{m}^{3}\right)$, and micrograms per cubic meter of air $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$. Areas are either in attainment of the air quality standards or in nonattainment. Attainment means that the air quality is better than the standard.

## Calvert County

Based on EPA data, Calvert County, Maryland, is in attainment for all the National Ambient Air Quality Standards (NAAQS) except for the 8 hour ozone standard (EPA, 2007a) as of December 5,2006 . The 8 hour ozone standard is 0.08 ppm and attainment is determined by whether the 3 year average of the fourth-highest daily maximum 8 hour average ozone concentrations measured at each monitor within an area over each year exceeds the standard. From Figure 2.3-13, it can be seen that the fourth-highest 8 hour average ozone concentration for

Calvert County during 2006 is greater than 0.08 ppm and less than or equal to 1.0 ppm . Nonattainment of the 8 hour ozone standard is due to its proximity to Washington, D.C. A nonattainment designation requires a state plan to be sent to the EPA describing how the area will implement air quality improvements. The NAAQS are presented in Table 2.3-1 (EPA, 2007b). Note that the Maryland Department of the Environment reported that ground-level ozone levels have continued to show significant improvements since the early 1990's (MDE, 2007).

Calvert County is part of the Southern Maryland Intrastate Air Quality Control Region (AQCR), as designated in 40 CFR 81.156, Southern Maryland Intrastate Air Quality Control Region, (CFR, 2007b). The attainment status of the Southern Maryland Intrastate AQCR with regard to national ambient air quality standards is listed as being better than national standards for total suspended particulates, sulphur dioxide, and nitrogen dioxide, and unclassifiable/attainment for carbon monoxide, PM-2.5 (particulate matter with diameter less than 2.5 microns), and for the 8 hour ozone standard (CFR, 2007c).

## Class 1 Federal Lands

Class 1 federal lands include areas such as national parks, national wilderness areas, and national monuments. These areas are granted special air quality protections under Section 162 (a) of the federal Clean Air Act. 40 CFR Section 51.307 requires the operator of any new major stationary source or major modification located within $62 \mathrm{mi}(100 \mathrm{~km})$ of a Class I area to contact the Federal Land Managers for that area.

The closest Class 1 Federal Lands to the CCNPP site are Shenandoah National Park and the Fish and Wildlife Service Brigantine site in New Jersey. The distance from the CCNPP site to Shenandoah National Park, Virginia, is approximately $87 \mathrm{mi}(140 \mathrm{~km})$. The distance from the CCNPP site to the Fish and Wildlife Service Brigantine site in New Jersey is approximately 112 mi (180 km).

### 2.3.1.2.2 Severe Weather Phenomena

### 2.3.1.2.2.1 Tornadoes and Waterspouts

Tornadoes occur infrequently in Maryland compared with areas such as the Great Plains. Of the ones that do occur, most are small and result in nominal losses. However, two strong tornadoes hit Central and Southern Maryland within an 8 month period in 2001 to 2002. About $25 \%$ of the total number of tornadoes in Maryland occur in Southern Maryland. Approximately 70\% of the tornadoes occur between 2:00 PM and 9:00 PM with most occurring from 3:00 PM to 6:00 PM. As can be seen in Figure 2.3-8 and Figure 2.3-10 (NOAA, 2000), the annual average number of tornadoes and strong-violent tornadoes (F2 to F5) during the period 1950 to 1995 are four and one, respectively. No waterspouts were reported in Calvert County between January 1, 1950, and October 31, 2006.

In the period from January 1, 1950 through December 31, 2006, 12 tornados were reported in Calvert County (NOAA, 2007a). This corresponds to an annual average of 0.2 tornados per year. The magnitude of the tornados ranged from F0 to F2, as designated by the National Weather Service. An F0 tornado has estimated wind speeds less than $73 \mathrm{mph}(33 \mathrm{~m} / \mathrm{sec}$ ). An F1 tornado has estimated wind speeds between 73 and 112 mph ( 33 and $50 \mathrm{~m} / \mathrm{sec}$ ). An F2 tornado has estimated wind speeds between 113 and 157 mph ( 50 and $70 \mathrm{~m} / \mathrm{sec}$ ). The widths of the paths of the 12 tornados in Calvert Count were estimated to range from 17 to 200 yards ( 16 to 183 m ).

In a study reported in the Journal of Weather and Forecasting of the American Meteorological Society (AMS, 2003), an estimate was made of the probability of an occurrence of a tornado day near any location in the contiguous U.S. for any time during the year. The study applied

Gaussian smoothers in space and time to the observed tornado days from 1980 to 1999 to produce daily maps and annual cycles at any point on a 50 mi by $50 \mathrm{mi}(80 \mathrm{~km}$ by 80 km$)$ grid. Figure 2.3-11 shows the date of maximum tornado threat for locations meeting the minimum data requirements of the study (the gray shaded areas). Areas with a white background signify that there was not enough information to predict the maximum tornado threat date, not that a tornado would not or could not occur. Late July is indicated as the date of maximum tornado threat for the part of Maryland that includes CCNPP Unit 3.

### 2.3.1.2.2.2 Hurricanes

Hurricanes sometimes move into but rarely pass entirely over the CCNPP Unit 3 area. National Hurricane Center statistics (NOAA, 2005) list only two direct hits on Maryland during the period from 1851 to 2004; neither of these was a major (greater than Category 2) hurricane. Note that the Saffir-Simpson Hurricane Scale ranks hurricanes on a scale of 1 to 5 based on the intensity of the storm (NOAA, 2007b). In the eastern U.S., hurricane season begins June $1^{\text {st }}$ and ends November $30^{\text {th }}$.

Table 2.3-2 shows the total and average number of tropical storms and hurricanes, by month, in the U.S., for the period 1851 to 2004 (NOAA, 2005). Note that most tropical storms and hurricanes occur in September.

The National Oceanic and Atmospheric Administration (NOAA) Coastal Services Center reports that there were 9642 tropical storms and hurricanes that passed within 100 nautical miles ( 185161 km) of Calvert County, Maryland, during the period from 1851 through 20056. Of these 9642 events, eightthree were Category 1 hurricanes, 2 hurricanes, and one was a Category 3 hurricane (NOAA, 2007c). The hurricanes occurred in the months of August, September, and October. The tropical storms occurred in the months of July, August, September, and October. -n addition to the hurricanes and tropical storms, therewere 41 extratropical storms, 33 tropicaldepressions, and four subtropical depressions that passed within 100 nautical miles ( 185 km ) of Calvert County, Maryland, during the period from 1851 through 2005.

Precipitation estimates from the remnants of Tropical Storm Ernesto, Bill, and Allison were presented in FSAR Section 2.3.1.2.2.2. These data were obtained from the National Climatic Data Center Storm Events database (NOAA, 2007a), under precipitation events in Calvert County for dates June 15, 2001 (Allison), July 3, 2003 (Bill), and September 1, 2006 (Ernesto).

Rainfall amounts for Calvert County, Maryland, were not included in the National Climatic Data Center Storm Events database for the remnants of Hurricane Floyd and were therefore unavailable for inclusion in the FSAR.

On September 1, 2006, the remnants of Tropical Storm Ernesto dropped between 7 to 10 in ( 178 to 254 mm ) of rain in Calvert County. On July 3, 2003, the remnants of Tropical Storm Bill dropped over 2 in ( 51 mm ) of rain in parts of Calvert County. On June 15, 2001, the remnants of Tropical Storm Allison dropped between one and one-half and three and one-half inches (38 to 89 mm ) of rain on Calvert County (NOAA, 2007a).

### 2.3.1.2.2.3 Thunderstorms

Thunderstorms are reported at any given station in the vicinity of Calvert County on an average of 30 to 40 days per year. They occur in all months of the year, but the majority ( $75 \%$ to $80 \%$ ) occurs in May through August. They occur less than once per month from November to

February. Thunderstorms are most likely to occur during the afternoon and evening hours. (NOAA, 2007e).

Table 2.3-3 presents the monthly mean number of days on which thunderstorms occurred in the region during the period from 1971 to 2002. The information is from certified data from the National Climatic Data Center (NOAA, 2002a) (NOAA, 2002b) (NOAA, 2002c).

### 2.3.1.2.2.4 Lightning

J. L. Marshall (Marshall, 1973) presented a methodology for estimating lightning strike frequencies which includes consideration of the attractive area of structures. His method consists of determining the number of lightning flashes to earth per year per square kilometer and then defining an area over which the structure can be expected to attract a lightning strike. There are 4 flashes to earth per year per square kilometer in the vicinity of the proposed CCNPP Unit 3 (conservatively estimated using Figure 2.3-12 (NOAA, 2007d). Marshall (Marshall, 1973) defines the total attractive area, $A$, of a structure with length $L$, width $W$, and height $H$, for lightning flashes with a current magnitude of $50 \%$ of all lightning flashes as:

$$
\mathrm{A}=\mathrm{LW}+4 \mathrm{H}(\mathrm{~L}+\mathrm{W})+12 \cdot 57 \mathrm{H}^{2} \quad \text { Eq. 2.3.1-1 }
$$

The following building dimensions were used to estimate conservatively the attractive area of CCNPP Unit 3 (these values are larger than the approximate dimensions of the combined containment, the four safeguards buildings, the access building, the fuel building, and the nuclear auxiliary building):

$$
L=215 \mathrm{~m}, \mathrm{~W}=140 \mathrm{~m}, \mathrm{H}=40 \mathrm{~m}
$$

The total attractive area is therefore equal to 0.11 square kilometers. Consequently, the lightning strike frequency computed using Marshall's (Marshall, 1973) methodology for CCNPP Unit 3 is 0.44 flashes per year.

### 2.3.1.2.2.5 Droughts

Droughts in Calvert County occur most frequently during the summer season based on data from the National Climatic Data Center. Annual precipitation deficits of over 16 in ( 406.4 mm ) occurred during extreme droughts of the 1930s, 1960s, and in the 1998 to 2002 period (NOAA, 2007ae).

### 2.3.1.2.2.6 High Winds

Table 2.3-4 presents occurrences of winds greater than 50 knots ( 58 mph or $26 \mathrm{~m} / \mathrm{sec}$ ) by storm type for Calvert County. These data were retrieved from the National Climatic Data Center (NOAA, 2007a). There were 17 events that occurred during the period from June 2, 1980, through December 31, 2006, with the wind speed ranging from 50 to 90 knots ( 58 to 104 mph ; 26 to $46 \mathrm{~m} / \mathrm{sec}$ ). The highest value occurred on April 21, 2000.

### 2.3.1.2.2.7 Hail

Table 2.3-5 presents twenty hail events which occurred in Calvert County, Maryland, between October 9, 1962, and December 31, 2006. These data were retrieved from the National Climatic Data Center (NOAA, 2007a). Hail stone diameters ranged from 0.75 to 2 in (19.1 to 50.8 mm ). The largest value occurred on July 15, 1996.

### 2.3.1.2.2.8 Dust/Sand Storms

There were no dust/sand storms reported in Calvert County, Maryland, between January 1, 1993, and December 31, 2006. These data were retrieved from the National Climatic Data Center (NOAA, 2007a).

### 2.3.1.2.2.9 Ice Storms

Table 2.3-6 presents five ice storm events which occurred in Calvert County, Maryland, between January 14, 1999, and December 31, 2006. These data were retrieved from the National Climatic Data Center (NOAA, 2007a). Ice thickness ranged from 0.2 to 1 in ( 5.1 to 25.4 mm ). The largest value occurred on January 30, 2000.

### 2.3.1.2.2.10 Snow Storms

Table 2.3-7 presents snow storm events which occurred in Calvert County, Maryland, between December 28, 1993, and December 31, 2006. These data were retrieved from the National Climatic Data Center (NOAA, 2007a). Snow amounts ranged from 1.0 to 16.5 in ( 25.4 to 419.1 mm ).

### 2.3.1.2.2.11 High Air Pollution Potential

It has been observed that major air pollution episodes are usually related to the presence of stagnating anticyclones. Such anticyclones may linger over an area four days or more. During such a period, surface wind speeds can fall to very low values. The near surface circulation is therefore insufficient to disperse accumulated pollutants. These air stagnation events were analyzed in "Air Stagnation Climatology for the U.S. (1948-1998)," (NOAA, 1999). It was determined that 12 air stagnation days occur per year, on average for the period 1948 to 1998, in the vicinity of CCNPP Unit 3 site. The maximum number of air stagnation days (averaged over the same period), around 80 per year, occurs near the border of California, Arizona, and Mexico. Most air stagnation events happen in an extended summer season from May to October as a result of weaker pressure and temperature gradients and the concomitant weaker wind circulations. The study found that the eastern U.S. has a prolonged but weaker air stagnation season than the rest of the country.

Air flow from over warm waters tends to inhibit temperature inversion formation at night along the immediate coast (Hosler, 1961). During the warmer months of the year, the pressure gradient reinforces the sea breeze circulation, which results in the production of relatively strong winds during nights along the coast. This helps to delay or even inhibit nocturnal radiation inversion formation.

A study (EPA, 1972) which derived climatological statistics on morning and afternoon mixing heights and associated vertically averaged wind speeds, indicates that the mean annual morning mixing height depth over CCNPP Unit 3 will be approximately $1,968 \mathrm{ft}(600 \mathrm{~m}$ ) and that the mean annual afternoon mixing height depth over CCNPP Unit 3 will be approximately $4,592 \mathrm{ft}(1,400 \mathrm{~m})$. The mean annual wind speed through the morning mixing layer was found to be approximately $12 \mathrm{mi} / \mathrm{hr}(5.5 \mathrm{~m} / \mathrm{sec})$ and the mean annual wind speed through the afternoon mixing layer was found to be approximately $15.7 \mathrm{mi} / \mathrm{hr}(7.0 \mathrm{~m} / \mathrm{sec})$.

### 2.3.1.2.2.12 Snow/Ice Load on Roofs of Safety Related Structures

The NRC Branch Position for Winter Precipitation Loads (NRC, 1975) establishes an acceptable method to develop a winter precipitation load for the design of nuclear power plants. The prescribed loads to be included in the combination of normal live loads are based on the weight of the 100 year snow pack or snowfall, whichever is greater, recorded at ground level.

Winter precipitation loads to be included in the combination of extreme live loads is based on the addition of the weight of the 100 year snow pack at ground level plus the weight of the 48 hour Probable Maximum Winter Precipitation (PMWP) at ground level for the month corresponding to the selected snow pack. Snow pack and snowfall are adjusted for density differences and ground level values are adjusted to represent appropriate weights on roofs. Values are expressed in the units used in the methodology.

As indicated in the NRC Branch Position for Winter Precipitation Loads (NRC, 1975), it is acceptable to determine the 100 year snow pack and snowfall utilizing information in American National Standards Institute (ANSI) A58.1,"Minimum Design Loads for Buildings and Other Structures" (ANSI, 1972) with an adjustment of 30 years or more of regional data and maximization of water content for snow depth. Based on more recent information (ASCE, 19982006) issued 2633 years since ANSI A58.1, the 50 year mean recurrence ground snow load in the CCNPP Unit 3 region is $25 \mathrm{lb} / \mathrm{ft}^{2}\left(122 \mathrm{~kg} / \mathrm{m}^{2}\right)$. The ANSI importance factor described in ASCE-7-98/SEI 7-05, "Minimum Design Loads for Buildings and Other Structures," (ASCE, 19982006) can be used to adjust the 50 year recurrence ground snow load to a 100 year recurrence. Using an importance factor of 1.2, the 100 year mean recurrence ground snow load is $30 \mathrm{lb} / \mathrm{ft}^{2}\left(146 \mathrm{~kg} / \mathrm{m}^{2}\right)$.

The 48 hour PMWP can be determined from Hydrometeorological Report (HMR) Number 3353 (USWB, 195680) by taking the probable maximum 48 hour precipitation during the winter months of December through February. The $10 \mathrm{mi}^{2}\left(26 \mathrm{~km}^{2}\right)$, 48 hour PMWP is conservatively selected for the site. The $200 \mathrm{mi}^{2}\left(518 \mathrm{~km}^{2}\right)$, 24 hour PMAWP is obtained directly from HMR Number 33 (USWB, 1956). The factors to adjust the $200 \mathrm{mi}^{2}\left(518 \mathrm{~km}^{2}\right), 24$ hour PMWP to a $10 \mathrm{mi}^{2}\left(26 \mathrm{~km}^{2}\right), 48$ hour PMWP are also provided in HMAR Number 33 (USWB, 1956). The PMWP is summarized in Table 2.3-8 (USWB, 1956)plotting (using a smooth curve) the probable maximum 6-hour, 24-hour, and 72-hour precipitation during the winter months of December through February. The 6-hour, 24-hour, and 72-hour PMWP values are provided in Table 2.3-8.

The plot of the probable maximum 6-hour, 24 -hour, and 72-hour precipitation is presented in Figure 2.3-222. The 10 -square mile ( $\mathrm{mi}^{2}$ ), 48 -hour PMWP is selected for the site from the plot using the December data since it is more conservative; the value of the 48 -hour PMWP is 22.5 inches ( 571.5 mm ).

The month of December provides the most conservative PMWP of 17.7 in ( 450 mm ). Note that the average total precipitation for December is 2.61 in ( 66.3 mm ) in the CCNPP site area. Considering that hourly temperature values measured in the CCNPP site area during the six-year period from 2000 to 2005 were below $32^{\circ} \mathrm{F}\left(0^{\circ} \mathrm{C}\right)$ about $10 \%$ of the time, most of this PMWP would occur as rain. In order to define the overall ground snow load, it was assumed that $25 \%$ of the PMWP combines with the 100 year mean recurrence ground snow load of $30 \mathrm{lb} / \mathrm{ft}^{2}\left(146 \mathrm{~kg} / \mathrm{m}^{2}\right)$. Therefore, the PMWP component is (where $62.4 \mathrm{lb} / \mathrm{ft}^{2}\left(305 \mathrm{~kg} / \mathrm{m}^{2}\right)$ is the density of water):

PMWP Load $=\left[(17.722 .5\right.$ inches $)\left(62.4 \mathrm{lb} / \mathrm{ft}^{2}\right) /(12$ inches $\left.)\right](0.25)=2329 \mathrm{lb} / \mathrm{ft}^{2}$
Eq. 2.3.1-3
( $112141 \mathrm{~kg} / \mathrm{m}^{2}$ )
Combining the 100 year mean recurrence ground snow load of $30 \mathrm{lb} / \mathrm{ft}^{2}\left(146 \mathrm{~kg} / \mathrm{m}^{2}\right)$ with the PMWP load of $2329 \mathrm{lb} / \mathrm{ft}^{2}\left(112141 \mathrm{~kg} / \mathrm{m}^{2}\right)$ yields an overall design ground snow load of 5359 $\mathrm{lb} / \mathrm{ft}^{2}\left(258288 \mathrm{~kg} / \mathrm{m}^{2}\right)$ for use in the design of roofs. This site-specific overall design ground snow load is bounded by the U.S. EPR design value.

### 2.3.1.2.2.13 Conditions for Maximum Evaporation and Potential Water Freezing in the Ultimate Heat Sink

In accordance with NRC Regulatory Guide 1.27, "Ulimate Heat Sink for Nuclear Power Plants," (NRC, 1976), the meteorological conditions resulting in maximum evaporation and drift lossshould be the worst 30 day average combination of controlling parameters (wet bulb and dry bulb temperatures). Monthly design wet bulb and meancoincident dry bulb temperatures were determined by the American Society of Heating, Refrigeration, and Air Conditioning Engineers (ASHRAE) using 20 years (1982 to 2001) of meteorological data from Patuxent River Naval Air Station (NAS), Maryland, a nearby representative site (ASHRAE, 2005). These 20 years of data were used instead of 30 years of data from another site because Patuxent River NAS is the closest source of atmospheric moisture data to the CCNPP site and is logated on the shores of the Chesapeake Bay, as is CCNPP Unit 3. The highest monthly design wet bulb and mean eoincident dry bulb temperatures reported were for the month of July. The $2 \%$ design values (the values that would be exceeded $2 \%$ of the time in the month of July or roughly 15 hours out of 744 ) are $79.6^{\circ} \mathrm{F}\left(26.4^{\circ} \mathrm{C}\right)$ and $89.2^{\circ} \mathrm{F}\left(31.8^{\circ} \mathrm{C}\right)$ for the wet and coincident dry bulbtemperatures, respectively. The $1.0 \%$ design values for the month of July are $80.3^{\circ} \mathrm{F}\left(26.8^{\circ} \mathrm{C}\right)$ and $89.9^{\circ} \mathrm{F}\left(32.2^{\circ} \mathrm{C}\right)$ for the wet and coincident dry bulb temperatures, respectively. The $0.4 \%$ design values for the month of July are $81.3^{\circ} \mathrm{F}\left(27.4^{\circ} \mathrm{C}\right)$ and $90.8^{\circ} \mathrm{F}\left(32.7^{\circ} \mathrm{C}\right)$ for the wet and coincident dry bulb temperatures, respectively.

Since a closed loop hybrid mechanical draft cooling tower will act as the heat sink for CCNPP Unit 3, another meteorological condition to consider is the maximum 1 hour dry bulbtemperatures. The maximum 1 hour dry bulb temperature determined for Baltimore, Aaryland, in Local Climatological Data, 2002 Annual Summary with Comparative Data, (NOAA, 2002a) is $105^{\circ} \mathrm{F}\left(10.6^{\circ} \mathrm{C}\right)$. This value was determine d over a 52 year period of record (1951 to z002).

The meteorologicalconditions resulting in minimum cooling due to evaporation of water should be periods of high wet bulb temperature values. Using 20 years (1982-2001) of meteorological data from Patuxent River NAS, Maryland, the wet bulb temperatures that areexceeded only $2 \%, 1 \%$, and $0.4 \%$ of the time per year are $76.5^{\circ} \mathrm{F}\left(24.7^{\circ} \mathrm{C}\right), 77.8^{\circ} \mathrm{F}\left(25.4^{\circ} \mathrm{C}\right)$, and $79.2^{\circ} \mathrm{F}\left(26.2^{\circ} \mathrm{C}\right)$, respectively (ASHRAE, 2005).

The meteorological conditions resulting in the potential for water freezing in the ultimate heat sink water storage facility should be low dry bulb temperature values and associated wind speeds. Using 20 years of meteorological data from Patuxent River NAS, Maryland, the coldest month wind speed and coincident dry bulb temperature that are exceeded only $1 \%$ of the timeper year are $24.2 \mathrm{mi} / \mathrm{hr}(10.8 \mathrm{~m} / \mathrm{sec})$ and $31.8^{\circ} \mathrm{F}\left(-0.1^{\circ} \mathrm{C}\right)$.

According to information from ASHRAE (ASHRAE, 2005), the 100-year return period values of maximum and minimum dry bulb temperature are $104.6^{\circ} \mathrm{F}\left(40.33^{\circ} \mathrm{C}\right)$ and $-9.1^{\circ} \mathrm{F}\left(-22.8^{\circ} \mathrm{C}\right)$, respectively. The 100 year return period value of maximum wet bulb temperature coincident with the 100 year return period value of maximum dry bulb temperature is $86.1^{\circ} \mathrm{F}\left(30.06^{\circ} \mathrm{C}\right)$.The 100 year return period value of maximum wet bulb temperature (non-coincident) is $94.8^{\circ} \mathrm{F}$ (34.9 ${ }^{\circ} \mathrm{C}$ ).

In accordance with Regulatory Guide 1.27, "Ultimate Heat Sink for Nuclear Power Plants," (NRC, 1976), the meteorological conditions resulting in maximum evaporation and drift loss should be the worst 30-day average combination of controlling parameters (wet bulb and dry bulb temperatures). The design of the UHS, as stated in the U.S. EPR FSAR Section 2.3.1.2, is based on meteorological conditions that exist for 72 hours, consistent with the sizing of the UHS cooling
tower basin. For CCNPP3, the worst meteorological conditions resulting in maximum evaporation and drift loss of water for the UHS over a 72 hour period are shown in Table 2.0-3.

A software routine used in the Ultimate Heat Sink analysis calculation evaluated 30 years of meteorological data (Reference 1) for Patuxent River Naval Air Station (11 miles away from the CCNPP site) and determined the worst 72 hour period from the perspective of maximum evaporation (highest evaporation potential, based on the combined effect of the dry bulb temperature and its coincident wet bulb temperature). These ambient temperature conditions are imposed on the cooling tower model for the first 72 hours of the design basis accident (DBA).

The table below provides a comparison of the Table 2.1-3 values in the U.S. EPR FSAR and the CCNPP site-specific values used for maximum evaporation from the UHS.

|  | US EPR FSAR Table 2.1-3 Value |  | Calvert Cliffs Site-Specific Value |  |
| :---: | :---: | :---: | :---: | :---: |
| Time (hr) | $\begin{gathered} \text { Wet Bulb Temp } \\ \left({ }^{\circ} \mathrm{F}\right) \end{gathered}$ | $\begin{gathered} \text { Dry Bulb Temp } \\ \left({ }^{\circ} \mathrm{F}\right) \end{gathered}$ | $\begin{gathered} \text { Wet Bulb Temp } \\ \left({ }^{\circ} \mathrm{F}\right) \end{gathered}$ | $\begin{gathered} \text { Dry Bulb Temp } \\ \left({ }^{\circ} \mathrm{F}\right) \end{gathered}$ |
| 1 | 69.87 | 84 | 69.87 | 84 |
| $\underline{2}$ | 68.69 | 82 | 68.69 | 82 |
| 3 | 66.82 | 78 | 66.82 | 78 |
| 4 | $\underline{67.02}$ | $\underline{77}$ | $\underline{67.02}$ | $\underline{77}$ |
| 5 | $\underline{69.04}$ | 78 | $\underline{69.04}$ | 78 |
| $\underline{6}$ | 68.48 | 78 | 68.48 | 78 |
| 7 | 68.14 | 77 | 68.14 | 77 |
| 8 | 67.10 | 74 | 67.10 | $\underline{74}$ |
| 9 | 67.10 | 74 | 67.10 | 74 |
| 10 | $\underline{67.80}$ | $\underline{76}$ | $\underline{67.80}$ | $\underline{76}$ |
| 11 | $\underline{67.23}$ | $\underline{76}$ | $\underline{67.23}$ | $\underline{76}$ |
| 12 | $\underline{69.79}$ | 82 | $\underline{69.79}$ | 82 |
| 13 | 70.98 | 84 | 70.98 | 84 |
| 14 | 72.71 | 86 | 72.71 | 86 |
| 15 | 74.15 | 89 | 74.15 | 89 |
| 16 | 74.71 | 93 | 74.71 | 93 |
| 17 | 74.98 | 94 | 74.98 | 94 |
| 18 | 75.92 | $\underline{93}$ | 75.92 | $\underline{93}$ |
| 19 | 74.98 | $\underline{98}$ | 74.98 | $\underline{98}$ |
| $\underline{20}$ | 74.20 | $\underline{97}$ | $\underline{74.20}$ | $\underline{97}$ |
| $\underline{21}$ | 74.19 | 97 | 74.19 | $\underline{97}$ |
| $\underline{22}$ | 74.16 | 95 | $\underline{74.16}$ | 95 |
| $\underline{23}$ | 74.15 | 93 | 74.15 | 93 |
| $\underline{24}$ | 72.22 | $\underline{90}$ | $\underline{72.22}$ | $\underline{90}$ |
| $\underline{25}$ | $\underline{70.49}$ | 86 | $\underline{70.49}$ | 86 |
| $\underline{26}$ | $\underline{71.03}$ | $\underline{86}$ | $\underline{71.03}$ | 86 |
| $\underline{27}$ | $\underline{71.03}$ | 86 | $\underline{71.03}$ | 86 |
| $\underline{28}$ | $\underline{71.03}$ | 86 | $\underline{71.03}$ | 86 |
| $\underline{29}$ | 71.03 | 86 | 71.03 | 86 |
| 30 | 70.02 | 81 | 70.02 | 81 |
| 31 | $\underline{68.24}$ | $\underline{79}$ | $\underline{68.24}$ | 79 |
| 32 | $\underline{68.25}$ | $\underline{79}$ | $\underline{68.25}$ | $\underline{79}$ |
| 33 | $\underline{68.13}$ | 77 | $\underline{68.13}$ | 77 |
| 34 | 68.13 | 77 | 68.13 | 77 |
| 35 | 69.70 | 80 | $\underline{69.70}$ | 80 |


|  | US EPR FSAR Table 2.1-3 Value |  | Calvert Cliffs Site-Specific Value |  |
| :---: | :---: | :---: | :---: | :---: |
| Time (hr) | Wet Bulb Temp ( ${ }^{\circ} \mathrm{F}$ ) | Dry Bulb Temp ( ${ }^{\circ}$ F) | Wet Bulb Temp ( ${ }^{\circ} \mathrm{F}$ ) | Dry Bulb Temp ( ${ }^{\circ} \mathrm{F}$ ) |
| 36 | 71.79 | 83 | 71.79 | 83 |
| 37 | 72.98 | 85 | 72.98 | 85 |
| 38 | $\underline{75.02}$ | 88 | $\underline{75.02}$ | 88 |
| $\underline{39}$ | $\underline{76.71}$ | $\underline{92}$ | $\underline{76.71}$ | $\underline{92}$ |
| 40 | $\underline{77.49}$ | $\underline{95}$ | $\underline{77.49}$ | $\underline{95}$ |
| 41 | $\underline{78.24}$ | 98 | $\underline{78.24}$ | 98 |
| 42 | 78.72 | 100 | 78.72 | 100 |
| 43 | 78.48 | 99 | 78.48 | 99 |
| 44 | $\underline{77.91}$ | 99 | 77.91 | 99 |
| $\underline{45}$ | $\underline{77.91}$ | $\underline{99}$ | $\underline{77.91}$ | $\underline{99}$ |
| 46 | $\underline{77.10}$ | $\underline{98}$ | $\underline{77.10}$ | $\underline{98}$ |
| $\underline{47}$ | $\underline{76.85}$ | $\underline{97}$ | $\underline{76.85}$ | $\underline{97}$ |
| 48 | 75.24 | 93 | 75.24 | 93 |
| $\underline{49}$ | 74.14 | 91 | 74.14 | 91 |
| 50 | 72.99 | 87 | $\underline{72.99}$ | 87 |
| $\underline{51}$ | $\underline{70.96}$ | $\underline{84}$ | $\underline{70.96}$ | 84 |
| $\underline{52}$ | $\underline{69.33}$ | $\underline{84}$ | $\underline{69.33}$ | $\underline{84}$ |
| $\underline{53}$ | 68.90 | 81 | 68.90 | 81 |
| $\underline{54}$ | $\underline{69.46}$ | 81 | $\underline{69.46}$ | 81 |
| 55 | $\underline{69.13}$ | 80 | $\underline{69.13}$ | 80 |
| 56 | 69.69 | 80 | $\underline{69.69}$ | 80 |
| 57 | 67.70 | 79 | 67.70 | 79 |
| 58 | $\underline{67.70}$ | $\underline{79}$ | $\underline{67.70}$ | $\underline{79}$ |
| $\underline{59}$ | $\underline{68.58}$ | $\underline{80}$ | $\underline{68.58}$ | 80 |
| 60 | 71.53 | 84 | 71.53 | 84 |
| 61 | $\underline{72.40}$ | $\underline{85}$ | $\underline{72.40}$ | 85 |
| 62 | 73 | $\underline{87}$ | 73 | $\underline{87}$ |
| 63 | 73.29 | 88 | 73.29 | 88 |
| 64 | 73.58 | 89 | 73.58 | 89 |
| 65 | 73.58 | 89 | 73.58 | 89 |
| 66 | $\underline{73.33}$ | $\underline{92}$ | $\underline{73.33}$ | $\underline{92}$ |
| $\underline{67}$ | $\underline{73.08}$ | $\underline{93}$ | $\underline{73.08}$ | $\underline{93}$ |
| $\underline{68}$ | $\underline{73.36}$ | $\underline{94}$ | $\underline{73.36}$ | $\underline{94}$ |
| 69 | $\underline{74.42}$ | 94 | $\underline{74.42}$ | 94 |
| 70 | 74.14 | $\underline{93}$ | 74.14 | $\underline{93}$ |
| 71 | 74.68 | 93 | 74.68 | 93 |
| 72 | 73.28 | 88 | 73.28 | 88 |

The Ultimate Heat Sink analysis calculation uses 3-day meteorological data that maximizes inventory loss. The temperatures used in this evaluation are provided in the response to Sub question 2 b above.

Review of the Ultimate Heat Sink sizing criteria calculation indicates the design basis accident heat load decreases during the period $t=72$ hours through $t=720$ hours with no anticipated increases during that period. As heat load decreases, the cooling tower range decreases. Lower range values yield lower evaporation rates for a given ambient wet bulb temperature. The 72nd hour of the DBA scenario represents the peak anticipated evaporation loss during the last 27 days of the DBA.

Drift loss is a fixed percentage of the cooling water flowrate and is provided by the cooling tower vendor based on the drift eliminator configuration used. Seepage loss is an estimated value that is assumed to remain constant throughout the 30-day DBA scenario. Blowdown is secured during the DBA.

Makeup flow to the UHS towers under DBA conditions is the sum of the evaporation loss, drift loss, and seepage loss. The makeup flowrate to the cooling tower, when based on the inventory loss at the end of the initial 72 -hour period, is sufficient to replenish losses through the end of the 30-day DBA scenario.

Drift loss is a percentage of the cooling water flowrate and is provided by the cooling tower vendor based on the drift eliminator configuration used. This drift loss value is independent of ambient environmental conditions.

The U.S. EPR FSAR also states that the design of the UHS is based on a consideration of air temperature data listed in U.S. EPR FSAR Table 2.1-1. Site-specific values for these parameters were determined using 30 years (1978-2007) of meteorological data from Patuxent River Naval Air Station (NAS), Maryland, a nearby representative site (NCDC, 2008). The 0\% exceedance maximum dry bulb and coincident wet bulb temperature values are $102^{\circ} \mathrm{F}\left(39^{\circ} \mathrm{C}\right)$ and $80^{\circ} \mathrm{F}$ $\left(27^{\circ} \mathrm{C}\right)$, respectively. The $0 \%$ exceedance non-coincident maximum wet bulb temperature value is $85^{\circ} \mathrm{F}\left(29^{\circ} \mathrm{C}\right)$. The highest monthly (July) $1 \%$ design values are $80^{\circ} \mathrm{F}\left(27^{\circ} \mathrm{C}\right)$ and $89.5^{\circ} \mathrm{F}\left(31.9^{\circ} \mathrm{C}\right)$ for the wet and mean coincident dry bulb temperatures, respectively. The U.S. EPR FSAR design values listed In Table 2.1-1 bound the calculated values for CCNPP3 listed above except for the $0 \%$ exceedance non-coincident wet bulb temperature value. This comparison is shown in Table 2.0-1. The acceptability of the $0 \%$ exceedance non-coincident wet bulb temperature design value is described in FSAR Section 9.2.1.1.

Since a closed loop hybrid cooling tower will act as the normal heat sink for CCNPP Unit 3, another meteorological condition to consider is the maximum one-hour dry bulb temperatures. The maximum one-hour dry bulb temperature determined for Baltimore, Maryland, in Local Climatological Data, 2002 Annual Summary with Comparative Data, (NOAA, 2002a) is $105^{\circ} \mathrm{F}\left(40.6^{\circ} \mathrm{C}\right)$. This value was determined over a 52 -year period of record (1951-2002). The maximum one-hour dry bulb temperature determined for Patuxent River NAS, Maryland, is $103^{\circ} \mathrm{F}\left(39.4^{\circ} \mathrm{C}\right)$ over the period 1978 through 2007.

The meteorological conditions resulting in minimum cooling due to evaporation of water are presented in Table 2.0-4.

A software routine used in the Ultimate Heat Sink analysis calculation evaluated 30 years of meteorological data (Reference 1) for Patuxent River Naval Air Station (11 miles away from the CCNPP site) and determined the worst 24 hour period from the perspective of minimum cooling. These ambient temperature conditions are imposed on the cooling tower model for the first 24 hours of the DBA.

The table below provides a comparison of the Table 2.1-4 values In the U.S. EPR FSAR and the CCNPP site-specific values used for minimum cooling from the UHS.

|  | US EPR FSAR Table 2.1-4 Value |  | Calvert Cliffs Site-Specific Value |  |
| :---: | :---: | :---: | :---: | :---: |
| $\frac{\text { Time }}{\text { (hr) }}$ | $\begin{gathered} \text { Wet Bulb Temp } \\ \left({ }^{\circ} \mathrm{F}\right) \end{gathered}$ | $\begin{gathered} \text { Dry Bulb Temp } \\ \left({ }^{\circ} \mathrm{F}\right) \end{gathered}$ | $\begin{gathered} \text { Wet Bulb Temp } \\ \left({ }^{\circ} \mathrm{F}\right) \end{gathered}$ | $\begin{gathered} \text { Dry Bulb Temp } \\ \left({ }^{\circ} \mathrm{F}\right) \end{gathered}$ |
| 1 | 75.8 | 82 | 75.8 | 82 |
| $\underline{2}$ | 76.1 | $\underline{83}$ | 76.1 | $\underline{83}$ |
| $\underline{3}$ | $\underline{76.1}$ | $\underline{83}$ | $\underline{76.1}$ | $\underline{83}$ |
| 4 | 77.3 | $\underline{85}$ | 77.3 | 85 |
| 5 | 79.7 | $\underline{89}$ | 79.7 | $\underline{89}$ |
| $\underline{6}$ | 80.8 | $\underline{91}$ | 80.8 | $\underline{91}$ |
| $\underline{7}$ | 82 | 93 | 82 | 93 |
| 8 | 84.6 | 99 | 84.6 | 99 |
| 9 | 85.3 | 99 | 85.3 | 99 |
| 10 | 85.3 | $\underline{99}$ | 85.3 | $\underline{99}$ |
| 11 | 84.2 | 100 | 84.2 | 100 |
| 12 | 84.2 | 100 | 84.2 | 100 |
| 13 | 84.6 | 99 | 84.6 | 99 |
| 14 | 83.9 | $\underline{99}$ | 83.9 | 99 |
| 15 | 83.9 | 99 | 83.9 | 99 |
| 16 | 82.6 | $\underline{96}$ | 82.6 | 96 |
| 17 | 82.6 | $\underline{93}$ | 82.6 | $\underline{93}$ |
| 18 | 82.1 | $\underline{91}$ | 82.1 | $\underline{91}$ |
| 19 | 82.1 | $\underline{91}$ | 82.1 | $\underline{91}$ |
| $\underline{20}$ | 81.9 | $\underline{90}$ | 81.9 | 90 |
| $\underline{21}$ | 80.7 | 88 | 80.7 | 88 |
| $\underline{22}$ | 80.7 | 88 | 80.7 | 88 |
| $\underline{23}$ | 79.5 | 86 | 79.5 | 86 |
| $\underline{24}$ | 79.5 | 86 | 79.5 | 86 |

The meteorological conditions resulting in the potential for water freezing in the ultimate heat sink water storage facility should be below dry bulb temperature values and associated wind speeds. Using 30 years of meteorological data from Patuxent River NAS, Maryland, the coldest month (December) wind speed and mean coincident dry bulb temperature that are exceeded only $1 \%$ of the time are $24 \mathrm{mph}(10.7 \mathrm{mps})$ and $32.3^{\circ} \mathrm{F}\left(0.2^{\circ} \mathrm{C}\right)$. The $0 \%$ exceedance minimum dry bulb temperature value is $0^{\circ} \mathrm{F}\left(-18^{\circ} \mathrm{C}\right)$.

The UHS makeup water system consists of four independent safety-related trains which provide makeup water from the Chesapeake Bay to the ESW System to meet the maximum evaporative and drift water losses for the period from 72 hours post-accident up to 30 days post-accident. The maximum drift loss (percent of water flow) for a single cooling tower will not exceed $0.005 \%$ as described in U.S. EPR FSAR Table 9.2.5-2. Figure 9.2-3 provides the interface between the ESW and the UHS makeup water system. U.S. EPR FSAR Section 9.2 provides a detailed discussion of the ESW system, including a simplified flow arrangement for the ESW system.

Section 9.2.5.1 provides the design bases for the UHS Makeup Water System; Sections 9.2.5.2 and 9.2.5.3 provide a general description of the system and its components; and Section 9.2.5.1 provides the safety evaluation for the system.

A marine weather dataset from the International Comprehensive Ocean Atmosphere Data Set (ICOADS) maintained by the National Center for Atmospheric Research (NCAR) Computational \& Information Systems Laboratory (CISL) for the period 1940 through 2005 was reviewed for a region extending from $33^{\circ}$ latitude to $41^{\circ}$ latitude and from $277^{\circ}$ longitude to $288^{\circ}$ longitude to determine the historical maximum sea surface temperature experienced in the region nearest
the plant (NCAR, 2006). This area encompasses a rectangle of approximately 480 miles by 600 miles, centered on the CCNPP Unit 3 site. This review indicates a maximum surface temperature of the water in Chesapeake Bay of $93^{\circ} \mathrm{F}$ which is less than the maximum allowable ESW inlet temperature of $95^{\circ} \mathrm{F}$ as described in U.S. EPR FSAR Section 9.2.1. Therefore, UHS makeup water flow to the cooling tower will not increase the cooling tower basin water temperature beyond $95^{\circ} \mathrm{F}$, and therefore, will not adversely impact ESW system safety function.

Additional information on the UHS is provided in Section 9.2.5.

### 2.3.1.2.2.14 Tornado Parameters

Using the methodology from NRC Regulatory Guide 1.76, "Design-Basis Tornado and Tornado Missiles for Nuclear Power Plants," (NRC, 2007), the design-basis tornado characteristics for CCNPP Unit 3 are presented in Table 2.3-9. The maximum tornado wind speed is $200 \mathrm{mi} / \mathrm{hr}$ ( 89 $\mathrm{m} / \mathrm{sec}$ ) and the pressure drop is $0.9 \mathrm{psi}(63 \mathrm{mbar}$ ).

### 2.3.1.2.2.15 100 Year Return Period 3 Second Wind Gust

In accordance with ASCE 7-05, "Minimum Design Loads for Buildings and Other Structures," (ASCE, 2006), the basic wind speed to be used in the determination of design wind loads on buildings and other structures is given in Figure 6-1 of that document. This value for the CCNPP site is $95 \mathrm{mph}(42 \mathrm{mps}$ ). Note that this value is the 3 second wind gust for a 50 year return period. Using the appropriate conversion factor from Table C6-7 of ASCE 7-05 (ASCE, 2006), the 100 year return period 3 second wind gust value is $95 \mathrm{mph} \times 1.07=101.65 \mathrm{mph}(45.4 \mathrm{mps})$.

### 2.3.1.2.2.16 Temperature and Humidity for Heating, Ventilation and Air Conditioning

Fable 2.3-10 through Table 2.3-15 (ASHRAE, 2005) present data for Patuxent River NAS, Maryland, from Weather Data Viewer. Patuxent River NAS is located about $11 \mathrm{mi}(17.7 \mathrm{~km})$ south of the CCNPP site.

The annual $1 \%$ exceedance dry bulb temperature and coincident wet bulb temperature are$89.9^{\circ} \mathrm{F}\left(32.2^{\circ} \mathrm{C}\right)$ and $75.5^{\circ} \mathrm{F}\left(24.2^{\circ} \mathrm{C}\right)$ respectively. The annual $2 \%$ exceedance dry bulb temperature and coincident wet bulb temperature are $87.6^{\circ} \mathrm{F}\left(30.9^{\circ} \mathrm{C}\right)$ and $74.6^{\circ} \mathrm{F}\left(23.7^{\circ} \mathrm{C}\right)$ respectively.

The annual $1 \%$ excee dance wet bulb temperature and coincident dry bulb temperature are$77.8^{\circ} \mathrm{F}\left(25.4^{\circ} \mathrm{C}\right)$ and $86.4^{\circ} \mathrm{F}\left(30.2^{\circ} \mathrm{C}\right)$ respectively. The annual $2 \%$ exceedance wet bulbtemperature and coincident dry bulb temperature are $76.5^{\circ} \mathrm{F}\left(24.7^{\circ} \mathrm{C}\right)$ and $84.5^{\circ} \mathrm{F}\left(29.2^{\circ} \mathrm{C}\right)$ respectively. The annual $99.6 \%$ and $99 \%$ exceedance dry bulb termperatures are $16.6^{\circ} \mathrm{F}\left(-8.6^{\circ}\right.$ $\mathrm{C})$ and $20.9^{\circ} \mathrm{F}\left(-6.2^{\circ} \mathrm{C}\right)$, respectively.

According to information from ASHRAE (ASHRAE, 2005), the 100 year return period values of maximum and minimum dry bulb temperature are $104.6^{\circ} \mathrm{F}\left(40.33^{\circ} \mathrm{C}\right)$ and $-9.1^{\circ} \mathrm{F}\left(-22.8^{\circ} \mathrm{C}\right.$, respectively. The 100 year return period value of maximum wet bulb temperature coincident with the 100 year return period value of maximum dry bulb temperature is $86.1^{\circ} \mathrm{F}\left(30.06^{\circ} \mathrm{C}\right)$. The 100 year return period value of maximum wet bulb temperature (non-coincident) is $94.8^{\circ} \mathrm{F}$ ( $34.9^{\circ} \mathrm{C}$ ).U.S. EPR FSAR Section 2.3.1.1 indicates that the U.S. EPR design is based on the $0 \%$ and $1 \%$ exceedance dry-bulb and coincident wet-bulb temperatures listed in U.S. EPR FSAR Table 2.1-1. Site-specific values for these parameters were determined using 30 years (1978-2007) of meteorological data from Patuxent River Naval Air Station (NAS), Maryland, a nearby representative site (NCDC, 2008).

The $1 \%$ exceedance maximum dry bulb and coincident wet bulb temperature values are $95^{\circ} \mathrm{F}$ $\left(35^{\circ} \mathrm{C}\right)$ and $77.5^{\circ} \mathrm{F}\left(25.3^{\circ} \mathrm{C}\right)$ for the hottest month (July). The $1 \%$ exceedance minimum dry bulb temperature value is $32.3^{\circ} \mathrm{F}\left(0.2^{\circ} \mathrm{C}\right)$ for the coldest month (December). The $0 \%$ exceedance maximum dry bulb and coincident wet bulb temperature values are $102^{\circ} \mathrm{F}\left(39^{\circ} \mathrm{C}\right)$ and $80^{\circ} \mathrm{F}$ $\left(27^{\circ} \mathrm{C}\right)$, respectively. The U.S. EPR FSAR design values listed in Table 2.1-1 bound the calculated values for CCNPP3 listed above.

The 100 year return temperature values have been calculated based on SRP 2.3.1 requesting the information. The calculated 100-year return period values of maximum and minimum dry bulb temperature are $104.6^{\circ} \mathrm{F}\left(40.33^{\circ} \mathrm{C}\right)$ and $-9.1^{\circ} \mathrm{F}\left(-22.8^{\circ} \mathrm{C}\right)$, respectively. The 100 -year return period value of maximum wet bulb temperature coincident with the 100 -year return period value of maximum dry bulb temperature is $86.1^{\circ} \mathrm{F}\left(30.36^{\circ} \mathrm{C}\right)$. The 100 -year return period value of maximum wet bulb temperature (non-coincident) is $94.8^{\circ} \mathrm{F}\left(34.9^{\circ} \mathrm{C}\right)$. These values were determined using the 20 years of meteorological data provided by ASHRAE and the following equation (ASHRAE,2005):
$\mathrm{Tn}=\mathrm{M}+\mathrm{I}^{*} \mathrm{~F}^{*} \mathrm{~s}$
where Tn is the n -year return period value of extreme dry bulb temperature (in this case the 50 -year values of $103.4^{\circ} \mathrm{F}$ and $-5.9^{\circ} \mathrm{F}$ ), M is the mean of the annual extreme maximum or minimum dry bulb temperatures, $s$ is the standard deviation of the annual extreme maximum or minimum dry bulb, l is 1 if maximum dry bulb temperatures are being considered or -1 if minimum dry bulb temperatures are being considered, and $F$ is given by:
$F=-\sqrt{6} / \Pi(0.5772+\ln (\ln (100 / 99)))$
Although these calculated 100-year return temperature values are higher than the 0\% exceedance values described above, the 100-year return values are not used in the design of HVAC systems at CCNPP3. Reliable, sequential hourly meteorological data does not exist for the duration of 100 years. As a result, the use of extrapolated maximum/minimum 100 year return period temperature values would be overly conservative and exceed any recorded values in the available 30-year Pax River NAS data set. In contrast, the site-specific maximum and minimum $0 \%$ exceedance dry-bulb and wet-bulb temperature values are conservatively calculated using the maximum and minimum observed temperatures at each $1^{\circ} \mathrm{F}$ temperature increments. recorded at Pax River NAS for the most recent 30 years.

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### 2.3.2 LOCAL METEOROLOGY

The U.S. EPR FSAR includes the following COL Item in Section 2.3.2:
A COL applicant that references the U.S. EPR design certification will provide site-specific characteristics for local meteorology.

This COL Item is addressed as follows:
\{Sections 2.3.2.1 through Section 2.3.2.4 are added as a supplement to the U.S. EPR FSAR.
Sections 2.3.2.1 and 2.3.2.2 present local summaries of meteorological data based on onsite measurements made in accordance with Nuclear Regulatory Commission (NRC) Regulatory Guide 1.23, "Meteorological Monitoring Programs for Nuclear Power Plants," Revision 1, (NRC, 2007a) and National Weather Service station summaries from appropriate nearby locations.

Onsite meteorological data compiled for Calvert Cliffs Nuclear Power Plant (CCNPP) Units 1 and 2 were used in this analysis for CCNPP Unit 3. CCNPP Unit 3 is located approximately 2,000 ft ( 610 m ) south of CCNPP Units 1 and 2.

These data are from the existing units' onsite meteorological monitoring program which was designed, and has been operated, according to Safety Guide 23 (Regulatory Guide 1.23, Revision 0), Onsite Meteorological Programs, (NRC, 1972).

The data recovery goal of $90 \%$ was met for each of the 6 years of data ( 2000 to 2005). The pre-operational meteorological monitoring program also meets the requirements of Regulatory Guide 1.23, Revision 1 (NRC, 2007a), with the following deviations: no atmospheric moisture measurements (required for plants utilizing cooling towers), tower not sited at approximately the same elevation as finished plant grade, and tower, guyed wire, and anchor inspection performance of once every 5 years instead of an annual inspection for tower and guyed wire and an anchor inspection of once every 3 years. These deviations are discussed further in Section 2.3.3.1.7.

Local meteorological values used for design and operating bases are bounded by those in the U.S. EPR FSAR.

### 2.3.2.1 Normal and Extreme Values of Meteorological Parameters

Monthly and annual summaries of meteorological data are provided in Sections 2.3.2.1.1 through 2.3.2.1.6.

### 2.3.2.1.1 Wind Speed and Direction

Table 2.3-16 and Table 2.3-17 present annual joint frequency distributions (JFD) of wind speed and direction as a function of atmospheric stability derived from the CCNPP onsite meteorological monitoring program. Table 2.3-18 through Table 2.3-41 present monthly joint frequency distributions of wind speed and direction as a function of atmospheric stability. These tables were developed using 6 years of onsite meteorological data (2000 to 2005) following the guidance in Regulatory Guide 1.23 (NRC, 2007a). Note that additional wind speed classes were added to provide greater coverage of the lower wind speeds that are most important for atmospheric dispersion.

Table 2.3-134 and Table 2.3-135 present annual joint frequency distributions (JFD's) of wind speed and direction as a function of atmospheric stability derived from the 2000-2006 data from the CCNPP on-site meteorological monitoring program. The hourly data used to calculate these tables were used to determine the atmospheric dispersion and deposition factors presented in Sections 2.3.4 and 2.3.5.

Figure 2.3-14 and Figure 2.3-15 present annual wind rose plots of the 2000 to 2005 meteorological data for the $33 \mathrm{ft}(10 \mathrm{~m})$ and $197 \mathrm{ft}(60 \mathrm{~m})$ elevations using the wind speed classes utilized for the JFD tables. Figure 2.3-16 through Figure 2.3-39 present monthly wind rose plots of the 2000 to 2005 meteorological data for the $33 \mathrm{ft}(10 \mathrm{~m})$ and $197 \mathrm{ft}(60 \mathrm{~m})$ elevations using the wind speed classes provided in Regulatory Guide 1.23 (NRC, 2007a).

Figure 2.3-223 and Figure 2.3-40 through Figure 2.3-42 present multi-year average annual wind rose plots for National Weather Service (NWS) stations around the CCNPP site (Patuxent River NAS, Maryland, Baltimore/Washington International (BWI) Airport, Norfolk International Airport, Virginia, and Richmond International Airport, Virginia). Meteorological data used to create the plots were received from the National Climatic Data Center for Patuxent River NAS (NCDC 2008), and from the U.S. Environmental Protection Agency Support Center for Regulatory Air Models (EPA, 2007a) and were measured at approximately $33 \mathrm{ft}(10 \mathrm{~m})$ above ground level. For Patuxent River NAS, the meteorological data were from 2000 through 2005. For Norfolk and Richmond International Airports, the meteorological data were from 1984 through 1992. For BWI, the meteorological data were from 1984 through 1992, with the exception of 1989.

The annual prevailing wind direction (the direction from which the wind blows most often) at the CCNPP site at the $33 \mathrm{ft}(10 \mathrm{~m})$ level is from the southwest, approximately $14 \%$ of the time. Winds from the southwest through west sectors occur approximately $26 \%$ of the time. Conversely, winds from the northeast through east sectors occur approximately $14 \%$ of the time. The annual prevailing wind direction at the CCNPP site at the $197 \mathrm{ft}(60 \mathrm{~m})$ level is from the southwest, approximately $10 \%$ of the time. Winds from the southwest through west sectors occur approximately $20 \%$ of the time. Conversely, winds from the northeast through east sectors occur approximately $13 \%$ of the time. As is normally the case, there are more observations of calm winds at the lower level than at the upper level ( $0.33 \%$ versus $0.03 \%$ ). At both the $33 \mathrm{ft}(10 \mathrm{~m})$ and $197 \mathrm{ft}(60 \mathrm{~m})$ levels, winds occur most infrequently from the east-southeast.

A comparison of the CCNPP $33 \mathrm{ft}(10 \mathrm{~m})$ annual wind rose with the Patuxent River NAS annual wind rose was made over the period 2000 through 2005. The annual prevailing wind direction (the direction from which the wind blows most often) at the CCNPP site at the $33 \mathrm{ft}(10 \mathrm{~m})$ level is from the southwest approximately $14 \%$ of the time. The annual prevailing wind direction at Patuxent River NAS is from the north, approximately $10 \%$ of the time. Winds from the southwest through west sectors occur approximately $26 \%$ of the time at CCNPP. Conversely, winds from the northeast through east sectors occur approximately $14 \%$ of the time at CCNPP. Winds from the southwest through west sectors occur approximately $23 \%$ of the time at Patuxent River NAS. Conversely, winds from the northeast through east sectors occur approximately $17 \%$ of the time at Patuxent River NAS. At both sites, winds occur most infrequently from the east-southeast (approximately $2.5 \%$ at CCNPP and approximately $1.5 \%$ at Patuxent River NAS). The mismatch in prevailing wind direction may be due to the differences in the location of the sites with respect to the Chesapeake Bay (CCNPP has the Bay to the east, Patuxent River NAS has the Bay to the north).

The annual prevailing wind direction at Baltimore/Washington International (BWI) Airport is from the west, approximately $13 \%$ of the time. At Norfolk, Virginia, the annual prevailing wind direction is from the southwest, approximately $11 \%$ of the time. At Richmond, Virginia, the annual prevailing wind direction is from the south-southwest, approximately $10 \%$ of the time. Note that there are more observations of calm winds at these three NWS sites than at the CCNPP site. This may be due to:

1. The CCNPP site is located directly on the Chesapeake Bay. Of the three NWS stations, Richmond International Airport is approximately $50 \mathrm{mi}(80 \mathrm{~km})$ inland, BWI is approximately $4 \mathrm{mi}(6.4 \mathrm{~km})$ from the Chesapeake Bay, and Norfolk International Airport is approximately $2 \mathrm{mi}(3.2 \mathrm{~km})$ from the Chesapeake Bay. The sea/land breeze phenomenon is stronger at the coast line than further inland.
2. The use of different wind measurement instruments due to the different needs at the sites. The NWS sites are at airports, where high wind speeds are more important than low wind speeds since they have a greater impact on aviation. At the CCNPP site, wind measurements are made to determine atmospheric dispersion to aid in dose assessment; therefore, low wind speeds are more important since they will lead to less dispersion and higher dose.

During the winter months (December through February), the prevailing wind direction at both levels is from the northwest, approximately $13 \%$. Winds from the southwest are the next most dominant, occurring approximately $11 \%$ of the time at the $33 \mathrm{ft}(10 \mathrm{~m}$ ) level and approximately $9 \%$ of the time at the $197 \mathrm{ft}(60 \mathrm{~m}$ ) level. During the spring months (March through May), the prevailing wind direction at both levels is from the southwest, approximately $12 \%$ of the time at the lower level and $11 \%$ of the time at the upper level.

During the summer months (June through August), the prevailing wind direction at both levels is from the southwest, approximately $18 \%$ of the time at the lower level and $14 \%$ of the time at the upper level. During the autumn months (September through November), the prevailing wind direction at the $33 \mathrm{ft}(10 \mathrm{~m}$ ) level is from the southwest, approximately $12 \%$ of the time. At the $197 \mathrm{ft}(60 \mathrm{~m}$ ) level, the prevailing wind directions are from the north-northeast and from the south-southwest, approximately $9 \%$ of the time. The north-northeast flow dominates in September and October and the south-southwest flow dominates in November.

The most prevalent wind speed class at the CCNPP site on an annual basis for the 33 ft ( 10 m ) level is the 4.7 to $6.7 \mathrm{mph}(2.1$ to 3.0 mps ) class, which occurs approximately $28 \%$ of the time. The most prevalent wind speed class on an annual basis for the $197 \mathrm{ft}(60 \mathrm{~m})$ level is the 13.6 to 17.9 mph ( 6.1 to 8.0 mps ) class, which occurs approximately $21 \%$ of the time.

Figure 2.3-224 presents the wind speed class frequency distribution for Patuxent River Naval Air Station (NAS), Maryland, for the years 2000 through 2005. The most prevalent wind speed class at Patuxent River NAS is $6.7-8.9 \mathrm{mph}(3.0-4.0 \mathrm{mps})$. The average wind speed at BWI is 8.8 mph ( 3.92 mps ) and there have been observations of wind speeds greater than $25 \mathrm{mph}(11 \mathrm{mps}$ ). At Norfolk International Airport, Virginia, the average wind speed is $11.0 \mathrm{mph}(4.92 \mathrm{mps})$ and there have been observations of wind speeds greater than $25 \mathrm{mph}(11 \mathrm{mps})$. At Richmond International Airport, Virginia, the average wind speed is $8.3 \mathrm{mph}(3.70 \mathrm{mps})$ and there have been observations of wind speeds up to 25 mph ( 11 mps ).

Note that the most prevalent wind speed class on an annual basis for the $33 \mathrm{ft}(10 \mathrm{~m})$ level at CCNPP (4-7 mph (1.8-3.1 mps) ) is lower than the most prevalent wind speed class at Patuxent River NAS ( $6.7-8.9 \mathrm{mph}(3.0-4.0 \mathrm{mps})$ ). That value is lower than the average annual wind speeds
at the same measurement height presented for BWI, Norfolk and Richmond, this would lead to more conservative atmospheric dispersion estimates using the CCNPP meteorological data.

On a seasonal basis, the most prevalent wind speed class for the $33 \mathrm{ft}(10 \mathrm{~m})$ level is the 4.7 to 6.7 mph ( 2.1 to 3.0 mps ) class, which occurs approximately $25 \%$ of the time during the winter months (December through February), 27\% of the time during the spring months (March through May), $32 \%$ during the summer months (June through August), and $27 \%$ during the autumn months (September through November). At the $197 \mathrm{ft}(60 \mathrm{~m})$ level, the most prevalent wind speed class is the 13.6 to 17.9 mph ( 6.1 to 8.0 mps ) class, which occurs approximately $25 \%$ during the winter months (December through February), 24\% during the spring months (March through May), and 21\% during the autumn months (September through November). During the summer months (June through August), the most prevalent wind speed class is the 9.2 to 11.2 mph ( 4.1 to 5.0 mps ) class which occurs approximately $21 \%$ of the time.

The maximum hourly wind speed measured at the $33 \mathrm{ft}(10 \mathrm{~m})$ level is $30.1 \mathrm{mph}(13.5 \mathrm{mps}$ ); the maximum hourly wind speed measured at the $197 \mathrm{ft}(60 \mathrm{~m})$ level is $45.4 \mathrm{mph}(20.3 \mathrm{mps})$.

Table 2.3-42 through Table 2.3-55 present annual and overall wind direction persistence summaries for the $33 \mathrm{ft}(10 \mathrm{~m})$ and $197 \mathrm{ft}(60 \mathrm{~m})$ measurement levels at the CCNPP site. These tables were developed using 6 years of onsite meteorological data (2000 to 2005). Table 2.3-48 and Table 2.3-55 present an average of the six individual year summaries for the 33 ft ( 10 m ) and $197 \mathrm{ft}(60 \mathrm{~m})$ measurement levels respectively.

The majority of the time, approximately $86 \%$, wind direction persistence events last for less than 4 hours at both measurement levels. Wind direction persistence events lasting 12 hours occur six and eight times per year on the average for the lower and upper measurement levels, respectively. Wind direction persistence events lasting greater than 24 hours occur once per year on the average for the lower and upper measurement levels.

### 2.3.2.1.2 Temperature and Humidity

Monthly and annual temperature summaries from the CCNPP onsite meteorological monitoring program are presented in Table 2.3-56 through Table 2.3-63 for the period from January 2000 through December 2005. Table 2.3-131 presents monthly and annual temperature summaries from the CCNPP on-site meteorological monitoring program for the period from January 1987 through December 2006. The monthly mean extreme maximum temperature is defined as the highest of the monthly average values for each month over the data period. The monthly mean extreme minimum temperature is defined as the lowest of the monthly average values for each month over the data period. These values are determined by calculating the monthly average temperature for each month of each year and then identifying the maximum and minimum monthly average temperature value for each month over the data period.

The monthly mean temperature at the CCNPP site ranges from $34.3^{\circ} \mathrm{F}\left(1.3^{\circ} \mathrm{C}\right)$ in January to $75.1^{\circ} \mathrm{F}\left(23.9^{\circ} \mathrm{C}\right)$ in July. The monthly mean extreme maximum temperature at the CCNPP site was $78.3^{\circ} \mathrm{F}\left(25.7^{\circ} \mathrm{C}\right)$ in July and the monthly mean extreme minimum temperature was $29.5^{\circ} \mathrm{F}$ $\left(-1.4^{\circ} \mathrm{C}\right)$ in January. The monthly mean daily maximum temperature at the CCNPP site was $81.8^{\circ} \mathrm{F}\left(27.7^{\circ} \mathrm{C}\right)$ in July and the monthly mean daily minimum temperature was $28.5^{\circ} \mathrm{F}\left(-1.9^{\circ} \mathrm{C}\right)$ in January. The maximum hourly temperature at the CCNPP site was $96.3^{\circ} \mathrm{F}\left(35.7^{\circ} \mathrm{C}\right)$ in July and the minimum hourly temperature was $8.5^{\circ} \mathrm{F}\left(-13.1^{\circ} \mathrm{C}\right)$ in December. The frequency of occurrence of hourly temperature values falling below the freezing point $\left(32^{\circ} \mathrm{F}\right.$ or $0^{\circ} \mathrm{C}$ ) is less than 10\%.

Temperature and humidity statistics from sites around the CCNPP site are presented in Table 2.3-64 through Table 2.3-73. Dry bulb temperature values are from the 30 year period from 1971 to 2000. Wet bulb temperature values are from the 18 year period from 1983 to 2000. The monthly mean temperatures measured at the CCNPP site show good correspondence with the values presented in these tables, for example, almost all of the mean monthly temperatures measured at the CCNPP site fall within the range of values reported by the surrounding stations.

A comparison of the monthly average temperature values at CCNPP (Table 2.3-131) and the Patuxent River Naval Air Station (Table 2.3-64) was performed by determining the percent difference between the corresponding monthly values. The percent difference was defined as the absolute value of the difference between the monthly values times 100 and divided by the average of the monthly values. The comparison showed that the percent differences between the monthly average temperatures are within $3 \%$ of each other for all months, within $1.74 \%$ on average, and range from $0.26 \%$ to $2.65 \%$. This shows good agreement between the two sites.

Table 2.3-74 through Table 2.3-76 present the monthly design wet bulb temperature and the mean coincident dry bulb temperature for locations in the vicinity of the CCNPP site. These wet bulb temperature values correspond to $0.4 \%, 1.0 \%$, and $2.0 \%$ cumulative frequency of occurrence for the indicated month. The data were determined from the American Society of Heating, Refrigeration, and Air-Conditioning Engineers Weather Data Viewer (ASHRAE, 2005). Data for the Patuxent River Naval Air Station, Maryland, are from the period 1982 to 2001. Data from Salisbury Wicomico County Airport, Maryland, are from the period 1982 to 2001. Data from Baltimore, Maryland, are from 1972 to 2001.

### 2.3.2.1.3 Precipitation and Fog

The monthly and annual precipitation summary from the CCNPP onsite meteorological monitoring program is presented in Table 2.3-77 through Table 2.3-80 for the period from 2000 tothrough 2005. Table 2.3-132 presents the monthly and annual precipitation summary from the CCNPP on-site meteorological monitoring program for the period from January 1992 through December 2006. The rainfall rate distribution is provided in Table 2.3-79. Precipitation statistics from NWS sites around the CCNPP site are presented in Table 2.3-81 for the period from 1971 to 2000 and in Table 2.3-82 and Table 2.3-83 for the period from 1961 to 1990. Monthly and annual summaries of heavy fog (visibility less than one-quarter mile) are presented in Table 2.3-84 for sites around the CCNPP site.

Monthly average precipitation at the CCNPP site ranges from 1.53 in ( 38.86 mm ) in February to 4.53 in ( 115.06 mm ) in July. Monthly percent frequency of occurrence of precipitation at the CCNPP site ranges from $4.26 \%$ in September to $7.87 \%$ in April. The rainfall rate distribution presented in Table 2.3.2-642.3-83 indicates that heavy rainfalls occur infrequently at the CCNPP site. The maximum monthly precipitation measured at the CCNPP site corresponds well with the values from the NWS sites around the plant. The minimum monthly precipitation measured at CCNPP, however, does not correspond well with the values from the NWS sites around the plant; this may be due to the difference in the period of records ( 6 years for the CCNPP site versus 30 for the NWS sites).

A comparison of the monthly average precipitation values at CCNPP (Table 2.3-132) and the Patuxent River Naval Air Station (Table 2.3-81) was performed by determining the percent difference between the corresponding monthly values. The percent difference was defined as the absolute value of the difference between the monthly values times 100 and divided by the average of the monthly values. The comparison showed that the percent differences between the monthly average temperatures are within $33 \%$ on average and range from $8.73 \%$ to
$68.91 \%$. This shows poor agreement between the two sites. This may be due to the localized nature of convective precipitation events which are characterized by limited areal distribution, the suddenness with which they start and stop, and by rapid changes in intensity. Another potential factor to consider in light of the fact that the CCNPP monthly average values are all lower than the Patuxent River NAS values, is that CCNPP does not employ a wind screen. Wind screens are used in open, exposed areas, which are subject to strong gusty winds to minimize the wind-caused loss of precipitation falling into the rain gauge.

Figure 2.3-43 and Figure 2.3-44 present annual precipitation wind roses at the CCNPP site for the $33 \mathrm{ft}(10 \mathrm{~m})$ and $197 \mathrm{ft}(60 \mathrm{~m})$ elevations. These precipitation wind roses portray joint frequency distributions of wind speed and direction as a function of atmospheric stability for only the hours in which precipitation was recorded. These annual precipitation wind roses show that the most frequent wind direction has either a northerly or easterly component.

Figure 2.3-45 through Figure 2.3-212 present monthly precipitation wind roses of wind speed and direction as a function of precipitation rate class at the CCNPP for the $33 \mathrm{ft}(10 \mathrm{~m})$ and 197 ft $(60 \mathrm{~m})$ elevations. These precipitation wind roses portray joint frequency distributions of wind speed and direction as a function of precipitation rate class for only the hours in which precipitation was recorded. These figures show that for the larger precipitation rate classes (0.5 $\mathrm{in} / \mathrm{hr}(12.7 \mathrm{~mm} / \mathrm{hr})$ and greater) in the spring and summer where there is more than a single observation, the most frequent wind direction may have a southerly or westerly component. This could indicate high rainfall rates due to thunderstorms rather than offshore storms and their associated northeasterly winds.

Fog observations are not made as part of the onsite meteorological monitoring program. Fog observations were made at the NWS stations at Baltimore/Washington International Airport Maryland, Richmond International Airport, Virginia, and Norfolk International Airport, Virginia. The average number of days per year with heavy fog (visibility less than one-quarter mile) are 24.4, 27.1, and 19.7 for Baltimore, Richmond, and Norfolk, respectively. No information was provided on the duration of heavy fog events in the reference material reviewed (NOAA, 2002a) (NOAA, 2002b) (NOAA, 2002c).

### 2.3.2.1.4 Atmospheric Stability

Depending on the amount of incoming solar radiation and other factors, the atmosphere may be more or less turbulent at any given time. Meteorologists have defined atmospheric stability classes, each representing a different degree of turbulence in the atmosphere. When moderate to strong incoming solar radiation heats air near the ground, causing it to rise and generate large eddies, the atmosphere is considered unstable, or relatively turbulent. Unstable conditions are associated with atmospheric stability classes $A$ and $B$. When solar radiation is relatively weak or absent, air near the surface has a reduced tendency to rise, and less turbulence develops. In this case, the atmosphere is considered stable, or less turbulent, and the stability class would be E or F. Stability classes D and C represent conditions of more neutral stability, or moderate turbulence. Neutral conditions are associated with relatively strong wind speeds and moderate solar radiation.

Atmospheric stability is determined by the delta temperature method as defined in Regulatory Guide 1.23 (NRC, 2007a). This methodology classifies atmospheric stability based on the temperature change with height ( ${ }^{\circ} \mathrm{C}$ per 100 m ). At the CCNPP site, atmospheric stability is classified according to the difference between the temperature measurements at the 197 ft (60 m ) and 33 ft ( 10 m ) levels.

Table 2.3-85 through Table 2.3-98 present annual and overall atmospheric stability persistence summaries at the CCNPP site for the $33 \mathrm{ft}(10 \mathrm{~m})$ and $197 \mathrm{ft}(60 \mathrm{~m})$ measurement levels. The annual tables were developed using 6 years of onsite meteorological data ( 2000 to 2005). Note that there are slight differences between the $33 \mathrm{ft}(10 \mathrm{~m}$ ) and $197 \mathrm{ft}(60 \mathrm{~m})$ tables even though they use the same delta-temperature measurements to determine atmospheric stability. This is because the computer code used to develop the tables checks the validity of the wind speed and direction values as well as the delta-temperature values.

The majority of the time (approximately 78\%), stability persistence events last for less than 4 hours. Stability persistence events lasting 12 hours occur 19 times per year on the average and events lasting for greater than 24 hours occur nine times per year on the average.

Table 2.3-133 presents the monthly atmospheric stability summary. It was generated using six years of on-site meteorological data (2000-2005).

### 2.3.2.1.5 Monthly Mixing Height Data and Inversion Summary

Monthly average mixing height values for the period from 1996 through 2005 were calculated from the daily average values for each month of each year (as data were available) based on twice daily mixing height data from the National Climatic Data Center. These data were taken from the upper air and surface National Weather Service stations closest to the CCNPP site (Wallops Island and Patuxent River, respectively). Overall monthly average mixing height values were calculated from the individual monthly average values; for example, the January overall monthly average mixing height value of $1978 \mathrm{ft}(603 \mathrm{~m})$ is the average of all of the individual January mixing height values from 1996 through 2005. On average, the number of valid days of data per month ranged from 23 to 30 (that is, days that had both a morning and afternoon mixing height value); there were some months with no valid data. Data were unavailable for 17 out of 120 months with the majority of these months (15 of 17) being in 1996 and 1997. Since there are 6 years with 12 months of valid data and 2 years with 11 months of valid data, the missing data do not adversely impact the determination of the monthly and annual average mixing height values.

Figure 2.3-213 presents the monthly average mixing height values. Table 2.3-99 shows the monthly average mixing height values in tabular form. As shown, the monthly average mixing heights ranged from $1,881 \mathrm{ft}(573 \mathrm{~m}$ ) in December to $2,959 \mathrm{ft}(902 \mathrm{~m})$ in July. The annual average mixing height was $2,452 \mathrm{ft}$ ( 748 m ).

Frequency and persistence of temperature inversion conditions at the CCNPP site are shown in Table 2.3-1001 through Table 2.3-105106. These tables were developed using 6 years of onsite meteorological data (2000 through 2005). The maximum temperature inversion duration was 31 hours. Approximately two-thirds of the inversions lasted less than 9 hours.

### 2.3.2.1.6 Air Quality

Based on EPA data, Calvert County, Maryland, is in attainment for all the National Ambient Air Quality Standards (NAAQS) except for the 8 hour ozone standard (EPA, 2007b) as of December 5,2006 . Attainment means that the air quality is better than the standard. The 8 hour ozone standard is 0.08 ppm and attainment is determined by whether the 3 year average of the fourth-highest daily maximum 8 hour average ozone concentrations measured at each monitor within an area over each year exceeds the standard. From Figure 2.3-206 it can be seen that the fourth-highest, 8 hour average ozone concentration for Calvert County during 2006 is greater than 0.08 ppm and less than or equal to 1.0 ppm . Nonattainment of the 8 hour ozone standard is due to its proximity to Washington, D.C. A nonattainment designation requires a state plan to
be sent to the EPA describing how the area will implement air quality improvements. The NAAQS (EPA, 2007c) are presented in Table 2.3.2-912.3-107. Note that the Maryland Department of the Environment reported that ground-level ozone levels have continued to show significant improvements since the early 1990's (MDE, 2006).

Calvert County is part of the Southern Maryland Intrastate Air Quality Control Region (AQCR), as designated in 40 CFR 81.156 (CFR, 2007a). The attainment status of the Southern Maryland Intrastate AQCR with regard to national ambient air quality standards is listed as being better than national standards for total suspended particulates, sulphur dioxide, and nitrogen dioxide, and unclassifiable/attainment for carbon monoxide, $\mathrm{PM}_{2.5}$ (particulate matter with diameter less than 2.5 microns), and for the 8 hour ozone standard (CFR, 2007b).

### 2.3.2.2 Potential Influence of the Plant and its Facilities on Local Meteorology

The CCNPP site consists of low rolling hills. Elevations across the site range from 0 ft ( 0.6 ft NGVD29) above mean sea level (MSL) (at the shoreline of the Chesapeake Bay) to 150 ft MSL ( 150.6 ft NGVD29). There is a hill approximately 110 ft MSL ( 110.6 ft NGVD29) to the southeast of CCNPP Units 1 and 2. Another hill south-southeast of CCNPP Units 1 and 2 will be graded for CCNPP Unit 3; the CCNPP Unit 3 site grade will be approximately 84.1 ft MSL ( 84.7 ft NGVD29). The terrain falls off steeply to the shore of the Chesapeake Bay. The highest terrain in the vicinity of the site is in the west through north-northwest sectors. The Chesapeake Bay lies in the north through southwest sectors.

Figure 2.3-215 presents a map which shows the topography within a $1 \mathrm{mi}(1.6 \mathrm{~km})$ radius of the CCNPP site, the location of the meteorological tower, and CCNPP Units 1 and 2. Figure 2.3-216 presents a map which shows the topography within a $5 \mathrm{mi}(8 \mathrm{~km})$ radius of the CCNPP site. Figure 2.3-217 presents a map which shows the topography within a $50 \mathrm{mi}(80 \mathrm{~km})$ radius of the CCNPP site. Figure 2.3-218 presents a plot of maximum elevation versus distance from the center of the plant in each of the sixteen 22.5 degree compass point sectors (centered on true north, north-northeast, northeast, etc.) radiating from the plant to a distance of $50 \mathrm{mi}(80 \mathrm{~km})$.

CCNPP Unit 3 will be southeast of the existing Units 1 and 2 . Some portions of the CCNPP site will be cleared of existing vegetation and graded to accommodate CCNPP Unit 3 and its ancillary structures. These terrain modifications would be limited to the CCNPP Unit 3 area and the immediately surrounding area and, therefore, will not represent a significant alteration to the topographic character of the region around the CCNPP site.

Construction activity will meet all pertinent Federal and State air quality regulations.
Waste heat produced by CCNPP Unit 3 will be dissipated by a closed-cycle, wet-cooling system, consisting of a single hybrid mechanical draft cooling tower. The hybrid mechanical draft cooling tower has a lower profile than the CCNPP Unit 3 containment.

For CCNPP Unit 3, the impacts from fogging, icing, shadowing, and drift deposition from the cooling tower were modeled using the Electric Power Research Institute's Seasonal/Annual Cooling Tower Impact (SACTI) prediction code. This code incorporates the modeling concepts (Policastro, 1993), which were endorsed by the NRC in NUREG-1555 (NRC, 1999). The model provides predictions of seasonal, monthly, and annual cooling tower impacts from mechanical or natural draft cooling towers. It predicts average plume length, rise, drift deposition, fogging, icing, and shadowing, providing results that have been validated with experimental data (Policastro, 1993).

The modeling determined the following:

- Due to the varying directions that the plume travels and short average and median plume height and length, impacts from elevated plumes would be SMALL and not warrant mitigation.
- Impacts from the cooling tower from fogging and icing would be SMALL and would not require mitigation. Fogging and icing would occur for only a small percentage of the time and would occur most frequently onsite.
- Impacts from salt deposition from the cooling tower would be SMALL.
- Salt deposition was predicted at rates below the NUREG-1555 significance level where visible vegetation damage may occur for both onsite and offsite locations.
- Impacts from cloud shadowing and additional precipitation would be SMALL and would not require mitigation.
- Impacts from increases in absolute and relative humidity would be SMALL and mitigation would not be warranted.

As such, CCNPP Unit 3 is not expected to cause any significant influence on local meteorology.

### 2.3.2.3 Local Meteorological Conditions for Design and Operating Bases

Meteorological conditions for design and operating bases are discussed in Section 2.3.1.2.

### 2.3.2.4 References

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### 2.3.3 ONSITE METEOROLOGICAL MEASUREMENT PROGRAM

The U.S. EPR FSAR includes the following COL Item in Section 2.3.3:
A COL applicant that references the U.S. EPR design certification will provide the site-specific, onsite meteorological measurement program.

This COL Item is addressed as follows:
\{Sections 2.3.3.1 through 2.3.3.3 are added as a supplement to the U.S. EPR FSAR.

### 2.3.3.1 Preoperational Meteorological Measurement Program

The pre-operational meteorological measurement program for Calvert Cliffs Nuclear Power Plant (CCNPP) Unit 3 utilizes the existing operational meteorological measurement program and equipment established for CCNPP Units 1 and 2. Data from the CCNPP Units 1 and 2 operational meteorological measurement program were used in this analysis for CCNPP Unit 3. CCNPP Unit 3 is to be located approximately $2,000 \mathrm{ft}(610 \mathrm{~m})$ south of CCNPP Units 1 and 2.

> The pre-operational meteorological measurement program for Calvert Cliffs Nuclear Power Plant (CCNPP) Unit 3 utilizes the existing operational meteorological measurement program and equipment established for CCNPP Units 1 and 2. Data from the CCNPP Units 1 and 2 operational meteorological measurement program were used in this analysis for CCNPP Unit 3. CCNPP Unit 3 is to be located approximately $2,000 \mathrm{ft}(610 \mathrm{~m})$ south of CCNPP Units 1 and 2.

> The monthly mean temperatures measured at the CCNPP site show good correspondence with the monthly mean temperature values measured at surrounding National Weather Service
(NWS) sites as provided in Section 2.3.2.1.2. As a result, no additional measurement points are considered necessary for Unit 3.

This program was designed and maintained in accordance with the guidance provided in Safety Guide 23, "Onsite Meteorological Programs" (NRC, 1972). The pre-operational meteorological measurement program also meets the requirements of Regulatory Guide 1.23, Revision 1, "Meteorological Monitoring Programs for Nuclear Power Plants" (NRC, 2007), with the following deviations: no atmospheric moisture measurements (required for plants utilizing cooling towers), tower not sited at approximately the same elevation as finished plant grade, and tower, guyed wire, and anchor inspection performance of once every 5 years instead of an annual inspection for tower and guyed wire and an anchor inspection of once every 3 years. These deviations are discussed further in Section 2.3.3.1.7.

### 2.3.3.1.1 Tower Location

The meteorological tower for the CCNPP site is located in an open field off Calvert Cliffs Parkway north of the CCNPP Unit 1 and 2 Independent Spent Fuel Storage Installation (ISFSI). The elevation at the base of the tower is approximately $125 \mathrm{ft}(38 \mathrm{~m})$ above mean sea level.

Figure 2.3-219 shows the location of the meteorological tower as well as the topography of the CCNPP site. The meteorological tower has been sited for CCNPP Unit 1 and 2 according to the guidance provided in Safety Guide 23 (NRC, 1972). Figure 2.3-220 shows the detailed topography of the region.

The meteorological tower is located on level, open terrain at a distance at least 10 times the height of any nearby obstruction that exceeds one-half the height of the wind measurement with the exception of some trees that are located south of the tower. Even though there are no obstructions in any other sector and south is not the most prevalent wind direction, the tree heights and distances shall be calculated and an evaluation performed to determine whether the trees should be removed. The tower is located far enough away from proposed CCNPP Unit 3 structures and topographical features to avoid airflow modifications. The terrain height difference between the meteorological tower and the CCNPP Unit 3 reactor area is approximately $40 \mathrm{ft}(12 \mathrm{~m})$. The distance between the meteorological tower and the CCNPP Unit 3 reactor is approximately $2,900 \mathrm{ft}(880 \mathrm{~m})$. Therefore, the terrain profile has a very gentle slope and has an insignificant impact on site dispersion conditions.

### 2.3.3.1.2 Tower Design

The meteorological tower is $197 \mathrm{ft}(60 \mathrm{~m})$ tall with a lattice frame. Data from instruments on the tower are sent to the Met Building which is located near the tower.

The meteorological tower is designed to be capable of withstanding wind speeds of up to 100 $\mathrm{mph}(44.7 \mathrm{~m} / \mathrm{sec})$.

### 2.3.3.1.3 Instrumentation

The tower instrumentation consists of wind speed, wind direction, and duplicate sets of aspirated temperature sensors located at $197 \mathrm{ft}(60 \mathrm{~m})$ and $33 \mathrm{ft}(10 \mathrm{~m})$ above ground level. A tipping bucket rain gauge is located approximately $30 \mathrm{ft}(9.1 \mathrm{~m})$ from the meteorological tower in an open field and a barometric pressure device is located in the Met Building. No moisture measurements (dew point or wet bulb temperature, relative humidity) are currently taken. Consequently, meteorological data needed in the analysis of the Ultimate Heat Sink and potential plumes from cooling tower operation will be taken from other sources as described in Section 2.3.1.

CCNPP replaced their meteorological monitoring instrumentation in December 2005. The specifications of the previous instrumentation met or exceeded the accuracy and resolution requirements of Regulatory Guide 1.23 Revision 1 (NRC, 2007).

The instruments are positioned on the meteorological tower in accordance with the guidance in Regulatory Guide 1.23, Revision 1 (NRC, 2007).

Table 2.3-108 provides the current meteorological instrument accuracy and resolution and compares them with regulatory guidance provided in Regulatory Guide 1.23, Revision 1, (NRC, 2007).

Signals from the sensors are collected and processed by two data loggers. Each data logger collects the data from the meteorological tower, and performs calculations of average values, wind direction sigma theta, and temperature difference between the $197 \mathrm{ft}(60 \mathrm{~m})$ and $33 \mathrm{ft}(10$ m ) levels of the meteorological tower. The primary data logger sends the averaged data values to a personal computer ( PC ) that is dedicated to the meteorological measurement system. This PC is located in the Met Building and includes a printer for data output. The backup data logger is connected to a dial-up modem, which provides the capability for remote retrieval of meteorological data. The primary data logger and plant equipment are isolated from the telephone connection to the backup data logger.

### 2.3.3.1.4 Instrument Maintenance and Surveillance Schedules

The meteorological instruments are inspected and serviced at a frequency that assures at least a $90 \%$ data recovery rate for all parameters, including the combination of wind speed, wind direction, and delta temperature. The instrumentation specified in Regulatory Guide 1.23, Revision 1 are channel checked on a daily basis and instrument calibrations are performed semi-annually.

System calibrations encompass the entire data channel for each instrument, including recording devices and displays (those located at the tower, in emergency response facilities, and those used to compile the historical data set). The system calibrations are performed by either a series of sequential, overlapping, or total channel steps.

### 2.3.3.1.5 Data Reduction and Compilation

Wind and temperature data are averaged over 15 minute periods. The data loggers employ a validation mode that monitors the various sensors and activates alarms as necessary. The validation mode compares the data values from the $33 \mathrm{ft}(10 \mathrm{~m})$ and $197 \mathrm{ft}(60 \mathrm{~m})$ levels of the tower. The data loggers perform a daily check of the processor cards and will alarm if values are outside of specified limits.

Averaged data values from the data loggers are collected by the meteorological software, along with maximum and minimum values of ambient temperature and wind direction variance (sigma-theta). Hourly data values are determined from the 15 minute averaged values. Output options include various functions and averages as well as graphical displays.

The 15 minute averaged data are available for use in the determination of magnitude and continuous assessment of the impact of releases of radioactive materials to the environment during a radiological emergency (as required in 10 CFR 50.47 (CFR, 2007a) and 10 CFR 50 Appendix E (CFR, 2007b)). The hourly averaged data are available for use in:

1. Determining radiological effluent release limits associated with normal operations to ensure these limits are met for any individual located offsite.
2. Determining radiological dose consequences of postulated accidents meet prescribed dose limits at the Exclusion Area Boundary (EAB) and Low Population Zone (LPZ).
3. Evaluating personnel exposures in the control room during radiological and airborne hazardous material accident conditions.
4. Determining compliance with numerical guides for design objectives and limiting conditions for operation to meet the requirement that radioactive material in effluents released to unrestricted areas be kept as low as is reasonably achievable.
5. Determining compliance with dose limits for individual members of the public.

Annual summaries of meteorological data in the form of joint frequency distributions of wind speed and wind direction by atmospheric stability class are maintained onsite and are available upon request.

A summary of the 2000 through 2005 onsite meteorological data in the form of joint frequency distributions of wind speed and wind direction by atmospheric stability class are presented in Section 2.3.2. Wind roses (graphical depictions of joint frequency distribution tables) summarizing data from 1984 to 1992 for three National Weather Service (NWS) sites are also presented in Section 2.3.2.

A comparison of the CCNPP site and the Norfolk, Virginia data (of the three NWS sites, the Norfolk, Virginia site is closest to the Chesapeake Bay) reveals that both sites have the same prevailing wind direction - wind from the south-southwest. For the south-southwest wind direction, the wind speed is between 6.9 and 17.9 mph ( $3.1 \mathrm{and} 8.0 \mathrm{~m} / \mathrm{sec}$ ) approximately $5 \%$ of the time at the CCNPP site and the wind speed is between 7.6 and 24.6 mph ( 3.4 and 11.0 $\mathrm{m} / \mathrm{sec}$ ) approximately $9 \%$ of the time at the Norfolk, Virginia site. The most prevalent wind speed class at the CCNPP site, 4.7 to 6.7 mph ( 2.1 to 3.0 mps ), occurs approximately $28 \%$ of the time. The most prevalent wind speed class at the Norfolk, Virginia site, 7.6 to 12.5 mph ( 3.4 to 5.6 mps ), occurs approximately $36 \%$ of the time. These results indicate that the CCNPP onsite data also represent long-term conditions at the site.

A summary of the 2000 through 2005 onsite meteorological data in the form of joint frequency distributions of wind speed and wind direction by atmospheric stability class are presented in Section 2.3.2. Wind roses (graphical depictions of joint frequency distribution tables) summarizing data from 1984 to 1992 for three National Weather Service (NWS) sites are also presented in Section 2.3.2. A discussion of onsite temperature measurements compared to surrounding offsite data sources is provided in Section 2.3.2.1.2.

### 2.3.3.1.6 Nearby Obstructions to Air Flow

Downwind distances from the meteorological tower to nearby (within $0.5 \mathrm{mi}(0.8 \mathrm{~km})$ ) obstructions to air flow were determined using U.S. Geological Survey topographical maps. Highest terrain is to the north and north-northwest. Lowest terrain is to the northeast, east-northeast, and east (Chesapeake Bay). Table 2.3.3-22.3-109 presents the distances to nearby obstructions to air flow in each downwind sector.

The two tallest U.S. EPR structures are the Reactor Building and the Turbine Building. The Turbine Building is also the closest major building to the meteorological tower. Both buildings
will be at a finished grade of approximately 83 feet ( 25 m ) above mean seal level (MSL). Grade at the meteorological tower is approximately 125 feet $(38 \mathrm{~m}) \mathrm{MSL}$.
U.S. EPR buildings are greater than a factor of ten times their respective heights away from the meteorological tower, and as such are not expected to impact the meteorological measurements.

Specific information regarding existing nearby structures and CCNPP Unit 3 buildings.

| Building | Height | Distance to <br> Meteorological Tower |
| :--- | :---: | :---: |
| CCNPP Unit 3 Reactor Building | $62 \mathrm{~m}(203 \mathrm{ft})$ above grade | $850 \mathrm{~m}(2789 \mathrm{ft})$ |
| CCNPP Unit 3 Turbine Building | $55 \mathrm{~m}(180 \mathrm{ft})$ estimated | $773 \mathrm{~m}(2535 \mathrm{ft})$ |
| ISFSI for CCNPP Units 1 and 2 | $7 \mathrm{~mm}(23 \mathrm{ft})$ estimated | $206 \mathrm{~m}(676 \mathrm{ft})$ |

Routine checks of the meteorological data have indicated that the ISFSI for CCNPP Units 1 and 2 has had no impact on meteorological measurements.

From the information provided above and in Table 2.3-109 and Figures 2.3-215 and 2.3-216, it is concluded there are no significant nearby obstructions to airflow.

### 2.3.3.1.7 Deviations to Guidance from Regulatory Guide 1.23

The pre-operational meteorological monitoring program for CCNPP Unit 3 complies with Regulatory Guide 1.23, Revision 1 (NRC, 2007), except as follows. No atmospheric moisture measurements are taken. Atmospheric moisture data needed in the analysis of the CCNPP Unit 3 Ultimate Heat Sink and potential plumes from CCNPP Unit 3 cooling tower operation will be taken from other sources as described in Section 2.3.1. In addition, the meteorological tower is not sited at approximately the same elevation as finished CCNPP Unit 3 grade. This was done in order to assure that the meteorological tower is located on level, open terrain at a distance at least 10 times the height of any nearby obstruction that exceeds one-half the height of the wind measurement (i.e., the tower is located far enough away from CCNPP Unit 3 structures and topographical features to avoid airflow modifications). Further discussion is provided in Section 2.3.3.1.1.

The tower, guyed wire, and anchor inspections are performed once every 5 years instead of an annual inspection for tower and guyed wire and an anchor inspection of once every 3 years as provided in Regulatory Guide 1.23, Revision 1 (NRC, 2007). Note that this was not a requirement stipulated in Safety Guide 23 (NRC, 1972).

### 2.3.3.2 Operational Meteorological Measurement Program

The operational meteorological measurement program for CCNPP Unit 3 is based on the operational meteorological measurement program for CCNPP Units 1 and 2 with the addition of revised operational procedures. This program was designed according to the guidance provided in Safety Guide 23 (NRC, 1972) and has been upgraded for CCNPP Unit 3 to comply with Regulatory Guide 1.23, Revision 1 (NRC, 2007).

### 2.3.3.2.1 Tower Location

The meteorological tower for the CCNPP site is located in an open field off Calvert Cliffs Parkway north of the CCNPP Units 1 and 2 ISFSI. The elevation at the base of the tower is approximately $125 \mathrm{ft}(38 \mathrm{~m})$ above mean sea level. Figure 2.3-219 shows the location of the meteorological tower as well as the topography of the CCNPP site. The tower is sited according
to the guidance provided in Regulatory Guide 1.23, Revision 1 (NRC, 2007). Figure 2.3-220 shows the general topographic features of the region.

The meteorological tower is located on level, open terrain at a distance at least 10 times the height of any nearby obstruction that exceeds one-half the height of the wind measurement; i.e., the tower is located far enough away from CCNPP Unit 3 structures and topographical features to avoid airflow modifications. The terrain height difference between the meteorological tower and the CCNPP Unit 3 reactor area is approximately 40 ft ( 12 m ). The distance between the meteorological tower and the CCNPP Unit 3 reactor is approximately 2,789 feet ( 850 m ). Therefore, the terrain profile has a very gentle slope and has an insignificant impact on site dispersion conditions.

### 2.3.3.2.2 Tower Design

The meteorological tower is $197 \mathrm{ft}(60 \mathrm{~m})$ tall with a lattice frame. Data from instruments on the tower are sent to the Met Building which is located near the tower. The primary meteorological tower is designed to be capable of withstanding wind speeds of up to $100 \mathrm{mph}(44.7 \mathrm{~m} / \mathrm{sec})$.

### 2.3.3.2.3 Instrumentation

The tower instrumentation consists of wind speed, wind direction, and duplicate sets of aspirated temperature sensors located at $197 \mathrm{ft}(60 \mathrm{~m})$ and $33 \mathrm{ft}(10 \mathrm{~m})$ above ground level. A tipping bucket rain gauge is located approximately $30 \mathrm{ft}(9.1 \mathrm{~m})$ from the meteorological tower in an open field and a barometric pressure device is located in the Met Building.

The instruments are positioned on the meteorological tower in accordance with the guidance in Regulatory Guide 1.23, Revision 1 (NRC, 2007).

Table 2.3-108 presents meteorological instrument specifications and compares them with regulatory guidance provided in Regulatory Guide 1.23, Revision 1 (NRC, 2007).

Signals from the sensors are collected and processed by two data loggers. Each data logger collects the data from the meteorological tower, and performs calculations of average values, wind direction sigma theta, and temperature difference between the $197 \mathrm{ft}(60 \mathrm{~m})$ and 33 ft ( 10 m ) levels of the meteorological tower. The primary data logger sends the averaged data values to a personal computer ( PC ) that is dedicated to the meteorological measurement system. This PC is located in the Met Building and includes a printer for data output. The backup data logger is connected to a dial-up modem, which provides the capability for remote retrieval of meteorological data. The primary data logger and plant equipment are isolated from the telephone connection to the backup data logger. In addition, the averaged data values are transmitted to the appropriate locations for operational and emergency response purposes (CCNPP Unit 3 Control Room, Technical Support Center, Emergency Operations Facility) and shall be submitted to the NRC's Emergency Response Data System as provided for in Section VI of Appendix E to 10 CFR Part 50 (CFR, 2007b).

### 2.3.3.2.4 Instrument Maintenance and Surveillance Schedules

The meteorological instruments are inspected and serviced at a frequency that assures at least a $90 \%$ data recovery rate for all parameters, including the combination of wind speed, wind direction, and delta temperature. The instrumentation specified in Regulatory Guide 1.23, Revision 1 (NRC, 2007) are channel checked on a daily basis and instrument calibrations are performed semi-annually.

System calibrations encompass the entire data channel for each instrument, including recording devices and displays (those located at the tower, in emergency response facilities, and those used to compile the historical data set). The system calibrations are performed by either a series of sequential, overlapping, or total channel steps.

### 2.3.3.2.5 Data Reduction and Compilation

Wind and temperature data are averaged over 15 minute periods. The data loggers employ a validation mode that monitors the various sensors and activates alarms as necessary. The validation mode compares the data values from the $33 \mathrm{ft}(10 \mathrm{~m})$ and $197 \mathrm{ft}(60 \mathrm{~m}$ ) levels of the tower. The data loggers perform a daily check of the processor cards and will alarm if values are outside of specified limits.

Averaged data values from the data loggers are collected by the meteorological software, along with maximum and minimum values of ambient temperature and wind direction variance (sigma-theta). Hourly data values are determined from the 15 minute averaged values. Output options include various functions and averages as well as graphical displays.

The 15 minute averaged data are available for use in the determination of magnitude and continuous assessment of the impact of releases of radioactive materials to the environment during a radiological emergency (as required in 10 CFR 50.47 (CFR, 2007a) and 10 CFR 50 Appendix E (CFR, 2007b)). The hourly averaged data are available for use in:

1. Determining radiological effluent release limits associated with normal operations to ensure these limits are met for any individual located offsite.
2. Determining radiological dose consequences of postulated accidents meet prescribed dose limits at the EAB and LPZ.
3. Evaluating personnel exposures in the control room during radiological and airborne hazardous material accident conditions.
4. Determining compliance with numerical guides for design objectives and limiting conditions for operation to meet the requirement that radioactive material in effluents released to unrestricted areas be kept as low as is reasonably achievable.
5. Determining compliance with dose limits for individual members of the public.

Annual summaries of meteorological data in the form of joint frequency distributions of wind speed and wind direction by atmospheric stability class are maintained onsite and are available upon request.

A summary of the 2000 through 2005 onsite meteorological data in the form of joint frequency distributions of wind speed and wind direction by atmospheric stability class is presented in Section 2.3.2.

Wind roses (graphical depictions of joint frequency distribution tables) summarizing data from 1984 to 1992 for three NWS sites are also presented in Section 2.3.2.

A comparison of the CCNPP site and the Norfolk, Virginia data (of the three NWS sites, the Norfolk, Virginia site is closest to the Chesapeake Bay) reveals that both sites have the same prevailing wind direction - wind from the south-southwest. For the south-southwest wind direction, the wind speed is 6.9 to $17.9 \mathrm{mph}(3.1$ to 8.0 mps ) approximately $5 \%$ of the time at
the CCNPP site and the wind speed is 7.6 to 24.6 mph ( 3.4 to 11.0 mps ) approximately $9 \%$ of the time at the Norfolk, Virginia site. The most prevalent wind speed class at the CCNPP site, 4.7 to 6.7 mph ( 2.1 to 3.0 mps ), occurs approximately $28 \%$ of the time. The most prevalent wind speed class at the Norfolk, Virginia site, 7.6 to 12.5 mph ( 3.4 to 5.6 mps ), occurs approximately $36 \%$ of the time. These results indicate that the CCNPP onsite data also represent long-term conditions at the site.

### 2.3.3.2.6 Nearby Obstructions to Air Flow

Downwind distances from the meteorological tower to nearby (within $0.5 \mathrm{mi}(0.8 \mathrm{~km})$ ) obstructions to air flow were determined using U.S. Geological Survey topographical maps. Highest terrain is to the north and north-northwest. Lowest terrain is to the northeast, east-northeast, and east (Chesapeake Bay). Table 2.3-109 presents the distances to nearby obstructions to air flow in each downwind sector.

From the information provided in Section 2.3.3.1.6, Section 2.3.3.2.1, Table 2.3-109, Figure 2.3-219, and Figure 2.3-220 and with the knowledge that the base of the tower is at an elevation of approximately $125 \mathrm{ft}(38 \mathrm{~m})$, it can be seen that there are no significant nearby obstructions to airflow.

### 2.3.3.2.7 Deviations to Guidance from Regulatory Guide 1.23

The meteorological tower is not sited at approximately the same elevation as finished plant grade. This was done in order to assure that the meteorological tower is located on level, open terrain at a distance at least 10 times the height of any nearby obstruction that exceeds one-half the height of the wind measurement; i.e., the tower is located far enough away from CCNPP Unit 3 structures and topographical features to avoid airflow modifications. Further discussion is provided in Sections 2.3.3.1.6 and 2.3.3.2.1.

### 2.3.3.3 References

CFR, 2007a. Emergency Plans, Title 10, Code of Federal Regulations, Part 50.47, 2007.
CFR, 2007b. Emergency Planning and Preparedness for Production and Utilization Facilities, Title 10, Code of Federal Regulations, Part 50, Appendix E, 2007.

NRC, 1972. Onsite Meteorological Programs, Safety Guide 23 (Regulatory Guide 1.23, Revision 0), U.S. Nuclear Regulatory Commission, February 1972.

NRC, 2007. Meteorological Monitoring Programs for Nuclear Power Plants, Regulatory Guide 1.23, Revision 1, U.S. Nuclear Regulatory Commission, March 2007.\}

### 2.3.4 SHORT TERM ATMOSPHERIC DISPERSION ESTIMATES FOR ACCIDENT RELEASES

The U.S. EPR FSAR includes the following COL Items in Section 2.3.4:
A COL applicant that references the U.S. EPR design certification will confirm that site-specific $\chi / Q$ values, based on site-specific meteorological data, are bounded by those specified in Table 2.1-1 at the EAB and LPZ and by Table 2.3-1 at the control room.

For site-specific $\chi / \mathrm{Q}$ values that exceed the bounding $\chi / \mathrm{Q}$ values, a COL applicant that references the U.S. EPR design certification will demonstrate that the radiological consequences associated with the controlling design basis accident continue to meet the
dose reference values given in 10 CFR Part 50.34 and the control room operator dose limits given in GDC 19 using site-specific $\chi / Q$ values.

A COL applicant that references the U.S. EPR design certification will provide a description of the atmospheric dispersion modeling used in evaluating potential design basis events to calculate concentrations of hazardous materials (e.g., flammable or toxic clouds) outside building structures resulting from the onsite and/or offsite airborne releases of such materials.

A COL applicant that references the U.S. EPR design certification will provide $\chi / \mathrm{Q}$ values for each cumulative frequency distribution which exceeds the median value ( 50 percent of the time) as part of the assessment of the postulated impact of an accident on the environment.

These COL Items are addressed as follows:
\{These COL Items are addressed in Section 2.3.4.2.1 through 2.3.4.3.
Sections 2.3.4.1 through 2.3.4.4 are added as a supplement to the U.S. EPR FSAR.

### 2.3.4.1 Objective

This section provides, for appropriate time periods up to 30 days after an accident, conservative estimates of atmospheric dispersion factors ( $\chi / Q$ ) values at the exclusion area boundary (EAB), at the outer boundary of the low population zone (LPZ), and at the control room for postulated accidental radioactive airborne releases. This section also addresses atmospheric dispersion modeling used in Section 2.2.3 to evaluate potential design basis events resulting from the onsite and/or offsite airborne releases of hazardous materials (e.g., flammable vapor clouds, toxic chemicals, and smoke from fires). A discussion of the anticipated effects of the Chesapeake Bay on atmospheric dispersion is provided in Section 2.3.5.4.

### 2.3.4.2 Calculations

### 2.3.4.2.1 Conservative Short-Term (Accident Release) Atmospheric Dispersion Estimates for EAB and LPZ

Short-term atmospheric dispersion estimate ( $\chi / \mathrm{Q}$ ) values at the Exclusion Area Boundary (EAB) and Low Population Zone (LPZ) are provided in Table 2.1-1 of the U.S. EPR FSAR. Conservative estimates of site-specific atmospheric dispersion for the CCNPP Unit 3 EAB and the outer boundary of the site-specific LPZ were determined using computer code AEOLUS3 version 1 and seven years of meteorological data (2000 through 2006) from the onsite monitoring program at the existing CCNPP Units 1 and 2.

Site-specific local meteorological data are described in Section 2.3.2.
AEOLUS3 was developed and validated by Entech Engineering. It implements the guidance in Regulatory Guide 1.145, "Atmospheric Dispersion Models for Potential Accident Consequence Assessments at Nuclear Power Plants," (NRC, 1982) for accidental releases. The code has been used in past licensing submittals and its results have been found to be acceptable (NRC, 2005).

AEOLUS3 operates in a batch-input mode with various options that are user selectable. The program is based on a straight-line trajectory Gaussian plume model. The plume can be depleted by wet deposition, dry deposition, and radioactive decay. The computed
ground-level concentration can be modified to account for plume recirculation or stagnation. The program computes an effective plume height which accounts for physical release height, aerodynamic downwash, plume rise, and terrain heights. Other options include plume-meander effects and wind speed extrapolation.

Input details for AEOLUS3 version 1 are provided in Section 2.3.4.3
The determination of the site-specific atmospheric dispersion for the EAB and at the outer boundary of the LPZ complies with the guidance provided in Regulatory Guide 1.145, Revision 1, (NRC,1982) were made.

Conservative estimates of atmospheric dispersion for the EAB and the outer boundary of the LPZ for CCNPP Unit 3 are presented in Table 2.3-109110.

The values for the EAB and LPZ presented in Table 2.3-109110 are bounded by those in U.S. EPR FSAR Table 2.1-1 except for the 0-2 hr value for the LPZ. This represents a departure from the U.S. EPR FSAR. This departure and its associated justification are discussed in Section 15.0.3.

### 2.3.4.2.2 Realistic Short-Term (Accident Release) Atmospheric Dispersion Estimates for EAB and LPZ

Realistic estimates of the site-specific atmospheric dispersion for the CCNPP Unit 3 EAB and the outer boundary of the site-specific LPZ were determined using computer code AEOLUS3 and seven years of meteorological data (2000 through 2006) from the onsite monitoring program at the existing CCNPP Units 1 and 2 . Site-specific local meteorological data are described in Section 2.3.2.

In determining the $50^{\text {th }}$ Percentile $\chi / Q^{\prime}$ 's for Section 7.1 of the Environmental Report, use was made of the methodology in Sections 1.4 and 2.2 of Regulatory Guide 1.145 (NRC, 1982). In addition, the 0 to 2 hour $50^{\text {th }}$ percentile value, and the five percentile values for all accident time periods (determined using computer code AEOLUS3) and 7 years of onsite meteorological data from CCNPP Units 1 and 2 ( 2000 through 2006 were used), to determine the $50^{\text {th }}$ percentile 2 to 8 hour, 8 to 24 hour, 1 to 4 days, and 4 to 30 days time periods.

Regulatory Guide 1.145 (NRC, 1982) requires the following steps to be performed for computation of the accident atmospheric dispersion factors $(\chi / \mathrm{Q})$ at the LPZ:

1. The 2 hour accident $\chi / \mathrm{Q}$ and the annual average $\chi / \mathrm{Q}$ are determined for each sector at the outer LPZ boundary distances.
2. The two values for any given sector (the 2 hour accident $\chi / \mathrm{Q}$ and the annual average $\chi / Q)$ are plotted on a log-log graph, and values at other time intervals of interest are determined through logarithmic interpolation between these two points.
3. The time periods should be selected to represent appropriate meteorological time regimes (an 8 hour interval for releases during the first 8 hours of the postulated accident, a 16 hour interval for releases between 8 and 24 hours, a 3 day interval for releases between 1 and 4 days, and a 26 day interval for releases between 4 and 30 days).

Since the annual average $\chi / \mathrm{Q}$ is an integral part of the model for determination of accident $\chi / \mathrm{Q}$ values, it is possible to use the Regulatory Guide 1.145 (NRC, 1982) methodology in reverse order to determine the annual average $\chi / \mathrm{Q}$ which was used in the computation of the accident
$\chi / \mathrm{Q}$ values. The accident $\chi / \mathrm{Q}$ values and the annual average $\chi / \mathrm{Q}$ value should be on a straight line when plotted on a log-log graph. This was done and the $50^{\text {th }}$ percentile atmospheric dispersion factors were determined. These factors are presented in Table 2.3-115.

### 2.3.4.2.3 Short-Term (Accident Release) Atmospheric Dispersion Estimates for the Control Room

Short-term atmospheric dispersion estimates ( $\chi / \mathrm{Q}$ ) values estimated for the control room are provided in Table 2.3-1 of the U.S. EPR FSAR. Short-term atmospheric dispersion $\chi$ /Q estimates for unfiltered inleakage into the control room are provided in Table 2.3-2 of the U.S. EPR FSAR. Conservative estimates of the site-specific atmospheric dispersion for the control room were determined using computer code ARCON96 and seven years of meteorological data (2000 through 2006) from the onsite monitoring program at the existing CCNPP Units 1 and 2. The version of the ARCON96 code, i.e., version 1.0 which was used is the May 9, 1997 version which is endorsed in Regulatory Guide 1.194 (NRC, 2003). Site-specific local meteorological data are described in Section 2.3.2.

ARCON96 implements the guidance in Regulatory Guide 1.194, Atmospheric Relative Concentrations for Control Room Radiological Habitability Assessments at Nuclear Power Plants," (NRC, 2003). ARCON96 was specifically developed for the Nuclear Regulatory Commission (NRC, 1997). The determination of the site-specific atmospheric dispersion for the control room were made in compliance with the guidance provided in Regulatory Guide 1.194, Revision 0, (NRC, 2003) were made.

Input details for ARCON96 are provided in Table 2.3-117.
Conservative site-specific estimates of atmospheric dispersion for the CCNPP Unit 3 control room are presented in Table 2.3-110 through Table 2.3-114. The values for the control room presented in Table 2.3-110 through Table 2.3-114 are bounded by those in Table 2.3-1 within the U.S. EPR FSAR. The same meteorological data are used to calculate unfiltered $\chi / \mathrm{Q}$ values. Since the site-specific control room $\chi / Q$ values were demonstrated to be bounded by the U.S. EPR $\chi / Q$ values, the calculation of site-specific atmospheric dispersion factors for unfiltered inleakage was not necessary. CCNPP Unit 3 incorporates by reference the doses for the main control room presented in the U.S. EPR FSAR.
U.S. EPR FSAR Table 2.3-1 provides the locations of potential accident release pathways and their relationship to the control room, and Figures 2.1-1 and 2.3-221 provide the CCNPP site plan and control room location.

### 2.3.4.2.4 Atmospheric Dispersion Modeling for Hazardous Materials

The description of the atmospheric modeling used in the evaluation of potential design basis events to calculate concentration of hazardous material is provided in Section 2.2.3.1.

### 2.3.4.3 Input Details for Computer Codes AEOLUS3 (Version 1)

Assumptions made for AEOLUS3 modeling:

- Ground level release was assumed.
- Since a ground level release was assumed, the release point and receptor elevations were assumed to be the same.
- For EAB/LPZ atmospheric dispersion factors for DBAs, all post-accident release points were based on the ground level release model with no dispersion credit for building wake effects. However, plume meander, which predominates building wake effects during short time intervals, is accounted for.
- For the offsite receptors, accident atmospheric dispersion factors were calculated for a set of distances ranging from 0.25 mile to 5 miles. Bounding distances were selected based on actual site characteristics.
- For normal effluent analysis, receptor locations between distances at which terrain heights were determined using USGS topographical maps were assigned the maximum of the two values.

Specific input parameters and values are provided in Table 2.3-116.

### 2.3.4.4 References

NRC, 1977. Methods for Estimating Atmospheric Transport and Dispersion of Gaseous Effluents in Routine Releases from Light-Water-Cooled Reactors, Regulatory Guide 1.111, Revision 1, U.S. Nuclear Regulatory Commission, July 1977.

NRC, 1982. Atmospheric Dispersion Models for Potential Accident Consequence Assessments at Nuclear Power Plants, Regulatory Guide 1.145, Revision 1, U.S. Nuclear Regulatory Commission, November 1982.

NRC, 1997. Atmospheric Relative Concentrations in Building Wakes, NUREG/CR-6331, U.S. Nuclear Regulatory Commission, May 1997.

NRC, 2003. Atmospheric Relative Concentrations for Control Room Radiological Habitability Assessments at Nuclear Power Plants, Regulatory Guide 1.194, Revision 0, U.S. Nuclear Regulatory Commission, June 2003.

NRC, 2005. Letter NRC (Boska) to Entergy (Kansler), Pilgrim Nuclear Power Station, Issuance of Amendment (215), NRC Adams Accession Number ML 051040065, Dated April 28, 2005.\}

### 2.3.5 LONG-TERM ATMOSPHERIC DISPERSION ESTIMATES FOR ROUTINE RELEASES

The U.S. EPR FSAR includes the following COL Items in Section 2.3.5:
A COL applicant that references the U.S. EPR design certification will provide the site-specific, long-term diffusion estimates for routine releases. In developing this information, the COL applicant should consider the guidance provided in Regulatory Guides $1.23,1.109,1.111$, and 1.112 . The maximum annual average $\chi / \mathrm{Q}$ value at the site boundary, provided in Table 2.1-1, is used to calculate radionuclide concentrations associated with routine gaseous effluent releases, addressed in Section 11.3, for comparison with environmental release limits and dose limits given in 10 CFR Part 20. If a reactor site has an annual average $\chi / \mathrm{Q}$ value that exceeds the reference value, then a site-specific evaluation will be performed.

A COL applicant that references the U.S. EPR design certification will also provide estimates of annual average atmospheric dispersion ( $\chi / \mathrm{Q}$ values) and deposition ( $\mathrm{D} / \mathrm{Q}$ values) for 16 radial sectors to a distance of $50 \mathrm{mi}(80 \mathrm{~km})$ from the plant as part of its environmental assessment.

These COL Items are addressed as follows:
\{Sections 2.3.5.1 through 2.3.5.5 are added as a supplement to U.S. EPR FSAR.

### 2.3.5.1 Objective

This section provides realistic estimates of annual average atmospheric dispersion ( $\chi / \mathrm{Q}$ values) and deposition (D/Q values) to a distance of $50 \mathrm{mi}(80 \mathrm{~km})$ for annual average release limit calculations and person-rem estimates.

### 2.3.5.2 Calculations

Realistic estimates of site-specific annual average atmospheric transport and diffusion characteristics were determined using computer code AEOLUS3 version 1 and seven years of meteorological data (2000 through 2006) from the onsite monitoring program at the existing Calvert Cliffs Nuclear Power Plant (CCNPP) Units 1 and 2. Site-specific local meteorological data are described in Section 2.3.2.

AEOLUS3 was developed and validated by Entech Engineering. It implements the methodology of Regulatory Guide 1.111, "Methods for Estimating Atmospheric Transport and Dispersion of Gaseous Effluents in Routine Releases from Light-Water-Cooled Reactors," Revision 1, (NRC, 1977a) for routine releases. The code has been used in past licensing submittals and its results have been found to be acceptable (NRC, 2005).

AEOLUS3 operates in a batch-input mode with various options that are user selectable. The program is based on a straight-line trajectory Gaussian plume model. The plume can be depleted by wet deposition, dry deposition, and radioactive decay. The computed ground-level concentration can be modified to account for plume recirculation or stagnation. The program computes an effective plume height which accounts for physical release height, aerodynamic downwash, plume rise, and terrain heights. Other options include plume-meander effects and wind speed extrapolation.

AEOLUS3 produces the following dispersion parameters: the concentration $\chi / \mathrm{Q}$, which is used for the determination of airborne concentrations and inhalation doses at offsite receptors of interest as well as gamma air doses; the gamma $\chi / \mathrm{Q}$, which may be employed in the computation of external gamma radiation from the ensuing finite clouds of radioactive material; and the deposition factor $D / Q$, which is used as a measure of the relative deposition of released radioactivity. Doses calculated due to postulated normal effluents from CCNPP Unit 3 made use of the concentration $\chi / \mathrm{Q}$ and deposition factor $\mathrm{D} / \mathrm{Q}$ values. The gamma $\chi / \mathrm{Q}$ values, while not used to determine normal effluent doses for CCNPP Unit 3, represent an alternative methodology to determine gamma air doses.

AEOLUS3 computes plume standard deviations in the horizontal and vertical dimensions $\sigma_{y}$ and $\sigma_{z}$ respectively) using the analytical expressions from the Nuclear Regulatory Commission-sponsored computer program XOQDOQ. The onsite meteorological data used in the dispersion analysis has been shown to be representative of the region as discussed in Section 2.3.2. Thus, the atmospheric dispersion and deposition factors determined by AEOLUS3 from the site boundary to a radius of $50 \mathrm{mi}(80 \mathrm{~km})$ from the plant are appropriate for use in estimating the consequences of routine releases for CCNPP Unit 3.

Meteorological data summaries used as input to AEOLUS3 are provided in Section 2.3.2. The regulatory guidance described in Regulatory Guide 1.23, Revision 1 (NRC, 2007), was followed in the determination of appropriate onsite meteorological data. The regulatory guidance
described in Regulatory Guide 1.112 (NRC, 1977c) was followed in the determination of points of routine release of radioactive materials to the atmosphere and their characteristics. The regulatory guidance described in Regulatory Guide 1.109, Revision 1 (NRC, 1977b), was followed in the determination of potential receptors of interest.

AEOLUS3 implements the guidance in Regulatory Guide 1.145, Revision 1 (NRC, 1982) and Regulatory Guide 1.111, Revision 1 (NRC, 1977a).

The atmospheric transport and diffusion models used to determine the long-term atmospheric dispersion estimates for routine releases for CCNPP Unit 3 comply with the guidance provided in Regulatory Guide 1.111, Revision 1, (NRC, 1977a).

A mixed mode release from the CCNPP Unit 3 stack was modeled to determine routine release normal effluent atmospheric dispersion and deposition factors. Table 2.3-1 of the U.S. EPR FSAR indicates the location of the stack. As previously stated, seven years of meteorological data (2000 through 2006) from the onsite monitoring program at CCNPP Units 1 and 2 were used in the analysis. In Section 2.3.2, joint frequency distributions of wind speed and wind direction as a function of atmospheric stability class were determined using two sets of meteorological data from the on-site monitoring program: 2001-2005 and 2001-2006 (which included the most recent year of meteorological data). Since the differences in annual average atmospheric dispersion factor values seen when the 2006 meteorological data were included ranged from $-3.4 \%$ to $6.8 \%$ over downwind distances from 0.5 to 50 miles, the impact of the difference in data sets is not significant.

Credit for building wake effect was taken. The release point was $203 \mathrm{ft}(62 \mathrm{~m}$ ) above grade ( 6.6 $\mathrm{ft}(2 \mathrm{~m})$ above the Reactor Building). The gamma energy spectrum and relative intensity were set to 0.3 MeV and $1.0 \mathrm{MeV} / \mathrm{sec}$, respectively. The 0.3 MeV value was determined to provide the maximum gamma $\chi / Q$ values by running test cases using other gamma energy spectrum values. Terrain height values for downwind receptor locations were determined using topographic maps from the U.S. Geological Survey. The annual average height of the inversion layer and the maximum allowable plume centerline height were set to $2,454 \mathrm{ft}(748 \mathrm{~m})$. This value was determined from mixing height data from the National Climatic Data Center. A stack flow rate of $242,458 \mathrm{ft}^{3} / \mathrm{min}(6,865,646 \mathrm{I} / \mathrm{min})$ was used; this is a conservative value, since the actual flow rate for normal operations will be higher.

Specific input parameters and values are provided in Tables 2.3-116 and 2.3-117.
Table 2.3-118119 through Table 2.3-125129 present the site-specific normal effluent annual average atmospheric dispersion and deposition factors for a mixed mode release from the CCNPP Unit 3 stack. Locations of interest (i.e., site boundary, nearest resident, nearest garden) were derived from the annual CCNPP site land use census, and from regulatory guidance.

The specific locations of the potential receptors of interest are provided in Table 2.3-126130. At the time of the analysis, there were no meat cow or milk animal receptors reported within 5 mi $(8 \mathrm{~km})$ of the plant.

The maximum site-specific annual average $\chi / \mathrm{Q}$ and $\mathrm{D} / \mathrm{Q}$ values at the EAB boundary are $5.039 \mathrm{E}-06 \mathrm{sec} / \mathrm{m}^{3}$ and $3.7921 \mathrm{E}-081 / \mathrm{m}^{2}$, respectively. This represents a departure from the U.S. EPR FSAR. The maximum annual average $x / Q$ at the EAB boundary exceeds the value $4.973 \mathrm{E}-6 \mathrm{sec} / \mathrm{m}^{3}$ presented in Table 2.1-1 within the U.S. EPR FSAR. The site-specific evaluation of this departure is provided in Section 2.3.5.3.

### 2.3.5.3 Site-Specific Evaluation of Maximum Annual Average $\chi / Q$

A review of CCNPP Unit 3 Environmental Report, Table 5.4-6, "Distance to Nearest Gaseous Dose Receptors," indicates that the NE sector of the Exclusion Area Boundary (EAB) ( 0.5 mi radius centered on Reactor Building) intersects with the Site Area Boundary ( 0.28 mi ) at the shoreline of Chesapeake Bay. The Maximum Annual Average $\chi / \mathrm{Q}$ value is computed at 0.5 miles which is located approximately 0.22 miles offshore in the Chesapeake Bay. As presented in Table 2.3-118, all other Sectors annual average $\chi / \mathrm{Q}$ value at 0.5 miles are bounded by the maximum annual average $\chi / \mathrm{Q}$ value provided in U.S. EPR FSAR Table 2.1-1.

The justification for exceeding the Maximum Annual Average for Atmospheric Dispersion Factor $\chi / \mathrm{Q}$ value of $\leq 4.973 \mathrm{E}-6 \mathrm{sec} / \mathrm{m}^{3}$ is as follows:

- There are no persons currently living within the EAB or on its boundary in the NE sector.
- The boundary of the EAB in the NE sector lies on Chesapeake Bay, therefore, the probability of anyone living on a watercraft 0.22 mi offshore for an extended period of time is extremely low.
- The plant licensee will have control over the point in the NE sector at which EAB and the Site Boundary intersect.

In summary, although the Maximum Annual Average $\chi$ /Q value for CCNPP Unit 3 exceeds the $\chi / \mathrm{Q}$ limiting value specified in Table 2.1-1 of the U.S. EPR FSAR, operation of CCNPP Unit 3 is justified for the following reasons:

- Persons will not be living within the sector of the Maximum Annual Average $\chi / \mathrm{Q}$ value.
- CCNPP Unit 3 will have control over persons living within the EAB and site boundary.
- All other Sectors' Maximum Annual Average $\chi$ /Q value is within the limiting value specified in Table 2.1-1 of the U.S. EPR FSAR.

As such, dose limits of 10 CFR 50 Appendix I for the maximally exposed individual will not be exceeded.

### 2.3.5.4 Anticipated Influence of Chesapeake Bay on Atmospheric Dispersion

Previous meteorological data have been obtained and studied to estimate diffusion over Chesapeake Bay relative to that over land during conditions of off-shore air flow (Slade, 1962). The study measured wind and air temperatures on both the west and east sides of the Chesapeake Bay as well as Bay water temperatures.

The study indicated that dispersion is generally poorer over the water than over the land due to the reduction of wind fluctuations over the comparatively smooth surface of Chesapeake Bay. The study also showed that the magnitude of the overwater dispersion is greatly influenced by the water-air temperature difference.

The actual concentration ratios derived varied widely and, as noted in the study, may be open to considerable argument because of the numerous simplifications made. Nonetheless, the study further noted that "it is likely that diffusion over rather small inland water bodies is different enough from that over the adjoining land to indicate that this difference should be
considered in environmental evaluations of the effects of shoreline and over water pollution sources."

As a result, it is expected that effluent plumes originating at CCNPP Unit 3 and moving over the Chesapeake Bay will experience less efficient atmospheric dispersion than plumes that stay over land. Although less, there still will be important dispersion before the plume reaches receptors at the closest point in Eastern Maryland across Chesapeake Bay, a distance of approximately 7 miles ( 11 km ). For example, the distance to the maximum concentration for a release from the CCNPP Unit 3 stack ( 62 meters above grade), under the most stable atmospheric conditions, is between 4 and 5 miles ( 6 and 8 km ), which is considerably less than the distance to the Eastern shoreline (Turner, 1970, Figure 3-9).

Since potential recirculation of normal effluent was accounted for in Section 2.3.5.2, it is concluded that the atmospheric dispersion information provided for CCNPP Unit 3 is deemed acceptable.

### 2.3.5.5 References

NRC, 1977a. Methods for Estimating Atmospheric Transport and Dispersion of Gaseous Effluents in Routine Releases From Light-Water-Cooled Reactors, Regulatory Guide 1.111, Revision 1, U.S. Nuclear Regulatory Commission, July 1977.

NRC, 1977b. Calculation of Annual Dose to Man from Routine Releases of Reactor Effluents for the Purpose of Evaluating Compliance with 10 CFR Part 50, Appendix I, Regulatory Guide 1.109, Revision 1, U.S. Nuclear Regulatory Commission, October 1977.

NRC, 1977c. Calculation of Releases of Radioactive Materials in Gaseous and Liquid Effluents from Light-Water-Cooled Power Reactors, Regulatory Guide 1.112, Revision 0-R, U.S. Nuclear Regulatory Commission, May 1977.

NRC, 1982. Atmospheric Dispersion Models for Potential Accident Consequence Assessments at Nuclear Power Plants, Regulatory Guide 1.145, Revision 1, U.S. Nuclear Regulatory Commission, November 1982.

NRC, 2005. Letter NRC (Boska) to Entergy (Kansler), Pilgrim Nuclear Power Station, Issuance of Amendment (215), U.S. ML 051040065, U.S. Nuclear Regulatory Commission, April 28, 2005.

NRC, 2007. Meteorological Monitoring Programs for Nuclear Power Plants, Regulatory Guide 1.23, Revision 1, U.S. Nuclear Regulatory Commission, October 2007.

Slade, 1962. Atmospheric Dispersion Over Chesapeake Bay, Monthly Weather Review, David Slade, pp. 217-224, June 1962.

Turner, 1970. Workbook of Atmospheric Dispersion Estimates, Bruce Turner, U.S. Environmental Protection Agency, 1970.\}

### 2.3.6 REFERENCES

No departures or supplements.

Table 2.3-1—\{National Ambient Air Quality Standards\}

| Pollutant | Primary Standards | Averaging Times | Secondary <br> Standards |
| :---: | :---: | :---: | :---: |
| Carbon Monoxide | 9 ppm $\left(10 \mathrm{mg} / \mathrm{m}^{3}\right)$ | 8 hour $^{(1)}$ | None |
|  | $\begin{gathered} 35 \mathrm{ppm} \\ \left(40 \mathrm{mg} / \mathrm{m}^{3}\right) \end{gathered}$ | 1 hour $^{(1)}$ | None |
| Lead | $1.5 \mu \mathrm{~g} / \mathrm{m}^{3}$ | Quarterly Average | Same as Primary |
| Nitrogen Dioxide | $\begin{gathered} 0.053 \mathrm{ppm} \\ \left(100 \mu \mathrm{~g} / \mathrm{m}^{3}\right) \end{gathered}$ | Annual (Arithmetic Mean) | Same as Primary |
| Particulate Matter ( $\mathrm{PM}_{10}$ ) | Revoked ${ }^{(2)}$ | Annual ${ }^{(2)}$ (Arithmetic Mean) |  |
|  | $150 \mu \mathrm{~g} / \mathrm{m}^{3}$ | 24 hour ${ }^{(3)}$ |  |
| Particulate Matter ( $\mathrm{PM}_{2.5}$ ) | $15.0 \mu \mathrm{~g} / \mathrm{m}^{3}$ | Annual ${ }^{(4)}$ (Arithmetic Mean) | Same as Primary |
|  | $35 \mu \mathrm{~g} / \mathrm{m}^{3}$ | 24 hour ${ }^{(5)}$ |  |
| Ozone | 0.08 ppm | 8 hour $^{(6)}$ | Same as Primary |
|  | 0.12 ppm | 1 hour $^{(7)}$ (Applies only in limited areas) | Same as Primary |
| Sulfur Oxides | 0.03 ppm | Annual <br> (Arithmetic Mean) | ------- |
|  | 0.14 ppm | 24 hour ${ }^{(1)}$ | ------- |
|  | ------- | 3 hour ${ }^{(1)}$ | $\begin{gathered} 0.5 \mathrm{ppm} \\ \left(1,300 \mu \mathrm{~g} / \mathrm{m}^{3}\right) \end{gathered}$ |

## Notes:

(1) Not to be exceeded more than once per year.
(2) Due to a lack of evidence linking health problems to long-term exposure to coarse particle pollution, the agency revoked the annual PM ${ }_{10}$ Standard in 2006 (effective December 17, 2006).
(3) Not to be exceeded more than once per year on average over three years.
(4) To attain this standard, the three year average of the weighted annual mean $\mathrm{PM}_{2.5}$ concentrations from single or multiple community-oriented monitors must not exceed $15.0 \mu \mathrm{~g} / \mathrm{m}^{3}$.
(5) To attain this standard, the three year average of the 98 th percentile of 24 hour concentrations at each population-oriented monitor within an area must not exceed $35 \mu \mathrm{~g} / \mathrm{m}^{3}$ (effective December 17, 2006).
(6) To attain this standard, the three year average of the fourth-highest daily maximum 8 hour average ozone concentrations measured at each monitor within an area over each year must not exceed 0.08 ppm .
(7) (a)The standard is attained when the expected number of days per calendar year with maximum hourly average concentrations above 0.12 ppm is $<1$, as determined by Appendix H .
(b)As of June 15, 2005 EPA revoked the 1 hour ozone standard in all areas except the fourteen 8 hour ozone nonattainment Early Action Compact Areas.

Table 2.3-2—\{Total and Average Numbers of Tropical Storms and Hurricanes\}

| Month | Tropical Storms ${ }^{(1)}$ |  | Hurricanes |  | U.S. Hurricanes |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Average | Total | Average | Total | Average |
| January-April | 5 | * | 1 | * | 0 | 0.00 |
| May | 18 | 0.1 | 4 | * | 0 | 0.00 |
| June | 76 | 0.5 | 28 | 0.2 | 19 | 0.12 |
| July | 94 | 0.6 | 47 | 0.3 | 23 | 0.15 |
| August | 336 | 2.2 | 214 | 1.4 | 74 | 0.48 |
| September | 448 | 2.9 | 309 | 2.0 | 102 | 0.67 |
| October | 273 | 1.8 | 154 | 1.0 | 50 | 0.33 |
| November | 58 | 0.4 | 38 | 0.2 | 5 | 0.03 |
| December | 8 | 0.1 | 4 | * | 0 | 0.00 |
| Year | 1,316 | 8.5 | 799 | 5.2 | 273 | 1.78 |
| Notes: <br> (1) Includes subtropical storms after 1967. <br> * Less than 0.05 . |  |  |  |  |  |  |

Table 2.3-3—\{Monthly Mean Number of Days with Thunderstorms\}

| SITE | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC | ANNUAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Baltimore/Washington International Airport | 0.3 | 0.2 | 0.8 | 2.4 | 4.0 | 5.4 | 5.8 | 4.9 | 2.0 | 1.0 | 0.4 | 0.1 | 27.3 |
| Norfolk, VA | 0.4 | 0.6 | 1.9 | 2.7 | 5.0 | 5.6 | 8.0 | 6.5 | 2.7 | 1.3 | 0.5 | 0.4 | 35.6 |
| Richmond, VA | 0.2 | 0.4 | 1.6 | 2.5 | 5.3 | 6.5 | 8.1 | 6.2 | 2.9 | 1.0 | 0.6 | 0.2 | 35.5 |

Table 2.3-4—\{High Winds by Storm Type for Calvert County\}

| Date | Time | Wind Speed Knots (m/sec) | Storm <br> Type |
| :---: | :---: | :---: | :---: |
| 6/3/1980 | 4:20 PM | 52 (27) | Thunderstorm |
| 7/1/1990 | 2:15 PM | 52 (27) | Thunderstorm |
| 5/4/1996 | 9:08 PM | 60 (31) | Thunderstorm |
| 10/8/1996 | 2:30 PM | 67 (34) | High Wind |
| 1/13/2000 | 12:00 PM | 56 (29) | High Wind |
| 4/21/2000 | 3:00 PM | 90 (46) | Thunderstorm |
| 3/13/2001 | 10:20 PM | 52 (27) | Thunderstorm |
| 6/11/2003 | 9:35 PM | 50 (26) | Thunderstorm |
| 6/27/2003 | 2:38 PM | 50 (26) | Thunderstorm |
| 7/18/2003 | 3:55 PM | 50 (26) | Thunderstorm |
| 8/5/2003 | 9:00 PM | 50 (26) | Thunderstorm |
| 8/16/2003 | 4:11 PM | 50 (26) | Thunderstorm |
| 8/26/2003 | 4:15 PM | 55 (28) | Thunderstorm |
| 5/25/2004 | 9:05 PM | 50 (26) | Thunderstorm |
| 7/5/2005 | 6:45 PM | 50 (26) | Thunderstorm |
| 1/14/2006 | 5:15 PM | 52 (27) | High Wind |
| 9/1/2006 | 11:00 AM | 55 (28) | High Wind |

Table 2.3-5—\{Hail Events in Calvert County\}

| Date | Time | Type | Diameter |
| :---: | :---: | :---: | :---: |
| 10/9/1962 | 6:00 AM | Hail | 0.75 in ( 19.05 mm ) |
| 4/1/1993 | 5:45 PM | Hail | 0.88 in ( 22.35 mm ) |
| 9/26/1994 | 4:25 PM | Hail | 0.75 in ( 19.05 mm ) |
| 7/15/1996 | 3:07 PM | Hail | 2.00 in ( 50.80 mm ) |
| 3/29/1997 | 1:30 PM | Hail | 1.75 in ( 44.45 mm ) |
| 6/15/1998 | 5:45 PM | Hail | 1.75 in ( 44.45 mm ) |
| 6/15/1998 | 6:55 PM | Hail | 0.75 in ( 19.05 mm ) |
| 4/9/1999 | 5:30 PM | Hail | 1.50 in ( 38.10 mm ) |
| 4/9/1999 | 5:30 PM | Hail | 1.25 in ( 31.75 mm ) |
| 4/9/1999 | 5:30 PM | Hail | 1.00 in ( 25.40 mm ) |
| 4/23/1999 | 3:40 PM | Hail | 1.00 in ( 25.40 mm ) |
| 4/23/1999 | 3:45 PM | Hail | 1.50 in ( 38.10 mm ) |
| 4/23/1999 | 4:42 PM | Hail | 0.75 in ( 19.05 mm ) |
| 4/23/1999 | 4:42 PM | Hail | 1.50 in ( 38.10 mm ) |
| 4/21/2000 | 5:15 PM | Hail | 1.00 in ( 25.40 mm ) |
| 7/16/2000 | 1:30 PM | Hail | 0.88 in ( 22.35 mm ) |
| 4/28/2002 | 6:25 PM | Hail | 1.75 in ( 44.45 mm ) |
| 4/28/2002 | 6:35 PM | Hail | 1.75 in ( 44.45 mm ) |
| 5/5/2004 | 5:35 PM | Hail | 0.88 in ( 22.35 mm ) |
| 4/23/2005 | 4:23 PM | Hail | 0.75 in ( 19.05 mm ) |

Table 2.3-6—\{Ice Storm Events in Calvert County\}

| Start Date and Time | End Date and Time | Ice Thickness |
| :---: | :---: | :---: |
| $01 / 14 / 1999$ 1:00 AM | $01 / 15 / 199911: 00 \mathrm{AM}$ | Trace to 0.25 in <br> (Trace to 6.35 mm ) |
| $01 / 30 / 2000$ 3:00 AM | $01 / 30 / 20008: 00 \mathrm{PM}$ | 0.25 to 1.0 inches <br> $(6.35$ to 25.4 mm ) |
| $12 / 14 / 2003$ 3:00 AM | $12 / 14 / 20037: 00 \mathrm{PM}$ | Light <br> accumulations |
| $01 / 17 / 20046: 00 \mathrm{PM}$ | $01 / 18 / 20044: 00 \mathrm{PM}$ | Up to 0.20 in <br> (Up to 5.08 mm ) |
| $12 / 09 / 20053: 00 \mathrm{AM}$ | $12 / 09 / 20058: 00 \mathrm{AM}$ | Up to 0.20 in <br> (Up to 5.08 mm ) |

Table 2.3-7—\{Snow Storm Events in Calvert County\}

| Date | Snow Amount |
| :--- | :--- |
| $12 / 28 / 1993$ | No amounts provided |
| $01 / 06 / 1996$ | Approximately 15 in $(381 \mathrm{~mm})$ in Calvert County <br> Approximately 23 in $(584 \mathrm{~mm})$ at BWI Airport |
| $01 / 12 / 1996$ | 4 to 6 in $(102$ to 152 mm$)$ |
| $02 / 02 / 1996$ | 8 to 13 in $(203$ to 330 mm$)$ |
| $02 / 02 / 1996$ | 4 to 6 in $(102$ to 152 mm$)$ during the afternoon followed by 9 in $(230 \mathrm{~mm})$ overnight |
| $02 / 16 / 1996$ | 10 to 13 in (254 to 330 mm$)$ |
| $02 / 08 / 1997$ | 4 to 8 in $(102$ to 203 mm$)$ |
| $03 / 09 / 1999$ | 4 to 8 in $(102$ to 203 mm$)$ |
| $01 / 20 / 2000$ | 3 to 8 in $(76$ to 203 mm$)$ |
| $01 / 25 / 2000$ | 16.5 in $(419 \mathrm{~mm})$ in Hollywood, St. Mary's County |
| $02 / 22 / 2001$ | 3 to 7 in $(76$ to 178 mm$)$ |
| $01 / 03 / 2002$ | 1 to 4 in $(25$ to 102 mm$)$ |
| $01 / 19 / 2002$ | 1 to 2 in $(25$ to 51 mm$)$ |
| $12 / 05 / 2002$ | 3 to 5 in $(76$ to 127 mm$)$ |
| $02 / 06 / 2003$ | 5 to 8 in $(127$ to 203 mm$)$ |
| $02 / 14 / 2003$ | 7.5 in $(191 \mathrm{~mm})$ of mainly sleet in Hollywood, St. Mary's County |
| $02 / 26 / 2003$ | 5 to 8 in $(127$ to 203 mm$)$ |
| $12 / 04 / 2003$ | 1 to 2 in $(25$ to 51 mm$)$ |
| $12 / 14 / 2003$ | 1 to 3 in $(25$ to 76 mm$)$ |
| $01 / 17 / 2004$ | $1 / 4$ to 2 in $(6$ to 51 mm$)$ |
| $01 / 25 / 2004$ | 3 to 4 in $(76$ to 102 mm$)$ |
| $02 / 24 / 2005$ | 4 to 8 in $(102$ to 203 mm$)$ |
| $12 / 06 / 2005$ | 4 to 6.5 in $(102$ to 165 mm$)$ |
| $12 / 09 / 2005$ | 1 to 4 in $(25$ to 102 mm$)$ |
| $02 / 11 / 2006$ | 8 to 14 in $(203$ to 356 mm$)$ |
|  |  |

Table 2.3-8-\{Probable Maximum Winter Precipitation (PMWP) Values\}

| Winter Months | $\begin{gathered} 200 \mathrm{mi}^{2} \\ \text { 24-Hour } \\ \text { PMWP in (mm) } \end{gathered}$ | $10 \mathrm{mi}^{2}$ <br> 48-Hour Adjustment for Zone 6 | $\begin{gathered} 10 \mathrm{mi}^{2} \\ \text { 48-Hour } \\ \text { PMWP in (mm) } \end{gathered}$ |
| :---: | :---: | :---: | :---: |
| December | 13.0 (330.2) | 1.36 | 17.7 (449.6) |
| tanuary | 11.0 (279.4) | 1.38 | 15.2 (386.1) |
| February | 11.5 (292.1) | 1.38 | 15.9 (403.9) |


| $\underline{\text { Duration (hours) }}$ | $\underline{\text { Jan-Feb PMP Depth }}$ <br> (inches) | $\underline{\text { Dec PMP Depth }}$ <br> (inches) |
| :---: | :---: | :---: |
| $\underline{6}$ | $\underline{10.5}$ | $\underline{12.25}$ |
| $\underline{24}$ | $\underline{16.5}$ | $\underline{18.5}$ |
| $\underline{72}$ | $\underline{20.5}$ | $\underline{23.5}$ |

Table 2.3-9—\{Design Basis Tornado Characteristics for CCNPP Unit 3\}

|  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Maximum <br> Wind Speed <br> $\mathbf{m} / \mathbf{s}(\mathbf{m p h})$ | Translational <br> Speed <br> $\mathbf{m} / \mathbf{s}(\mathbf{m p h})$ | Maximum <br> Rotational <br> Speed <br> $\mathbf{m} / \mathbf{s}(\mathbf{m p h})$ | Maximum <br> Rotational <br> Speed <br> $\mathbf{m}(\mathbf{f t})$ | Pressure Drop <br> $\mathbf{m b}(\mathbf{p s i})$ |
| Region | Rate of Pressure <br> Drop <br> $\mathbf{m b / s}(\mathbf{p s i} / \mathbf{s})$ |  |  |  |  |
| II | $89(200)$ | $18(40)$ | $72(160)$ | $45.7(150)$ | $63(0.9)$ |

Table 2.3-10—\{AnnualHeating and Humidification Design Conditions for Patuxent River Naval Air Station, Maryland (1982-2001)\}

| Coldest month | Annual Heating and Humidification Design Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Heating DB |  | Humidification DP/MCDB-and HR |  |  |  |  |  | Coldest month WS/MCDB |  |  |  | MCWS/PCWD$\text { to } 99.6 \% \text { DB }$ |  |
|  |  |  | 99.6\% |  |  | 99\% |  |  | 0.4\% |  | 1\% |  |  |  |
|  | 99.6\% | 99\% | DP | HR | ACDB | DP | HR | ACDB | WS | ACDB | WS | MCDB | MCWS | $\begin{gathered} \hline \text { PCW } \\ \text { D } \end{gathered}$ |
| $z$ | 3 a | 3b | 4 a | 4b | 4 E | 4d | 4 e | $4 f$ | 53 | $5 b$ | 56 | 5d | $6 a$ | 6 b |
| 7 | $16.6^{\circ} \mathrm{F}$ | $20.9^{\circ} \mathrm{F}$ | $0.3^{\circ} \mathrm{F}$ | 5.6 | $20.5^{\circ} \mathrm{F}$ | $5.0^{\circ} \mathrm{F}$ | 7.7 | $23.4{ }^{\circ} \mathrm{F}$ | $\begin{aligned} & 26.9 \\ & \mathrm{mph} \end{aligned}$ | $36.5^{\circ} \mathrm{F}$ | $\begin{aligned} & 24.2 \\ & \mathrm{mph} \end{aligned}$ | $31.8^{\circ} \mathrm{F}$ | $\begin{gathered} 8.1 \\ \mathrm{mph} \end{gathered}$ | 340 |
| 7 | $-8.6{ }^{\circ} \mathrm{C}$ | $-6.2^{\circ} \mathrm{C}$ | $\begin{gathered} -17.6^{\circ} \\ \epsilon \end{gathered}$ | 5.6 | $-6.4^{\circ} \mathrm{C}$ | $\begin{gathered} -15.0^{\circ} \\ \epsilon \end{gathered}$ | 7.4 | $-4.8{ }^{\circ} \mathrm{C}$ | $\begin{aligned} & 12.0 \\ & \mathrm{mps} \end{aligned}$ | $2.5^{\circ} \mathrm{C}$ | $\begin{aligned} & 10.8 \\ & \text { mps } \end{aligned}$ | ${ }^{-0.10} \mathrm{C}$ | $\begin{aligned} & 3.6 \\ & \mathrm{mps} \end{aligned}$ | 340 |

Notes:
$D B=$ dry bulb
$D P=$ dew point
$H R=$ humidity ratio
$\mathrm{MCDB}=$ mean coincident dry bulb
WS $=$ wind speed
ACWS = mean coincident wind speed
PCWD = prevailing coincident wind direction, degrees with respect to True North
Table 2.3-11—\{Annual Cooling, Dehumidification, and Enthalpy Design Conditions for Patuxent River Naval Air Station, Maryland (1982-2001) \}

| Annual-Cooling, Dehumidification, and Enthalpy-Design-Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hottest month | Hottest month DB range | Cooling DB/MCWB |  |  |  |  |  | Evaporation WB/MCDB |  |  |  |  |  | MCWSIPCWD to 0.4\% DB |  |
|  |  | 0.4\% |  | 1\% |  | 2\% |  | 0.4\% |  | 1\% |  | 2\% |  |  |  |
|  |  | DB | MCWB | DB | MCWB | DB | MCWB | WB | MCDB | WB | MCDB | WB | MCDB | MCWS | PCWD |
| 7 | 8 | 93 | 96 | 96 | 9 d | 9 e | $9 f$ | 10a | 10 b | $10 \epsilon$ | 10d | 10e | $10 f$ | 11a | 11b |
| 7 | $15.5^{\circ} \mathrm{F}$ | 92.5 ${ }^{\circ} \mathrm{F}$ | $76.2^{\circ} \mathrm{F}$ | $89.9{ }^{\circ} \mathrm{F}$ | $75.5^{\circ} \mathrm{F}$ | $87.6^{\circ} \mathrm{F}$ | $74.6{ }^{\circ} \mathrm{F}$ | $79.2^{\circ} \mathrm{F}$ | $88.3^{\circ} \mathrm{F}$ | $77.8{ }^{\circ} \mathrm{F}$ | $86.4{ }^{\circ} \mathrm{F} \quad 7$ | $76.5{ }^{\circ} \mathrm{F} \quad 8$ | $84.5^{\circ} \mathrm{F}$ | 8.8 mph | 240 |
| 7 | $27.9^{\circ} \mathrm{C}$ | $33.6{ }^{\circ} \mathrm{C}$ | $24.6^{\circ} \mathrm{C}$ | $32.2{ }^{\circ} \mathrm{C}$ | $24.2{ }^{\circ} \mathrm{C}$ | $30.9{ }^{\circ} \mathrm{C}$ | $23.7^{\circ} \mathrm{C}$ | $26.2^{\circ} \mathrm{C}$ | $31.3^{\circ} \mathrm{C}$ | $25.4^{\circ} \mathrm{C}$ | $30.2{ }^{\circ} \mathrm{C} \quad 2$ | $24.7^{\circ} \mathrm{C}$ | $29.2{ }^{\circ} \mathrm{C}$ | 3.9 mps | 240 |
| Dehumidification-DP/MCDB-andHR |  |  |  |  |  |  |  |  | Enthalpy/MCDB |  |  |  |  |  |  |
|  | 0.4\% |  | 1\% |  |  | 2\% |  |  | 0.4\% |  | \% |  | 2\% |  |  |
| DP | HR | MCDB | DP | HR | MCDB | DP | HR | MCDB | Enth | MCDB | Enth | MCDB | Enth |  | MCDB |
| 12 a | 12b | 12 C | 12d | 12e | 12 f | 12 g | 12h | 12i | 13a | 13b | 136 | 13d | 13e |  | 13f |
| $76.6^{\circ} \mathrm{F}$ | 139.0 | $84.0^{\circ} \mathrm{F}$ | $75.1^{\circ} \mathrm{F}$ | 132.0 | $82.7^{\circ} \mathrm{F}$ | $73.8^{\circ} \mathrm{F}$ | 126.1 | $81.3^{\circ} \mathrm{F}$ | $34.8 \mathrm{~kJ} / \mathrm{kg}$ | $88.3^{\circ} \mathrm{F}$ | $33.4 \mathrm{~kJ} / \mathrm{kg}$ | $86.4{ }^{\circ} \mathrm{F}$ | [ $32.1 \mathrm{~kJ} / \mathrm{kg}$ |  | $84.8^{\circ} \mathrm{F}$ |
| $24.8{ }^{\circ} \mathrm{C}$ | 139.0 | $28.9{ }^{\circ} \mathrm{C}$ | $23.9{ }^{\circ} \mathrm{C}$ | 132.0 | $28.2^{\circ} \mathrm{C}$ | $23.2{ }^{\circ} \mathrm{C}$ | 126.4 | $27.4^{\circ} \mathrm{C}$ | $34.8 \mathrm{~kJ} / \mathrm{kg}$ | $31.3^{\circ} \mathrm{C}$ | $33.4 \mathrm{~kJ} / \mathrm{kg}$ | $30.2^{\circ} \mathrm{C}$ | $32.1 \mathrm{~kJ} / \mathrm{kg}$ |  | $29.3{ }^{\circ} \mathrm{C}$ |

Notes:
$\mathrm{DB}=$ dry bulb
$\mathrm{MCDB}=$ mean coincident dry bulb
MCWB = mean coincident wet bulb
ACWS = mean coincident wind speed
PCWD = prevailing coincident wind direction, degrees with respect to True North
$\mathrm{HR}=$ humidity ratio
Enth = Enthalpy
WS = wind speed
$W B=$ wet bulb
$D B=$ dry bulb

Table 2.3-13-\{Monthly Design Dry Bulb and Mean Coincident Wet Bulb TemperatureValues for Patuxent River Naval Air Station, Maryland (1982-2001) \}

| Menthly Design Dry Bulb and Mean Coincident Wet Bulb Temperatures |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Jan |  | Feb |  | Mar |  | Apr |  | May |  | Jth |  |
|  | DB | MCWB | DB | MCWB | DB | ACWB | DB | MCWB | DB | MCWB | DB | MCWB |
|  | 18a | 18b | 18¢ | 18d | 18e | 18f | 189 | 18h | 18i | 18j | 18k | 181 |
| 0.4\% | $64.4{ }^{\circ} \mathrm{F}$ | $58.0^{\circ} \mathrm{F}$ | $69.9^{\circ} \mathrm{F}$ | $57.7{ }^{\circ} \mathrm{F}$ | $80.3^{\circ} \mathrm{F}$ | $63.7^{\circ} \mathrm{F}$ | $85.2^{\circ} \mathrm{F}$ | $65.7^{\circ} \mathrm{F}$ | $89.8{ }^{\circ} \mathrm{F}$ | $72.3{ }^{\circ} \mathrm{F}$ | $93.2{ }^{\circ} \mathrm{F}$ | $76.0^{\circ} \mathrm{F}$ |
|  | $18.0^{\circ} \mathrm{C}$ | $14.4{ }^{\circ} \mathrm{C}$ | $21.1^{\circ} \mathrm{C}$ | $14.3{ }^{\circ} \mathrm{C}$ | $26.8^{\circ} \mathrm{C}$ | $17.6^{\circ} \mathrm{C}$ | $29.6{ }^{\circ} \mathrm{C}$ | $18.7^{\circ} \mathrm{C}$ | $32.1{ }^{\circ} \mathrm{C}$ | $22.4{ }^{\circ} \mathrm{C}$ | $34.0{ }^{\circ} \mathrm{C}$ | $24.4{ }^{\circ} \mathrm{C}$ |
| 1\% | $62.7{ }^{\circ} \mathrm{F}$ | $56.9{ }^{\circ} \mathrm{F}$ | $66.2^{\circ} \mathrm{F}$ | $56.8{ }^{\circ} \mathrm{F}$ | $74.9{ }^{\circ} \mathrm{F}$ | $60.6^{\circ} \mathrm{F}$ | $81.2^{\circ} \mathrm{F}$ | $64.0^{\circ} \mathrm{F}$ | $87.7^{\circ} \mathrm{F}$ | $72.0{ }^{\circ} \mathrm{F}$ | $91.5^{\circ} \mathrm{F}$ | $75.5^{\circ} \mathrm{F}$ |
|  | $17.1^{\circ} \mathrm{C}$ | $13.8{ }^{\circ} \mathrm{C}$ | $19.0^{\circ} \mathrm{C}$ | $13.8{ }^{\circ} \mathrm{C}$ | $23.8^{\circ} \mathrm{C}$ | $15.9{ }^{\circ} \mathrm{C}$ | $27.3^{\circ} \mathrm{C}$ | $17.8{ }^{\circ} \mathrm{C}$ | $30.9{ }^{\circ} \mathrm{C}$ | $22.2{ }^{\circ} \mathrm{C}$ | $33.1{ }^{\circ} \mathrm{C}$ | $24.2{ }^{\circ} \mathrm{C}$ |
| 2\% | $59.6{ }^{\circ} \mathrm{F}$ | $53.1^{\circ} \mathrm{F}$ | $62.9^{\circ} \mathrm{F}$ | $55.5^{\circ} \mathrm{F}$ | $70.8^{\circ} \mathrm{F}$ | $58.9^{\circ} \mathrm{F}$ | $77.3^{\circ} \mathrm{F}$ | $62.5^{\circ} \mathrm{F}$ | $85.4{ }^{\circ} \mathrm{F}$ | $70.4^{\circ} \mathrm{F}$ | $90.0^{\circ} \mathrm{F}$ | $74.8{ }^{\circ} \mathrm{F}$ |
|  | $15.3{ }^{\circ} \mathrm{C}$ | $11.7^{\circ} \mathrm{C}$ | $17.2{ }^{\circ} \mathrm{C}$ | $13.1{ }^{\circ} \mathrm{C}$ | $21.6^{\circ} \mathrm{C}$ | $14.9{ }^{\circ} \mathrm{C}$ | $25.2{ }^{\circ} \mathrm{C}$ | $16.9{ }^{\circ} \mathrm{C}$ | $29.7{ }^{\circ} \mathrm{C}$ | $21.3{ }^{\circ} \mathrm{C}$ | $32.2{ }^{\circ} \mathrm{C}$ | $23.8{ }^{\circ} \mathrm{C}$ |
|  | Jul |  | Aug |  | Sep |  | Oct |  | Nov |  | Def |  |
|  | DB | ACWB | DB | MCWB | DB | ACWB | DB | ACWB | DB | MCWB | DB | ACWB |
|  | 18m | 18n | 180 | 18p | 18q | 18r | 18s | 18 t | 18u | 18v | 18w | 18x |
| 0.4\% | $96.9^{\circ} \mathrm{F}$ | $76.8{ }^{\circ} \mathrm{F}$ | $94.7^{\circ} \mathrm{F}$ | $76.7^{\circ} \mathrm{F}$ | $92.0^{\circ} \mathrm{F}$ | $74.7^{\circ} \mathrm{F}$ | $83.3^{\circ} \mathrm{F}$ | $71.2^{\circ} \mathrm{F}$ | $75.1^{\circ} \mathrm{F}$ | $64.5^{\circ} \mathrm{F}$ | $70.2^{\circ} \mathrm{F}$ | $61.7^{\circ} \mathrm{F}$ |
|  | $36.1{ }^{\circ} \mathrm{C}$ | $24.9{ }^{\circ} \mathrm{C}$ | $34.8{ }^{\circ} \mathrm{C}$ | $24.8{ }^{\circ} \mathrm{C}$ | $33.3^{\circ} \mathrm{C}$ | $23.7{ }^{\circ} \mathrm{C}$ | $28.5{ }^{\circ} \mathrm{C}$ | $21.8^{\circ} \mathrm{C}$ | $23.9{ }^{\circ} \mathrm{C}$ | $18.1^{\circ} \mathrm{C}$ | $21.2^{\circ} \mathrm{C}$ | $16.5^{\circ} \mathrm{C}$ |
| 1\% | $95.2^{\circ} \mathrm{F}$ | $77.1^{\circ} \mathrm{F}$ | $92.4{ }^{\circ} \mathrm{F}$ | $77.3^{\circ} \mathrm{F}$ | $89.4{ }^{\circ} \mathrm{F}$ | $74.9{ }^{\circ} \mathrm{F}$ | $81.0^{\circ} \mathrm{F}$ | $69.7^{\circ} \mathrm{F}$ | $72.5{ }^{\circ} \mathrm{F}$ | $62.8{ }^{\circ} \mathrm{F}$ | $67.6^{\circ} \mathrm{F}$ | $60.4{ }^{\circ} \mathrm{F}$ |
|  | $35.1{ }^{\circ} \mathrm{C}$ | $35.1^{\circ} \mathrm{C}$ | $33.6{ }^{\circ} \mathrm{C}$ | $25.2{ }^{\circ} \mathrm{C}$ | $31.9{ }^{\circ} \mathrm{C}$ | $23.8{ }^{\circ} \mathrm{C}$ | $27.2{ }^{\circ} \mathrm{C}$ | $20.9{ }^{\circ} \mathrm{C}$ | $22.5{ }^{\circ} \mathrm{C}$ | $17.1^{\circ} \mathrm{C}$ | $19.8{ }^{\circ} \mathrm{C}$ | $15.8{ }^{\circ} \mathrm{C}$ |
| 2\% | $93.3{ }^{\circ} \mathrm{F}$ | $76.3^{\circ} \mathrm{F}$ | $90.4^{\circ} \mathrm{F}$ | $76.7{ }^{\circ} \mathrm{F}$ | $86.7^{\circ} \mathrm{F}$ | $73.9^{\circ} \mathrm{F}$ | $78.7{ }^{\circ} \mathrm{F}$ | $68.7^{\circ} \mathrm{F}$ | $70.2^{\circ} \mathrm{F}$ | $62.0{ }^{\circ} \mathrm{F}$ | $64.9{ }^{\circ} \mathrm{F}$ | $57.9^{\circ} \mathrm{F}$ |
|  | $34.1^{\circ} \mathrm{C}$ | $24.6{ }^{\circ} \mathrm{C}$ | $32.4{ }^{\circ} \mathrm{C}$ | $24.8{ }^{\circ} \mathrm{C}$ | $30.4{ }^{\circ} \mathrm{C}$ | $23.3{ }^{\circ} \mathrm{C}$ | $25.9{ }^{\circ} \mathrm{C}$ | $20.4{ }^{\circ} \mathrm{C}$ | $21.2^{\circ} \mathrm{C}$ | $16.7^{\circ} \mathrm{C}$ | $18.3{ }^{\circ} \mathrm{C}$ | $14.4{ }^{\circ} \mathrm{C}$ |

Notes:
$D B=$ dry bulb
ACWB = mean coincident wet bulb

Table 2.3-14—\{Monthly Design Wet Bulb-and Mean Coincident Dry Bulb TemperatureValues for Patuxent River Naval Air Station, Maryland (1982-2001) \}

|  | Jan |  | Feb |  | Mar |  | Apr |  | May |  | Jun |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | WB | MCDB | WB | MCDB | WB | ACDB | WB | MCDB | WB | MCDB | WB | ACDB |
|  | 19a | 19b | 19e | 49d | 19e | 199 | 19 g | 19h | 19i | 19ز | 19* | 191 |
| 0.4\% | $60.2^{\circ} \mathrm{F}$ | $63.7^{\circ} \mathrm{F}$ | $61.3^{\circ} \mathrm{F}$ | $67.1^{\circ} \mathrm{F}$ | $65.1^{\circ} \mathrm{F}$ | $77.6^{\circ} \mathrm{F}$ | $68.8^{\circ} \mathrm{F}$ | $79.7{ }^{\circ} \mathrm{F}$ | $76.0^{\circ} \mathrm{F}$ | $86.3^{\circ} \mathrm{F}$ | $79.5{ }^{\circ} \mathrm{F}$ | $88.4{ }^{\circ} \mathrm{F}$ |
|  | $15.7{ }^{\circ} \mathrm{C}$ | $17.6^{\circ} \mathrm{C}$ | $16.3{ }^{\circ} \mathrm{C}$ | $19.5{ }^{\circ} \mathrm{C}$ | $18.4{ }^{\circ} \mathrm{C}$ | $25.3{ }^{\circ} \mathrm{C}$ | $20.4{ }^{\circ} \mathrm{C}$ | $26.5{ }^{\circ} \mathrm{C}$ | $24.4{ }^{\circ} \mathrm{C}$ | $30.2{ }^{\circ} \mathrm{C}$ | $26.4{ }^{\circ} \mathrm{C}$ | $31.3{ }^{\circ} \mathrm{C}$ |
| 1\% | $57.5^{\circ} \mathrm{F}$ | $61.8^{\circ} \mathrm{F}$ | $58.8{ }^{\circ} \mathrm{F}$ | $64.4{ }^{\circ} \mathrm{F}$ | $63.0^{\circ} \mathrm{F}$ | $72.3^{\circ} \mathrm{F}$ | $67.1^{\circ} \mathrm{F}$ | $76.9{ }^{\circ} \mathrm{F}$ | $74.6{ }^{\circ} \mathrm{F}$ | $83.9^{\circ} \mathrm{F}$ | $78.2^{\circ} \mathrm{F}$ | $86.9{ }^{\circ} \mathrm{F}$ |
|  | $14.2{ }^{\circ} \mathrm{C}$ | $16.6{ }^{\circ} \mathrm{C}$ | $14.9{ }^{\circ} \mathrm{C}$ | $18.0^{\circ} \mathrm{C}$ | $17.2{ }^{\circ} \mathrm{C}$ | $22.4{ }^{\circ} \mathrm{C}$ | $19.5{ }^{\circ} \mathrm{C}$ | $24.9{ }^{\circ} \mathrm{C}$ | $23.7{ }^{\circ} \mathrm{C}$ | $28.8{ }^{\circ} \mathrm{C}$ | $25.7^{\circ} \mathrm{C}$ | $30.5^{\circ} \mathrm{C}$ |
| 2\% | $55.0^{\circ} \mathrm{F}$ | $58.5^{\circ} \mathrm{F}$ | $56.0^{\circ} \mathrm{F}$ | $61.9^{\circ} \mathrm{F}$ | $60.8^{\circ} \mathrm{F}$ | $68.7^{\circ} \mathrm{F}$ | $65.5^{\circ} \mathrm{F}$ | $74.3{ }^{\circ} \mathrm{F}$ | $73.0^{\circ} \mathrm{F}$ | $81.8^{\circ} \mathrm{F}$ | $77.4{ }^{\circ} \mathrm{F}$ | $85.9{ }^{\circ} \mathrm{F}$ |
|  | $12.8{ }^{\circ} \mathrm{C}$ | $14.7{ }^{\circ} \mathrm{C}$ | $13.3{ }^{\circ} \mathrm{C}$ | $16.6^{\circ} \mathrm{C}$ | $16.0^{\circ} \mathrm{C}$ | $20.4{ }^{\circ} \mathrm{C}$ | $18.6{ }^{\circ} \mathrm{C}$ | $23.5{ }^{\circ} \mathrm{C}$ | $22.8{ }^{\circ} \mathrm{C}$ | $27.7{ }^{\circ} \mathrm{C}$ | $25.2{ }^{\circ} \mathrm{C}$ | $29.9{ }^{\circ} \mathrm{C}$ |
|  | Jul |  | Aug |  | Sep |  | Oct |  | Nov |  | Dee |  |
|  | $\begin{aligned} & \text { WB } \\ & \text { 19m } \end{aligned}$ | MCDB <br> 19n | $\begin{aligned} & \text { WB } \\ & 190 \end{aligned}$ | $\begin{aligned} & \text { MCDB } \\ & 19 p \end{aligned}$ | $\begin{aligned} & \text { WB } \\ & 19 \mathrm{q} \end{aligned}$ | $\begin{aligned} & \text { MCDB } \\ & \text { 19\% } \end{aligned}$ | $\begin{aligned} & \text { WB } \\ & \text { 19s } \end{aligned}$ | $\begin{aligned} & \text { ACDB } \\ & \text { 19t } \end{aligned}$ | $\begin{aligned} & \text { WB } \\ & 19 u \end{aligned}$ | MCDB <br> 19v | $\begin{aligned} & \text { WB } \\ & \text { 19w } \end{aligned}$ | $\begin{aligned} & \text { ACDB } \\ & \text { 19* } \end{aligned}$ |
| 0.4\% | $81.3^{\circ} \mathrm{F}$ | $90.8^{\circ} \mathrm{F}$ | $80.9^{\circ} \mathrm{F}$ | $88.2^{\circ} \mathrm{F}$ | $78.4^{\circ} \mathrm{F}$ | $85.5^{\circ} \mathrm{F}$ | $72.8{ }^{\circ} \mathrm{F}$ | $80.0^{\circ} \mathrm{F}$ | $67.1^{\circ} \mathrm{F}$ | $72.0^{\circ} \mathrm{F}$ | $63.5^{\circ} \mathrm{F}$ | $68.9{ }^{\circ} \mathrm{F}$ |
|  | $27.4{ }^{\circ} \mathrm{C}$ | $32.7{ }^{\circ} \mathrm{C}$ | $27.2{ }^{\circ} \mathrm{C}$ | $31.2^{\circ} \mathrm{C}$ | $25.8^{\circ} \mathrm{C}$ | $29.7{ }^{\circ} \mathrm{C}$ | $22.7^{\circ} \mathrm{C}$ | $26.7^{\circ} \mathrm{C}$ | $19.5{ }^{\circ} \mathrm{C}$ | $22.2{ }^{\circ} \mathrm{C}$ | $17.5^{\circ} \mathrm{C}$ | $20.5^{\circ} \mathrm{C}$ |
| 1\% | $80.3^{\circ} \mathrm{F}$ | $89.9{ }^{\circ} \mathrm{F}$ | $79.7{ }^{\circ} \mathrm{F}$ | $88.4{ }^{\circ} \mathrm{F}$ | $77.4{ }^{\circ} \mathrm{F}$ | $84.6{ }^{\circ} \mathrm{F}$ | $71.3^{\circ} \mathrm{F}$ | $78.6^{\circ} \mathrm{F}$ | $65.5^{\circ} \mathrm{F}$ | $69.9{ }^{\circ} \mathrm{F}$ | $61.3{ }^{\circ} \mathrm{F}$ | $65.9{ }^{\circ} \mathrm{F}$ |
|  | $26.8^{\circ} \mathrm{C}$ | $32.2{ }^{\circ} \mathrm{C}$ | $26.5{ }^{\circ} \mathrm{C}$ | $31.3{ }^{\circ} \mathrm{C}$ | $25.2{ }^{\circ} \mathrm{C}$ | $29.2{ }^{\circ} \mathrm{C}$ | $21.8{ }^{\circ} \mathrm{C}$ | $25.9^{\circ} \mathrm{C}$ | $18.6{ }^{\circ} \mathrm{C}$ | $21.1^{\circ} \mathrm{C}$ | $16.3^{\circ} \mathrm{C}$ | $18.8{ }^{\circ} \mathrm{C}$ |
| 2\% | $79.6{ }^{\circ} \mathrm{F}$ | $89.2^{\circ} \mathrm{F}$ | $78.6{ }^{\circ} \mathrm{F}$ | $87.0^{\circ} \mathrm{F}$ | $76.4^{\circ} \mathrm{F}$ | $83.3^{\circ} \mathrm{F}$ | $70.2^{\circ} \mathrm{F}$ | $76.6^{\circ} \mathrm{F}$ | $64.0^{\circ} \mathrm{F}$ | $68.2^{\circ} \mathrm{F}$ | $59.4{ }^{\circ} \mathrm{F}$ | $64.2^{\circ} \mathrm{F}$ |
|  | $26.4{ }^{\circ} \mathrm{C}$ | $31.8^{\circ} \mathrm{C}$ | $25.9{ }^{\circ} \mathrm{C}$ | $30.6{ }^{\circ} \mathrm{C}$ | $24.7{ }^{\circ} \mathrm{C}$ | $28.5{ }^{\circ} \mathrm{C}$ | $21.2^{\circ} \mathrm{C}$ | $24.8^{\circ} \mathrm{C}$ | $17.8{ }^{\circ} \mathrm{C}$ | $20.1^{\circ} \mathrm{C}$ | $15.2{ }^{\circ} \mathrm{C}$ | $17.9^{\circ} \mathrm{C}$ |

Notes:
WB = wet bulb
$A C D B=$ mean coincident dry bulb

Table 2.3-15—\{Monthly Mean Daily Temperature Range for Patuxent River Naval Air Station, Maryland (1982-2001)

| Monthly Mean Daily Temperature Range |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Jan | Feb | Mar | Apf | May | Jun | Jul | Aug | Sep | Oct | Nov | Det |
| 20a | 206 | 20¢ | 20d | 20e | 209 | 20 g | 20h | $20 i$ | $20{ }^{\text {j }}$ | 20k | 201 |
| $14.4{ }^{\circ} \mathrm{F}$ | $15.0^{\circ} \mathrm{F}$ | $16.1^{\circ} \mathrm{F}$ | $17.4{ }^{\circ} \mathrm{F}$ | $16.9^{\circ} \mathrm{F}$ | $16.2^{\circ} \mathrm{F}$ | $15.5^{\circ} \mathrm{F}$ | $14.8{ }^{\circ} \mathrm{F}$ | $15.1^{\circ} \mathrm{F}$ | $16.3^{\circ} \mathrm{F}$ | $16.2^{\circ} \mathrm{F}$ | $14.5^{\circ} \mathrm{F}$ |
| $8.0^{\circ} \mathrm{C}$ | $8.3{ }^{\circ} \mathrm{C}$ | $9.0{ }^{\circ} \mathrm{C}$ | $9.7{ }^{\circ} \mathrm{C}$ | $9.4{ }^{\circ} \mathrm{C}$ | $9.0^{\circ} \mathrm{C}$ | $8.6{ }^{\circ} \mathrm{C}$ | $8.2{ }^{\circ} \mathrm{C}$ | $8.4{ }^{\circ} \mathrm{C}$ | $9.0{ }^{\circ} \mathrm{C}$ | $9.0^{\circ} \mathrm{C}$ | $8.1{ }^{\circ} \mathrm{C}$ |

CC JANOO-DEC05 MET DATA JOINT FREQUENCY DISTR
33.0 FT WIND DATA
STABILITY CLASS A
Table 2.3-16-\{CCNPP 33 ft ( 10 m) Annual JFD $\}$

## (Page 1 of 8 )

(60-METER TOWER)


## 

## Table 2.3-16—\{CCNPP 33 ft ( 10 m) Annual JFD\}

## Page 2 of 8 )

CC JANOO-DECO5 MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
33.0 FT WIND DATA STABILITY CLASS B CLASS FREQUENCY (PERCENT) = 4.58

| $\begin{aligned} & \text { SPEED } \\ & \text { mps } \end{aligned}$ | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 04 | . 00 | . 00 | . 00 | . 00 | . 00 | . 04 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 6 |
| (1) | . 04 | . 00 | . 04 | . 00 | . 04 | . 00 | . 04 | . 00 | . 04 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 04 | . 00 | . 25 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 |
| 1.1-1.5 | 3 | 4 | 3 | 2 | 8 | 1 | 4 | 2 | 3 | 4 | 7 | 3 | 4 | 3 | 0 | 0 | 0 | 51 |
| (1) | . 13 | . 17 | . 13 | . 08 | . 34 | . 04 | . 17 | . 08 | . 13 | . 17 | . 30 | . 13 | . 17 | . 13 | . 00 | . 00 | . 00 | 2.16 |
| (2) | . 01 | . 01 | . 01 | . 00 | . 02 | . 00 | . 01 | . 00 | . 01 | . 01 | . 01 | . 01 | . 01 | . 01 | . 00 | . 00 | . 00 | . 10 |
| 1.6-2.0 | 11 | 11 | 25 | 21 | 13 | 18 | 11 | 3 | 11 | 10 | 20 | 19 | 10 | 5 | 4 | 5 | 0 | 197 |
| (1) | . 47 | . 47 | 1.06 | . 89 | . 55 | . 76 | . 47 | . 13 | . 47 | . 42 | . 85 | . 81 | . 42 | . 21 | . 17 | . 21 | . 00 | 8.35 |
| (2) | . 02 | . 02 | . 05 | . 04 | . 03 | . 03 | . 02 | . 01 | . 02 | . 02 | . 04 | . 04 | . 02 | . 01 | . 01 | . 01 | . 00 | . 38 |
| 2.1-3.0 | 87 | 122 | 64 | 64 | 45 | 33 | 44 | 41 | 36 | 42 | 61 | 67 | 42 | 28 | 16 | 13 | 0 | 805 |
| (1) | 3.69 | 5.17 | 2.71 | 2.71 | 1.91 | 1.40 | 1.87 | 1.74 | 1.53 | 1.78 | 2.59 | 2.84 | 1.78 | 1.19 | . 68 | . 55 | . 00 | 34.14 |
| (2) | . 17 | . 24 | . 12 | . 12 | . 09 | . 06 | . 09 | . 08 | . 07 | . 08 | . 12 | . 13 | . 08 | . 05 | . 03 | . 03 | . 00 | 1.56 |
| 3.1-4.0 | 94 | 76 | 43 | 12 | 8 | 12 | 45 | 80 | 14 | 34 | 69 | 50 | 27 | 28 | 30 | 17 | 0 | 639 |
| (1) | 3.99 | 3.22 | 1.82 | . 51 | . 34 | . 51 | 1.91 | 3.39 | . 59 | 1.44 | 2.93 | 2.12 | 1.15 | 1.19 | 1.27 | . 72 | . 00 | 27.10 |
| (2) | . 18 | . 15 | . 08 | . 02 | . 02 | . 02 | . 09 | . 16 | . 03 | . 07 | . 13 | . 10 | . 05 | . 05 | . 06 | . 03 | . 00 | 1.24 |
| 4.1-5.0 | 47 | 16 | 28 | 3 | 1 | 3 | 11 | 31 | 9 | 19 | 35 | 22 | 19 | 23 | 43 | 25 | 0 | 335 |
| (1) | 1.99 | . 68 | 1.19 | . 13 | . 04 | . 13 | . 47 | 1.31 | . 38 | . 81 | 1.48 | . 93 | . 81 | . 98 | 1.82 | 1.06 | . 00 | 14.21 |
| (2) | . 09 | . 03 | . 05 | . 01 | . 00 | . 01 | . 02 | . 06 | . 02 | . 04 | . 07 | . 04 | . 04 | . 04 | . 08 | . 05 | . 00 | . 65 |
| 5.1-6.0 | 38 | 8 | 15 | 4 | 0 | 1 | 4 | 18 | 3 | 5 | 15 | 1 | 11 | 21 | 40 | 14 | 0 | 198 |
| (1) | 1.61 | . 34 | . 64 | . 17 | . 00 | . 04 | . 17 | . 76 | . 13 | . 21 | . 64 | . 04 | . 47 | . 89 | 1.70 | . 59 | . 00 | 8.40 |
| (2) | . 07 | . 02 | . 03 | . 01 | . 00 | . 00 | . 01 | . 03 | . 01 | . 01 | . 03 | . 00 | . 02 | . 04 | . 08 | . 03 | . 00 | . 38 |
| 6.1-8.0 | 9 | 2 | 4 | 4 | 0 | 0 | 1 | 9 | 1 | 4 | 3 | 3 | 3 | 32 | 32 | 9 | 0 | 116 |
| (1) | . 38 | . 08 | . 17 | . 17 | . 00 | . 00 | . 04 | . 38 | . 04 | . 17 | . 13 | . 13 | . 13 | 1.36 | 1.36 | . 38 | . 00 | 4.92 |
| (2) | . 02 | . 00 | . 01 | . 01 | . 00 | . 00 | . 00 | . 02 | . 00 | . 01 | . 01 | . 01 | . 01 | . 06 | . 06 | . 02 | . 00 | . 23 |
| 8.1-10.0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 9 |
| (1) | . 04 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 04 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 30 | . 00 | . 00 | . 38 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 00 | . 00 | . 02 |
| 10.1-89.5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 04 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 04 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 292 | 239 | 183 | 110 | 76 | 68 | 121 | 185 | 78 | 118 | 210 | 166 | 116 | 140 | 172 | 84 | 0 | 2358 |
| (1) | 12.38 | 10.14 | 7.76 | 4.66 | 3.22 | 2.88 | 5.13 | 7.85 | 3.31 | 5.00 | 8.91 | 7.04 | 4.92 | 5.94 | 7.29 | 3.56 | . 00 | 100.00 |
| (2) | . 57 | . 46 | . 36 | . 21 | . 15 | . 13 | . 23 | . 36 | . 15 | . 23 | . 41 | . 32 | . 23 | . 27 | . 33 | . 16 | . 00 | 4.58 |

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

## 

## Table 2.3-16—\{CCNPP 33 ft ( 10 m) Annual JFD\}

## Page 3 of 8 )

CC JANOO-DECO5 MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

## (H)

## Table 2.3-16—\{CCNPP 33 ft ( 10 m) Annual JFD\}

## Page 4 of 8 )

CC JANOO-DEC05 MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
33.0 FT WIND DATA STABILITY CLASS D CLASS FREQUENCY (PERCENT) = 34.33

| WIND DIRECTION FROM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 3 | 0 | 0 | 1 | 2 | 1 | 0 | 9 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 02 | . 00 | . 00 | . 01 | . 01 | . 01 | . 00 | . 05 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| .2- . 4 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 2 | 1 | 2 | 4 | 4 | 0 | 1 | 0 | 17 |
| (1) | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 00 | . 01 | . 01 | . 01 | . 01 | . 02 | . 02 | . 00 | . 01 | . 00 | . 10 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 01 | . 00 | . 00 | . 00 | . 03 |
| .5-1.0 | 30 | 35 | 39 | 20 | 38 | 44 | 31 | 31 | 33 | 48 | 55 | 33 | 25 | 35 | 22 | 35 | 0 | 554 |
| (1) | . 17 | . 20 | . 22 | . 11 | . 21 | . 25 | . 18 | . 18 | . 19 | . 27 | . 31 | . 19 | . 14 | . 20 | . 12 | . 20 | . 00 | 3.13 |
| (2) | . 06 | . 07 | . 08 | . 04 | . 07 | . 09 | . 06 | . 06 | . 06 | . 09 | . 11 | . 06 | . 05 | . 07 | . 04 | . 07 | . 00 | 1.08 |
| 1.1-1.5 | 74 | 81 | 76 | 86 | 141 | 90 | 72 | 75 | 66 | 76 | 95 | 57 | 54 | 40 | 43 | 43 | 0 | 1169 |
| (1) | . 42 | . 46 | . 43 | . 49 | . 80 | . 51 | . 41 | . 42 | . 37 | . 43 | . 54 | . 32 | . 31 | . 23 | . 24 | . 24 | . 00 | 6.61 |
| (2) | . 14 | . 16 | . 15 | . 17 | . 27 | . 17 | . 14 | . 15 | . 13 | . 15 | . 18 | . 11 | . 10 | . 08 | . 08 | . 08 | . 00 | 2.27 |
| 1.6-2.0 | 153 | 215 | 152 | 198 | 209 | 145 | 126 | 120 | 126 | 119 | 126 | 93 | 70 | 50 | 80 | 69 | 0 | 2051 |
| (1) | . 86 | 1.22 | . 86 | 1.12 | 1.18 | . 82 | . 71 | . 68 | . 71 | . 67 | . 71 | . 53 | . 40 | . 28 | . 45 | . 39 | . 00 | 11.60 |
| (2) | . 30 | . 42 | . 30 | . 38 | . 41 | . 28 | . 24 | . 23 | . 24 | . 23 | . 24 | . 18 | . 14 | . 10 | . 16 | . 13 | . 00 | 3.98 |
| 2.1-3.0 | 418 | 501 | 394 | 506 | 390 | 241 | 265 | 404 | 249 | 194 | 311 | 230 | 149 | 146 | 257 | 263 | 0 | 4918 |
| (1) | 2.36 | 2.83 | 2.23 | 2.86 | 2.20 | 1.36 | 1.50 | 2.28 | 1.41 | 1.10 | 1.76 | 1.30 | . 84 | . 83 | 1.45 | 1.49 | . 00 | 27.80 |
| (2) | . 81 | . 97 | . 76 | . 98 | . 76 | . 47 | . 51 | . 78 | . 48 | . 38 | . 60 | . 45 | . 29 | . 28 | . 50 | . 51 | . 00 | 9.54 |
| 3.1-4.0 | 403 | 316 | 427 | 398 | 166 | 99 | 127 | 354 | 163 | 139 | 247 | 166 | 94 | 110 | 320 | 391 | 0 | 3920 |
| (1) | 2.28 | 1.79 | 2.41 | 2.25 | . 94 | . 56 | . 72 | 2.00 | . 92 | . 79 | 1.40 | . 94 | . 53 | . 62 | 1.81 | 2.21 | . 00 | 22.16 |
| (2) | . 78 | . 61 | . 83 | . 77 | . 32 | . 19 | . 25 | . 69 | . 32 | . 27 | . 48 | . 32 | . 18 | . 21 | . 62 | . 76 | . 00 | 7.61 |
| 4.1-5.0 | 340 | 264 | 359 | 226 | 45 | 16 | 45 | 187 | 71 | 62 | 164 | 60 | 57 | 123 | 287 | 287 | 0 | 2593 |
| (1) | 1.92 | 1.49 | 2.03 | 1.28 | . 25 | . 09 | . 25 | 1.06 | . 40 | . 35 | . 93 | . 34 | . 32 | . 70 | 1.62 | 1.62 | . 00 | 14.66 |
| (2) | . 66 | . 51 | . 70 | . 44 | . 09 | . 03 | . 09 | . 36 | . 14 | . 12 | . 32 | . 12 | . 11 | . 24 | . 56 | . 56 | . 00 | 5.03 |
| 5.1-6.0 | 244 | 172 | 237 | 110 | 1 | 4 | 13 | 94 | 22 | 25 | 66 | 18 | 25 | 103 | 218 | 112 | 0 | 1464 |
| (1) | 1.38 | . 97 | 1.34 | . 62 | . 01 | . 02 | . 07 | . 53 | . 12 | . 14 | . 37 | . 10 | . 14 | . 58 | 1.23 | . 63 | . 00 | 8.28 |
| (2) | . 47 | . 33 | . 46 | . 21 | . 00 | . 01 | . 03 | . 18 | . 04 | . 05 | . 13 | . 03 | . 05 | . 20 | . 42 | . 22 | . 00 | 2.84 |
| 6.1-8.0 | 167 | 78 | 174 | 50 | 3 | 2 | 5 | 52 | 16 | 17 | 13 | 8 | 13 | 103 | 133 | 36 | 0 | 870 |
| (1) | . 94 | . 44 | . 98 | . 28 | . 02 | . 01 | . 03 | . 29 | . 09 | . 10 | . 07 | . 05 | . 07 | . 58 | . 75 | . 20 | . 00 | 4.92 |
| (2) | . 32 | . 15 | . 34 | . 10 | . 01 | . 00 | . 01 | . 10 | . 03 | . 03 | . 03 | . 02 | . 03 | . 20 | . 26 | . 07 | . 00 | 1.69 |
| 8.1-10.0 | 23 | 6 | 25 | 8 | 1 | 0 | 2 | 2 | 1 | 0 | 1 | 0 | 4 | 21 | 13 | 2 | 0 | 109 |
| (1) | . 13 | . 03 | . 14 | . 05 | . 01 | . 00 | . 01 | . 01 | . 01 | . 00 | . 01 | . 00 | . 02 | . 12 | . 07 | . 01 | . 00 | . 62 |
| (2) | . 04 | . 01 | . 05 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 04 | . 03 | . 00 | . 00 | . 21 |
| 10.1-89.5 | 4 | 2 | 2 | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 14 |
| (1) | . 02 | . 01 | . 01 | . 01 | . 01 | . 00 | . 01 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 01 | . 00 | . 00 | . 08 |
| (2) | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 03 |
| ALL SPEEDS | 1857 | 1670 | 1885 | 1603 | 995 | 641 | 688 | 1320 | 748 | 684 | 1082 | 667 | 495 | 737 | 1376 | 1240 | 0 | 17688 |
| (1) | 10.50 | 9.44 | 10.66 | 9.06 | 5.63 | 3.62 | 3.89 | 7.46 | 4.23 | 3.87 | 6.12 | 3.77 | 2.80 | 4.17 | 7.78 | 7.01 | . 00 | 100.00 |
| (2) | 3.60 | 3.24 | 3.66 | 3.11 | 1.93 | 1.24 | 1.34 | 2.56 | 1.45 | 1.33 | 2.10 | 1.29 | . 96 | 1.43 | 2.67 | 2.41 | . 00 | 34.33 |
| (1) = PERCENT | OF ALI | GOOD | OBSERV | TIONS | FOR | HIS PA |  |  |  |  |  |  |  |  |  |  |  |  |
| (2) =PERCENT | F ALL G | OD OB | SERVATIO | NS FOR | THIS | ERIOD |  |  |  |  |  |  |  |  |  |  |  |  |

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Table 2.3-16—\{CCNPP 33 ft ( 10 m) Annual JFD $\}$
(Page 5 of 8)
CC JANOO-DECO5 MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
33.0 FT WIND DATA STABILITY CLASS E CLASS FREQUENCY (PERCENT) = 26.80


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## Table 2.3-16—\{CCNPP 33 ft (10 m) Annual JFD\}

## Page 6 of 8)

CC JANOO-DEC05 MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)

| 33.0 FT WIND DATA |  |  | STABILITY CLASS F |  |  |  |  |  | CLASS FREQUENCY |  |  | $($ PERCENT $)=10.37$ |  |  | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  | ND DI | RECTI | N FROM |  |  |  |  |  |  |  |  |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW |  |  |  |  |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 3 | 2 | 2 | 2 | 1 | 3 | 1 | 6 | 8 | 9 | 8 | 3 | 4 | 4 | 0 | 0 | 56 |
|  | . 00 | . 06 | . 04 | . 04 | . 04 | . 02 | . 06 | . 02 | . 11 | . 15 | . 17 | . 15 | . 06 | . 07 | . 07 | . 00 | . 00 | 1.05 |
|  | . 00 | . 01 | . 00 | . 00 | . 00 | . 00 | . 01 | . 00 | . 01 | . 02 | . 02 | . 02 | . 01 | . 01 | . 01 | . 00 | . 00 | . 11 |
| . $2-$ | 0 | 2 | 6 | 1 | 9 | 7 | 7 | 11 | 8 | 15 | 9 | 5 | 7 | 6 | 1 | 5 | 0 | 99 |
|  | . 00 | . 04 | . 11 | . 02 | . 17 | . 13 | . 13 | . 21 | . 15 | . 28 | . 17 | . 09 | . 13 | . 11 | . 02 | . 09 | . 00 | 1.85 |
|  | . 00 | . 00 | . 01 | . 00 | . 02 | . 01 | . 01 | . 02 | . 02 | . 03 | . 02 | . 01 | . 01 | . 01 | . 00 | . 01 | . 00 | . 19 |
| 5-1.0 | 26 | 25 | 34 | 22 | 16 | 34 | 24 | 40 | 86 | 133 | 150 | 95 | 71 | 61 | 24 | 27 | 0 | 868 |
| (1) | . 49 | . 47 | . 64 | . 41 | . 30 | . 64 | . 45 | . 75 | 1.61 | 2.49 | 2.81 | 1.78 | 1.33 | 1.14 | . 45 | . 51 | . 00 | 16.24 |
| $\begin{array}{r} \text { (2) } \\ 1.1-1.5 \end{array}$ | . 05 | . 05 | . 07 | . 04 | . 03 | . 07 | . 05 | . 08 | . 17 | . 26 | . 29 | . 18 | . 14 | . 12 | . 05 | . 05 | . 00 | 1.68 |
|  | 19 | 22 | 19 | 13 | 12 | 16 | 21 | 62 | 177 | 304 | 283 | 155 | 92 | 109 | 62 | 22 | 0 | 1388 |
| $\begin{array}{r} 1.1-1.5 \\ (1) \end{array}$ | . 36 | . 41 | . 36 | . 24 | . 22 | . 30 | . 39 | 1.16 | 3.31 | 5.69 | 5.30 | 2.90 | 1.72 | 2.04 | 1.16 | . 41 | . 00 | 25.97 |
| (2) | . 04 | . 04 | . 04 | . 03 | . 02 | . 03 | . 04 | . 12 | . 34 | . 59 | . 55 | . 30 | . 18 | . 21 | . 12 | . 04 | . 00 | 2.69 |
|  | 18 | 21 | 11 | 12 | 6 | 6 | 21 | 71 | 153 | 282 | 308 | 164 | 118 | 131 | 95 | 22 | 0 | 1439 |
| $\begin{array}{r} 1.6-2.0 \\ (1) \end{array}$ | . 34 | . 39 | . 21 | . 22 | . 11 | . 11 | . 39 | 1.33 | 2.86 | 5.28 | 5.76 | 3.07 | 2.21 | 2.45 | 1.78 | . 41 | . 00 | 26.93 |
| (2) | . 03 | . 04 | . 02 | . 02 | . 01 | . 01 | . 04 | . 14 | . 30 | . 55 | . 60 | . 32 | . 23 | . 25 | . 18 | . 04 | . 00 | 2.79 |
|  | 18 | 29 | 11 | 8 | 4 | 1 | 14 | 32 | 92 | 186 | 397 | 165 | 86 | 106 | 118 | 10 | 0 | 1277 |
| $2.1-3.0$ <br> (1) | . 34 | . 54 | . 21 | . 15 | . 07 | . 02 | . 26 | . 60 | 1.72 | 3.48 | 7.43 | 3.09 | 1.61 | 1.98 | 2.21 | . 19 | . 00 | 23.90 |
| (2) | . 03 | . 06 | . 02 | . 02 | . 01 | . 00 | . 03 | . 06 | . 18 | . 36 | . 77 | . 32 | . 17 | . 21 | . 23 | . 02 | . 00 | 2.48 |
|  | 2 | 6 | 2 | 2 | 0 | 0 | 0 | 1 | 11 | 25 | 71 | 15 | 6 | 5 | 11 | 0 | 0 | 157 |
| $\begin{array}{r} 3.1-4.0 \\ (1) \end{array}$ | . 04 | . 11 | . 04 | . 04 | . 00 | . 00 | . 00 | . 02 | . 21 | . 47 | 1.33 | . 28 | . 11 | . 09 | . 21 | . 00 | . 00 | 2.94 |
| (2) | . 00 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 05 | . 14 | . 03 | . 01 | . 01 | . 02 | . 00 | . 00 | . 30 |
|  | 3 | 4 | 3 | 8 | 2 | 0 | 0 | 0 | 1 | 1 | 11 | 0 | 1 | 0 | 2 | 0 | 0 | 36 |
| $\begin{array}{r} 4.1-5.0 \\ (1) \end{array}$ | . 06 | . 07 | . 06 | . 15 | . 04 | . 00 | . 00 | . 00 | . 02 | . 02 | . 21 | . 00 | . 02 | . 00 | . 04 | . 00 | . 00 | . 67 |
| (2) | . 01 | . 01 | . 01 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 |
| 5.1-6.0 | 5 | 1 | 2 | 6 | 2 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 2 | 0 | 21 |
| (1) | . 09 | . 02 | . 04 | . 11 | . 04 | . 00 | . 00 | . 00 | . 00 | . 00 | . 04 | . 00 | . 02 | . 00 | . 00 | . 04 | . 00 | . 39 |
| $6.1-8.0$ | . 01 | . 00 | . 00 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 04 |
|  | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| $\begin{array}{r} 6.1-8.0 \\ (1) \end{array}$ | . 02 | . 00 | . 04 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 06 |
| 8.1-10.0 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 |
|  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 92 | 113 | 92 | 74 | 53 | 65 | 90 | 218 | 534 | 954 | 1240 | 607 | 385 | 422 | 317 | 88 | 0 | 5344 |
| (1) | 1.72 | 2.11 | 1.72 | 1.38 | . 99 | 1.22 | 1.68 | 4.08 | 9.99 | 17.85 | 23.20 | 11.36 | 7.20 | 7.90 | 5.93 | 1.65 | . 00 | 100.00 |
| (2) | . 18 | . 22 | . 18 | . 14 | . 10 | . 13 | . 17 | . 42 | 1.04 | 1.85 | 2.41 | 1.18 | . 75 | . 82 | . 62 | . 17 | . 00 | 10.37 |

Table 2.3-16—\{CCNPP 33 ft ( 10 m) Annual JFD $\}$
(Page 7 of 8 )
CC JANOO-DECO5 MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
33.0 FT WIND DATA STABILITY CLASS G CLASS FREQUENCY (PERCENT) = 7.17

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Table 2．3－16—\｛CCNPP 33 ft（ 10 m）Annual JFD\}
（Page 8 of 8 ）
CC JANOO－DECO5 MET DATA JOINT FREQUENCY DISTRIBUTION（60－METER TOWER）
33．0 FT WIND DATA STABILITY CLASS ALL CLASS FREQUENCY（PERCENT）$=100.00$

|  |  |  |  |  |  |  |  | IND DI | EECTIO | N FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT | 3 | 7 | 2 | 4 | 5 | 3 | 8 | 10 | 21 | 18 | 32 | 30 | 9 | 6 | 10 | 4 | 0 | 172 |
|  | ． 01 | ． 01 | ． 00 | ． 01 | ． 01 | ． 01 | ． 02 | ． 02 | ． 04 | ． 03 | ． 06 | ． 06 | ． 02 | ． 01 | ． 02 | ． 01 | ． 00 | ． 33 |
|  | ． 01 | ． 01 | ． 00 | ． 01 | ． 01 | ． 01 | ． 02 | ． 02 | ． 04 | ． 03 | ． 06 | ． 06 | ． 02 | ． 01 | ． 02 | ． 01 | ． 00 | ． 33 |
| $\xrightarrow{.2-} \begin{array}{r}\text {（1）} \\ \text {（1）} \\ \text {（2）}\end{array}$ | 4 | 4 | 12 | 5 | 12 | 19 | 19 | 25 | 36 | 51 | 35 | 36 | 40 | 21 | 14 | 9 | 0 | 342 |
|  | ． 01 | ． 01 | ． 02 | ． 01 | ． 02 | ． 04 | ． 04 | ． 05 | ． 07 | ． 10 | ． 07 | ． 07 | ． 08 | ． 04 | ． 03 | ． 02 | ． 00 | ． 66 |
|  | ． 01 | ． 01 | ． 02 | ． 01 | ． 02 | ． 04 | ． 04 | ． 05 | ． 07 | ． 10 | ． 07 | ． 07 | ． 08 | ． 04 | ． 03 | ． 02 | ． 00 | ． 66 |
| ．5－1．0 | 115 | 101 | 112 | 83 | 118 | 139 | 127 | 172 | 276 | 385 | 474 | 380 | 285 | 236 | 120 | 129 | 0 | 3252 |
| （1） | ． 22 | ． 20 | ． 22 | ． 16 | ． 23 | ． 27 | ． 25 | ． 33 | ． 54 | ． 75 | ． 92 | ． 74 | ． 55 | ． 46 | ． 23 | ． 25 | ． 00 | 6.31 |
| 1．1－ $\begin{array}{r}\text {（2）} \\ \hline 1.5\end{array}$ | ． 22 | ． 20 | ． 22 | ． 16 | ． 23 | ． 27 | ． 25 | ． 33 | ． 54 | ． 75 | ． 92 | ． 74 | ． 55 | ． 46 | ． 23 | ． 25 | ． 00 | 6.31 |
|  | 201 | 214 | 182 | 182 | 238 | 190 | 201 | 284 | 546 | 975 | 1031 | 591 | 417 | 361 | 249 | 140 | 0 | 6002 |
| 1．1－1．5 | ． 39 | ． 42 | ． 35 | ． 35 | ． 46 | ． 37 | ． 39 | ． 55 | 1.06 | 1.89 | 2.00 | 1.15 | ． 81 | ． 70 | ． 48 | ． 27 | ． 00 | 11.65 |
| （2） | ． 39 | ． 42 | ． 35 | ． 35 | ． 46 | ． 37 | ． 39 | ． 55 | 1.06 | 1.89 | 2.00 | 1.15 | ． 81 | ． 70 | ． 48 | ． 27 | ． 00 | 11.65 |
| 1．6－2．0 | 320 | 433 | 281 | 349 | 360 | 269 | 282 | 391 | 629 | 950 | 1127 | 614 | 475 | 475 | 410 | 265 | 0 | 7630 |
| （1） | ． 62 | ． 84 | ． 55 | ． 68 | ． 70 | ． 52 | ． 55 | ． 76 | 1.22 | 1.84 | 2.19 | 1.19 | ． 92 | ． 92 | ． 80 | ． 51 | ． 00 | 14.81 |
| （2） | ． 62 | ． 84 | ． 55 | ． 68 | ． 70 | ． 52 | ． 55 | ． 76 | 1.22 | 1.84 | 2.19 | 1.19 | ． 92 | ． 92 | ． 80 | ． 51 | ． 00 | 14.81 |
| 2．1－3．0 | 972 | 1151 | 795 | 800 | 646 | 438 | 514 | 836 | 980 | 1205 | 1969 | 1084 | 624 | 676 | 1008 | 630 | 0 | 14328 |
| （1） | 1.89 | 2.23 | 1.54 | 1.55 | 1.25 | ． 85 | 1.00 | 1.62 | 1.90 | 2.34 | 3.82 | 2.10 | 1.21 | 1.31 | 1.96 | 1.22 | ． 00 | 27.81 |
| （2） | 1.89 | 2.23 | 1.54 | 1.55 | 1.25 | ． 85 | 1.00 | 1.62 | 1.90 | 2.34 | 3.82 | 2.10 | 1.21 | 1.31 | 1.96 | 1.22 | ． 00 | 27.81 |
| 3．1－4．0 | 1030 | 791 | 724 | 477 | 223 | 167 | 308 | 803 | 474 | 659 | 1406 | 625 | 365 | 394 | 794 | 669 | 0 | 9909 |
| （1） | 2.00 | 1.54 | 1.41 | ． 93 | ． 43 | ． 32 | ． 60 | 1.56 | ． 92 | 1.28 | 2.73 | 1.21 | ． 71 | ． 76 | 1.54 | 1.30 | ． 00 | 19.23 |
| （2） | 2.00 | 1.54 | 1.41 | ． 93 | ． 43 | ． 32 | ． 60 | 1.56 | ． 92 | 1.28 | 2.73 | 1.21 | ． 71 | ． 76 | 1.54 | 1.30 | ． 00 | 19.23 |
| 4．1－5．0 | 675 | 422 | 488 | 261 | 64 | 35 | 116 | 420 | 182 | 311 | 671 | 212 | 196 | 375 | 597 | 435 | 0 | 5460 |
| （1） | 1.31 | ． 82 | ． 95 | ． 51 | ． 12 | ． 07 | ． 23 | ． 82 | ． 35 | ． 60 | 1.30 | ． 41 | ． 38 | ． 73 | 1.16 | ． 84 | ． 00 | 10.60 |
| （2） | 1.31 | ． 82 | ． 95 | ． 51 | ． 12 | ． 07 | ． 23 | ． 82 | ． 35 | ． 60 | 1.30 | ． 41 | ． 38 | ． 73 | 1.16 | ． 84 | ． 00 | 10.60 |
| 5．1－6．0 | 397 | 226 | 306 | 130 | 5 | 7 | 34 | 192 | 52 | 97 | 245 | 57 | 93 | 281 | 428 | 182 | 0 | 2732 |
| （1） | ． 77 | ． 44 | ． 59 | ． 25 | ． 01 | ． 01 | ． 07 | ． 37 | ． 10 | ． 19 | ． 48 | ． 11 | ． 18 | ． 55 | ． 83 | ． 35 | ． 00 | 5.30 |
| （2） | ． 77 | ． 44 | ． 59 | ． 25 | ． 01 | ． 01 | ． 07 | ． 37 | ． 10 | ． 19 | ． 48 | ． 11 | ． 18 | ． 55 | ． 83 | ． 35 | ． 00 | 5.30 |
| 6．1－8．0 | 216 | 85 | 211 | 65 | 3 | 3 | 10 | 107 | 24 | 41 | 49 | 23 | 41 | 249 | 309 | 68 | 0 | 1504 |
| （1） | ． 42 | ． 16 | ． 41 | ． 13 | ． 01 | ． 01 | ． 02 | ． 21 | ． 05 | ． 08 | ． 10 | ． 04 | ． 08 | ． 48 | ． 60 | ． 13 | ． 00 | 2.92 |
| （2） | ． 42 | ． 16 | ． 41 | ． 13 | ． 01 | ． 01 | ． 02 | ． 21 | ． 05 | ． 08 | ． 10 | ． 04 | ． 08 | ． 48 | ． 60 | ． 13 | ． 00 | 2.92 |
| 8．1－10．0 | 27 | 7 | 30 | 10 | 1 | 0 | 3 | 6 | 1 | 2 | 1 | 1 | 5 | 40 | 32 | 3 | 0 | 169 |
| （1） | ． 05 | ． 01 | ． 06 | ． 02 | ． 00 | ． 00 | ． 01 | ． 01 | ． 00 | ． 00 | ． 00 | ． 00 | ． 01 | ． 08 | ． 06 | ． 01 | ． 00 | ． 33 |
| （2） | ． 05 | ． 01 | ． 06 | ． 02 | ． 00 | ． 00 | ． 01 | ． 01 | ． 00 | ． 00 | ． 00 | ． 00 | ． 01 | ． 08 | ． 06 | ． 01 | ． 00 | ． 33 |
| 10．1－89．5 | 5 | 2 | 4 | 3 |  | 2 | 3 |  | 0 | 0 | 0 | 0 | 1 | 2 | 1 | 0 | 0 | 25 |
| （1） | ． 01 | ． 00 | ． 01 | ． 01 | ． 00 | ． 00 | ． 01 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 05 |
| （2） | ． 01 | ． 00 | ． 01 | ． 01 | ． 00 | ． 00 | ． 01 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 05 |
| ALL SPEEDS | 3965 | 3443 | 3147 | 2369 | 1676 | 1272 | 1625 | 3247 | 3221 | 4694 | 7040 | 3653 | 2551 | 3116 | 3972 | 2534 | 0 | 51525 |
| （1）$(2)$ | 7.70 | 6.68 | 6.11 | 4.60 | 3.25 | 2.47 | 3.15 | 6.30 | 6.25 | 9.11 | 13.66 | 7.09 | 4.95 | 6.05 | 7.71 | 4.92 | ． 00 | 100.00 |
|  | 7.70 | 6.68 | 6.11 | 4.60 | 3.25 | 2.47 | 3.15 | 6.30 | 6.25 | 9.11 | 13.66 | 7.09 | 4.95 | 6.05 | 7.71 | 4.92 | ． 00 | 100.00 |
| （1）＝PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE（2）＝PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

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Table 2.3-17—\{CCNPP 197 ft ( 60 m) Annual JFD $\}$
(Page 1 of 8 )
CC JANOO-DECO5 MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA

STABILITY CLASS A
CLASS FREQUE
RECTION FROM

(1) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

## 킥키아d IHפוy

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CC JANOO-DECO5 MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS B CLASS FREQUENCY (PERCENT) = 4.58

|  |  |  |  |  |  |  |  | IND DI | RECTIO | V FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 7 |
| (1) | . 00 | . 04 | . 04 | . 00 | . 04 | . 00 | . 00 | . 04 | . 00 | . 00 | . 00 | . 00 | . 04 | . 00 | . 08 | . 00 | . 00 | . 30 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 |
| 1.1-1.5 | 2 | 4 | 2 | 5 | 3 | 3 | 3 | 1 | 0 | 0 | 4 | 2 | 1 | 0 | 0 | 0 | 0 | 30 |
| (1) | . 08 | . 17 | . 08 | . 21 | . 13 | . 13 | . 13 | . 04 | . 00 | . 00 | . 17 | . 08 | . 04 | . 00 | . 00 | . 00 | . 00 | 1.27 |
| (2) | . 00 | . 01 | . 00 | . 01 | . 01 | . 01 | . 01 | . 00 | . 00 | . 00 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 06 |
| 1.6-2.0 | 6 | 10 | 12 | 17 | 10 | 10 | 3 | 1 | 4 | 2 | 7 | 5 | 0 | 1 | 3 | 1 | 0 | 92 |
| (1) | . 25 | . 42 | . 51 | . 72 | . 42 | . 42 | . 13 | . 04 | . 17 | . 08 | . 30 | . 21 | . 00 | . 04 | . 13 | . 04 | . 00 | 3.89 |
| (2) | . 01 | . 02 | . 02 | . 03 | . 02 | . 02 | . 01 | . 00 | . 01 | . 00 | . 01 | . 01 | . 00 | . 00 | . 01 | . 00 | . 00 | . 18 |
| 2.1-3.0 | 56 | 75 | 43 | 33 | 58 | 28 | 22 | 15 | 12 | 22 | 21 | 31 | 14 | 9 | 4 | 13 | 0 | 456 |
| (1) | 2.37 | 3.17 | 1.82 | 1.40 | 2.45 | 1.18 | . 93 | . 63 | . 51 | . 93 | . 89 | 1.31 | . 59 | . 38 | . 17 | . 55 | . 00 | 19.28 |
| (2) | . 11 | . 15 | . 08 | . 06 | . 11 | . 05 | . 04 | . 03 | . 02 | . 04 | . 04 | . 06 | . 03 | . 02 | . 01 | . 03 | . 00 | . 88 |
| 3.1-4.0 | 79 | 78 | 14 | 9 | 13 | 18 | 35 | 40 | 17 | 22 | 43 | 34 | 27 | 24 | 12 | 15 | 0 | 480 |
| (1) | 3.34 | 3.30 | . 59 | . 38 | . 55 | . 76 | 1.48 | 1.69 | . 72 | . 93 | 1.82 | 1.44 | 1.14 | 1.01 | . 51 | . 63 | . 00 | 20.30 |
| (2) | . 15 | . 15 | . 03 | . 02 | . 03 | . 03 | . 07 | . 08 | . 03 | . 04 | . 08 | . 07 | . 05 | . 05 | . 02 | . 03 | . 00 | . 93 |
| 4.1-5.0 | 66 | 35 | 8 | 4 | 5 | 10 | 26 | 53 | 13 | 26 | 44 | 32 | 17 | 17 | 19 | 16 | 0 | 391 |
| (1) | 2.79 | 1.48 | . 34 | . 17 | . 21 | . 42 | 1.10 | 2.24 | . 55 | 1.10 | 1.86 | 1.35 | . 72 | . 72 | . 80 | . 68 | . 00 | 16.53 |
| (2) | . 13 | . 07 | . 02 | . 01 | . 01 | . 02 | . 05 | . 10 | . 03 | . 05 | . 09 | . 06 | . 03 | . 03 | . 04 | . 03 | . 00 | . 76 |
| 5.1-6.0 | 41 | 22 | 8 | 1 | 3 | 1 | 21 | 39 | 6 | 32 | 46 | 21 | 15 | 19 | 25 | 17 | 0 | 317 |
| (1) | 1.73 | . 93 | . 34 | . 04 | . 13 | . 04 | . 89 | 1.65 | . 25 | 1.35 | 1.95 | . 89 | . 63 | . 80 | 1.06 | . 72 | . 00 | 13.40 |
| (2) | . 08 | . 04 | . 02 | . 00 | . 01 | . 00 | . 04 | . 08 | . 01 | . 06 | . 09 | . 04 | . 03 | . 04 | . 05 | . 03 | . 00 | . 61 |
| 6.1-8.0 | 41 | 18 | 16 | 3 | 2 | 3 | 6 | 26 | 6 | 31 | 46 | 17 | 22 | 34 | 52 | 32 | 0 | 355 |
| (1) | 1.73 | . 76 | . 68 | . 13 | . 08 | . 13 | . 25 | 1.10 | . 25 | 1.31 | 1.95 | . 72 | . 93 | 1.44 | 2.20 | 1.35 | . 00 | 15.01 |
| (2) | . 08 | . 03 | . 03 | . 01 | . 00 | . 01 | . 01 | . 05 | . 01 | . 06 | . 09 | . 03 | . 04 | . 07 | . 10 | . 06 | . 00 | . 69 |
| 8.1-10.0 | 24 | 9 | 9 | 3 | 0 | 0 | 1 | 15 | 3 | 16 | 10 | 1 | 6 | 32 | 36 | 14 | 0 | 179 |
| (1) | 1.01 | . 38 | . 38 | . 13 | . 00 | . 00 | . 04 | . 63 | . 13 | . 68 | . 42 | . 04 | . 25 | 1.35 | 1.52 | . 59 | . 00 | 7.57 |
| (2) | . 05 | . 02 | . 02 | . 01 | . 00 | . 00 | . 00 | . 03 | . 01 | . 03 | . 02 | . 00 | . 01 | . 06 | . 07 | . 03 | . 00 | . 35 |
| 10.1-89.5 | 5 | 7 | 2 | 1 | 0 | 0 | 0 | 3 | 3 | 0 | 2 | 2 | 1 | 11 | 16 | 5 | 0 | 58 |
| (1) | . 21 | . 30 | . 08 | . 04 | . 00 | . 00 | . 00 | . 13 | . 13 | . 00 | . 08 | . 08 | . 04 | . 47 | . 68 | . 21 | . 00 | 2.45 |
| (2) | . 01 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 01 | . 00 | . 00 | . 00 | . 00 | . 02 | . 03 | . 01 | . 00 | . 11 |
| ALL SPEEDS | 320 | 259 | 115 | 76 | 95 | 73 | 117 | 194 | 64 | 151 | 223 | 145 | 104 | 147 | 169 | 113 | 0 | 2365 |
| (1) | 13.53 | 10.95 | 4.86 | 3.21 | 4.02 | 3.09 | 4.95 | 8.20 | 2.71 | 6.38 | 9.43 | 6.13 | 4.40 | 6.22 | 7.15 | 4.78 | . 00 | 100.00 |
| (2) | . 62 | . 50 | . 22 | . 15 | . 18 | . 14 | . 23 | . 38 | . 12 | . 29 | . 43 | . 28 | . 20 | . 28 | . 33 | . 22 | . 00 | 4.58 |

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## פᄏIכヨIOपd IHפוy

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CC JANOO-DECO5 MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS C CLASS FREQUENCY (PERCENT) = 5.03

| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 1 | 1 | 1 | 0 | 0 | 2 | 1 | 1 | 1 | 1 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 13 |
| (1) | . 04 | . 04 | . 04 | . 00 | . 00 | . 08 | . 04 | . 04 | . 04 | . 04 | . 00 | . 12 | . 00 | . 04 | . 00 | . 00 | . 00 | . 50 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 03 |
| 1.1-1.5 | 3 | 7 | 8 | 8 | 7 | 1 | 2 | 1 | 2 | 1 | 4 | 4 | 2 | 1 | 3 | 3 | 0 | 57 |
| (1) | . 12 | . 27 | . 31 | . 31 | . 27 | . 04 | . 08 | . 04 | . 08 | . 04 | . 15 | . 15 | . 08 | . 04 | . 12 | . 12 | . 00 | 2.19 |
| (2) | . 01 | . 01 | . 02 | . 02 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 01 | . 00 | . 00 | . 01 | . 01 | . 00 | . 11 |
| 1.6-2.0 | 14 | 30 | 21 | 26 | 26 | 10 | 6 | 6 | 2 | 3 | 15 | 10 | 7 | 5 | 4 | 3 | 0 | 188 |
| (1) | . 54 | 1.15 | . 81 | 1.00 | 1.00 | . 38 | . 23 | . 23 | . 08 | . 12 | . 58 | . 38 | . 27 | . 19 | . 15 | . 12 | . 00 | 7.24 |
| (2) | . 03 | . 06 | . 04 | . 05 | . 05 | . 02 | . 01 | . 01 | . 00 | . 01 | . 03 | . 02 | . 01 | . 01 | . 01 | . 01 | . 00 | . 36 |
| 2.1-3.0 | 60 | 91 | 46 | 54 | 48 | 37 | 31 | 25 | 18 | 13 | 35 | 22 | 17 | 17 | 4 | 10 | 0 | 528 |
| (1) | 2.31 | 3.50 | 1.77 | 2.08 | 1.85 | 1.42 | 1.19 | . 96 | . 69 | . 50 | 1.35 | . 85 | . 65 | . 65 | . 15 | . 38 | . 00 | 20.32 |
| (2) | . 12 | . 18 | . 09 | . 10 | . 09 | . 07 | . 06 | . 05 | . 03 | . 03 | . 07 | . 04 | . 03 | . 03 | . 01 | . 02 | . 00 | 1.02 |
| 3.1-4.0 | 94 | 84 | 24 | 13 | 15 | 23 | 26 | 37 | 21 | 20 | 46 | 44 | 22 | 17 | 26 | 28 | 0 | 540 |
| (1) | 3.62 | 3.23 | . 92 | . 50 | . 58 | . 89 | 1.00 | 1.42 | . 81 | . 77 | 1.77 | 1.69 | . 85 | . 65 | 1.00 | 1.08 | . 00 | 20.79 |
| (2) | . 18 | . 16 | . 05 | . 03 | . 03 | . 04 | . 05 | . 07 | . 04 | . 04 | . 09 | . 09 | . 04 | . 03 | . 05 | . 05 | . 00 | 1.05 |
| 4.1-5.0 | 55 | 41 | 10 | 3 | 9 | 7 | 16 | 64 | 14 | 32 | 42 | 33 | 20 | 18 | 30 | 29 | 0 | 423 |
| (1) | 2.12 | 1.58 | . 38 | . 12 | . 35 | . 27 | . 62 | 2.46 | . 54 | 1.23 | 1.62 | 1.27 | . 77 | . 69 | 1.15 | 1.12 | . 00 | 16.28 |
| (2) | . 11 | . 08 | . 02 | . 01 | . 02 | . 01 | . 03 | . 12 | . 03 | . 06 | . 08 | . 06 | . 04 | . 03 | . 06 | . 06 | . 00 | . 82 |
| 5.1-6.0 | 41 | 23 | 7 | 6 | 1 | 2 | 4 | 38 | 9 | 22 | 36 | 23 | 15 | 18 | 21 | 21 | 0 | 287 |
| (1) | 1.58 | . 89 | . 27 | . 23 | . 04 | . 08 | . 15 | 1.46 | . 35 | . 85 | 1.39 | . 89 | . 58 | . 69 | . 81 | . 81 | . 00 | 11.05 |
| (2) | . 08 | . 04 | . 01 | . 01 | . 00 | . 00 | . 01 | . 07 | . 02 | . 04 | . 07 | . 04 | . 03 | . 03 | . 04 | . 04 | . 00 | . 56 |
| 6.1-8.0 | 34 | 26 | 18 | 5 | 1 | 2 | 8 | 32 | 9 | 31 | 34 | 18 | 19 | 29 | 50 | 26 | 0 | 342 |
| (1) | 1.31 | 1.00 | . 69 | . 19 | . 04 | . 08 | . 31 | 1.23 | . 35 | 1.19 | 1.31 | . 69 | . 73 | 1.12 | 1.92 | 1.00 | . 00 | 13.16 |
| (2) | . 07 | . 05 | . 03 | . 01 | . 00 | . 00 | . 02 | . 06 | . 02 | . 06 | . 07 | . 03 | . 04 | . 06 | . 10 | . 05 | . 00 | . 66 |
| 8.1-10.0 | 13 | 23 | 9 | 3 | 1 | 0 | 1 | 9 | 2 | 8 | 15 | 2 | 5 | 28 | 29 | 7 | 0 | 155 |
| (1) | . 50 | . 89 | . 35 | . 12 | . 04 | . 00 | . 04 | . 35 | . 08 | . 31 | . 58 | . 08 | . 19 | 1.08 | 1.12 | . 27 | . 00 | 5.97 |
| (2) | . 03 | . 04 | . 02 | . 01 | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 03 | . 00 | . 01 | . 05 | . 06 | . 01 | . 00 | . 30 |
| 10.1-89.5 | 10 | 7 | 6 | 2 | 0 | 0 | 0 | 0 | 0 | 2 | 3 | 0 | 2 | 10 | 22 | 1 | 0 | 65 |
| (1) | . 38 | . 27 | . 23 | . 08 | . 00 | . 00 | . 00 | . 00 | . 00 | . 08 | . 12 | . 00 | . 08 | . 38 | . 85 | . 04 | . 00 | 2.50 |
| (2) | . 02 | . 01 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 00 | . 00 | . 02 | . 04 | . 00 | . 00 | . 13 |
| ALL SPEEDS | 325 | 333 | 150 | 120 | 108 | 84 | 95 | 213 | 78 | 133 | 230 | 159 | 109 | 144 | 189 | 128 | 0 | 2598 |
| (1) | 12.51 | 12.82 | 5.77 | 4.62 | 4.16 | 3.23 | 3.66 | 8.20 | 3.00 | 5.12 | 8.85 | 6.12 | 4.20 | 5.54 | 7.27 | 4.93 | . 00 | 100.00 |
| (2) | . 63 | . 64 | . 29 | . 23 | . 21 | . 16 | . 18 | . 41 | . 15 | . 26 | . 45 | . 31 | . 21 | . 28 | . 37 | . 25 | . 00 | 5.03 |

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Table 2.3-17—\{CCNPP 197 ft ( 60 m) Annual JFD\}

## (Page 4 of 8)

CC JANOO-DECO5 MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS D CLASS FREQUENCY (PERCENT) = 34.33

| $\begin{aligned} & \text { SPEED } \\ & \text { mps } \end{aligned}$ | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
|  | . 00 | . 01 | . 00 | . 00 | . 00 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 |
|  | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-$ | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 1 | 1 | 0 | 9 |
|  | . 00 | . 01 | . 00 | . 00 | . 01 | . 00 | . 00 | . 01 | . 00 | . 00 | . 00 | . 00 | . 01 | . 01 | . 01 | . 01 | . 00 | . 05 |
|  | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| . $5-1.0$ | 18 | 18 | 25 | 20 | 25 | 12 | 10 | 12 | 10 | 12 | 10 | 9 | 8 | 10 | 6 | 16 | 0 | 221 |
| (1) | . 10 | . 10 | . 14 | . 11 | . 14 | . 07 | . 06 | . 07 | . 06 | . 07 | . 06 | . 05 | . 05 | . 06 | . 03 | . 09 | . 00 | 1.25 |
|  | . 03 | . 03 | . 05 | . 04 | . 05 | . 02 | . 02 | . 02 | . 02 | . 02 | . 02 | . 02 | . 02 | . 02 | . 01 | . 03 | . 00 | . 43 |
|  | 40 | 42 | 42 | 49 | 54 | 33 | 23 | 14 | 15 | 16 | 18 | 21 | 21 | 15 | 18 | 20 | 0 | 441 |
| $\begin{array}{r} 1.1-1.5 \\ (1) \end{array}$ | . 23 | . 24 | . 24 | . 28 | . 30 | . 19 | . 13 | . 08 | . 08 | . 09 | . 10 | . 12 | . 12 | . 08 | . 10 | . 11 | . 00 | 2.49 |
| (2) | . 08 | . 08 | . 08 | . 09 | . 10 | . 06 | . 04 | . 03 | . 03 | . 03 | . 03 | . 04 | . 04 | . 03 | . 03 | . 04 | . 00 | . 85 |
|  | 63 | 96 | 66 | 84 | 109 | 57 | 35 | 20 | 28 | 17 | 48 | 32 | 28 | 24 | 27 | 46 | 0 | 780 |
| (1) | . 36 | . 54 | . 37 | . 47 | . 61 | . 32 | . 20 | . 11 | . 16 | . 10 | . 27 | . 18 | . 16 | . 14 | . 15 | . 26 | . 00 | 4.40 |
| 2.1- 3.0 | . 12 | . 19 | . 13 | . 16 | . 21 | . 11 | . 07 | . 04 | . 05 | . 03 | . 09 | . 06 | . 05 | . 05 | . 05 | . 09 | . 00 | 1.51 |
|  | 261 | 294 | 165 | 226 | 232 | 132 | 142 | 147 | 98 | 98 | 91 | 95 | 71 | 52 | 82 | 86 | 0 | 2272 |
| (1) | 1.47 | 1.66 | . 93 | 1.28 | 1.31 | . 74 | . 80 | . 83 | . 55 | . 55 | . 51 | . 54 | . 40 | . 29 | . 46 | . 49 | . 00 | 12.82 |
| 3.1-4.0 | . 51 | . 57 | . 32 | . 44 | . 45 | . 26 | . 28 | . 28 | . 19 | . 19 | . 18 | . 18 | . 14 | . 10 | . 16 | . 17 | . 00 | 4.40 |
|  | 247 | 242 | 158 | 261 | 209 | 175 | 175 | 210 | 152 | 109 | 146 | 123 | 82 | 94 | 125 | 176 | 0 | 2684 |
| (1) | 1.39 | 1.37 | . 89 | 1.47 | 1.18 | . 99 | . 99 | 1.18 | . 86 | . 61 | . 82 | . 69 | . 46 | . 53 | . 71 | . 99 | . 00 | 15.14 |
| $\begin{array}{r} (2) \\ 4.1-5.0 \end{array}$ | . 48 | . 47 | . 31 | . 51 | . 40 | . 34 | . 34 | . 41 | . 29 | . 21 | . 28 | . 24 | . 16 | . 18 | . 24 | . 34 | . 00 | 5.20 |
|  | 248 | 201 | 224 | 259 | 193 | 115 | 154 | 284 | 135 | 138 | 135 | 114 | 66 | 84 | 160 | 223 | 0 | 2733 |
| (1) | 1.40 | 1.13 | 1.26 | 1.46 | 1.09 | . 65 | . 87 | 1.60 | . 76 | . 78 | . 76 | . 64 | . 37 | . 47 | . 90 | 1.26 | . 00 | 15.42 |
| 5.1- 6.0 | . 48 | . 39 | . 43 | . 50 | . 37 | . 22 | . 30 | . 55 | . 26 | . 27 | . 26 | . 22 | . 13 | . 16 | . 31 | . 43 | . 00 | 5.29 |
|  | 224 | 215 | 241 | 200 | 83 | 69 | 101 | 264 | 87 | 114 | 141 | 107 | 57 | 93 | 239 | 286 | 0 | 2521 |
| (1) | 1.26 | 1.21 | 1.36 | 1.13 | . 47 | . 39 | . 57 | 1.49 | . 49 | . 64 | . 80 | . 60 | . 32 | . 52 | 1.35 | 1.61 | . 00 | 14.22 |
| 6.1- $\begin{array}{r}(2) \\ 8.0\end{array}$ | . 43 | . 42 | . 47 | . 39 | . 16 | . 13 | . 20 | . 51 | . 17 | . 22 | . 27 | . 21 | . 11 | . 18 | . 46 | . 55 | . 00 | 4.88 |
|  | 406 | 430 | 377 | 194 | 62 | 41 | 82 | 283 | 105 | 151 | 264 | 106 | 68 | 189 | 439 | 434 | 0 | 3631 |
| 6.1- 8.0 | 2.29 | 2.43 | 2.13 | 1.09 | . 35 | . 23 | . 46 | 1.60 | . 59 | . 85 | 1.49 | . 60 | . 38 | 1.07 | 2.48 | 2.45 | . 00 | 20.49 |
| $\begin{array}{r} (2) \\ 8.1-10.0 \end{array}$ | . 79 | . 83 | . 73 | . 38 | . 12 | . 08 | . 16 | . 55 | . 20 | . 29 | . 51 | . 21 | . 13 | . 37 | . 85 | . 84 | . 00 | 7.03 |
|  | 278 | 302 | 215 | 46 | 3 | 3 | 21 | 97 | 36 | 71 | 103 | 12 | 23 | 139 | 217 | 148 | 0 | 1714 |
| (1) | 1.57 | 1.70 | 1.21 | . 26 | . 02 | . 02 | . 12 | . 55 | . 20 | . 40 | . 58 | . 07 | . 13 | . 78 | 1.22 | . 84 | . 00 | 9.67 |
| $10.1-89.5$ | . 54 | . 58 | . 42 | . 09 | . 01 | . 01 | . 04 | . 19 | . 07 | . 14 | . 20 | . 02 | . 04 | . 27 | . 42 | . 29 | . 00 | 3.32 |
|  | 148 | 186 | 94 | 17 | 2 | 2 | 7 | 25 | 10 | 20 | 11 | 7 | 11 | 70 | 68 | 38 | 0 | 716 |
| $10.1-89.5$ <br> (1) | . 84 | 1.05 | . 53 | . 10 | . 01 | . 01 | . 04 | . 14 | . 06 | . 11 | . 06 | . 04 | . 06 | . 39 | . 38 | . 21 | . 00 | 4.04 |
| (2) | . 29 | . 36 | . 18 | . 03 | . 00 | . 00 | . 01 | . 05 | . 02 | . 04 | . 02 | . 01 | . 02 | . 14 | . 13 | . 07 | . 00 | 1.39 |
|  | 1933 | 2029 | 1607 | 1356 | 973 | 640 | 750 | 1357 | 676 | 746 | 967 | 626 | 436 | 772 | 1382 | 1474 | 0 | 17724 |
| ALL SPEEDS ${ }^{\text {(1) }}$ | 10.91 | 11.45 | 9.07 | 7.65 | 5.49 | 3.61 | 4.23 | 7.66 | 3.81 | 4.21 | 5.46 | 3.53 | 2.46 | 4.36 | 7.80 | 8.32 | . 00 | 100.00 |
|  | 3.74 | 3.93 | 3.11 | 2.63 | 1.88 | 1.24 | 1.45 | 2.63 | 1.31 | 1.44 | 1.87 | 1.21 | . 84 | 1.50 | 2.68 | 2.85 | . 00 | 34.33 |
| (1) = PERCENT | OF ALL | GOOD | OBSERV | TIONS | FOR | IS PA |  |  |  |  |  |  |  |  |  |  |  |  |

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Table 2.3-17—\{CCNPP 197 ft ( 60 m) Annual JFD\}
(Page 5 of 8)
CC JANOO-DECO5 MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS E CLASS FREQUENCY (PERCENT) = 26.79

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

CC JANOO-DECO5 MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS F CLASS FREQUENCY (PERCENT) = 10.32

|  |  |  |  |  |  |  |  | IND DI | IRECTIO | ON FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 3 |
| (1) | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 06 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 |
| . $2-.4$ | 2 | 1 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 9 |
| (1) | . 04 | . 02 | . 00 | . 00 | . 00 | . 02 | . 02 | . 02 | . 02 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 17 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| .5-1.0 | 6 | 5 | 6 | 10 | 10 | 12 | 7 | 8 | 6 | 10 | 10 | 5 | 6 | 5 | 7 | 5 | 0 | 118 |
| (1) | . 11 | . 09 | . 11 | . 19 | . 19 | . 23 | . 13 | . 15 | . 11 | . 19 | . 19 | . 09 | . 11 | . 09 | . 13 | . 09 | . 00 | 2.21 |
| (2) | . 01 | . 01 | . 01 | . 02 | . 02 | . 02 | . 01 | . 02 | . 01 | . 02 | . 02 | . 01 | . 01 | . 01 | . 01 | . 01 | . 00 | . 23 |
| 1.1-1.5 | 6 | 9 | 8 | 7 | 15 | 5 | 8 | 12 | 11 | 7 | 6 | 2 | 9 | 9 | 9 | 8 | 0 | 131 |
| (1) | . 11 | . 17 | . 15 | . 13 | . 28 | . 09 | . 15 | . 23 | . 21 | . 13 | . 11 | . 04 | . 17 | . 17 | . 17 | . 15 | . 00 | 2.46 |
| (2) | . 01 | . 02 | . 02 | . 01 | . 03 | . 01 | . 02 | . 02 | . 02 | . 01 | . 01 | . 00 | . 02 | . 02 | . 02 | . 02 | . 00 | . 25 |
| 1.6-2.0 | 7 | 6 | 11 | 14 | 16 | 13 | 17 | 10 | 12 | 14 | 12 | 11 | 9 | 10 | 10 | 11 | 0 | 183 |
| (1) | . 13 | . 11 | . 21 | . 26 | . 30 | . 24 | . 32 | . 19 | . 23 | . 26 | . 23 | . 21 | . 17 | . 19 | . 19 | . 21 | . 00 | 3.43 |
| (2) | . 01 | . 01 | . 02 | . 03 | . 03 | . 03 | . 03 | . 02 | . 02 | . 03 | . 02 | . 02 | . 02 | . 02 | . 02 | . 02 | . 00 | . 35 |
| 2.1-3.0 | 44 | 36 | 27 | 22 | 28 | 23 | 25 | 31 | 40 | 40 | 37 | 31 | 30 | 44 | 20 | 35 | 0 | 513 |
| (1) | . 83 | . 68 | . 51 | . 41 | . 53 | . 43 | . 47 | . 58 | . 75 | . 75 | . 69 | . 58 | . 56 | . 83 | . 38 | . 66 | . 00 | 9.63 |
| (2) | . 09 | . 07 | . 05 | . 04 | . 05 | . 04 | . 05 | . 06 | . 08 | . 08 | . 07 | . 06 | . 06 | . 09 | . 04 | . 07 | . 00 | . 99 |
| 3.1-4.0 | 40 | 20 | 25 | 16 | 16 | 25 | 46 | 50 | 90 | 80 | 81 | 65 | 53 | 49 | 48 | 49 | 0 | 753 |
| (1) | . 75 | . 38 | . 47 | . 30 | . 30 | . 47 | . 86 | . 94 | 1.69 | 1.50 | 1.52 | 1.22 | . 99 | . 92 | . 90 | . 92 | . 00 | 14.13 |
| (2) | . 08 | . 04 | . 05 | . 03 | . 03 | . 05 | . 09 | . 10 | . 17 | . 15 | . 16 | . 13 | . 10 | . 09 | . 09 | . 09 | . 00 | 1.46 |
| 4.1-5.0 | 38 | 20 | 9 | 5 | 4 | 9 | 34 | 83 | 135 | 139 | 125 | 96 | 90 | 86 | 80 | 90 | 0 | 1043 |
| (1) | . 71 | . 38 | . 17 | . 09 | . 08 | . 17 | . 64 | 1.56 | 2.53 | 2.61 | 2.35 | 1.80 | 1.69 | 1.61 | 1.50 | 1.69 | . 00 | 19.57 |
| (2) | . 07 | . 04 | . 02 | . 01 | . 01 | . 02 | . 07 | . 16 | . 26 | . 27 | . 24 | . 19 | . 17 | . 17 | . 15 | . 17 | . 00 | 2.02 |
| 5.1-6.0 | 15 | 9 | 4 | 3 | 0 | 3 | 23 | 92 | 243 | 226 | 147 | 105 | 101 | 95 | 111 | 69 | 0 | 1246 |
| (1) | . 28 | . 17 | . 08 | . 06 | . 00 | . 06 | . 43 | 1.73 | 4.56 | 4.24 | 2.76 | 1.97 | 1.90 | 1.78 | 2.08 | 1.29 | . 00 | 23.38 |
| (2) | . 03 | . 02 | . 01 | . 01 | . 00 | . 01 | . 04 | . 18 | . 47 | . 44 | . 28 | . 20 | . 20 | . 18 | . 21 | . 13 | . 00 | 2.41 |
| 6.1-8.0 | 10 | 12 | 10 | 8 | 3 | 1 | 8 | 61 | 203 | 317 | 252 | 115 | 49 | 54 | 125 | 18 | 0 | 1246 |
| (1) | . 19 | . 23 | . 19 | . 15 | . 06 | . 02 | . 15 | 1.14 | 3.81 | 5.95 | 4.73 | 2.16 | . 92 | 1.01 | 2.35 | . 34 | . 00 | 23.38 |
| (2) | . 02 | . 02 | . 02 | . 02 | . 01 | . 00 | . 02 | . 12 | . 39 | . 61 | . 49 | . 22 | . 09 | . 10 | . 24 | . 03 | . 00 | 2.41 |
| 8.1-10.0 | 5 | 2 | 1 | 3 | 0 | 0 | 0 | 0 | 5 | 24 | 30 | 2 | 1 | 1 | 1 | 0 | 0 | 75 |
| (1) | . 09 | . 04 | . 02 | . 06 | . 00 | . 00 | . 00 | . 00 | . 09 | . 45 | . 56 | . 04 | . 02 | . 02 | . 02 | . 00 | . 00 | 1.41 |
| (2) | . 01 | . 00 | . 00 | . 01 | . 00 | . 00 | . 00 | . 00 | . 01 | . 05 | . 06 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 15 |
| 10.1-89.5 | 4 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| (1) | . 08 | . 06 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 17 |
| (2) | . 01 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| ALL SPEEDS | 177 | 123 | 101 | 89 | 92 | 93 | 169 | 348 | 746 | 858 | 702 | 434 | 348 | 353 | 411 | 285 | 0 | 5329 |
| (1) | 3.32 | 2.31 | 1.90 | 1.67 | 1.73 | 1.75 | 3.17 | 6.53 | 14.00 | 16.10 | 13.17 | 8.14 | 6.53 | 6.62 | 7.71 | 5.35 | . 00 | 100.00 |
| (2) | . 34 | . 24 | . 20 | . 17 | . 18 | . 18 | . 33 | . 67 | 1.44 | 1.66 | 1.36 | . 84 | . 67 | . 68 | . 80 | . 55 | . 00 | 10.32 |

(1) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
ग्0
$\stackrel{N}{i}$
$i$

## 

Table 2.3-17—\{CCNPP 197 ft ( 60 m) Annual JFD\}

## (Page 7 of 8)

CC JANOO-DECO5 MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS G CLASS FREQUENCY (PERCENT) = 7.20

(1) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
ग्0
$\stackrel{0}{2}$
$i$

Table 2.3-17—\{CCNPP 197 ft ( 60 m) Annual JFD $\}$
(Page 8 of 8)
CC JANOO-DECO5 MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS ALL CLASS FREQUENCY (PERCENT) = 100.00

ग्0
$\stackrel{0}{2}$
$i$
CC JANUARY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) = Percent of all good observations for this period

| CC JANUARY MET DATA JOINT | FREQUENCY DISTRIBUTION | (60-METER TOWER) |  |
| :--- | :---: | :---: | :---: |
| 33.0 FT WIND DATA | STABILITY CLASS B | CLASS FREQUENCY | (PERCENT) $=3.36$ |

33.0 FT WIND DATA STABILITY CLASS B WIND DIRECTION FROM

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

| CC JANUARY MET DATA JOINT | FREQUENCY DISTRIBUTION | ( 60 -METER TOWER) |
| :--- | :---: | ---: | :---: |
| 33.0 FT WIND DATA | STABILITY CLASS C | CLASS FREQUENCY (PERCENT) $=4.20$ |


P
$\stackrel{0}{2}$
$i$



Table 2.3-18—\{CCNPP 33 ft (10 m) January JFD (2000-2005)\} (Page 4 of 8)

| CC JANUARY MET DATA JOINT FREQUENCY DISTRIBUTION | （60－METER TOWER） |  |
| :--- | :---: | :---: |
| 33．0 FT WIND DATA | STABILITY CLASS E | CLASS FREQUENCY（PERCENT）$=31.35$ |


| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT ． 2 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 7 |
| （1） | ． 07 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 07 | ． 15 | ． 00 | ． 07 | ． 00 | ． 00 | ． 00 | ． 07 | ． 07 | ． 00 | ． 00 | ． 52 |
| （2） | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 05 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 02 | ． 02 | ． 00 | ． 00 | ． 16 |
| ． $2-.4$ | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 7 |
| （1） | ． 00 | ． 07 | ． 07 | ． 00 | ． 00 | ． 00 | ． 07 | ． 07 | ． 00 | ． 00 | ． 00 | ． 07 | ． 07 | ． 00 | ． 07 | ． 00 | ． 00 | ． 52 |
| （2） | ． 00 | ． 02 | ． 02 | ． 00 | ． 00 | ． 00 | ． 02 | ． 02 | ． 00 | ． 00 | ． 00 | ． 02 | ． 02 | ． 00 | ． 02 | ． 00 | ． 00 | ． 16 |
| ． $5-1.0$ | 7 | 2 | 5 | 6 | 6 | 6 | 7 | 6 | 9 | 6 | 5 | 6 | 2 | 1 | 4 | 6 | 0 | 84 |
| （1） | ． 52 | ． 15 | ． 37 | ． 45 | ． 45 | ． 45 | ． 52 | ． 45 | ． 67 | ． 45 | ． 37 | ． 45 | ． 15 | ． 07 | ． 30 | ． 45 | ． 00 | 6.25 |
| （2） | ． 16 | ． 05 | ． 12 | ． 14 | ． 14 | ． 14 | ． 16 | ． 14 | ． 21 | ． 14 | ． 12 | ． 14 | ． 05 | ． 02 | ． 09 | ． 14 | ． 00 | 1.96 |
| 1．1－1．5 | 8 | 11 | 7 | 6 | 3 | 5 | 5 | 6 | 6 | 11 | 9 | 11 | 8 | 11 | 17 | 8 | 0 | 132 |
| （1） | ． 59 | ． 82 | ． 52 | ． 45 | ． 22 | ． 37 | ． 37 | ． 45 | ． 45 | ． 82 | ． 67 | ． 82 | ． 59 | ． 82 | 1.26 | ． 59 | ． 00 | 9.81 |
| （2） | ． 19 | ． 26 | ． 16 | ． 14 | ． 07 | ． 12 | ． 12 | ． 14 | ． 14 | ． 26 | ． 21 | ． 26 | ． 19 | ． 26 | ． 40 | ． 19 | ． 00 | 3.08 |
| 1．6－2．0 | 13 | 17 | 0 | 6 | 2 | 1 | 5 | 12 | 14 | 11 | 10 | 12 | 21 | 21 | 26 | 13 | 0 | 184 |
| （1） | ． 97 | 1.26 | ． 00 | ． 45 | ． 15 | ． 07 | ． 37 | ． 89 | 1.04 | ． 82 | ． 74 | ． 89 | 1.56 | 1.56 | 1.93 | ． 97 | ． 00 | 13.68 |
| （2） | ． 30 | ． 40 | ． 00 | ． 14 | ． 05 | ． 02 | ． 12 | ． 28 | ． 33 | ． 26 | ． 23 | ． 28 | ． 49 | ． 49 | ． 61 | ． 30 | ． 00 | 4.29 |
| 2．1－3．0 | 24 | 23 | 5 | 7 | 2 | 7 | 7 | 12 | 34 | 34 | 38 | 19 | 38 | 35 | 63 | 32 | 0 | 380 |
| （1） | 1.78 | 1.71 | ． 37 | ． 52 | ． 15 | ． 52 | ． 52 | ． 89 | 2.53 | 2.53 | 2.83 | 1.41 | 2.83 | 2.60 | 4.68 | 2.38 | ． 00 | 28.25 |
| （2） | ． 56 | ． 54 | ． 12 | ． 16 | ． 05 | ． 16 | ． 16 | ． 28 | ． 79 | ． 79 | ． 89 | ． 44 | ． 89 | ． 82 | 1.47 | ． 75 | ． 00 | 8.86 |
| 3．1－4．0 | 14 | 11 | 6 | 4 | 0 | 2 | 1 | 10 | 9 | 40 | 97 | 15 | 6 | 22 | 65 | 20 | 0 | 322 |
| （1） | 1.04 | ． 82 | ． 45 | ． 30 | ． 00 | ． 15 | ． 07 | ． 74 | ． 67 | 2.97 | 7.21 | 1.12 | ． 45 | 1.64 | 4.83 | 1.49 | ． 00 | 23.94 |
| （2） | ． 33 | ． 26 | ． 14 | ． 09 | ． 00 | ． 05 | ． 02 | ． 23 | ． 21 | ． 93 | 2.26 | ． 35 | ． 14 | ． 51 | 1.52 | ． 47 | ． 00 | 7.51 |
| 4．1－5．0 | 4 | 3 | 0 | 1 | 0 | 0 | 0 | 7 | 6 | 8 | 47 | 8 | 4 | 24 | 24 | 6 | 0 | 142 |
| (1) | ． 30 | ． 22 | ． 00 | ． 07 | ． 00 | ． 00 | ． 00 | ． 52 | ． 45 | ． 59 | 3.49 | ． 59 | ． 30 | 1.78 | 1.78 | ． 45 | ． 00 | 10.56 |
| （2） | ． 09 | ． 07 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 16 | ． 14 | ． 19 | 1.10 | ． 19 | ． 09 | ． 56 | ． 56 | ． 14 | ． 00 | 3.31 |
| 5．1－6．0 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 2 | 11 | 25 | 3 | 0 | 3 | 9 | 1 | 0 | 59 |
| （1） | ． 15 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 07 | ． 15 | ． 15 | ． 82 | 1.86 | ． 22 | ． 00 | ． 22 | ． 67 | ． 07 | ． 00 | 4.39 |
| （2） | ． 05 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 05 | ． 05 | ． 26 | ． 58 | ． 07 | ． 00 | ． 07 | ． 21 | ． 02 | ． 00 | 1.38 |
| 6．1－8．0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 4 | 2 | 1 | 0 | 8 | 5 | 0 | 0 | 25 |
| （1） | ． 07 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 15 | ． 15 | ． 30 | ． 15 | ． 07 | ． 00 | ． 59 | ． 37 | ． 00 | ． 00 | 1.86 |
| （2） | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 05 | ． 05 | ． 09 | ． 05 | ． 02 | ． 00 | ． 19 | ． 12 | ． 00 | ． 00 | ． 58 |
| 8．1－10．0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 2 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 07 | ． 07 | ． 00 | ． 00 | ． 15 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 02 | ． 00 | ． 00 | ． 05 |
| 10．1－89．5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 07 | ． 00 | ． 00 | ． 00 | ． 07 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 02 |
| ALL SPEEDS | 74 | 68 | 24 | 30 | 13 | 21 | 28 | 60 | 82 | 126 | 233 | 76 | 80 | 128 | 216 | 86 | 0 | 1345 |
| （1） | 5.50 | 5.06 | 1.78 | 2.23 | ． 97 | 1.56 | 2.08 | 4.46 | 6.10 | 9.37 | 17.32 | 5.65 | 5.95 | 9.52 | 16.06 | 6.39 | .00 | 100.00 |
| （2） | 1.72 | 1.59 | ． 56 | ． 70 | ． 30 | ． 49 | ． 65 | 1.40 | 1.91 | 2.94 | 5.43 | 1.77 | 1.86 | 2.98 | 5.03 | 2.00 | ． 00 | 31.35 |


| CC JANUARY MET DATA JOINT FREQUENCY DISTRIBUTION | $(60-M E T E R ~ T O W E R)$ |  |  |
| :--- | :---: | :---: | :---: |
| 33.0 FT WIND DATA | STABILITY CLASS F | CLASS FREQUENCY | (PERCENT) $=8$ |


|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { SPEED } \\ & \text { mps } \end{aligned}$ | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| LT . 2 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 6 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 26 | . 00 | . 00 | . 00 | . 00 | . 26 | . 52 | . 26 | . 00 | . 00 | . 26 | . 00 | . 00 | 1.57 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 | . 05 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 14 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 26 | . 00 | . 26 | . 00 | . 00 | . 52 | . 26 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.31 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 05 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 12 |
| .5-1.0 | 1 | 2 | 6 | 3 | 3 | 2 | 1 | 1 | 4 | 5 | 7 | 13 | 4 | 5 | 3 | 1 | 0 | 61 |
| (1) | . 26 | . 52 | 1.57 | . 79 | . 79 | . 52 | . 26 | . 26 | 1.05 | 1.31 | 1.84 | 3.41 | 1.05 | 1.31 | . 79 | . 26 | . 00 | 16.01 |
| (2) | . 02 | . 05 | . 14 | . 07 | . 07 | . 05 | . 02 | . 02 | . 09 | . 12 | . 16 | . 30 | . 09 | . 12 | . 07 | . 02 | . 00 | 1.42 |
| 1.1-1.5 | 2 | 2 | 3 | 4 | 2 | 0 | 1 | 2 | 9 | 8 | 9 | 11 | 11 | 5 | 3 | 1 | 0 | 73 |
| (1) | . 52 | . 52 | . 79 | 1.05 | . 52 | . 00 | . 26 | . 52 | 2.36 | 2.10 | 2.36 | 2.89 | 2.89 | 1.31 | . 79 | . 26 | . 00 | 19.16 |
| (2) | . 05 | . 05 | . 07 | . 09 | . 05 | . 00 | . 02 | . 05 | . 21 | . 19 | . 21 | . 26 | . 26 | . 12 | . 07 | . 02 | . 00 | 1.70 |
| 1.6-2.0 | 1 | 1 | 1 | 1 | 0 | 0 | 4 | 3 | 12 | 22 | 12 | 10 | 6 | 5 | 1 | 1 | 0 | 80 |
| (1) | . 26 | . 26 | . 26 | . 26 | . 00 | . 00 | 1.05 | . 79 | 3.15 | 5.77 | 3.15 | 2.62 | 1.57 | 1.31 | . 26 | . 26 | . 00 | 21.00 |
| (2) | . 02 | . 02 | . 02 | . 02 | . 00 | . 00 | . 09 | . 07 | . 28 | . 51 | . 28 | . 23 | . 14 | . 12 | . 02 | . 02 | . 00 | 1.86 |
| 2.1-3.0 | 0 | 4 | 0 | 2 | 0 | 0 | 1 | 4 | 7 | 32 | 34 | 13 | 10 | 6 | 6 | 0 | 0 | 119 |
| (1) | . 00 | 1.05 | . 00 | . 52 | . 00 | . 00 | . 26 | 1.05 | 1.84 | 8.40 | 8.92 | 3.41 | 2.62 | 1.57 | 1.57 | . 00 | . 00 | 31.23 |
| (2) | . 00 | . 09 | . 00 | . 05 | . 00 | . 00 | . 02 | . 09 | . 16 | . 75 | . 79 | . 30 | . 23 | . 14 | . 14 | . 00 | . 00 | 2.77 |
| $3.1-4.0$ | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 6 | 12 | 2 | 1 | 0 | 1 | 0 | 0 | 25 |
| (1) | . 00 | . 52 | . 00 | . 26 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.57 | 3.15 | . 52 | . 26 | . 00 | . 26 | . 00 | . 00 | 6.56 |
| (2) | . 00 | . 05 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 14 | . 28 | . 05 | . 02 | . 00 | . 02 | . 00 | . 00 | . 58 |
| 4.1-5.0 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| (1) | . 26 | . 79 | . 00 | . 00 | . 00 | . 00 | . 00 | .00 | . 00 | . 26 | . 26 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.57 |
| (2) | . 02 | . 07 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 14 |
| 5.1-6.0 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| (1) | 1.05 | . 26 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.31 |
| (2) | . 09 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 12 |
| $6.1-8.0$ | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 26 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 26 |
| (2) | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | O |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 10 | 15 | 10 | 11 | 7 | 2 | 8 | 10 | 32 | 77 | 78 | 50 | 32 | 21 | 15 | 3 | 0 | 381 |
| (1) | 2.62 | 3.94 | 2.62 | 2.89 | 1.84 | . 52 | 2.10 | 2.62 | 8.40 | 20.21 | 20.47 | 13.12 | 8.40 | 5.51 | 3.94 | . 79 | . 00 | 100.00 |
| (2) | . 23 | . 35 | . 23 | . 26 | . 16 | . 05 | . 19 | . 23 | . 75 | 1.79 | 1.82 | 1.17 | . 75 | . 49 | . 35 | . 07 | . 00 | 8.88 |


| CC JANUARY MET DATA JOINT FREQUENCY DISTRIBUTION | $(60-M E T E R ~ T O W E R)$ |  |  |
| :--- | :---: | ---: | :---: |
| 33.0 FT WIND DATA | STABILITY CLASS G | CLASS FREQUENCY | (PERCENT) $=3.50$ |


| $\begin{aligned} & \text { SPEED } \\ & \text { mps } \end{aligned}$ | N | NNE |  |  | E |  |  |  |  | SSW |  |  |  |  | NW |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 67 | . 00 | 1.33 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 2.00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 67 | . 00 | . 67 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.33 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 |
| . $5-1.0$ | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 4 | 4 | 4 | 1 | 2 | 2 | 2 | 1 | 0 | 0 | 23 |
| (1) | . 67 | . 00 | . 67 | . 67 | . 00 | . 00 | . 00 | 2.67 | 2.67 | 2.67 | . 67 | 1.33 | 1.33 | 1.33 | . 67 | . 00 | . 00 | 15.33 |
| (2) | . 02 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 09 | . 09 | . 09 | . 02 | . 05 | . 05 | . 05 | . 02 | . 00 | . 00 | . 54 |
| 1.1-1.5 | 1 | 1 | 0 | 5 | 0 | 1 | 0 | 1 | 4 | 4 | 5 | 3 | 2 | 2 | 1 | 0 | 0 | 30 |
| (1) | . 67 | . 67 | . 00 | 3.33 | . 00 | . 67 | . 00 | . 67 | 2.67 | 2.67 | 3.33 | 2.00 | 1.33 | 1.33 | . 67 | . 00 | . 00 | 20.00 |
| (2) | . 02 | . 02 | . 00 | . 12 | . 00 | . 02 | . 00 | . 02 | . 09 | . 09 | . 12 | . 07 | . 05 | . 05 | . 02 | . 00 | . 00 | . 70 |
| 1.6-2.0 | 0 | 1 | 0 | 2 | 0 | 4 | 1 | 4 | 6 | 16 | 10 | 4 | 1 | 3 | 0 | 1 | 0 | 53 |
| (1) | . 00 | . 67 | . 00 | 1.33 | . 00 | 2.67 | . 67 | 2.67 | 4.00 | 10.67 | 6.67 | 2.67 | . 67 | 2.00 | . 00 | . 67 | . 00 | 35.33 |
| (2) | . 00 | . 02 | . 00 | . 05 | . 00 | . 09 | . 02 | . 09 | . 14 | . 37 | . 23 | . 09 | . 02 | . 07 | . 00 | . 02 | . 00 | 1.24 |
| 2.1-3.0 | 0 | 0 | 2 | 0 | 0 | 1 | 0 | 1 | 3 | 10 | 17 | 2 | 0 | 0 | 1 | 0 | 0 | 37 |
| (1) | . 00 | . 00 | 1.33 | . 00 | . 00 | . 67 | . 00 | . 67 | 2.00 | 6.67 | 11.33 | 1.33 | . 00 | . 00 | . 67 | . 00 | . 00 | 24.67 |
| (2) | . 00 | . 00 | . 05 | . 00 | . 00 | . 02 | . 00 | . 02 | . 07 | . 23 | . 40 | . 05 | . 00 | . 00 | . 02 | . 00 | . 00 | . 86 |
| 3.1-4.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 67 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 67 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| 4.1-5.0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 67 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 67 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| 5.1-6.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 6.1-8.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 2 | 3 | 3 | 8 | 0 | 7 | 1 | 12 | 18 | 34 | 35 | 11 | 5 | 7 | 3 | 1 | 0 | 150 |
| (1) | 1.33 | 2.00 | 2.00 | 5.33 | . 00 | 4.67 | . 67 | 8.00 | 12.00 | 22.67 | 23.33 | 7.33 | 3.33 | 4.67 | 2.00 | . 67 | . 00 | 100.00 |
| (2) | . 05 | . 07 | . 07 | . 19 | . 00 | . 16 | . 02 | . 28 | . 42 | . 79 | . 82 | . 26 | . 12 | . 16 | . 07 | . 02 | . 00 | 3.50 |

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

Table 2.3-18—\{CCNPP 33 ft ( 10 m) January JFD (2000-2005)\} (Page 8 of 8 )


#### Abstract

CC JANUARY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER) 33.0 FT WIND DATA STABILITY CLASS ALL CLASS FREQUENCY (PERCENT) = 100.00


|  | WIND DIRECTION FROM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | EnE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 2 | 1 | 3 | 4 | 1 | 0 | 1 | 2 | 0 | 0 | 17 |
| (1) | . 02 | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 05 | . 02 | . 07 | . 09 | . 02 | . 00 | . 02 | . 05 | . 00 | . 00 | . 40 |
| (2) | . 02 | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 05 | . 02 | . 07 | . 09 | . 02 | . 00 | . 02 | . 05 | . 00 | . 00 | . 40 |
| . $2-.4$ | 0 | 1 | 1 | 0 | 1 | 1 | 2 | 2 | 0 | 2 | 1 | 1 | 1 | 0 | 1 | 0 | 0 | 14 |
| (1) | . 00 | . 02 | . 02 | . 00 | . 02 | . 02 | . 05 | . 05 | . 00 | . 05 | . 02 | . 02 | . 02 | . 00 | . 02 | . 00 | . 00 | . 33 |
| (2) | . 00 | . 02 | . 02 | . 00 | . 02 | . 02 | . 05 | . 05 | . 00 | . 05 | . 02 | . 02 | . 02 | . 00 | . 02 | . 00 | . 00 | . 33 |
| .5-1.0 | 9 | 7 | 16 | 11 | 11 | 10 | 14 | 13 | 19 | 21 | 18 | 25 | 10 | 13 | 12 | 9 | 0 | 218 |
| (1) | . 21 | . 16 | . 37 | . 26 | . 26 | . 23 | . 33 | . 30 | . 44 | . 49 | . 42 | . 58 | . 23 | . 30 | . 28 | . 21 | . 00 | 5.08 |
| (2) | . 21 | . 16 | . 37 | . 26 | . 26 | . 23 | . 33 | . 30 | . 44 | . 49 | . 42 | . 58 | . 23 | . 30 | . 28 | . 21 | . 00 | 5.08 |
| 1.1-1.5 | 14 | 24 | 19 | 26 | 13 | 10 | 12 | 14 | 24 | 29 | 32 | 29 | 26 | 19 | 28 | 13 | 0 | 332 |
| (1) | . 33 | . 56 | . 44 | . 61 | . 30 | . 23 | . 28 | . 33 | . 56 | . 68 | . 75 | . 68 | . 61 | . 44 | . 65 | . 30 | . 00 | 7.74 |
| (2) | . 33 | . 56 | . 44 | . 61 | . 30 | . 23 | . 28 | . 33 | . 56 | . 68 | . 75 | . 68 | . 61 | . 44 | . 65 | . 30 | . 00 | 7.74 |
| 1.6-2.0 | 31 | 35 | 15 | 27 | 12 | 13 | 22 | 30 | 42 | 66 | 39 | 36 | 42 | 34 | 36 | 18 | 0 | 498 |
| (1) | . 72 | . 82 | . 35 | . 63 | . 28 | . 30 | . 51 | . 70 | . 98 | 1.54 | . 91 | . 84 | . 98 | . 79 | . 84 | . 42 | . 00 | 11.61 |
| (2) | . 72 | . 82 | . 35 | . 63 | . 28 | . 30 | . 51 | . 70 | . 98 | 1.54 | . 91 | . 84 | . 98 | . 79 | . 84 | . 42 | . 00 | 11.61 |
| 2.1-3.0 | 74 | 79 | 36 | 39 | 21 | 17 | 25 | 34 | 59 | 98 | 126 | 79 | 76 | 69 | 121 | 67 | 0 | 1020 |
| (1) | 1.72 | 1.84 | . 84 | . 91 | . 49 | . 40 | . 58 | . 79 | 1.38 | 2.28 | 2.94 | 1.84 | 1.77 | 1.61 | 2.82 | 1.56 | . 00 | 23.78 |
| (2) | 1.72 | 1.84 | . 84 | . 91 | . 49 | . 40 | . 58 | . 79 | 1.38 | 2.28 | 2.94 | 1.84 | 1.77 | 1.61 | 2.82 | 1.56 | . 00 | 23.78 |
| 3.1-4.0 | 81 | 60 | 20 | 16 | 2 | 4 | 13 | 43 | 17 | 81 | 167 | 73 | 38 | 62 | 159 | 116 | 0 | 952 |
| (1) | 1.89 | 1.40 | . 47 | . 37 | . 05 | . 09 | . 30 | 1.00 | . 40 | 1.89 | 3.89 | 1.70 | . 89 | 1.45 | 3.71 | 2.70 | . 00 | 22.19 |
| (2) | 1.89 | 1.40 | . 47 | . 37 | . 05 | . 09 | . 30 | 1.00 | . 40 | 1.89 | 3.89 | 1.70 | . 89 | 1.45 | 3.71 | 2.70 | . 00 | 22.19 |
| 4.1-5.0 | 82 | 65 | 18 | 5 | 0 | 1 | 2 | 17 | 15 | 35 | 94 | 19 | 32 | 83 | 118 | 80 | 0 | 666 |
| (1) | 1.91 | 1.52 | . 42 | . 12 | . 00 | . 02 | . 05 | . 40 | . 35 | . 82 | 2.19 | . 44 | . 75 | 1.93 | 2.75 | 1.86 | . 00 | 15.52 |
| (2) | 1.91 | 1.52 | . 42 | . 12 | . 00 | . 02 | . 05 | . 40 | . 35 | . 82 | 2.19 | . 44 | . 75 | 1.93 | 2.75 | 1.86 | . 00 | 15.52 |
| 5.1-6.0 | 52 | 23 | 9 | 0 | 0 | 0 | 2 | 4 | 5 | 16 | 42 | 6 | 8 | 45 | 105 | 41 | 0 | 358 |
| (1) | 1.21 | . 54 | . 21 | . 00 | . 00 | . 00 | . 05 | . 09 | . 12 | . 37 | . 98 | . 14 | . 19 | 1.05 | 2.45 | . 96 | . 00 | 8.34 |
| (2) | 1.21 | . 54 | . 21 | . 00 | . 00 | . 00 | . 05 | . 09 | . 12 | . 37 | . 98 | . 14 | . 19 | 1.05 | 2.45 | . 96 | . 00 | 8.34 |
| 6.1-8.0 | 32 | 3 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 13 | 6 | 3 | 3 | 46 | 68 | 12 | 0 | 190 |
| (1) | . 75 | . 07 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 05 | . 30 | . 14 | . 07 | . 07 | 1.07 | 1.59 | . 28 | . 00 | 4.43 |
| (2) | . 75 | . 07 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 05 | . 30 | . 14 | . 07 | . 07 | 1.07 | 1.59 | . 28 | . 00 | 4.43 |
| 8.1-10.0 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 5 | 4 | 0 | 0 | 17 |
| (1) | . 12 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 12 | . 09 | . 00 | . 00 | . 40 |
| (2) | . 12 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 12 | . 09 | . 00 | . 00 | . 40 |
| 10.1-89.5 | 4 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 8 |
| (1) | . 09 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 00 | . 00 | . 19 |
| (2) | . 09 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 00 | . 00 | . 19 |
| ALL SPEEDS | 385 | 300 | 134 | 124 | 61 | 56 | 93 | 161 | 184 | 364 | 529 | 272 | 238 | 379 | 654 | 356 | 0 | 4290 |
| (1) | 8.97 | 6.99 | 3.12 | 2.89 | 1.42 | 1.31 | 2.17 | 3.75 | 4.29 | 8.48 | 12.33 | 6.34 | 5.55 | 8.83 | 15.24 | 8.30 | . 00 | 100.00 |
| (2) | 8.97 | 6.99 | 3.12 | 2.89 | 1.42 | 1.31 | 2.17 | 3.75 | 4.29 | 8.48 | 12.33 | 6.34 | 5.55 | 8.83 | 15.24 | 8.30 | . 00 | 100.00 |

## 

Table 2.3-19—\{CCNPP 33 ft ( 10 m ) February JFD (2000-2005) \}

## (Page 1 of 8)

CC FEBRUARY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
33.0 FT WIND DATA STABILITY CLASS A CLASS FREQUENCY (PERCENT) = 10.15

(1) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

| CC FEBRUARY MET DATA | JOINT | FREQUENCY DISTRIBUTION | （60－METER TOWER） |
| :--- | :--- | :--- | :--- |
| 33．0 FT WIND DATA | STABILITY CLASS B | CLASS FREQUENCY | （PERCENT）$=$ |


|  |  |  |  |  |  |  |  | D | CT | FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT ． 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| ． $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| ．5－1．0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| （1） | ． 00 | ． 00 | ． 57 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 57 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | 1.15 |
| （2） | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 05 |
| 1．1－1．5 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| （1） | ． 57 | ． 00 | ． 00 | ． 00 | ． 57 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | 1.15 |
| （2） | ． 02 | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 05 |
| 1．6－2．0 | 1 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 6 |
| （1） | ． 57 | ． 57 | ． 00 | ． 00 | ． 00 | ． 57 | ． 00 | ． 00 | ． 57 | ． 00 | ． 57 | ． 57 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | 3.45 |
| （2） | ． 02 | ． 02 | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 02 | ． 00 | ． 02 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 15 |
| 2．1－3．0 | 5 | 5 | 4 | 7 | 3 | 0 | 0 | 2 | 2 | 1 | 3 | 4 | 3 | 1 | 1 | 2 | 0 | 43 |
| （1） | 2.87 | 2.87 | 2.30 | 4.02 | 1.72 | ． 00 | ． 00 | 1.15 | 1.15 | ． 57 | 1.72 | 2.30 | 1.72 | ． 57 | ． 57 | 1.15 | ． 00 | 24.71 |
| （2） | ． 12 | ． 12 | ． 10 | ． 17 | ． 07 | ． 00 | ． 00 | ． 05 | ． 05 | ． 02 | ． 07 | ． 10 | ． 07 | ． 02 | ． 02 | ． 05 | ． 00 | 1.06 |
| $3.1-4.0$ | 10 | 3 | 4 | 0 | 2 | 0 | 1 | 5 | 1 | 2 | 5 | 3 | 2 | 1 | 2 | 0 | 0 | 41 |
| （1） | 5.75 | 1.72 | 2.30 | ． 00 | 1.15 | ． 00 | ． 57 | 2.87 | ． 57 | 1.15 | 2.87 | 1.72 | 1.15 | ． 57 | 1.15 | ． 00 | ． 00 | 23.56 |
| （2） | ． 25 | ． 07 | ． 10 | ． 00 | ． 05 | ． 00 | ． 02 | ． 12 | ． 02 | ． 05 | ． 12 | ． 07 | ． 05 | ． 02 | ． 05 | ． 00 | ． 00 | 1.01 |
| 4．1－5．0 | 8 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 2 | 6 | 4 | 7 | 2 | 1 | 5 | 3 | 0 | 40 |
| （1） | 4.60 | ． 00 | 1.15 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | 1.15 | 3.45 | 2.30 | 4.02 | 1.15 | ． 57 | 2.87 | 1.72 | ． 00 | 22.99 |
| （2） | ． 20 | ． 00 | ． 05 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 05 | ． 15 | ． 10 | ． 17 | ． 05 | ． 02 | ． 12 | ． 07 | ． 00 | ． 99 |
| 5．1－6．0 | 9 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 2 | 0 | 3 | 1 | 11 | 2 | 0 | 32 |
| （1） | 5.17 | ． 57 | ． 57 | ． 00 | ． 00 | ． 00 | ． 00 | ． 57 | ． 00 | ． 57 | 1.15 | ． 00 | 1.72 | ． 57 | 6.32 | 1.15 | ． 00 | 18.39 |
| （2） | ． 22 | ． 02 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 02 | ． 05 | ． 00 | ． 07 | ． 02 | ． 27 | ． 05 | ． 00 | ． 79 |
| $6.1-8.0$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 3 | 2 | 1 | 0 | 8 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 57 | ． 57 | ． 00 | 1.72 | 1.15 | ． 57 | ． 00 | 4.60 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 02 | ． 00 | ． 07 | ． 05 | ． 02 | ． 00 | ． 20 |
| 8．1－10．0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| 10．1－89．5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| ALL SPEEDS | 34 | 10 | 12 | 7 | 6 | 1 | 1 | 8 | 7 | 10 | 16 | 16 | 10 | 7 | 21 | 8 | 0 | 174 |
| （1） | 19.54 | 5.75 | 6.90 | 4.02 | 3.45 | ． 57 | ． 57 | 4.60 | 4.02 | 5.75 | 9.20 | 9.20 | 5.75 | 4.02 | 12.07 | 4.60 | ． 00 | 100.00 |
| （2） | ． 84 | ． 25 | ． 30 | ． 17 | ． 15 | ． 02 | ． 02 | ． 20 | ． 17 | ． 25 | ． 40 | ． 40 | ． 25 | ． 17 | ． 52 | ． 20 | ． 00 | 4.31 |

ग्0
$\stackrel{0}{2}$
$i$
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| CC FEBRUARY MET DATA JOINT | FREQUENCY DISTRIBUTION | $(60$-METER TOWER) |
| :--- | :--- | :--- | :--- | :--- |
| 33.0 FT WIND DATA | STABILITY CLASS C | CLASS FREQUENCY (PERCENT) $=3.94$ |


|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { SPEED } \\ & \text { mps } \end{aligned}$ | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 63 | . 00 | . 00 | . 00 | . 00 | . 00 | . 63 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| 1.1-1.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 2 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 63 | . 00 | . 63 | . 00 | 1.26 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 05 |
| 1.6-2.0 | 1 | 1 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 9 |
| (1) | . 63 | . 63 | . 00 | 1.26 | . 63 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.26 | . 63 | . 63 | . 00 | . 00 | . 00 | . 00 | 5.66 |
| (2) | . 02 | . 02 | . 00 | . 05 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 22 |
| 2.1-3.0 | 6 | 8 | 6 | 6 | 1 | 0 | 1 | 3 | 2 | 3 | 5 | 5 | 3 | 1 | 1 | 1 | 0 | 52 |
| (1) | 3.77 | 5.03 | 3.77 | 3.77 | . 63 | . 00 | . 63 | 1.89 | 1.26 | 1.89 | 3.14 | 3.14 | 1.89 | . 63 | . 63 | . 63 | . 00 | 32.70 |
| (2) | . 15 | . 20 | . 15 | . 15 | . 02 | . 00 | . 02 | . 07 | . 05 | . 07 | . 12 | . 12 | . 07 | . 02 | . 02 | . 02 | . 00 | 1.29 |
| 3.1-4.0 | 6 | 7 | 11 | 0 | 0 | 0 | 2 | 5 | 2 | 3 | 3 | 5 | 1 | 2 | 1 | 1 | 0 | 49 |
| (1) | 3.77 | 4.40 | 6.92 | . 00 | . 00 | . 00 | 1.26 | 3.14 | 1.26 | 1.89 | 1.89 | 3.14 | . 63 | 1.26 | . 63 | . 63 | . 00 | 30.82 |
| (2) | . 15 | . 17 | . 27 | . 00 | . 00 | . 00 | . 05 | . 12 | . 05 | . 07 | . 07 | . 12 | . 02 | . 05 | . 02 | . 02 | . 00 | 1.21 |
| 4.1-5.0 | 6 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 5 | 3 | 0 | 1 | 4 | 5 | 0 | 29 |
| (1) | 3.77 | . 00 | 1.26 | . 00 | . 00 | . 00 | . 00 | . 00 | . 63 | 1.26 | 3.14 | 1.89 | . 00 | . 63 | 2.52 | 3.14 | . 00 | 18.24 |
| (2) | . 15 | . 00 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 05 | . 12 | . 07 | . 00 | . 02 | . 10 | . 12 | . 00 | . 72 |
| 5.1-6.0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 2 | 2 | 1 | 0 | 9 |
| (1) | . 63 | . 00 | . 63 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 63 | . 63 | . 00 | 1.26 | 1.26 | . 63 | . 00 | 5.66 |
| (2) | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 05 | . 05 | . 02 | . 00 | . 22 |
| $6.1-8.0$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 5 | 0 | 0 | 8 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 63 | . 00 | . 00 | 1.26 | 3.14 | . 00 | . 00 | 5.03 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 05 | . 12 | . 00 | . 00 | . 20 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 20 | 16 | 20 | 8 | 2 | 0 | 3 | 8 | 5 | 8 | 17 | 16 | 5 | 9 | 13 | 9 | 0 | 159 |
| (1) | 12.58 | 10.06 | 12.58 | 5.03 | 1.26 | . 00 | 1.89 | 5.03 | 3.14 | 5.03 | 10.69 | 10.06 | 3.14 | 5.66 | 8.18 | 5.66 | . 00 | 100.00 |
| (2) | . 50 | . 40 | . 50 | . 20 | . 05 | . 00 | . 07 | . 20 | . 12 | . 20 | . 42 | . 40 | . 12 | . 22 | . 32 | . 22 | . 00 | 3.94 |
| (1) = PERCENT | OF ALI | G GOOD | OBSERV | TIONS | FOR | IS PA |  |  |  |  |  |  |  |  |  |  |  |  |

P
$\stackrel{0}{2}$
$i$


Table 2.3-19—\{CCNPP 33 ft (10 m) February JFD (2000-2005)\}
(Page 4 of 8)
CC FEBRUARY MET DA
33.0 FT WIND DATA

CLASS FREQ

T
$\stackrel{0}{0}$
$i$
$i$


Table 2.3-19—\{CCNPP 33 ft (10 m) February JFD (2000-2005)\}
(Page 5 of 8)
CC FEBRUARY MET DA
33.0 FT WIND DATA

CLASS FREQ


| CC FEBRUARY MET DATA JOINT | FREQUENCY DISTRIBUTION | $(60$-METER TOWER) |  |
| :--- | :--- | :--- | :--- |
| 33.0 FT WIND DATA | STABILITY CLASS F | CLASS FREQUENCY | (PERCENT) $=10.57$ |


| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 5 |
| (1) | . 00 | . 23 | . 00 | . 23 | . 00 | . 00 | . 23 | . 00 | . 00 | . 00 | . 23 | . 23 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.17 |
| (2) | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 12 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 2 | 1 | 1 | 1 | 0 | 2 | 1 | 0 | 1 | 0 | 0 | 2 | 0 | 11 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 47 | . 23 | . 23 | . 23 | . 00 | . 47 | . 23 | . 00 | . 23 | . 00 | . 00 | . 47 | . 00 | 2.58 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 05 | . 02 | . 02 | . 02 | . 00 | . 05 | . 02 | . 00 | . 02 | . 00 | . 00 | . 05 | . 00 | . 27 |
| . 5- 1.0 | 1 | 2 | 1 | 2 | 2 | 3 | 2 | 2 | 9 | 3 | 6 | 4 | 3 | 2 | 3 | 3 | 0 | 48 |
| (1) | . 23 | . 47 | . 23 | . 47 | . 47 | . 70 | . 47 | . 47 | 2.11 | . 70 | 1.41 | . 94 | . 70 | . 47 | . 70 | . 70 | . 00 | 11.24 |
| (2) | . 02 | . 05 | . 02 | . 05 | . 05 | . 07 | . 05 | . 05 | . 22 | . 07 | . 15 | . 10 | . 07 | . 05 | . 07 | . 07 | . 00 | 1.19 |
| 1.1-1.5 | 4 | 6 | 4 | 0 | 4 | 3 | 2 | 3 | 15 | 15 | 9 | 8 | 3 | 4 | 7 | 2 | 0 | 89 |
| (1) | . 94 | 1.41 | . 94 | . 00 | . 94 | . 70 | . 47 | . 70 | 3.51 | 3.51 | 2.11 | 1.87 | . 70 | . 94 | 1.64 | . 47 | . 00 | 20.84 |
| (2) | . 10 | . 15 | . 10 | . 00 | . 10 | . 07 | . 05 | . 07 | . 37 | . 37 | . 22 | . 20 | . 07 | . 10 | . 17 | . 05 | . 00 | 2.20 |
| 1.6-2.0 | 5 | 7 | 5 | 2 | 2 | 0 | 2 | 9 | 16 | 27 | 31 | 20 | 12 | 4 | 4 | 1 | 0 | 147 |
| (1) | 1.17 | 1.64 | 1.17 | . 47 | . 47 | . 00 | . 47 | 2.11 | 3.75 | 6.32 | 7.26 | 4.68 | 2.81 | . 94 | . 94 | . 23 | . 00 | 34.43 |
| (2) | . 12 | . 17 | . 12 | . 05 | . 05 | . 00 | . 05 | . 22 | . 40 | . 67 | . 77 | . 50 | . 30 | . 10 | . 10 | . 02 | . 00 | 3.64 |
| 2.1-3.0 | 3 | 6 | 4 | 2 | 0 | 0 | 1 | 7 | 10 | 21 | 20 | 20 | 12 | 6 | 4 | 0 | 0 | 116 |
| (1) | . 70 | 1.41 | . 94 | . 47 | . 00 | . 00 | . 23 | 1.64 | 2.34 | 4.92 | 4.68 | 4.68 | 2.81 | 1.41 | . 94 | . 00 | . 00 | 27.17 |
| (2) | . 07 | . 15 | . 10 | . 05 | . 00 | . 00 | . 02 | . 17 | . 25 | . 52 | . 50 | . 50 | . 30 | . 15 | . 10 | . 00 | . 00 | 2.87 |
| 3.1-4.0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 3 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 9 |
| (1) | . 23 | . 23 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 47 | . 70 | . 23 | . 00 | . 23 | . 00 | . 00 | . 00 | . 00 | 2.11 |
| (2) | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 07 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 22 |
| 4.1-5.0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| (1) | . 23 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 23 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 47 |
| (2) | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 |
| 5.1-6.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | .00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 6.1-8.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 15 | 23 | 14 | 7 | 10 | 7 | 9 | 22 | 52 | 71 | 70 | 53 | 32 | 16 | 18 | 8 | 0 | 427 |
| (1) | 3.51 | 5.39 | 3.28 | 1.64 | 2.34 | 1.64 | 2.11 | 5.15 | 12.18 | 16.63 | 16.39 | 12.41 | 7.49 | 3.75 | 4.22 | 1.87 | . 00 | 100.00 |
| (2) | . 37 | . 57 | . 35 | . 17 | . 25 | . 17 | . 22 | . 54 | 1.29 | 1.76 | 1.73 | 1.31 | . 79 | . 40 | . 45 | . 20 | . 00 | 10.57 |


| CC FEBRUARY MET DATA JOINT | FREQUENCY DISTRIBUTION | ( 60 -METER TOWER) |  |
| :--- | :--- | :--- | :--- | :--- |
| 33.0 FT WIND DATA | STABILITY CLASS G | CLASS FREQUENCY | (PERCENT) $=\quad 3.84$ |


|  | WIND DIRECTION F |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 |
| (1) | . 00 | . 65 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 65 | . 00 | . 00 | 1.29 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 05 |
| . $2-.4$ | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| (1) | . 00 | . 00 | . 00 | . 65 | . 00 | . 65 | . 00 | . 00 | . 65 | . 65 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 2.58 |
| (2) | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 10 |
| .5-1.0 | 0 | 0 | 3 | 1 | 2 | 0 | 1 | 3 | 2 | 3 | 1 | 4 | 2 | 0 | 0 | 1 | 0 | 23 |
| (1) | . 00 | . 00 | 1.94 | . 65 | 1.29 | . 00 | . 65 | 1.94 | 1.29 | 1.94 | . 65 | 2.58 | 1.29 | . 00 | . 00 | . 65 | . 00 | 14.84 |
| (2) | . 00 | . 00 | . 07 | . 02 | . 05 | . 00 | . 02 | . 07 | . 05 | . 07 | . 02 | . 10 | . 05 | . 00 | . 00 | . 02 | . 00 | . 57 |
| 1.1-1.5 | 0 | 3 | 2 | 1 | 1 | 1 | 0 | 2 | 6 | 5 | 10 | 8 | 3 | 1 | 0 | 0 | 0 | 43 |
| (1) | . 00 | 1.94 | 1.29 | . 65 | . 65 | . 65 | . 00 | 1.29 | 3.87 | 3.23 | 6.45 | 5.16 | 1.94 | . 65 | . 00 | . 00 | . 00 | 27.74 |
| (2) | . 00 | . 07 | . 05 | . 02 | . 02 | . 02 | . 00 | . 05 | . 15 | . 12 | . 25 | . 20 | . 07 | . 02 | . 00 | . 00 | . 00 | 1.06 |
| 1.6-2.0 | 0 | 3 | 0 | 4 | 0 | 0 | 0 | 0 | 5 | 11 | 13 | 11 | 1 | 1 | 0 | 0 | 0 | 49 |
| (1) | . 00 | 1.94 | . 00 | 2.58 | . 00 | . 00 | . 00 | . 00 | 3.23 | 7.10 | 8.39 | 7.10 | . 65 | . 65 | . 00 | . 00 | . 00 | 31.61 |
| (2) | . 00 | . 07 | . 00 | . 10 | . 00 | . 00 | . 00 | . 00 | . 12 | . 27 | . 32 | . 27 | . 02 | . 02 | . 00 | . 00 | . 00 | 1.21 |
| 2.1-3.0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 4 | 10 | 9 | 2 | 2 | 0 | 0 | 0 | 32 |
| (1) | . 00 | . 65 | . 00 | . 00 | . 00 | . 00 | . 65 | . 65 | 1.29 | 2.58 | 6.45 | 5.81 | 1.29 | 1.29 | . 00 | . 00 | . 00 | 20.65 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 05 | . 10 | . 25 | . 22 | . 05 | . 05 | . 00 | . 00 | . 00 | . 79 |
| 3.1-4.0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| (1) | . 00 | . 65 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 65 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.29 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 |
| 4.1-5.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 5.1-6.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 6.1-8.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 0 | 9 | 5 | 7 | 3 | 2 | 2 | 6 | 16 | 24 | 35 | 32 | 8 | 4 | 1 | 1 | 0 | 155 |
| (1) | . 00 | 5.81 | 3.23 | 4.52 | 1.94 | 1.29 | 1.29 | 3.87 | 10.32 | 15.48 | 22.58 | 20.65 | 5.16 | 2.58 | . 65 | . 65 | . 00 | 100.00 |
| (2) | . 00 | . 22 | . 12 | . 17 | . 07 | . 05 | . 05 | . 15 | . 40 | . 59 | . 87 | . 79 | . 20 | . 10 | . 02 | . 02 | . 00 | 3.84 |

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
Table 2.3-19—\{CCNPP 33 ft (10 m) February JFD (2000-2005)\} (Page 8 of 8)
CC FEBRUARY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)

$\stackrel{70}{\stackrel{7}{i}}$

Table 2.3-20—\{CCNPP 33 ft ( 10 m ) March JFD (2000-2005) \}
(Page 1 of 8)
CC MARCH MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
33.0 FT WIND DATA STABILITY CLASS A CLASS FREQUENCY (PERCENT) = 12.30

(1) =PERCENT OF ALL GOOD OBSERVATIONS FOR this PAGE
(2) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
 CC MARCH MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)


## 

CC MARCH MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
33.0 FT WIND DATA STABILITY CLASS C CLASS FREQUENCY (PERCENT) = 4.18

| SPEED | N | NNE | NE | ENE | E | ESE | SE ${ }^{\text {W }}$ | WIND DIRECTION FROM |  |  | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT $\begin{array}{r}\text {. } 2 \\ \\ \\ \\ \\ \\ (1)\end{array}$ |  |  |  |  |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
|  | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-\quad \begin{array}{r}\text { (1) } \\ (1) \\ \\ \\ \text { (2) }\end{array}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
|  | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 55 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 55 |
| 1.1- 1.5 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
|  | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 55 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 55 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| 1.6-2.0 | 1 | 1 | 2 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 10 |
| (1) | . 55 | . 55 | 1.10 | . 00 | . 00 | . 55 | . 00 | . 00 | . 55 | . 00 | 1.66 | . 00 | . 55 | . 00 | . 00 | . 00 | . 00 | 5.52 |
| $\begin{array}{r} (2) \\ 2.1-3.0 \end{array}$ | . 02 | . 02 | . 05 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 07 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 23 |
|  | 7 | 9 | 4 | 5 | 3 | 4 | 1 | 1 | 1 | 2 | 4 | 5 | 2 | 2 | 1 | 1 | 0 | 52 |
| $\begin{array}{r} 2.1-3.0 \\ (1) \end{array}$ | 3.87 | 4.97 | 2.21 | 2.76 | 1.66 | 2.21 | . 55 | . 55 | . 55 | 1.10 | 2.21 | 2.76 | 1.10 | 1.10 | . 55 | . 55 | . 00 | 28.73 |
| $3.1-4.0$ | . 16 | . 21 | . 09 | . 12 | . 07 | . 09 | . 02 | . 02 | . 02 | . 05 | . 09 | . 12 | . 05 | . 05 | . 02 | . 02 | . 00 | 1.20 |
|  | 8 | 3 | 5 | 4 | 1 | 3 | 0 | 7 | 3 | 2 | 2 | 3 | 1 | 2 | 3 | 2 | 0 | 49 |
| $\begin{array}{r} 3.1-4.0 \\ (1) \end{array}$ | 4.42 | 1.66 | 2.76 | 2.21 | . 55 | 1.66 | . 00 | 3.87 | 1.66 | 1.10 | 1.10 | 1.66 | . 55 | 1.10 | 1.66 | 1.10 | . 00 | 27.07 |
| $4.1-5.0$ | . 18 | . 07 | . 12 | . 09 | . 02 | . 07 | . 00 | . 16 | . 07 | . 05 | . 05 | . 07 | . 02 | . 05 | . 07 | . 05 | . 00 | 1.13 |
|  | 4 | 2 | 1 | 1 | 0 | 0 | 2 | 6 | 1 | 1 | 2 | 2 | 2 | 2 | 5 | 3 | 0 | 34 |
| $\begin{array}{r} 4.1-5.0 \\ (1) \end{array}$ | 2.21 | 1.10 | . 55 | . 55 | . 00 | . 00 | 1.10 | 3.31 | . 55 | . 55 | 1.10 | 1.10 | 1.10 | 1.10 | 2.76 | 1.66 | . 00 | 18.78 |
| $5.1-6.0$ | . 09 | . 05 | . 02 | . 02 | . 00 | . 00 | . 05 | . 14 | . 02 | . 02 | . 05 | . 05 | . 05 | . 05 | . 12 | . 07 | . 00 | . 78 |
|  | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 4 | 1 | 0 | 1 | 0 | 1 | 3 | 3 | 0 | 0 | 14 |
| (1) | . 00 | . 00 | . 55 | . 00 | . 00 | . 00 | . 00 | 2.21 | . 55 | . 00 | . 55 | . 00 | . 55 | 1.66 | 1.66 | . 00 | . 00 | 7.73 |
| $6.1-8.0$ | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 09 | . 02 | . 00 | . 02 | . 00 | . 02 | . 07 | . 07 | . 00 | . 00 | . 32 |
|  | 2 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 3 | 7 | 3 | 0 | 19 |
| $\begin{array}{r} 6.1-8.0 \\ (1) \end{array}$ | 1.10 | 1.10 | . 55 | . 00 | . 00 | . 00 | . 00 | . 55 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.66 | 3.87 | 1.66 | . 00 | 10.50 |
| 8.1-10.0 | . 05 | . 05 | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 | . 16 | . 07 | . 00 | . 44 |
|  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 55 | . 00 | . 55 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 |
|  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10.1-89.5 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
|  | 22 | 17 | 14 | 10 | 4 | 9 | 3 | 19 | 7 | 5 | 13 | 10 | 7 | 12 | 19 | 10 | 0 | 181 |
| ALL SPEEDS <br> (1) | 12.15 | 9.39 | 7.73 | 5.52 | 2.21 | 4.97 | 1.66 | 10.50 | 3.87 | 2.76 | 7.18 | 5.52 | 3.87 | 6.63 | 10.50 | 5.52 | . 00 | 100.00 |
| (2) | . 51 | . 39 | . 32 | . 23 | . 09 | . 21 | . 07 | . 44 | . 16 | . 12 | . 30 | . 23 | . 16 | . 28 | . 44 | . 23 | . 00 | 4.18 |
| (1) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

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ग्0
$\stackrel{N}{i}$
$i$

CC MARCH MET DATA JOINT FREQUENCY DISTRIBUTION（60－METER TOWER）
33．0 FT WIND DATA STABILITY CLASS D CLASS FREQUENCY（PERCENT）＝ 37.34

|  |  |  |  |  |  |  |  | D | T | N FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT ． 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| ． $2-.4$ | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 3 |
| （1） | ． 06 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 06 | ． 06 | ． 00 | ． 00 | ． 00 | ． 19 |
| （2） | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 02 | ． 00 | ． 00 | ． 00 | ． 07 |
| ．5－1．0 | 3 | 3 | 3 | 1 | 2 | 4 | 1 | 2 | 2 | 3 | 6 | 1 | 1 | 2 | 2 | 1 | 0 | 37 |
| （1） | ． 19 | ． 19 | ． 19 | ． 06 | ． 12 | ． 25 | ． 06 | ． 12 | ． 12 | ． 19 | ． 37 | ． 06 | ． 06 | ． 12 | ． 12 | ． 06 | ． 00 | 2.29 |
| （2） | ． 07 | ． 07 | ． 07 | ． 02 | ． 05 | ． 09 | ． 02 | ． 05 | ． 05 | ． 07 | ． 14 | ． 02 | ． 02 | ． 05 | ． 05 | ． 02 | ． 00 | ． 85 |
| 1．1－1．5 | 7 | 10 | 2 | 6 | 9 | 6 | 7 | 5 | 6 | 2 | 6 | 6 | 2 | 2 | 4 | 3 | 0 | 83 |
| （1） | ． 43 | ． 62 | ． 12 | ． 37 | ． 56 | ． 37 | ． 43 | ． 31 | ． 37 | ． 12 | ． 37 | ． 37 | ． 12 | ． 12 | ． 25 | ． 19 | ． 00 | 5.13 |
| （2） | ． 16 | ． 23 | ． 05 | ． 14 | ． 21 | ． 14 | ． 16 | ． 12 | ． 14 | ． 05 | ． 14 | ． 14 | ． 05 | ． 05 | ． 09 | ． 07 | ． 00 | 1.92 |
| 1．6－2．0 | 13 | 18 | 14 | 19 | 11 | 13 | 7 | 6 | 13 | 7 | 5 | 2 | 2 | 1 | 6 | 4 | 0 | 141 |
| （1） | ． 80 | 1.11 | ． 87 | 1.17 | ． 68 | ． 80 | ． 43 | ． 37 | ． 80 | ． 43 | ． 31 | ． 12 | ． 12 | ． 06 | ． 37 | ． 25 | ． 00 | 8.71 |
| （2） | ． 30 | ． 42 | ． 32 | ． 44 | ． 25 | ． 30 | ． 16 | ． 14 | ． 30 | ． 16 | ． 12 | ． 05 | ． 05 | ． 02 | ． 14 | ． 09 | ． 00 | 3.25 |
| 2．1－3．0 | 36 | 37 | 40 | 44 | 29 | 22 | 21 | 35 | 20 | 14 | 12 | 13 | 7 | 6 | 10 | 20 | 0 | 366 |
| （1） | 2.22 | 2.29 | 2.47 | 2.72 | 1.79 | 1.36 | 1.30 | 2.16 | 1.24 | ． 87 | ． 74 | ． 80 | ． 43 | ． 37 | ． 62 | 1.24 | ． 00 | 22.62 |
| （2） | ． 83 | ． 85 | ． 92 | 1.02 | ． 67 | ． 51 | ． 48 | ． 81 | ． 46 | ． 32 | ． 28 | ． 30 | ． 16 | ． 14 | ． 23 | ． 46 | ． 00 | 8.45 |
| 3．1－4．0 | 36 | 15 | 26 | 42 | 20 | 7 | 15 | 36 | 18 | 11 | 11 | 8 | 10 | 12 | 24 | 33 | 0 | 324 |
| （1） | 2.22 | ． 93 | 1.61 | 2.60 | 1.24 | ． 43 | ． 93 | 2.22 | 1.11 | ． 68 | ． 68 | ． 49 | ． 62 | ． 74 | 1.48 | 2.04 | ． 00 | 20.02 |
| （2） | ． 83 | ． 35 | ． 60 | ． 97 | ． 46 | ． 16 | ． 35 | ． 83 | ． 42 | ． 25 | ． 25 | ． 18 | ． 23 | ． 28 | ． 55 | ． 76 | ． 00 | 7.48 |
| 4．1－5．0 | 35 | 34 | 17 | 23 | 7 | 1 | 9 | 27 | 6 | 7 | 17 | 8 | 7 | 13 | 39 | 38 | 0 | 288 |
| （1） | 2.16 | 2.10 | 1.05 | 1.42 | ． 43 | ． 06 | ． 56 | 1.67 | ． 37 | ． 43 | 1.05 | ． 49 | ． 43 | ． 80 | 2.41 | 2.35 | ． 00 | 17.80 |
| （2） | ． 81 | ． 78 | ． 39 | ． 53 | ． 16 | ． 02 | ． 21 | ． 62 | ． 14 | ． 16 | ． 39 | ． 18 | ． 16 | ． 30 | ． 90 | ． 88 | ． 00 | 6.65 |
| 5．1－6．0 | 40 | 18 | 25 | 15 | 0 | 2 | 0 | 17 | 1 | 3 | 7 | 3 | 3 | 17 | 37 | 13 | 0 | 201 |
| （1） | 2.47 | 1.11 | 1.55 | ． 93 | ． 00 | ． 12 | ． 00 | 1.05 | ． 06 | ． 19 | ． 43 | ． 19 | ． 19 | 1.05 | 2.29 | ． 80 | ． 00 | 12.42 |
| （2） | ． 92 | ． 42 | ． 58 | ． 35 | ． 00 | ． 05 | ． 00 | ． 39 | ． 02 | ． 07 | ． 16 | ． 07 | ． 07 | ． 39 | ． 85 | ． 30 | ． 00 | 4.64 |
| 6．1－8．0 | 35 | 15 | 16 | 15 | 0 | 1 | 0 | 10 | 2 | 0 | 1 | 0 | 3 | 10 | 31 | 12 | 0 | 151 |
| （1） | 2.16 | ． 93 | ． 99 | ． 93 | ． 00 | ． 06 | ． 00 | ． 62 | ． 12 | ． 00 | ． 06 | ． 00 | ． 19 | ． 62 | 1.92 | ． 74 | ． 00 | 9.33 |
| （2） | ． 81 | ． 35 | ． 37 | ． 35 | ． 00 | ． 02 | ． 00 | ． 23 | ． 05 | ． 00 | ． 02 | ． 00 | ． 07 | ． 23 | ． 72 | ． 28 | ． 00 | 3.48 |
| 8．1－10．0 | 3 | 1 | 0 | 6 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 4 | 5 | 2 | 0 | 23 |
| （1） | ． 19 | ． 06 | ． 00 | ． 37 | ． 00 | ． 00 | ． 00 | ． 06 | ． 06 | ． 00 | ． 00 | ． 00 | ． 00 | ． 25 | ． 31 | ． 12 | ． 00 | 1.42 |
| （2） | ． 07 | ． 02 | ． 00 | ． 14 | ． 00 | ． 00 | ． 00 | ． 02 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 09 | ． 12 | ． 05 | ． 00 | ． 53 |
| 10．1－89．5 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| （1） | ． 00 | ． 00 | ． 00 | ． 06 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 06 |
| （2） | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 |
| ALL SPEEDS | 209 | 151 | 143 | 172 | 78 | 56 | 60 | 139 | 69 | 47 | 65 | 41 | 36 | 68 | 158 | 126 | 0 | 1618 |
| （1） | 12.92 | 9.33 | 8.84 | 10.63 | 4.82 | 3.46 | 3.71 | 8.59 | 4.26 | 2.90 | 4.02 | 2.53 | 2.22 | 4.20 | 9.77 | 7.79 | ． 00 | 100.00 |
| （2） | 4.82 | 3.48 | 3.30 | 3.97 | 1.80 | 1.29 | 1.38 | 3.21 | 1.59 | 1.08 | 1.50 | ． 95 | ． 83 | 1.57 | 3.65 | 2.91 | ． 00 | 37.34 |


#### Abstract

CC MARCH MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER) 33.0 FT WIND DATA STABILITY CLASS E CLASS FREQUENCY (PERCENT) = 29.22


| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 1 | 0 | 7 |
| (1) | . 00 | . 08 | . 00 | . 00 | . 00 | . 08 | . 08 | . 00 | . 00 | . 00 | . 16 | . 08 | . 00 | . 00 | . 00 | . 08 | . 00 | . 55 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 05 | . 02 | . 00 | . 00 | . 00 | . 02 | . 00 | . 16 |
| . $2-.4$ | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 2 | 2 | 0 | 0 | 1 | 1 | 1 | 1 | 0 | 11 |
| (1) | . 08 | . 00 | . 00 | . 00 | . 00 | . 08 | . 08 | . 00 | . 16 | . 16 | . 00 | . 00 | . 08 | . 08 | . 08 | . 08 | . 00 | . 87 |
| (2) | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 05 | . 05 | . 00 | . 00 | . 02 | . 02 | . 02 | . 02 | . 00 | . 25 |
| .5-1.0 | 7 | 8 | 1 | 4 | 1 | 4 | 5 | 3 | 3 | 6 | 6 | 8 | 4 | 5 | 6 | 8 | 0 | 79 |
| (1) | . 55 | . 63 | . 08 | . 32 | . 08 | . 32 | . 39 | . 24 | . 24 | . 47 | . 47 | . 63 | . 32 | . 39 | . 47 | . 63 | . 00 | 6.24 |
| (2) | . 16 | . 18 | . 02 | . 09 | . 02 | . 09 | . 12 | . 07 | . 07 | . 14 | . 14 | . 18 | . 09 | . 12 | . 14 | . 18 | . 00 | 1.82 |
| 1.1-1.5 | 11 | 3 | 8 | 6 | 10 | 9 | 3 | 3 | 9 | 8 | 18 | 8 | 2 | 6 | 9 | 9 | 0 | 122 |
| (1) | . 87 | . 24 | . 63 | . 47 | . 79 | . 71 | . 24 | . 24 | . 71 | . 63 | 1.42 | . 63 | . 16 | . 47 | . 71 | . 71 | . 00 | 9.64 |
| (2) | . 25 | . 07 | . 18 | . 14 | . 23 | . 21 | . 07 | . 07 | . 21 | . 18 | . 42 | . 18 | . 05 | . 14 | . 21 | . 21 | . 00 | 2.82 |
| 1.6-2.0 | 15 | 9 | 10 | 7 | 10 | 7 | 12 | 6 | 11 | 11 | 10 | 6 | 11 | 20 | 6 | 21 | 0 | 172 |
| (1) | 1.18 | . 71 | . 79 | . 55 | . 79 | . 55 | . 95 | . 47 | . 87 | . 87 | . 79 | . 47 | . 87 | 1.58 | . 47 | 1.66 | . 00 | 13.59 |
| (2) | . 35 | . 21 | . 23 | . 16 | . 23 | . 16 | . 28 | . 14 | . 25 | . 25 | . 23 | . 14 | . 25 | . 46 | . 14 | . 48 | . 00 | 3.97 |
| 2.1-3.0 | 30 | 23 | 13 | 7 | 6 | 2 | 3 | 21 | 49 | 36 | 17 | 12 | 13 | 28 | 51 | 31 | 0 | 342 |
| (1) | 2.37 | 1.82 | 1.03 | . 55 | . 47 | . 16 | . 24 | 1.66 | 3.87 | 2.84 | 1.34 | . 95 | 1.03 | 2.21 | 4.03 | 2.45 | . 00 | 27.01 |
| (2) | . 69 | . 53 | . 30 | . 16 | . 14 | . 05 | . 07 | . 48 | 1.13 | . 83 | . 39 | . 28 | . 30 | . 65 | 1.18 | . 72 | . 00 | 7.89 |
| 3.1-4.0 | 32 | 7 | 9 | 10 | 1 | 3 | 2 | 17 | 40 | 35 | 44 | 16 | 7 | 17 | 25 | 27 | 0 | 292 |
| (1) | 2.53 | . 55 | . 71 | . 79 | . 08 | . 24 | . 16 | 1.34 | 3.16 | 2.76 | 3.48 | 1.26 | . 55 | 1.34 | 1.97 | 2.13 | . 00 | 23.06 |
| (2) | . 74 | . 16 | . 21 | . 23 | . 02 | . 07 | . 05 | . 39 | . 92 | . 81 | 1.02 | . 37 | . 16 | . 39 | . 58 | . 62 | . 00 | 6.74 |
| 4.1-5.0 | 16 | 8 | 2 | 1 | 1 | 1 | 2 | 13 | 12 | 26 | 40 | 2 | 6 | 11 | 18 | 6 | 0 | 165 |
| (1) | 1.26 | . 63 | . 16 | . 08 | . 08 | . 08 | . 16 | 1.03 | . 95 | 2.05 | 3.16 | . 16 | . 47 | . 87 | 1.42 | . 47 | . 00 | 13.03 |
| (2) | . 37 | . 18 | . 05 | . 02 | . 02 | . 02 | . 05 | . 30 | . 28 | . 60 | . 92 | . 05 | . 14 | . 25 | . 42 | . 14 | . 00 | 3.81 |
| 5.1-6.0 | 12 | 2 | 0 | 0 | 0 | 1 | 1 | 2 | 11 | 6 | 8 | 0 | 1 | 2 | 6 | 4 | 0 | 56 |
| (1) | . 95 | . 16 | . 00 | . 00 | . 00 | . 08 | . 08 | . 16 | . 87 | . 47 | . 63 | . 00 | . 08 | . 16 | . 47 | . 32 | . 00 | 4.42 |
| (2) | . 28 | . 05 | . 00 | . 00 | . 00 | . 02 | . 02 | . 05 | . 25 | . 14 | . 18 | . 00 | . 02 | . 05 | . 14 | . 09 | . 00 | 1.29 |
| 6.1-8.0 | 4 | 0 | 0 | 0 | 0 | 1 | 2 | 3 | 2 | 1 | 1 | 0 | 0 | 1 | 2 | 0 | 0 | 17 |
| (1) | . 32 | . 00 | . 00 | . 00 | . 00 | . 08 | . 16 | . 24 | . 16 | . 08 | . 08 | . 00 | . 00 | . 08 | . 16 | . 00 | . 00 | 1.34 |
| (2) | . 09 | . 00 | . 00 | . 00 | . 00 | . 02 | . 05 | . 07 | . 05 | . 02 | . 02 | . 00 | . 00 | . 02 | . 05 | . 00 | . 00 | . 39 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 3 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 08 | . 00 | . 00 | . 00 | . 00 | . 00 | . 16 | . 00 | . 00 | . 00 | . 24 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 00 | . 00 | . 07 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 128 | 61 | 43 | 35 | 29 | 30 | 32 | 69 | 139 | 131 | 146 | 53 | 45 | 93 | 124 | 108 | 0 | 1266 |
| (1) | 10.11 | 4.82 | 3.40 | 2.76 | 2.29 | 2.37 | 2.53 | 5.45 | 10.98 | 10.35 | 11.53 | 4.19 | 3.55 | 7.35 | 9.79 | 8.53 | . 00 | 100.00 |
| (2) | 2.95 | 1.41 | . 99 | . 81 | . 67 | . 69 | . 74 | 1.59 | 3.21 | 3.02 | 3.37 | 1.22 | 1.04 | 2.15 | 2.86 | 2.49 | . 00 | 29.22 |


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$\begin{array}{lcccc}\text { CC MARCH MET DATA JOINT FREQUENCY DISTRIBUTION } & \text { (60-METER TOWER) } & \\ \text { 33.0 FT WIND DATA } & \text { STABILITY CLASS F } & \text { CLASS FREQUENCY (PERCENT) }=\mathbf{9 . 7 9 ~}\end{array}$

| WIND DIRECTION FROM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { SPEED } \\ & \text { mps } \end{aligned}$ | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| LT . 2 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 6 |
| (1) | . 00 | . 24 | . 24 | . 00 | . 24 | . 00 | . 00 | . 00 | . 00 | . 00 | . 24 | . 24 | . 00 | . 24 | . 00 | . 00 | . 00 | 1.42 |
| (2) | . 00 | . 02 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 14 |
| . $2-.4$ | 0 | 1 | 0 | 0 | 1 | 1 | 1 | 1 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 8 |
| (1) | . 00 | . 24 | . 00 | . 00 | . 24 | . 24 | . 24 | . 24 | . 00 | . 00 | . 24 | . 00 | . 24 | . 24 | . 00 | . 00 | . 00 | 1.89 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 02 | . 02 | . 02 | . 02 | . 00 | . 00 | . 02 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 18 |
| . $5-1.0$ | 3 | 5 | 6 | 0 | 1 | 3 | 1 | 0 | 3 | 2 | 7 | 4 | 6 | 3 | 2 | 1 | 0 | 47 |
| (1) | . 71 | 1.18 | 1.42 | . 00 | . 24 | . 71 | . 24 | . 00 | . 71 | . 47 | 1.65 | . 94 | 1.42 | . 71 | . 47 | . 24 | . 00 | 11.08 |
| (2) | . 07 | . 12 | . 14 | . 00 | . 02 | . 07 | . 02 | . 00 | . 07 | . 05 | . 16 | . 09 | . 14 | . 07 | . 05 | . 02 | . 00 | 1.08 |
| 1.1-1.5 | 2 | 5 | 6 | 0 | 1 | 2 | 3 | 0 | 9 | 12 | 15 | 6 | 8 | 4 | 1 | 1 | 0 | 75 |
| (1) | . 47 | 1.18 | 1.42 | . 00 | . 24 | . 47 | . 71 | . 00 | 2.12 | 2.83 | 3.54 | 1.42 | 1.89 | . 94 | . 24 | . 24 | . 00 | 17.69 |
| (2) | . 05 | . 12 | . 14 | . 00 | . 02 | . 05 | . 07 | . 00 | . 21 | . 28 | . 35 | . 14 | . 18 | . 09 | . 02 | . 02 | . 00 | 1.73 |
| 1.6-2.0 | 5 | 4 | 2 | 6 | 3 | 2 | 0 | 3 | 13 | 17 | 12 | 9 | 13 | 11 | 6 | 3 | 0 | 109 |
| (1) | 1.18 | . 94 | . 47 | 1.42 | . 71 | . 47 | . 00 | . 71 | 3.07 | 4.01 | 2.83 | 2.12 | 3.07 | 2.59 | 1.42 | . 71 | . 00 | 25.71 |
| (2) | . 12 | . 09 | . 05 | . 14 | . 07 | . 05 | . 00 | . 07 | . 30 | . 39 | . 28 | . 21 | . 30 | . 25 | . 14 | . 07 | . 00 | 2.52 |
| 2.1-3.0 | 7 | 14 | 4 | 3 | 2 | 0 | 2 | 6 | 9 | 19 | 25 | 9 | 5 | 7 | 5 | 2 | 0 | 119 |
| (1) | 1.65 | 3.30 | . 94 | . 71 | . 47 | . 00 | . 47 | 1.42 | 2.12 | 4.48 | 5.90 | 2.12 | 1.18 | 1.65 | 1.18 | . 47 | . 00 | 28.07 |
| (2) | . 16 | . 32 | . 09 | . 07 | . 05 | . 00 | . 05 | . 14 | . 21 | . 44 | . 58 | . 21 | . 12 | . 16 | . 12 | . 05 | . 00 | 2.75 |
| 3.1-4.0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 6 | 9 | 9 | 3 | 2 | 1 | 0 | 0 | 0 | 34 |
| (1) | . 24 | . 47 | . 00 | . 00 | . 00 | . 00 | . 00 | . 24 | 1.42 | 2.12 | 2.12 | . 71 | . 47 | . 24 | . 00 | . 00 | . 00 | 8.02 |
| (2) | . 02 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 14 | . 21 | . 21 | . 07 | . 05 | . 02 | . 00 | . 00 | . 00 | . 78 |
| 4.1-5.0 | 0 | 0 | 2 | 6 | 2 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 2 | 0 | 0 | 15 |
| (1) | . 00 | . 00 | . 47 | 1.42 | . 47 | . 00 | . 00 | . 00 | . 00 | . 00 | . 47 | . 00 | . 24 | . 00 | . 47 | . 00 | . 00 | 3.54 |
| (2) | . 00 | . 00 | . 05 | . 14 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 02 | . 00 | . 05 | . 00 | . 00 | . 35 |
| 5.1-6.0 | 1 | 0 | 2 | 4 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 11 |
| (1) | . 24 | . 00 | . 47 | . 94 | . 47 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 47 | . 00 | 2.59 |
| (2) | . 02 | . 00 | . 05 | . 09 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 25 |
| 6.1-8.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 19 | 32 | 23 | 19 | 13 | 8 | 7 | 11 | 40 | 59 | 72 | 32 | 36 | 28 | 16 | 9 | 0 | 424 |
| (1) | 4.48 | 7.55 | 5.42 | 4.48 | 3.07 | 1.89 | 1.65 | 2.59 | 9.43 | 13.92 | 16.98 | 7.55 | 8.49 | 6.60 | 3.77 | 2.12 | . 00 | 100.00 |
| (2) | . 44 | . 74 | . 53 | . 44 | . 30 | . 18 | . 16 | . 25 | . 92 | 1.36 | 1.66 | . 74 | . 83 | . 65 | . 37 | . 21 | . 00 | 9.79 |
| (1) = PERCENT (2) =PERCENT | OF ALI | GOOD | OBSERV | ATIONS | FOR T | HIS PA ERIOD |  |  |  |  |  |  |  |  |  |  |  |  |

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CC MARCH MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)


CC MARCH MET DATA JOINT FREQUENCY DISTRIBUTION ( 60 -METER TOWER)
33.0 FT WIND DATA STABILITY CLASS ALL CLASS FREQUENCY (PERCENT) $=100.00$


## ग्0 $\stackrel{0}{2}$ $i$ <br> -^әу 60て-乙

CC APRIL MET DATA JOINT FREQUENCY DISTRIBUTION ( 60 -METER TOWER)
33.0 FT WIND DATA STABILITY CLASS A CLASS FREQUENCY (PERCENT) = 12.22

|  | WIND DIRECTION |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .2- . 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 1.1-1.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 20 | . 00 | . 00 | . 00 | . 00 | . 20 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 |
| 1.6-2.0 | 0 | 1 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 7 |
| (1) | . 00 | . 20 | . 20 | . 20 | . 00 | . 20 | . 00 | . 00 | . 00 | . 40 | . 00 | . 00 | . 00 | . 20 | . 00 | . 00 | . 00 | 1.41 |
| (2) | . 00 | . 02 | . 02 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 05 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 17 |
| 2.1-3.0 | 1 | 7 | 7 | 0 | 3 | 0 | 1 | 4 | 0 | 5 | 8 | 13 | 2 | 2 | 0 | 0 | 0 | 53 |
| (1) | . 20 | 1.41 | 1.41 | . 00 | . 60 | . 00 | . 20 | . 80 | . 00 | 1.01 | 1.61 | 2.62 | . 40 | . 40 | . 00 | . 00 | . 00 | 10.66 |
| (2) | . 02 | . 17 | . 17 | . 00 | . 07 | . 00 | . 02 | . 10 | . 00 | . 12 | . 20 | . 32 | . 05 | . 05 | . 00 | . 00 | . 00 | 1.30 |
| 3.1-4.0 | 14 | 27 | 15 | 6 | 3 | 6 | 3 | 12 | 2 | 9 | 24 | 24 | 7 | 4 | 5 | 3 | 0 | 164 |
| (1) | 2.82 | 5.43 | 3.02 | 1.21 | . 60 | 1.21 | . 60 | 2.41 | . 40 | 1.81 | 4.83 | 4.83 | 1.41 | . 80 | 1.01 | . 60 | . 00 | 33.00 |
| (2) | . 34 | . 66 | . 37 | . 15 | . 07 | . 15 | . 07 | . 29 | . 05 | . 22 | . 59 | . 59 | . 17 | . 10 | . 12 | . 07 | . 00 | 4.03 |
| 4.1-5.0 | 18 | 15 | 6 | 1 | 1 | 4 | 9 | 8 | 1 | 10 | 31 | 11 | 6 | 7 | 11 | 3 | 0 | 142 |
| (1) | 3.62 | 3.02 | 1.21 | . 20 | . 20 | . 80 | 1.81 | 1.61 | . 20 | 2.01 | 6.24 | 2.21 | 1.21 | 1.41 | 2.21 | . 60 | . 00 | 28.57 |
| (2) | . 44 | . 37 | . 15 | . 02 | . 02 | . 10 | . 22 | . 20 | . 02 | . 25 | . 76 | . 27 | . 15 | . 17 | . 27 | . 07 | . 00 | 3.49 |
| 5.1-6.0 | 10 | 4 | 1 | 1 | 0 | 0 | 4 | 9 | 0 | 2 | 8 | 4 | 3 | 11 | 11 | 2 | 0 | 70 |
| (1) | 2.01 | . 80 | . 20 | . 20 | . 00 | . 00 | . 80 | 1.81 | . 00 | . 40 | 1.61 | . 80 | . 60 | 2.21 | 2.21 | . 40 | . 00 | 14.08 |
| (2) | . 25 | . 10 | . 02 | . 02 | . 00 | . 00 | . 10 | . 22 | . 00 | . 05 | . 20 | . 10 | . 07 | . 27 | . 27 | . 05 | . 00 | 1.72 |
| 6.1-8.0 | 2 | 0 | 6 | 0 | 0 | 0 | 0 | 6 | 0 | 5 | 4 | 2 | 6 | 9 | 8 | 2 | 0 | 50 |
| (1) | . 40 | . 00 | 1.21 | . 00 | . 00 | . 00 | . 00 | 1.21 | . 00 | 1.01 | . 80 | . 40 | 1.21 | 1.81 | 1.61 | . 40 | . 00 | 10.06 |
| (2) | . 05 | . 00 | . 15 | . 00 | . 00 | . 00 | . 00 | . 15 | . 00 | . 12 | . 10 | . 05 | . 15 | . 22 | . 20 | . 05 | . 00 | 1.23 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 6 | 2 | 0 | 0 | 10 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 40 | . 00 | . 00 | . 00 | 1.21 | . 40 | . 00 | . 00 | 2.01 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 00 | . 00 | . 15 | . 05 | . 00 | . 00 | . 25 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 45 | 54 | 36 | 9 | 7 | 11 | 17 | 39 | 3 | 35 | 75 | 54 | 25 | 40 | 37 | 10 | 0 | 497 |
| (1) | 9.05 | 10.87 | 7.24 | 1.81 | 1.41 | 2.21 | 3.42 | 7.85 | . 60 | 7.04 | 15.09 | 10.87 | 5.03 | 8.05 | 7.44 | 2.01 | . 00 | 100.00 |
| (2) | 1.11 | 1.33 | . 88 | . 22 | . 17 | . 27 | . 42 | . 96 | . 07 | . 86 | 1.84 | 1.33 | . 61 | . 98 | . 91 | . 25 | . 00 | 12.22 |

(1) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAG
(2) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

Table 2.3-21—\{CCNPP 33 ft (10 m) April JFD (2000-2005)\} (Page 2 of 8)
CC APRIL MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)

(1) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

CC APRIL MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

Table 2.3-21—\{CCNPP 33 ft ( 10 m) April JFD (2000-2005)\} (Page 4 of 8)
CC APRIL MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)

| 33.0 FT | WIND D | DATA |  | STABI | LITY | LASS D |  | IND DI | $\begin{gathered} \text { CLASS } \\ \text { RECTIOI } \end{gathered}$ | FREQU <br> N FROM | ENCY | PERCEN | T) $=$ | 39.95 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 12 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 12 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 3 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 06 | . 00 | . 00 | . 06 | . 00 | . 06 | . 00 | . 00 | . 00 | . 00 | . 00 | . 18 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 |
| . $5-1.0$ | 4 | 2 | 0 | 3 | 3 | 7 | 5 | 2 | 2 | 3 | 6 | 0 | 1 | 0 | 2 | 1 | 0 | 41 |
| (1) | . 25 | . 12 | . 00 | . 18 | . 18 | . 43 | . 31 | . 12 | . 12 | . 18 | . 37 | . 00 | . 06 | . 00 | . 12 | . 06 | . 00 | 2.52 |
| (2) | . 10 | . 05 | . 00 | . 07 | . 07 | . 17 | . 12 | . 05 | . 05 | . 07 | . 15 | . 00 | . 02 | . 00 | . 05 | . 02 | . 00 | 1.01 |
| 1.1-1.5 | 6 | 3 | 11 | 9 | 9 | 7 | 8 | 7 | 4 | 1 | 4 | 3 | 2 | 5 | 1 | 4 | 0 | 84 |
| (1) | . 37 | . 18 | . 68 | . 55 | . 55 | . 43 | . 49 | . 43 | . 25 | . 06 | . 25 | . 18 | . 12 | . 31 | . 06 | . 25 | . 00 | 5.17 |
| (2) | . 15 | . 07 | . 27 | . 22 | . 22 | . 17 | . 20 | . 17 | . 10 | . 02 | . 10 | . 07 | . 05 | . 12 | . 02 | . 10 | . 00 | 2.06 |
| 1.6-2.0 | 9 | 16 | 9 | 21 | 24 | 11 | 3 | 10 | 7 | 5 | 6 | 5 | 5 | 7 | 3 | 8 | 0 | 149 |
| (1) | . 55 | . 98 | . 55 | 1.29 | 1.48 | . 68 | . 18 | . 62 | . 43 | . 31 | . 37 | . 31 | . 31 | . 43 | . 18 | . 49 | . 00 | 9.17 |
| (2) | . 22 | . 39 | . 22 | . 52 | . 59 | . 27 | . 07 | . 25 | . 17 | . 12 | . 15 | . 12 | . 12 | . 17 | . 07 | . 20 | . 00 | 3.66 |
| 2.1-3.0 | 38 | 67 | 41 | 47 | 37 | 26 | 29 | 31 | 20 | 15 | 16 | 13 | 14 | 13 | 19 | 18 | 0 | 444 |
| (1) | 2.34 | 4.12 | 2.52 | 2.89 | 2.28 | 1.60 | 1.78 | 1.91 | 1.23 | . 92 | . 98 | . 80 | . 86 | . 80 | 1.17 | 1.11 | . 00 | 27.32 |
| (2) | . 93 | 1.65 | 1.01 | 1.16 | . 91 | . 64 | . 71 | . 76 | . 49 | . 37 | . 39 | . 32 | . 34 | . 32 | . 47 | . 44 | . 00 | 10.91 |
| 3.1-4.0 | 43 | 24 | 49 | 23 | 12 | 14 | 18 | 42 | 28 | 13 | 23 | 18 | 7 | 13 | 27 | 33 | 0 | 387 |
| (1) | 2.65 | 1.48 | 3.02 | 1.42 | . 74 | . 86 | 1.11 | 2.58 | 1.72 | . 80 | 1.42 | 1.11 | . 43 | . 80 | 1.66 | 2.03 | . 00 | 23.82 |
| (2) | 1.06 | . 59 | 1.20 | . 57 | . 29 | . 34 | . 44 | 1.03 | . 69 | . 32 | . 57 | . 44 | . 17 | . 32 | . 66 | . 81 | . 00 | 9.51 |
| 4.1-5.0 | 26 | 28 | 37 | 32 | 3 | 1 | 8 | 23 | 3 | 6 | 17 | 7 | 3 | 6 | 25 | 29 | 0 | 254 |
| (1) | 1.60 | 1.72 | 2.28 | 1.97 | . 18 | . 06 | . 49 | 1.42 | . 18 | . 37 | 1.05 | . 43 | . 18 | . 37 | 1.54 | 1.78 | . 00 | 15.63 |
| (2) | . 64 | . 69 | . 91 | . 79 | . 07 | . 02 | . 20 | . 57 | . 07 | . 15 | . 42 | . 17 | . 07 | . 15 | . 61 | . 71 | . 00 | 6.24 |
| 5.1-6.0 | 12 | 16 | 13 | 15 | 0 | 0 | 5 | 15 | 2 | 5 | 7 | 2 | 0 | 10 | 9 | 9 | 0 | 120 |
| (1) | . 74 | . 98 | . 80 | . 92 | . 00 | . 00 | . 31 | . 92 | . 12 | . 31 | . 43 | . 12 | . 00 | . 62 | . 55 | . 55 | . 00 | 7.38 |
| (2) | . 29 | . 39 | . 32 | . 37 | . 00 | . 00 | . 12 | . 37 | . 05 | . 12 | . 17 | . 05 | . 00 | . 25 | . 22 | . 22 | . 00 | 2.95 |
| 6.1-8.0 | 13 | 10 | 27 | 15 | 0 | 0 | 0 | 19 | 4 | 6 | 0 | 1 | 2 | 14 | 14 | 3 | 0 | 128 |
| (1) | . 80 | . 62 | 1.66 | . 92 | . 00 | . 00 | . 00 | 1.17 | . 25 | . 37 | . 00 | . 06 | . 12 | . 86 | . 86 | . 18 | . 00 | 7.88 |
| (2) | . 32 | . 25 | . 66 | . 37 | . 00 | . 00 | . 00 | . 47 | . 10 | . 15 | . 00 | . 02 | . 05 | . 34 | . 34 | . 07 | . 00 | 3.15 |
| 8.1-10.0 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 13 |
| (1) | . 00 | . 00 | . 55 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 25 | . 00 | . 00 | . 00 | . 80 |
| (2) | . 00 | . 00 | . 22 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 10 | . 00 | . 00 | . 00 | . 32 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 151 | 166 | 196 | 165 | 88 | 66 | 77 | 149 | 70 | 55 | 81 | 50 | 34 | 72 | 100 | 105 | 0 | 1625 |
| (1) | 9.29 | 10.22 | 12.06 | 10.15 | 5.42 | 4.06 | 4.74 | 9.17 | 4.31 | 3.38 | 4.98 | 3.08 | 2.09 | 4.43 | 6.15 | 6.46 | . 00 | 100.00 |
| (2) | 3.71 | 4.08 | 4.82 | 4.06 | 2.16 | 1.62 | 1.89 | 3.66 | 1.72 | 1.35 | 1.99 | 1.23 | . 84 | 1.77 | 2.46 | 2.58 | . 00 | 39.95 |
| (1) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

OヨノכヨノOYd $\perp H$ Iy

CC APRIL MET DATA JOINT FREQUENCY DISTRIBUTION（ 60 －METER TOWER）


CC APRIL MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

CC APRIL MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)


Table 2.3-21—\{CCNPP 33 ft (10 m) April JFD (2000-2005)\}

## (Page 8 of 8)

CC APRIL MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
33.0 FT WIND DATA STABILITY CLASS ALL CLASS FREQUENCY (PERCENT) = 100.00


Table 2.3-22-\{CCNPP 33 ft ( 10 m ) May JFD (2000-2005) \} (Page 1 of 8)

CC MAY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
33.0 FT WIND DATA STABILITY CLASS A CLASS FREQUENCY (PERCENT) = 13.37

(1) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD


CC MAY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
OヨノכヨノOYd $\perp H$ Iy

Table 2．3－22—\｛CCNPP 33 ft（10 m）May JFD（2000－2005）\} （Page 3 of 8）
CC MAY MET DATA JOINT FREQUENCY DISTRIBUTION（60－METER TOWER）

| 33．0 FT WIND DATA |  |  | STABILITY CLASS C |  |  |  | CLASS FREQUENCY WIND DIRECTION FROM |  |  |  |  | （PERCENT） |  | 5.50 | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW |  |  |  |  |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT ． 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| ． $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| ．5－1．0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 41 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 41 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 |
| 1．1－1．5 | 1 | 0 | 1 | 2 | 0 | 3 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 10 |
| （1） | ． 41 | ． 00 | ． 41 | ． 82 | ． 00 | 1.22 | ． 00 | ． 00 | ． 41 | ． 41 | ． 00 | ． 00 | ． 00 | ． 00 | ． 41 | ． 00 | ． 00 | 4.08 |
| （2） | ． 02 | ． 00 | ． 02 | ． 04 | ． 00 | ． 07 | ． 00 | ． 00 | ． 02 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 22 |
| 1．6－2．0 | 1 | 0 | 1 | 1 | 4 | 1 | 2 | 3 | 1 | 2 | 1 | 1 | 2 | 0 | 1 | 0 | 0 | 21 |
| （1） | ． 41 | ． 00 | ． 41 | ． 41 | 1.63 | ． 41 | ． 82 | 1.22 | ． 41 | ． 82 | ． 41 | ． 41 | ． 82 | ． 00 | ． 41 | ． 00 | ． 00 | 8.57 |
| （2） | ． 02 | ． 00 | ． 02 | ． 02 | ． 09 | ． 02 | ． 04 | ． 07 | ． 02 | ． 04 | ． 02 | ． 02 | ． 04 | ． 00 | ． 02 | ． 00 | ． 00 | ． 47 |
| 2．1－3．0 | 8 | 12 | 5 | 8 | 7 | 7 | 2 | 10 | 2 | 7 | 4 | 6 | 4 | 3 | 1 | 1 | 0 | 87 |
| （1） | 3.27 | 4.90 | 2.04 | 3.27 | 2.86 | 2.86 | ． 82 | 4.08 | ． 82 | 2.86 | 1.63 | 2.45 | 1.63 | 1.22 | ． 41 | ． 41 | ． 00 | 35.51 |
| （2） | ． 18 | ． 27 | ． 11 | ． 18 | ． 16 | ． 16 | ． 04 | ． 22 | ． 04 | ． 16 | ． 09 | ． 13 | ． 09 | ． 07 | ． 02 | ． 02 | ． 00 | 1.95 |
| 3．1－4．0 | 7 | 7 | 10 | 3 | 1 | 1 | 2 | 13 | 3 | 0 | 8 | 9 | 3 | 1 | 5 | 1 | 0 | 74 |
| （1） | 2.86 | 2.86 | 4.08 | 1.22 | ． 41 | ． 41 | ． 82 | 5.31 | 1.22 | ． 00 | 3.27 | 3.67 | 1.22 | ． 41 | 2.04 | ． 41 | ． 00 | 30.20 |
| （2） | ． 16 | ． 16 | ． 22 | ． 07 | ． 02 | ． 02 | ． 04 | ． 29 | ． 07 | ． 00 | ． 18 | ． 20 | ． 07 | ． 02 | ． 11 | ． 02 | ． 00 | 1.66 |
| 4．1－5．0 | 6 | 0 | 2 | 1 | 2 | 1 | 2 | 8 | 1 | 0 | 3 | 0 | 2 | 1 | 2 | 2 | 0 | 33 |
| （1） | 2.45 | ． 00 | ． 82 | ． 41 | ． 82 | ． 41 | ． 82 | 3.27 | ． 41 | ． 00 | 1.22 | ． 00 | ． 82 | ． 41 | ． 82 | ． 82 | ． 00 | 13.47 |
| （2） | ． 13 | ． 00 | ． 04 | ． 02 | ． 04 | ． 02 | ． 04 | ． 18 | ． 02 | ． 00 | ． 07 | ． 00 | ． 04 | ． 02 | ． 04 | ． 04 | ． 00 | ． 74 |
| 5．1－6．0 | 0 | 0 | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 5 | 1 | 1 | 1 | 0 | 0 | 0 | 12 |
| （1） | ． 00 | ． 00 | ． 82 | ． 41 | ． 00 | ． 00 | ． 41 | ． 00 | ． 00 | ． 00 | 2.04 | ． 41 | ． 41 | ． 41 | ． 00 | ． 00 | ． 00 | 4.90 |
| （2） | ． 00 | ． 00 | ． 04 | ． 02 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 11 | ． 02 | ． 02 | ． 02 | ． 00 | ． 00 | ． 00 | ． 27 |
| 6．1－8．0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 5 |
| （1） | ． 00 | ． 00 | ． 41 | ． 41 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 41 | ． 82 | ． 00 | ． 00 | ． 00 | 2.04 |
| （2） | ． 00 | ． 00 | ． 02 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 04 | ． 00 | ． 00 | ． 00 | ． 11 |
| 8．1－10．0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| （1） | ． 00 | ． 00 | ． 82 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 82 |
| （2） | ． 00 | ． 00 | ． 04 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 04 |
| 10．1－89．5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| ALL SPEEDS | 23 | 19 | 24 | 17 | 14 | 13 | 10 | 34 | 8 | 10 | 21 | 17 | 13 | 8 | 10 | 4 | 0 | 245 |
| （1） | 9.39 | 7.76 | 9.80 | 6.94 | 5.71 | 5.31 | 4.08 | 13.88 | 3.27 | 4.08 | 8.57 | 6.94 | 5.31 | 3.27 | 4.08 | 1.63 | ． 00 | 100.00 |
| （2） | ． 52 | ． 43 | ． 54 | ． 38 | ． 31 | ． 29 | ． 22 | ． 76 | ． 18 | ． 22 | ． 47 | ． 38 | ． 29 | ． 18 | ． 22 | ． 09 | ． 00 | 5.50 |

（1）＝PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
（2）＝PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

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Table 2.3-22—\{CCNPP 33 ft (10 m) May JFD (2000-2005)\} (Page 4 of 8)
CC MAY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
33.0 FT WIND DATA STABILITY CLASS D CLASS FREQUENCY (PERCENT) $=35.50$

|  |  |  |  |  |  |  |  | WIND DI | RECTIO | N FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
|  | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| $\xrightarrow{.2-} \begin{array}{r}\text { (1) } \\ \text { (1) } \\ \text { (2) }\end{array}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 2 |
|  | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 06 | . 00 | . 06 | . 00 | . 13 |
|  | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 04 |
| . 5-1.0 | 1 | 3 | 3 | 5 | 8 | 6 | 7 | 4 | 8 | 4 | 4 | 1 | 2 | 1 | 2 | 5 | 0 | 64 |
| (1) | . 06 | . 19 | . 19 | . 32 | . 51 | . 38 | . 44 | . 25 | . 51 | . 25 | . 25 | . 06 | . 13 | . 06 | . 13 | . 32 | . 00 | 4.05 |
| 1.1- 1.5 | . 02 | . 07 | . 07 | . 11 | . 18 | . 13 | . 16 | . 09 | . 18 | . 09 | . 09 | . 02 | . 04 | . 02 | . 04 | . 11 | . 00 | 1.44 |
|  | 7 | 6 | 4 | 8 | 15 | 7 | 11 | 10 | 7 | 12 | 6 | 2 | 2 | 5 | 4 | 3 | 0 | 109 |
| (1) | . 44 | . 38 | . 25 | . 51 | . 95 | . 44 | . 70 | . 63 | . 44 | . 76 | . 38 | . 13 | . 13 | . 32 | . 25 | . 19 | . 00 | 6.90 |
| (2) | . 16 | . 13 | . 09 | . 18 | . 34 | . 16 | . 25 | . 22 | . 16 | . 27 | . 13 | . 04 | . 04 | . 11 | . 09 | . 07 | . 00 | 2.45 |
| 1.6-2.0 | 13 | 17 | 24 | 17 | 22 | 17 | 18 | 14 | 18 | 11 | 11 | 7 | 9 | 3 | 3 | 2 | 0 | 206 |
| (1) | . 82 | 1.08 | 1.52 | 1.08 | 1.39 | 1.08 | 1.14 | . 89 | 1.14 | . 70 | . 70 | . 44 | . 57 | . 19 | . 19 | . 13 | . 00 | 13.04 |
| (2) | . 29 | . 38 | . 54 | . 38 | . 49 | . 38 | . 40 | . 31 | . 40 | . 25 | . 25 | . 16 | . 20 | . 07 | . 07 | . 04 | . 00 | 4.63 |
| 2.1-3.0 | 33 | 49 | 54 | 69 | 56 | 33 | 35 | 57 | 39 | 14 | 23 | 25 | 13 | 13 | 14 | 25 | 0 | 552 |
| (1) | 2.09 | 3.10 | 3.42 | 4.37 | 3.54 | 2.09 | 2.22 | 3.61 | 2.47 | . 89 | 1.46 | 1.58 | . 82 | . 82 | . 89 | 1.58 | . 00 | 34.94 |
| (2) | . 74 | 1.10 | 1.21 | 1.55 | 1.26 | . 74 | . 79 | 1.28 | . 88 | . 31 | . 52 | . 56 | . 29 | . 29 | . 31 | . 56 | . 00 | 12.40 |
| 3.1-4.0 | 25 | 21 | 42 | 49 | 24 | 23 | 28 | 58 | 19 | 6 | 27 | 12 | 8 | 2 | 22 | 32 | 0 | 398 |
| (1) | 1.58 | 1.33 | 2.66 | 3.10 | 1.52 | 1.46 | 1.77 | 3.67 | 1.20 | . 38 | 1.71 | . 76 | . 51 | . 13 | 1.39 | 2.03 | . 00 | 25.19 |
| (2) | . 56 | . 47 | . 94 | 1.10 | . 54 | . 52 | . 63 | 1.30 | . 43 | . 13 | . 61 | . 27 | . 18 | . 04 | . 49 | . 72 | . 00 | 8.94 |
| 4.1- 5.0 | 18 | 8 | 14 | 17 | 8 | 3 | 9 | 21 | 3 | 3 | 15 | 2 | 6 | 1 | 1 | 12 | 0 | 141 |
|  | 1.14 | . 51 | . 89 | 1.08 | . 51 | . 19 | . 57 | 1.33 | . 19 | . 19 | . 95 | . 13 | . 38 | . 06 | . 06 | . 76 | . 00 | 8.92 |
| (2) | . 40 | . 18 | . 31 | . 38 | . 18 | . 07 | . 20 | . 47 | . 07 | . 07 | . 34 | . 04 | . 13 | . 02 | . 02 | . 27 | . 00 | 3.17 |
| 5.1-6.0 | 8 | 20 | 16 | 16 | 0 | 1 | 0 | 2 | 1 | 2 | 6 | 1 | 1 | 5 | 1 | 3 | 0 | 83 |
| (1) | . 51 | 1.27 | 1.01 | 1.01 | . 00 | . 06 | . 00 | . 13 | . 06 | . 13 | . 38 | . 06 | . 06 | . 32 | . 06 | . 19 | . 00 | 5.25 |
| (2) | . 18 | . 45 | . 36 | . 36 | . 00 | . 02 | . 00 | . 04 | . 02 | . 04 | . 13 | . 02 | . 02 | . 11 | . 02 | . 07 | . 00 | 1.86 |
| 6.1-8.0 | 1 | 2 |  | 4 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 21 |
| (1) | . 06 | . 13 | . 57 | . 25 | . 00 | . 06 | . 00 | . 06 | . 00 | . 00 | . 00 | . 00 | . 06 | . 06 | . 00 | . 06 | . 00 | 1.33 |
| (2) | . 02 | . 04 | . 20 | . 09 | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 02 | . 00 | . 47 |
| 8.1-10.0 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| (1) | . 00 | . 00 | . 19 | . 06 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 25 |
| (2) | . 00 | . 00 | . 07 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 09 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 106 | 126 | 169 | 186 | 133 | 91 | 108 | 167 | 95 | 52 | 92 | 50 | 42 | 32 | 47 | 84 | 0 | 1580 |
| (1) | 6.71 | 7.97 | 10.70 | 11.77 | 8.42 | 5.76 | 6.84 | 10.57 | 6.01 | 3.29 | 5.82 | 3.16 | 2.66 | 2.03 | 2.97 | 5.32 | . 00 | 100.00 |
| (2) | 2.38 | 2.83 | 3.80 | 4.18 | 2.99 | 2.04 | 2.43 | 3.75 | 2.13 | 1.17 | 2.07 | 1.12 | . 94 | . 72 | 1.06 | 1.89 | . 00 | 35.50 |
| (1) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Table 2.3-22—\{CCNPP 33 ft (10 m) May JFD (2000-2005)\} (Page 5 of 8)
CC MAY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)

(1) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

CC MAY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)


Table 2.3-22—\{CCNPP 33 ft (10 m) May JFD (2000-2005)\} (Page 7 of 8)
CC MAY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

Table 2.3-22—\{CCNPP 33 ft (10 m) May JFD (2000-2005)\} (Page 8 of 8)

CC MAY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
33.0 FT WIND DATA STABILITY CLASS ALL CLASS FREQUENCY (PERCENT) = 100.00

ग्0
$\stackrel{0}{2}$
$i$

Table 2.3-23—\{CCNPP 33 ft (10 m) June JFD (2000-2005)\}
(Page 1 of 8)
CC JUNE MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
33.0 FT WIND DATA STABILITY CLASS A CLASS FREQUENCY (PERCENT) = 13.90

|  |  |  |  |  |  |  |  | IND D | RECTI | FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 1.1-1.5 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 3 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 7 |
| (1) | . 00 | . 00 | . 00 | . 17 | . 00 | . 00 | . 17 | . 00 | . 00 | . 50 | . 00 | . 17 | . 00 | . 17 | . 00 | . 00 | . 00 | 1.17 |
| (2) | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 07 | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 16 |
| 1.6-2.0 | 0 | 3 | 1 | 2 | 1 | 4 | 0 | 3 | 2 | 5 | 12 | 4 | 2 | 0 | 0 | 1 | 0 | 40 |
| (1) | . 00 | . 50 | . 17 | . 33 | . 17 | . 67 | . 00 | . 50 | . 33 | . 83 | 2.00 | . 67 | . 33 | . 00 | . 00 | . 17 | . 00 | 6.67 |
| (2) | . 00 | . 07 | . 02 | . 05 | . 02 | . 09 | . 00 | . 07 | . 05 | . 12 | . 28 | . 09 | . 05 | . 00 | . 00 | . 02 | . 00 | . 93 |
| 2.1-3.0 | 9 | 25 | 15 | 16 | 20 | 11 | 9 | 11 | 11 | 22 | 30 | 23 | 9 | 5 | 4 | 0 | 0 | 220 |
| (1) | 1.50 | 4.17 | 2.50 | 2.67 | 3.33 | 1.83 | 1.50 | 1.83 | 1.83 | 3.67 | 5.00 | 3.83 | 1.50 | . 83 | . 67 | . 00 | . 00 | 36.67 |
| (2) | . 21 | . 58 | . 35 | . 37 | . 46 | . 25 | . 21 | . 25 | . 25 | . 51 | . 69 | . 53 | . 21 | . 12 | . 09 | . 00 | . 00 | 5.10 |
| 3.1-4.0 | 29 | 17 | 5 | 2 | 0 | 3 | 19 | 24 | 8 | 18 | 47 | 31 | 13 | 2 | 6 | 4 | 0 | 228 |
| (1) | 4.83 | 2.83 | . 83 | . 33 | . 00 | . 50 | 3.17 | 4.00 | 1.33 | 3.00 | 7.83 | 5.17 | 2.17 | . 33 | 1.00 | . 67 | . 00 | 38.00 |
| (2) | . 67 | . 39 | . 12 | . 05 | . 00 | . 07 | . 44 | . 56 | . 19 | . 42 | 1.09 | . 72 | . 30 | . 05 | . 14 | . 09 | . 00 | 5.28 |
| 4.1-5.0 | 8 | 2 | 0 | 0 | 0 | 0 | 7 | 17 | 6 | 7 | 12 | 7 | 3 | 3 | 4 | 3 | 0 | 79 |
| (1) | 1.33 | . 33 | . 00 | . 00 | . 00 | . 00 | 1.17 | 2.83 | 1.00 | 1.17 | 2.00 | 1.17 | . 50 | . 50 | . 67 | . 50 | . 00 | 13.17 |
| (2) | . 19 | . 05 | . 00 | . 00 | . 00 | . 00 | . 16 | . 39 | . 14 | . 16 | . 28 | . 16 | . 07 | . 07 | . 09 | . 07 | . 00 | 1.83 |
| 5.1-6.0 | 0 | 0 | 3 | 0 | 0 | 0 | 2 | 8 | 0 | 0 | 3 | 0 | 2 | 0 | 1 | 1 | 0 | 20 |
| (1) | . 00 | . 00 | . 50 | . 00 | . 00 | . 00 | . 33 | 1.33 | . 00 | . 00 | . 50 | . 00 | . 33 | . 00 | . 17 | . 17 | . 00 | 3.33 |
| (2) | . 00 | . 00 | . 07 | . 00 | . 00 | . 00 | . 05 | . 19 | . 00 | . 00 | . 07 | . 00 | . 05 | . 00 | . 02 | . 02 | . 00 | . 46 |
| 6.1-8.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 6 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 67 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 33 | . 00 | . 00 | 1.00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 09 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 00 | . 14 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 46 | 47 | 24 | 21 | 21 | 18 | 38 | 67 | 27 | 55 | 104 | 66 | 29 | 11 | 17 | 9 | 0 | 600 |
| (1) | 7.67 | 7.83 | 4.00 | 3.50 | 3.50 | 3.00 | 6.33 | 11.17 | 4.50 | 9.17 | 17.33 | 11.00 | 4.83 | 1.83 | 2.83 | 1.50 | . 00 | 100.00 |
| (2) | 1.07 | 1.09 | . 56 | . 49 | . 49 | . 42 | . 88 | 1.55 | . 63 | 1.27 | 2.41 | 1.53 | . 67 | . 25 | . 39 | . 21 | . 00 | 13.90 |

(1) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD


CC JUNE MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD


CC JUNE MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

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Table 2.3-23—\{CCNPP 33 ft (10 m) June JFD (2000-2005)\}
(Page 4 of 8)
CC JUNE MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
33.0 FT WIND DATA STABILITY CLASS D CLASS FREQUENCY (PERCENT) $=30.58$

| WIND DIRECTION FROM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 08 | . 00 | . 00 | . 00 | . 08 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 02 |
| .5-1.0 | 3 | 4 | 5 | 2 | 2 | 1 | 5 | 3 | 2 | 3 | 10 | 9 | 5 | 3 | 2 | 5 | 0 | 64 |
| (1) | . 23 | . 30 | . 38 | . 15 | . 15 | . 08 | . 38 | . 23 | . 15 | . 23 | . 76 | . 68 | . 38 | . 23 | . 15 | . 38 | . 00 | 4.85 |
| (2) | . 07 | . 09 | . 12 | . 05 | . 05 | . 02 | . 12 | . 07 | . 05 | . 07 | . 23 | . 21 | . 12 | . 07 | . 05 | . 12 | . 00 | 1.48 |
| 1.1-1.5 | 8 | 9 | 6 | 10 | 11 | 8 | 7 | 6 | 5 | 11 | 12 | 7 | 8 | 6 | 3 | 4 | 0 | 121 |
| (1) | . 61 | . 68 | . 45 | . 76 | . 83 | . 61 | . 53 | . 45 | . 38 | . 83 | . 91 | . 53 | . 61 | . 45 | . 23 | . 30 | . 00 | 9.17 |
| (2) | . 19 | . 21 | . 14 | . 23 | . 25 | . 19 | . 16 | . 14 | . 12 | . 25 | . 28 | . 16 | . 19 | . 14 | . 07 | . 09 | . 00 | 2.80 |
| 1.6-2.0 | 11 | 20 | 15 | 18 | 20 | 15 | 7 | 11 | 9 | 18 | 18 | 13 | 7 | 13 | 7 | 7 | 0 | 209 |
| (1) | . 83 | 1.52 | 1.14 | 1.36 | 1.52 | 1.14 | . 53 | . 83 | . 68 | 1.36 | 1.36 | . 98 | . 53 | . 98 | . 53 | . 53 | . 00 | 15.83 |
| (2) | . 25 | . 46 | . 35 | . 42 | . 46 | . 35 | . 16 | . 25 | . 21 | . 42 | . 42 | . 30 | . 16 | . 30 | . 16 | . 16 | . 00 | 4.84 |
| 2.1-3.0 | 40 | 41 | 34 | 37 | 40 | 20 | 9 | 47 | 24 | 30 | 48 | 25 | 27 | 19 | 24 | 19 | 0 | 484 |
| (1) | 3.03 | 3.11 | 2.58 | 2.80 | 3.03 | 1.52 | . 68 | 3.56 | 1.82 | 2.27 | 3.64 | 1.89 | 2.05 | 1.44 | 1.82 | 1.44 | . 00 | 36.67 |
| (2) | . 93 | . 95 | . 79 | . 86 | . 93 | . 46 | . 21 | 1.09 | . 56 | . 69 | 1.11 | . 58 | . 63 | . 44 | . 56 | . 44 | . 00 | 11.21 |
| 3.1-4.0 | 24 | 20 | 25 | 50 | 30 | 5 | 1 | 34 | 3 | 8 | 23 | 10 | 7 | 4 | 19 | 11 | 0 | 274 |
| (1) | 1.82 | 1.52 | 1.89 | 3.79 | 2.27 | . 38 | . 08 | 2.58 | . 23 | . 61 | 1.74 | . 76 | . 53 | . 30 | 1.44 | . 83 | . 00 | 20.76 |
| (2) | . 56 | . 46 | . 58 | 1.16 | . 69 | . 12 | . 02 | . 79 | . 07 | . 19 | . 53 | . 23 | . 16 | . 09 | . 44 | . 25 | . 00 | 6.35 |
| 4.1-5.0 | 18 | 4 | 16 | 20 | 4 | 2 | 1 | 16 | 2 | 1 | 8 | 4 | 0 | 2 | 11 | 12 | 0 | 121 |
| (1) | 1.36 | . 30 | 1.21 | 1.52 | . 30 | . 15 | . 08 | 1.21 | . 15 | . 08 | . 61 | . 30 | . 00 | . 15 | . 83 | . 91 | . 00 | 9.17 |
| (2) | . 42 | . 09 | . 37 | . 46 | . 09 | . 05 | . 02 | . 37 | . 05 | . 02 | . 19 | . 09 | . 00 | . 05 | . 25 | . 28 | . 00 | 2.80 |
| 5.1-6.0 | 7 | 4 | 4 | 5 | 1 | 1 | 0 | 7 | 0 | 0 | 1 | 0 | 0 | 2 | 3 | 4 | 0 | 39 |
| (1) | . 53 | . 30 | . 30 | . 38 | . 08 | . 08 | . 00 | . 53 | . 00 | . 00 | . 08 | . 00 | . 00 | . 15 | . 23 | . 30 | . 00 | 2.95 |
| (2) | . 16 | . 09 | . 09 | . 12 | . 02 | . 02 | . 00 | . 16 | . 00 | . 00 | . 02 | . 00 | . 00 | . 05 | . 07 | . 09 | . 00 | . 90 |
| 6.1-8.0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 3 | 0 | 0 | 7 |
| (1) | . 08 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 23 | . 23 | . 00 | . 00 | . 53 |
| (2) | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 | . 07 | . 00 | . 00 | . 16 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 112 | 102 | 105 | 142 | 108 | 52 | 30 | 124 | 45 | 71 | 120 | 68 | 54 | 53 | 72 | 62 | 0 | 1320 |
| (1) | 8.48 | 7.73 | 7.95 | 10.76 | 8.18 | 3.94 | 2.27 | 9.39 | 3.41 | 5.38 | 9.09 | 5.15 | 4.09 | 4.02 | 5.45 | 4.70 | . 00 | 100.00 |
| (2) | 2.59 | 2.36 | 2.43 | 3.29 | 2.50 | 1.20 | . 69 | 2.87 | 1.04 | 1.64 | 2.78 | 1.58 | 1.25 | 1.23 | 1.67 | 1.44 | . 00 | 30.58 |
| (1) = PERCENT | OF ALI | GOOD | OBSERV | ATIONS | FOR | HIS PA |  |  |  |  |  |  |  |  |  |  |  |  |
| (2) =PERCENT | ALL G | OD OBS | ERVATI | ONS FOR | THIS | ERIOD |  |  |  |  |  |  |  |  |  |  |  |  |

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CC JUNE MET DATA JOINT FREQUENCY DISTRIBUTION（60－METER TOWER）


CC JUNE MET DATA JOINT FREQUENCY DISTRIBUTION（60－METER TOWER）
33．0 FT WIND DATA STABILITY CLASS F CLASS FREQUENCY（PERCENT）＝ 12.74


## CC JUNE MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)


(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD


Table 2.3-23—\{CCNPP 33 ft ( 10 m) June JFD (2000-2005) \} (Page 8 of 8)

CC JUNE MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)

| 33.0 FT WIND DATA |  |  |  | STABILITY CLASS ALL |  |  |  |  | CLASS |  |  | PERCENT) $=100.00$ |  |  | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW |  |  |  |  |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 3 | 4 | 5 | 3 | 1 | 0 | 0 | 0 | 0 | 18 |
|  | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 07 | . 09 | . 12 | . 07 | . 02 | . 00 | . 00 | . 00 | . 00 | . 42 |
|  | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 07 | . 09 | . 12 | . 07 | . 02 | . 00 | . 00 | . 00 | . 00 | . 42 |
| . $2-$ | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 4 | 1 | 4 | 3 | 7 | 3 | 1 | 0 | 0 | 0 | 25 |
|  | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 09 | . 02 | . 09 | . 07 | . 16 | . 07 | . 02 | . 00 | . 00 | . 00 | . 58 |
|  | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 09 | . 02 | . 09 | . 07 | . 16 | . 07 | . 02 | . 00 | . 00 | . 00 | . 58 |
| . $5-1.0$ | 9 | 7 | 8 | 3 | 5 | 6 | 12 | 14 | 19 | 44 | 50 | 44 | 27 | 19 | 8 | 14 | 0 | 289 |
| (1) | . 21 | . 16 | . 19 | . 07 | . 12 | . 14 | . 28 | . 32 | . 44 | 1.02 | 1.16 | 1.02 | . 63 | . 44 | . 19 | . 32 | . 00 | 6.69 |
|  | . 21 | . 16 | . 19 | . 07 | . 12 | . 14 | . 28 | . 32 | . 44 | 1.02 | 1.16 | 1.02 | . 63 | . 44 | . 19 | . 32 | . 00 | 6.69 |
|  | 15 | 14 | 9 | 15 | 15 | 13 | 15 | 22 | 60 | 141 | 150 | 76 | 45 | 38 | 7 | 10 | 0 | 645 |
| $\begin{array}{r} 1.1-1.5 \\ (1) \end{array}$ | . 35 | . 32 | . 21 | . 35 | . 35 | . 30 | . 35 | . 51 | 1.39 | 3.27 | 3.47 | 1.76 | 1.04 | . 88 | . 16 | . 23 | . 00 | 14.94 |
| (2) | . 35 | . 32 | . 21 | . 35 | . 35 | . 30 | . 35 | . 51 | 1.39 | 3.27 | 3.47 | 1.76 | 1.04 | . 88 | . 16 | . 23 | . 00 | 14.94 |
| $1.6-2.0$ | 21 | 29 | 24 | 29 | 30 | 29 | 17 | 36 | 63 | 117 | 175 | 105 | 50 | 36 | 30 | 16 | 0 | 807 |
| $\begin{array}{r} 1.6-2.0 \\ (1) \end{array}$ | . 49 | . 67 | . 56 | . 67 | . 69 | . 67 | . 39 | . 83 | 1.46 | 2.71 | 4.05 | 2.43 | 1.16 | . 83 | . 69 | . 37 | . 00 | 18.69 |
| $\begin{array}{r} (2) \\ 2.1-3.0 \end{array}$ | . 49 | . 67 | . 56 | . 67 | . 69 | . 67 | . 39 | . 83 | 1.46 | 2.71 | 4.05 | 2.43 | 1.16 | . 83 | . 69 | . 37 | . 00 | 18.69 |
|  | 90 | 100 | 81 | 72 | 76 | 43 | 35 | 93 | 88 | 119 | 239 | 124 | 73 | 70 | 69 | 44 | 0 | 1416 |
| $\begin{array}{r} 2.1-3.0 \\ (1) \end{array}$ | 2.08 | 2.32 | 1.88 | 1.67 | 1.76 | 1.00 | . 81 | 2.15 | 2.04 | 2.76 | 5.54 | 2.87 | 1.69 | 1.62 | 1.60 | 1.02 | . 00 | 32.80 |
| $3.1-4.0$ | 2.08 | 2.32 | 1.88 | 1.67 | 1.76 | 1.00 | . 81 | 2.15 | 2.04 | 2.76 | 5.54 | 2.87 | 1.69 | 1.62 | 1.60 | 1.02 | . 00 | 32.80 |
|  | 68 | 41 | 37 | 55 | 36 | 11 | 28 | 97 | 18 | 55 | 148 | 56 | 32 | 20 | 36 | 27 | 0 | 765 |
| $\begin{array}{r} 3.1-4.0 \\ (1) \end{array}$ | 1.58 | . 95 | . 86 | 1.27 | . 83 | . 25 | . 65 | 2.25 | . 42 | 1.27 | 3.43 | 1.30 | . 74 | . 46 | . 83 | . 63 | . 00 | 17.72 |
| $\begin{array}{r} (2) \\ 4.1-5.0 \end{array}$ | 1.58 | . 95 | . 86 | 1.27 | . 83 | . 25 | . 65 | 2.25 | . 42 | 1.27 | 3.43 | 1.30 | . 74 | . 46 | . 83 | . 63 | . 00 | 17.72 |
|  | 31 | 6 | 19 | 22 | 5 | 5 | 8 | 41 | 10 | 14 | 36 | 16 | 5 | 6 | 20 | 19 | 0 | 263 |
| $\begin{array}{r} 4.1-5.0 \\ (1) \end{array}$ | . 72 | . 14 | . 44 | . 51 | . 12 | . 12 | . 19 | . 95 | . 23 | . 32 | . 83 | . 37 | . 12 | . 14 | . 46 | . 44 | . 00 | 6.09 |
| (2) | . 72 | . 14 | . 44 | . 51 | . 12 | . 12 | . 19 | . 95 | . 23 | . 32 | . 83 | . 37 | . 12 | . 14 | . 46 | . 44 | . 00 | 6.09 |
| 5.1-6.0 | 9 | 5 | 7 | 5 | 1 | 1 | 2 | 18 | 0 | 0 | 4 | 0 | 4 | 4 | 4 | 7 | 0 | 71 |
| (1) | . 21 | . 12 | . 16 | . 12 | . 02 | . 02 | . 05 | . 42 | . 00 | . 00 | . 09 | . 00 | . 09 | . 09 | . 09 | . 16 | . 00 | 1.64 |
|  | . 21 | . 12 | . 16 | . 12 | . 02 | . 02 | . 05 | . 42 | . 00 | . 00 | . 09 | . 00 | . 09 | . 09 | . 09 | . 16 | . 00 | 1.64 |
|  | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 1 | 3 | 7 | 0 | 0 | 18 |
| $\begin{array}{r} 6.1-8.0 \\ (1) \end{array}$ | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 12 | . 00 | . 00 | . 00 | . 00 | . 02 | . 07 | . 16 | . 00 | . 00 | . 42 |
| 8.1-10.0 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 12 | . 00 | . 00 | . 00 | . 00 | . 02 | . 07 | . 16 | . 00 | . 00 | . 42 |
|  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) <br> (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
|  | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
|  | 244 | 202 | 187 | 201 | 168 | 110 | 118 | 330 | 262 | 498 | 810 | 431 | 241 | 197 | 181 | 137 | 0 | 4317 |
| ALL SPEEDS <br> (1) | 5.65 | 4.68 | 4.33 | 4.66 | 3.89 | 2.55 | 2.73 | 7.64 | 6.07 | 11.54 | 18.76 | 9.98 | 5.58 | 4.56 | 4.19 | 3.17 | . 00 | 100.00 |
| (2) | 5.65 | 4.68 | 4.33 | 4.66 | 3.89 | 2.55 | 2.73 | 7.64 | 6.07 | 11.54 | 18.76 | 9.98 | 5.58 | 4.56 | 4.19 | 3.17 | . 00 | 100.00 |
| (1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE (2) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

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CC JULY MET DATA JOINT FREQUENCY DISTRIBUTION（ 60 －METER TOWER）
33．0 FT WIND DATA STABILITY CLASS A CLASS FREQUENCY（PERCENT）＝ 12.47

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { SPEED } \\ & \text { mps } \end{aligned}$ | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| LT ． 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| ． $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| ．5－1．0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| 1．1－1．5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 4 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 56 | ． 00 | ． 19 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 74 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 07 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 09 |
| 1．6－2．0 | 0 | 2 | 2 | 1 | 0 | 1 | 1 | 0 | 1 | 1 | 6 | 2 | 1 | 0 | 0 | 0 | 0 | 18 |
| （1） | ． 00 | ． 37 | ． 37 | ． 19 | ． 00 | ． 19 | ． 19 | ． 00 | ． 19 | ． 19 | 1.11 | ． 37 | ． 19 | ． 00 | ． 00 | ． 00 | ． 00 | 3.33 |
| （2） | ． 00 | ． 05 | ． 05 | ． 02 | ． 00 | ． 02 | ． 02 | ． 00 | ． 02 | ． 02 | ． 14 | ． 05 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 42 |
| 2．1－3．0 | 21 | 20 | 16 | 7 | 10 | 12 | 19 | 10 | 11 | 26 | 44 | 20 | 3 | 0 | 4 | 4 | 0 | 227 |
| （1） | 3.89 | 3.70 | 2.96 | 1.30 | 1.85 | 2.22 | 3.52 | 1.85 | 2.04 | 4.81 | 8.15 | 3.70 | ． 56 | ． 00 | ． 74 | ． 74 | ． 00 | 42.04 |
| （2） | ． 48 | ． 46 | ． 37 | ． 16 | ． 23 | ． 28 | ． 44 | ． 23 | ． 25 | ． 60 | 1.02 | ． 46 | ． 07 | ． 00 | ． 09 | ． 09 | ． 00 | 5.24 |
| 3．1－4．0 | 31 | 30 | 11 | 1 | 0 | 3 | 16 | 27 | 9 | 14 | 18 | 19 | 11 | 3 | 1 | 3 | 0 | 197 |
| （1） | 5.74 | 5.56 | 2.04 | ． 19 | ． 00 | ． 56 | 2.96 | 5.00 | 1.67 | 2.59 | 3.33 | 3.52 | 2.04 | ． 56 | ． 19 | ． 56 | ． 00 | 36.48 |
| （2） | ． 72 | ． 69 | ． 25 | ． 02 | ． 00 | ． 07 | ． 37 | ． 62 | ． 21 | ． 32 | ． 42 | ． 44 | ． 25 | ． 07 | ． 02 | ． 07 | ． 00 | 4.55 |
| 4．1－5．0 | 13 | 4 | 12 | 2 | 0 | 2 | 8 | 13 | 1 | 3 | 6 | 2 | 2 | 3 | 9 | 2 | 0 | 82 |
| （1） | 2.41 | ． 74 | 2.22 | ． 37 | ． 00 | ． 37 | 1.48 | 2.41 | ． 19 | ． 56 | 1.11 | ． 37 | ． 37 | ． 56 | 1.67 | ． 37 | ． 00 | 15.19 |
| (2) | ． 30 | ． 09 | ． 28 | ． 05 | ． 00 | ． 05 | ． 18 | ． 30 | ． 02 | ． 07 | ． 14 | ． 05 | ． 05 | ． 07 | ． 21 | ． 05 | ． 00 | 1.89 |
| 5．1－6．0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 1 | 0 | 0 | 0 | 2 | 1 | 0 | 10 |
| （1） | ． 00 | ． 19 | ． 37 | ． 00 | ． 00 | ． 00 | ． 00 | ． 37 | ． 19 | ． 00 | ． 19 | ． 00 | ． 00 | ． 00 | ． 37 | ． 19 | ． 00 | 1.85 |
| （2） | ． 00 | ． 02 | ． 05 | ． 00 | ． 00 | ． 00 | ． 00 | ． 05 | ． 02 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 05 | ． 02 | ． 00 | ． 23 |
| 6．1－8．0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| （1） | ． 00 | ． 00 | ． 19 | ． 19 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 37 |
| （2） | ． 00 | ． 00 | ． 02 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 05 |
| 8．1－10．0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| 10．1－89．5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | ， |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| ALL SPEEDS | 65 | 57 | 44 | 12 | 10 | 18 | 44 | 52 | 23 | 47 | 75 | 44 | 17 | 6 | 16 | 10 | 0 | 540 |
| （1） | 12.04 | 10.56 | 8.15 | 2.22 | 1.85 | 3.33 | 8.15 | 9.63 | 4.26 | 8.70 | 13.89 | 8.15 | 3.15 | 1.11 | 2.96 | 1.85 | ． 00 | 100.00 |
| （2） | 1.50 | 1.32 | 1.02 | ． 28 | ． 23 | ． 42 | 1.02 | 1.20 | ． 53 | 1.09 | 1.73 | 1.02 | ． 39 | ． 14 | ． 37 | ． 23 | ． 00 | 12.47 |

（1）＝PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
（2）＝PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

CC JULY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

## CC JULY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)


(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

## 

Table 2.3-24—\{CCNPP 33 ft ( 10 m ) July JFD (2000-2005) \} (Page 4 of 8 )
CC JULY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
33.0 FT WIND DATA STABILITY CLASS D CLASS FREQUENCY (PERCENT) = 30.65


Table 2.3-24—\{CCNPP 33 ft ( 10 m) July JFD (2000-2005)\} (Page 5 of 8)
CC JULY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
33.0 FT WIND DATA STABILITY CLASS E CLASS FREQUENCY (PERCENT) = 23.30

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

## CC JULY MET DATA JOINT FREQUENCY DISTRIBUTION（60－METER TOWER

33．0 FT WIND DATA STABILITY CLASS F CLASS FREQUENCY（PERCENT）＝ 11.20



CC JULY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)


## 

Table 2.3-24—_\{CNPP 33 ft (10 m) July JFD (2000-2005)\} (Page 8 of 8)
CC JULY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)

| 33.0 FT WIND DATA |  |  |  | STABILITY CLASS ALL |  |  |  |  | CLASS FREQUENCY ( |  |  | $($ PERCENT $)=100.00$ |  |  | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW |  |  |  |  |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 1 | 4 | 4 | 0 | 0 | 0 | 1 | 0 | 14 |
|  | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 05 | . 02 | . 09 | . 09 | . 00 | . 00 | . 00 | . 02 | . 00 | . 32 |
|  | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 05 | . 02 | . 09 | . 09 | . 00 | . 00 | . 00 | . 02 | . 00 | . 32 |
| . $2-$ | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 3 | 2 | 3 | 2 | 5 | 7 | 2 | 2 | 1 | 0 | 30 |
|  | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 02 | . 07 | . 05 | . 07 | . 05 | . 12 | . 16 | . 05 | . 05 | . 02 | . 00 | . 69 |
|  | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 02 | . 07 | . 05 | . 07 | . 05 | . 12 | . 16 | . 05 | . 05 | . 02 | . 00 | . 69 |
| . $5-1.0$ | 10 | 5 | 6 | 3 | 7 | 8 | 8 | 22 | 40 | 64 | 64 | 47 | 36 | 21 | 13 | 9 | 0 | 363 |
| (1) | . 23 | . 12 | . 14 | . 07 | . 16 | . 18 | . 18 | . 51 | . 92 | 1.48 | 1.48 | 1.09 | . 83 | . 48 | . 30 | . 21 | . 00 | 8.38 |
|  | . 23 | . 12 | . 14 | . 07 | . 16 | . 18 | . 18 | . 51 | . 92 | 1.48 | 1.48 | 1.09 | . 83 | . 48 | . 30 | . 21 | . 00 | 8.38 |
|  | 16 | 12 | 11 | 12 | 21 | 17 | 17 | 33 | 69 | 141 | 171 | 107 | 65 | 33 | 23 | 7 | 0 | 755 |
| $\begin{array}{r} 1.1-1.5 \\ (1) \end{array}$ | . 37 | . 28 | . 25 | . 28 | . 48 | . 39 | . 39 | . 76 | 1.59 | 3.26 | 3.95 | 2.47 | 1.50 | . 76 | . 53 | . 16 | . 00 | 17.44 |
| (2) | . 37 | . 28 | . 25 | . 28 | . 48 | . 39 | . 39 | . 76 | 1.59 | 3.26 | 3.95 | 2.47 | 1.50 | . 76 | . 53 | . 16 | . 00 | 17.44 |
| $1.6-2.0$ | 25 | 47 | 31 | 29 | 45 | 35 | 28 | 38 | 49 | 92 | 174 | 98 | 51 | 45 | 34 | 19 | 0 | 840 |
| $\begin{array}{r} 1.6-2.0 \\ (1) \end{array}$ | . 58 | 1.09 | . 72 | . 67 | 1.04 | . 81 | . 65 | . 88 | 1.13 | 2.12 | 4.02 | 2.26 | 1.18 | 1.04 | . 79 | . 44 | . 00 | 19.40 |
| $\begin{array}{r} (2) \\ 2.1-3.0 \end{array}$ | . 58 | 1.09 | . 72 | . 67 | 1.04 | . 81 | . 65 | . 88 | 1.13 | 2.12 | 4.02 | 2.26 | 1.18 | 1.04 | . 79 | . 44 | . 00 | 19.40 |
|  | 105 | 114 | 77 | 77 | 66 | 47 | 67 | 80 | 72 | 92 | 226 | 154 | 46 | 24 | 39 | 35 | 0 | 1321 |
| $\begin{array}{r} 2.1-3.0 \\ (1) \end{array}$ | 2.42 | 2.63 | 1.78 | 1.78 | 1.52 | 1.09 | 1.55 | 1.85 | 1.66 | 2.12 | 5.22 | 3.56 | 1.06 | . 55 | . 90 | . 81 | . 00 | 30.51 |
| $3.1-4.0$ | 2.42 | 2.63 | 1.78 | 1.78 | 1.52 | 1.09 | 1.55 | 1.85 | 1.66 | 2.12 | 5.22 | 3.56 | 1.06 | . 55 | . 90 | . 81 | . 00 | 30.51 |
|  | 89 | 61 | 54 | 54 | 26 | 15 | 30 | 76 | 33 | 39 | 88 | 45 | 22 | 8 | 10 | 14 | 0 | 664 |
| $\begin{array}{r} 3.1-4.0 \\ (1) \end{array}$ | 2.06 | 1.41 | 1.25 | 1.25 | . 60 | . 35 | . 69 | 1.76 | . 76 | . 90 | 2.03 | 1.04 | . 51 | . 18 | . 23 | . 32 | . 00 | 15.33 |
| $\begin{array}{r} (2) \\ 4.1-5.0 \end{array}$ | 2.06 | 1.41 | 1.25 | 1.25 | . 60 | . 35 | . 69 | 1.76 | . 76 | . 90 | 2.03 | 1.04 | . 51 | . 18 | . 23 | . 32 | . 00 | 15.33 |
|  | 19 | 12 | 55 | 39 | 14 | 5 | 8 | 25 | 6 | 5 | 22 | 7 | 2 | 6 | 13 | 7 | 0 | 245 |
| (1) | . 44 | . 28 | 1.27 | . 90 | . 32 | . 12 | . 18 | . 58 | . 14 | . 12 | . 51 | . 16 | . 05 | . 14 | . 30 | . 16 | . 00 | 5.66 |
| $\begin{array}{r} \text { (2) } \\ 5.1-6.0 \end{array}$ | . 44 | . 28 | 1.27 | . 90 | . 32 | . 12 | . 18 | . 58 | . 14 | . 12 | . 51 | . 16 | . 05 | . 14 | . 30 | . 16 | . 00 | 5.66 |
|  | 5 | 8 | 24 | 16 | 1 | 0 | 1 | 3 | 2 | 0 | 9 | 0 | 0 | 0 | 4 | 2 | 0 | 75 |
| $5.1-6.0$ <br> (1) | . 12 | . 18 | . 55 | . 37 | . 02 | . 00 | . 02 | . 07 | . 05 | . 00 | . 21 | . 00 | . 00 | . 00 | . 09 | . 05 | . 00 | 1.73 |
| (2) | . 12 | . 18 | . 55 | . 37 | . 02 | . 00 | . 02 | . 07 | . 05 | . 00 | . 21 | . 00 | . 00 | . 00 | . 09 | . 05 | . 00 | 1.73 |
| 6.1-8.0 | 2 | 3 | 10 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 23 |
| (1) | . 05 | . 07 | . 23 | . 12 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 53 |
| $\begin{array}{r} (2) \\ 8.1-10.0 \end{array}$ | . 05 | . 07 | . 23 | . 12 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 53 |
|  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) <br> (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
|  | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 271 | 262 | 269 | 235 | 182 | 127 | 160 | 282 | 275 | 437 | 760 | 467 | 229 | 140 | 139 | 95 | 0 | 4330 |
| (1) | 6.26 | 6.05 | 6.21 | 5.43 | 4.20 | 2.93 | 3.70 | 6.51 | 6.35 | 10.09 | 17.55 | 10.79 | 5.29 | 3.23 | 3.21 | 2.19 | . 00 | 100.00 |
| (2) | 6.26 | 6.05 | 6.21 | 5.43 | 4.20 | 2.93 | 3.70 | 6.51 | 6.35 | 10.09 | 17.55 | 10.79 | 5.29 | 3.23 | 3.21 | 2.19 | . 00 | 100.00 |
| (1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE <br> (2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

CC AUGUST MET DATA JOINT FREQUENCY DISTRIBUTION ( $60-$ METER TOWER)


[^0](2) =PERCENT OF ALL GOod ObSERVAtions for this period

| CC AUGUST MET DATA JOINT FREQUENCY DISTRIBUTION | $(60$-METER TOWER) |  |  |
| :--- | :---: | :---: | :---: |
| 33.0 FT WIND DATA | STABILITY CLASS B | CLASS FREQUENCY | (PERCENT) $=\quad 5.84$ |

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| CC AUGUST MET DATA JOINT FREQUENCY DISTRIBUTION | $(60-M E T E R ~ T O W E R) ~$ |  |  |
| :--- | :---: | :---: | :---: |
| 33.0 FT WIND DATA | STABILITY CLASS C | CLASS FREQUENCY | (PERCENT) $=6.13$ |



Table 2.3-25—\{CCNPP 33 ft (10 m) August JFD (2000-2005)\} (Page 4 of 8)
CC AUGUST MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
33.0 FT WIND DATA STABILITY CLASS D CLASS FREQUENCY (PERCENT) = 28.67


| CC AUGUST MET DATA JOINT FREQUENCY DISTRIBUTION | $(60-M E T E R ~ T O W E R)$ |  |  |
| :--- | :---: | :---: | :---: |
| $33.0 ~ F T ~ W I N D ~ D A T A ~$ | STABILITY CLASS E | CLASS FREQUENCY | (PERCENT) $=27.43$ |


(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

| CC AUGUST MET DATA JOINT FREQUENCY DISTRIBUTION | $(60$-METER TOWER) |  |  |
| :--- | :---: | :---: | :---: |
| 33.0 FT WIND DATA | STABILITY CLASS F | CLASS FREQUENCY | (PERCENT) $=11.97$ |


| CC AUGUST MET DATA JOINT FREQUENCY DISTRIBUTION | $(60$-METER TOWER) |  |  |
| :--- | :---: | :---: | :---: |
| 33.0 FT WIND DATA | STABILITY CLASS G | CLASS FREQUENCY | (PERCENT) $=\mathbf{7 . 9 7}$ |



Table 2.3-25—\{CCNPP 33 ft ( 10 m) August JFD (2000-2005) \} (Page 8 of 8)
CC AUGUST MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
33.0 FT WIND DATA STABILITY CLASS ALL CLASS FREQUENCY (PERCENT) = 100.00

| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 3 | 1 | 4 | 0 | 0 | 3 | 0 | 0 | 14 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 02 | . 07 | . 02 | . 09 | . 00 | . 00 | . 07 | . 00 | . 00 | . 32 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 02 | . 07 | . 02 | . 09 | . 00 | . 00 | . 07 | . 00 | . 00 | . 32 |
| . $2-.4$ | 0 | 0 | 2 | 0 | 1 | 2 | 0 | 1 | 6 | 6 | 7 | 2 | 5 | 3 | 2 | 1 | 0 | 38 |
| (1) | . 00 | . 00 | . 05 | . 00 | . 02 | . 05 | . 00 | . 02 | . 14 | . 14 | . 16 | . 05 | . 11 | . 07 | . 05 | . 02 | . 00 | . 86 |
| (2) | . 00 | . 00 | . 05 | . 00 | . 02 | . 05 | . 00 | . 02 | . 14 | . 14 | . 16 | . 05 | . 11 | . 07 | . 05 | . 02 | . 00 | . 86 |
| .5-1.0 | 7 | 1 | 5 | 2 | 10 | 12 | 10 | 21 | 39 | 74 | 84 | 58 | 47 | 24 | 12 | 17 | 0 | 423 |
| (1) | . 16 | . 02 | . 11 | . 05 | . 23 | . 27 | . 23 | . 48 | . 88 | 1.67 | 1.90 | 1.31 | 1.06 | . 54 | . 27 | . 38 | . 00 | 9.57 |
| (2) | . 16 | . 02 | . 11 | . 05 | . 23 | . 27 | . 23 | . 48 | . 88 | 1.67 | 1.90 | 1.31 | 1.06 | . 54 | . 27 | . 38 | . 00 | 9.57 |
| 1.1-1.5 | 16 | 13 | 15 | 7 | 35 | 22 | 19 | 39 | 59 | 163 | 179 | 92 | 38 | 26 | 15 | 12 | 0 | 750 |
| (1) | . 36 | . 29 | . 34 | . 16 | . 79 | . 50 | . 43 | . 88 | 1.34 | 3.69 | 4.05 | 2.08 | . 86 | . 59 | . 34 | . 27 | . 00 | 16.97 |
| (2) | . 36 | . 29 | . 34 | . 16 | . 79 | . 50 | . 43 | . 88 | 1.34 | 3.69 | 4.05 | 2.08 | . 86 | . 59 | . 34 | . 27 | . 00 | 16.97 |
| 1.6-2.0 | 27 | 27 | 26 | 37 | 39 | 27 | 28 | 53 | 71 | 134 | 174 | 67 | 35 | 38 | 35 | 22 | 0 | 840 |
| (1) | . 61 | . 61 | . 59 | . 84 | . 88 | . 61 | . 63 | 1.20 | 1.61 | 3.03 | 3.94 | 1.52 | . 79 | . 86 | . 79 | . 50 | . 00 | 19.01 |
| (2) | . 61 | . 61 | . 59 | . 84 | . 88 | . 61 | . 63 | 1.20 | 1.61 | 3.03 | 3.94 | 1.52 | . 79 | . 86 | . 79 | . 50 | . 00 | 19.01 |
| 2.1-3.0 | 92 | 114 | 66 | 63 | 50 | 41 | 59 | 123 | 107 | 120 | 310 | 106 | 33 | 31 | 43 | 41 | 0 | 1399 |
| (1) | 2.08 | 2.58 | 1.49 | 1.43 | 1.13 | . 93 | 1.34 | 2.78 | 2.42 | 2.72 | 7.02 | 2.40 | . 75 | . 70 | . 97 | . 93 | . 00 | 31.66 |
| (2) | 2.08 | 2.58 | 1.49 | 1.43 | 1.13 | . 93 | 1.34 | 2.78 | 2.42 | 2.72 | 7.02 | 2.40 | . 75 | . 70 | . 97 | . 93 | . 00 | 31.66 |
| 3.1-4.0 | 77 | 69 | 69 | 26 | 14 | 17 | 21 | 63 | 21 | 32 | 141 | 38 | 13 | 8 | 12 | 26 | 0 | 647 |
| (1) | 1.74 | 1.56 | 1.56 | . 59 | . 32 | . 38 | . 48 | 1.43 | . 48 | . 72 | 3.19 | . 86 | . 29 | . 18 | . 27 | . 59 | . 00 | 14.64 |
| (2) | 1.74 | 1.56 | 1.56 | . 59 | . 32 | . 38 | . 48 | 1.43 | . 48 | . 72 | 3.19 | . 86 | . 29 | . 18 | . 27 | . 59 | . 00 | 14.64 |
| 4.1-5.0 | 43 | 43 | 22 | 16 | 4 | 4 | 14 | 23 | 7 | 10 | 13 | 4 | 1 | 4 | 2 | 6 | 0 | 216 |
| (1) | . 97 | . 97 | . 50 | . 36 | . 09 | . 09 | . 32 | . 52 | . 16 | . 23 | . 29 | . 09 | . 02 | . 09 | . 05 | . 14 | . 00 | 4.89 |
| (2) | . 97 | . 97 | . 50 | . 36 | . 09 | . 09 | . 32 | . 52 | . 16 | . 23 | . 29 | . 09 | . 02 | . 09 | . 05 | . 14 | . 00 | 4.89 |
| 5.1-6.0 | 13 | 18 | 16 | 4 | 1 | 1 | 2 | 6 | 0 | 0 | 2 | 1 | 1 | 0 | 1 | 1 | 0 | 67 |
| (1) | . 29 | . 41 | . 36 | . 09 | . 02 | . 02 | . 05 | . 14 | . 00 | . 00 | . 05 | . 02 | . 02 | . 00 | . 02 | . 02 | . 00 | 1.52 |
| (2) | . 29 | . 41 | . 36 | . 09 | . 02 | . 02 | . 05 | . 14 | . 00 | . 00 | . 05 | . 02 | . 02 | . 00 | . 02 | . 02 | . 00 | 1.52 |
| 6.1-8.0 | 5 | 3 | 6 | 4 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 22 |
| (1) | . 11 | . 07 | . 14 | . 09 | . 05 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 50 |
| (2) | . 11 | . 07 | . 14 | . 09 | . 05 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 50 |
| 8.1-10.0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 3 |
| (1) | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 07 |
| (2) | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 07 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 280 | 288 | 228 | 160 | 157 | 126 | 153 | 331 | 311 | 542 | 911 | 372 | 173 | 134 | 126 | 127 | 0 | 4419 |
| (1) | 6.34 | 6.52 | 5.16 | 3.62 | 3.55 | 2.85 | 3.46 | 7.49 | 7.04 | 12.27 | 20.62 | 8.42 | 3.91 | 3.03 | 2.85 | 2.87 | . 00 | 100.00 |
| (2) | 6.34 | 6.52 | 5.16 | 3.62 | 3.55 | 2.85 | 3.46 | 7.49 | 7.04 | 12.27 | 20.62 | 8.42 | 3.91 | 3.03 | 2.85 | 2.87 | . 00 | 100.00 |
| (1) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| (2) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

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$i$

Table 2．3－26—\｛CCNPP 33 ft（ 10 m ）September JFD（2000－2005）\}

## （Page 1 of 8）

CC SEPTEMBER MET DATA JOINT FREQUENCY DISTRIBUTION（60－METER TOWER）

| 33．0 FT WIND DATA |  |  | STABILITY CLASS A |  |  |  | CLASS FREQUENCY（PERCENT）$=11.82$EECTION FROM |  |  |  |  |  |  |  | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW |  |  |  |  |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT ． 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| ． $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| ． $5-1.0$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| 1．1－1．5 | 0 | 1 | 2 | 1 | 1 | 0 | 2 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 1 | 0 | 11 |
| （1） | ． 00 | ． 20 | ． 40 | ． 20 | ． 20 | ． 00 | ． 40 | ． 00 | ． 00 | ． 00 | ． 60 | ． 00 | ． 00 | ． 00 | ． 00 | ． 20 | ． 00 | 2.20 |
| （2） | ． 00 | ． 02 | ． 05 | ． 02 | ． 02 | ． 00 | ． 05 | ． 00 | ． 00 | ． 00 | ． 07 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 26 |
| 1．6－2．0 | 3 | 4 | 4 | 0 | 2 | 2 | 1 | 4 | 1 | 2 | 5 | 1 | 2 | 2 | 1 | 0 | 0 | 34 |
| （1） | ． 60 | ． 80 | ． 80 | ． 00 | ． 40 | ． 40 | ． 20 | ． 80 | ． 20 | ． 40 | 1.00 | ． 20 | ． 40 | ． 40 | ． 20 | ． 00 | ． 00 | 6.81 |
| （2） | ． 07 | ． 09 | ． 09 | ． 00 | ． 05 | ． 05 | ． 02 | ． 09 | ． 02 | ． 05 | ． 12 | ． 02 | ． 05 | ． 05 | ． 02 | ． 00 | ． 00 | ． 81 |
| 2．1－3．0 | 30 | 29 | 16 | 5 | 7 | 7 | 6 | 7 | 7 | 17 | 26 | 14 | 3 | 2 | 2 | 1 | 0 | 179 |
| （1） | 6.01 | 5.81 | 3.21 | 1.00 | 1.40 | 1.40 | 1.20 | 1.40 | 1.40 | 3.41 | 5.21 | 2.81 | ． 60 | ． 40 | ． 40 | ． 20 | ． 00 | 35.87 |
| （2） | ． 71 | ． 69 | ． 38 | ． 12 | ． 17 | ． 17 | ． 14 | ． 17 | ． 17 | ． 40 | ． 62 | ． 33 | ． 07 | ． 05 | ． 05 | ． 02 | ． 00 | 4.24 |
| 3．1－4．0 | 45 | 38 | 18 | 0 | 0 | 5 | 25 | 18 | 4 | 13 | 14 | 10 | 0 | 3 | 0 | 4 | 0 | 197 |
| （1） | 9.02 | 7.62 | 3.61 | ． 00 | ． 00 | 1.00 | 5.01 | 3.61 | ． 80 | 2.61 | 2.81 | 2.00 | ． 00 | ． 60 | ． 00 | ． 80 | ． 00 | 39.48 |
| （2） | 1.07 | ． 90 | ． 43 | ． 00 | ． 00 | ． 12 | ． 59 | ． 43 | ． 09 | ． 31 | ． 33 | ． 24 | ． 00 | ． 07 | ． 00 | ． 09 | ． 00 | 4.66 |
| 4．1－5．0 | 11 | 9 | 7 | 1 | 0 | 0 | 4 | 6 | 2 | 5 | 2 | 1 | 0 | 2 | 0 | 0 | 0 | 50 |
| （1） | 2.20 | 1.80 | 1.40 | ． 20 | ． 00 | ． 00 | ． 80 | 1.20 | ． 40 | 1.00 | ． 40 | ． 20 | ． 00 | ． 40 | ． 00 | ． 00 | ． 00 | 10.02 |
| （2） | ． 26 | ． 21 | ． 17 | ． 02 | ． 00 | ． 00 | ． 09 | ． 14 | ． 05 | ． 12 | ． 05 | ． 02 | ． 00 | ． 05 | ． 00 | ． 00 | ． 00 | 1.18 |
| 5．1－6．0 | 4 | 6 | 11 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 25 |
| （1） | ． 80 | 1.20 | 2.20 | ． 00 | ． 00 | ． 00 | ． 00 | ． 40 | ． 00 | ． 20 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 20 | ． 00 | 5.01 |
| （2） | ． 09 | ． 14 | ． 26 | ． 00 | ． 00 | ． 00 | ． 00 | ． 05 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 59 |
| 6．1－8．0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 3 |
| （1） | ． 00 | ． 00 | ． 20 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 40 | ． 00 | ． 00 | ． 60 |
| （2） | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 05 | ． 00 | ． 00 | ． 07 |
| 8．1－10．0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| 10．1－89．5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| ALL SPEEDS | 93 | 87 | 59 | 7 | 10 | 14 | 38 | 37 | 14 | 38 | 50 | 26 | 5 | 9 | 5 | 7 | 0 | 499 |
| （1） | 18.64 | 17.43 | 11.82 | 1.40 | 2.00 | 2.81 | 7.62 | 7.41 | 2.81 | 7.62 | 10.02 | 5.21 | 1.00 | 1.80 | 1.00 | 1.40 | ． 00 | 100.00 |
| （2） | 2.20 | 2.06 | 1.40 | ． 17 | ． 24 | ． 33 | ． 90 | ． 88 | ． 33 | ． 90 | 1.18 | ． 62 | ． 12 | ． 21 | ． 12 | ． 17 | ． 00 | 11.82 |
| （1）＝PERCENT | OF ALI | GOOD | OBSERV | ATIONS | FOR T | HIS PA |  |  |  |  |  |  |  |  |  |  |  |  |

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Table 2.3-26—\{CCNPP 33 ft ( 10 m) September JFD (2000-2005)\} (Page 2 of 8)
CC SEPTEMBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
33.0 FT WIND DATA STABILITY CLASS B CLASS FREQUENCY (PERCENT) = 5.49

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 43 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 43 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| 1.1-1.5 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| (1) | . 00 | . 43 | . 00 | . 43 | . 43 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.29 |
| (2) | . 00 | . 02 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 |
| 1.6-2.0 | 2 | 1 | 4 | 3 | 1 | 2 | 1 | 0 | 2 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 19 |
| (1) | . 86 | . 43 | 1.72 | 1.29 | . 43 | . 86 | . 43 | . 00 | . 86 | . 43 | . 43 | . 43 | . 00 | . 00 | . 00 | . 00 | . 00 | 8.19 |
| (2) | . 05 | . 02 | . 09 | . 07 | . 02 | . 05 | . 02 | . 00 | . 05 | . 02 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 45 |
| 2.1-3.0 | 11 | 15 | 6 | 7 | 4 | 4 | 5 | 7 | 3 | 2 | 6 | 2 | 2 | 4 | 1 | 2 | 0 | 81 |
| (1) | 4.74 | 6.47 | 2.59 | 3.02 | 1.72 | 1.72 | 2.16 | 3.02 | 1.29 | . 86 | 2.59 | . 86 | . 86 | 1.72 | . 43 | . 86 | . 00 | 34.91 |
| (2) | . 26 | . 36 | . 14 | . 17 | . 09 | . 09 | . 12 | . 17 | . 07 | . 05 | . 14 | . 05 | . 05 | . 09 | . 02 | . 05 | . 00 | 1.92 |
| 3.1-4.0 | 17 | 13 | 10 | 1 | 0 | 1 | 4 | 8 | 0 | 3 | 3 | 3 | 0 | 2 | 3 | 0 | 0 | 68 |
| (1) | 7.33 | 5.60 | 4.31 | . 43 | . 00 | . 43 | 1.72 | 3.45 | . 00 | 1.29 | 1.29 | 1.29 | . 00 | . 86 | 1.29 | . 00 | . 00 | 29.31 |
| (2) | . 40 | . 31 | . 24 | . 02 | . 00 | . 02 | . 09 | . 19 | . 00 | . 07 | . 07 | . 07 | . 00 | . 05 | . 07 | . 00 | . 00 | 1.61 |
| 4.1-5.0 | 7 | 2 | 8 | 1 | 0 | 0 | 2 | 5 | 2 | 0 | 1 | 0 | 0 | 2 | 3 | 0 | 0 | 33 |
| (1) | 3.02 | . 86 | 3.45 | . 43 | . 00 | . 00 | . 86 | 2.16 | . 86 | . 00 | . 43 | . 00 | . 00 | . 86 | 1.29 | . 00 | . 00 | 14.22 |
| (2) | . 17 | . 05 | . 19 | . 02 | . 00 | . 00 | . 05 | . 12 | . 05 | . 00 | . 02 | . 00 | . 00 | . 05 | . 07 | . 00 | . 00 | . 78 |
| 5.1-6.0 | 4 | 3 | 7 | 0 | 0 | 0 | 2 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 21 |
| (1) | 1.72 | 1.29 | 3.02 | . 00 | . 00 | . 00 | . 86 | . 86 | . 43 | . 00 | . 00 | . 00 | . 00 | . 00 | . 86 | . 00 | . 00 | 9.05 |
| (2) | . 09 | . 07 | . 17 | . 00 | . 00 | . 00 | . 05 | . 05 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 00 | . 50 |
| 6.1-8.0 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 6 |
| (1) | . 43 | . 43 | . 43 | . 43 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 43 | . 43 | . 00 | . 00 | 2.59 |
| (2) | . 02 | . 02 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 14 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 42 | 36 | 36 | 14 | 6 | 7 | 15 | 22 | 8 | 6 | 11 | 6 | 2 | 9 | 10 | 2 | 0 | 232 |
| (1) | 18.10 | 15.52 | 15.52 | 6.03 | 2.59 | 3.02 | 6.47 | 9.48 | 3.45 | 2.59 | 4.74 | 2.59 | . 86 | 3.88 | 4.31 | . 86 | . 00 | 100.00 |
| (2) | . 99 | . 85 | . 85 | . 33 | . 14 | . 17 | . 36 | . 52 | . 19 | . 14 | . 26 | . 14 | . 05 | . 21 | . 24 | . 05 | . 00 | 5.49 |

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD


#### Abstract

CC SEPTEMBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER 33.0 FT WIND DATA STABILITY CLASS C CLASS FREQUENCY (PERCENT) = 5.78


|  |  |  |  |  |  |  |  | NIND D | ET | FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 2 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 41 | . 00 | . 00 | . 00 | . 00 | . 41 | . 00 | . 82 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 05 |
| 1.1-1.5 | 0 | 1 | 1 | 1 | 3 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 3 | 0 | 0 | 0 | 0 | 15 |
| (1) | . 00 | . 41 | . 41 | . 41 | 1.23 | . 00 | . 41 | . 82 | . 00 | . 00 | . 41 | . 82 | 1.23 | . 00 | . 00 | . 00 | . 00 | 6.15 |
| (2) | . 00 | . 02 | . 02 | . 02 | . 07 | . 00 | . 02 | . 05 | . 00 | . 00 | . 02 | . 05 | . 07 | . 00 | . 00 | . 00 | . 00 | . 36 |
| 1.6-2.0 | 2 | 14 | 3 | 3 | 4 | 4 | 4 | 4 | 4 | 1 | 0 | 0 | 1 | 0 | 2 | 1 | 0 | 47 |
| (1) | . 82 | 5.74 | 1.23 | 1.23 | 1.64 | 1.64 | 1.64 | 1.64 | 1.64 | . 41 | . 00 | . 00 | . 41 | . 00 | . 82 | . 41 | . 00 | 19.26 |
| (2) | . 05 | . 33 | . 07 | . 07 | . 09 | . 09 | . 09 | . 09 | . 09 | . 02 | . 00 | . 00 | . 02 | . 00 | . 05 | . 02 | . 00 | 1.11 |
| 2.1-3.0 | 12 | 19 | 7 | 8 | 6 | 5 | 8 | 6 | 3 | 1 | 5 | 3 | 1 | 6 | 1 | 2 | 0 | 93 |
| (1) | 4.92 | 7.79 | 2.87 | 3.28 | 2.46 | 2.05 | 3.28 | 2.46 | 1.23 | . 41 | 2.05 | 1.23 | . 41 | 2.46 | . 41 | . 82 | . 00 | 38.11 |
| (2) | . 28 | . 45 | . 17 | . 19 | . 14 | . 12 | . 19 | . 14 | . 07 | . 02 | . 12 | . 07 | . 02 | . 14 | . 02 | . 05 | . 00 | 2.20 |
| 3.1-4.0 | 13 | 4 | 11 | 2 | 1 | 0 | 1 | 10 | 1 | 1 | 2 | 0 | 1 | 2 | 5 | 2 | 0 | 56 |
| (1) | 5.33 | 1.64 | 4.51 | . 82 | . 41 | . 00 | . 41 | 4.10 | . 41 | . 41 | . 82 | . 00 | . 41 | . 82 | 2.05 | . 82 | . 00 | 22.95 |
| (2) | . 31 | . 09 | . 26 | . 05 | . 02 | . 00 | . 02 | . 24 | . 02 | . 02 | . 05 | . 00 | . 02 | . 05 | . 12 | . 05 | . 00 | 1.33 |
| 4.1-5.0 | 4 | 1 | 4 | 1 | 0 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 16 |
| (1) | 1.64 | . 41 | 1.64 | . 41 | . 00 | . 00 | . 41 | 1.64 | . 00 | . 00 | . 00 | . 00 | . 00 | . 41 | . 00 | . 00 | . 00 | 6.56 |
| (2) | . 09 | . 02 | . 09 | . 02 | . 00 | . 00 | . 02 | . 09 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 38 |
| 5.1-6.0 | 1 | 1 | 7 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 13 |
| (1) | . 41 | . 41 | 2.87 | . 82 | . 00 | . 00 | . 00 | . 41 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 41 | . 00 | . 00 | 5.33 |
| (2) | . 02 | . 02 | . 17 | . 05 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 31 |
| 6.1-8.0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| (1) | . 82 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 82 |
| (2) | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 34 | 40 | 33 | 17 | 14 | 9 | 15 | 27 | 8 | 3 | 9 | 5 | 6 | 9 | 9 | 6 | 0 | 244 |
| (1) | 13.93 | 16.39 | 13.52 | 6.97 | 5.74 | 3.69 | 6.15 | 11.07 | 3.28 | 1.23 | 3.69 | 2.05 | 2.46 | 3.69 | 3.69 | 2.46 | . 00 | 100.00 |
| (2) | . 81 | . 95 | . 78 | . 40 | . 33 | . 21 | . 36 | . 64 | . 19 | . 07 | . 21 | . 12 | . 14 | . 21 | . 21 | . 14 | . 00 | 5.78 |

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
T
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$i$
$\begin{array}{lll}\text { CC SEPTEMBER MET DATA } & \text { JOINT FREQUENCY DISTRIBUTION } & \text { ( } 60 \text {-METER TOWER) } \\ \text { 33.0 FT WIND DATA } & \text { STABILITY CLASS D } & \text { CLASS FREQUENCY } \\ \text { (PERCENT) })=34.31\end{array}$

| WIND DIRECTION FROM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { SPEED } \\ & \text { mps } \end{aligned}$ | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| . 5- 1.0 | 1 | 2 | 5 | 1 | 5 | 5 | 1 | 4 | 1 | 4 | 3 | 1 | 1 | 4 | 1 | 3 | 0 | 42 |
| (1) | . 07 | . 14 | . 35 | . 07 | . 35 | . 35 | . 07 | . 28 | . 07 | . 28 | . 21 | . 07 | . 07 | . 28 | . 07 | . 21 | . 00 | 2.90 |
| (2) | . 02 | . 05 | . 12 | . 02 | . 12 | . 12 | . 02 | . 09 | . 02 | . 09 | . 07 | . 02 | . 02 | . 09 | . 02 | . 07 | . 00 | . 99 |
| 1.1-1.5 | 14 | 16 | 8 | 11 | 13 | 6 | 6 | 4 | 8 | 7 | 9 | 6 | 4 | 2 | 2 | 4 | 0 | 120 |
| (1) | . 97 | 1.10 | . 55 | . 76 | . 90 | . 41 | . 41 | . 28 | . 55 | . 48 | . 62 | . 41 | . 28 | . 14 | . 14 | . 28 | . 00 | 8.28 |
| (2) | . 33 | . 38 | . 19 | . 26 | . 31 | . 14 | . 14 | . 09 | . 19 | . 17 | . 21 | . 14 | . 09 | . 05 | . 05 | . 09 | . 00 | 2.84 |
| 1.6-2.0 | 14 | 27 | 13 | 17 | 25 | 14 | 15 | 9 | 7 | 8 | 13 | 4 | 4 | 8 | 6 | 7 | 0 | 191 |
| (1) | . 97 | 1.86 | . 90 | 1.17 | 1.73 | . 97 | 1.04 | . 62 | . 48 | . 55 | . 90 | . 28 | . 28 | . 55 | . 41 | . 48 | . 00 | 13.18 |
| (2) | . 33 | . 64 | . 31 | . 40 | . 59 | . 33 | . 36 | . 21 | . 17 | . 19 | . 31 | . 09 | . 09 | . 19 | . 14 | . 17 | . 00 | 4.52 |
| 2.1-3.0 | 39 | 40 | 26 | 52 | 63 | 33 | 23 | 28 | 14 | 4 | 21 | 6 | 7 | 13 | 14 | 19 | 0 | 402 |
| (1) | 2.69 | 2.76 | 1.79 | 3.59 | 4.35 | 2.28 | 1.59 | 1.93 | . 97 | . 28 | 1.45 | . 41 | . 48 | . 90 | . 97 | 1.31 | . 00 | 27.74 |
| (2) | . 92 | . 95 | . 62 | 1.23 | 1.49 | . 78 | . 54 | . 66 | . 33 | . 09 | . 50 | . 14 | . 17 | . 31 | . 33 | . 45 | . 00 | 9.52 |
| 3.1-4.0 | 25 | 15 | 34 | 44 | 19 | 12 | 4 | 25 | 8 | 4 | 15 | 8 | 5 | 3 | 11 | 20 | 0 | 252 |
| (1) | 1.73 | 1.04 | 2.35 | 3.04 | 1.31 | . 83 | . 28 | 1.73 | . 55 | . 28 | 1.04 | . 55 | . 35 | . 21 | . 76 | 1.38 | . 00 | 17.39 |
| (2) | . 59 | . 36 | . 81 | 1.04 | . 45 | . 28 | . 09 | . 59 | . 19 | . 09 | . 36 | . 19 | . 12 | . 07 | . 26 | . 47 | . 00 | 5.97 |
| 4.1-5.0 | 22 | 16 | 55 | 39 | 4 | 1 | 5 | 11 | 8 | 1 | 0 | 0 | 0 | 1 | 6 | 7 | 0 | 176 |
| (1) | 1.52 | 1.10 | 3.80 | 2.69 | . 28 | . 07 | . 35 | . 76 | . 55 | . 07 | . 00 | . 00 | . 00 | . 07 | . 41 | . 48 | . 00 | 12.15 |
| (2) | . 52 | . 38 | 1.30 | . 92 | . 09 | . 02 | . 12 | . 26 | . 19 | . 02 | . 00 | . 00 | . 00 | . 02 | . 14 | . 17 | . 00 | 4.17 |
| 5.1-6.0 | 17 | 19 | 49 | 26 | 0 | 0 | 5 | 10 | 1 | 0 | 0 | 0 | 3 | 0 | 3 | 5 | 0 | 138 |
| (1) | 1.17 | 1.31 | 3.38 | 1.79 | . 00 | . 00 | . 35 | . 69 | . 07 | . 00 | . 00 | . 00 | . 21 | . 00 | . 21 | . 35 | . 00 | 9.52 |
| (2) | . 40 | . 45 | 1.16 | . 62 | . 00 | . 00 | . 12 | . 24 | . 02 | . 00 | . 00 | . 00 | . 07 | . 00 | . 07 | . 12 | . 00 | 3.27 |
| 6.1-8.0 | 22 | 20 | 50 | 6 | 0 | 0 | 2 | 5 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 109 |
| (1) | 1.52 | 1.38 | 3.45 | . 41 | . 00 | . 00 | . 14 | . 35 | . 28 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 7.52 |
| (2) | . 52 | . 47 | 1.18 | . 14 | . 00 | . 00 | . 05 | . 12 | . 09 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 2.58 |
| 8.1-10.0 | 2 | 2 | 8 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 |
| (1) | . 14 | . 14 | . 55 | . 00 | . 07 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 90 |
| (2) | . 05 | . 05 | . 19 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 31 |
| 10.1-89.5 | 0 | 0 | 2 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| (1) | . 00 | . 00 | . 14 | . 00 | . 07 | . 00 | . 07 | . 07 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 35 |
| (2) | . 00 | . 00 | . 05 | . 00 | . 02 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 12 |
| ALL SPEEDS | 156 | 157 | 250 | 196 | 131 | 71 | 62 | 97 | 51 | 28 | 62 | 25 | 24 | 31 | 43 | 65 | 0 | 1449 |
| (1) | 10.77 | 10.84 | 17.25 | 13.53 | 9.04 | 4.90 | 4.28 | 6.69 | 3.52 | 1.93 | 4.28 | 1.73 | 1.66 | 2.14 | 2.97 | 4.49 | . 00 | 100.00 |
| (2) | 3.69 | 3.72 | 5.92 | 4.64 | 3.10 | 1.68 | 1.47 | 2.30 | 1.21 | . 66 | 1.47 | . 59 | . 57 | . 73 | 1.02 | 1.54 | . 00 | 34.31 |
| $\begin{aligned} & (1)=\text { PERCENT } \\ & (2)=\text { PERCENT } \end{aligned}$ | OF ALI | GOOD OBS | OBSERV | VATIONS ONS FOR | $\begin{gathered} \text { FOR I } \\ \text { THIS } \end{gathered}$ | HIS PF ERIOD |  |  |  |  |  |  |  |  |  |  |  |  |

Table 2.3-26—\{CCNPP 33 ft (10 m) September JFD (2000-2005)\} (Page 5 of 8)
CC SEPTEMBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
33.0 FT WIND DATA STABILITY CLASS E CLASS FREQUENCY (PERCENT) = 22.42

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$$
\begin{array}{lccc}
\text { CC SEPTEMBER MET DATA JOINT FREQUENCY DISTRIBUTION } & (60-M E T E R ~ T O W E R) \\
33.0 ~ F T ~ W I N D ~ D A T A ~ & \text { STABILITY CLASS F } & \text { CLASS FREQUENCY } & \text { (PERCENT) }=10.02
\end{array}
$$



## CC SEPTEMBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER <br> 33.0 FT WIND DATA STABILITY CLASS G CLASS FREQUENCY (PERCENT) = 10.16

|  | WIND DIRECTION FROM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 7 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 23 | . 00 | . 47 | . 23 | . 23 | . 47 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.63 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 05 | . 02 | . 02 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 17 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 0 | 6 | 1 | 4 | 2 | 3 | 1 | 0 | 21 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 23 | . 23 | . 23 | . 23 | . 00 | 1.40 | . 23 | . 93 | . 47 | . 70 | . 23 | . 00 | 4.90 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 02 | . 02 | . 00 | . 14 | . 02 | . 09 | . 05 | . 07 | . 02 | . 00 | . 50 |
| .5-1.0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 6 | 5 | 10 | 27 | 27 | 35 | 29 | 3 | 3 | 0 | 147 |
| (1) | . 23 | . 23 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.40 | 1.17 | 2.33 | 6.29 | 6.29 | 8.16 | 6.76 | . 70 | . 70 | . 00 | 34.27 |
| (2) | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 14 | . 12 | . 24 | . 64 | . 64 | . 83 | . 69 | . 07 | . 07 | . 00 | 3.48 |
| 1.1-1.5 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 15 | 37 | 33 | 19 | 28 | 24 | 3 | 0 | 0 | 163 |
| (1) | . 23 | . 23 | . 00 | . 00 | . 00 | . 00 | . 00 | . 47 | 3.50 | 8.62 | 7.69 | 4.43 | 6.53 | 5.59 | . 70 | . 00 | . 00 | 38.00 |
| (2) | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 36 | . 88 | . 78 | . 45 | . 66 | . 57 | . 07 | . 00 | . 00 | 3.86 |
| 1.6-2.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 13 | 30 | 9 | 8 | 10 | 2 | 0 | 0 | 75 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 70 | 3.03 | 6.99 | 2.10 | 1.86 | 2.33 | . 47 | . 00 | . 00 | 17.48 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 | . 31 | . 71 | . 21 | . 19 | . 24 | . 05 | . 00 | . 00 | 1.78 |
| 2.1-3.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 3 | 3 | 3 | 1 | 0 | 0 | 16 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.40 | . 70 | . 70 | . 70 | . 23 | . 00 | . 00 | 3.73 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 14 | . 07 | . 07 | . 07 | . 02 | . 00 | . 00 | . 38 |
| 3.1-4.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 4.1-5.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 5.1-6.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 6.1-8.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 2 | 2 | 0 | 0 | 0 | 1 | 2 | 9 | 26 | 61 | 103 | 61 | 78 | 68 | 12 | 4 | 0 | 429 |
| (1) | . 47 | . 47 | . 00 | . 00 | . 00 | . 23 | . 47 | 2.10 | 6.06 | 14.22 | 24.01 | 14.22 | 18.18 | 15.85 | 2.80 | . 93 | . 00 | 100.00 |
| (2) | . 05 | . 05 | . 00 | . 00 | . 00 | . 02 | . 05 | . 21 | . 62 | 1.44 | 2.44 | 1.44 | 1.85 | 1.61 | . 28 | . 09 | . 00 | 10.16 |

Table 2.3-26—\{CCNPP 33 ft (10 m) September JFD (2000-2005)\} (Page 8 of 8)
CC SEPTEMBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
33.0 FT WIND DATA STABILITY CLASS ALL CLASS FREQUENCY (PERCENT) $=100.00$

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { SPEED } \\ & \text { mps } \end{aligned}$ | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| LT . 2 | 0 | 1 | 0 | 0 | 0 | 0 | 2 | 1 | 4 | 2 | 4 | 3 | 3 | 1 | 1 | 0 | 0 | 22 |
| (1) | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 05 | . 02 | . 09 | . 05 | . 09 | . 07 | . 07 | . 02 | . 02 | . 00 | . 00 | . 52 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 05 | . 02 | . 09 | . 05 | . 09 | . 07 | . 07 | . 02 | . 02 | . 00 | . 00 | . 52 |
| .2- . 4 | 0 | 0 | 2 | 0 | 0 | 1 | 3 | 6 | 1 | 2 | 8 | 3 | 5 | 4 | 4 | 1 | 0 | 40 |
| (1) | . 00 | . 00 | . 05 | . 00 | . 00 | . 02 | . 07 | . 14 | . 02 | . 05 | . 19 | . 07 | . 12 | . 09 | . 09 | . 02 | . 00 | . 95 |
| (2) | . 00 | . 00 | . 05 | . 00 | . 00 | . 02 | . 07 | . 14 | . 02 | . 05 | . 19 | . 07 | . 12 | . 09 | . 09 | . 02 | . 00 | . 95 |
| .5-1.0 | 11 | 5 | 7 | 4 | 14 | 17 | 17 | 18 | 30 | 33 | 54 | 42 | 44 | 44 | 8 | 16 | 0 | 364 |
| (1) | . 26 | . 12 | . 17 | . 09 | . 33 | . 40 | . 40 | . 43 | . 71 | . 78 | 1.28 | . 99 | 1.04 | 1.04 | . 19 | . 38 | . 00 | 8.62 |
| (2) | . 26 | . 12 | . 17 | . 09 | . 33 | . 40 | . 40 | . 43 | . 71 | . 78 | 1.28 | . 99 | 1.04 | 1.04 | . 19 | . 38 | . 00 | 8.62 |
| 1.1-1.5 | 28 | 24 | 14 | 18 | 27 | 19 | 26 | 37 | 60 | 97 | 93 | 47 | 55 | 43 | 27 | 19 | 0 | 634 |
| (1) | . 66 | . 57 | . 33 | . 43 | . 64 | . 45 | . 62 | . 88 | 1.42 | 2.30 | 2.20 | 1.11 | 1.30 | 1.02 | . 64 | . 45 | . 00 | 15.01 |
| (2) | . 66 | . 57 | . 33 | . 43 | . 64 | . 45 | . 62 | . 88 | 1.42 | 2.30 | 2.20 | 1.11 | 1.30 | 1.02 | . 64 | . 45 | . 00 | 15.01 |
| 1.6-2.0 | 28 | 59 | 30 | 27 | 36 | 34 | 30 | 44 | 64 | 43 | 75 | 23 | 28 | 42 | 38 | 18 | 0 | 619 |
| (1) | . 66 | 1.40 | . 71 | . 64 | . 85 | . 81 | . 71 | 1.04 | 1.52 | 1.02 | 1.78 | . 54 | . 66 | . 99 | . 90 | . 43 | . 00 | 14.66 |
| (2) | . 66 | 1.40 | . 71 | . 64 | . 85 | . 81 | . 71 | 1.04 | 1.52 | 1.02 | 1.78 | . 54 | . 66 | . 99 | . 90 | . 43 | . 00 | 14.66 |
| 2.1-3.0 | 104 | 120 | 64 | 86 | 91 | 56 | 54 | 70 | 78 | 61 | 118 | 45 | 32 | 59 | 81 | 48 | 0 | 1167 |
| (1) | 2.46 | 2.84 | 1.52 | 2.04 | 2.15 | 1.33 | 1.28 | 1.66 | 1.85 | 1.44 | 2.79 | 1.07 | . 76 | 1.40 | 1.92 | 1.14 | . 00 | 27.63 |
| (2) | 2.46 | 2.84 | 1.52 | 2.04 | 2.15 | 1.33 | 1.28 | 1.66 | 1.85 | 1.44 | 2.79 | 1.07 | . 76 | 1.40 | 1.92 | 1.14 | . 00 | 27.63 |
| 3.1-4.0 | 106 | 78 | 94 | 50 | 21 | 18 | 35 | 68 | 27 | 28 | 68 | 27 | 7 | 13 | 40 | 39 | 0 | 719 |
| (1) | 2.51 | 1.85 | 2.23 | 1.18 | . 50 | . 43 | . 83 | 1.61 | . 64 | . 66 | 1.61 | . 64 | . 17 | . 31 | . 95 | . 92 | . 00 | 17.03 |
| (2) | 2.51 | 1.85 | 2.23 | 1.18 | . 50 | . 43 | . 83 | 1.61 | . 64 | . 66 | 1.61 | . 64 | . 17 | . 31 | . 95 | . 92 | . 00 | 17.03 |
| 4.1-5.0 | 45 | 28 | 82 | 42 | 4 | 1 | 12 | 27 | 17 | 8 | 10 | 2 | 0 | 9 | 9 | 9 | 0 | 305 |
| (1) | 1.07 | . 66 | 1.94 | . 99 | . 09 | . 02 | . 28 | . 64 | . 40 | . 19 | . 24 | . 05 | . 00 | . 21 | . 21 | . 21 | . 00 | 7.22 |
| (2) | 1.07 | . 66 | 1.94 | . 99 | . 09 | . 02 | . 28 | . 64 | . 40 | . 19 | . 24 | . 05 | . 00 | . 21 | . 21 | . 21 | . 00 | 7.22 |
| 5.1-6.0 | 28 | 31 | 75 | 28 | 0 | 0 | 7 | 15 | 2 | 1 | 0 | 0 | 4 | 0 | 6 | 6 | 0 | 203 |
| (1) | . 66 | . 73 | 1.78 | . 66 | . 00 | . 00 | . 17 | . 36 | . 05 | . 02 | . 00 | . 00 | . 09 | . 00 | . 14 | . 14 | . 00 | 4.81 |
| (2) | . 66 | . 73 | 1.78 | . 66 | . 00 | . 00 | . 17 | . 36 | . 05 | . 02 | . 00 | . 00 | . 09 | . 00 | . 14 | . 14 | . 00 | 4.81 |
| $6.1-8.0$ | 25 | 21 | 52 | 8 | 0 | 0 | 2 | 7 | 4 | 0 | 1 | 0 | 0 | 1 | 3 | 0 | 0 | 124 |
| (1) | . 59 | . 50 | 1.23 | . 19 | . 00 | . 00 | . 05 | . 17 | . 09 | . 00 | . 02 | .00 | . 00 | . 02 | . 07 | . 00 | . 00 | 2.94 |
| (2) | . 59 | . 50 | 1.23 | . 19 | . 00 | . 00 | . 05 | . 17 | . 09 | . 00 | . 02 | . 00 | . 00 | . 02 | . 07 | . 00 | . 00 | 2.94 |
| 8.1-10.0 | 3 | 2 | 8 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 |
| (1) | . 07 | . 05 | . 19 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 33 |
| (2) | . 07 | . 05 | . 19 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 33 |
| 10.1-89.5 | 0 | 0 | 3 | 2 | 1 | 2 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 |
| (1) | . 00 | . 00 | . 07 | . 05 | . 02 | . 05 | . 07 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 28 |
| (2) | . 00 | . 00 | . 07 | . 05 | . 02 | . 05 | . 07 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 28 |
| ALL SPEEDS | 378 | 369 | 431 | 265 | 195 | 148 | 191 | 294 | 287 | 275 | 431 | 192 | 178 | 216 | 217 | 156 | 0 | 4223 |
| (1) | 8.95 | 8.74 | 10.21 | 6.28 | 4.62 | 3.50 | 4.52 | 6.96 | 6.80 | 6.51 | 10.21 | 4.55 | 4.22 | 5.11 | 5.14 | 3.69 | . 00 | 100.00 |
| (2) | 8.95 | 8.74 | 10.21 | 6.28 | 4.62 | 3.50 | 4.52 | 6.96 | 6.80 | 6.51 | 10.21 | 4.55 | 4.22 | 5.11 | 5.14 | 3.69 | . 00 | 100.00 |

T
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$i$
$i$
CC OCTOBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER
33.0 FT WIND DATA STABILITY CLASS A CLASS FREQUENCY (PERCENT) = 12.81

(1) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

| CC OCTOBER MET DATA JOINT FREQUENCY DISTRIBUTION | $(60-M E T E R ~ T O W E R)$ |  |  |
| :--- | :---: | :---: | :---: |
| 33.0 FT WIND DATA | STABILITY CLASS B | CLASS FREQUENCY | (PERCENT) $=3.98$ |


|  |  |  |  |  |  |  |  | ND DIR | ReCIION | FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 1.1-1.5 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 4 |
| (1) | . 00 | . 57 | . 00 | . 00 | . 57 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.14 | . 00 | . 00 | . 00 | 2.27 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 00 | . 00 | . 09 |
| 1.6-2.0 | 0 | 1 | 1 | 1 | 0 | 2 | 2 | 0 | 0 | 1 | 3 | 1 | 0 | 1 | 0 | 4 | 0 | 17 |
| (1) | . 00 | . 57 | . 57 | . 57 | . 00 | 1.14 | 1.14 | . 00 | . 00 | . 57 | 1.70 | . 57 | . 00 | . 57 | . 00 | 2.27 | . 00 | 9.66 |
| (2) | . 00 | . 02 | . 02 | . 02 | . 00 | . 05 | . 05 | . 00 | . 00 | . 02 | . 07 | . 02 | . 00 | . 02 | . 00 | . 09 | . 00 | . 38 |
| 2.1-3.0 | 7 | 8 | 4 | 5 | 1 | 3 | 4 | 1 | 2 | 4 | 5 | 5 | 1 | 2 | 7 | 3 | 0 | 62 |
| (1) | 3.98 | 4.55 | 2.27 | 2.84 | . 57 | 1.70 | 2.27 | . 57 | 1.14 | 2.27 | 2.84 | 2.84 | . 57 | 1.14 | 3.98 | 1.70 | . 00 | 35.23 |
| (2) | . 16 | . 18 | . 09 | . 11 | . 02 | . 07 | . 09 | . 02 | . 05 | . 09 | . 11 | . 11 | . 02 | . 05 | . 16 | . 07 | . 00 | 1.40 |
| 3.1-4.0 | 11 | 10 | 1 | 1 | 0 | 0 | 1 | 6 | 1 | 1 | 4 | 1 | 1 | 4 | 6 | 5 | 0 | 53 |
| (1) | 6.25 | 5.68 | . 57 | . 57 | . 00 | . 00 | . 57 | 3.41 | . 57 | . 57 | 2.27 | . 57 | . 57 | 2.27 | 3.41 | 2.84 | . 00 | 30.11 |
| (2) | . 25 | . 23 | . 02 | . 02 | . 00 | . 00 | . 02 | . 14 | . 02 | . 02 | . 09 | . 02 | . 02 | . 09 | . 14 | . 11 | . 00 | 1.20 |
| 4.1-5.0 | 2 | 0 | 1 | 0 | 0 | 0 | 2 | 5 | 0 | 0 | 1 | 1 | 1 | 2 | 7 | 2 | 0 | 24 |
| (1) | 1.14 | . 00 | . 57 | . 00 | . 00 | . 00 | 1.14 | 2.84 | . 00 | . 00 | . 57 | . 57 | . 57 | 1.14 | 3.98 | 1.14 | . 00 | 13.64 |
| (2) | . 05 | . 00 | . 02 | . 00 | . 00 | . 00 | . 05 | . 11 | . 00 | . 00 | . 02 | . 02 | . 02 | . 05 | . 16 | . 05 | . 00 | . 54 |
| 5.1-6.0 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 1 | 2 | 2 | 0 | 0 | 12 |
| (1) | . 57 | . 00 | 1.14 | . 00 | . 00 | . 00 | . 00 | 2.27 | . 00 | . 00 | . 00 | . 00 | . 57 | 1.14 | 1.14 | . 00 | . 00 | 6.82 |
| (2) | . 02 | . 00 | . 05 | . 00 | . 00 | . 00 | . 00 | . 09 | . 00 | . 00 | . 00 | . 00 | . 02 | . 05 | . 05 | . 00 | . 00 | . 27 |
| 6.1-8.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 4 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 57 | . 00 | . 00 | . 00 | . 00 | 1.14 | . 00 | . 57 | . 00 | . 00 | 2.27 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 02 | . 00 | . 00 | . 09 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 21 | 20 | 9 | 7 | 2 | 5 | 9 | 17 | 3 | 6 | 13 | 8 | 6 | 13 | 23 | 14 | 0 | 176 |
| (1) | 11.93 | 11.36 | 5.11 | 3.98 | 1.14 | 2.84 | 5.11 | 9.66 | 1.70 | 3.41 | 7.39 | 4.55 | 3.41 | 7.39 | 13.07 | 7.95 | . 00 | 100.00 |
| (2) | . 47 | . 45 | . 20 | . 16 | . 05 | . 11 | . 20 | . 38 | . 07 | . 14 | . 29 | . 18 | . 14 | . 29 | . 52 | . 32 | . 00 | 3.98 |

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD


Table 2.3-27—\{CCNPP 33 ft ( 10 m) October JFD (2000-2005) \} (Page 3 of 8)

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
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Table 2．3－27—\｛CCNPP 33 ft（10 m）October JFD（2000－2005）\}

CC OCTOBER MET DATA JOINT FREQUENCY DISTRIBUTION（60－METER TOWER


| CC OCTOBER MET DATA JOINT FREQUENCY DISTRIBUTION | $(60-M E T E R ~ T O W E R)$ |  |
| :--- | :---: | :---: | :---: |
| 33.0 FT WIND DATA | STABILITY CLASS E | CLASS FREQUENCY (PERCENT) $=20.20$ |


|  |  |  |  |  |  |  |  | IND DI | RECTI | N FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| (1) | . 11 | . 11 | . 00 | . 00 | . 11 | . 00 | . 00 | . 00 | . 11 | . 00 | . 11 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 56 |
| (2) | . 02 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 11 |
| .2- . 4 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 5 |
| (1) | . 00 | . 11 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 11 | . 11 | . 00 | . 11 | . 00 | . 00 | . 11 | . 00 | . 00 | . 56 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 11 |
| .5-1.0 | 3 | 1 | 7 | 0 | 7 | 5 | 3 | 0 | 3 | 1 | 6 | 6 | 4 | 2 | 3 | 2 | 0 | 53 |
| (1) | . 34 | . 11 | . 78 | . 00 | . 78 | . 56 | . 34 | . 00 | . 34 | . 11 | . 67 | . 67 | . 45 | . 22 | . 34 | . 22 | . 00 | 5.93 |
| (2) | . 07 | . 02 | . 16 | . 00 | . 16 | . 11 | . 07 | . 00 | . 07 | . 02 | . 14 | . 14 | . 09 | . 05 | . 07 | . 05 | . 00 | 1.20 |
| 1.1-1.5 | 6 | 3 | 4 | 6 | 3 | 6 | 3 | 6 | 10 | 11 | 8 | 1 | 5 | 9 | 12 | 3 | 0 | 96 |
| (1) | . 67 | . 34 | . 45 | . 67 | . 34 | . 67 | . 34 | . 67 | 1.12 | 1.23 | . 89 | . 11 | . 56 | 1.01 | 1.34 | . 34 | . 00 | 10.74 |
| (2) | . 14 | . 07 | . 09 | . 14 | . 07 | . 14 | . 07 | . 14 | . 23 | . 25 | . 18 | . 02 | . 11 | . 20 | . 27 | . 07 | . 00 | 2.17 |
| 1.6-2.0 | 7 | 5 | 2 | 7 | 17 | 11 | 8 | 9 | 15 | 11 | 13 | 6 | 9 | 16 | 19 | 13 | 0 | 168 |
| (1) | . 78 | . 56 | . 22 | . 78 | 1.90 | 1.23 | . 89 | 1.01 | 1.68 | 1.23 | 1.45 | . 67 | 1.01 | 1.79 | 2.13 | 1.45 | . 00 | 18.79 |
| (2) | . 16 | . 11 | . 05 | . 16 | . 38 | . 25 | . 18 | . 20 | . 34 | . 25 | . 29 | . 14 | . 20 | . 36 | . 43 | . 29 | . 00 | 3.80 |
| 2.1-3.0 | 11 | 12 | 11 | 13 | 16 | 9 | 3 | 22 | 35 | 30 | 58 | 15 | 23 | 24 | 41 | 13 | 0 | 336 |
| (1) | 1.23 | 1.34 | 1.23 | 1.45 | 1.79 | 1.01 | . 34 | 2.46 | 3.91 | 3.36 | 6.49 | 1.68 | 2.57 | 2.68 | 4.59 | 1.45 | . 00 | 37.58 |
| (2) | . 25 | . 27 | . 25 | . 29 | . 36 | . 20 | . 07 | . 50 | . 79 | . 68 | 1.31 | . 34 | . 52 | . 54 | . 93 | . 29 | . 00 | 7.59 |
| $3.1-4.0$ | 8 | 11 | 4 | 3 | 0 | 0 | 0 | 6 | 13 | 17 | 25 | 15 | 11 | 21 | 41 | 13 | 0 | 188 |
| (1) | . 89 | 1.23 | . 45 | . 34 | . 00 | . 00 | . 00 | . 67 | 1.45 | 1.90 | 2.80 | 1.68 | 1.23 | 2.35 | 4.59 | 1.45 | . 00 | 21.03 |
| (2) | . 18 | . 25 | . 09 | . 07 | . 00 | . 00 | . 00 | . 14 | . 29 | . 38 | . 56 | . 34 | . 25 | . 47 | . 93 | . 29 | . 00 | 4.25 |
| 4.1-5.0 | 5 | 1 | 2 | 0 | 0 | 0 | 0 | 1 | 1 | 10 | 4 | 1 | 0 | 3 | 3 | 4 | 0 | 35 |
| (1) | . 56 | . 11 | . 22 | . 00 | . 00 | . 00 | . 00 | . 11 | . 11 | 1.12 | . 45 | . 11 | . 00 | . 34 | . 34 | . 45 | . 00 | 3.91 |
| (2) | . 11 | . 02 | . 05 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 23 | . 09 | . 02 | . 00 | . 07 | . 07 | . 09 | . 00 | . 79 |
| 5.1-6.0 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 1 | 0 | 7 |
| (1) | . 22 | . 00 | . 11 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 11 | . 22 | . 00 | . 00 | . 00 | . 00 | . 11 | . 00 | . 78 |
| (2) | . 05 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 05 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 16 |
| 6.1-8.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 11 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 11 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | .00 | . 00 | . 00 | . 00 | .00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 43 | 35 | 31 | 29 | 44 | 31 | 17 | 45 | 79 | 82 | 117 | 45 | 52 | 75 | 120 | 49 | 0 | 894 |
| (1) | 4.81 | 3.91 | 3.47 | 3.24 | 4.92 | 3.47 | 1.90 | 5.03 | 8.84 | 9.17 | 13.09 | 5.03 | 5.82 | 8.39 | 13.42 | 5.48 | . 00 | 100.00 |
| (2) | . 97 | . 79 | . 70 | . 66 | . 99 | . 70 | . 38 | 1.02 | 1.78 | 1.85 | 2.64 | 1.02 | 1.17 | 1.69 | 2.71 | 1.11 | . 00 | 20.20 |

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

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Table 2.3-27—\{CCNPP 33 ft (10 m) October JFD (2000-2005)\} (Page 6 of 8)

CC OCTOBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)

(1) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

| CC OCTOBER MET DATA JOINT FREQUENCY DISTRIBUTION | $(60-M E T E R ~ T O W E R)$ |  |  |
| :--- | :---: | :---: | :---: |
| $33.0 ~ F T ~ W I N D ~ D A T A ~$ | STABILITY CLASS G | CLASS FREQUENCY | (PERCENT) $=14.26$ |


|  |  |  |  |  |  |  |  | D | +CIIO | N FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 5 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 16 | . 00 | . 00 | . 16 | . 16 | . 00 | . 32 | . 00 | . 00 | . 00 | . 00 | . 00 | . 79 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 02 | . 00 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 11 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 6 | 4 | 2 | 1 | 3 | 0 | 0 | 0 | 0 | 18 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 16 | . 16 | . 00 | . 00 | . 95 | . 63 | . 32 | . 16 | . 48 | . 00 | . 00 | . 00 | . 00 | 2.85 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 14 | . 09 | . 05 | . 02 | . 07 | . 00 | . 00 | . 00 | . 00 | . 41 |
| .5-1.0 | 4 | 0 | 1 | 0 | 1 | 2 | 2 | 2 | 9 | 15 | 25 | 32 | 19 | 14 | 2 | 0 | 0 | 128 |
| (1) | . 63 | . 00 | . 16 | . 00 | . 16 | . 32 | . 32 | . 32 | 1.43 | 2.38 | 3.96 | 5.07 | 3.01 | 2.22 | . 32 | . 00 | . 00 | 20.29 |
| (2) | . 09 | . 00 | . 02 | . 00 | . 02 | . 05 | . 05 | . 05 | . 20 | . 34 | . 56 | . 72 | . 43 | . 32 | . 05 | . 00 | . 00 | 2.89 |
| 1.1-1.5 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 1 | 19 | 59 | 72 | 33 | 23 | 21 | 2 | 0 | 0 | 233 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 48 | . 00 | . 16 | 3.01 | 9.35 | 11.41 | 5.23 | 3.65 | 3.33 | . 32 | . 00 | . 00 | 36.93 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 | . 00 | . 02 | . 43 | 1.33 | 1.63 | . 75 | . 52 | . 47 | . 05 | . 00 | . 00 | 5.26 |
| 1.6-2.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 23 | 25 | 55 | 25 | 13 | 28 | 4 | 2 | 0 | 176 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 16 | 3.65 | 3.96 | 8.72 | 3.96 | 2.06 | 4.44 | . 63 | . 32 | . 00 | 27.89 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 52 | . 56 | 1.24 | . 56 | . 29 | . 63 | . 09 | . 05 | . 00 | 3.98 |
| 2.1-3.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 4 | 20 | 11 | 9 | 18 | 6 | 1 | 0 | 71 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 16 | . 16 | . 63 | 3.17 | 1.74 | 1.43 | 2.85 | . 95 | . 16 | . 00 | 11.25 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 09 | . 45 | . 25 | . 20 | . 41 | . 14 | . 02 | . 00 | 1.60 |
| $3.1-4.0$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 4.1-5.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 5.1-6.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 6.1-8.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 4 | 0 | 1 | 0 | 2 | 7 | 2 | 5 | 59 | 108 | 174 | 104 | 67 | 81 | 14 | 3 | 0 | 631 |
| (1) | . 63 | . 00 | . 16 | . 00 | . 32 | 1.11 | . 32 | . 79 | 9.35 | 17.12 | 27.58 | 16.48 | 10.62 | 12.84 | 2.22 | . 48 | . 00 | 100.00 |
| (2) | . 09 | . 00 | . 02 | . 00 | . 05 | . 16 | . 05 | . 11 | 1.33 | 2.44 | 3.93 | 2.35 | 1.51 | 1.83 | . 32 | . 07 | . 00 | 14.26 |

## 

Table 2.3-27—\{CCNPP 33 ft (10 m) October JFD (2000-2005)\} (Page 8 of 8)
CC OCTOBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)

ग्0
$\stackrel{0}{2}$
$i$

CC NOVEMBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
33.0 FT WIND DATA STABILITY CLASS A CLASS FREQUENCY (PERCENT) = 13.17

(1) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

| CC NOVEMBER MET DATA JOINT | FREQUENCY DISTRIBUTION | (60-METER TOWER) |  |
| :--- | :--- | :--- | :--- | :--- |
| 33.0 FT WIND DATA | STABILITY CLASS B | CLASS FREQUENCY | (PERCENT) $=3.59$ |


|  |  |  |  |  |  |  |  | ND | CT | FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 65 | . 00 | . 00 | . 00 | . 00 | . 00 | . 65 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 1.1-1.5 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 3 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 65 | . 65 | . 00 | . 00 | . 00 | . 65 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.94 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 |
| 1.6-2.0 | 1 | 0 | 2 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 9 |
| (1) | . 65 | . 00 | 1.29 | . 00 | . 65 | . 65 | . 00 | . 00 | . 00 | . 00 | 1.29 | 1.29 | . 00 | . 00 | . 00 | . 00 | . 00 | 5.81 |
| (2) | . 02 | . 00 | . 05 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 05 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 21 |
| 2.1-3.0 | 2 | 4 | 2 | 1 | 2 | 4 | 1 | 3 | 0 | 3 | 5 | 6 | 2 | 3 | 2 | 0 | 0 | 40 |
| (1) | 1.29 | 2.58 | 1.29 | . 65 | 1.29 | 2.58 | . 65 | 1.94 | . 00 | 1.94 | 3.23 | 3.87 | 1.29 | 1.94 | 1.29 | . 00 | . 00 | 25.81 |
| (2) | . 05 | . 09 | . 05 | . 02 | . 05 | . 09 | . 02 | . 07 | . 00 | . 07 | . 12 | . 14 | . 05 | . 07 | . 05 | . 00 | . 00 | . 93 |
| 3.1-4.0 | 4 | 5 | 0 | 0 | 1 | 0 | 1 | 5 | 1 | 4 | 6 | 3 | 1 | 2 | 2 | 1 | 0 | 36 |
| (1) | 2.58 | 3.23 | . 00 | . 00 | . 65 | . 00 | . 65 | 3.23 | . 65 | 2.58 | 3.87 | 1.94 | . 65 | 1.29 | 1.29 | . 65 | . 00 | 23.23 |
| (2) | . 09 | . 12 | . 00 | . 00 | . 02 | . 00 | . 02 | . 12 | . 02 | . 09 | . 14 | . 07 | . 02 | . 05 | . 05 | . 02 | . 00 | . 83 |
| 4.1-5.0 | 3 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 1 | 3 | 5 | 5 | 3 | 4 | 0 | 33 |
| (1) | 1.94 | 2.58 | . 65 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 2.58 | . 65 | 1.94 | 3.23 | 3.23 | 1.94 | 2.58 | . 00 | 21.29 |
| (2) | . 07 | . 09 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 09 | . 02 | . 07 | . 12 | . 12 | . 07 | . 09 | . 00 | . 76 |
| 5.1-6.0 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 4 | 5 | 4 | 0 | 20 |
| (1) | 1.94 | . 65 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.29 | . 00 | . 65 | 2.58 | 3.23 | 2.58 | . 00 | 12.90 |
| (2) | . 07 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 02 | . 09 | . 12 | . 09 | . 00 | . 46 |
| 6.1-8.0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 3 | 4 | 0 | 0 | 11 |
| (1) | 1.29 | . 65 | . 00 | . 00 | . 00 | . 00 | . 00 | . 65 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.94 | 2.58 | . 00 | . 00 | 7.10 |
| (2) | . 05 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 | . 09 | . 00 | . 00 | . 25 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 65 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 65 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| 10.1-89.5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 65 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 65 |
| (2) | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| ALL SPEEDS | 16 | 15 | 5 | 1 | 4 | 5 | 3 | 11 | 1 | 11 | 16 | 16 | 9 | 17 | 16 | 9 | 0 | 155 |
| (1) | 10.32 | 9.68 | 3.23 | . 65 | 2.58 | 3.23 | 1.94 | 7.10 | . 65 | 7.10 | 10.32 | 10.32 | 5.81 | 10.97 | 10.32 | 5.81 | . 00 | 100.00 |
| (2) | . 37 | . 35 | . 12 | . 02 | . 09 | . 12 | . 07 | . 25 | . 02 | . 25 | . 37 | . 37 | . 21 | . 39 | . 37 | . 21 | . 00 | 3.59 |



CC NOVEMBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)

| 33.0 FT | WIND | DATA |  | STABILITY CLASS C |  |  |  | WIND D | CLASS | FREQU $N$ FROM | ENCY | (PERCENT) |  | 3.68 | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW |  |  |  |  |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 6 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 63 | . 00 | . 00 | . 63 | 1.26 | . 00 | . 00 | . 00 | . 63 | . 00 | . 63 | . 00 | . 00 | 3.77 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 05 | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 14 |
| 1.1-1.5 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| (1) | . 00 | . 63 | . 00 | . 00 | . 63 | . 00 | . 00 | . 63 | . 00 | . 63 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 2.52 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 09 |
| 1.6-2.0 | 0 | 1 | 1 | 1 | 1 | 2 | 2 | 0 | 0 | 2 | 1 | 2 | 0 | 0 | 1 | 0 | 0 | 14 |
| (1) | . 00 | . 63 | . 63 | . 63 | . 63 | 1.26 | 1.26 | . 00 | . 00 | 1.26 | . 63 | 1.26 | . 00 | . 00 | . 63 | . 00 | . 00 | 8.81 |
| (2) | . 00 | . 02 | . 02 | . 02 | . 02 | . 05 | . 05 | . 00 | . 00 | . 05 | . 02 | . 05 | . 00 | . 00 | . 02 | . 00 | . 00 | . 32 |
| 2.1-3.0 | 3 | 4 | 5 | 4 | 2 | 4 | 2 | 6 | 1 | 5 | 8 | 4 | 1 | 0 | 3 | 1 | 0 | 53 |
| (1) | 1.89 | 2.52 | 3.14 | 2.52 | 1.26 | 2.52 | 1.26 | 3.77 | . 63 | 3.14 | 5.03 | 2.52 | . 63 | . 00 | 1.89 | . 63 | . 00 | 33.33 |
| (2) | . 07 | . 09 | . 12 | . 09 | . 05 | . 09 | . 05 | . 14 | . 02 | . 12 | . 19 | . 09 | . 02 | . 00 | . 07 | . 02 | . 00 | 1.23 |
| 3.1-4.0 | 2 | 2 | 0 | 0 | 0 | 0 | 1 | 6 | 1 | 0 | 3 | 4 | 2 | 4 | 1 | 1 | 0 | 27 |
| (1) | 1.26 | 1.26 | . 00 | . 00 | . 00 | . 00 | . 63 | 3.77 | . 63 | . 00 | 1.89 | 2.52 | 1.26 | 2.52 | . 63 | . 63 | . 00 | 16.98 |
| (2) | . 05 | . 05 | . 00 | . 00 | . 00 | . 00 | . 02 | . 14 | . 02 | . 00 | . 07 | . 09 | . 05 | . 09 | . 02 | . 02 | . 00 | . 62 |
| 4.1-5.0 | 3 | 4 | 0 | 0 | 0 | 0 | 2 | 1 | 2 | 2 | 0 | 1 | 1 | 2 | 1 | 0 | 0 | 19 |
| (1) | 1.89 | 2.52 | . 00 | . 00 | . 00 | . 00 | 1.26 | . 63 | 1.26 | 1.26 | . 00 | . 63 | . 63 | 1.26 | . 63 | . 00 | . 00 | 11.95 |
| (2) | . 07 | . 09 | . 00 | . 00 | . 00 | . 00 | . 05 | . 02 | . 05 | . 05 | . 00 | . 02 | . 02 | . 05 | . 02 | . 00 | . 00 | . 44 |
| 5.1-6.0 |  | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 1 | 4 | 0 | 15 |
| (1) | . 63 | 1.89 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 63 | 1.26 | . 00 | . 00 | . 63 | 1.26 | . 63 | 2.52 | . 00 | 9.43 |
| (2) | . 02 | . 07 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 05 | . 00 | . 00 | . 02 | . 05 | . 02 | . 09 | . 00 | . 35 |
| 6.1-8.0 | 5 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 2 | 5 | 3 | 1 | 0 | 19 |
| (1) | 3.14 | 1.26 | . 00 | . 00 | . 00 | . 00 | . 00 | . 63 | . 00 | . 00 | . 00 | . 00 | 1.26 | 3.14 | 1.89 | . 63 | . 00 | 11.95 |
| (2) | . 12 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 05 | . 12 | . 07 | . 02 | . 00 | . 44 |
| 8.1-10.0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 2 |
| (1) | . 63 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 63 | . 00 | . 00 | . 00 | 1.26 |
| (2) | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 05 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 15 | 17 | 6 | 5 | 5 | 6 | 7 | 16 | 7 | 12 | 12 | 11 | 8 | 14 | 11 | 7 | 0 | 159 |
| (1) | 9.43 | 10.69 | 3.77 | 3.14 | 3.14 | 3.77 | 4.40 | 10.06 | 4.40 | 7.55 | 7.55 | 6.92 | 5.03 | 8.81 | 6.92 | 4.40 | . 00 | 100.00 |
| (2) | . 35 | . 39 | . 14 | . 12 | . 12 | . 14 | . 16 | . 37 | . 16 | . 28 | . 28 | . 25 | . 19 | . 32 | . 25 | . 16 | . 00 | 3.68 |

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

CC NOVEMBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)


## OヨIכヨIOपd IHפוyגdO)

Table 2.3-28—\{CCNPP 33 ft ( 10 m) November JFD (2000-2005)\} (Page 5 of 8)
CC NOVEMBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)

| 33.0 FT | WIND D |  |  | STABI | LITY C | CLASS E |  | vIND D | CLAS <br> RECTI | S FREQU ON FROM | $\begin{aligned} & \text { UENCY } \\ & M \end{aligned}$ | PERCEN |  | 28.56 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { SPEED } \\ & \text { mps } \end{aligned}$ | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 08 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 08 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 0 | 1 | 1 | 2 | 1 | 0 | 0 | 9 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 08 | . 08 | . 16 | . 00 | . 08 | . 08 | . 16 | . 08 | . 00 | . 00 | . 73 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 05 | . 00 | . 02 | . 02 | . 05 | . 02 | . 00 | . 00 | . 21 |
| . $5-1.0$ | 5 | 4 | 0 | 6 | 7 | 7 | 5 | 10 | 7 | 6 | 10 | 10 | 3 | 3 | 4 | 5 | 0 | 92 |
| (1) | . 41 | . 32 | . 00 | . 49 | . 57 | . 57 | . 41 | . 81 | . 57 | . 49 | . 81 | . 81 | . 24 | . 24 | . 32 | . 41 | . 00 | 7.46 |
| (2) | . 12 | . 09 | . 00 | . 14 | . 16 | . 16 | . 12 | . 23 | . 16 | . 14 | . 23 | . 23 | . 07 | . 07 | . 09 | . 12 | . 00 | 2.13 |
| 1.1-1.5 | 5 | 8 | 13 | 12 | 8 | 10 | 2 | 10 | 18 | 20 | 17 | 9 | 9 | 11 | 5 | 8 | 0 | 165 |
| (1) | . 41 | . 65 | 1.05 | . 97 | . 65 | . 81 | . 16 | . 81 | 1.46 | 1.62 | 1.38 | . 73 | . 73 | . 89 | . 41 | . 65 | . 00 | 13.37 |
| (2) | . 12 | . 19 | . 30 | . 28 | . 19 | . 23 | . 05 | . 23 | . 42 | . 46 | . 39 | . 21 | . 21 | . 25 | . 12 | . 19 | . 00 | 3.82 |
| 1.6-2.0 | 8 | 6 | 6 | 6 | 13 | 2 | 11 | 11 | 13 | 22 | 19 | 13 | 11 | 12 | 26 | 11 | 0 | 190 |
| (1) | . 65 | . 49 | . 49 | . 49 | 1.05 | . 16 | . 89 | . 89 | 1.05 | 1.78 | 1.54 | 1.05 | . 89 | . 97 | 2.11 | . 89 | . 00 | 15.40 |
| (2) | . 19 | . 14 | . 14 | . 14 | . 30 | . 05 | . 25 | . 25 | . 30 | . 51 | . 44 | . 30 | . 25 | . 28 | . 60 | . 25 | . 00 | 4.40 |
| 2.1-3.0 | 9 | 8 | 6 | 5 | 6 | 7 | 3 | 7 | 36 | 69 | 59 | 34 | 17 | 22 | 70 | 34 | 0 | 392 |
| (1) | . 73 | . 65 | . 49 | . 41 | . 49 | . 57 | . 24 | . 57 | 2.92 | 5.59 | 4.78 | 2.76 | 1.38 | 1.78 | 5.67 | 2.76 | . 00 | 31.77 |
| (2) | . 21 | . 19 | . 14 | . 12 | . 14 | . 16 | . 07 | . 16 | . 83 | 1.60 | 1.37 | . 79 | . 39 | . 51 | 1.62 | . 79 | . 00 | 9.07 |
| 3.1-4.0 | 8 | 4 | 1 | 1 | 3 | 0 | 1 | 12 | 28 | 30 | 68 | 13 | 15 | 15 | 42 | 17 | 0 | 258 |
| (1) | . 65 | . 32 | . 08 | . 08 | . 24 | . 00 | . 08 | . 97 | 2.27 | 2.43 | 5.51 | 1.05 | 1.22 | 1.22 | 3.40 | 1.38 | . 00 | 20.91 |
| (2) | . 19 | . 09 | . 02 | . 02 | . 07 | . 00 | . 02 | . 28 | . 65 | . 69 | 1.57 | . 30 | . 35 | . 35 | . 97 | . 39 | . 00 | 5.97 |
| 4.1-5.0 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 4 | 12 | 10 | 30 | 1 | 3 | 6 | 13 | 10 | 0 | 92 |
| (1) | . 16 | . 00 | . 00 | . 00 | . 08 | . 00 | . 00 | . 32 | . 97 | . 81 | 2.43 | . 08 | . 24 | . 49 | 1.05 | . 81 | . 00 | 7.46 |
| (2) | . 05 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 09 | . 28 | . 23 | . 69 | . 02 | . 07 | . 14 | . 30 | . 23 | . 00 | 2.13 |
| 5.1-6.0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 1 | 6 | 3 | 4 | 4 | 5 | 1 | 0 | 30 |
| (1) | . 08 | . 08 | . 00 | . 00 | . 00 | . 00 | . 00 | . 32 | . 00 | . 08 | . 49 | . 24 | . 32 | . 32 | . 41 | . 08 | . 00 | 2.43 |
| (2) | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 09 | . 00 | . 02 | . 14 | . 07 | . 09 | . 09 | . 12 | . 02 | . 00 | . 69 |
| 6.1-8.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 3 | 0 | 0 | 0 | 5 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 08 | . 00 | . 00 | . 08 | . 00 | . 00 | . 24 | . 00 | . 00 | . 00 | . 41 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 07 | . 00 | . 00 | . 00 | . 12 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 38 | 31 | 26 | 30 | 38 | 26 | 22 | 61 | 115 | 160 | 210 | 84 | 63 | 78 | 166 | 86 | 0 | 1234 |
| (1) | 3.08 | 2.51 | 2.11 | 2.43 | 3.08 | 2.11 | 1.78 | 4.94 | 9.32 | 12.97 | 17.02 | 6.81 | 5.11 | 6.32 | 13.45 | 6.97 | . 00 | 100.00 |
| (2) | . 88 | . 72 | . 60 | . 69 | . 88 | . 60 | . 51 | 1.41 | 2.66 | 3.70 | 4.86 | 1.94 | 1.46 | 1.81 | 3.84 | 1.99 | . 00 | 28.56 |

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## Table 2.3-28—\{CCNPP 33 ft (10 m) November JFD (2000-2005)\}

 (Page 6 of 8)CC NOVEMBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)


| CC NOVEMBER MET DATA JOINT | FREQUENCY DISTRIBUTION | $(60$-METER TOWER) |  |
| :--- | :--- | :--- | :--- |
| 33.0 FT WIND DATA | STABILITY CLASS G | CLASS FREQUENCY | (PERCENT) $=9.03$ |


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Table 2．3－28—\｛CCNPP 33 ft（ 10 m）November JFD（2000－2005）\} （Page 8 of 8）
CC NOVEMBER MET DATA JOINT FREQUENCY DISTRIBUTION（60－METER TOWER）

| 33．0 FT WIND DATA |  |  | StAbILITY CLASS ALL |  |  |  |  |  | CLASS FREQUENCY（PERCENT）$=100.00$ |  |  |  |  |  | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | WIND DIRECTION FROM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW |  |  |  |  |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT ． 2 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 4 | 0 | 1 | 5 | 1 | 1 | 1 | 1 | 0 | 20 |
| （1） | ． 00 | ． 00 | ． 02 | ． 05 | ． 00 | ． 00 | ． 02 | ． 05 | ． 09 | ． 00 | ． 02 | ． 12 | ． 02 | ． 02 | ． 02 | ． 02 | ． 00 | ． 46 |
| （2） | ． 00 | ． 00 | ． 02 | ． 05 | ． 00 | ． 00 | ． 02 | ． 05 | ． 09 | ． 00 | ． 02 | ． 12 | ． 02 | ． 02 | ． 02 | ． 02 | ． 00 | ． 46 |
| ． $2-.4$ | 0 | 0 | 0 | 1 | 0 | 5 | 0 | 2 | 3 | 10 | 3 | 3 | 2 | 3 | 1 | 0 | 0 | 33 |
| （1） | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 12 | ． 00 | ． 05 | ． 07 | ． 23 | ． 07 | ． 07 | ． 05 | ． 07 | ． 02 | ． 00 | ． 00 | ． 76 |
| （2） | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 12 | ． 00 | ． 05 | ． 07 | ． 23 | ． 07 | ． 07 | ． 05 | ． 07 | ． 02 | ． 00 | ． 00 | ． 76 |
| ．5－1．0 | 13 | 10 | 8 | 10 | 9 | 13 | 6 | 20 | 24 | 31 | 48 | 33 | 20 | 23 | 8 | 5 | 0 | 281 |
| （1） | ． 30 | ． 23 | ． 19 | ． 23 | ． 21 | ． 30 | ． 14 | ． 46 | ． 56 | ． 72 | 1.11 | ． 76 | ． 46 | ． 53 | ． 19 | ． 12 | ． 00 | 6.50 |
| （2） | ． 30 | ． 23 | ． 19 | ． 23 | ． 21 | ． 30 | ． 14 | ． 46 | ． 56 | ． 72 | 1.11 | ． 76 | ． 46 | ． 53 | ． 19 | ． 12 | ． 00 | 6.50 |
| 1．1－1．5 | 11 | 15 | 23 | 20 | 24 | 18 | 15 | 30 | 55 | 79 | 70 | 49 | 25 | 24 | 14 | 16 | 0 | 488 |
| （1） | ． 25 | ． 35 | ． 53 | ． 46 | ． 56 | ． 42 | ． 35 | ． 69 | 1.27 | 1.83 | 1.62 | 1.13 | ． 58 | ． 56 | ． 32 | ． 37 | ． 00 | 11.30 |
| （2） | ． 25 | ． 35 | ． 53 | ． 46 | ． 56 | ． 42 | ． 35 | ． 69 | 1.27 | 1.83 | 1.62 | 1.13 | ． 58 | ． 56 | ． 32 | ． 37 | ． 00 | 11.30 |
| 1．6－2．0 | 18 | 28 | 18 | 23 | 24 | 19 | 32 | 33 | 63 | 104 | 84 | 43 | 37 | 44 | 48 | 17 | 0 | 635 |
| （1） | ． 42 | ． 65 | ． 42 | ． 53 | ． 56 | ． 44 | ． 74 | ． 76 | 1.46 | 2.41 | 1.94 | 1.00 | ． 86 | 1.02 | 1.11 | ． 39 | ． 00 | 14.70 |
| （2） | ． 42 | ． 65 | ． 42 | ． 53 | ． 56 | ． 44 | ． 74 | ． 76 | 1.46 | 2.41 | 1.94 | 1.00 | ． 86 | 1.02 | 1.11 | ． 39 | ． 00 | 14.70 |
| 2．1－3．0 | 37 | 46 | 31 | 38 | 44 | 42 | 47 | 55 | 81 | 143 | 173 | 86 | 45 | 60 | 130 | 51 | 0 | 1109 |
| （1） | ． 86 | 1.06 | ． 72 | ． 88 | 1.02 | ． 97 | 1.09 | 1.27 | 1.88 | 3.31 | 4.00 | 1.99 | 1.04 | 1.39 | 3.01 | 1.18 | ． 00 | 25.67 |
| （2） | ． 86 | 1.06 | ． 72 | ． 88 | 1.02 | ． 97 | 1.09 | 1.27 | 1.88 | 3.31 | 4.00 | 1.99 | 1.04 | 1.39 | 3.01 | 1.18 | ． 00 | 25.67 |
| 3．1－4．0 | 58 | 41 | 16 | 13 | 15 | 9 | 22 | 73 | 58 | 70 | 151 | 47 | 33 | 41 | 76 | 65 | 0 | 788 |
| （1） | 1.34 | ． 95 | ． 37 | ． 30 | ． 35 | ． 21 | ． 51 | 1.69 | 1.34 | 1.62 | 3.50 | 1.09 | ． 76 | ． 95 | 1.76 | 1.50 | ． 00 | 18.24 |
| （2） | 1.34 | ． 95 | ． 37 | ． 30 | ． 35 | ． 21 | ． 51 | 1.69 | 1.34 | 1.62 | 3.50 | 1.09 | ． 76 | ． 95 | 1.76 | 1.50 | ． 00 | 18.24 |
| 4．1－5．0 | 55 | 26 | 18 | 3 | 2 | 4 | 7 | 41 | 36 | 40 | 86 | 18 | 22 | 44 | 63 | 63 | 0 | 528 |
| （1） | 1.27 | ． 60 | ． 42 | ． 07 | ． 05 | ． 09 | ． 16 | ． 95 | ． 83 | ． 93 | 1.99 | ． 42 | ． 51 | 1.02 | 1.46 | 1.46 | ． 00 | 12.22 |
| （2） | 1.27 | ． 60 | ． 42 | ． 07 | ． 05 | ． 09 | ． 16 | ． 95 | ． 83 | ． 93 | 1.99 | ． 42 | ． 51 | 1.02 | 1.46 | 1.46 | ． 00 | 12.22 |
| 5．1－6．0 | 27 | 20 | 12 | 1 | 0 | 0 | 0 | 29 | 7 | 14 | 20 | 7 | 16 | 51 | 37 | 32 | 0 | 273 |
| （1） | ． 63 | ． 46 | ． 28 | ． 02 | ． 00 | ． 00 | ． 00 | ． 67 | ． 16 | ． 32 | ． 46 | ． 16 | ． 37 | 1.18 | ． 86 | ． 74 | ． 00 | 6.32 |
| （2） | ． 63 | ． 46 | ． 28 | ． 02 | ． 00 | ． 00 | ． 00 | ． 67 | ． 16 | ． 32 | ． 46 | ． 16 | ． 37 | 1.18 | ． 86 | ． 74 | ． 00 | 6.32 |
| 6．1－8．0 | 25 | 11 | 2 | 0 | 0 | 0 | 0 | 12 | 4 | 0 | 1 | 2 | 4 | 44 | 29 | 10 | 0 | 144 |
| （1） | ． 58 | ． 25 | ． 05 | ． 00 | ． 00 | ． 00 | ． 00 | ． 28 | ． 09 | ． 00 | ． 02 | ． 05 | ． 09 | 1.02 | ． 67 | ． 23 | ． 00 | 3.33 |
| （2） | ． 58 | ． 25 | ． 05 | ． 00 | ． 00 | ． 00 | ． 00 | ． 28 | ． 09 | ． 00 | ． 02 | ． 05 | ． 09 | 1.02 | ． 67 | ． 23 | ． 00 | 3.33 |
| 8．1－10．0 | 6 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 7 | 1 | 0 | 0 | 19 |
| （1） | ． 14 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 05 | ． 00 | ． 00 | ． 00 | ． 00 | ． 05 | ． 16 | ． 02 | ． 00 | ． 00 | ． 44 |
| （2） | ． 14 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 05 | ． 00 | ． 00 | ． 00 | ． 00 | ． 05 | ． 16 | ． 02 | ． 00 | ． 00 | ． 44 |
| 10．1－89．5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 2 |
| （1） | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 05 |
| （2） | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 05 |
| LL SPEEDS | 251 | 198 | 129 | 111 | 118 | 110 | 130 | 299 | 335 | 491 | 637 | 293 | 208 | 342 | 408 | 260 | 0 | 4320 |
| （1） | 5.81 | 4.58 | 2.99 | 2.57 | 2.73 | 2.55 | 3.01 | 6.92 | 7.75 | 11.37 | 14.75 | 6.78 | 4.81 | 7.92 | 9.44 | 6.02 | ． 00 | 100.00 |
| （2） | 5.81 | 4.58 | 2.99 | 2.57 | 2.73 | 2.55 | 3.01 | 6.92 | 7.75 | 11.37 | 14.75 | 6.78 | 4.81 | 7.92 | 9.44 | 6.02 | ． 00 | 100.00 |

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Table 2.3-29—\{CCNPP $33 \mathrm{ft}(10 \mathrm{~m})$ December JFD (2000-2005)\}

## (Page 1 of 8)

CC DECEMBER MET DATA JOINT FREQUENCY DISTRIBUTIO
33.0 FT WIND DATA
STABILITY CLASS A

CLASS FREQUENCY (PERCENT) $=8.36$

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
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| CC DECEMBER MET DATA JOINT | FREQUENCY DISTRIBUTION | $(60$-METER TOWER) |
| :--- | :--- | :---: | :---: | :---: |
| 33.0 FT WIND DATA | STABILITY CLASS B | CLASS FREQUENCY (PERCENT) $=4.22$ |


| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 1.1-1.5 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 55 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 55 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| 1.6-2.0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 2 | 0 | 0 | 7 |
| (1) | . 00 | . 00 | . 55 | . 55 | . 00 | . 00 | . 00 | . 00 | . 00 | . 55 | . 00 | . 55 | . 55 | . 00 | 1.10 | . 00 | . 00 | 3.85 |
| (2) | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 02 | . 00 | . 05 | . 00 | . 00 | . 16 |
| 2.1-3.0 | 3 | 8 | 3 | 1 | 2 | 0 | 1 | 1 | 1 | 2 | 2 | 3 | 4 | 2 | 1 | 3 | 0 | 37 |
| (1) | 1.65 | 4.40 | 1.65 | . 55 | 1.10 | . 00 | . 55 | . 55 | . 55 | 1.10 | 1.10 | 1.65 | 2.20 | 1.10 | . 55 | 1.65 | . 00 | 20.33 |
| (2) | . 07 | . 19 | . 07 | . 02 | . 05 | . 00 | . 02 | . 02 | . 02 | . 05 | . 05 | . 07 | . 09 | . 05 | . 02 | . 07 | . 00 | . 86 |
| 3.1-4.0 | 5 | 6 | 2 | 0 | 0 | 0 | 0 | 1 | 1 | 6 | 10 | 4 | 3 | 5 | 6 | 3 | 0 | 52 |
| (1) | 2.75 | 3.30 | 1.10 | . 00 | . 00 | . 00 | . 00 | . 55 | . 55 | 3.30 | 5.49 | 2.20 | 1.65 | 2.75 | 3.30 | 1.65 | . 00 | 28.57 |
| (2) | . 12 | . 14 | . 05 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 14 | . 23 | . 09 | . 07 | . 12 | . 14 | . 07 | . 00 | 1.21 |
| 4.1-5.0 | 9 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 4 | 3 | 4 | 3 | 11 | 1 | 0 | 42 |
| (1) | 4.95 | 2.20 | . 55 | . 00 | . 00 | . 00 | . 00 | . 00 | . 55 | . 55 | 2.20 | 1.65 | 2.20 | 1.65 | 6.04 | . 55 | . 00 | 23.08 |
| (2) | . 21 | . 09 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 09 | . 07 | . 09 | . 07 | . 26 | . 02 | . 00 | . 97 |
| 5.1-6.0 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 1 | 8 | 5 | 3 | 0 | 23 |
| (1) | 1.10 | . 00 | . 55 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 55 | 1.10 | . 00 | . 55 | 4.40 | 2.75 | 1.65 | . 00 | 12.64 |
| (2) | . 05 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 05 | . 00 | . 02 | . 19 | . 12 | . 07 | . 00 | . 53 |
| 6.1-8.0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 3 | 9 | 1 | 0 | 17 |
| (1) | . 55 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 55 | . 00 | . 00 | . 55 | . 55 | 1.65 | 4.95 | . 55 | . 00 | 9.34 |
| (2) | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 02 | . 07 | . 21 | . 02 | . 00 | . 39 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.65 | . 00 | . 00 | 1.65 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 | . 00 | . 00 | . 07 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 20 | 19 | 8 | 2 | 2 | 0 | 1 | 2 | 4 | 11 | 18 | 12 | 14 | 21 | 37 | 11 | 0 | 182 |
| (1) | 10.99 | 10.44 | 4.40 | 1.10 | 1.10 | . 00 | . 55 | 1.10 | 2.20 | 6.04 | 9.89 | 6.59 | 7.69 | 11.54 | 20.33 | 6.04 | . 00 | 100.00 |
| (2) | . 46 | . 44 | . 19 | . 05 | . 05 | . 00 | . 02 | . 05 | . 09 | . 26 | . 42 | . 28 | . 32 | . 49 | . 86 | . 26 | . 00 | 4.22 |
| (1) = PERCENT | OF ALL | GOOD | OBSERV | TIONS | FOR | S PA |  |  |  |  |  |  |  |  |  |  |  |  |


| CC DECEMBER MET DATA JOINT FREQUENCY DISTRIBUTION | $(60$-METER TOWER) |  |  |
| :--- | :--- | :---: | :---: | :---: |
| 33.0 FT WIND DATA | STABILITY CLASS C | CLASS FREQUENCY | (PERCENT) $=4.36$ |


|  |  |  |  |  |  |  |  | D | ECTI | FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 53 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 53 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| 1.1-1.5 | 0 | 2 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 5 |
| (1) | . 00 | 1.06 | . 53 | . 00 | . 53 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 53 | . 00 | . 00 | . 00 | . 00 | . 00 | 2.66 |
| (2) | . 00 | . 05 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 12 |
| 1.6-2.0 | 0 | 1 | 0 | 1 | 2 | 1 | 1 | 0 | 1 | 0 | 1 | 1 | 2 | 3 | 1 | 1 | 0 | 16 |
| (1) | . 00 | . 53 | . 00 | . 53 | 1.06 | . 53 | . 53 | . 00 | . 53 | . 00 | . 53 | . 53 | 1.06 | 1.60 | . 53 | . 53 | . 00 | 8.51 |
| (2) | . 00 | . 02 | . 00 | . 02 | . 05 | . 02 | . 02 | . 00 | . 02 | . 00 | . 02 | . 02 | . 05 | . 07 | . 02 | . 02 | . 00 | . 37 |
| 2.1-3.0 | 5 | 3 | 4 | 1 | 2 | 2 | 0 | 0 | 2 | 3 | 2 | 2 | 5 | 3 | 2 | 2 | 0 | 38 |
| (1) | 2.66 | 1.60 | 2.13 | . 53 | 1.06 | 1.06 | . 00 | . 00 | 1.06 | 1.60 | 1.06 | 1.06 | 2.66 | 1.60 | 1.06 | 1.06 | . 00 | 20.21 |
| (2) | . 12 | . 07 | . 09 | . 02 | . 05 | . 05 | . 00 | . 00 | . 05 | . 07 | . 05 | . 05 | . 12 | . 07 | . 05 | . 05 | . 00 | . 88 |
| 3.1-4.0 | 8 | 4 | 1 | 1 | 0 | 0 | 1 | 3 | 6 | 4 | 10 | 5 | 4 | 5 | 6 | 4 | 0 | 62 |
| (1) | 4.26 | 2.13 | . 53 | . 53 | . 00 | . 00 | . 53 | 1.60 | 3.19 | 2.13 | 5.32 | 2.66 | 2.13 | 2.66 | 3.19 | 2.13 | . 00 | 32.98 |
| (2) | . 19 | . 09 | . 02 | . 02 | . 00 | . 00 | . 02 | . 07 | . 14 | . 09 | . 23 | . 12 | . 09 | . 12 | . 14 | . 09 | . 00 | 1.44 |
| 4.1-5.0 | 2 | 2 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 3 | 4 | 5 | 7 | 2 | 0 | 32 |
| (1) | 1.06 | 1.06 | 1.06 | . 53 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 2.13 | 1.60 | 2.13 | 2.66 | 3.72 | 1.06 | . 00 | 17.02 |
| (2) | . 05 | . 05 | . 05 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 09 | . 07 | . 09 | . 12 | . 16 | . 05 | . 00 | . 74 |
| 5.1-6.0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 1 | 4 | 6 | 2 | 0 | 18 |
| (1) | . 53 | . 53 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.06 | . 53 | . 53 | 2.13 | 3.19 | 1.06 | . 00 | 9.57 |
| (2) | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 02 | . 02 | . 09 | . 14 | . 05 | . 00 | . 42 |
| 6.1-8.0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 5 | 4 | 2 | 0 | 13 |
| (1) | . 53 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 53 | . 00 | . 00 | 2.66 | 2.13 | 1.06 | . 00 | 6.91 |
| (2) | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 12 | . 09 | . 05 | . 00 | . 30 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 3 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 53 | 1.06 | . 00 | . 00 | 1.60 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 05 | . 00 | . 00 | . 07 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 17 | 13 | 8 | 4 | 5 | 3 | 3 | 3 | 9 | 7 | 20 | 13 | 16 | 26 | 28 | 13 | 0 | 188 |
| (1) | 9.04 | 6.91 | 4.26 | 2.13 | 2.66 | 1.60 | 1.60 | 1.60 | 4.79 | 3.72 | 10.64 | 6.91 | 8.51 | 13.83 | 14.89 | 6.91 | .00 | 100.00 |
| (2) | . 39 | . 30 | . 19 | . 09 | . 12 | . 07 | . 07 | . 07 | . 21 | . 16 | . 46 | . 30 | . 37 | . 60 | . 65 | . 30 | . 00 | 4.36 |

Oヨ८כヨノOYd $\perp$ HפוyגdOכ

CC DECEMBER MET DA
33．0 FT WIND DATA
Table 2．3－29—\｛CCNPP 33 ft（10 m）December JFD（2000－2005）\} （Page 4 of 8）

| 33．0 FT WIND DATA |  |  |  | STABILITY CLASS D |  |  | CLASS FREQU |  |  |  |  | PERCENT） |  | 35.54 |  | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW |  |  |  |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 3 |
|  | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 07 | ． 07 | ． 00 | ． 00 | ． 07 | ． 00 | ． 00 | ． 00 | ． 20 |
|  | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 02 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 07 |
| $\begin{array}{rr}.2- & .4 \\ (1) \\ & (2)\end{array}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
|  | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 07 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 07 |
|  | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 |
| ．5－1．0 | 2 | 7 | 3 | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 2 | 2 | 3 | 0 | 1 | 2 | 0 | 28 |
| （1） | ． 13 | ． 46 | ． 20 | ． 07 | ． 13 | ． 00 | ． 00 | ． 07 | ． 13 | ． 00 | ． 13 | ． 13 | ． 20 | ． 00 | ． 07 | ． 13 | ． 00 | 1.83 |
| 1．1－ 1.5 | ． 05 | ． 16 | ． 07 | ． 02 | ． 05 | ． 00 | ． 00 | ． 02 | ． 05 | ． 00 | ． 05 | ． 05 | ． 07 | ． 00 | ． 02 | ． 05 | ． 00 | ． 65 |
|  | 5 | 3 | 5 | 3 | 4 | 6 | 2 | 2 | 2 | 1 | 5 | 7 | 10 | 4 | 7 | 1 | 0 | 67 |
| （1） | ． 33 | ． 20 | ． 33 | ． 20 | ． 26 | ． 39 | ． 13 | ． 13 | ． 13 | ． 07 | ． 33 | ． 46 | ． 65 | ． 26 | ． 46 | ． 07 | ． 00 | 4.38 |
| 1．6－ 2.0 | ． 12 | ． 07 | ． 12 | ． 07 | ． 09 | ． 14 | ． 05 | ． 05 | ． 05 | ． 02 | ． 12 | ． 16 | ． 23 | ． 09 | ． 16 | ． 02 | ． 00 | 1.56 |
|  | 17 | 12 | 4 | 8 | 9 | 7 | 5 | 5 | 9 | 8 | 3 | 8 | 11 | 5 | 10 | 9 | 0 | 130 |
| （1） | 1.11 | ． 78 | ． 26 | ． 52 | ． 59 | ． 46 | ． 33 | ． 33 | ． 59 | ． 52 | ． 20 | ． 52 | ． 72 | ． 33 | ． 65 | ． 59 | ． 00 | 8.49 |
| 2．1－3．0 | ． 39 | ． 28 | ． 09 | ． 19 | ． 21 | ． 16 | ． 12 | ． 12 | ． 21 | ． 19 | ． 07 | ． 19 | ． 26 | ． 12 | ． 23 | ． 21 | ． 00 | 3.02 |
|  | 25 | 29 | 24 | 32 | 15 | 10 | 11 | 19 | 17 | 20 | 19 | 19 | 15 | 26 | 35 | 37 | 0 | 353 |
| （1） | 1.63 | 1.89 | 1.57 | 2.09 | ． 98 | ． 65 | ． 72 | 1.24 | 1.11 | 1.31 | 1.24 | 1.24 | ． 98 | 1.70 | 2.29 | 2.42 | ． 00 | 23.06 |
| （2） | ． 58 | ． 67 | ． 56 | ． 74 | ． 35 | ． 23 | ． 26 | ． 44 | ． 39 | ． 46 | ． 44 | ． 44 | ． 35 | ． 60 | ． 81 | ． 86 | ． 00 | 8.19 |
| 3．1－4．0 | 38 | 42 | 30 | 29 | 7 | 1 | 7 | 12 | 17 | 23 | 26 | 19 | 17 | 21 | 48 | 40 | 0 | 377 |
| （1） | 2.48 | 2.74 | 1.96 | 1.89 | ． 46 | ． 07 | ． 46 | ． 78 | 1.11 | 1.50 | 1.70 | 1.24 | 1.11 | 1.37 | 3.14 | 2.61 | ． 00 | 24.62 |
| （2） | ． 88 | ． 97 | ． 70 | ． 67 | ． 16 | ． 02 | ． 16 | ． 28 | ． 39 | ． 53 | ． 60 | ． 44 | ． 39 | ． 49 | 1.11 | ． 93 | ． 00 | 8.75 |
| 4．1－5．0 | 43 | 29 | 36 | 9 | 1 | 0 | 1 | 8 | 8 | 2 | 16 | 15 | 13 | 29 | 52 | 26 | 0 | 288 |
| （1） | 2.81 | 1.89 | 2.35 | ． 59 | ． 07 | ． 00 | ． 07 | ． 52 | ． 52 | ． 13 | 1.05 | ． 98 | ． 85 | 1.89 | 3.40 | 1.70 | ． 00 | 18.81 |
| （2） | 1.00 | ． 67 | ． 84 | ． 21 | ． 02 | ． 00 | ． 02 | ． 19 | ． 19 | ． 05 | ． 37 | ． 35 | ． 30 | ． 67 | 1.21 | ． 60 | ． 00 | 6.69 |
| 5．1－ 6.0 | 28 | 16 | 17 | 6 | 0 | 0 | 1 | 5 | 8 | 1 | 11 | 1 | 11 | 15 | 35 | 11 | 0 | 166 |
|  | 1.83 | 1.05 | 1.11 | ． 39 | ． 00 | ． 00 | ． 07 | ． 33 | ． 52 | ． 07 | ． 72 | ． 07 | ． 72 | ． 98 | 2.29 | ． 72 | ． 00 | 10.84 |
| （2） | ． 65 | ． 37 | ． 39 | ． 14 | ． 00 | ． 00 | ． 02 | ． 12 | ． 19 | ． 02 | ． 26 | ． 02 | ． 26 | ． 35 | ． 81 | ． 26 | ． 00 | 3.85 |
| 6．1－8．0 | 14 | 1 | 11 | 2 | 0 | 0 | 3 | 5 | 2 | 0 | 0 | 4 | 5 | 28 | 23 | 3 | 0 | 101 |
| （1） | ． 91 | ． 07 | ． 72 | ． 13 | ． 00 | ． 00 | ． 20 | ． 33 | ． 13 | ． 00 | ． 00 | ． 26 | ． 33 | 1.83 | 1.50 | ． 20 | ． 00 | 6.60 |
| （2） | ． 32 | ． 02 | ． 26 | ． 05 | ． 00 | ． 00 | ． 07 | ． 12 | ． 05 | ． 00 | ． 00 | ． 09 | ． 12 | ． 65 | ． 53 | ． 07 | ． 00 | 2.34 |
| 8．1－10．0 | 3 | 1 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 3 | 0 | 0 | 16 |
| （1） | ． 20 | ． 07 | ． 07 | ． 00 | ． 00 | ． 00 | ． 13 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 07 | ． 33 | ． 20 | ． 00 | ． 00 | 1.05 |
| （2） | ． 07 | ． 02 | ． 02 | ． 00 | ． 00 | ． 00 | ． 05 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 12 | ． 07 | ． 00 | ． 00 | ． 37 |
| 10．1－89．5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 07 | ． 00 | ． 00 | ． 07 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 02 |
| ALL SPEEDS | 175 | 140 | 131 | 90 | 38 | 24 | 32 | 57 | 66 | 56 | 83 | 75 | 86 | 134 | 215 | 129 | 0 | 1531 |
| （1） | 11.43 | 9.14 | 8.56 | 5.88 | 2.48 | 1.57 | 2.09 | 3.72 | 4.31 | 3.66 | 5.42 | 4.90 | 5.62 | 8.75 | 14.04 | 8.43 | ． 00 | 100.00 |
| （2） | 4.06 | 3.25 | 3.04 | 2.09 | ． 88 | ． 56 | ． 74 | 1.32 | 1.53 | 1.30 | 1.93 | 1.74 | 2.00 | 3.11 | 4.99 | 2.99 | ． 00 | 35.54 |
| （1）＝PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| （2）＝PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


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#### Abstract

CC DECEMBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER



(1) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

| CC DECEMBER MET DATA JOINT FREQUENCY DISTRIBUTION | $(60$-METER TOWER) |  |  |
| :--- | :--- | :---: | :---: |
| 33.0 FT WIND DATA | STABILITY CLASS F | CLASS FREQUENCY | (PERCENT) $=8.73$ |


| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 6 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 27 | . 53 | . 27 | . 27 | . 00 | . 27 | . 00 | . 00 | . 00 | 1.60 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 05 | . 02 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 14 |
| . $2-.4$ | 0 | 0 | 1 | 1 | 2 | 0 | 0 | 1 | 0 | 1 | 2 | 0 | 1 | 1 | 0 | 0 | 0 | 10 |
| (1) | . 00 | . 00 | . 27 | . 27 | . 53 | . 00 | . 00 | . 27 | . 00 | . 27 | . 53 | . 00 | . 27 | . 27 | . 00 | . 00 | . 00 | 2.66 |
| (2) | . 00 | . 00 | . 02 | . 02 | . 05 | . 00 | . 00 | . 02 | . 00 | . 02 | . 05 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 23 |
| .5-1.0 | 4 | 1 | 3 | 1 | 4 | 3 | 2 | 2 | 2 | 5 | 12 | 8 | 4 | 7 | 1 | 1 | 0 | 60 |
| (1) | 1.06 | . 27 | . 80 | . 27 | 1.06 | . 80 | . 53 | . 53 | . 53 | 1.33 | 3.19 | 2.13 | 1.06 | 1.86 | . 27 | . 27 | . 00 | 15.96 |
| (2) | . 09 | . 02 | . 07 | . 02 | . 09 | . 07 | . 05 | . 05 | . 05 | . 12 | . 28 | . 19 | . 09 | . 16 | . 02 | . 02 | . 00 | 1.39 |
| 1.1-1.5 | 1 | 0 | 0 | 3 | 0 | 3 | 0 | 5 | 4 | 17 | 17 | 9 | 13 | 17 | 7 | 0 | 0 | 96 |
| (1) | . 27 | . 00 | . 00 | . 80 | . 00 | . 80 | . 00 | 1.33 | 1.06 | 4.52 | 4.52 | 2.39 | 3.46 | 4.52 | 1.86 | . 00 | . 00 | 25.53 |
| (2) | . 02 | . 00 | . 00 | . 07 | . 00 | . 07 | . 00 | . 12 | . 09 | . 39 | . 39 | . 21 | . 30 | . 39 | . 16 | . 00 | . 00 | 2.23 |
| 1.6-2.0 | 1 | 2 | 0 | 1 | 0 | 0 | 2 | 3 | 13 | 23 | 13 | 9 | 14 | 14 | 9 | 1 | 0 | 105 |
| (1) | . 27 | . 53 | . 00 | . 27 | . 00 | . 00 | . 53 | . 80 | 3.46 | 6.12 | 3.46 | 2.39 | 3.72 | 3.72 | 2.39 | . 27 | . 00 | 27.93 |
| (2) | . 02 | . 05 | . 00 | . 02 | . 00 | . 00 | . 05 | . 07 | . 30 | . 53 | . 30 | . 21 | . 32 | . 32 | . 21 | . 02 | . 00 | 2.44 |
| 2.1-3.0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 27 | 28 | 9 | 1 | 2 | 7 | 0 | 0 | 87 |
| (1) | . 27 | . 53 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 2.66 | 7.18 | 7.45 | 2.39 | . 27 | . 53 | 1.86 | . 00 | . 00 | 23.14 |
| (2) | . 02 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 23 | . 63 | . 65 | . 21 | . 02 | . 05 | . 16 | . 00 | . 00 | 2.02 |
| 3.1-4.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 11 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 53 | 2.39 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 2.93 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 21 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 26 |
| 4.1-5.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 27 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 27 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| 5.1-6.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 6.1-8.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 7 | 5 | 4 | 6 | 6 | 6 | 4 | 11 | 31 | 77 | 82 | 36 | 33 | 42 | 24 | 2 | 0 | 376 |
| (1) | 1.86 | 1.33 | 1.06 | 1.60 | 1.60 | 1.60 | 1.06 | 2.93 | 8.24 | 20.48 | 21.81 | 9.57 | 8.78 | 11.17 | 6.38 | . 53 | . 00 | 100.00 |
| (2) | . 16 | . 12 | . 09 | . 14 | . 14 | . 14 | . 09 | . 26 | . 72 | 1.79 | 1.90 | . 84 | . 77 | . 97 | . 56 | . 05 | . 00 | 8.73 |
| )=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PA |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| (2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

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| CC DECEMBER MET DATA JOINT | FREQUENCY DISTRIBUTION | ( 60 -METER TOWER) |
| :--- | :---: | :---: | :---: | :---: |
| 33.0 FT WIND DATA | STABILITY CLASS G | CLASS FREQUENCY (PERCENT) $=\quad 2.74$ |


|  |  |  |  |  |  |  |  | D DI | RECTIO | N FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 85 | . 00 | . 00 | . 00 | . 85 | . 00 | . 85 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 2.54 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 2 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.69 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.69 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 |
| .5-1.0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 2 | 4 | 5 | 3 | 1 | 1 | 0 | 0 | 18 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 85 | . 85 | . 00 | . 00 | . 00 | 1.69 | 3.39 | 4.24 | 2.54 | . 85 | . 85 | . 00 | . 00 | 15.25 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 05 | . 09 | . 12 | . 07 | . 02 | . 02 | . 00 | . 00 | . 42 |
| 1.1-1.5 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 9 | 12 | 11 | 6 | 2 | 1 | 0 | 1 | 0 | 45 |
| (1) | . 85 | . 00 | . 00 | . 85 | . 00 | . 00 | . 85 | . 00 | 7.63 | 10.17 | 9.32 | 5.08 | 1.69 | . 85 | . 00 | . 85 | . 00 | 38.14 |
| (2) | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 21 | . 28 | . 26 | . 14 | . 05 | . 02 | . 00 | . 02 | . 00 | 1.04 |
| 1.6-2.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 6 | 11 | 12 | 0 | 2 | 0 | 0 | 0 | 0 | 32 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 85 | 5.08 | 9.32 | 10.17 | . 00 | 1.69 | . 00 | . 00 | . 00 | . 00 | 27.12 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 14 | . 26 | . 28 | . 00 | . 05 | . 00 | . 00 | . 00 | . 00 | . 74 |
| 2.1-3.0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 5 | 3 | 0 | 3 | 1 | 0 | 0 | 0 | 17 |
| (1) | . 85 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 3.39 | 4.24 | 2.54 | . 00 | 2.54 | . 85 | . 00 | . 00 | . 00 | 14.41 |
| (2) | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 09 | . 12 | . 07 | . 00 | . 07 | . 02 | . 00 | . 00 | . 00 | . 39 |
| 3.1-4.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 85 | . 00 | . 00 | . 85 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 |
| 4.1-5.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 5.1-6.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 6.1-8.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 2 | 0 | 0 | 1 | 2 | 1 | 1 | 1 | 20 | 30 | 31 | 13 | 10 | 3 | 2 | 1 | 0 | 118 |
| (1) | 1.69 | . 00 | . 00 | . 85 | 1.69 | . 85 | . 85 | . 85 | 16.95 | 25.42 | 26.27 | 11.02 | 8.47 | 2.54 | 1.69 | . 85 | . 00 | 100.00 |
| (2) | . 05 | . 00 | . 00 | . 02 | . 05 | . 02 | . 02 | . 02 | . 46 | . 70 | . 72 | . 30 | . 23 | . 07 | . 05 | . 02 | . 00 | 2.74 |

## פヨוכヨIOपd IHפוyגdO)

Table 2.3-29—\{CCNPP 33 ft ( 10 m ) December JFD (2000-2005)\} (Page 8 of 8 )
CC DECEMBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)

ग्0
$\stackrel{0}{2}$
$i$

CC JANUARY MET DATA JOINT FREQUENCY DISTRIBUTION ( $60-$ METER TOWER)
197.0 FT WIND DATA STABILITY CLASS A CLASS FREQUENCY (PERCENT) = 7.94

(1) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

| CC JANUARY MET DATA JOINT FREQUENCY DISTRIBUTION | $(60$-METER TOWER) |  |  |
| :---: | :---: | :---: | :---: |
| $197.0 ~ F T ~ W I N D ~ D A T A ~$ | STABILITY CLASS B | CLASS FREQUENCY | (PERCENT) $=3.36$ |


| 197.0 FT WIND DATA |  |  | STABILITY CLASS B |  |  |  |  | CLASS FREQUENCY (PERCENT) = |  |  |  |  |  | 3.36 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | EnE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 1.1-1.5 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 69 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 69 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| 1.6-2.0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| (1) | . 00 | 1.38 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 69 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 2.07 |
| (2) | . 00 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 |
| 2.1-3.0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 2 | 2 | 2 | 0 | 1 | 0 | 9 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 69 | . 00 | . 69 | . 00 | . 00 | . 00 | 1.38 | 1.38 | 1.38 | . 00 | . 69 | . 00 | 6.21 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 05 | . 05 | . 05 | . 00 | . 02 | . 00 | . 21 |
| 3.1-4.0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 3 | 2 | 2 | 1 | 0 | 1 | 1 | 0 | 14 |
| (1) | 2.07 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 69 | . 00 | 2.07 | 1.38 | 1.38 | . 69 | . 00 | . 69 | . 69 | . 00 | 9.66 |
| (2) | . 07 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 07 | . 05 | . 05 | . 02 | . 00 | . 02 | . 02 | . 00 | . 32 |
| 4.1-5.0 | 5 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 3 | 3 | 0 | 5 | 0 | 1 | 0 | 21 |
| (1) | 3.45 | . 69 | . 00 | . 00 | . 00 | . 00 | . 69 | . 69 | . 00 | . 69 | 2.07 | 2.07 | . 00 | 3.45 | . 00 | . 69 | . 00 | 14.48 |
| (2) | . 12 | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 02 | . 07 | . 07 | . 00 | . 12 | . 00 | . 02 | . 00 | . 49 |
| 5.1-6.0 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 2 | 2 | 2 | 5 | 0 | 3 | 2 | 0 | 22 |
| (1) | 2.07 | . 00 | . 00 | . 00 | . 00 | . 00 | . 69 | 1.38 | . 00 | 1.38 | 1.38 | 1.38 | 3.45 | . 00 | 2.07 | 1.38 | . 00 | 15.17 |
| (2) | . 07 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 05 | . 00 | . 05 | . 05 | . 05 | . 12 | . 00 | . 07 | . 05 | . 00 | . 51 |
| 6.1-8.0 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 2 | 3 | 9 | 12 | 6 | 0 | 46 |
| (1) | 2.76 | . 69 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 6.21 | 1.38 | 2.07 | 6.21 | 8.28 | 4.14 | . 00 | 31.72 |
| (2) | . 09 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 21 | . 05 | . 07 | . 21 | . 28 | . 14 | . 00 | 1.06 |
| 8.1-10.0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 4 | 11 | 3 | 0 | 24 |
| (1) | 2.07 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 69 | . 69 | . 00 | . 69 | 2.76 | 7.59 | 2.07 | . 00 | 16.55 |
| (2) | . 07 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 02 | . 09 | . 25 | . 07 | . 00 | . 56 |
| 10.1-89.5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 1 | 0 | 5 |
| (1) | . 69 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 69 | . 69 | . 00 | . 69 | . 00 | . 69 | . 00 | 3.45 |
| (2) | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 02 | . 00 | . 02 | . 00 | . 12 |
| ALL SPEEDS | 19 | 4 | 0 | 0 | 1 | 1 | 2 | 5 | 0 | 7 | 19 | 12 | 12 | 21 | 27 | 15 | 0 | 145 |
| (1) | 13.10 | 2.76 | . 00 | . 00 | . 69 | . 69 | 1.38 | 3.45 | . 00 | 4.83 | 13.10 | 8.28 | 8.28 | 14.48 | 18.62 | 10.34 | . 00 | 100.00 |
| (2) | . 44 | . 09 | . 00 | . 00 | . 02 | . 02 | . 05 | . 12 | . 00 | . 16 | . 44 | . 28 | . 28 | . 49 | . 63 | . 35 | . 00 | 3.36 |

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

| CC JANUARY MET DATA JOINT | FREQUENCY DISTRIBUTION | （60－METER TOWER） |  |
| :---: | :---: | :---: | :---: |
| $197.0 ~ F T ~ W I N D ~ D A T A ~$ | STABILITY CLASS C | CLASS FREQUENCY | （PERCENT）$=4.79$ |


|  |  |  |  |  |  |  |  |  |  | Frn |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT ． 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| ． $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| ．5－1．0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |
| 1．1－1．5 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| （1） | ． 00 | ． 00 | ． 00 | ． 48 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 48 |
| （2） | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 |
| 1．6－2．0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 0 | 6 |
| （1） | ． 00 | ． 97 | ． 48 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 48 | ． 00 | ． 48 | ． 00 | ． 48 | ． 00 | ． 00 | 2.90 |
| （2） | ． 00 | ． 05 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 02 | ． 00 | ． 02 | ． 00 | ． 00 | ． 14 |
| 2．1－3．0 | 2 | 5 | 4 | 3 | 1 | 1 | 1 | 0 | 0 | 1 | 2 | 4 | 3 | 1 | 2 | 1 | 0 | 31 |
| （1） | ． 97 | 2.42 | 1.93 | 1.45 | ． 48 | ． 48 | ． 48 | ． 00 | ． 00 | ． 48 | ． 97 | 1.93 | 1.45 | ． 48 | ． 97 | ． 48 | ． 00 | 14.98 |
| （2） | ． 05 | ． 12 | ． 09 | ． 07 | ． 02 | ． 02 | ． 02 | ． 00 | ． 00 | ． 02 | ． 05 | ． 09 | ． 07 | ． 02 | ． 05 | ． 02 | ． 00 | ． 72 |
| 3．1－4．0 | 1 | 2 | 0 | 0 | 1 | 0 | 1 | 3 | 1 | 3 | 5 | 2 | 2 | 2 | 0 | 3 | 0 | 26 |
| （1） | ． 48 | ． 97 | ． 00 | ． 00 | ． 48 | ． 00 | ． 48 | 1.45 | ． 48 | 1.45 | 2.42 | ． 97 | ． 97 | ． 97 | ． 00 | 1.45 | ． 00 | 12.56 |
| （2） | ． 02 | ． 05 | ． 00 | ． 00 | ． 02 | ． 00 | ． 02 | ． 07 | ． 02 | ． 07 | ． 12 | ． 05 | ． 05 | ． 05 | ． 00 | ． 07 | ． 00 | ． 60 |
| 4．1－5．0 | 3 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 2 | 3 | 4 | 3 | 4 | 9 | 2 | 0 | 33 |
| （1） | 1.45 | ． 48 | ． 00 | ． 00 | ． 00 | ． 00 | ． 48 | ． 48 | ． 00 | ． 97 | 1.45 | 1.93 | 1.45 | 1.93 | 4.35 | ． 97 | ． 00 | 15.94 |
| （2） | ． 07 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 02 | ． 00 | ． 05 | ． 07 | ． 09 | ． 07 | ． 09 | ． 21 | ． 05 | ． 00 | ． 76 |
| 5．1－6．0 | 7 | 3 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 2 | 0 | 3 | 5 | 1 | 0 | 24 |
| （1） | 3.38 | 1.45 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 97 | ． 00 | ． 48 | ． 00 | ． 97 | ． 00 | 1.45 | 2.42 | ． 48 | ． 00 | 11.59 |
| （2） | ． 16 | ． 07 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 05 | ． 00 | ． 02 | ． 00 | ． 05 | ． 00 | ． 07 | ． 12 | ． 02 | ． 00 | ． 56 |
| 6．1－8．0 | 6 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 5 | 1 | 3 | 7 | 12 | 7 | 0 | 50 |
| （1） | 2.90 | 2.42 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 48 | 1.45 | 2.42 | ． 48 | 1.45 | 3.38 | 5.80 | 3.38 | ． 00 | 24.15 |
| （2） | ． 14 | ． 12 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 07 | ． 12 | ． 02 | ． 07 | ． 16 | ． 28 | ． 16 | ． 00 | 1.16 |
| 8．1－10．0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 10 | 0 | 0 | 20 |
| （1） | ． 97 | ． 97 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | 1.45 | ． 00 | ． 00 | 1.45 | 4.83 | ． 00 | ． 00 | 9.66 |
| （2） | ． 05 | ． 05 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 07 | ． 00 | ． 00 | ． 07 | ． 23 | ． 00 | ． 00 | ． 46 |
| 10．1－89．5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 2 | 3 | 7 | 0 | 0 | 16 |
| （1） | ． 48 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | 1.45 | ． 00 | ． 00 | ． 97 | 1.45 | 3.38 | ． 00 | ． 00 | 7.73 |
| （2） | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 07 | ． 00 | ． 00 | ． 05 | ． 07 | ． 16 | ． 00 | ． 00 | ． 37 |
| ALL SPEEDS | 22 | 20 | 5 | 4 | 2 | 1 | 3 | 6 | 2 | 13 | 19 | 13 | 14 | 23 | 46 | 14 | 0 | 207 |
| （1） | 10.63 | 9.66 | 2.42 | 1.93 | ． 97 | ． 48 | 1.45 | 2.90 | ． 97 | 6.28 | 9.18 | 6.28 | 6.76 | 11.11 | 22.22 | 6.76 | ． 00 | 100.00 |
| （2） | ． 51 | ． 46 | ． 12 | ． 09 | ． 05 | ． 02 | ． 07 | ． 14 | ． 05 | ． 30 | ． 44 | ． 30 | ． 32 | ． 53 | 1.06 | ． 32 | ． 00 | 4.79 |

（1）＝PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
（2）＝PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
T
$\stackrel{0}{0}$
$i$
$i$

Table 2.3-30—\{CCNPP 33 ft ( 10 m) January JFD (2000-2005)\} (Page 4 of 8)
CC JANUARY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS D CLASS FREQUENCY (PERCENT) = 42.11

|  | WIND DIRECTION FROM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . 5- 1.0 | 1 | 1 | 6 | 0 | 3 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 20 |
| (1) | . 05 | . 05 | . 33 | . 00 | . 16 | . 05 | . 05 | . 05 | . 05 | . 05 | . 05 | . 05 | . 05 | . 05 | . 00 | . 00 | . 00 | 1.10 |
| (2) | . 02 | . 02 | . 14 | . 00 | . 07 | . 02 | . 02 | . 02 | . 02 | . 02 | . 02 | . 02 | . 02 | . 02 | . 00 | . 00 | . 00 | . 46 |
| 1.1-1.5 | 1 | 2 | 6 | 6 | 5 | 1 | 3 | 0 | 1 | 4 | 0 | 0 | 1 | 1 | 3 | 1 | 0 | 35 |
| (1) | . 05 | . 11 | . 33 | . 33 | . 27 | . 05 | . 16 | . 00 | . 05 | . 22 | . 00 | . 00 | . 05 | . 05 | . 16 | . 05 | . 00 | 1.92 |
| (2) | . 02 | . 05 | . 14 | . 14 | . 12 | . 02 | . 07 | . 00 | . 02 | . 09 | . 00 | . 00 | . 02 | . 02 | . 07 | . 02 | . 00 | . 81 |
| 1.6-2.0 | 2 | 5 | 4 | 6 | 6 | 3 | 1 | 2 | 2 | 3 | 5 | 3 | 4 | 3 | 1 | 5 | 0 | 55 |
| (1) | . 11 | . 27 | . 22 | . 33 | . 33 | . 16 | . 05 | . 11 | . 11 | . 16 | . 27 | . 16 | . 22 | . 16 | . 05 | . 27 | . 00 | 3.02 |
| (2) | . 05 | . 12 | . 09 | . 14 | . 14 | . 07 | . 02 | . 05 | . 05 | . 07 | . 12 | . 07 | . 09 | . 07 | . 02 | . 12 | . 00 | 1.27 |
| 2.1-3.0 | 17 | 13 | 11 | 10 | 14 | 11 | 16 | 10 | 9 | 10 | 8 | 14 | 12 | 3 | 9 | 13 | 0 | 180 |
| (1) | . 93 | . 71 | . 60 | . 55 | . 77 | . 60 | . 88 | . 55 | . 49 | . 55 | . 44 | . 77 | . 66 | . 16 | . 49 | . 71 | . 00 | 9.90 |
| (2) | . 39 | . 30 | . 25 | . 23 | . 32 | . 25 | . 37 | . 23 | . 21 | . 23 | . 19 | . 32 | . 28 | . 07 | . 21 | . 30 | . 00 | 4.17 |
| 3.1-4.0 | 27 | 18 | 12 | 15 | 10 | 7 | 14 | 16 | 13 | 13 | 12 | 12 | 5 | 6 | 13 | 19 | 0 | 212 |
| (1) | 1.48 | . 99 | . 66 | . 82 | . 55 | . 38 | . 77 | . 88 | . 71 | . 71 | . 66 | . 66 | . 27 | . 33 | . 71 | 1.04 | . 00 | 11.65 |
| (2) | . 63 | . 42 | . 28 | . 35 | . 23 | . 16 | . 32 | . 37 | . 30 | . 30 | . 28 | . 28 | . 12 | . 14 | . 30 | . 44 | . 00 | 4.91 |
| 4.1-5.0 | 36 | 17 | 8 | 7 | 4 | 8 | 10 | 18 | 7 | 8 | 14 | 9 | 11 | 13 | 39 | 26 | 0 | 235 |
| (1) | 1.98 | . 93 | . 44 | . 38 | . 22 | . 44 | . 55 | . 99 | . 38 | . 44 | . 77 | . 49 | . 60 | . 71 | 2.14 | 1.43 | . 00 | 12.92 |
| (2) | . 83 | . 39 | . 19 | . 16 | . 09 | . 19 | . 23 | . 42 | . 16 | . 19 | . 32 | . 21 | . 25 | . 30 | . 90 | . 60 | . 00 | 5.44 |
| 5.1-6.0 | 21 | 19 | 8 | 5 | 0 | 3 | 3 | 16 | 8 | 16 | 14 | 18 | 10 | 23 | 60 | 60 | 0 | 284 |
| (1) | 1.15 | 1.04 | . 44 | . 27 | . 00 | . 16 | . 16 | . 88 | . 44 | . 88 | . 77 | . 99 | . 55 | 1.26 | 3.30 | 3.30 | . 00 | 15.61 |
| (2) | . 49 | . 44 | . 19 | . 12 | . 00 | . 07 | . 07 | . 37 | . 19 | . 37 | . 32 | . 42 | . 23 | . 53 | 1.39 | 1.39 | . 00 | 6.57 |
| 6.1-8.0 | 66 | 51 | 8 | 2 | 0 | 1 | 5 | 14 | 14 | 25 | 36 | 15 | 8 | 47 | 124 | 79 | 0 | 495 |
| (1) | 3.63 | 2.80 | . 44 | . 11 | . 00 | . 05 | . 27 | . 77 | . 77 | 1.37 | 1.98 | . 82 | . 44 | 2.58 | 6.82 | 4.34 | . 00 | 27.21 |
| (2) | 1.53 | 1.18 | . 19 | . 05 | . 00 | . 02 | . 12 | . 32 | . 32 | . 58 | . 83 | . 35 | . 19 | 1.09 | 2.87 | 1.83 | . 00 | 11.46 |
| 8.1-10.0 | 48 | 34 | 1 | 0 | 0 | 0 | 3 | 2 | 5 | 18 | 15 | 0 | 0 | 19 | 62 | 28 | 0 | 235 |
| (1) | 2.64 | 1.87 | . 05 | . 00 | . 00 | . 00 | . 16 | . 11 | . 27 | . 99 | . 82 | . 00 | . 00 | 1.04 | 3.41 | 1.54 | . 00 | 12.92 |
| (2) | 1.11 | . 79 | . 02 | . 00 | . 00 | . 00 | . 07 | . 05 | . 12 | . 42 | . 35 | . 00 | . 00 | . 44 | 1.44 | . 65 | . 00 | 5.44 |
| 10.1-89.5 | 21 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 3 | 2 | 1 | 10 | 15 | 9 | 0 | 68 |
| (1) | 1.15 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 27 | . 16 | . 11 | . 05 | . 55 | . 82 | . 49 | . 00 | 3.74 |
| (2) | . 49 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 12 | . 07 | . 05 | . 02 | . 23 | . 35 | . 21 | . 00 | 1.57 |
| ALL SPEEDS | 240 | 161 | 64 | 51 | 42 | 35 | 56 | 79 | 61 | 103 | 108 | 74 | 53 | 126 | 326 | 240 | 0 | 1819 |
| (1) | 13.19 | 8.85 | 3.52 | 2.80 | 2.31 | 1.92 | 3.08 | 4.34 | 3.35 | 5.66 | 5.94 | 4.07 | 2.91 | 6.93 | 17.92 | 13.19 | . 00 | 100.00 |
| (2) | 5.56 | 3.73 | 1.48 | 1.18 | . 97 | . 81 | 1.30 | 1.83 | 1.41 | 2.38 | 2.50 | 1.71 | 1.23 | 2.92 | 7.55 | 5.56 | . 00 | 42.11 |
| (1) = PERCENT | OF ALI | GOOD | OBSERV | ATIONS | FOR | HIS PA |  |  |  |  |  |  |  |  |  |  |  |  |

CC JANUARY MET DATA
197.0 FT WIND DATA

Table 2.3-30—\{CCNPP 33 ft (10 m) January JFD (2000-2005)\} (Page 5 of 8)
CC JANUARY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)

| SPEED | N | NNE | NE | ENE | E | ESE | WIND DIRECTION FROM |  |  |  |  | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  | SE | SSE | S | SSW | SW |  |  |  |  |  |  |  |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .2- . 4 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 08 | . 00 | . 00 | . 00 | . 08 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 16 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 |
| .5-1.0 | 1 | 1 | 1 | 1 | 4 | 1 | 1 | 3 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 2 | 0 | 17 |
| (1) | . 08 | . 08 | . 08 | . 08 | . 32 | . 08 | . 08 | . 24 | . 00 | . 00 | . 00 | . 08 | . 00 | . 08 | . 00 | . 16 | . 00 | 1.35 |
| (2) | . 02 | . 02 | . 02 | . 02 | . 09 | . 02 | . 02 | . 07 | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 05 | . 00 | . 39 |
| 1.1-1.5 | 2 | 3 | 1 | 2 | 3 | 1 | 5 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 1 | 2 | 0 | 22 |
| (1) | . 16 | . 24 | . 08 | . 16 | . 24 | . 08 | . 40 | . 00 | . 00 | . 00 | . 16 | . 00 | . 00 | . 00 | . 08 | . 16 | . 00 | 1.74 |
| (2) | . 05 | . 07 | . 02 | . 05 | . 07 | . 02 | . 12 | . 00 | . 00 | . 00 | . 05 | . 00 | . 00 | . 00 | . 02 | . 05 | . 00 | . 51 |
| 1.6-2.0 | 1 | 6 | 3 | 2 | 2 | 3 | 2 | 2 | 0 | 1 | 2 | 2 | 0 | 2 | 1 | 0 | 0 | 29 |
| (1) | . 08 | . 48 | . 24 | . 16 | . 16 | . 24 | . 16 | . 16 | . 00 | . 08 | . 16 | . 16 | . 00 | . 16 | . 08 | . 00 | . 00 | 2.30 |
| (2) | . 02 | . 14 | . 07 | . 05 | . 05 | . 07 | . 05 | . 05 | . 00 | . 02 | . 05 | . 05 | . 00 | . 05 | . 02 | . 00 | . 00 | . 67 |
| 2.1-3.0 | 8 | 5 | 5 | 7 | 6 | 3 | 6 | 3 | 3 | 2 | 5 | 3 | 5 | 7 | 4 | 6 | 0 | 78 |
| (1) | . 63 | . 40 | . 40 | . 56 | . 48 | . 24 | . 48 | . 24 | . 24 | . 16 | . 40 | . 24 | . 40 | . 56 | . 32 | . 48 | . 00 | 6.19 |
| (2) | . 19 | . 12 | . 12 | . 16 | . 14 | . 07 | . 14 | . 07 | . 07 | . 05 | . 12 | . 07 | . 12 | . 16 | . 09 | . 14 | . 00 | 1.81 |
| $3.1-4.0$ | 21 | 11 | 7 | 3 | 3 | 3 | 2 | 11 | 7 | 4 | 8 | 7 | 10 | 24 | 22 | 35 | 0 | 178 |
| (1) | 1.67 | . 87 | . 56 | . 24 | . 24 | . 24 | . 16 | . 87 | . 56 | . 32 | . 63 | . 56 | . 79 | 1.90 | 1.74 | 2.78 | . 00 | 14.12 |
| (2) | . 49 | . 25 | . 16 | . 07 | . 07 | . 07 | . 05 | . 25 | . 16 | . 09 | . 19 | . 16 | . 23 | . 56 | . 51 | . 81 | . 00 | 4.12 |
| 4.1-5.0 | 17 | 10 | 8 | 4 | 1 | 1 | 5 | 17 | 7 | 7 | 8 | 9 | 15 | 38 | 58 | 38 | 0 | 243 |
| (1) | 1.35 | . 79 | . 63 | . 32 | . 08 | . 08 | . 40 | 1.35 | . 56 | . 56 | . 63 | . 71 | 1.19 | 3.01 | 4.60 | 3.01 | . 00 | 19.27 |
| (2) | . 39 | . 23 | . 19 | . 09 | . 02 | . 02 | . 12 | . 39 | . 16 | . 16 | . 19 | . 21 | . 35 | . 88 | 1.34 | . 88 | . 00 | 5.63 |
| 5.1-6.0 | 16 | 12 | 2 | 3 | 1 | 1 | 3 | 10 | 26 | 18 | 18 | 8 | 13 | 35 | 66 | 23 | 0 | 255 |
| (1) | 1.27 | . 95 | . 16 | . 24 | . 08 | . 08 | . 24 | . 79 | 2.06 | 1.43 | 1.43 | . 63 | 1.03 | 2.78 | 5.23 | 1.82 | . 00 | 20.22 |
| (2) | . 37 | . 28 | . 05 | . 07 | . 02 | . 02 | . 07 | . 23 | . 60 | . 42 | . 42 | . 19 | . 30 | . 81 | 1.53 | . 53 | . 00 | 5.90 |
| 6.1-8.0 | 10 | 4 | 4 | 0 | 0 | 2 | 1 | 18 | 13 | 73 | 96 | 22 | 7 | 27 | 34 | 22 | 0 | 333 |
| (1) | . 79 | . 32 | . 32 | . 00 | . 00 | . 16 | . 08 | 1.43 | 1.03 | 5.79 | 7.61 | 1.74 | . 56 | 2.14 | 2.70 | 1.74 | . 00 | 26.41 |
| (2) | . 23 | . 09 | . 09 | . 00 | . 00 | . 05 | . 02 | . 42 | . 30 | 1.69 | 2.22 | . 51 | . 16 | . 63 | . 79 | . 51 | . 00 | 7.71 |
| 8.1-10.0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 8 | 25 | 46 | 2 | 0 | 5 | 6 | 1 | 0 | 102 |
| (1) | . 32 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 40 | . 63 | 1.98 | 3.65 | . 16 | . 00 | . 40 | . 48 | . 08 | . 00 | 8.09 |
| (2) | . 09 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 12 | . 19 | . 58 | 1.06 | . 05 | . 00 | . 12 | . 14 | . 02 | . 00 | 2.36 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 08 | . 00 | . 00 | . 08 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 16 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 |
| ALL SPEEDS | 80 | 52 | 31 | 22 | 21 | 15 | 25 | 70 | 65 | 130 | 186 | 54 | 50 | 139 | 192 | 129 | 0 | 1261 |
| (1) | 6.34 | 4.12 | 2.46 | 1.74 | 1.67 | 1.19 | 1.98 | 5.55 | 5.15 | 10.31 | 14.75 | 4.28 | 3.97 | 11.02 | 15.23 | 10.23 | . 00 | 100.00 |
| (2) | 1.85 | 1.20 | . 72 | . 51 | . 49 | . 35 | . 58 | 1.62 | 1.50 | 3.01 | 4.31 | 1.25 | 1.16 | 3.22 | 4.44 | 2.99 | . 00 | 29.19 |

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| CC JANUARY MET DATA JOINT FREQUENCY DISTRIBUTION | ( 60 -METER TOWER) |  |
| :---: | :---: | :---: |
| $197.0 ~ F T ~ W I N D ~ D A T A ~$ | STABILITY CLASS F | CLASS FREQUENCY (PERCENT) $=\mathbf{9 . 0 7}$ |


(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
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| CC JANUARY MET DATA JOINT FREQUENCY DISTRIBUTION | $(60-M E T E R ~ T O W E R) ~$ |  |
| :---: | :---: | :---: | :---: |
| 197.0 FT WIND DATA | STABILITY CLASS G | CLASS FREQUENCY (PERCENT) $=\mathbf{3 . 5 4}$ |


|  |  |  |  |  |  |  |  | IND D | RECTIO | N FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 6 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.31 | . 65 | . 00 | . 00 | . 00 | . 65 | . 65 | . 00 | . 65 | . 00 | . 00 | 3.92 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 02 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 02 | . 00 | . 00 | . 14 |
| 1.1-1.5 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 7 |
| (1) | . 00 | . 65 | . 00 | . 65 | . 65 | . 00 | . 00 | . 65 | . 00 | . 00 | . 00 | . 65 | . 65 | . 65 | . 00 | . 00 | . 00 | 4.58 |
| (2) | . 00 | . 02 | . 00 | . 02 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 02 | . 02 | . 02 | . 00 | . 00 | . 00 | . 16 |
| 1.6-2.0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 6 |
| (1) | . 00 | . 00 | . 00 | 1.31 | . 00 | . 65 | . 00 | . 00 | . 00 | . 00 | 1.31 | . 00 | . 65 | . 00 | . 00 | . 00 | . 00 | 3.92 |
| (2) | . 00 | . 00 | . 00 | . 05 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 14 |
| 2.1-3.0 | 1 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 3 | 2 | 1 | 3 | 1 | 0 | 0 | 0 | 0 | 14 |
| (1) | . 65 | . 00 | . 00 | . 65 | . 00 | . 65 | . 65 | . 00 | 1.96 | 1.31 | . 65 | 1.96 | . 65 | . 00 | . 00 | . 00 | . 00 | 9.15 |
| (2) | . 02 | . 00 | . 00 | . 02 | . 00 | . 02 | . 02 | . 00 | . 07 | . 05 | . 02 | . 07 | . 02 | . 00 | . 00 | . 00 | . 00 | . 32 |
| 3.1-4.0 | 1 | 0 | 1 | 1 | 0 | 0 | 1 | 5 | 4 | 1 | 5 | 4 | 1 | 2 | 0 | 0 | 0 | 26 |
| (1) | . 65 | . 00 | . 65 | . 65 | . 00 | . 00 | . 65 | 3.27 | 2.61 | . 65 | 3.27 | 2.61 | . 65 | 1.31 | . 00 | . 00 | . 00 | 16.99 |
| (2) | . 02 | . 00 | . 02 | . 02 | . 00 | . 00 | . 02 | . 12 | . 09 | . 02 | . 12 | . 09 | . 02 | . 05 | . 00 | . 00 | . 00 | . 60 |
| 4.1-5.0 | 0 | 0 | 0 | 0 | 0 | 3 | 1 | 7 | 2 | 5 | 2 | 2 | 1 | 4 | 1 | 1 | 0 | 29 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | 1.96 | . 65 | 4.58 | 1.31 | 3.27 | 1.31 | 1.31 | . 65 | 2.61 | . 65 | . 65 | . 00 | 18.95 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 | . 02 | . 16 | . 05 | . 12 | . 05 | . 05 | . 02 | . 09 | . 02 | . 02 | . 00 | . 67 |
| 5.1-6.0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 3 | 6 | 3 | 8 | 2 | 2 | 1 | 0 | 2 | 0 | 28 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 65 | . 00 | 1.96 | 3.92 | 1.96 | 5.23 | 1.31 | 1.31 | . 65 | . 00 | 1.31 | . 00 | 18.30 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 07 | . 14 | . 07 | . 19 | . 05 | . 05 | . 02 | . 00 | . 05 | . 00 | . 65 |
| 6.1-8.0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 7 | 9 | 4 | 3 | 3 | 0 | 2 | 0 | 0 | 31 |
| (1) | . 00 | . 65 | . 00 | . 00 | . 00 | . 00 | . 65 | . 65 | 4.58 | 5.88 | 2.61 | 1.96 | 1.96 | . 00 | 1.31 | . 00 | . 00 | 20.26 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 16 | . 21 | . 09 | . 07 | . 07 | . 00 | . 05 | . 00 | . 00 | . 72 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 5 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 65 | . 00 | . 65 | . 00 | 1.31 | . 00 | . 00 | . 65 | . 00 | . 00 | 3.27 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 05 | . 00 | . 00 | . 02 | . 00 | . 00 | . 12 |
| 10.1-89.5 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 65 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 65 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| ALL SPEEDS | 2 | 3 | 1 | 5 | 1 | 6 | 6 | 19 | 22 | 21 | 22 | 18 | 11 | 8 | 5 | 3 | 0 | 153 |
| (1) | 1.31 | 1.96 | . 65 | 3.27 | . 65 | 3.92 | 3.92 | 12.42 | 14.38 | 13.73 | 14.38 | 11.76 | 7.19 | 5.23 | 3.27 | 1.96 | . 00 | 100.00 |
| (2) | . 05 | . 07 | . 02 | . 12 | . 02 | . 14 | . 14 | . 44 | . 51 | . 49 | . 51 | . 42 | . 25 | . 19 | . 12 | . 07 | . 00 | 3.54 |

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

Table 2.3-30—\{CCNPP 33 ft ( 10 m) January JFD (2000-2005)\} (Page 8 of 8 )
CC JANUARY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS ALL CLASS FREQUENCY (PERCENT) = 100.00

| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| (2) | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 |
| . $5-1.0$ | 3 | 3 | 7 | 2 | 7 | 3 | 4 | 5 | 1 | 2 | 2 | 6 | 4 | 2 | 1 | 2 | 0 | 54 |
| (1) | . 07 | . 07 | . 16 | . 05 | . 16 | . 07 | . 09 | . 12 | . 02 | . 05 | . 05 | . 14 | . 09 | . 05 | . 02 | . 05 | . 00 | 1.25 |
| (2) | . 07 | . 07 | . 16 | . 05 | . 16 | . 07 | . 09 | . 12 | . 02 | . 05 | . 05 | . 14 | . 09 | . 05 | . 02 | . 05 | . 00 | 1.25 |
| 1.1-1.5 | 3 | 7 | 7 | 11 | 13 | 3 | 9 | 1 | 1 | 4 | 3 | 1 | 2 | 3 | 6 | 5 | 0 | 79 |
| (1) | . 07 | . 16 | . 16 | . 25 | . 30 | . 07 | . 21 | . 02 | . 02 | . 09 | . 07 | . 02 | . 05 | . 07 | . 14 | . 12 | . 00 | 1.83 |
| (2) | . 07 | . 16 | . 16 | . 25 | . 30 | . 07 | . 21 | . 02 | . 02 | . 09 | . 07 | . 02 | . 05 | . 07 | . 14 | . 12 | . 00 | 1.83 |
| 1.6-2.0 | 4 | 16 | 11 | 11 | 11 | 8 | 4 | 6 | 2 | 5 | 12 | 7 | 7 | 8 | 3 | 7 | 0 | 122 |
| (1) | . 09 | . 37 | . 25 | . 25 | . 25 | . 19 | . 09 | . 14 | . 05 | . 12 | . 28 | . 16 | . 16 | . 19 | . 07 | . 16 | . 00 | 2.82 |
| (2) | . 09 | . 37 | . 25 | . 25 | . 25 | . 19 | . 09 | . 14 | . 05 | . 12 | . 28 | . 16 | . 16 | . 19 | . 07 | . 16 | . 00 | 2.82 |
| 2.1-3.0 | 31 | 28 | 23 | 21 | 22 | 19 | 24 | 15 | 18 | 17 | 24 | 30 | 28 | 22 | 16 | 25 | 0 | 363 |
| (1) | . 72 | . 65 | . 53 | . 49 | . 51 | . 44 | . 56 | . 35 | . 42 | . 39 | . 56 | . 69 | . 65 | . 51 | . 37 | . 58 | . 00 | 8.40 |
| (2) | . 72 | . 65 | . 53 | . 49 | . 51 | . 44 | . 56 | . 35 | . 42 | . 39 | . 56 | . 69 | . 65 | . 51 | . 37 | . 58 | . 00 | 8.40 |
| 3.1-4.0 | 62 | 32 | 22 | 24 | 16 | 11 | 19 | 41 | 30 | 26 | 43 | 39 | 35 | 49 | 43 | 62 | 0 | 554 |
| (1) | 1.44 | . 74 | . 51 | . 56 | . 37 | . 25 | . 44 | . 95 | . 69 | . 60 | 1.00 | . 90 | . 81 | 1.13 | 1.00 | 1.44 | . 00 | 12.82 |
| (2) | 1.44 | . 74 | . 51 | . 56 | . 37 | . 25 | . 44 | . 95 | . 69 | . 60 | 1.00 | . 90 | . 81 | 1.13 | 1.00 | 1.44 | . 00 | 12.82 |
| 4.1-5.0 | 65 | 30 | 17 | 11 | 6 | 14 | 23 | 52 | 22 | 33 | 47 | 42 | 48 | 75 | 126 | 76 | 0 | 687 |
| (1) | 1.50 | . 69 | . 39 | . 25 | . 14 | . 32 | . 53 | 1.20 | . 51 | . 76 | 1.09 | . 97 | 1.11 | 1.74 | 2.92 | 1.76 | . 00 | 15.90 |
| (2) | 1.50 | . 69 | . 39 | . 25 | . 14 | . 32 | . 53 | 1.20 | . 51 | . 76 | 1.09 | . 97 | 1.11 | 1.74 | 2.92 | 1.76 | . 00 | 15.90 |
| 5.1-6.0 | 54 | 39 | 12 | 9 | 1 | 6 | 8 | 36 | 45 | 54 | 61 | 43 | 44 | 79 | 146 | 92 | 0 | 729 |
| (1) | 1.25 | . 90 | . 28 | . 21 | . 02 | . 14 | . 19 | . 83 | 1.04 | 1.25 | 1.41 | 1.00 | 1.02 | 1.83 | 3.38 | 2.13 | . 00 | 16.87 |
| (2) | 1.25 | . 90 | . 28 | . 21 | . 02 | . 14 | . 19 | . 83 | 1.04 | 1.25 | 1.41 | 1.00 | 1.02 | 1.83 | 3.38 | 2.13 | . 00 | 16.87 |
| 6.1-8.0 | 95 | 68 | 14 | 2 | 0 | 3 | 8 | 41 | 51 | 147 | 186 | 59 | 38 | 123 | 219 | 125 | 0 | 1179 |
| (1) | 2.20 | 1.57 | . 32 | . 05 | . 00 | . 07 | . 19 | . 95 | 1.18 | 3.40 | 4.31 | 1.37 | . 88 | 2.85 | 5.07 | 2.89 | . 00 | 27.29 |
| (2) | 2.20 | 1.57 | . 32 | . 05 | . 00 | . 07 | . 19 | . 95 | 1.18 | 3.40 | 4.31 | 1.37 | . 88 | 2.85 | 5.07 | 2.89 | . 00 | 27.29 |
| 8.1-10.0 | 63 | 38 | 1 | 0 | 0 | 0 | 3 | 8 | 14 | 47 | 71 | 4 | 3 | 45 | 113 | 34 | 0 | 444 |
| (1) | 1.46 | . 88 | . 02 | . 00 | . 00 | . 00 | . 07 | . 19 | . 32 | 1.09 | 1.64 | . 09 | . 07 | 1.04 | 2.62 | . 79 | . 00 | 10.28 |
| (2) | 1.46 | . 88 | . 02 | . 00 | . 00 | . 00 | . 07 | . 19 | . 32 | 1.09 | 1.64 | . 09 | . 07 | 1.04 | 2.62 | . 79 | . 00 | 10.28 |
| 10.1-89.5 | 27 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 8 | 5 | 3 | 3 | 17 | 29 | 10 | 0 | 106 |
| (1) | . 63 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 19 | . 12 | . 07 | . 07 | . 39 | . 67 | . 23 | . 00 | 2.45 |
| (2) | . 63 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 19 | . 12 | . 07 | . 07 | . 39 | . 67 | . 23 | . 00 | 2.45 |
| ALL SPEEDS | 407 | 263 | 114 | 92 | 77 | 67 | 102 | 206 | 186 | 343 | 454 | 234 | 212 | 423 | 702 | 438 | 0 | 4320 |
| (1) | 9.42 | 6.09 | 2.64 | 2.13 | 1.78 | 1.55 | 2.36 | 4.77 | 4.31 | 7.94 | 10.51 | 5.42 | 4.91 | 9.79 | 16.25 | 10.14 | . 00 | 100.00 |
| (2) | 9.42 | 6.09 | 2.64 | 2.13 | 1.78 | 1.55 | 2.36 | 4.77 | 4.31 | 7.94 | 10.51 | 5.42 | 4.91 | 9.79 | 16.25 | 10.14 | . 00 | 100.00 |

## Table 2.3-31—\{CCNPP 197 ft ( 60 m) February JFD (2000-2005)\}

## (Page 1 of 8)

CC FEBRUARY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS A CLASS FREQUENCY (PERCENT) = 10.15

| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 1.1-1.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 1.6-2.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 2 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 24 | . 00 | . 00 | . 00 | . 00 | . 24 | . 00 | . 49 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 05 |
| 2.1-3.0 | 3 | 4 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 1 | 3 | 3 | 0 | 0 | 1 | 0 | 0 | 20 |
| (1) | . 73 | . 98 | . 00 | . 24 | . 98 | . 00 | . 00 | . 00 | . 00 | . 24 | . 73 | . 73 | . 00 | . 00 | . 24 | . 00 | . 00 | 4.88 |
| (2) | . 07 | . 10 | . 00 | . 02 | . 10 | . 00 | . 00 | . 00 | . 00 | . 02 | . 07 | . 07 | . 00 | . 00 | . 02 | . 00 | . 00 | . 50 |
| 3.1-4.0 | 8 | 6 | 1 | 0 | 0 | 1 | 1 | 3 | 3 | 5 | 8 | 10 | 5 | 3 | 2 | 1 | 0 | 57 |
| (1) | 1.95 | 1.46 | . 24 | . 00 | . 00 | . 24 | . 24 | . 73 | . 73 | 1.22 | 1.95 | 2.44 | 1.22 | . 73 | . 49 | . 24 | . 00 | 13.90 |
| (2) | . 20 | . 15 | . 02 | . 00 | . 00 | . 02 | . 02 | . 07 | . 07 | . 12 | . 20 | . 25 | . 12 | . 07 | . 05 | . 02 | . 00 | 1.41 |
| 4.1-5.0 | 14 | 13 | 0 | 0 | 0 | 0 | 3 | 3 | 4 | 8 | 8 | 11 | 9 | 5 | 4 | 3 | 0 | 85 |
| (1) | 3.41 | 3.17 | . 00 | . 00 | . 00 | . 00 | . 73 | . 73 | . 98 | 1.95 | 1.95 | 2.68 | 2.20 | 1.22 | . 98 | . 73 | . 00 | 20.73 |
| (2) | . 35 | . 32 | . 00 | . 00 | . 00 | . 00 | . 07 | . 07 | . 10 | . 20 | . 20 | . 27 | . 22 | . 12 | . 10 | . 07 | . 00 | 2.10 |
| 5.1-6.0 | 8 | 8 | 1 | 0 | 0 | 0 | 0 | 6 | 1 | 6 | 12 | 6 | 4 | 6 | 13 | 5 | 0 | 76 |
| (1) | 1.95 | 1.95 | . 24 | . 00 | . 00 | . 00 | . 00 | 1.46 | . 24 | 1.46 | 2.93 | 1.46 | . 98 | 1.46 | 3.17 | 1.22 | . 00 | 18.54 |
| (2) | . 20 | . 20 | . 02 | . 00 | . 00 | . 00 | . 00 | . 15 | . 02 | . 15 | . 30 | . 15 | . 10 | . 15 | . 32 | . 12 | . 00 | 1.88 |
| 6.1-8.0 | 18 | 5 | 1 | 0 | 0 | 0 | 2 | 3 | 1 | 12 | 11 | 4 | 5 | 20 | 20 | 5 | 0 | 107 |
| (1) | 4.39 | 1.22 | . 24 | . 00 | . 00 | . 00 | . 49 | . 73 | . 24 | 2.93 | 2.68 | . 98 | 1.22 | 4.88 | 4.88 | 1.22 | . 00 | 26.10 |
| (2) | . 45 | . 12 | . 02 | . 00 | . 00 | . 00 | . 05 | . 07 | . 02 | . 30 | . 27 | . 10 | . 12 | . 50 | . 50 | . 12 | . 00 | 2.65 |
| 8.1-10.0 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 7 | 0 | 1 | 10 | 14 | 1 | 0 | 46 |
| (1) | 1.22 | . 24 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.71 | 1.71 | . 00 | . 24 | 2.44 | 3.41 | . 24 | . 00 | 11.22 |
| (2) | . 12 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 17 | . 17 | . 00 | . 02 | . 25 | . 35 | . 02 | . 00 | 1.14 |
| 10.1-89.5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 4 | 8 | 2 | 0 | 17 |
| (1) | . 24 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 49 | . 00 | . 00 | . 00 | . 98 | 1.95 | . 49 | . 00 | 4.15 |
| (2) | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 00 | . 00 | . 10 | . 20 | . 05 | . 00 | . 42 |
| ALL SPEEDS | 57 | 37 | 3 | 1 | 4 | 1 | 6 | 15 | 9 | 41 | 50 | 34 | 24 | 48 | 62 | 18 | 0 | 410 |
| (1) | 13.90 | 9.02 | . 73 | . 24 | . 98 | . 24 | 1.46 | 3.66 | 2.20 | 10.00 | 12.20 | 8.29 | 5.85 | 11.71 | 15.12 | 4.39 | . 00 | 100.00 |
| (2) | 1.41 | . 92 | . 07 | . 02 | . 10 | . 02 | . 15 | . 37 | . 22 | 1.02 | 1.24 | . 84 | . 59 | 1.19 | 1.54 | . 45 | . 00 | 10.15 |

(1) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

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Table 2.3-31—\{CCNPP 197 ft (60 m) February JFD (2000-2005)\}

## Page 2 of 8 )

(1) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

| CC FEBRUARY MET DATA JOINT | FREQUENCY DISTRIBUTION | (60-METER TOWER) |  |
| :---: | :---: | :---: | :---: |
| 197.0 FT WIND DATA | STABILITY CLASS C | CLASS FREQUENCY | (PERCENT) $=3.94$ |


|  |  |  |  |  |  |  |  | IND DI | RECTIO | N FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 63 | . 00 | . 00 | . 00 | . 00 | . 00 | . 63 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| 1.1-1.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 1.6-2.0 | 1 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 6 |
| (1) | . 63 | . 00 | . 00 | 1.26 | . 63 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 63 | . 00 | . 63 | . 00 | . 00 | . 00 | 3.77 |
| (2) | . 02 | . 00 | . 00 | . 05 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 15 |
| 2.1-3.0 | 6 | 3 | 2 | 3 | 0 | 0 | 1 | 2 | 0 | 1 | 2 | 2 | 1 | 1 | 0 | 1 | 0 | 25 |
| (1) | 3.77 | 1.89 | 1.26 | 1.89 | . 00 | . 00 | . 63 | 1.26 | . 00 | . 63 | 1.26 | 1.26 | . 63 | . 63 | . 00 | . 63 | . 00 | 15.72 |
| (2) | . 15 | . 07 | . 05 | . 07 | . 00 | . 00 | . 02 | . 05 | . 00 | . 02 | . 05 | . 05 | . 02 | . 02 | . 00 | . 02 | . 00 | . 62 |
| 3.1-4.0 | 3 | 9 | 4 | 1 | 1 | 0 | 0 | 3 | 1 | 1 | 2 | 3 | 1 | 2 | 0 | 3 | 0 | 34 |
| (1) | 1.89 | 5.66 | 2.52 | . 63 | . 63 | . 00 | . 00 | 1.89 | . 63 | . 63 | 1.26 | 1.89 | . 63 | 1.26 | . 00 | 1.89 | . 00 | 21.38 |
| (2) | . 07 | . 22 | . 10 | . 02 | . 02 | . 00 | . 00 | . 07 | . 02 | . 02 | . 05 | . 07 | . 02 | . 05 | . 00 | . 07 | . 00 | . 84 |
| 4.1-5.0 | 6 | 5 | 2 | 0 | 0 | 0 | 3 | 3 | 0 | 5 | 4 | 3 | 2 | 1 | 1 | 1 | 0 | 36 |
| (1) | 3.77 | 3.14 | 1.26 | . 00 | . 00 | . 00 | 1.89 | 1.89 | . 00 | 3.14 | 2.52 | 1.89 | 1.26 | . 63 | . 63 | . 63 | . 00 | 22.64 |
| (2) | . 15 | . 12 | . 05 | . 00 | . 00 | . 00 | . 07 | . 07 | . 00 | . 12 | . 10 | . 07 | . 05 | . 02 | . 02 | . 02 | . 00 | . 89 |
| 5.1-6.0 | 4 | 4 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 2 | 2 | 0 | 1 | 3 | 0 | 0 | 18 |
| (1) | 2.52 | 2.52 | . 00 | . 00 | . 00 | . 00 | . 63 | . 00 | . 00 | . 63 | 1.26 | 1.26 | . 00 | . 63 | 1.89 | . 00 | . 00 | 11.32 |
| (2) | . 10 | . 10 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 05 | . 05 | . 00 | . 02 | . 07 | . 00 | . 00 | . 45 |
| 6.1-8.0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 2 | 2 | 0 | 2 | 3 | 7 | 0 | 26 |
| (1) | 2.52 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 63 | 3.14 | 1.26 | 1.26 | . 00 | 1.26 | 1.89 | 4.40 | . 00 | 16.35 |
| (2) | . 10 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 12 | . 05 | . 05 | . 00 | . 05 | . 07 | . 17 | . 00 | . 64 |
| 8.1-10.0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 4 | 2 | 0 | 0 | 11 |
| (1) | . 63 | . 63 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 63 | . 63 | . 00 | . 63 | 2.52 | 1.26 | . 00 | . 00 | 6.92 |
| (2) | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 02 | . 10 | . 05 | . 00 | . 00 | . 27 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 63 | . 00 | . 00 | . 00 | . 00 | . 63 | . 00 | . 00 | 1.26 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 05 |
| ALL SPEEDS | 25 | 22 | 8 | 6 | 2 | 0 | 5 | 8 | 2 | 15 | 13 | 14 | 5 | 12 | 10 | 12 | 0 | 159 |
| (1) | 15.72 | 13.84 | 5.03 | 3.77 | 1.26 | . 00 | 3.14 | 5.03 | 1.26 | 9.43 | 8.18 | 8.81 | 3.14 | 7.55 | 6.29 | 7.55 | . 00 | 100.00 |
| (2) | . 62 | . 54 | . 20 | . 15 | . 05 | . 00 | . 12 | . 20 | . 05 | . 37 | . 32 | . 35 | . 12 | . 30 | . 25 | . 30 | . 00 | 3.94 |

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CC FEBRUARY MET DATA JOINT FREQUENCY DISTRIBUTION（60－METER TOWER）
197．0 FT WIND DATA STABILITY CLASS D CLASS FREQUENCY（PERCENT）＝ 34.93


## 

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CC FEBRUARY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS E CLASS FREQUENCY (PERCENT) = 32.19

| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 08 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 08 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 7 |
| (1) | . 00 | . 00 | . 08 | . 00 | . 00 | . 08 | . 08 | . 00 | . 00 | . 15 | . 00 | . 00 | . 00 | . 08 | . 00 | . 08 | . 00 | . 54 |
| (2) | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 05 | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 17 |
| 1.1-1.5 | 1 | 3 | 1 | 0 | 3 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 3 | 0 | 1 | 0 | 14 |
| (1) | . 08 | . 23 | . 08 | . 00 | . 23 | . 00 | . 08 | . 00 | . 08 | . 00 | . 00 | . 00 | . 00 | . 23 | . 00 | . 08 | . 00 | 1.08 |
| (2) | . 02 | . 07 | . 02 | . 00 | . 07 | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 07 | . 00 | . 02 | . 00 | . 35 |
| 1.6-2.0 | 1 | 3 | 6 | 9 | 6 | 2 | 2 | 2 | 1 | 0 | 1 | 2 | 4 | 0 | 0 | 0 | 0 | 39 |
| (1) | . 08 | . 23 | . 46 | . 69 | . 46 | . 15 | . 15 | . 15 | . 08 | . 00 | . 08 | . 15 | . 31 | . 00 | . 00 | . 00 | . 00 | 3.00 |
| (2) | . 02 | . 07 | . 15 | . 22 | . 15 | . 05 | . 05 | . 05 | . 02 | . 00 | . 02 | . 05 | . 10 | . 00 | . 00 | . 00 | . 00 | . 97 |
| 2.1-3.0 | 8 | 8 | 10 | 13 | 14 | 6 | 5 | 8 | 5 | 2 | 3 | 4 | 5 | 6 | 9 | 9 | 0 | 115 |
| (1) | . 62 | . 62 | . 77 | 1.00 | 1.08 | . 46 | . 38 | . 62 | . 38 | . 15 | . 23 | . 31 | . 38 | . 46 | . 69 | . 69 | . 00 | 8.85 |
| (2) | . 20 | . 20 | . 25 | . 32 | . 35 | . 15 | . 12 | . 20 | . 12 | . 05 | . 07 | . 10 | . 12 | . 15 | . 22 | . 22 | . 00 | 2.85 |
| 3.1-4.0 | 20 | 20 | 8 | 11 | 13 | 7 | 10 | 16 | 14 | 10 | 10 | 11 | 5 | 13 | 11 | 28 | 0 | 207 |
| (1) | 1.54 | 1.54 | . 62 | . 85 | 1.00 | . 54 | . 77 | 1.23 | 1.08 | . 77 | . 77 | . 85 | . 38 | 1.00 | . 85 | 2.15 | . 00 | 15.92 |
| (2) | . 50 | . 50 | . 20 | . 27 | . 32 | . 17 | . 25 | . 40 | . 35 | . 25 | . 25 | . 27 | . 12 | . 32 | . 27 | . 69 | . 00 | 5.13 |
| 4.1-5.0 | 35 | 11 | 11 | 6 | 2 | 8 | 6 | 15 | 24 | 8 | 8 | 12 | 9 | 23 | 40 | 30 | 0 | 248 |
| (1) | 2.69 | . 85 | . 85 | . 46 | . 15 | . 62 | . 46 | 1.15 | 1.85 | . 62 | . 62 | . 92 | . 69 | 1.77 | 3.08 | 2.31 | . 00 | 19.08 |
| (2) | . 87 | . 27 | . 27 | . 15 | . 05 | . 20 | . 15 | . 37 | . 59 | . 20 | . 20 | . 30 | . 22 | . 57 | . 99 | . 74 | . 00 | 6.14 |
| 5.1-6.0 | 22 | 12 | 3 | 1 | 1 | 3 | 5 | 27 | 28 | 24 | 20 | 24 | 7 | 26 | 49 | 29 | 0 | 281 |
| (1) | 1.69 | . 92 | . 23 | . 08 | . 08 | . 23 | . 38 | 2.08 | 2.15 | 1.85 | 1.54 | 1.85 | . 54 | 2.00 | 3.77 | 2.23 | . 00 | 21.62 |
| (2) | . 54 | . 30 | . 07 | . 02 | . 02 | . 07 | . 12 | . 67 | . 69 | . 59 | . 50 | . 59 | . 17 | . 64 | 1.21 | . 72 | . 00 | 6.96 |
| 6.1-8.0 | 22 | 14 | 2 | 0 | 0 | 0 | 1 | 21 | 39 | 55 | 37 | 17 | 14 | 24 | 22 | 25 | 0 | 293 |
| (1) | 1.69 | 1.08 | . 15 | . 00 | . 00 | . 00 | . 08 | 1.62 | 3.00 | 4.23 | 2.85 | 1.31 | 1.08 | 1.85 | 1.69 | 1.92 | . 00 | 22.54 |
| (2) | . 54 | . 35 | . 05 | . 00 | . 00 | . 00 | . 02 | . 52 | . 97 | 1.36 | . 92 | . 42 | . 35 | . 59 | . 54 | . 62 | . 00 | 7.25 |
| 8.1-10.0 | 12 | 1 | 0 | 0 | 0 | 0 | 1 | 9 | 6 | 19 | 15 | 1 | 2 | 6 | 2 | 8 | 0 | 82 |
| (1) | . 92 | . 08 | . 00 | . 00 | . 00 | . 00 | . 08 | . 69 | . 46 | 1.46 | 1.15 | . 08 | . 15 | . 46 | . 15 | . 62 | . 00 | 6.31 |
| (2) | . 30 | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 | . 22 | . 15 | . 47 | . 37 | . 02 | . 05 | . 15 | . 05 | . 20 | . 00 | 2.03 |
| 10.1-89.5 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 4 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 13 |
| (1) | . 08 | . 00 | . 08 | . 00 | . 00 | . 00 | . 00 | . 00 | . 15 | . 31 | . 38 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.00 |
| (2) | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 10 | . 12 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 32 |
| ALL SPEEDS | 122 | 72 | 43 | 40 | 39 | 27 | 32 | 98 | 120 | 125 | 99 | 71 | 46 | 102 | 133 | 131 | 0 | 1300 |
| (1) | 9.38 | 5.54 | 3.31 | 3.08 | 3.00 | 2.08 | 2.46 | 7.54 | 9.23 | 9.62 | 7.62 | 5.46 | 3.54 | 7.85 | 10.23 | 10.08 | . 00 | 100.00 |
| (2) | 3.02 | 1.78 | 1.06 | . 99 | . 97 | . 67 | . 79 | 2.43 | 2.97 | 3.09 | 2.45 | 1.76 | 1.14 | 2.53 | 3.29 | 3.24 | . 00 | 32.19 |
| (1) = PERCENT | F ALI | GOOD | OBSERV | ATIONS | FOR | HIS PA |  |  |  |  |  |  |  |  |  |  |  |  |

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\begin{array}{lll}
\text { CC FEBRUARY MET DATA JOINT FREQUENCY DISTRIBUTION } & (60-M E T E R ~ T O W E R) \\
197.0 ~ F T ~ W I N D ~ D A T A ~ & \text { STABILITY CLASS F } & \text { CLASS FREQUENCY }
\end{array}
$$


(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
CC FEBRUARY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS G CLASS FREQUENCY (PERCENT) = 3.89

| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTA |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 0 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 0 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| (1) | . 00 | . 00 | . 00 | . 00 | . 64 | . 00 | . 00 | . 00 | . 00 | . 64 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.2 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 |
| .5-1.0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| (1) | . 00 | . 64 | . 00 | . 00 | . 64 | . 00 | . 00 | . 64 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.91 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . |
| 1.1-1.5 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |  |
| (1) | . 00 | . 00 | . 00 | . 64 | . 64 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.27 | . 00 | . 64 | . 00 | . 00 | . 00 | . 00 | 3.1 |
| (2) | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 1 |
| 1.6-2.0 | 0 | 0 | 0 | 1 | 2 | 1 | 0 | 0 | 1 | 1 | 1 | 0 | 3 | 0 | 2 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 64 | 1.27 | . 64 | . 00 | . 00 | . 64 | . 64 | . 64 | . 00 | 1.91 | . 00 | 1.27 | . 00 | . 00 | 7.6 |
| (2) | . 00 | . 00 | . 00 | . 02 | . 05 | . 02 | . 00 | . 00 | . 02 | . 02 | . 02 | . 00 | . 07 | . 00 | . 05 | . 00 | . 00 | . 3 |
| 2.1-3.0 | 1 | 0 | 3 | 0 | 1 | 0 | 2 | 0 | 3 | 5 | 3 | 3 | 1 | 3 | 0 | 0 | 0 | 2 |
| (1) | . 64 | . 00 | 1.91 | . 00 | . 64 | . 00 | 1.27 | . 00 | 1.91 | 3.18 | 1.91 | 1.91 | . 64 | 1.91 | . 00 | . 00 | . 00 | 15.92 |
| (2) | . 02 | . 00 | . 07 | . 00 | . 02 | . 00 | . 05 | . 00 | . 07 | . 12 | . 07 | . 07 | . 02 | . 07 | . 00 | . 00 | . 00 | . 6 |
| 3.1-4.0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 4 | 4 | 1 | 2 | 4 | 2 | 1 | 2 | 3 | 0 | 2 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 64 | . 64 | 1.27 | 2.55 | 2.55 | . 64 | 1.27 | 2.55 | 1.27 | . 64 | 1.27 | 1.91 | . 00 | 17.20 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 05 | . 10 | . 10 | . 02 | . 05 | . 10 | . 05 | . 02 | . 05 | . 07 | . 00 | . 6 |
| 4.1-5.0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 3 | 4 | 5 | 5 | 1 | 3 | 3 | 0 | 0 | 0 | 25 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 64 | . 00 | 1.91 | 2.55 | 3.18 | 3.18 | . 64 | 1.91 | 1.91 | . 00 | . 00 | . 00 | 15.92 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 07 | . 10 | . 12 | . 12 | . 02 | . 07 | . 07 | . 00 | . 00 | . 00 | . 6 |
| 5.1-6.0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 7 | 4 | 3 | 1 | 4 | 0 | 1 | 1 | 0 | 0 | 2 |
| (1) | . 00 | . 64 | . 00 | . 00 | . 00 | . 64 | . 00 | 4.46 | 2.55 | 1.91 | . 64 | 2.55 | . 00 | . 64 | . 64 | . 00 | . 00 | 14.65 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 00 | . 02 | . 00 | . 17 | . 10 | . 07 | . 02 | . 10 | . 00 | . 02 | . 02 | . 00 | . 00 | . 5 |
| 6.1-8.0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 2 | 4 | 6 | 8 | 8 | 1 | 2 | 1 | 0 | 0 | 3 |
| (1) | . 00 | 1.27 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.27 | 2.55 | 3.82 | 5.10 | 5.10 | . 64 | 1.27 | . 64 | . 00 | . 00 | 21.6 |
| (2) | . 00 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 10 | . 15 | . 20 | . 20 | . 02 | . 05 | . 02 | . 00 | . 00 | . 8 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 |  |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 64 | . 00 | . 00 | . 00 | . 00 | . 00 | . 6 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 0 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 0 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 0 |
| ALL SPEEDS | 1 | 4 | 3 | 2 | 7 | 4 | 4 | 17 | 20 | 22 | 22 | 21 | 11 | 10 | 6 | 3 | 0 | 15 |
| (1) | . 64 | 2.55 | 1.91 | 1.27 | 4.46 | 2.55 | 2.55 | 10.83 | 12.74 | 14.01 | 14.01 | 13.38 | 7.01 | 6.37 | 3.82 | 1.91 | . 00 | 100.0 |
| (2) | . 02 | . 10 | . 07 | . 05 | . 17 | . 10 | . 10 | . 42 | . 50 | . 54 | . 54 | . 52 | . 27 | . 25 | . 15 | . 07 | . 00 | 3.8 |

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
GヨレכヨıOyd $\perp H פ ו y \wedge d O כ$

CC FEBRUARY MET DATA JOINT FREQUENCY DISTRIBUTION（60－METER TOWER）
197．0 FT WIND DATA STABILITY CLASS ALL CLASS FREQUENCY（PERCENT）＝ 100.00

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { SPEED } \\ & \text { mps } \end{aligned}$ | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| LT ． 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 |
| ． $2-.4$ | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 05 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 07 |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 05 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 07 |
| ．5－1．0 | 1 | 3 | 3 | 3 | 2 | 3 | 4 | 5 | 1 | 5 | 1 | 1 | 0 | 1 | 0 | 4 | 0 | 37 |
| （1） | ． 02 | ． 07 | ． 07 | ． 07 | ． 05 | ． 07 | ． 10 | ． 12 | ． 02 | ． 12 | ． 02 | ． 02 | ． 00 | ． 02 | ． 00 | ． 10 | ． 00 | ． 92 |
| （2） | ． 02 | ． 07 | ． 07 | ． 07 | ． 05 | ． 07 | ． 10 | ． 12 | ． 02 | ． 12 | ． 02 | ． 02 | ． 00 | ． 02 | ． 00 | ． 10 | ． 00 | ． 92 |
| 1．1－1．5 | 3 | 3 | 3 | 5 | 8 | 2 | 1 | 2 | 4 | 2 | 3 | 0 | 2 | 4 | 2 | 5 | 0 | 49 |
| （1） | ． 07 | ． 07 | ． 07 | ． 12 | ． 20 | ． 05 | ． 02 | ． 05 | ． 10 | ． 05 | ． 07 | ． 00 | ． 05 | ． 10 | ． 05 | ． 12 | ． 00 | 1.21 |
| （2） | ． 07 | ． 07 | ． 07 | ． 12 | ． 20 | ． 05 | ． 02 | ． 05 | ． 10 | ． 05 | ． 07 | ． 00 | ． 05 | ． 10 | ． 05 | ． 12 | ． 00 | 1.21 |
| 1．6－2．0 | 8 | 14 | 11 | 18 | 19 | 5 | 5 | 5 | 8 | 2 | 7 | 4 | 8 | 3 | 4 | 5 | 0 | 126 |
| （1） | ． 20 | ． 35 | ． 27 | ． 45 | ． 47 | ． 12 | ． 12 | ． 12 | ． 20 | ． 05 | ． 17 | ． 10 | ． 20 | ． 07 | ． 10 | ． 12 | ． 00 | 3.12 |
| （2） | ． 20 | ． 35 | ． 27 | ． 45 | ． 47 | ． 12 | ． 12 | ． 12 | ． 20 | ． 05 | ． 17 | ． 10 | ． 20 | ． 07 | ． 10 | ． 12 | ． 00 | 3.12 |
| 2．1－3．0 | 47 | 37 | 37 | 41 | 35 | 16 | 28 | 31 | 19 | 15 | 15 | 22 | 11 | 16 | 20 | 27 | 0 | 417 |
| （1） | 1.16 | ． 92 | ． 92 | 1.02 | ． 87 | ． 40 | ． 69 | ． 77 | ． 47 | ． 37 | ． 37 | ． 54 | ． 27 | ． 40 | ． 50 | ． 67 | ． 00 | 10.32 |
| （2） | 1.16 | ． 92 | ． 92 | 1.02 | ． 87 | ． 40 | ． 69 | ． 77 | ． 47 | ． 37 | ． 37 | ． 54 | ． 27 | ． 40 | ． 50 | ． 67 | ． 00 | 10.32 |
| 3．1－4．0 | 57 | 67 | 26 | 34 | 27 | 17 | 30 | 57 | 40 | 24 | 42 | 45 | 25 | 27 | 31 | 52 | 0 | 601 |
| （1） | 1.41 | 1.66 | ． 64 | ． 84 | ． 67 | ． 42 | ． 74 | 1.41 | ． 99 | ． 59 | 1.04 | 1.11 | ． 62 | ． 67 | ． 77 | 1.29 | ． 00 | 14.88 |
| （2） | 1.41 | 1.66 | ． 64 | ． 84 | ． 67 | ． 42 | ． 74 | 1.41 | ． 99 | ． 59 | 1.04 | 1.11 | ． 62 | ． 67 | ． 77 | 1.29 | ． 00 | 14.88 |
| 4．1－5．0 | 86 | 52 | 40 | 17 | 7 | 14 | 29 | 53 | 53 | 45 | 39 | 55 | 34 | 47 | 64 | 69 | 0 | 704 |
| （1） | 2.13 | 1.29 | ． 99 | ． 42 | ． 17 | ． 35 | ． 72 | 1.31 | 1.31 | 1.11 | ． 97 | 1.36 | ． 84 | 1.16 | 1.58 | 1.71 | ． 00 | 17.43 |
| （2） | 2.13 | 1.29 | ． 99 | ． 42 | ． 17 | ． 35 | ． 72 | 1.31 | 1.31 | 1.11 | ． 97 | 1.36 | ． 84 | 1.16 | 1.58 | 1.71 | ． 00 | 17.43 |
| 5．1－6．0 | 72 | 55 | 19 | 10 | 1 | 7 | 16 | 63 | 52 | 59 | 56 | 56 | 27 | 53 | 95 | 69 | 0 | 710 |
| （1） | 1.78 | 1.36 | ． 47 | ． 25 | ． 02 | ． 17 | ． 40 | 1.56 | 1.29 | 1.46 | 1.39 | 1.39 | ． 67 | 1.31 | 2.35 | 1.71 | ． 00 | 17.58 |
| （2） | 1.78 | 1.36 | ． 47 | ． 25 | ． 02 | ． 17 | ． 40 | 1.56 | 1.29 | 1.46 | 1.39 | 1.39 | ． 67 | 1.31 | 2.35 | 1.71 | ． 00 | 17.58 |
| 6．1－8．0 | 110 | 78 | 31 | 5 | 3 | 2 | 6 | 49 | 65 | 109 | 91 | 55 | 39 | 77 | 121 | 88 | 0 | 929 |
| （1） | 2.72 | 1.93 | ． 77 | ． 12 | ． 07 | ． 05 | ． 15 | 1.21 | 1.61 | 2.70 | 2.25 | 1.36 | ． 97 | 1.91 | 3.00 | 2.18 | ． 00 | 23.00 |
| （2） | 2.72 | 1.93 | ． 77 | ． 12 | ． 07 | ． 05 | ． 15 | 1.21 | 1.61 | 2.70 | 2.25 | 1.36 | ． 97 | 1.91 | 3.00 | 2.18 | ． 00 | 23.00 |
| 8．1－10．0 | 63 | 34 | 11 | 0 | 0 | 1 | 3 | 11 | 7 | 39 | 41 | 6 | 5 | 38 | 58 | 30 | 0 | 347 |
| （1） | 1.56 | ． 84 | ． 27 | ． 00 | ． 00 | ． 02 | ． 07 | ． 27 | ． 17 | ． 97 | 1.02 | ． 15 | ． 12 | ． 94 | 1.44 | ． 74 | ． 00 | 8.59 |
| （2） | 1.56 | ． 84 | ． 27 | ． 00 | ． 00 | ． 02 | ． 07 | ． 27 | ． 17 | ． 97 | 1.02 | ． 15 | ． 12 | ． 94 | 1.44 | ． 74 | ． 00 | 8.59 |
| 10．1－89．5 | 8 | 31 | 8 | 0 | 0 | 0 | 0 | 0 | 2 | 14 | 12 | 0 | 0 | 11 | 24 | 5 | 0 | 115 |
| （1） | ． 20 | ． 77 | ． 20 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 05 | ． 35 | ． 30 | ． 00 | ． 00 | ． 27 | ． 59 | ． 12 | ． 00 | 2.85 |
| （2） | ． 20 | ． 77 | ． 20 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 05 | ． 35 | ． 30 | ． 00 | ． 00 | ． 27 | ． 59 | ． 12 | ． 00 | 2.85 |
| ALL SPEEDS | 455 | 374 | 189 | 133 | 104 | 67 | 122 | 276 | 251 | 316 | 307 | 244 | 151 | 277 | 419 | 354 | 0 | 4039 |
| （1） | 11.27 | 9.26 | 4.68 | 3.29 | 2.57 | 1.66 | 3.02 | 6.83 | 6.21 | 7.82 | 7.60 | 6.04 | 3.74 | 6.86 | 10.37 | 8.76 | ． 00 | 100.00 |
| （2） | 11.27 | 9.26 | 4.68 | 3.29 | 2.57 | 1.66 | 3.02 | 6.83 | 6.21 | 7.82 | 7.60 | 6.04 | 3.74 | 6.86 | 10.37 | 8.76 | ． 00 | 100.00 |

Table 2.3-32—\{CCNPP 197 ft ( 60 m ) March JFD (2000-2005)\}
(Page 1 of 8)
CC MARCH MET DATA JOINT FREQUENCY DISTRIBUTION ( 60 -METER TOWER)
197.0 FT WIND DATA STABILITY CLASS A CLASS FREQUENCY (PERCENT) = 12.40

|  | WIND DIRECTION FROM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 1.1-1.5 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 19 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 19 |
| (2) | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| 1.6-2.0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 3 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 38 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 19 | . 00 | . 00 | . 00 | . 00 | . 00 | . 56 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 |
| 2.1-3.0 | 2 | 3 | 3 | 0 | 1 | 1 | 0 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 |
| (1) | . 38 | . 56 | . 56 | . 00 | . 19 | . 19 | . 00 | . 38 | . 19 | . 19 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 2.63 |
| (2) | . 05 | . 07 | . 07 | . 00 | . 02 | . 02 | . 00 | . 05 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 33 |
| 3.1-4.0 | 5 | 15 | 6 | 2 | 5 | 2 | 4 | 4 | 2 | 3 | 5 | 5 | 2 | 0 | 1 | 1 | 0 | 62 |
| (1) | . 94 | 2.81 | 1.13 | . 38 | . 94 | . 38 | . 75 | . 75 | . 38 | . 56 | . 94 | . 94 | . 38 | . 00 | . 19 | . 19 | . 00 | 11.63 |
| (2) | . 12 | . 35 | . 14 | . 05 | . 12 | . 05 | . 09 | . 09 | . 05 | . 07 | . 12 | . 12 | . 05 | . 00 | . 02 | . 02 | . 00 | 1.44 |
| 4.1-5.0 | 21 | 9 | 1 | 0 | 4 | 5 | 1 | 10 | 2 | 8 | 12 | 5 | 4 | 2 | 5 | 2 | 0 | 91 |
| (1) | 3.94 | 1.69 | . 19 | . 00 | . 75 | . 94 | . 19 | 1.88 | . 38 | 1.50 | 2.25 | . 94 | . 75 | . 38 | . 94 | . 38 | . 00 | 17.07 |
| (2) | . 49 | . 21 | . 02 | . 00 | . 09 | . 12 | . 02 | . 23 | . 05 | . 19 | . 28 | . 12 | . 09 | . 05 | . 12 | . 05 | . 00 | 2.12 |
| 5.1-6.0 | 8 | 3 | 1 | 0 | 1 | 1 | 4 | 15 | 3 | 7 | 21 | 6 | 6 | 9 | 14 | 7 | 0 | 106 |
| (1) | 1.50 | . 56 | . 19 | . 00 | . 19 | . 19 | . 75 | 2.81 | . 56 | 1.31 | 3.94 | 1.13 | 1.13 | 1.69 | 2.63 | 1.31 | . 00 | 19.89 |
| (2) | . 19 | . 07 | . 02 | . 00 | . 02 | . 02 | . 09 | . 35 | . 07 | . 16 | . 49 | . 14 | . 14 | . 21 | . 33 | . 16 | . 00 | 2.47 |
| 6.1-8.0 | 12 | 4 | 1 | 0 | 2 | 0 | 4 | 15 | 2 | 17 | 28 | 11 | 11 | 26 | 31 | 8 | 0 | 172 |
| (1) | 2.25 | . 75 | . 19 | . 00 | . 38 | . 00 | . 75 | 2.81 | . 38 | 3.19 | 5.25 | 2.06 | 2.06 | 4.88 | 5.82 | 1.50 | . 00 | 32.27 |
| (2) | . 28 | . 09 | . 02 | . 00 | . 05 | . 00 | . 09 | . 35 | . 05 | . 40 | . 65 | . 26 | . 26 | . 60 | . 72 | . 19 | . 00 | 4.00 |
| 8.1-10.0 | 1 | 0 | 1 | 0 | 0 | 0 | 2 | 4 | 0 | 3 | 10 | 3 | 0 | 27 | 16 | 2 | 0 | 69 |
| (1) | . 19 | . 00 | . 19 | . 00 | . 00 | . 00 | . 38 | . 75 | . 00 | . 56 | 1.88 | . 56 | . 00 | 5.07 | 3.00 | . 38 | . 00 | 12.95 |
| (2) | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 05 | . 09 | . 00 | . 07 | . 23 | . 07 | . 00 | . 63 | . 37 | . 05 | . 00 | 1.60 |
| 10.1-89.5 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 2 | 3 | 5 | 1 | 0 | 15 |
| (1) | . 00 | . 00 | . 19 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 19 | . 38 | . 38 | . 56 | . 94 | . 19 | . 00 | 2.81 |
| (2) | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 05 | . 05 | . 07 | . 12 | . 02 | . 00 | . 35 |
| ALL SPEEDS | 49 | 34 | 14 | 3 | 15 | 9 | 15 | 50 | 10 | 39 | 77 | 33 | 25 | 67 | 72 | 21 | 0 | 533 |
| (1) | 9.19 | 6.38 | 2.63 | . 56 | 2.81 | 1.69 | 2.81 | 9.38 | 1.88 | 7.32 | 14.45 | 6.19 | 4.69 | 12.57 | 13.51 | 3.94 | . 00 | 100.00 |
| (2) | 1.14 | . 79 | . 33 | . 07 | . 35 | . 21 | . 35 | 1.16 | . 23 | . 91 | 1.79 | . 77 | . 58 | 1.56 | 1.67 | . 49 | . 00 | 12.40 |

(1) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOod ObSERVAtions for this period
CC MARCH MET DATA JOINT FREQUENCY DISTRIBUTION（60－METER TOWER）
197．0 FT WIND DATA STABILITY CLASS B CLASS FREQUENCY（PERCENT）＝ 3.44

（1）＝PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
（2）＝PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

CC MARCH MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS C CLASS FREQUENCY (PERCENT) = 4.21

|  |  |  |  |  |  |  |  | IND DI | RECTI | N FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 1.1-1.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 55 | . 00 | . 00 | . 00 | . 00 | . 00 | . 55 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| 1.6-2.0 | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 6 |
| (1) | . 00 | 1.10 | . 00 | . 00 | . 00 | . 55 | . 00 | . 00 | . 00 | . 00 | 1.10 | . 00 | . 00 | . 55 | . 00 | . 00 | . 00 | 3.31 |
| (2) | . 00 | . 05 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 14 |
| 2.1-3.0 | 5 | 4 | 7 | 3 | 3 | 2 | 1 | 0 | 1 | 1 | 1 | 2 | 1 | 1 | 0 | 0 | 0 | 32 |
| (1) | 2.76 | 2.21 | 3.87 | 1.66 | 1.66 | 1.10 | . 55 | . 00 | . 55 | . 55 | . 55 | 1.10 | . 55 | . 55 | . 00 | . 00 | . 00 | 17.68 |
| (2) | . 12 | . 09 | . 16 | . 07 | . 07 | . 05 | . 02 | . 00 | . 02 | . 02 | . 02 | . 05 | . 02 | . 02 | . 00 | . 00 | . 00 | . 74 |
| $3.1-4.0$ | 5 | 3 | 4 | 1 | 2 | 2 | 1 | 2 | 3 | 2 | 1 | 2 | 2 | 0 | 1 | 3 | 0 | 34 |
| (1) | 2.76 | 1.66 | 2.21 | . 55 | 1.10 | 1.10 | . 55 | 1.10 | 1.66 | 1.10 | . 55 | 1.10 | 1.10 | . 00 | . 55 | 1.66 | . 00 | 18.78 |
| (2) | . 12 | . 07 | . 09 | . 02 | . 05 | . 05 | . 02 | . 05 | . 07 | . 05 | . 02 | . 05 | . 05 | . 00 | . 02 | . 07 | . 00 | . 79 |
| 4.1-5.0 | 5 | 1 | 1 | 0 | 0 | 2 | 1 | 6 | 2 | 3 | 2 | 1 | 0 | 1 | 1 | 4 | 0 | 30 |
| (1) | 2.76 | . 55 | . 55 | . 00 | . 00 | 1.10 | . 55 | 3.31 | 1.10 | 1.66 | 1.10 | . 55 | . 00 | . 55 | . 55 | 2.21 | . 00 | 16.57 |
| (2) | . 12 | . 02 | . 02 | . 00 | . 00 | . 05 | . 02 | . 14 | . 05 | . 07 | . 05 | . 02 | . 00 | . 02 | . 02 | . 09 | . 00 | . 70 |
| 5.1-6.0 | 1 | 3 | 0 | 1 | 0 | 0 | 1 | 3 | 0 | 1 | 1 | 5 | 1 | 2 | 2 | 1 | 0 | 22 |
| (1) | . 55 | 1.66 | . 00 | . 55 | . 00 | . 00 | . 55 | 1.66 | . 00 | . 55 | . 55 | 2.76 | . 55 | 1.10 | 1.10 | . 55 | . 00 | 12.15 |
| (2) | . 02 | . 07 | . 00 | . 02 | . 00 | . 00 | . 02 | . 07 | . 00 | . 02 | . 02 | . 12 | . 02 | . 05 | . 05 | . 02 | . 00 | . 51 |
| 6.1-8.0 | 2 | 1 | 2 | 0 | 0 | 0 | 1 | 6 | 1 | 1 | 1 | 0 | 3 | 1 | 7 | 4 | 0 | 30 |
| (1) | 1.10 | . 55 | 1.10 | . 00 | . 00 | . 00 | . 55 | 3.31 | . 55 | . 55 | . 55 | . 00 | 1.66 | . 55 | 3.87 | 2.21 | . 00 | 16.57 |
| (2) | . 05 | . 02 | . 05 | . 00 | . 00 | . 00 | . 02 | . 14 | . 02 | . 02 | . 02 | . 00 | . 07 | . 02 | . 16 | . 09 | . 00 | . 70 |
| 8.1-10.0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 4 | 4 | 2 | 0 | 15 |
| (1) | . 00 | . 55 | . 55 | . 00 | . 00 | . 00 | . 00 | . 55 | . 00 | . 55 | . 55 | . 00 | . 00 | 2.21 | 2.21 | 1.10 | . 00 | 8.29 |
| (2) | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 02 | . 00 | . 00 | . 09 | . 09 | . 05 | . 00 | . 35 |
| 10.1-89.5 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 0 | 0 | 11 |
| (1) | 1.66 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 55 | 3.87 | . 00 | . 00 | 6.08 |
| (2) | . 07 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 16 | . 00 | . 00 | . 26 |
| ALL SPEEDS | 21 | 15 | 15 | 5 | 5 | 7 | 5 | 18 | 7 | 9 | 9 | 11 | 7 | 11 | 22 | 14 | 0 | 181 |
| (1) | 11.60 | 8.29 | 8.29 | 2.76 | 2.76 | 3.87 | 2.76 | 9.94 | 3.87 | 4.97 | 4.97 | 6.08 | 3.87 | 6.08 | 12.15 | 7.73 | . 00 | 100.00 |
| (2) | . 49 | . 35 | . 35 | . 12 | . 12 | . 16 | . 12 | . 42 | . 16 | . 21 | . 21 | . 26 | . 16 | . 26 | . 51 | . 33 | . 00 | 4.21 |

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

## IᄏIכ

Table 2.3-32—\{CCNPP 197 ft (60 m) March JFD (2000-2005) \}

CC MARCH MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS D CLASS FREQUENCY (PERCENT) = 37.65

| SPEED | N | NNE | NE | ENE | E | ESE | SE | D DIRECTION |  | FROMSSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  | SSE | S |  |  |  |  |  |  |  |  |  |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
|  | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| $\begin{array}{rr}.2- & .4 \\ (1) \\ \\ (2)\end{array}$ | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 2 |
|  | . 00 | . 06 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 06 | . 00 | . 00 | . 00 | . 12 |
|  | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 05 |
| . $5-1.0$ | 2 | 0 | 2 | 0 | 2 | 1 | 0 | 0 | 1 | 0 | 2 | 1 | 1 | 1 | 2 | 1 | 0 | 16 |
| (1) | . 12 | . 00 | . 12 | . 00 | . 12 | . 06 | . 00 | . 00 | . 06 | . 00 | . 12 | . 06 | . 06 | . 06 | . 12 | . 06 | . 00 | . 99 |
| $\begin{array}{r} (2) \\ 1.1-1.5 \end{array}$ | . 05 | . 00 | . 05 | . 00 | . 05 | . 02 | . 00 | . 00 | . 02 | . 00 | . 05 | . 02 | . 02 | . 02 | . 05 | . 02 | . 00 | . 37 |
|  | 4 | 1 | 1 | 3 | 2 | 2 | 1 | 1 | 1 | 0 | 1 | 4 | 2 | 0 | 0 | 0 | 0 | 23 |
| $\begin{array}{r} 1.1-1.5 \\ (1) \end{array}$ | . 25 | . 06 | . 06 | . 19 | . 12 | . 12 | . 06 | . 06 | . 06 | . 00 | . 06 | . 25 | . 12 | . 00 | . 00 | . 00 | . 00 | 1.42 |
| 1.6- 2.0 | . 09 | . 02 | . 02 | . 07 | . 05 | . 05 | . 02 | . 02 | . 02 | . 00 | . 02 | . 09 | . 05 | . 00 | . 00 | . 00 | . 00 | . 53 |
|  | 4 | 6 | 5 | 8 | 9 | 5 | 2 | 0 | 0 | 0 | 4 | 2 | 2 | 1 | 1 | 2 | 0 | 51 |
| 1.6-2.0 | . 25 | . 37 | . 31 | . 49 | . 56 | . 31 | . 12 | . 00 | . 00 | . 00 | . 25 | . 12 | . 12 | . 06 | . 06 | . 12 | . 00 | 3.15 |
| 2.1- 3.0 | . 09 | . 14 | . 12 | . 19 | . 21 | . 12 | . 05 | . 00 | . 00 | . 00 | . 09 | . 05 | . 05 | . 02 | . 02 | . 05 | . 00 | 1.19 |
|  | 18 | 28 | 18 | 24 | 19 | 9 | 15 | 11 | 9 | 9 | 6 | 6 | 2 | 2 | 9 | 6 | 0 | 191 |
| 2.1-3.0 | 1.11 | 1.73 | 1.11 | 1.48 | 1.17 | . 56 | . 93 | . 68 | . 56 | . 56 | . 37 | . 37 | . 12 | . 12 | . 56 | . 37 | . 00 | 11.80 |
| $\begin{array}{r} (2) \\ 3.1-4.0 \end{array}$ | . 42 | . 65 | . 42 | . 56 | . 44 | . 21 | . 35 | . 26 | . 21 | . 21 | . 14 | . 14 | . 05 | . 05 | . 21 | . 14 | . 00 | 4.44 |
|  | 26 | 30 | 19 | 19 | 14 | 19 | 15 | 23 | 11 | 4 | 9 | 6 | 3 | 3 | 3 | 16 | 0 | 220 |
| $3.1-4.0$ <br> (1) | 1.61 | 1.85 | 1.17 | 1.17 | . 86 | 1.17 | . 93 | 1.42 | . 68 | . 25 | . 56 | . 37 | . 19 | . 19 | . 19 | . 99 | . 00 | 13.59 |
| $\begin{array}{r} (2) \\ 4.1-5.0 \end{array}$ | . 60 | . 70 | . 44 | . 44 | . 33 | . 44 | . 35 | . 53 | . 26 | . 09 | . 21 | . 14 | . 07 | . 07 | . 07 | . 37 | . 00 | 5.12 |
|  | 15 | 15 | 12 | 25 | 19 | 11 | 18 | 31 | 6 | 9 | 3 | 9 | 2 | 5 | 12 | 18 | 0 | 210 |
| $\begin{array}{r} 4.1-5.0 \\ (1) \end{array}$ | . 93 | . 93 | . 74 | 1.54 | 1.17 | . 68 | 1.11 | 1.91 | . 37 | . 56 | . 19 | . 56 | . 12 | . 31 | . 74 | 1.11 | . 00 | 12.97 |
| 5.1-6.0 | . 35 | . 35 | . 28 | . 58 | . 44 | . 26 | . 42 | . 72 | . 14 | . 21 | . 07 | . 21 | . 05 | . 12 | . 28 | . 42 | . 00 | 4.88 |
|  | 23 | 5 | 11 | 23 | 8 | 4 | 19 | 20 | 9 | 6 | 4 | 6 | 6 | 14 | 19 | 18 | 0 | 195 |
| 5.1- 6.0 | 1.42 | . 31 | . 68 | 1.42 | . 49 | . 25 | 1.17 | 1.24 | . 56 | . 37 | . 25 | . 37 | . 37 | . 86 | 1.17 | 1.11 | . 00 | 12.04 |
| 6.1- $\begin{array}{r}\text { (2) } \\ 8.0\end{array}$ | . 53 | . 12 | . 26 | . 53 | . 19 | . 09 | . 44 | . 47 | . 21 | . 14 | . 09 | . 14 | . 14 | . 33 | . 44 | . 42 | . 00 | 4.53 |
|  | 43 | 24 | 29 | 28 | 5 | 1 | 11 | 35 | 7 | 12 | 23 | 10 | 5 | 22 | 64 | 52 | 0 | 371 |
| (1) | 2.66 | 1.48 | 1.79 | 1.73 | . 31 | . 06 | . 68 | 2.16 | . 43 | . 74 | 1.42 | . 62 | . 31 | 1.36 | 3.95 | 3.21 | . 00 | 22.92 |
| $\begin{array}{r} (2) \\ 8.1-10.0 \end{array}$ | 1.00 | . 56 | . 67 | . 65 | . 12 | . 02 | . 26 | . 81 | . 16 | . 28 | . 53 | . 23 | . 12 | . 51 | 1.49 | 1.21 | . 00 | 8.63 |
|  | 44 | 33 | 17 | 9 | 0 | 2 | 0 | 16 | 1 | 8 | 12 | 1 | 3 | 20 | 44 | 16 | 0 | 226 |
| (1) | 2.72 | 2.04 | 1.05 | . 56 | . 00 | . 12 | . 00 | . 99 | . 06 | . 49 | . 74 | . 06 | . 19 | 1.24 | 2.72 | . 99 | . 00 | 13.96 |
| (2) | 1.02 | . 77 | . 40 | . 21 | . 00 | . 05 | . 00 | . 37 | . 02 | . 19 | . 28 | . 02 | . 07 | . 47 | 1.02 | . 37 | . 00 | 5.26 |
| 10.1-89.5 | 36 | 13 | 10 | 11 | 0 |  | 0 | 6 | 0 | 0 | 1 | 0 | 2 | 11 | 13 | 10 | 0 | 114 |
| (1) | 2.22 | . 80 | . 62 | . 68 | . 00 | . 06 | . 00 | . 37 | . 00 | . 00 | . 06 | . 00 | . 12 | . 68 | . 80 | . 62 | . 00 | 7.04 |
| (2) | . 84 | . 30 | . 23 | . 26 | . 00 | . 02 | . 00 | . 14 | . 00 | . 00 | . 02 | . 00 | . 05 | . 26 | . 30 | . 23 | . 00 | 2.65 |
|  | 215 | 156 | 124 | 150 | 78 | 55 | 81 | 143 | 45 | 48 | 65 | 45 | 28 | 80 | 167 | 139 | 0 | 1619 |
| ALL SPEEDS | 13.28 | 9.64 | 7.66 | 9.26 | 4.82 | 3.40 | 5.00 | 8.83 | 2.78 | 2.96 | 4.01 | 2.78 | 1.73 | 4.94 | 10.32 | 8.59 | . 00 | 100.00 |
| (2) | 5.00 | 3.63 | 2.88 | 3.49 | 1.81 | 1.28 | 1.88 | 3.33 | 1.05 | 1.12 | 1.51 | 1.05 | . 65 | 1.86 | 3.88 | 3.23 | . 00 | 37.65 |
| (1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE <br> (2) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

OヨノכヨノOyd $\perp H פ ו y \wedge d O כ$

CC MARCH MET DATA JOINT FREQUENCY DISTRIBUTION（60－METER TOWER）
197．0 FT WIND DATA STABILITY CLASS E CLASS FREQUENCY（PERCENT）＝ 28.91



Table 2.3-32—\{CCNPP 197 ft (60 m) March JFD (2000-2005)\}
(Page 6 of 8)
CC MARCH MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS F CLASS FREQUENCY (PERCENT) = 9.63

| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 24 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 24 |
| (2) | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| .5-1.0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 7 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 24 | . 24 | . 24 | . 00 | . 00 | . 24 | . 00 | . 00 | . 24 | . 00 | . 48 | . 00 | . 00 | 1.69 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 05 | . 00 | . 00 | . 16 |
| 1.1-1.5 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 2 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 8 |
| (1) | . 24 | . 00 | . 24 | . 00 | . 00 | . 24 | . 00 | . 48 | . 00 | . 24 | . 00 | . 00 | . 24 | . 24 | . 00 | . 00 | . 00 | 1.93 |
| (2) | . 02 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 05 | . 00 | . 02 | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 19 |
| 1.6-2.0 | 0 | 0 | 2 | 3 | 1 | 1 | 2 | 1 | 2 | 0 | 1 | 1 | 0 | 2 | 1 | 1 | 0 | 18 |
| (1) | . 00 | . 00 | . 48 | . 72 | . 24 | . 24 | . 48 | . 24 | . 48 | . 00 | . 24 | . 24 | . 00 | . 48 | . 24 | . 24 | . 00 | 4.35 |
| (2) | . 00 | . 00 | . 05 | . 07 | . 02 | . 02 | . 05 | . 02 | . 05 | . 00 | . 02 | . 02 | . 00 | . 05 | . 02 | . 02 | . 00 | . 42 |
| 2.1-3.0 | 7 | 7 | 1 | 3 | 7 | 3 | 3 | 2 | 1 | 2 | 2 | 1 | 3 | 3 | 3 | 2 | 0 | 50 |
| (1) | 1.69 | 1.69 | . 24 | . 72 | 1.69 | . 72 | . 72 | . 48 | . 24 | . 48 | . 48 | . 24 | . 72 | . 72 | . 72 | . 48 | . 00 | 12.08 |
| (2) | . 16 | . 16 | . 02 | . 07 | . 16 | . 07 | . 07 | . 05 | . 02 | . 05 | . 05 | . 02 | . 07 | . 07 | . 07 | . 05 | . 00 | 1.16 |
| 3.1-4.0 | 3 | 3 | 11 | 1 | 1 | 4 | 2 | 2 | 5 | 4 | 4 | 7 | 5 | 3 | 3 | 4 | 0 | 62 |
| (1) | . 72 | . 72 | 2.66 | . 24 | . 24 | . 97 | . 48 | . 48 | 1.21 | . 97 | . 97 | 1.69 | 1.21 | . 72 | . 72 | . 97 | . 00 | 14.98 |
| (2) | . 07 | . 07 | . 26 | . 02 | . 02 | . 09 | . 05 | . 05 | . 12 | . 09 | . 09 | . 16 | . 12 | . 07 | . 07 | . 09 | . 00 | 1.44 |
| 4.1-5.0 | 5 | 4 | 3 | 3 | 1 | 0 | 1 | 2 | 3 | 6 | 10 | 2 | 7 | 5 | 3 | 7 | 0 | 62 |
| (1) | 1.21 | . 97 | . 72 | . 72 | . 24 | . 00 | . 24 | . 48 | . 72 | 1.45 | 2.42 | . 48 | 1.69 | 1.21 | . 72 | 1.69 | . 00 | 14.98 |
| (2) | . 12 | . 09 | . 07 | . 07 | . 02 | . 00 | . 02 | . 05 | . 07 | . 14 | . 23 | . 05 | . 16 | . 12 | . 07 | . 16 | . 00 | 1.44 |
| 5.1-6.0 | 2 | 2 | 3 | 2 | 0 | 1 | 0 | 3 | 18 | 11 | 2 | 4 | 5 | 6 | 11 | 6 | 0 | 76 |
| (1) | . 48 | . 48 | . 72 | . 48 | . 00 | . 24 | . 00 | . 72 | 4.35 | 2.66 | . 48 | . 97 | 1.21 | 1.45 | 2.66 | 1.45 | . 00 | 18.36 |
| (2) | . 05 | . 05 | . 07 | . 05 | . 00 | . 02 | . 00 | . 07 | . 42 | . 26 | . 05 | . 09 | . 12 | . 14 | . 26 | . 14 | . 00 | 1.77 |
| 6.1-8.0 | 3 | 2 | 5 | 7 | 3 | 0 | 3 | 8 | 24 | 18 | 21 | 10 | 7 | 1 | 10 | 0 | 0 | 122 |
| (1) | . 72 | . 48 | 1.21 | 1.69 | . 72 | . 00 | . 72 | 1.93 | 5.80 | 4.35 | 5.07 | 2.42 | 1.69 | . 24 | 2.42 | . 00 | . 00 | 29.47 |
| (2) | . 07 | . 05 | . 12 | . 16 | . 07 | . 00 | . 07 | . 19 | . 56 | . 42 | . 49 | . 23 | . 16 | . 02 | . 23 | . 00 | . 00 | 2.84 |
| 8.1-10.0 | 2 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| (1) | . 48 | . 00 | . 24 | . 24 | . 00 | . 00 | . 00 | . 00 | . 00 | . 97 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.93 |
| (2) | . 05 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 09 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 19 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 24 | 18 | 27 | 20 | 14 | 11 | 12 | 20 | 53 | 47 | 40 | 25 | 29 | 21 | 33 | 20 | 0 | 414 |
| (1) | 5.80 | 4.35 | 6.52 | 4.83 | 3.38 | 2.66 | 2.90 | 4.83 | 12.80 | 11.35 | 9.66 | 6.04 | 7.00 | 5.07 | 7.97 | 4.83 | . 00 | 100.00 |
| (2) | . 56 | . 42 | . 63 | . 47 | . 33 | . 26 | . 28 | . 47 | 1.23 | 1.09 | . 93 | . 58 | . 67 | . 49 | . 77 | . 47 | . 00 | 9.63 |

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

CC MARCH MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS G CLASS FREQUENCY (PERCENT) = 3.77

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
GヨЬכヨ८Oyd $\perp$ HפוyגdOכ

CC MARCH MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS ALL CLASS FREQUENCY (PERCENT) = 100.00

|  | WIND DIRECTION FROM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 4 |
| (1) | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 09 |
| (2) | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 09 |
| .5-1.0 | 4 | 2 | 5 | 0 | 7 | 2 | 1 | 2 | 2 | 3 | 3 | 1 | 2 | 1 | 7 | 1 | 0 | 43 |
| (1) | . 09 | . 05 | . 12 | . 00 | . 16 | . 05 | . 02 | . 05 | . 05 | . 07 | . 07 | . 02 | . 05 | . 02 | . 16 | . 02 | . 00 | 1.00 |
| (2) | . 09 | . 05 | . 12 | . 00 | . 16 | . 05 | . 02 | . 05 | . 05 | . 07 | . 07 | . 02 | . 05 | . 02 | . 16 | . 02 | . 00 | 1.00 |
| 1.1-1.5 | 6 | 4 | 5 | 8 | 4 | 4 | 3 | 4 | 2 | 1 | 3 | 6 | 4 | 2 | 1 | 1 | 0 | 58 |
| (1) | . 14 | . 09 | . 12 | . 19 | . 09 | . 09 | . 07 | . 09 | . 05 | . 02 | . 07 | . 14 | . 09 | . 05 | . 02 | . 02 | . 00 | 1.35 |
| (2) | . 14 | . 09 | . 12 | . 19 | . 09 | . 09 | . 07 | . 09 | . 05 | . 02 | . 07 | . 14 | . 09 | . 05 | . 02 | . 02 | . 00 | 1.35 |
| 1.6-2.0 | 8 | 13 | 15 | 13 | 15 | 9 | 5 | 4 | 7 | 1 | 8 | 5 | 3 | 6 | 3 | 4 | 0 | 119 |
| (1) | . 19 | . 30 | . 35 | . 30 | . 35 | . 21 | . 12 | . 09 | . 16 | . 02 | . 19 | . 12 | . 07 | . 14 | . 07 | . 09 | . 00 | 2.77 |
| (2) | . 19 | . 30 | . 35 | . 30 | . 35 | . 21 | . 12 | . 09 | . 16 | . 02 | . 19 | . 12 | . 07 | . 14 | . 07 | . 09 | . 00 | 2.77 |
| 2.1-3.0 | 45 | 57 | 46 | 41 | 52 | 28 | 22 | 19 | 18 | 18 | 18 | 15 | 9 | 16 | 16 | 17 | 0 | 437 |
| (1) | 1.05 | 1.33 | 1.07 | . 95 | 1.21 | . 65 | . 51 | . 44 | . 42 | . 42 | . 42 | . 35 | . 21 | . 37 | . 37 | . 40 | . 00 | 10.16 |
| (2) | 1.05 | 1.33 | 1.07 | . 95 | 1.21 | . 65 | . 51 | . 44 | . 42 | . 42 | . 42 | . 35 | . 21 | . 37 | . 37 | . 40 | . 00 | 10.16 |
| 3.1-4.0 | 59 | 63 | 50 | 29 | 31 | 33 | 34 | 44 | 32 | 21 | 33 | 29 | 17 | 12 | 19 | 46 | 0 | 552 |
| (1) | 1.37 | 1.47 | 1.16 | . 67 | . 72 | . 77 | . 79 | 1.02 | . 74 | . 49 | . 77 | . 67 | . 40 | . 28 | . 44 | 1.07 | . 00 | 12.84 |
| (2) | 1.37 | 1.47 | 1.16 | . 67 | . 72 | . 77 | . 79 | 1.02 | . 74 | . 49 | . 77 | . 67 | . 40 | . 28 | . 44 | 1.07 | . 00 | 12.84 |
| 4.1-5.0 | 69 | 41 | 27 | 34 | 29 | 24 | 33 | 82 | 33 | 35 | 40 | 24 | 22 | 44 | 59 | 74 | 0 | 670 |
| (1) | 1.60 | . 95 | . 63 | . 79 | . 67 | . 56 | . 77 | 1.91 | . 77 | . 81 | . 93 | . 56 | . 51 | 1.02 | 1.37 | 1.72 | . 00 | 15.58 |
| (2) | 1.60 | . 95 | . 63 | . 79 | . 67 | . 56 | . 77 | 1.91 | . 77 | . 81 | . 93 | . 56 | . 51 | 1.02 | 1.37 | 1.72 | . 00 | 15.58 |
| 5.1-6.0 | 59 | 31 | 21 | 27 | 15 | 11 | 31 | 74 | 71 | 50 | 35 | 37 | 34 | 54 | 87 | 62 | 0 | 699 |
| (1) | 1.37 | . 72 | . 49 | . 63 | . 35 | . 26 | . 72 | 1.72 | 1.65 | 1.16 | . 81 | . 86 | . 79 | 1.26 | 2.02 | 1.44 | . 00 | 16.26 |
| (2) | 1.37 | . 72 | . 49 | . 63 | . 35 | . 26 | . 72 | 1.72 | 1.65 | 1.16 | . 81 | . 86 | . 79 | 1.26 | 2.02 | 1.44 | . 00 | 16.26 |
| 6.1-8.0 | 84 | 44 | 41 | 37 | 11 | 8 | 23 | 105 | 85 | 108 | 130 | 48 | 43 | 74 | 157 | 100 | 0 | 1098 |
| (1) | 1.95 | 1.02 | . 95 | . 86 | . 26 | . 19 | . 53 | 2.44 | 1.98 | 2.51 | 3.02 | 1.12 | 1.00 | 1.72 | 3.65 | 2.33 | . 00 | 25.53 |
| (2) | 1.95 | 1.02 | . 95 | . 86 | . 26 | . 19 | . 53 | 2.44 | 1.98 | 2.51 | 3.02 | 1.12 | 1.00 | 1.72 | 3.65 | 2.33 | . 00 | 25.53 |
| 8.1-10.0 | 64 | 36 | 21 | 11 | 0 | 3 | 3 | 31 | 12 | 43 | 49 | 5 | 6 | 61 | 72 | 24 | 0 | 441 |
| (1) | 1.49 | . 84 | . 49 | . 26 | . 00 | . 07 | . 07 | . 72 | . 28 | 1.00 | 1.14 | . 12 | . 14 | 1.42 | 1.67 | . 56 | . 00 | 10.26 |
| (2) | 1.49 | . 84 | . 49 | . 26 | . 00 | . 07 | . 07 | . 72 | . 28 | 1.00 | 1.14 | . 12 | . 14 | 1.42 | 1.67 | . 56 | . 00 | 10.26 |
| 10.1-89.5 | 45 | 17 | 11 | 11 | 0 | 2 | 4 | 9 | 2 | 5 | 5 | 2 | 4 | 22 | 28 | 12 | 0 | 179 |
| (1) | 1.05 | . 40 | . 26 | . 26 | . 00 | . 05 | . 09 | . 21 | . 05 | . 12 | . 12 | . 05 | . 09 | . 51 | . 65 | . 28 | . 00 | 4.16 |
| (2) | 1.05 | . 40 | . 26 | . 26 | . 00 | . 05 | . 09 | . 21 | . 05 | . 12 | . 12 | . 05 | . 09 | . 51 | . 65 | . 28 | . 00 | 4.16 |
| ALL SPEEDS | 444 | 309 | 242 | 211 | 164 | 124 | 159 | 375 | 264 | 285 | 324 | 172 | 144 | 293 | 449 | 341 | 0 | 4300 |
| (1) | 10.33 | 7.19 | 5.63 | 4.91 | 3.81 | 2.88 | 3.70 | 8.72 | 6.14 | 6.63 | 7.53 | 4.00 | 3.35 | 6.81 | 10.44 | 7.93 | . 00 | 100.00 |
| (2) | 10.33 | 7.19 | 5.63 | 4.91 | 3.81 | 2.88 | 3.70 | 8.72 | 6.14 | 6.63 | 7.53 | 4.00 | 3.35 | 6.81 | 10.44 | 7.93 | . 00 | 100.00 |
| 1) = PERCENT | OF ALL | GOOD | SER | IONS | FOR | IS PA |  |  |  |  |  |  |  |  |  |  |  |  |

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Table 2.3-33—\{CCNPP 197 ft ( 60 m) April JFD (2000-2005)\}
(Page 1 of 8)
CC APRIL MET DATA JOINT FREQUENCY DISTRIBUTION ( 60 -METER TOWER)
197.0 FT WIND DATA STABILITY CLASS A CLASS FREQUENCY (PERCENT) = 12.16

|  |  |  |  |  |  |  |  | IND DI | RECTIO | N FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 1.1-1.5 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 20 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 20 |
| (2) | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| 1.6-2.0 | 0 | 0 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 5 |
| (1) | . 00 | . 00 | . 20 | . 20 | . 20 | . 20 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 20 | . 00 | . 00 | . 00 | . 00 | 1.00 |
| (2) | . 00 | . 00 | . 02 | . 02 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 12 |
| 2.1-3.0 | 2 | 1 | 5 | 1 | 1 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 1 | 1 | 0 | 0 | 0 | 18 |
| (1) | . 40 | . 20 | 1.00 | . 20 | . 20 | . 00 | . 00 | . 00 | . 20 | . 20 | . 20 | . 60 | . 20 | . 20 | . 00 | . 00 | . 00 | 3.61 |
| (2) | . 05 | . 02 | . 12 | . 02 | . 02 | . 00 | . 00 | . 00 | . 02 | . 02 | . 02 | . 07 | . 02 | . 02 | . 00 | . 00 | . 00 | . 44 |
| 3.1-4.0 | 2 | 16 | 3 | 3 | 2 | 1 | 2 | 8 | 1 | 3 | 5 | 9 | 0 | 0 | 1 | 0 | 0 | 56 |
| (1) | . 40 | 3.21 | . 60 | . 60 | . 40 | . 20 | . 40 | 1.61 | . 20 | . 60 | 1.00 | 1.81 | . 00 | . 00 | . 20 | . 00 | . 00 | 11.24 |
| (2) | . 05 | . 39 | . 07 | . 07 | . 05 | . 02 | . 05 | . 20 | . 02 | . 07 | . 12 | . 22 | . 00 | . 00 | . 02 | . 00 | . 00 | 1.37 |
| 4.1-5.0 | 11 | 12 | 2 | 1 | 2 | 4 | 3 | 5 | 2 | 7 | 10 | 11 | 5 | 5 | 3 | 1 | 0 | 84 |
| (1) | 2.21 | 2.41 | . 40 | . 20 | . 40 | . 80 | . 60 | 1.00 | . 40 | 1.41 | 2.01 | 2.21 | 1.00 | 1.00 | . 60 | . 20 | . 00 | 16.87 |
| (2) | . 27 | . 29 | . 05 | . 02 | . 05 | . 10 | . 07 | . 12 | . 05 | . 17 | . 24 | . 27 | . 12 | . 12 | . 07 | . 02 | . 00 | 2.05 |
| 5.1-6.0 | 14 | 5 | 2 | 0 | 2 | 1 | 7 | 4 | 1 | 8 | 18 | 11 | 6 | 5 | 6 | 2 | 0 | 92 |
| (1) | 2.81 | 1.00 | . 40 | . 00 | . 40 | . 20 | 1.41 | . 80 | . 20 | 1.61 | 3.61 | 2.21 | 1.20 | 1.00 | 1.20 | . 40 | . 00 | 18.47 |
| (2) | . 34 | . 12 | . 05 | . 00 | . 05 | . 02 | . 17 | . 10 | . 02 | . 20 | . 44 | . 27 | . 15 | . 12 | . 15 | . 05 | . 00 | 2.25 |
| 6.1-8.0 | 17 | 21 | 1 | 1 | 1 | 2 | 5 | 16 | 3 | 14 | 32 | 11 | 5 | 13 | 14 | 2 | 0 | 158 |
| (1) | 3.41 | 4.22 | . 20 | . 20 | . 20 | . 40 | 1.00 | 3.21 | . 60 | 2.81 | 6.43 | 2.21 | 1.00 | 2.61 | 2.81 | . 40 | . 00 | 31.73 |
| (2) | . 42 | . 51 | . 02 | . 02 | . 02 | . 05 | . 12 | . 39 | . 07 | . 34 | . 78 | . 27 | . 12 | . 32 | . 34 | . 05 | . 00 | 3.86 |
| 8.1-10.0 | 6 | 7 | 0 | 1 | 0 | 0 | 0 | 4 | 0 | 6 | 3 | 4 | 4 | 8 | 8 | 0 | 0 | 51 |
| (1) | 1.20 | 1.41 | . 00 | . 20 | . 00 | . 00 | . 00 | . 80 | . 00 | 1.20 | . 60 | . 80 | . 80 | 1.61 | 1.61 | . 00 | . 00 | 10.24 |
| (2) | . 15 | . 17 | . 00 | . 02 | . 00 | . 00 | . 00 | . 10 | . 00 | . 15 | . 07 | . 10 | . 10 | . 20 | . 20 | . 00 | . 00 | 1.25 |
| 10.1-89.5 | 2 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 3 | 0 | 3 | 9 | 8 | 0 | 0 | 33 |
| (1) | . 40 | . 40 | . 20 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.00 | . 60 | . 00 | . 60 | 1.81 | 1.61 | . 00 | . 00 | 6.63 |
| (2) | . 05 | . 05 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 12 | . 07 | . 00 | . 07 | . 22 | . 20 | . 00 | . 00 | . 81 |
| ALL SPEEDS | 54 | 64 | 16 | 8 | 9 | 9 | 17 | 37 | 8 | 44 | 72 | 49 | 25 | 41 | 40 | 5 | 0 | 498 |
| (1) | 10.84 | 12.85 | 3.21 | 1.61 | 1.81 | 1.81 | 3.41 | 7.43 | 1.61 | 8.84 | 14.46 | 9.84 | 5.02 | 8.23 | 8.03 | 1.00 | . 00 | 100.00 |
| (2) | 1.32 | 1.56 | . 39 | . 20 | . 22 | . 22 | . 42 | . 90 | . 20 | 1.07 | 1.76 | 1.20 | . 61 | 1.00 | . 98 | . 12 | . 00 | 12.16 |

(2) = PERCENT

## 

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CC APRIL MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS B CLASS FREQUENCY (PERCENT) = 4.10

|  |  |  |  |  |  |  |  |  | RECTIO | FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 1.1-1.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 1.6-2.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 60 | . 00 | . 00 | . 60 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 |
| 2.1-3.0 | 2 | 2 | 5 | 5 | 7 | 1 | 2 | 0 | 0 | 1 | 1 | 3 | 0 | 2 | 0 | 0 | 0 | 31 |
| (1) | 1.19 | 1.19 | 2.98 | 2.98 | 4.17 | . 60 | 1.19 | . 00 | . 00 | . 60 | . 60 | 1.79 | . 00 | 1.19 | . 00 | . 00 | . 00 | 18.45 |
| (2) | . 05 | . 05 | . 12 | . 12 | . 17 | . 02 | . 05 | . 00 | . 00 | . 02 | . 02 | . 07 | . 00 | . 05 | . 00 | . 00 | . 00 | . 76 |
| 3.1-4.0 | 6 | 7 | 1 | 2 | 0 | 2 | 0 | 2 | 0 | 2 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 25 |
| (1) | 3.57 | 4.17 | . 60 | 1.19 | . 00 | 1.19 | . 00 | 1.19 | . 00 | 1.19 | . 60 | . 60 | . 60 | . 00 | . 00 | . 00 | . 00 | 14.88 |
| (2) | . 15 | . 17 | . 02 | . 05 | . 00 | . 05 | . 00 | . 05 | . 00 | . 05 | . 02 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 61 |
| 4.1-5.0 | 4 | 2 | 3 | 1 | 0 | 0 | 2 | 2 | 1 | 0 | 3 | 1 | 2 | 1 | 1 | 0 | 0 | 23 |
| (1) | 2.38 | 1.19 | 1.79 | . 60 | . 00 | . 00 | 1.19 | 1.19 | . 60 | . 00 | 1.79 | . 60 | 1.19 | . 60 | . 60 | . 00 | . 00 | 13.69 |
| (2) | . 10 | . 05 | . 07 | . 02 | . 00 | . 00 | . 05 | . 05 | . 02 | . 00 | . 07 | . 02 | . 05 | . 02 | . 02 | . 00 | . 00 | . 56 |
| 5.1-6.0 | 3 | 2 | 2 | 0 | 0 | 1 | 1 | 6 | 2 | 3 | 3 | 4 | 1 | 1 | 1 | 1 | 0 | 31 |
| (1) | 1.79 | 1.19 | 1.19 | . 00 | . 00 | . 60 | . 60 | 3.57 | 1.19 | 1.79 | 1.79 | 2.38 | . 60 | . 60 | . 60 | . 60 | . 00 | 18.45 |
| (2) | . 07 | . 05 | . 05 | . 00 | . 00 | . 02 | . 02 | . 15 | . 05 | . 07 | . 07 | . 10 | . 02 | . 02 | . 02 | . 02 | . 00 | . 76 |
| 6.1-8.0 | 4 | 3 | 4 | 1 | 0 | 1 | 1 | 3 | 0 | 3 | 3 | 3 | 0 | 2 | 2 | 2 | 0 | 32 |
| (1) | 2.38 | 1.79 | 2.38 | . 60 | . 00 | . 60 | . 60 | 1.79 | . 00 | 1.79 | 1.79 | 1.79 | . 00 | 1.19 | 1.19 | 1.19 | . 00 | 19.05 |
| (2) | . 10 | . 07 | . 10 | . 02 | . 00 | . 02 | . 02 | . 07 | . 00 | . 07 | . 07 | . 07 | . 00 | . 05 | . 05 | . 05 | . 00 | . 78 |
| 8.1-10.0 | 3 | 0 | 0 | 3 | 0 | 0 | 0 | 4 | 0 | 4 | 2 | 0 | 1 | 0 | 1 | 0 | 0 | 18 |
| (1) | 1.79 | . 00 | . 00 | 1.79 | . 00 | . 00 | . 00 | 2.38 | . 00 | 2.38 | 1.19 | . 00 | . 60 | . 00 | . 60 | . 00 | . 00 | 10.71 |
| (2) | . 07 | . 00 | . 00 | . 07 | . 00 | . 00 | . 00 | . 10 | . 00 | . 10 | . 05 | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 44 |
| 10.1-89.5 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 1 | 0 | 7 |
| (1) | . 00 | . 60 | . 00 | . 00 | . 00 | . 00 | . 00 | . 60 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.19 | 1.19 | . 60 | . 00 | 4.17 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 05 | . 02 | . 00 | . 17 |
| ALL SPEEDS | 22 | 17 | 15 | 12 | 7 | 5 | 6 | 18 | 3 | 13 | 13 | 12 | 5 | 8 | 8 | 4 | 0 | 168 |
| (1) | 13.10 | 10.12 | 8.93 | 7.14 | 4.17 | 2.98 | 3.57 | 10.71 | 1.79 | 7.74 | 7.74 | 7.14 | 2.98 | 4.76 | 4.76 | 2.38 | . 00 | 100.00 |
| (2) | . 54 | . 42 | . 37 | . 29 | . 17 | . 12 | . 15 | . 44 | . 07 | . 32 | . 32 | . 29 | . 12 | . 20 | . 20 | . 10 | . 00 | 4.10 |

(1) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

$\begin{array}{ccccc}\text { CC APRIL MET DATA JOINT FREQUENCY DISTRIBUTION } & (60-M E T E R ~ T O W E R) & & \\ 197.0 \text { FT WIND DATA } & \text { STABILITY CLASS C } & \text { CLASS FREQUENCY } & \text { (PERCENT) }=\quad 5.32\end{array}$

|  | WIND DIRECTION FROM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 1.1-1.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 2 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 92 | . 00 | . 00 | . 00 | . 00 | . 00 | . 92 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 |
| 1.6-2.0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 46 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 46 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| 2.1-3.0 | 4 | 4 | 7 | 5 | 7 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 30 |
| (1) | 1.83 | 1.83 | 3.21 | 2.29 | 3.21 | . 00 | . 00 | . 46 | . 00 | . 00 | . 46 | . 46 | . 00 | . 00 | . 00 | . 00 | . 00 | 13.76 |
| (2) | . 10 | . 10 | . 17 | . 12 | . 17 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 73 |
| 3.1-4.0 | 10 | 4 | 6 | 2 | 1 | 2 | 3 | 0 | 1 | 2 | 4 | 4 | 2 | 0 | 0 | 0 | 0 | 41 |
| (1) | 4.59 | 1.83 | 2.75 | . 92 | . 46 | . 92 | 1.38 | . 00 | . 46 | . 92 | 1.83 | 1.83 | . 92 | . 00 | . 00 | . 00 | . 00 | 18.81 |
| (2) | . 24 | . 10 | . 15 | . 05 | . 02 | . 05 | . 07 | . 00 | . 02 | . 05 | . 10 | . 10 | . 05 | . 00 | . 00 | . 00 | . 00 | 1.00 |
| 4.1-5.0 | 4 | 8 | 0 | 0 | 3 | 1 | 1 | 7 | 0 | 2 | 1 | 0 | 2 | 1 | 2 | 0 | 0 | 32 |
| (1) | 1.83 | 3.67 | . 00 | . 00 | 1.38 | . 46 | . 46 | 3.21 | . 00 | . 92 | . 46 | . 00 | . 92 | . 46 | . 92 | . 00 | . 00 | 14.68 |
| (2) | . 10 | . 20 | . 00 | . 00 | . 07 | . 02 | . 02 | . 17 | . 00 | . 05 | . 02 | . 00 | . 05 | . 02 | . 05 | . 00 | . 00 | . 78 |
| 5.1-6.0 | 6 | 1 | 2 | 2 | 0 | 1 | 1 | 4 | 0 | 4 | 5 | 3 | 1 | 1 | 1 | 2 | 0 | 34 |
| (1) | 2.75 | . 46 | . 92 | . 92 | . 00 | . 46 | . 46 | 1.83 | . 00 | 1.83 | 2.29 | 1.38 | . 46 | . 46 | . 46 | . 92 | . 00 | 15.60 |
| (2) | . 15 | . 02 | . 05 | . 05 | . 00 | . 02 | . 02 | . 10 | . 00 | . 10 | . 12 | . 07 | . 02 | . 02 | . 02 | . 05 | . 00 | . 83 |
| 6.1-8.0 | 3 | 3 | 2 | 2 | 0 | 0 | 1 | 4 | 0 | 6 | 3 | 4 | 1 | 5 | 7 | 2 | 0 | 43 |
| (1) | 1.38 | 1.38 | . 92 | . 92 | . 00 | . 00 | . 46 | 1.83 | . 00 | 2.75 | 1.38 | 1.83 | . 46 | 2.29 | 3.21 | . 92 | . 00 | 19.72 |
| (2) | . 07 | . 07 | . 05 | . 05 | . 00 | . 00 | . 02 | . 10 | . 00 | . 15 | . 07 | . 10 | . 02 | . 12 | . 17 | . 05 | . 00 | 1.05 |
| 8.1-10.0 | 2 | 5 | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 2 | 3 | 0 | 1 | 1 | 1 | 1 | 0 | 22 |
| (1) | . 92 | 2.29 | . 46 | . 92 | . 00 | . 00 | . 46 | . 92 | . 00 | . 92 | 1.38 | . 00 | . 46 | . 46 | . 46 | . 46 | . 00 | 10.09 |
| (2) | . 05 | . 12 | . 02 | . 05 | . 00 | . 00 | . 02 | . 05 | . 00 | . 05 | . 07 | . 00 | . 02 | . 02 | . 02 | . 02 | . 00 | . 54 |
| 10.1-89.5 | 2 | 1 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 3 | 0 | 0 | 13 |
| (1) | . 92 | . 46 | . 92 | . 92 | . 00 | . 00 | . 00 | . 00 | . 00 | . 46 | . 00 | . 00 | . 00 | . 92 | 1.38 | . 00 | . 00 | 5.96 |
| (2) | . 05 | . 02 | . 05 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 05 | . 07 | . 00 | . 00 | . 32 |
| ALL SPEEDS | 31 | 27 | 20 | 15 | 11 | 4 | 7 | 18 | 1 | 17 | 17 | 14 | 7 | 10 | 14 | 5 | 0 | 218 |
| (1) | 14.22 | 12.39 | 9.17 | 6.88 | 5.05 | 1.83 | 3.21 | 8.26 | . 46 | 7.80 | 7.80 | 6.42 | 3.21 | 4.59 | 6.42 | 2.29 | . 00 | 100.00 |
| (2) | . 76 | . 66 | . 49 | . 37 | . 27 | . 10 | . 17 | . 44 | . 02 | . 42 | . 42 | . 34 | . 17 | . 24 | . 34 | . 12 | . 00 | 5.32 |

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD


CC APRIL MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS D CLASS FREQUENCY (PERCENT) = 39.77

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$\stackrel{0}{0}$
$i$
$i$

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CC APRIL MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS E CLASS FREQUENCY (PERCENT) = 26.21

|  |  |  |  |  |  |  |  | IND DI | IRECTIO | N FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 1 | 2 | 4 | 0 | 2 | 0 | 3 | 2 | 3 | 2 | 0 | 0 | 0 | 3 | 1 | 0 | 23 |
| (1) | . 00 | . 09 | . 19 | . 37 | . 00 | . 19 | . 00 | . 28 | . 19 | . 28 | . 19 | . 00 | . 00 | . 00 | . 28 | . 09 | . 00 | 2.14 |
| (2) | . 00 | . 02 | . 05 | . 10 | . 00 | . 05 | . 00 | . 07 | . 05 | . 07 | . 05 | . 00 | . 00 | . 00 | . 07 | . 02 | . 00 | . 56 |
| 1.1-1.5 | 1 | 2 | 1 | 0 | 2 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 3 | 2 | 1 | 0 | 0 | 14 |
| (1) | . 09 | . 19 | . 09 | . 00 | . 19 | . 00 | . 00 | . 09 | . 00 | . 09 | . 00 | . 00 | . 28 | . 19 | . 09 | . 00 | . 00 | 1.30 |
| (2) | . 02 | . 05 | . 02 | . 00 | . 05 | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 07 | . 05 | . 02 | . 00 | . 00 | . 34 |
| 1.6-2.0 | 2 | 4 | 3 | 2 | 2 | 3 | 2 | 1 | 3 | 7 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 32 |
| (1) | . 19 | . 37 | . 28 | . 19 | . 19 | . 28 | . 19 | . 09 | . 28 | . 65 | . 00 | . 00 | . 00 | . 28 | . 00 | . 00 | . 00 | 2.98 |
| (2) | . 05 | . 10 | . 07 | . 05 | . 05 | . 07 | . 05 | . 02 | . 07 | . 17 | . 00 | . 00 | . 00 | . 07 | . 00 | . 00 | . 00 | . 78 |
| 2.1-3.0 | 5 | 12 | 7 | 5 | 8 | 1 | 6 | 4 | 5 | 8 | 3 | 3 | 3 | 2 | 4 | 4 | 0 | 80 |
| (1) | . 47 | 1.12 | . 65 | . 47 | . 75 | . 09 | . 56 | . 37 | . 47 | . 75 | . 28 | . 28 | . 28 | . 19 | . 37 | . 37 | . 00 | 7.46 |
| (2) | . 12 | . 29 | . 17 | . 12 | . 20 | . 02 | . 15 | . 10 | . 12 | . 20 | . 07 | . 07 | . 07 | . 05 | . 10 | . 10 | . 00 | 1.95 |
| 3.1-4.0 | 15 | 12 | 8 | 8 | 7 | 4 | 3 | 8 | 4 | 4 | 10 | 4 | 7 | 11 | 11 | 6 | 0 | 122 |
| (1) | 1.40 | 1.12 | . 75 | . 75 | . 65 | . 37 | . 28 | . 75 | . 37 | . 37 | . 93 | . 37 | . 65 | 1.03 | 1.03 | . 56 | . 00 | 11.37 |
| (2) | . 37 | . 29 | . 20 | . 20 | . 17 | . 10 | . 07 | . 20 | . 10 | . 10 | . 24 | . 10 | . 17 | . 27 | . 27 | . 15 | . 00 | 2.98 |
| 4.1-5.0 | 15 | 19 | 11 | 6 | 2 | 4 | 3 | 7 | 13 | 9 | 8 | 6 | 5 | 12 | 19 | 22 | 0 | 161 |
| (1) | 1.40 | 1.77 | 1.03 | . 56 | . 19 | . 37 | . 28 | . 65 | 1.21 | . 84 | . 75 | . 56 | . 47 | 1.12 | 1.77 | 2.05 | . 00 | 15.00 |
| (2) | . 37 | . 46 | . 27 | . 15 | . 05 | . 10 | . 07 | . 17 | . 32 | . 22 | . 20 | . 15 | . 12 | . 29 | . 46 | . 54 | . 00 | 3.93 |
| 5.1-6.0 | 22 | 5 | 6 | 2 | 2 | 2 | 2 | 21 | 20 | 27 | 14 | 11 | 11 | 16 | 26 | 18 | 0 | 205 |
| (1) | 2.05 | . 47 | . 56 | . 19 | . 19 | . 19 | . 19 | 1.96 | 1.86 | 2.52 | 1.30 | 1.03 | 1.03 | 1.49 | 2.42 | 1.68 | . 00 | 19.11 |
| (2) | . 54 | . 12 | . 15 | . 05 | . 05 | . 05 | . 05 | . 51 | . 49 | . 66 | . 34 | . 27 | . 27 | . 39 | . 64 | . 44 | . 00 | 5.01 |
| 6.1-8.0 | 13 | 18 | 4 | 1 | 0 | 1 | 3 | 26 | 53 | 71 | 41 | 23 | 9 | 14 | 15 | 20 | 0 | 312 |
| (1) | 1.21 | 1.68 | . 37 | . 09 | . 00 | . 09 | . 28 | 2.42 | 4.94 | 6.62 | 3.82 | 2.14 | . 84 | 1.30 | 1.40 | 1.86 | . 00 | 29.08 |
| (2) | . 32 | . 44 | . 10 | . 02 | . 00 | . 02 | . 07 | . 64 | 1.29 | 1.73 | 1.00 | . 56 | . 22 | . 34 | . 37 | . 49 | . 00 | 7.62 |
| 8.1-10.0 | 7 | 8 | 1 | 0 | 0 | 0 | 0 | 2 | 15 | 35 | 21 | 3 | 1 | 5 | 2 | 4 | 0 | 104 |
| (1) | . 65 | . 75 | . 09 | . 00 | . 00 | . 00 | . 00 | . 19 | 1.40 | 3.26 | 1.96 | . 28 | . 09 | . 47 | . 19 | . 37 | . 00 | 9.69 |
| (2) | . 17 | . 20 | . 02 | . 00 | . 00 | . 00 | . 00 | . 05 | . 37 | . 85 | . 51 | . 07 | . 02 | . 12 | . 05 | . 10 | . 00 | 2.54 |
| 10.1-89.5 | 1 | 5 | 1 | 0 | 0 | 0 | 0 | 2 | 0 | 4 | 2 | 1 | 2 | 2 | 0 | 0 | 0 | 20 |
| (1) | . 09 | . 47 | . 09 | . 00 | . 00 | . 00 | . 00 | . 19 | . 00 | . 37 | . 19 | . 09 | . 19 | . 19 | . 00 | . 00 | . 00 | 1.86 |
| (2) | . 02 | . 12 | . 02 | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 10 | . 05 | . 02 | . 05 | . 05 | . 00 | . 00 | . 00 | . 49 |
| ALL SPEEDS | 81 | 86 | 44 | 28 | 23 | 17 | 19 | 75 | 115 | 169 | 101 | 51 | 41 | 67 | 81 | 75 | 0 | 1073 |
| (1) | 7.55 | 8.01 | 4.10 | 2.61 | 2.14 | 1.58 | 1.77 | 6.99 | 10.72 | 15.75 | 9.41 | 4.75 | 3.82 | 6.24 | 7.55 | 6.99 | . 00 | 100.00 |
| (2) | 1.98 | 2.10 | 1.07 | . 68 | . 56 | . 42 | . 46 | 1.83 | 2.81 | 4.13 | 2.47 | 1.25 | 1.00 | 1.64 | 1.98 | 1.83 | . 00 | 26.21 |



CC APRIL MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS F CLASS FREQUENCY (PERCENT) = 7.72


CC APRIL MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS G CLASS FREQUENCY (PERCENT) = 4.71

|  | WIND DIRECTION FROM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 52 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 52 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 5 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 52 | 1.04 | . 00 | . 00 | . 00 | . 00 | . 52 | . 00 | . 00 | . 00 | . 52 | . 00 | 2.59 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 05 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 02 | . 00 | . 12 |
| 1.1-1.5 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 8 |
| (1) | . 00 | . 00 | . 52 | . 00 | . 00 | . 52 | . 52 | . 00 | . 52 | . 52 | . 00 | . 00 | . 52 | . 52 | . 00 | . 52 | . 00 | 4.15 |
| (2) | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 02 | . 00 | . 02 | . 02 | . 00 | . 00 | . 02 | . 02 | . 00 | . 02 | . 00 | . 20 |
| 1.6-2.0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 4 |
| (1) | . 00 | . 00 | . 52 | . 00 | . 00 | . 00 | . 00 | . 00 | . 52 | . 00 | . 52 | . 00 | . 52 | . 00 | . 00 | . 00 | . 00 | 2.07 |
| (2) | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 10 |
| 2.1-3.0 | 0 | 2 | 0 | 0 | 0 | 2 | 2 | 1 | 1 | 2 | 2 | 2 | 6 | 2 | 3 | 1 | 0 | 26 |
| (1) | . 00 | 1.04 | . 00 | . 00 | . 00 | 1.04 | 1.04 | . 52 | . 52 | 1.04 | 1.04 | 1.04 | 3.11 | 1.04 | 1.55 | . 52 | . 00 | 13.47 |
| (2) | . 00 | . 05 | . 00 | . 00 | . 00 | . 05 | . 05 | . 02 | . 02 | . 05 | . 05 | . 05 | . 15 | . 05 | . 07 | . 02 | . 00 | . 64 |
| 3.1-4.0 | 0 | 1 | 0 | 0 | 0 | 0 | 2 | 1 | 2 | 4 | 3 | 3 | 2 | 2 | 0 | 0 | 0 | 20 |
| (1) | . 00 | . 52 | . 00 | . 00 | . 00 | . 00 | 1.04 | . 52 | 1.04 | 2.07 | 1.55 | 1.55 | 1.04 | 1.04 | . 00 | . 00 | . 00 | 10.36 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 05 | . 02 | . 05 | . 10 | . 07 | . 07 | . 05 | . 05 | . 00 | . 00 | . 00 | . 49 |
| 4.1-5.0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 8 | 7 | 4 | 3 | 3 | 5 | 2 | 1 | 0 | 38 |
| (1) | . 52 | . 00 | . 00 | . 00 | . 00 | . 00 | . 52 | 1.55 | 4.15 | 3.63 | 2.07 | 1.55 | 1.55 | 2.59 | 1.04 | . 52 | . 00 | 19.69 |
| (2) | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 07 | . 20 | . 17 | . 10 | . 07 | . 07 | . 12 | . 05 | . 02 | . 00 | . 93 |
| 5.1-6.0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 3 | 9 | 2 | 5 | 6 | 1 | 0 | 0 | 0 | 27 |
| (1) | . 00 | . 00 | . 52 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.55 | 4.66 | 1.04 | 2.59 | 3.11 | . 52 | . 00 | . 00 | . 00 | 13.99 |
| (2) | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 | . 22 | . 05 | . 12 | . 15 | . 02 | . 00 | . 00 | . 00 | . 66 |
| 6.1-8.0 | 0 | 0 | 6 | 2 | 0 | 0 | 0 | 0 | 6 | 13 | 9 | 4 | 2 | 1 | 2 | 0 | 0 | 45 |
| (1) | . 00 | . 00 | 3.11 | 1.04 | . 00 | . 00 | . 00 | . 00 | 3.11 | 6.74 | 4.66 | 2.07 | 1.04 | . 52 | 1.04 | . 00 | . 00 | 23.32 |
| (2) | . 00 | . 00 | . 15 | . 05 | . 00 | . 00 | . 00 | . 00 | . 15 | . 32 | . 22 | . 10 | . 05 | . 02 | . 05 | . 00 | . 00 | 1.10 |
| 8.1-10.0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 5 |
| (1) | . 00 | . 00 | 1.04 | . 52 | . 00 | . 00 | . 00 | . 00 | . 00 | . 52 | . 00 | . 52 | . 00 | . 00 | . 00 | . 00 | . 00 | 2.59 |
| (2) | . 00 | . 00 | . 05 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 12 |
| 10.1-89.5 | 0 | 2 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 |
| (1) | . 00 | 1.04 | 6.22 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 7.25 |
| (2) | . 00 | . 05 | . 29 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 34 |
| ALL SPEEDS | 1 | 5 | 23 | 3 | 0 | 4 | 9 | 5 | 22 | 37 | 21 | 19 | 21 | 12 | 7 | 4 | 0 | 193 |
| (1) | . 52 | 2.59 | 11.92 | 1.55 | . 00 | 2.07 | 4.66 | 2.59 | 11.40 | 19.17 | 10.88 | 9.84 | 10.88 | 6.22 | 3.63 | 2.07 | . 00 | 100.00 |
| (2) | . 02 | . 12 | . 56 | . 07 | . 00 | . 10 | . 22 | . 12 | . 54 | . 90 | . 51 | . 46 | . 51 | . 29 | . 17 | . 10 | . 00 | 4.71 |

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
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CC APRIL MET DATA JOINT FREQUENCY DISTRIBUTION（60－METER TOWER
197．0 FT WIND DATA STABILITY CLASS ALL CLASS FREQUENCY（PERCENT）＝ 100.00

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CC MAY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS A CLASS FREQUENCY (PERCENT) = 13.37

(1) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD


CC MAY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS B CLASS FREQUENCY (PERCENT) = 5.12

|  |  |  |  |  |  |  |  | ND | T | FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 44 | . 00 | . 00 | . 44 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 |
| 1.1-1.5 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 3 |
| (1) | . 00 | . 00 | . 00 | . 44 | . 00 | . 44 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 44 | . 00 | . 00 | . 00 | . 00 | 1.32 |
| (2) | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 07 |
| 1.6-2.0 | 0 | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 5 |
| (1) | . 00 | . 44 | . 44 | . 88 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 44 | . 00 | . 00 | . 00 | . 00 | . 00 | 2.19 |
| (2) | . 00 | . 02 | . 02 | . 04 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 11 |
| 2.1-3.0 | 4 | 6 | 4 | 3 | 6 | 3 | 2 | 1 | 0 | 1 | 0 | 3 | 3 | 2 | 0 | 0 | 0 | 38 |
| (1) | 1.75 | 2.63 | 1.75 | 1.32 | 2.63 | 1.32 | . 88 | . 44 | . 00 | . 44 | . 00 | 1.32 | 1.32 | . 88 | . 00 | . 00 | . 00 | 16.67 |
| (2) | . 09 | . 13 | . 09 | . 07 | . 13 | . 07 | . 04 | . 02 | . 00 | . 02 | . 00 | . 07 | . 07 | . 04 | . 00 | . 00 | . 00 | . 85 |
| 3.1-4.0 | 7 | 6 | 4 | 2 | 2 | 4 | 6 | 3 | 3 | 2 | 4 | 5 | 1 | 2 | 0 | 1 | 0 | 52 |
| (1) | 3.07 | 2.63 | 1.75 | . 88 | . 88 | 1.75 | 2.63 | 1.32 | 1.32 | . 88 | 1.75 | 2.19 | . 44 | . 88 | . 00 | . 44 | . 00 | 22.81 |
| (2) | . 16 | . 13 | . 09 | . 04 | . 04 | . 09 | . 13 | . 07 | . 07 | . 04 | . 09 | . 11 | . 02 | . 04 | . 00 | . 02 | . 00 | 1.17 |
| 4.1-5.0 | 6 | 2 | 1 | 0 | 1 | 4 | 8 | 7 | 2 | 3 | 5 | 3 | 4 | 2 | 0 | 0 | 0 | 48 |
| (1) | 2.63 | . 88 | . 44 | . 00 | . 44 | 1.75 | 3.51 | 3.07 | . 88 | 1.32 | 2.19 | 1.32 | 1.75 | . 88 | . 00 | . 00 | . 00 | 21.05 |
| (2) | . 13 | . 04 | . 02 | . 00 | . 02 | . 09 | . 18 | . 16 | . 04 | . 07 | . 11 | . 07 | . 09 | . 04 | . 00 | . 00 | . 00 | 1.08 |
| 5.1-6.0 | 5 | 0 | 0 | 0 | 2 | 0 | 2 | 7 | 0 | 0 | 7 | 4 | 1 | 2 | 1 | 0 | 0 | 31 |
| (1) | 2.19 | . 00 | . 00 | . 00 | . 88 | . 00 | . 88 | 3.07 | . 00 | . 00 | 3.07 | 1.75 | . 44 | . 88 | . 44 | . 00 | . 00 | 13.60 |
| (2) | . 11 | . 00 | . 00 | . 00 | . 04 | . 00 | . 04 | . 16 | . 00 | . 00 | . 16 | . 09 | . 02 | . 04 | . 02 | . 00 | . 00 | . 70 |
| 6.1-8.0 | 2 | 1 | 1 | 1 | 0 | 1 | 2 | 6 | 0 | 2 | 6 | 0 | 5 | 1 | 3 | 0 | 0 | 31 |
| (1) | . 88 | . 44 | . 44 | . 44 | . 00 | . 44 | . 88 | 2.63 | . 00 | . 88 | 2.63 | . 00 | 2.19 | . 44 | 1.32 | . 00 | . 00 | 13.60 |
| (2) | . 04 | . 02 | . 02 | . 02 | . 00 | . 02 | . 04 | . 13 | . 00 | . 04 | . 13 | . 00 | . 11 | . 02 | . 07 | . 00 | . 00 | . 70 |
| 8.1-10.0 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 2 | 0 | 0 | 2 | 0 | 3 | 0 | 14 |
| (1) | . 44 | . 00 | . 88 | . 00 | . 00 | . 00 | . 00 | . 88 | . 88 | . 00 | . 88 | . 00 | . 00 | . 88 | . 00 | 1.32 | . 00 | 6.14 |
| (2) | . 02 | . 00 | . 04 | . 00 | . 00 | . 00 | . 00 | . 04 | . 04 | . 00 | . 04 | . 00 | . 00 | . 04 | . 00 | . 07 | . 00 | . 31 |
| 10.1-89.5 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 5 |
| (1) | . 00 | . 00 | . 88 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 44 | . 44 | . 00 | . 44 | . 00 | 2.19 |
| (2) | . 00 | . 00 | . 04 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 02 | . 00 | . 11 |
| ALL SPEEDS | 25 | 16 | 15 | 9 | 11 | 13 | 20 | 26 | 7 | 8 | 24 | 16 | 16 | 12 | 5 | 5 | 0 | 228 |
| (1) | 10.96 | 7.02 | 6.58 | 3.95 | 4.82 | 5.70 | 8.77 | 11.40 | 3.07 | 3.51 | 10.53 | 7.02 | 7.02 | 5.26 | 2.19 | 2.19 | . 00 | 100.00 |
| (2) | . 56 | . 36 | . 34 | . 20 | . 25 | . 29 | . 45 | . 58 | . 16 | . 18 | . 54 | . 36 | . 36 | . 27 | . 11 | . 11 | . 00 | 5.12 |

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD


CC MAY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS C CLASS FREQUENCY (PERCENT) $=5.53$

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
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Table 2.3-34—\{CCNPP 197 ft ( 60 m) May JFD (2000-2005)\} (Page 4 of 8)
CC MAY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS D CLASS FREQUENCY (PERCENT) = 35.60

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## аэІכэІІу

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CC MAY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS E CLASS FREQUENCY (PERCENT) $=23.21$

|  | WIND DIRECTION |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 1 | 1 | 2 | 0 | 5 | 1 | 0 | 1 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 |
| (1) | . 10 | . 10 | . 19 | . 00 | . 48 | . 10 | . 00 | . 10 | . 19 | . 10 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.36 |
| (2) | . 02 | . 02 | . 04 | . 00 | . 11 | . 02 | . 00 | . 02 | . 04 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 31 |
| 1.1-1.5 | 2 | 1 | 1 | 2 | 0 | 3 | 3 | 3 | 4 | 1 | 4 | 0 | 0 | 0 | 1 | 0 | 0 | 25 |
| (1) | . 19 | . 10 | . 10 | . 19 | . 00 | . 29 | . 29 | . 29 | . 39 | . 10 | . 39 | . 00 | . 00 | . 00 | . 10 | . 00 | . 00 | 2.42 |
| (2) | . 04 | . 02 | . 02 | . 04 | . 00 | . 07 | . 07 | . 07 | . 09 | . 02 | . 09 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 56 |
| 1.6-2.0 | 2 | 0 | 4 | 0 | 2 | 3 | 0 | 3 | 0 | 3 | 2 | 1 | 0 | 1 | 0 | 1 | 0 | 22 |
| (1) | . 19 | . 00 | . 39 | . 00 | . 19 | . 29 | . 00 | . 29 | . 00 | . 29 | . 19 | . 10 | . 00 | . 10 | . 00 | . 10 | . 00 | 2.13 |
| (2) | . 04 | . 00 | . 09 | . 00 | . 04 | . 07 | . 00 | . 07 | . 00 | . 07 | . 04 | . 02 | . 00 | . 02 | . 00 | . 02 | . 00 | . 49 |
| 2.1-3.0 | 9 | 6 | 5 | 4 | 2 | 3 | 12 | 10 | 6 | 4 | 12 | 6 | 2 | 8 | 4 | 5 | 0 | 98 |
| (1) | . 87 | . 58 | . 48 | . 39 | . 19 | . 29 | 1.16 | . 97 | . 58 | . 39 | 1.16 | . 58 | . 19 | . 77 | . 39 | . 48 | . 00 | 9.49 |
| (2) | . 20 | . 13 | . 11 | . 09 | . 04 | . 07 | . 27 | . 22 | . 13 | . 09 | . 27 | . 13 | . 04 | . 18 | . 09 | . 11 | . 00 | 2.20 |
| 3.1-4.0 | 4 | 4 | 5 | 4 | 12 | 9 | 11 | 13 | 12 | 6 | 10 | 11 | 5 | 4 | 6 | 8 | 0 | 124 |
| (1) | . 39 | . 39 | . 48 | . 39 | 1.16 | . 87 | 1.06 | 1.26 | 1.16 | . 58 | . 97 | 1.06 | . 48 | . 39 | . 58 | . 77 | . 00 | 12.00 |
| (2) | . 09 | . 09 | . 11 | . 09 | . 27 | . 20 | . 25 | . 29 | . 27 | . 13 | . 22 | . 25 | . 11 | . 09 | . 13 | . 18 | . 00 | 2.79 |
| 4.1-5.0 | 10 | 5 | 4 | 0 | 3 | 8 | 16 | 25 | 27 | 12 | 10 | 15 | 9 | 13 | 21 | 16 | 0 | 194 |
| (1) | . 97 | . 48 | . 39 | . 00 | . 29 | . 77 | 1.55 | 2.42 | 2.61 | 1.16 | . 97 | 1.45 | . 87 | 1.26 | 2.03 | 1.55 | . 00 | 18.78 |
| (2) | . 22 | . 11 | . 09 | . 00 | . 07 | . 18 | . 36 | . 56 | . 61 | . 27 | . 22 | . 34 | . 20 | . 29 | . 47 | . 36 | . 00 | 4.36 |
| 5.1-6.0 | 11 | 3 | 1 | 2 | 4 | 0 | 6 | 29 | 26 | 21 | 27 | 18 | 7 | 15 | 14 | 31 | 0 | 215 |
| (1) | 1.06 | . 29 | . 10 | . 19 | . 39 | . 00 | . 58 | 2.81 | 2.52 | 2.03 | 2.61 | 1.74 | . 68 | 1.45 | 1.36 | 3.00 | . 00 | 20.81 |
| (2) | . 25 | . 07 | . 02 | . 04 | . 09 | . 00 | . 13 | . 65 | . 58 | . 47 | . 61 | . 40 | . 16 | . 34 | . 31 | . 70 | . 00 | 4.83 |
| $6.1-8.0$ | 12 | 4 | 0 | 0 | 0 | 1 | 4 | 15 | 24 | 48 | 86 | 8 | 9 | 12 | 22 | 14 | 0 | 259 |
| (1) | 1.16 | . 39 | . 00 | . 00 | . 00 | . 10 | . 39 | 1.45 | 2.32 | 4.65 | 8.33 | . 77 | . 87 | 1.16 | 2.13 | 1.36 | . 00 | 25.07 |
| (2) | . 27 | . 09 | . 00 | . 00 | . 00 | . 02 | . 09 | . 34 | . 54 | 1.08 | 1.93 | . 18 | . 20 | . 27 | . 49 | . 31 | . 00 | 5.82 |
| 8.1-10.0 | 3 | 2 | 0 | 1 | 0 | 0 | 0 | 2 | 4 | 21 | 24 | 7 | 4 | 5 | 0 | 1 | 0 | 74 |
| (1) | . 29 | . 19 | . 00 | . 10 | . 00 | . 00 | . 00 | . 19 | . 39 | 2.03 | 2.32 | . 68 | . 39 | . 48 | . 00 | . 10 | . 00 | 7.16 |
| (2) | . 07 | . 04 | . 00 | . 02 | . 00 | . 00 | . 00 | . 04 | . 09 | . 47 | . 54 | . 16 | . 09 | . 11 | . 00 | . 02 | . 00 | 1.66 |
| 10.1-89.5 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| (1) | . 00 | . 10 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 58 | . 10 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 77 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 13 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 18 |
| ALL SPEEDS | 54 | 27 | 22 | 13 | 28 | 28 | 52 | 101 | 105 | 123 | 176 | 66 | 36 | 58 | 68 | 76 | 0 | 1033 |
| (1) | 5.23 | 2.61 | 2.13 | 1.26 | 2.71 | 2.71 | 5.03 | 9.78 | 10.16 | 11.91 | 17.04 | 6.39 | 3.48 | 5.61 | 6.58 | 7.36 | . 00 | 100.00 |
| (2) | 1.21 | . 61 | . 49 | . 29 | . 63 | . 63 | 1.17 | 2.27 | 2.36 | 2.76 | 3.96 | 1.48 | . 81 | 1.30 | 1.53 | 1.71 | . 00 | 23.21 |

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAG
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD


CC MAY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS F CLASS FREQUENCY (PERCENT) $=10.5$

|  | WIND DIRECTION |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 21 | . 00 | . 00 | . 00 | . 21 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 43 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 04 |
| .5-1.0 | 1 | 0 | 0 | 1 | 0 | 2 | 0 | 2 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 9 |
| (1) | . 21 | . 00 | . 00 | . 21 | . 00 | . 43 | . 00 | . 43 | . 21 | . 21 | . 00 | . 00 | . 21 | . 00 | . 00 | . 00 | . 00 | 1.92 |
| (2) | . 02 | . 00 | . 00 | . 02 | . 00 | . 04 | . 00 | . 04 | . 02 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 20 |
| 1.1-1.5 | 0 | 1 | 1 | 1 | 2 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 9 |
| (1) | . 00 | . 21 | . 21 | . 21 | . 43 | . 21 | . 00 | . 00 | . 21 | . 00 | . 21 | . 00 | . 21 | . 00 | . 00 | . 00 | . 00 | 1.92 |
| (2) | . 00 | . 02 | . 02 | . 02 | . 04 | . 02 | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 20 |
| 1.6-2.0 | 1 | 0 | 1 | 2 | 0 | 1 | 2 | 1 | 1 | 0 | 1 | 1 | 0 | 1 | 4 | 0 | 0 | 16 |
| (1) | . 21 | . 00 | . 21 | . 43 | . 00 | . 21 | . 43 | . 21 | . 21 | . 00 | . 21 | . 21 | . 00 | . 21 | . 85 | . 00 | . 00 | 3.41 |
| (2) | . 02 | . 00 | . 02 | . 04 | . 00 | . 02 | . 04 | . 02 | . 02 | . 00 | . 02 | . 02 | . 00 | . 02 | . 09 | . 00 | . 00 | . 36 |
| 2.1-3.0 | 6 | 1 | 3 | 2 | 2 | 3 | 1 | 2 | 2 | 3 | 3 | 2 | 4 | 4 | 0 | 2 | 0 | 40 |
| (1) | 1.28 | . 21 | . 64 | . 43 | . 43 | . 64 | . 21 | . 43 | . 43 | . 64 | . 64 | . 43 | . 85 | . 85 | . 00 | . 43 | . 00 | 8.53 |
| (2) | . 13 | . 02 | . 07 | . 04 | . 04 | . 07 | . 02 | . 04 | . 04 | . 07 | . 07 | . 04 | . 09 | . 09 | . 00 | . 04 | . 00 | . 90 |
| 3.1-4.0 | 1 | 1 | 1 | 1 | 3 | 1 | 3 | 3 | 8 | 7 | 4 | 3 | 3 | 2 | 3 | 2 | 0 | 46 |
| (1) | . 21 | . 21 | . 21 | . 21 | . 64 | . 21 | . 64 | . 64 | 1.71 | 1.49 | . 85 | . 64 | . 64 | . 43 | . 64 | . 43 | . 00 | 9.81 |
| (2) | . 02 | . 02 | . 02 | . 02 | . 07 | . 02 | . 07 | . 07 | . 18 | . 16 | . 09 | . 07 | . 07 | . 04 | . 07 | . 04 | . 00 | 1.03 |
| 4.1-5.0 | 5 | 2 | 1 | 0 | 0 | 0 | 4 | 10 | 9 | 7 | 5 | 6 | 7 | 5 | 8 | 11 | 0 | 80 |
| (1) | 1.07 | . 43 | . 21 | . 00 | . 00 | . 00 | . 85 | 2.13 | 1.92 | 1.49 | 1.07 | 1.28 | 1.49 | 1.07 | 1.71 | 2.35 | . 00 | 17.06 |
| (2) | . 11 | . 04 | . 02 | . 00 | . 00 | . 00 | . 09 | . 22 | . 20 | . 16 | . 11 | . 13 | . 16 | . 11 | . 18 | . 25 | . 00 | 1.80 |
| 5.1-6.0 | 2 | 2 | 0 | 0 | 0 | 0 | 5 | 6 | 20 | 14 | 11 | 7 | 9 | 4 | 10 | 10 | 0 | 100 |
| (1) | . 43 | . 43 | . 00 | . 00 | . 00 | . 00 | 1.07 | 1.28 | 4.26 | 2.99 | 2.35 | 1.49 | 1.92 | . 85 | 2.13 | 2.13 | . 00 | 21.32 |
| (2) | . 04 | . 04 | . 00 | . 00 | . 00 | . 00 | . 11 | . 13 | . 45 | . 31 | . 25 | . 16 | . 20 | . 09 | . 22 | . 22 | . 00 | 2.25 |
| $6.1-8.0$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 20 | 51 | 52 | 10 | 6 | 5 | 15 | 1 | 0 | 163 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 64 | 4.26 | 10.87 | 11.09 | 2.13 | 1.28 | 1.07 | 3.20 | . 21 | . 00 | 34.75 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 | . 45 | 1.15 | 1.17 | . 22 | . 13 | . 11 | . 34 | . 02 | . 00 | 3.66 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 4 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 21 | . 00 | . 21 | . 43 | . 00 | . 00 | . 00 | . 00 | . 00 | . 85 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 04 | . 00 | . 00 | . 00 | . 00 | . 00 | . 09 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 16 | 7 | 7 | 7 | 7 | 8 | 16 | 27 | 63 | 83 | 79 | 31 | 31 | 21 | 40 | 26 | 0 | 469 |
| (1) | 3.41 | 1.49 | 1.49 | 1.49 | 1.49 | 1.71 | 3.41 | 5.76 | 13.43 | 17.70 | 16.84 | 6.61 | 6.61 | 4.48 | 8.53 | 5.54 | . 00 | 100.00 |
| (2) | . 36 | . 16 | . 16 | . 16 | . 16 | . 18 | . 36 | . 61 | 1.42 | 1.87 | 1.78 | . 70 | . 70 | . 47 | . 90 | . 58 | . 00 | 10.54 |

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD


CC MAY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS G CLASS FREQUENCY (PERCENT) = 6.63

|  | WIND DIRECTION |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| (1) | . 00 | . 34 | . 00 | . 00 | . 00 | . 00 | . 34 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 68 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 04 |
| .5-1.0 | 3 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 7 |
| (1) | 1.02 | . 34 | . 00 | . 00 | . 00 | . 00 | . 34 | . 00 | . 00 | . 34 | . 00 | . 00 | . 34 | . 00 | . 00 | . 00 | . 00 | 2.37 |
| (2) | . 07 | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 16 |
| 1.1-1.5 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 9 |
| (1) | . 00 | . 00 | . 68 | . 00 | . 00 | . 00 | . 00 | . 68 | . 68 | . 00 | . 68 | . 34 | . 00 | . 00 | . 00 | . 00 | . 00 | 3.05 |
| (2) | . 00 | . 00 | . 04 | . 00 | . 00 | . 00 | . 00 | . 04 | . 04 | . 00 | . 04 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 20 |
| 1.6-2.0 | 2 | 2 | 1 | 1 | 0 | 1 | 2 | 0 | 2 | 2 | 2 | 1 | 2 | 1 | 0 | 0 | 0 | 19 |
| (1) | . 68 | . 68 | . 34 | . 34 | . 00 | . 34 | . 68 | . 00 | . 68 | . 68 | . 68 | . 34 | . 68 | . 34 | . 00 | . 00 | . 00 | 6.44 |
| (2) | . 04 | . 04 | . 02 | . 02 | . 00 | . 02 | . 04 | . 00 | . 04 | . 04 | . 04 | . 02 | . 04 | . 02 | . 00 | . 00 | . 00 | . 43 |
| 2.1-3.0 | 2 | 2 | 0 | 3 | 3 | 2 | 0 | 2 | 3 | 2 | 2 | 3 | 2 | 0 | 2 | 2 | 0 | 30 |
| (1) | . 68 | . 68 | . 00 | 1.02 | 1.02 | . 68 | . 00 | . 68 | 1.02 | . 68 | . 68 | 1.02 | . 68 | . 00 | . 68 | . 68 | . 00 | 10.17 |
| (2) | . 04 | . 04 | . 00 | . 07 | . 07 | . 04 | . 00 | . 04 | . 07 | . 04 | . 04 | . 07 | . 04 | . 00 | . 04 | . 04 | . 00 | . 67 |
| 3.1-4.0 | 5 | 1 | 0 | 1 | 1 | 0 | 2 | 3 | 5 | 4 | 3 | 4 | 1 | 2 | 2 | 2 | 0 | 36 |
| (1) | 1.69 | . 34 | . 00 | . 34 | . 34 | . 00 | . 68 | 1.02 | 1.69 | 1.36 | 1.02 | 1.36 | . 34 | . 68 | . 68 | . 68 | . 00 | 12.20 |
| (2) | . 11 | . 02 | . 00 | . 02 | . 02 | . 00 | . 04 | . 07 | . 11 | . 09 | . 07 | . 09 | . 02 | . 04 | . 04 | . 04 | . 00 | . 81 |
| 4.1-5.0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 8 | 8 | 5 | 4 | 5 | 4 | 7 | 3 | 0 | 53 |
| (1) | . 68 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 2.37 | 2.71 | 2.71 | 1.69 | 1.36 | 1.69 | 1.36 | 2.37 | 1.02 | . 00 | 17.97 |
| (2) | . 04 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 16 | . 18 | . 18 | . 11 | . 09 | . 11 | . 09 | . 16 | . 07 | . 00 | 1.19 |
| 5.1-6.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 9 | 15 | 11 | 4 | 1 | 8 | 5 | 2 | 0 | 58 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.02 | 3.05 | 5.08 | 3.73 | 1.36 | . 34 | 2.71 | 1.69 | . 68 | . 00 | 19.66 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 | . 20 | . 34 | . 25 | . 09 | . 02 | . 18 | . 11 | . 04 | . 00 | 1.30 |
| $6.1-8.0$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 15 | 19 | 14 | 7 | 9 | 6 | 8 | 0 | 0 | 80 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 68 | 5.08 | 6.44 | 4.75 | 2.37 | 3.05 | 2.03 | 2.71 | . 00 | . 00 | 27.12 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 04 | . 34 | . 43 | . 31 | . 16 | . 20 | . 13 | . 18 | . 00 | . 00 | 1.80 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 34 | . 00 | . 00 | . 34 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 14 | 7 | 3 | 5 | 4 | 3 | 6 | 19 | 44 | 51 | 39 | 24 | 21 | 21 | 25 | 9 | 0 | 295 |
| (1) | 4.75 | 2.37 | 1.02 | 1.69 | 1.36 | 1.02 | 2.03 | 6.44 | 14.92 | 17.29 | 13.22 | 8.14 | 7.12 | 7.12 | 8.47 | 3.05 | . 00 | 100.00 |
| (2) | . 31 | . 16 | . 07 | . 11 | . 09 | . 07 | . 13 | . 43 | . 99 | 1.15 | . 88 | . 54 | . 47 | . 47 | . 56 | . 20 | . 00 | 6.63 |

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD



Table 2.3-34—\{CCNPP 197 ft ( 60 m) May JFD (2000-2005) \} (Page 8 of 8)
CC MAY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS ALL CLASS FREQUENCY (PERCENT) = 100.00

$\stackrel{70}{\stackrel{7}{i}}$

Table 2.3-35—\{CCNPP 197 ft ( 60 m) June JFD (2000-2005) \}
(Page 1 of 8 )
CC JUNE MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS A CLASS FREQUENCY (PERCENT) = 13.90

(1) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD


CC JUNE MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS B CLASS FREQUENCY (PERCENT) = 5.54

|  |  |  |  |  |  |  |  | ND | RECTIO | N FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| (1) | . 00 | . 42 | . 00 | . 00 | . 42 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 84 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 |
| 1.1-1.5 | 0 | 0 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| (1) | . 00 | . 00 | . 42 | . 42 | . 42 | . 42 | . 00 | . 00 | . 00 | . 00 | 1.26 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 2.93 |
| (2) | . 00 | . 00 | . 02 | . 02 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 07 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 16 |
| 1.6-2.0 | 2 | 1 | 0 | 2 | 4 | 4 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15 |
| (1) | . 84 | . 42 | . 00 | . 84 | 1.67 | 1.67 | . 00 | . 00 | . 42 | . 42 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 6.28 |
| (2) | . 05 | . 02 | . 00 | . 05 | . 09 | . 09 | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 35 |
| 2.1-3.0 | 6 | 13 | 5 | 6 | 8 | 5 | 6 | 6 | 3 | 3 | 4 | 2 | 1 | 1 | 0 | 3 | 0 | 72 |
| (1) | 2.51 | 5.44 | 2.09 | 2.51 | 3.35 | 2.09 | 2.51 | 2.51 | 1.26 | 1.26 | 1.67 | . 84 | . 42 | . 42 | . 00 | 1.26 | . 00 | 30.13 |
| (2) | . 14 | . 30 | . 12 | . 14 | . 19 | . 12 | . 14 | . 14 | . 07 | . 07 | . 09 | . 05 | . 02 | . 02 | . 00 | . 07 | . 00 | 1.67 |
| 3.1-4.0 | 2 | 8 | 1 | 2 | 3 | 3 | 4 | 3 | 3 | 3 | 4 | 4 | 3 | 5 | 1 | 1 | 0 | 50 |
| (1) | . 84 | 3.35 | . 42 | . 84 | 1.26 | 1.26 | 1.67 | 1.26 | 1.26 | 1.26 | 1.67 | 1.67 | 1.26 | 2.09 | . 42 | . 42 | . 00 | 20.92 |
| (2) | . 05 | . 19 | . 02 | . 05 | . 07 | . 07 | . 09 | . 07 | . 07 | . 07 | . 09 | . 09 | . 07 | . 12 | . 02 | . 02 | . 00 | 1.16 |
| 4.1-5.0 | 1 | 1 | 0 | 1 | 1 | 1 | 2 | 8 | 0 | 5 | 7 | 4 | 2 | 2 | 4 | 1 | 0 | 40 |
| (1) | . 42 | . 42 | . 00 | . 42 | . 42 | . 42 | . 84 | 3.35 | . 00 | 2.09 | 2.93 | 1.67 | . 84 | . 84 | 1.67 | . 42 | . 00 | 16.74 |
| (2) | . 02 | . 02 | . 00 | . 02 | . 02 | . 02 | . 05 | . 19 | . 00 | . 12 | . 16 | . 09 | . 05 | . 05 | . 09 | . 02 | . 00 | . 93 |
| 5.1-6.0 | 4 | 1 | 0 | 0 | 0 | 0 | 1 | 5 | 0 | 6 | 8 | 0 | 1 | 1 | 0 | 1 | 0 | 28 |
| (1) | 1.67 | . 42 | . 00 | . 00 | . 00 | . 00 | . 42 | 2.09 | . 00 | 2.51 | 3.35 | . 00 | . 42 | . 42 | . 00 | . 42 | . 00 | 11.72 |
| (2) | . 09 | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 | . 12 | . 00 | . 14 | . 19 | . 00 | . 02 | . 02 | . 00 | . 02 | . 00 | . 65 |
| 6.1-8.0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 4 | 0 | 5 | 1 | 1 | 1 | 0 | 1 | 2 | 0 | 18 |
| (1) | . 42 | . 00 | . 00 | . 00 | . 84 | . 00 | . 00 | 1.67 | . 00 | 2.09 | . 42 | . 42 | . 42 | . 00 | . 42 | . 84 | . 00 | 7.53 |
| (2) | . 02 | . 00 | . 00 | . 00 | . 05 | . 00 | . 00 | . 09 | . 00 | . 12 | . 02 | . 02 | . 02 | . 00 | . 02 | . 05 | . 00 | . 42 |
| 8.1-10.0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 6 |
| (1) | . 00 | . 42 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.26 | . 00 | . 42 | . 00 | . 00 | . 00 | . 00 | . 00 | . 42 | . 00 | 2.51 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 14 |
| 10.1-89.5 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 42 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 42 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| ALL SPEEDS | 16 | 27 | 7 | 12 | 20 | 14 | 13 | 29 | 7 | 24 | 27 | 11 | 8 | 9 | 6 | 9 | 0 | 239 |
| (1) | 6.69 | 11.30 | 2.93 | 5.02 | 8.37 | 5.86 | 5.44 | 12.13 | 2.93 | 10.04 | 11.30 | 4.60 | 3.35 | 3.77 | 2.51 | 3.77 | .00 | 100.00 |
| (2) | . 37 | . 63 | . 16 | . 28 | . 46 | . 32 | . 30 | . 67 | . 16 | . 56 | . 63 | . 25 | . 19 | . 21 | . 14 | . 21 | . 00 | 5.54 |

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

## 

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CC JUNE MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS C CLASS FREQUENCY (PERCENT) = 6.23

| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 37 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 37 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| 1.1-1.5 | 0 | 1 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 6 |
| (1) | . 00 | . 37 | . 00 | . 37 | . 74 | . 00 | . 00 | . 00 | . 00 | . 00 | . 37 | . 00 | . 37 | . 00 | . 00 | . 00 | . 00 | 2.23 |
| (2) | . 00 | . 02 | . 00 | . 02 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 14 |
| 1.6-2.0 | 2 | 0 | 2 | 7 | 1 | 0 | 1 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 16 |
| (1) | . 74 | . 00 | . 74 | 2.60 | . 37 | . 00 | . 37 | . 00 | . 00 | . 37 | . 74 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 5.95 |
| (2) | . 05 | . 00 | . 05 | . 16 | . 02 | . 00 | . 02 | . 00 | . 00 | . 02 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 37 |
| 2.1-3.0 | 14 | 15 | 5 | 5 | 6 | 4 | 8 | 2 | 0 | 0 | 7 | 0 | 1 | 2 | 1 | 5 | 0 | 75 |
| (1) | 5.20 | 5.58 | 1.86 | 1.86 | 2.23 | 1.49 | 2.97 | . 74 | . 00 | . 00 | 2.60 | . 00 | . 37 | . 74 | . 37 | 1.86 | . 00 | 27.88 |
| (2) | . 32 | . 35 | . 12 | . 12 | . 14 | . 09 | . 19 | . 05 | . 00 | . 00 | . 16 | . 00 | . 02 | . 05 | . 02 | . 12 | . 00 | 1.74 |
| 3.1-4.0 | 13 | 7 | 0 | 2 | 4 | 2 | 2 | 5 | 5 | 0 | 7 | 3 | 3 | 3 | 7 | 1 | 0 | 64 |
| (1) | 4.83 | 2.60 | . 00 | . 74 | 1.49 | . 74 | . 74 | 1.86 | 1.86 | . 00 | 2.60 | 1.12 | 1.12 | 1.12 | 2.60 | . 37 | . 00 | 23.79 |
| (2) | . 30 | . 16 | . 00 | . 05 | . 09 | . 05 | . 05 | . 12 | . 12 | . 00 | . 16 | . 07 | . 07 | . 07 | . 16 | . 02 | . 00 | 1.48 |
| 4.1-5.0 | 2 | 2 | 1 | 1 | 3 | 0 | 1 | 4 | 2 | 6 | 3 | 7 | 2 | 2 | 6 | 2 | 0 | 44 |
| (1) | . 74 | . 74 | . 37 | . 37 | 1.12 | . 00 | . 37 | 1.49 | . 74 | 2.23 | 1.12 | 2.60 | . 74 | . 74 | 2.23 | . 74 | . 00 | 16.36 |
| (2) | . 05 | . 05 | . 02 | . 02 | . 07 | . 00 | . 02 | . 09 | . 05 | . 14 | . 07 | . 16 | . 05 | . 05 | . 14 | . 05 | . 00 | 1.02 |
| 5.1-6.0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 7 | 2 | 2 | 10 | 1 | 3 | 2 | 2 | 3 | 0 | 36 |
| (1) | . 74 | . 74 | . 00 | . 00 | . 00 | . 00 | . 00 | 2.60 | . 74 | . 74 | 3.72 | . 37 | 1.12 | . 74 | . 74 | 1.12 | . 00 | 13.38 |
| (2) | . 05 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 16 | . 05 | . 05 | . 23 | . 02 | . 07 | . 05 | . 05 | . 07 | . 00 | . 83 |
| 6.1-8.0 | 1 | 2 | 1 | 1 | 0 | 1 | 0 | 4 | 0 | 3 | 2 | 1 | 1 | 0 | 1 | 1 | 0 | 19 |
| (1) | . 37 | . 74 | . 37 | . 37 | . 00 | . 37 | . 00 | 1.49 | . 00 | 1.12 | . 74 | . 37 | . 37 | . 00 | . 37 | . 37 | . 00 | 7.06 |
| (2) | . 02 | . 05 | . 02 | . 02 | . 00 | . 02 | . 00 | . 09 | . 00 | . 07 | . 05 | . 02 | . 02 | . 00 | . 02 | . 02 | . 00 | . 44 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 0 | 5 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 37 | . 00 | . 00 | . 37 | . 00 | . 00 | . 37 | . 00 | . 00 | . 00 | . 37 | . 37 | . 00 | 1.86 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 12 |
| 10.1-89.5 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 3 |
| (1) | . 00 | . 00 | . 37 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 37 | . 00 | . 37 | . 00 | . 00 | 1.12 |
| (2) | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 07 |
| ALL SPEEDS | 34 | 29 | 10 | 17 | 17 | 7 | 12 | 24 | 9 | 12 | 33 | 12 | 12 | 9 | 19 | 13 | 0 | 269 |
| (1) | 12.64 | 10.78 | 3.72 | 6.32 | 6.32 | 2.60 | 4.46 | 8.92 | 3.35 | 4.46 | 12.27 | 4.46 | 4.46 | 3.35 | 7.06 | 4.83 | . 00 | 100.00 |
| (2) | . 79 | . 67 | . 23 | . 39 | . 39 | . 16 | . 28 | . 56 | . 21 | . 28 | . 76 | . 28 | . 28 | . 21 | . 44 | . 30 | . 00 | 6.23 |

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD


CC JUNE MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS D CLASS FREQUENCY (PERCENT) = 30.53

| IND DIRECTION FROM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 08 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 08 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| . $2-.4$ | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 08 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 08 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| .5-1.0 | 3 | 1 | 2 | 2 | 2 | 1 | 2 | 1 | 1 | 1 | 1 | 2 | 2 | 1 | 2 | 3 | 0 | 27 |
| (1) | . 23 | . 08 | . 15 | . 15 | . 15 | . 08 | . 15 | . 08 | . 08 | . 08 | . 08 | . 15 | . 15 | . 08 | . 15 | . 23 | . 00 | 2.05 |
| (2) | . 07 | . 02 | . 05 | . 05 | . 05 | . 02 | . 05 | . 02 | . 02 | . 02 | . 02 | . 05 | . 05 | . 02 | . 05 | . 07 | . 00 | . 63 |
| 1.1-1.5 | 5 | 6 | 2 | 6 | 10 | 2 | 1 | 1 | 2 | 3 | 3 | 5 | 4 | 2 | 4 | 1 | 0 | 57 |
| (1) | . 38 | . 46 | . 15 | . 46 | . 76 | . 15 | . 08 | . 08 | . 15 | . 23 | . 23 | . 38 | . 30 | . 15 | . 30 | . 08 | . 00 | 4.32 |
| (2) | . 12 | . 14 | . 05 | . 14 | . 23 | . 05 | . 02 | . 02 | . 05 | . 07 | . 07 | . 12 | . 09 | . 05 | . 09 | . 02 | . 00 | 1.32 |
| 1.6-2.0 | 8 | 7 | 9 | 7 | 8 | 13 | 5 | 1 | 2 | 3 | 5 | 8 | 4 | 3 | 3 | 2 | 0 | 88 |
| (1) | . 61 | . 53 | . 68 | . 53 | . 61 | . 99 | . 38 | . 08 | . 15 | . 23 | . 38 | . 61 | . 30 | . 23 | . 23 | . 15 | . 00 | 6.68 |
| (2) | . 19 | . 16 | . 21 | . 16 | . 19 | . 30 | . 12 | . 02 | . 05 | . 07 | . 12 | . 19 | . 09 | . 07 | . 07 | . 05 | . 00 | 2.04 |
| 2.1-3.0 | 26 | 35 | 12 | 20 | 16 | 10 | 9 | 12 | 4 | 16 | 10 | 12 | 8 | 6 | 8 | 6 | 0 | 210 |
| (1) | 1.97 | 2.66 | . 91 | 1.52 | 1.21 | . 76 | . 68 | . 91 | . 30 | 1.21 | . 76 | . 91 | . 61 | . 46 | . 61 | . 46 | . 00 | 15.93 |
| (2) | . 60 | . 81 | . 28 | . 46 | . 37 | . 23 | . 21 | . 28 | . 09 | . 37 | . 23 | . 28 | . 19 | . 14 | . 19 | . 14 | . 00 | 4.86 |
| $3.1-4.0$ | 19 | 14 | 7 | 20 | 20 | 16 | 9 | 15 | 19 | 22 | 14 | 13 | 8 | 14 | 19 | 12 | 0 | 241 |
| (1) | 1.44 | 1.06 | . 53 | 1.52 | 1.52 | 1.21 | . 68 | 1.14 | 1.44 | 1.67 | 1.06 | . 99 | . 61 | 1.06 | 1.44 | . 91 | . 00 | 18.29 |
| (2) | . 44 | . 32 | . 16 | . 46 | . 46 | . 37 | . 21 | . 35 | . 44 | . 51 | . 32 | . 30 | . 19 | . 32 | . 44 | . 28 | . 00 | 5.58 |
| 4.1-5.0 | 21 | 7 | 13 | 40 | 22 | 4 | 1 | 27 | 11 | 18 | 21 | 11 | 10 | 10 | 10 | 16 | 0 | 242 |
| (1) | 1.59 | . 53 | . 99 | 3.03 | 1.67 | . 30 | . 08 | 2.05 | . 83 | 1.37 | 1.59 | . 83 | . 76 | . 76 | . 76 | 1.21 | . 00 | 18.36 |
| (2) | . 49 | . 16 | . 30 | . 93 | . 51 | . 09 | . 02 | . 63 | . 25 | . 42 | . 49 | . 25 | . 23 | . 23 | . 23 | . 37 | . 00 | 5.61 |
| 5.1-6.0 | 21 | 17 | 13 | 28 | 8 | 3 | 3 | 35 | 4 | 13 | 20 | 11 | 4 | 4 | 16 | 10 | 0 | 210 |
| (1) | 1.59 | 1.29 | . 99 | 2.12 | . 61 | . 23 | . 23 | 2.66 | . 30 | . 99 | 1.52 | . 83 | . 30 | . 30 | 1.21 | . 76 | . 00 | 15.93 |
| (2) | . 49 | . 39 | . 30 | . 65 | . 19 | . 07 | . 07 | . 81 | . 09 | . 30 | . 46 | . 25 | . 09 | . 09 | . 37 | . 23 | . 00 | 4.86 |
| 6.1-8.0 | 24 | 17 | 20 | 14 | 13 | 2 | 6 | 23 | 1 | 14 | 23 | 5 | 1 | 3 | 16 | 14 | 0 | 196 |
| (1) | 1.82 | 1.29 | 1.52 | 1.06 | . 99 | . 15 | . 46 | 1.75 | . 08 | 1.06 | 1.75 | . 38 | . 08 | . 23 | 1.21 | 1.06 | . 00 | 14.87 |
| (2) | . 56 | . 39 | . 46 | . 32 | . 30 | . 05 | . 14 | . 53 | . 02 | . 32 | . 53 | . 12 | . 02 | . 07 | . 37 | . 32 | . 00 | 4.54 |
| 8.1-10.0 | 7 | 6 | 2 | 2 | 2 | 0 | 0 | 5 | 0 | 1 | 1 | 0 | 1 | 4 | 1 | 5 | 0 | 37 |
| (1) | . 53 | . 46 | . 15 | . 15 | . 15 | . 00 | . 00 | . 38 | . 00 | . 08 | . 08 | . 00 | . 08 | . 30 | . 08 | . 38 | . 00 | 2.81 |
| (2) | . 16 | . 14 | . 05 | . 05 | . 05 | . 00 | . 00 | . 12 | . 00 | . 02 | . 02 | . 00 | . 02 | . 09 | . 02 | . 12 | . 00 | . 86 |
| 10.1-89.5 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 3 | 0 | 0 | 8 |
| (1) | . 00 | . 23 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 15 | . 23 | . 00 | . 00 | . 61 |
| (2) | . 00 | . 07 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 07 | . 00 | . 00 | . 19 |
| ALL SPEEDS | 134 | 114 | 80 | 139 | 101 | 52 | 36 | 120 | 44 | 91 | 98 | 67 | 42 | 49 | 82 | 69 | 0 | 1318 |
| (1) | 10.17 | 8.65 | 6.07 | 10.55 | 7.66 | 3.95 | 2.73 | 9.10 | 3.34 | 6.90 | 7.44 | 5.08 | 3.19 | 3.72 | 6.22 | 5.24 | . 00 | 100.00 |
| (2) | 3.10 | 2.64 | 1.85 | 3.22 | 2.34 | 1.20 | . 83 | 2.78 | 1.02 | 2.11 | 2.27 | 1.55 | . 97 | 1.14 | 1.90 | 1.60 | . 00 | 30.53 |
| (1) = PERCENT | OF ALI | GOOD | OBSERV | VATIONS | FOR T | IS PA |  |  |  |  |  |  |  |  |  |  |  |  |
| (2)=PERCENT | F ALL G | OD OBS | ervatio | ONS FOR | THIS P | ERIOD |  |  |  |  |  |  |  |  |  |  |  |  |

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Table 2.3-35—\{CCNPP 197 ft ( 60 m) June JFD (2000-2005) \}
(Page 5 of 8)
CC JUNE MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS E CLASS FREQUENCY (PERCENT) = 21.82

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
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CC JUNE MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS F CLASS FREQUENCY (PERCENT) = 12.90

|  | WIND DIRECTION FROM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 6 |
| (1) | . 00 | . 00 | . 18 | . 00 | . 18 | . 00 | . 00 | . 18 | . 00 | . 00 | . 18 | . 00 | . 00 | . 00 | . 36 | . 00 | . 00 | 1.08 |
| (2) | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 05 | . 00 | . 00 | . 14 |
| 1.1-1.5 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 7 |
| (1) | . 00 | . 18 | . 00 | . 00 | . 00 | . 00 | . 18 | . 36 | . 18 | . 18 | . 00 | . 00 | . 00 | . 00 | . 00 | . 18 | . 00 | 1.26 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 | . 05 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 16 |
| 1.6-2.0 | 0 | 2 | 0 | 2 | 0 | 1 | 2 | 1 | 2 | 1 | 2 | 1 | 2 | 1 | 1 | 2 | 0 | 20 |
| (1) | . 00 | . 36 | . 00 | . 36 | . 00 | . 18 | . 36 | . 18 | . 36 | . 18 | . 36 | . 18 | . 36 | . 18 | . 18 | . 36 | . 00 | 3.59 |
| (2) | . 00 | . 05 | . 00 | . 05 | . 00 | . 02 | . 05 | . 02 | . 05 | . 02 | . 05 | . 02 | . 05 | . 02 | . 02 | . 05 | . 00 | . 46 |
| 2.1-3.0 | 4 | 2 | 1 | 1 | 0 | 2 | 4 | 1 | 4 | 2 | 3 | 7 | 2 | 2 | 2 | 3 | 0 | 40 |
| (1) | . 72 | . 36 | . 18 | . 18 | . 00 | . 36 | . 72 | . 18 | . 72 | . 36 | . 54 | 1.26 | . 36 | . 36 | . 36 | . 54 | . 00 | 7.18 |
| (2) | . 09 | . 05 | . 02 | . 02 | . 00 | . 05 | . 09 | . 02 | . 09 | . 05 | . 07 | . 16 | . 05 | . 05 | . 05 | . 07 | . 00 | . 93 |
| 3.1-4.0 | 4 | 0 | 0 | 0 | 0 | 1 | 3 | 2 | 9 | 12 | 6 | 6 | 5 | 8 | 2 | 2 | 0 | 60 |
| (1) | . 72 | . 00 | . 00 | . 00 | . 00 | . 18 | . 54 | . 36 | 1.62 | 2.15 | 1.08 | 1.08 | . 90 | 1.44 | . 36 | . 36 | . 00 | 10.77 |
| (2) | . 09 | . 00 | . 00 | . 00 | . 00 | . 02 | . 07 | . 05 | . 21 | . 28 | . 14 | . 14 | . 12 | . 19 | . 05 | . 05 | . 00 | 1.39 |
| 4.1-5.0 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 6 | 23 | 24 | 18 | 13 | 12 | 6 | 6 | 3 | 0 | 114 |
| (1) | . 36 | . 00 | . 00 | . 00 | . 00 | . 00 | . 18 | 1.08 | 4.13 | 4.31 | 3.23 | 2.33 | 2.15 | 1.08 | 1.08 | . 54 | . 00 | 20.47 |
| (2) | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 14 | . 53 | . 56 | . 42 | . 30 | . 28 | . 14 | . 14 | . 07 | . 00 | 2.64 |
| 5.1-6.0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 38 | 38 | 23 | 19 | 15 | 12 | 13 | 3 | 0 | 174 |
| (1) | . 18 | . 00 | . 00 | . 00 | . 00 | . 00 | . 36 | 1.80 | 6.82 | 6.82 | 4.13 | 3.41 | 2.69 | 2.15 | 2.33 | . 54 | . 00 | 31.24 |
| (2) | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 23 | . 88 | . 88 | . 53 | . 44 | . 35 | . 28 | . 30 | . 07 | . 00 | 4.03 |
| 6.1-8.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 13 | 39 | 34 | 15 | 4 | 4 | 18 | 1 | 0 | 133 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 90 | 2.33 | 7.00 | 6.10 | 2.69 | . 72 | . 72 | 3.23 | . 18 | . 00 | 23.88 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 12 | . 30 | . 90 | . 79 | . 35 | . 09 | . 09 | . 42 | . 02 | . 00 | 3.08 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 18 | . 36 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 54 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 11 | 5 | 2 | 3 | 1 | 4 | 13 | 28 | 90 | 118 | 89 | 61 | 40 | 33 | 44 | 15 | 0 | 557 |
| (1) | 1.97 | . 90 | . 36 | . 54 | . 18 | . 72 | 2.33 | 5.03 | 16.16 | 21.18 | 15.98 | 10.95 | 7.18 | 5.92 | 7.90 | 2.69 | . 00 | 100.00 |
| (2) | . 25 | . 12 | . 05 | . 07 | . 02 | . 09 | . 30 | . 65 | 2.08 | 2.73 | 2.06 | 1.41 | . 93 | . 76 | 1.02 | . 35 | . 00 | 12.90 |

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Table 2.3-35—\{CCNPP 197 ft ( 60 m) June JFD (2000-2005)\}
(Page 7 of 8)
CC JUNE MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS G CLASS FREQUENCY (PERCENT) = 9.08

| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| (1) | . 00 | . 00 | . 26 | . 00 | . 26 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 51 |
| (2) | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 |
| .5-1.0 | 1 | 0 | 1 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 1 | 0 | 0 | 2 | 2 | 1 | 0 | 12 |
| (1) | . 26 | . 00 | . 26 | . 00 | . 00 | . 26 | . 51 | . 00 | . 00 | . 26 | . 26 | . 00 | . 00 | . 51 | . 51 | . 26 | . 00 | 3.06 |
| (2) | . 02 | . 00 | . 02 | . 00 | . 00 | . 02 | . 05 | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 05 | . 05 | . 02 | . 00 | . 28 |
| 1.1-1.5 | 2 | 2 | 1 | 1 | 4 | 3 | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 | 2 | 1 | 0 | 22 |
| (1) | . 51 | . 51 | . 26 | . 26 | 1.02 | . 77 | . 00 | . 26 | . 26 | . 26 | . 00 | . 26 | . 26 | . 26 | . 51 | . 26 | . 00 | 5.61 |
| (2) | . 05 | . 05 | . 02 | . 02 | . 09 | . 07 | . 00 | . 02 | . 02 | . 02 | . 00 | . 02 | . 02 | . 02 | . 05 | . 02 | . 00 | . 51 |
| 1.6-2.0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 1 | 1 | 0 | 1 | 1 | 2 | 1 | 2 | 0 | 0 | 14 |
| (1) | . 00 | . 00 | . 00 | . 26 | . 26 | . 26 | . 51 | . 26 | . 26 | . 00 | . 26 | . 26 | . 51 | . 26 | . 51 | . 00 | . 00 | 3.57 |
| (2) | . 00 | . 00 | . 00 | . 02 | . 02 | . 02 | . 05 | . 02 | . 02 | . 00 | . 02 | . 02 | . 05 | . 02 | . 05 | . 00 | . 00 | . 32 |
| 2.1-3.0 | 3 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 3 | 1 | 4 | 3 | 2 | 3 | 0 | 25 |
| (1) | . 77 | . 00 | . 26 | . 26 | . 00 | . 00 | . 00 | . 00 | . 26 | . 77 | . 77 | . 26 | 1.02 | . 77 | . 51 | . 77 | . 00 | 6.38 |
| (2) | . 07 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 | . 07 | . 07 | . 02 | . 09 | . 07 | . 05 | . 07 | . 00 | . 58 |
| 3.1-4.0 | 2 | 0 | 0 | 1 | 1 | 0 | 0 | 4 | 4 | 7 | 10 | 6 | 9 | 9 | 3 | 5 | 0 | 61 |
| (1) | . 51 | . 00 | . 00 | . 26 | . 26 | . 00 | . 00 | 1.02 | 1.02 | 1.79 | 2.55 | 1.53 | 2.30 | 2.30 | . 77 | 1.28 | . 00 | 15.56 |
| (2) | . 05 | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 09 | . 09 | . 16 | . 23 | . 14 | . 21 | . 21 | . 07 | . 12 | . 00 | 1.41 |
| 4.1-5.0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 8 | 18 | 28 | 13 | 7 | 10 | 4 | 4 | 0 | 95 |
| (1) | . 26 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 51 | 2.04 | 4.59 | 7.14 | 3.32 | 1.79 | 2.55 | 1.02 | 1.02 | . 00 | 24.23 |
| (2) | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 19 | . 42 | . 65 | . 30 | . 16 | . 23 | . 09 | . 09 | . 00 | 2.20 |
| 5.1-6.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15 | 24 | 18 | 12 | 17 | 6 | 5 | 2 | 0 | 99 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 3.83 | 6.12 | 4.59 | 3.06 | 4.34 | 1.53 | 1.28 | . 51 | . 00 | 25.26 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 35 | . 56 | . 42 | . 28 | . 39 | . 14 | . 12 | . 05 | . 00 | 2.29 |
| 6.1-8.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 11 | 13 | 4 | 7 | 10 | 8 | 4 | 1 | 0 | 61 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 77 | 2.81 | 3.32 | 1.02 | 1.79 | 2.55 | 2.04 | 1.02 | . 26 | . 00 | 15.56 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 | . 25 | . 30 | . 09 | . 16 | . 23 | . 19 | . 09 | . 02 | . 00 | 1.41 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 26 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 26 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 9 | 2 | 4 | 4 | 7 | 5 | 4 | 11 | 41 | 68 | 65 | 41 | 50 | 40 | 24 | 17 | 0 | 392 |
| (1) | 2.30 | . 51 | 1.02 | 1.02 | 1.79 | 1.28 | 1.02 | 2.81 | 10.46 | 17.35 | 16.58 | 10.46 | 12.76 | 10.20 | 6.12 | 4.34 | . 00 | 100.00 |
| (2) | . 21 | . 05 | . 09 | . 09 | . 16 | . 12 | . 09 | . 25 | . 95 | 1.58 | 1.51 | . 95 | 1.16 | . 93 | . 56 | . 39 | . 00 | 9.08 |

(1) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD ObSERVATIONS FOR THIS PERIOD
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CC JUNE MET DATA JOINT FREQUENCY DISTRIBUTION（60－METER TOWER）
197．0 FT WIND DATA STABILITY CLASS ALL CLASS FREQUENCY（PERCENT）＝100．00

| WIND DIRECTION FROM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT $\begin{array}{r}\text { ．} 2 \\ \\ \\ \\ \\ \\ \text {（1）} \\ \text {（2）}\end{array}$ | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
|  | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 |
|  | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 |
| ． $2-\begin{array}{r}\text {（1）} \\ (2) \\ \text {（2）}\end{array}$ | 0 | 1 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
|  | ． 00 | ． 02 | ． 05 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 09 |
|  | ． 00 | ． 02 | ． 05 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 09 |
| ． $5-1.0$ | 4 | 2 | 5 | 3 | 4 | 3 | 5 | 3 | 2 | 2 | 4 | 2 | 3 | 3 | 8 | 4 | 0 | 57 |
| （1） | ． 09 | ． 05 | ． 12 | ． 07 | ． 09 | ． 07 | ． 12 | ． 07 | ． 05 | ． 05 | ． 09 | ． 05 | ． 07 | ． 07 | ． 19 | ． 09 | ． 00 | 1.32 |
| （2） | ． 09 | ． 05 | ． 12 | ． 07 | ． 09 | ． 07 | ． 12 | ． 07 | ． 05 | ． 05 | ． 09 | ． 05 | ． 07 | ． 07 | ． 19 | ． 09 | ． 00 | 1.32 |
| 1．1－1．5 | 8 | 10 | 8 | 13 | 17 | 6 | 3 | 6 | 4 | 7 | 8 | 6 | 7 | 4 | 6 | 4 | 0 | 117 |
| （1） | ． 19 | ． 23 | ． 19 | ． 30 | ． 39 | ． 14 | ． 07 | ． 14 | ． 09 | ． 16 | ． 19 | ． 14 | ． 16 | ． 09 | ． 14 | ． 09 | ． 00 | 2.71 |
| （2） | ． 19 | ． 23 | ． 19 | ． 30 | ． 39 | ． 14 | ． 07 | ． 14 | ． 09 | ． 16 | ． 19 | ． 14 | ． 16 | ． 09 | ． 14 | ． 09 | ． 00 | 2.71 |
| 1．6－2．0 | 14 | 11 | 12 | 23 | 22 | 19 | 13 | 4 | 8 | 8 | 14 | 13 | 9 | 6 | 7 | 6 | 0 | 189 |
| （1） | ． 32 | ． 25 | ． 28 | ． 53 | ． 51 | ． 44 | ． 30 | ． 09 | ． 19 | ． 19 | ． 32 | ． 30 | ． 21 | ． 14 | ． 16 | ． 14 | ． 00 | 4.38 |
| （2） | ． 32 | ． 25 | ． 28 | ． 53 | ． 51 | ． 44 | ． 30 | ． 09 | ． 19 | ． 19 | ． 32 | ． 30 | ． 21 | ． 14 | ． 16 | ． 14 | ． 00 | 4.38 |
| 2．1－3．0 | 65 | 81 | 36 | 50 | 45 | 37 | 38 | 28 | 27 | 35 | 53 | 35 | 22 | 25 | 19 | 28 | 0 | 624 |
| （1） | 1.51 | 1.88 | ． 83 | 1.16 | 1.04 | ． 86 | ． 88 | ． 65 | ． 63 | ． 81 | 1.23 | ． 81 | ． 51 | ． 58 | ． 44 | ． 65 | ． 00 | 14.45 |
| （2） | 1.51 | 1.88 | ． 83 | 1.16 | 1.04 | ． 86 | ． 88 | ． 65 | ． 63 | ． 81 | 1.23 | ． 81 | ． 51 | ． 58 | ． 44 | ． 65 | ． 00 | 14.45 |
| 3．1－4．0 | 64 | 50 | 12 | 28 | 38 | 34 | 32 | 48 | 69 | 64 | 70 | 63 | 48 | 50 | 48 | 32 | 0 | 750 |
| （1） | 1.48 | 1.16 | ． 28 | ． 65 | ． 88 | ． 79 | ． 74 | 1.11 | 1.60 | 1.48 | 1.62 | 1.46 | 1.11 | 1.16 | 1.11 | ． 74 | ． 00 | 17.37 |
| （2） | 1.48 | 1.16 | ． 28 | ． 65 | ． 88 | ． 79 | ． 74 | 1.11 | 1.60 | 1.48 | 1.62 | 1.46 | 1.11 | 1.16 | 1.11 | ． 74 | ． 00 | 17.37 |
| 4．1－5．0 | 54 | 21 | 15 | 44 | 27 | 11 | 27 | 88 | 80 | 116 | 145 | 82 | 49 | 50 | 49 | 42 | 0 | 900 |
| （1） | 1.25 | ． 49 | ． 35 | 1.02 | ． 63 | ． 25 | ． 63 | 2.04 | 1.85 | 2.69 | 3.36 | 1.90 | 1.14 | 1.16 | 1.14 | ． 97 | ． 00 | 20.85 |
| （2） | 1.25 | ． 49 | ． 35 | 1.02 | ． 63 | ． 25 | ． 63 | 2.04 | 1.85 | 2.69 | 3.36 | 1.90 | 1.14 | 1.16 | 1.14 | ． 97 | ． 00 | 20.85 |
| 5．1－6．0 | 43 | 28 | 13 | 28 | 9 | 3 | 18 | 82 | 102 | 131 | 134 | 74 | 52 | 37 | 49 | 39 | 0 | 842 |
| （1） | 1.00 | ． 65 | ． 30 | ． 65 | ． 21 | ． 07 | ． 42 | 1.90 | 2.36 | 3.03 | 3.10 | 1.71 | 1.20 | ． 86 | 1.14 | ． 90 | ． 00 | 19.50 |
| （2） | 1.00 | ． 65 | ． 30 | ． 65 | ． 21 | ． 07 | ． 42 | 1.90 | 2.36 | 3.03 | 3.10 | 1.71 | 1.20 | ． 86 | 1.14 | ． 90 | ． 00 | 19.50 |
| 6．1－8．0 | 27 | 22 | 22 | 15 | 16 | 6 | 15 | 72 | 45 | 159 | 157 | 48 | 22 | 21 | 53 | 35 | 0 | 735 |
| （1） | ． 63 | ． 51 | ． 51 | ． 35 | ． 37 | ． 14 | ． 35 | 1.67 | 1.04 | 3.68 | 3.64 | 1.11 | ． 51 | ． 49 | 1.23 | ． 81 | ． 00 | 17.03 |
| （2） | ． 63 | ． 51 | ． 51 | ． 35 | ． 37 | ． 14 | ． 35 | 1.67 | 1.04 | 3.68 | 3.64 | 1.11 | ． 51 | ． 49 | 1.23 | ． 81 | ． 00 | 17.03 |
| 8．1－10．0 | 8 | 9 | 2 | 2 | 3 | 0 | 1 | 13 | 0 | 10 | 14 | 1 | 1 | 4 | 5 | 11 | 0 | 84 |
| （1） | ． 19 | ． 21 | ． 05 | ． 05 | ． 07 | ． 00 | ． 02 | ． 30 | ． 00 | ． 23 | ． 32 | ． 02 | ． 02 | ． 09 | ． 12 | ． 25 | ． 00 | 1.95 |
| （2） | ． 19 | ． 21 | ． 05 | ． 05 | ． 07 | ． 00 | ． 02 | ． 30 | ． 00 | ． 23 | ． 32 | ． 02 | ． 02 | ． 09 | ． 12 | ． 25 | ． 00 | 1.95 |
| 10．1－89．5 | 0 | 4 | 1 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 1 | 2 | 4 | 0 | 0 | 14 |
| （1） | ． 00 | ． 09 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 05 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 05 | ． 09 | ． 00 | ． 00 | ． 32 |
| ALL SPEEDS | ． 00 | ． 09 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 05 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 05 | ． 09 | ． 00 | ． 00 | ． 32 |
|  | 287 | 239 | 128 | 206 | 182 | 120 | 152 | 346 | 337 | 532 | 599 | 324 | 214 | 202 | 248 | 201 | 0 | 4317 |
| （1） | 6.65 | 5.54 | 2.97 | 4.77 | 4.22 | 2.78 | 3.52 | 8.01 | 7.81 | 12.32 | 13.88 | 7.51 | 4.96 | 4.68 | 5.74 | 4.66 | ． 00 | 100.00 |
| （2） | 6.65 | 5.54 | 2.97 | 4.77 | 4.22 | 2.78 | 3.52 | 8.01 | 7.81 | 12.32 | 13.88 | 7.51 | 4.96 | 4.68 | 5.74 | 4.66 | ． 00 | 100.00 |
| （1）＝PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| （2）＝PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

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Table 2.3-36—\{CCNPP 197 ft ( 60 m) July JFD (2000-2005) \}
(Page 1 of 8)
CC JULY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS A CLASS FREQUENCY (PERCENT) = 12.73

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD


CC JULY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS B CLASS FREQUENCY (PERCENT) = 5.92


CC JULY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS C CLASS FREQUENCY (PERCENT) = 6.79


CC JULY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS D CLASS FREQUENCY (PERCENT) = 30.62

| IND DIRECTION FROM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 2 | 3 | 4 | 5 | 0 | 2 | 1 | 1 | 1 | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 25 |
| (1) | . 00 | . 15 | . 22 | . 30 | . 37 | . 00 | . 15 | . 07 | . 07 | . 07 | . 07 | . 15 | . 00 | . 00 | . 07 | . 15 | . 00 | 1.86 |
| (2) | . 00 | . 05 | . 07 | . 09 | . 11 | . 00 | . 05 | . 02 | . 02 | . 02 | . 02 | . 05 | . 00 | . 00 | . 02 | . 05 | . 00 | . 57 |
| 1.1-1.5 | 5 |  | 5 | 4 | 4 | 5 | 2 | 3 | 3 | 2 | 1 | 1 | 3 | 1 | 0 | 1 | 0 | 44 |
| (1) | . 37 | . 30 | . 37 | . 30 | . 30 | . 37 | . 15 | . 22 | . 22 | . 15 | . 07 | . 07 | . 22 | . 07 | . 00 | . 07 | . 00 | 3.27 |
| (2) | . 11 | . 09 | . 11 | . 09 | . 09 | . 11 | . 05 | . 07 | . 07 | . 05 | . 02 | . 02 | . 07 | . 02 | . 00 | . 02 | . 00 | 1.00 |
| 1.6-2.0 | 6 | 17 | 5 | 9 | 15 | 3 | 6 | 1 | 5 | 3 | 9 | 3 | 6 | 3 | 4 | 6 | 0 | 101 |
| (1) | . 45 | 1.26 | . 37 | . 67 | 1.12 | . 22 | . 45 | . 07 | . 37 | . 22 | . 67 | . 22 | . 45 | . 22 | . 30 | . 45 | . 00 | 7.51 |
| (2) | . 14 | . 39 | . 11 | . 20 | . 34 | . 07 | . 14 | . 02 | . 11 | . 07 | . 20 | . 07 | . 14 | . 07 | . 09 | . 14 | . 00 | 2.30 |
| 2.1-3.0 | 29 | 38 | 10 | 20 | 19 | 14 | 10 | 14 | 5 | 15 | 16 | 12 | 9 | 13 | 8 | 7 | 0 | 239 |
| (1) | 2.16 | 2.83 | . 74 | 1.49 | 1.41 | 1.04 | . 74 | 1.04 | . 37 | 1.12 | 1.19 | . 89 | . 67 | . 97 | . 59 | . 52 | . 00 | 17.77 |
| (2) | . 66 | . 87 | . 23 | . 46 | . 43 | . 32 | . 23 | . 32 | . 11 | . 34 | . 36 | . 27 | . 20 | . 30 | . 18 | . 16 | . 00 | 5.44 |
| 3.1-4.0 | 19 | 28 | 19 | 27 | 30 | 18 | 18 | 12 | 4 | 14 | 30 | 26 | 8 | 10 | 6 | 11 | 0 | 280 |
| (1) | 1.41 | 2.08 | 1.41 | 2.01 | 2.23 | 1.34 | 1.34 | . 89 | . 30 | 1.04 | 2.23 | 1.93 | . 59 | . 74 | . 45 | . 82 | . 00 | 20.82 |
| (2) | . 43 | . 64 | . 43 | . 61 | . 68 | . 41 | . 41 | . 27 | . 09 | . 32 | . 68 | . 59 | . 18 | . 23 | . 14 | . 25 | . 00 | 6.38 |
| 4.1-5.0 | 26 | 13 | 26 | 24 | 16 | 5 | 15 | 24 | 10 | 16 | 21 | 13 | 4 | 1 | 4 | 6 | 0 | 224 |
| (1) | 1.93 | . 97 | 1.93 | 1.78 | 1.19 | . 37 | 1.12 | 1.78 | . 74 | 1.19 | 1.56 | . 97 | . 30 | . 07 | . 30 | . 45 | . 00 | 16.65 |
| (2) | . 59 | . 30 | . 59 | . 55 | . 36 | . 11 | . 34 | . 55 | . 23 | . 36 | . 48 | . 30 | . 09 | . 02 | . 09 | . 14 | . 00 | 5.10 |
| 5.1-6.0 | 14 | 11 | 26 | 28 | 15 | 11 | 7 | 21 | 8 | 7 | 15 | 7 | 4 | 0 | 3 | 5 | 0 | 182 |
| (1) | 1.04 | . 82 | 1.93 | 2.08 | 1.12 | . 82 | . 52 | 1.56 | . 59 | . 52 | 1.12 | . 52 | . 30 | . 00 | . 22 | . 37 | . 00 | 13.53 |
| (2) | . 32 | . 25 | . 59 | . 64 | . 34 | . 25 | . 16 | . 48 | . 18 | . 16 | . 34 | . 16 | . 09 | . 00 | . 07 | . 11 | . 00 | 4.14 |
| 6.1-8.0 | 7 | 29 | 53 | 24 | 12 | 2 | 0 | 15 | 4 | 6 | 13 | 4 | 0 | 1 | 5 | 4 | 0 | 179 |
| (1) | . 52 | 2.16 | 3.94 | 1.78 | . 89 | . 15 | . 00 | 1.12 | . 30 | . 45 | . 97 | . 30 | . 00 | . 07 | . 37 | . 30 | . 00 | 13.31 |
| (2) | . 16 | . 66 | 1.21 | . 55 | . 27 | . 05 | . 00 | . 34 | . 09 | . 14 | . 30 | . 09 | . 00 | . 02 | . 11 | . 09 | . 00 | 4.08 |
| 8.1-10.0 | 3 | 16 | 22 | 4 | 1 | 0 | 0 | 0 | 1 | 0 | 8 | 0 | 0 | 1 | 0 | 0 | 0 | 56 |
| (1) | . 22 | 1.19 | 1.64 | . 30 | . 07 | . 00 | . 00 | . 00 | . 07 | . 00 | . 59 | . 00 | . 00 | . 07 | . 00 | . 00 | . 00 | 4.16 |
| (2) | . 07 | . 36 | . 50 | . 09 | . 02 | . 00 | . 00 | . 00 | . 02 | . 00 | . 18 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | 1.28 |
| 10.1-89.5 | 0 | 12 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 15 |
| (1) | . 00 | . 89 | . 15 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 | . 00 | . 00 | 1.12 |
| (2) | . 00 | . 27 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 34 |
| ALL SPEEDS | 109 | 170 | 171 | 144 | 117 | 58 | 60 | 91 | 41 | 64 | 114 | 68 | 34 | 30 | 32 | 42 | 0 | 1345 |
| (1) | 8.10 | 12.64 | 12.71 | 10.71 | 8.70 | 4.31 | 4.46 | 6.77 | 3.05 | 4.76 | 8.48 | 5.06 | 2.53 | 2.23 | 2.38 | 3.12 | . 00 | 100.00 |
| (2) | 2.48 | 3.87 | 3.89 | 3.28 | 2.66 | 1.32 | 1.37 | 2.07 | . 93 | 1.46 | 2.60 | 1.55 | . 77 | . 68 | . 73 | . 96 | . 00 | 30.62 |
| $\begin{aligned} & \text { (1) = PERCENT } \\ & (2)=\text { PERCENT } \end{aligned}$ | OF ALI | GOOD | OBSERV SERVATI | VATIONS ONS FOR | $\begin{gathered} \text { FOR } \\ \text { THIS } \end{gathered}$ | HIS PA <br> ERIOD |  |  |  |  |  |  |  |  |  |  |  |  |

OヨノכヨノOYd $\perp H$ Iy

CC JULY MET DATA JOINT FREQUENCY DISTRIBUTION（60－METER TOWER）
197．0 FT WIND DATA STABILITY CLASS E CLASS FREQUENCY（PERCENT）＝ 23.11

CC JULY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS F CLASS FREQUENCY (PERCENT) $=10.82$



CC JULY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS G CLASS FREQUENCY (PERCENT) = 10.02

|  |  |  |  |  |  |  |  | IND D | IRECTIO | N FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 1 | 2 | 2 | 0 | 1 | 0 | 1 | 2 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 2 | 0 | 14 |
| (1) | . 23 | . 45 | . 45 | . 00 | . 23 | . 00 | . 23 | . 45 | . 23 | . 23 | . 00 | . 00 | . 23 | . 00 | . 00 | . 45 | . 00 | 3.18 |
| (2) | . 02 | . 05 | . 05 | . 00 | . 02 | . 00 | . 02 | . 05 | . 02 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 05 | . 00 | . 32 |
| 1.1-1.5 | 1 | 2 | 3 | 2 | 4 | 1 | 1 | 2 | 2 | 1 | 2 | 1 | 2 | 0 | 1 | 1 | 0 | 26 |
| (1) | . 23 | . 45 | . 68 | . 45 | . 91 | . 23 | . 23 | . 45 | . 45 | . 23 | . 45 | . 23 | . 45 | . 00 | . 23 | . 23 | . 00 | 5.91 |
| (2) | . 02 | . 05 | . 07 | . 05 | . 09 | . 02 | . 02 | . 05 | . 05 | . 02 | . 05 | . 02 | . 05 | . 00 | . 02 | . 02 | . 00 | . 59 |
| 1.6-2.0 | 3 | 3 | 3 | 1 | 2 | 0 | 2 | 0 | 6 | 1 | 2 | 3 | 3 | 0 | 0 | 2 | 0 | 31 |
| (1) | . 68 | . 68 | . 68 | . 23 | . 45 | . 00 | . 45 | . 00 | 1.36 | . 23 | . 45 | . 68 | . 68 | . 00 | . 00 | . 45 | . 00 | 7.05 |
| (2) | . 07 | . 07 | . 07 | . 02 | . 05 | . 00 | . 05 | . 00 | . 14 | . 02 | . 05 | . 07 | . 07 | . 00 | . 00 | . 05 | . 00 | . 71 |
| 2.1-3.0 | 4 | 3 | 3 | 1 | 3 | 1 | 1 | 6 | 4 | 7 | 6 | 6 | 9 | 5 | 2 | 1 | 0 | 62 |
| (1) | . 91 | . 68 | . 68 | . 23 | . 68 | . 23 | . 23 | 1.36 | . 91 | 1.59 | 1.36 | 1.36 | 2.05 | 1.14 | . 45 | . 23 | . 00 | 14.09 |
| (2) | . 09 | . 07 | . 07 | . 02 | . 07 | . 02 | . 02 | . 14 | . 09 | . 16 | . 14 | . 14 | . 20 | . 11 | . 05 | . 02 | . 00 | 1.41 |
| 3.1-4.0 | 2 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 5 | 6 | 18 | 24 | 16 | 4 | 5 | 9 | 0 | 93 |
| (1) | . 45 | . 00 | . 23 | . 00 | . 00 | . 00 | . 68 | . 00 | 1.14 | 1.36 | 4.09 | 5.45 | 3.64 | . 91 | 1.14 | 2.05 | . 00 | 21.14 |
| (2) | . 05 | . 00 | . 02 | . 00 | . 00 | . 00 | . 07 | . 00 | . 11 | . 14 | . 41 | . 55 | . 36 | . 09 | . 11 | . 20 | . 00 | 2.12 |
| 4.1-5.0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 13 | 16 | 28 | 30 | 19 | 8 | 8 | 2 | 0 | 127 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 23 | . 45 | 2.95 | 3.64 | 6.36 | 6.82 | 4.32 | 1.82 | 1.82 | . 45 | . 00 | 28.86 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 05 | . 30 | . 36 | . 64 | . 68 | . 43 | . 18 | . 18 | . 05 | . 00 | 2.89 |
| 5.1-6.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 11 | 12 | 7 | 8 | 5 | 7 | 1 | 0 | 63 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 2.73 | 2.50 | 2.73 | 1.59 | 1.82 | 1.14 | 1.59 | . 23 | . 00 | 14.32 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 27 | . 25 | . 27 | . 16 | . 18 | . 11 | . 16 | . 02 | . 00 | 1.43 |
| 6.1-8.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 3 | 1 | 1 | 3 | 3 | 6 | 0 | 0 | 24 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.59 | . 68 | . 23 | . 23 | . 68 | . 68 | 1.36 | . 00 | . 00 | 5.45 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 16 | . 07 | . 02 | . 02 | . 07 | . 07 | . 14 | . 00 | . 00 | . 55 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 11 | 10 | 12 | 4 | 10 | 2 | 9 | 12 | 50 | 46 | 69 | 72 | 61 | 25 | 29 | 18 | 0 | 440 |
| (1) | 2.50 | 2.27 | 2.73 | . 91 | 2.27 | . 45 | 2.05 | 2.73 | 11.36 | 10.45 | 15.68 | 16.36 | 13.86 | 5.68 | 6.59 | 4.09 | . 00 | 100.00 |
| (2) | . 25 | . 23 | . 27 | . 09 | . 23 | . 05 | . 20 | . 27 | 1.14 | 1.05 | 1.57 | 1.64 | 1.39 | . 57 | . 66 | . 41 | . 00 | 10.02 |



Table 2.3-36-\{CCNPP 197 ft ( $\mathbf{6 0}$ m) July JFD (2000-2005) \} (Page 8 of 8)
CC JULY MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS ALL CLASS FREQUENCY (PERCENT) $=100.00$
P
$\stackrel{0}{0}$
$i=1$

CC AUGUST MET DATA JOINT FREQUENCY DISTRIBUTION ( 60 -METER TOWER)
197.0 FT WIND DATA STABILITY CLASS A CLASS FREQUENCY (PERCENT) = 12.05

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD


Table 2.3-37—\{CCNPP 197 ft (60 m) August JFD (2000-2005)\} (Page 2 of 8)

$$
\begin{aligned}
& \text { CC AUGUST MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER) } \\
& \text { 197.0 FT WIND DATA STABILITY CLASS B CLASS FREQUENCY (PERCENT) = } 5.81 \\
& \text { (1) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE }
\end{aligned}
$$

(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
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CC AUGUST MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS C CLASS FREQUENCY (PERCENT) = 6.10
T
$\stackrel{0}{0}$
$i$
$i$

Table 2.3-37—\{CCNPP 197 ft ( 60 m) August JFD (2000-2005) \}
(Page 4 of 8)
CC AUGUST MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS D CLASS FREQUENCY (PERCENT) = 28.72

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CC AUGUST MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS E CLASS FREQUENCY (PERCENT) = 27.48

CC AUGUST MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS F CLASS FREQUENCY (PERCENT) = 11.91
Po
$\stackrel{0}{2}$
$i$

## OᄏIכヨIOपy IHפוy

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CC AUGUST MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS G CLASS FREQUENCY (PERCENT) = 7.93

Table 2.3-37—\{CCNPP 197 ft ( $\mathbf{6 0} \mathbf{~ m}$ ) August JFD ( $\mathbf{2 0 0 0 - 2 0 0 5 ) \}}$ (Page 8 of 8 )
CC AUGUST MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS ALL CLASS FREQUENCY (PERCENT) = 100.00

| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 1 | 0 | 0 | 4 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 05 | . 00 | . 02 | . 00 | . 00 | . 09 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 05 | . 00 | . 02 | . 00 | . 00 | . 09 |
| . $2-.4$ | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 0 | 8 |
| (1) | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 02 | . 02 | . 02 | . 02 | . 00 | . 18 |
| (2) | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 02 | . 02 | . 02 | . 02 | . 00 | . 18 |
| .5-1.0 | 5 | 4 | 5 | 7 | 6 | 6 | 6 | 1 | 5 | 8 | 3 | 3 | 1 | 4 | 2 | 3 | 0 | 69 |
| (1) | . 11 | . 09 | . 11 | . 16 | . 14 | . 14 | . 14 | . 02 | . 11 | . 18 | . 07 | . 07 | . 02 | . 09 | . 05 | . 07 | . 00 | 1.55 |
| (2) | . 11 | . 09 | . 11 | . 16 | . 14 | . 14 | . 14 | . 02 | . 11 | . 18 | . 07 | . 07 | . 02 | . 09 | . 05 | . 07 | . 00 | 1.55 |
| 1.1-1.5 | 16 | 6 | 10 | 12 | 12 | 7 | 11 | 8 | 5 | 9 | 3 | 12 | 4 | 6 | 3 | 3 | 0 | 127 |
| (1) | . 36 | . 14 | . 23 | . 27 | . 27 | . 16 | . 25 | . 18 | . 11 | . 20 | . 07 | . 27 | . 09 | . 14 | . 07 | . 07 | . 00 | 2.86 |
| (2) | . 36 | . 14 | . 23 | . 27 | . 27 | . 16 | . 25 | . 18 | . 11 | . 20 | . 07 | . 27 | . 09 | . 14 | . 07 | . 07 | . 00 | 2.86 |
| 1.6-2.0 | 17 | 27 | 15 | 27 | 35 | 13 | 14 | 9 | 17 | 18 | 17 | 15 | 10 | 4 | 6 | 5 | 0 | 249 |
| (1) | . 38 | . 61 | . 34 | . 61 | . 79 | . 29 | . 32 | . 20 | . 38 | . 41 | . 38 | . 34 | . 23 | . 09 | . 14 | . 11 | . 00 | 5.61 |
| (2) | . 38 | . 61 | . 34 | . 61 | . 79 | . 29 | . 32 | . 20 | . 38 | . 41 | . 38 | . 34 | . 23 | . 09 | . 14 | . 11 | . 00 | 5.61 |
| 2.1-3.0 | 78 | 58 | 33 | 50 | 61 | 39 | 33 | 33 | 47 | 54 | 75 | 35 | 23 | 10 | 15 | 28 | 0 | 672 |
| (1) | 1.76 | 1.31 | . 74 | 1.13 | 1.37 | . 88 | . 74 | . 74 | 1.06 | 1.22 | 1.69 | . 79 | . 52 | . 23 | . 34 | . 63 | . 00 | 15.14 |
| (2) | 1.76 | 1.31 | . 74 | 1.13 | 1.37 | . 88 | . 74 | . 74 | 1.06 | 1.22 | 1.69 | . 79 | . 52 | . 23 | . 34 | . 63 | . 00 | 15.14 |
| 3.1-4.0 | 75 | 79 | 22 | 29 | 27 | 38 | 51 | 92 | 76 | 90 | 123 | 65 | 30 | 28 | 31 | 43 | 0 | 899 |
| (1) | 1.69 | 1.78 | . 50 | . 65 | . 61 | . 86 | 1.15 | 2.07 | 1.71 | 2.03 | 2.77 | 1.46 | . 68 | . 63 | . 70 | . 97 | . 00 | 20.25 |
| (2) | 1.69 | 1.78 | . 50 | . 65 | . 61 | . 86 | 1.15 | 2.07 | 1.71 | 2.03 | 2.77 | 1.46 | . 68 | . 63 | . 70 | . 97 | . 00 | 20.25 |
| 4.1-5.0 | 58 | 38 | 25 | 22 | 15 | 25 | 39 | 115 | 126 | 138 | 130 | 67 | 35 | 31 | 24 | 64 | 0 | 952 |
| (1) | 1.31 | . 86 | . 56 | . 50 | . 34 | . 56 | . 88 | 2.59 | 2.84 | 3.11 | 2.93 | 1.51 | . 79 | . 70 | . 54 | 1.44 | . 00 | 21.44 |
| (2) | 1.31 | . 86 | . 56 | . 50 | . 34 | . 56 | . 88 | 2.59 | 2.84 | 3.11 | 2.93 | 1.51 | . 79 | . 70 | . 54 | 1.44 | . 00 | 21.44 |
| 5.1-6.0 | 35 | 38 | 24 | 14 | 3 |  | 20 | 66 | 99 | 135 | 154 | 56 | 24 | 15 | 21 | 51 | 0 | 765 |
| (1) | . 79 | . 86 | . 54 | . 32 | . 07 | . 23 | . 45 | 1.49 | 2.23 | 3.04 | 3.47 | 1.26 | . 54 | . 34 | . 47 | 1.15 | . 00 | 17.23 |
| (2) | . 79 | . 86 | . 54 | . 32 | . 07 | . 23 | . 45 | 1.49 | 2.23 | 3.04 | 3.47 | 1.26 | . 54 | . 34 | . 47 | 1.15 | . 00 | 17.23 |
| 6.1-8.0 | 39 | 38 | 30 | 13 | 3 | 8 | 7 | 35 | 53 | 129 | 152 | 12 | 4 | 10 | 12 | 22 | 0 | 567 |
| (1) | . 88 | . 86 | . 68 | . 29 | . 07 | . 18 | . 16 | . 79 | 1.19 | 2.91 | 3.42 | . 27 | . 09 | . 23 | . 27 | . 50 | . 00 | 12.77 |
| (2) | . 88 | . 86 | . 68 | . 29 | . 07 | . 18 | . 16 | . 79 | 1.19 | 2.91 | 3.42 | . 27 | . 09 | . 23 | . 27 | . 50 | . 00 | 12.77 |
| 8.1-10.0 | 14 | 34 | 21 | 1 | 1 | 0 | 1 | 5 | 1 | 9 | 7 | 1 | 1 | 1 | 1 | 2 | 0 | 100 |
| (1) | . 32 | . 77 | . 47 | . 02 | . 02 | . 00 | . 02 | . 11 | . 02 | . 20 | . 16 | . 02 | . 02 | . 02 | . 02 | . 05 | . 00 | 2.25 |
| (2) | . 32 | . 77 | . 47 | . 02 | . 02 | . 00 | . 02 | . 11 | . 02 | . 20 | . 16 | . 02 | . 02 | . 02 | . 02 | . 05 | . 00 | 2.25 |
| 10.1-89.5 | 3 | 11 | 6 | 4 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 1 | 0 | 28 |
| (1) | . 07 | . 25 | . 14 | . 09 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 63 |
| (2) | . 07 | . 25 | . 14 | . 09 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 63 |
| ALL SPEEDS | 341 | 333 | 191 | 179 | 163 | 147 | 183 | 364 | 430 | 591 | 665 | 267 | 135 | 110 | 118 | 223 | 0 | 4440 |
| (1) | 7.68 | 7.50 | 4.30 | 4.03 | 3.67 | 3.31 | 4.12 | 8.20 | 9.68 | 13.31 | 14.98 | 6.01 | 3.04 | 2.48 | 2.66 | 5.02 | . 00 | 100.00 |
| (2) | 7.68 | 7.50 | 4.30 | 4.03 | 3.67 | 3.31 | 4.12 | 8.20 | 9.68 | 13.31 | 14.98 | 6.01 | 3.04 | 2.48 | 2.66 | 5.02 | . 00 | 100.00 |

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
P
$\stackrel{0}{0}$
$i=1$

Table 2.3-38—\{CCNPP 197 ft ( 60 m) Septmber JFD (2000-2005) \}

## (Page 1 of 8)

CC SEPTEMBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS A CLASS FREQUENCY (PERCENT) = 11.81

|  |  |  |  |  |  |  |  | IND DI | RECTI | ON FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 1.1-1.5 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| (1) | . 20 | . 20 | . 20 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 20 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 80 |
| (2) | . 02 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 09 |
| 1.6-2.0 | 1 | 3 | 1 | 2 | 4 | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 17 |
| (1) | . 20 | . 60 | . 20 | . 40 | . 80 | . 00 | . 20 | . 20 | . 00 | . 00 | . 00 | . 20 | . 20 | . 00 | . 00 | . 40 | . 00 | 3.41 |
| (2) | . 02 | . 07 | . 02 | . 05 | . 09 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 05 | . 00 | . 40 |
| 2.1-3.0 | 11 | 18 | 6 | 5 | 5 | 8 | 4 | 2 | 4 | 5 | 8 | 1 | 2 | 2 | 1 | 1 | 0 | 83 |
| (1) | 2.20 | 3.61 | 1.20 | 1.00 | 1.00 | 1.60 | . 80 | . 40 | . 80 | 1.00 | 1.60 | . 20 | . 40 | . 40 | . 20 | . 20 | . 00 | 16.63 |
| (2) | . 26 | . 43 | . 14 | . 12 | . 12 | . 19 | . 09 | . 05 | . 09 | . 12 | . 19 | . 02 | . 05 | . 05 | . 02 | . 02 | . 00 | 1.96 |
| 3.1-4.0 | 33 | 27 | 3 | 1 | 0 | 6 | 7 | 5 | 4 | 12 | 13 | 8 | 1 | 3 | 1 | 1 | 0 | 125 |
| (1) | 6.61 | 5.41 | . 60 | . 20 | . 00 | 1.20 | 1.40 | 1.00 | . 80 | 2.40 | 2.61 | 1.60 | . 20 | . 60 | . 20 | . 20 | . 00 | 25.05 |
| (2) | . 78 | . 64 | . 07 | . 02 | . 00 | . 14 | . 17 | . 12 | . 09 | . 28 | . 31 | . 19 | . 02 | . 07 | . 02 | . 02 | . 00 | 2.96 |
| 4.1-5.0 | 33 | 23 | 1 | 0 | 0 | 4 | 15 | 12 | 3 | 17 | 16 | 3 | 1 | 2 | 0 | 6 | 0 | 136 |
| (1) | 6.61 | 4.61 | . 20 | . 00 | . 00 | . 80 | 3.01 | 2.40 | . 60 | 3.41 | 3.21 | . 60 | . 20 | . 40 | . 00 | 1.20 | . 00 | 27.25 |
| (2) | . 78 | . 54 | . 02 | . 00 | . 00 | . 09 | . 35 | . 28 | . 07 | . 40 | . 38 | . 07 | . 02 | . 05 | . 00 | . 14 | . 00 | 3.22 |
| 5.1-6.0 | 19 | 7 | 3 | 0 | 0 | 0 | 6 | 11 | 0 | 8 | 4 | 5 | 0 | 2 | 0 | 2 | 0 | 67 |
| (1) | 3.81 | 1.40 | . 60 | . 00 | . 00 | . 00 | 1.20 | 2.20 | . 00 | 1.60 | . 80 | 1.00 | . 00 | . 40 | . 00 | . 40 | . 00 | 13.43 |
| (2) | . 45 | . 17 | . 07 | . 00 | . 00 | . 00 | . 14 | . 26 | . 00 | . 19 | . 09 | . 12 | . 00 | . 05 | . 00 | . 05 | . 00 | 1.59 |
| 6.1-8.0 | 9 | 9 | 6 | 0 | 0 | 0 | 2 | 2 | 2 | 3 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 38 |
| (1) | 1.80 | 1.80 | 1.20 | . 00 | . 00 | . 00 | . 40 | . 40 | . 40 | . 60 | . 80 | . 20 | . 00 | . 00 | . 00 | . 00 | . 00 | 7.62 |
| (2) | . 21 | . 21 | . 14 | . 00 | . 00 | . 00 | . 05 | . 05 | . 05 | . 07 | . 09 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 90 |
| 8.1-10.0 | 5 | 6 | 5 | 0 | 0 | 0 | 0 | 1 | 0 | 6 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 26 |
| (1) | 1.00 | 1.20 | 1.00 | . 00 | . 00 | . 00 | . 00 | . 20 | . 00 | 1.20 | . 00 | . 00 | . 00 | . 00 | . 60 | . 00 | . 00 | 5.21 |
| (2) | . 12 | . 14 | . 12 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 14 | . 00 | . 00 | . 00 | . 00 | . 07 | . 00 | . 00 | . 62 |
| 10.1-89.5 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| (1) | . 00 | . 20 | . 20 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 20 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 60 |
| (2) | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 |
| ALL SPEEDS | 112 | 95 | 27 | 8 | 9 | 18 | 35 | 34 | 13 | 53 | 45 | 19 | 5 | 9 | 5 | 12 | 0 | 499 |
| (1) | 22.44 | 19.04 | 5.41 | 1.60 | 1.80 | 3.61 | 7.01 | 6.81 | 2.61 | 10.62 | 9.02 | 3.81 | 1.00 | 1.80 | 1.00 | 2.40 | . 00 | 100.00 |
| (2) | 2.65 | 2.25 | . 64 | . 19 | . 21 | . 43 | . 83 | . 80 | . 31 | 1.25 | 1.06 | . 45 | . 12 | . 21 | . 12 | . 28 | . 00 | 11.81 |

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
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Table 2.3-38—\{CCNPP 197 ft ( 60 m) Septmber JFD (2000-2005)\}

## (Page 2 of 8)

CC SEPTEMBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS B CLASS FREQUENCY (PERCENT) $=5.51$

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(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
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$$
\begin{aligned}
& \text { CC SEPTEMBER MET DATA JOINT FREQUENCY DISTRIBUTION } \\
& \text { 197.0 FT WIND DATA }
\end{aligned}
$$

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 41 | . 00 | . 00 | . 00 | . 00 | . 00 | . 41 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| 1.1-1.5 | 0 | 1 | 2 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 0 | 9 |
| (1) | . 00 | . 41 | . 81 | . 41 | . 81 | . 00 | . 00 | . 00 | . 00 | . 00 | . 41 | . 41 | . 00 | . 00 | . 00 | . 41 | . 00 | 3.66 |
| (2) | . 00 | . 02 | . 05 | . 02 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 02 | . 00 | . 21 |
| 1.6-2.0 | 2 | 10 | 5 | 2 | 3 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 1 | 1 | 0 | 1 | 0 | 31 |
| (1) | . 81 | 4.07 | 2.03 | . 81 | 1.22 | . 00 | . 41 | . 81 | . 00 | . 00 | . 41 | . 81 | . 41 | . 41 | . 00 | . 41 | . 00 | 12.60 |
| (2) | . 05 | . 24 | . 12 | . 05 | . 07 | . 00 | . 02 | . 05 | . 00 | . 00 | . 02 | . 05 | . 02 | . 02 | . 00 | . 02 | . 00 | . 73 |
| 2.1-3.0 | 2 | 13 | 4 | 7 | 7 | 6 | 7 | 6 | 7 | 1 | 0 | 0 | 2 | 2 | 1 | 0 | 0 | 65 |
| (1) | . 81 | 5.28 | 1.63 | 2.85 | 2.85 | 2.44 | 2.85 | 2.44 | 2.85 | . 41 | . 00 | . 00 | . 81 | . 81 | . 41 | . 00 | . 00 | 26.42 |
| (2) | . 05 | . 31 | . 09 | . 17 | . 17 | . 14 | . 17 | . 14 | . 17 | . 02 | . 00 | . 00 | . 05 | . 05 | . 02 | . 00 | . 00 | 1.54 |
| 3.1-4.0 | 16 | 10 | 2 | 0 | 1 | 4 | 3 | 2 | 1 | 0 | 1 | 1 | 3 | 1 | 3 | 1 | 0 | 49 |
| (1) | 6.50 | 4.07 | . 81 | . 00 | . 41 | 1.63 | 1.22 | . 81 | . 41 | . 00 | . 41 | . 41 | 1.22 | . 41 | 1.22 | . 41 | . 00 | 19.92 |
| (2) | . 38 | . 24 | . 05 | . 00 | . 02 | . 09 | . 07 | . 05 | . 02 | . 00 | . 02 | . 02 | . 07 | . 02 | . 07 | . 02 | . 00 | 1.16 |
| 4.1-5.0 | 6 | 5 | 1 | 1 | 1 | 0 | 2 | 4 | 0 | 1 | 5 | 0 | 0 | 2 | 3 | 3 | 0 | 34 |
| (1) | 2.44 | 2.03 | . 41 | . 41 | . 41 | . 00 | . 81 | 1.63 | . 00 | . 41 | 2.03 | . 00 | . 00 | . 81 | 1.22 | 1.22 | . 00 | 13.82 |
| (2) | . 14 | . 12 | . 02 | . 02 | . 02 | . 00 | . 05 | . 09 | . 00 | . 02 | . 12 | . 00 | . 00 | . 05 | . 07 | . 07 | . 00 | . 80 |
| 5.1-6.0 | 6 | 2 | 1 | 1 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 4 | 0 | 24 |
| (1) | 2.44 | . 81 | . 41 | . 41 | . 00 | . 00 | . 00 | 2.44 | . 00 | . 00 | . 00 | . 00 | . 41 | . 41 | . 81 | 1.63 | . 00 | 9.76 |
| (2) | . 14 | . 05 | . 02 | . 02 | . 00 | . 00 | . 00 | . 14 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 05 | . 09 | . 00 | . 57 |
| 6.1-8.0 | 1 | 1 | 4 | 0 | 0 | 0 | 2 | 4 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 17 |
| (1) | . 41 | . 41 | 1.63 | . 00 | . 00 | . 00 | . 81 | 1.63 | . 41 | 1.22 | . 00 | . 00 | . 00 | . 00 | . 00 | . 41 | . 00 | 6.91 |
| (2) | . 02 | . 02 | . 09 | . 00 | . 00 | . 00 | . 05 | . 09 | . 02 | . 07 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 40 |
| 8.1-10.0 | 2 | 3 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 14 |
| (1) | . 81 | 1.22 | 2.03 | . 41 | . 00 | . 00 | . 00 | . 00 | . 00 | . 41 | . 00 | . 00 | . 00 | . 00 | . 41 | . 41 | . 00 | 5.69 |
| (2) | . 05 | . 07 | . 12 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 33 |
| 10.1-89.5 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| (1) | . 00 | . 81 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 81 |
| (2) | . 00 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 |
| ALL SPEEDS | 35 | 47 | 24 | 13 | 14 | 10 | 15 | 24 | 9 | 6 | 8 | 5 | 7 | 7 | 10 | 12 | 0 | 246 |
| (1) | 14.23 | 19.11 | 9.76 | 5.28 | 5.69 | 4.07 | 6.10 | 9.76 | 3.66 | 2.44 | 3.25 | 2.03 | 2.85 | 2.85 | 4.07 | 4.88 | . 00 | 100.00 |
| (2) | . 83 | 1.11 | . 57 | . 31 | . 33 | . 24 | . 35 | . 57 | . 21 | . 14 | . 19 | . 12 | . 17 | . 17 | . 24 | . 28 | . 00 | 5.82 |

$\stackrel{7}{2}$
$\begin{array}{lcccc}\text { CC SEPTEMBER MET DATA JOINT FREQUENCY DISTRIBUTION } & (60 \text {-METER TOWER) } \\ 197.0 \text { FT WIND DATA } & \text { STABILITY CLASS D } & \text { CLASS FREQUENCY (PERCENT) }=34.29\end{array}$


## IᄏIכヨIOपd IHפוy

Table 2.3-38—\{CCNPP 197 ft (60 m) Septmber JFD (2000-2005)\} (Page 5 of 8)
CC SEPTEMBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS E CLASS FREQUENCY (PERCENT) = 22.43

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$$
\begin{array}{lccc}
\text { CC SEPTEMBER MET DATA JOINT FREQUENCY DISTRIBUTION } & (60 \text {-METER TOWER) } \\
197.0 \text { FT WIND DATA } & \text { STABILITY CLASS F } & \text { CLASS FREQUENCY } & \text { (PERCENT) }=10.01
\end{array}
$$


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## 

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$\begin{array}{lcccc}\text { CC SEPTEMBER MET DATA JOINT FREQUENCY DISTRIBUTION } & (60 \text {-METER TOWER) } \\ 197.0 \text { FT WIND DATA } & \text { STABILITY CLASS G } & \text { CLASS FREQUENCY } & \text { (PERCENT) }=10.13\end{array}$


Table 2．3－38—\｛CCNPP 197 ft（60 m）Septmber JFD（2000－2005）\} （Page 8 of 8）
CC SEPTEMBER MET DATA JOINT FREQUENCY DISTRIBUTION（60－METER TOWER）
197．0 FT WIND DATA STABILITY CLASS ALL CLASS FREQUENCY（PERCENT）＝ 100.00

| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT ． 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| （1） | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 05 |
| （2） | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 05 |
| ． $2-.4$ | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 3 |
| （1） | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 07 |
| （2） | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 07 |
| ．5－1．0 | 6 | 4 | 9 | 8 | 12 | 6 | 5 | 6 | 0 | 5 | 6 | 6 | 2 | 3 | 5 | 3 | 0 | 86 |
| （1） | ． 14 | ． 09 | ． 21 | ． 19 | ． 28 | ． 14 | ． 12 | ． 14 | ． 00 | ． 12 | ． 14 | ． 14 | ． 05 | ． 07 | ． 12 | ． 07 | ． 00 | 2.04 |
| （2） | ． 14 | ． 09 | ． 21 | ． 19 | ． 28 | ． 14 | ． 12 | ． 14 | ． 00 | ． 12 | ． 14 | ． 14 | ． 05 | ． 07 | ． 12 | ． 07 | ． 00 | 2.04 |
| 1．1－1．5 | 12 | 14 | 14 | 9 | 13 | 5 | 10 | 3 | 7 | 4 | 4 | 6 | 7 | 3 | 7 | 5 | 0 | 123 |
| （1） | ． 28 | ． 33 | ． 33 | ． 21 | ． 31 | ． 12 | ． 24 | ． 07 | ． 17 | ． 09 | ． 09 | ． 14 | ． 17 | ． 07 | ． 17 | ． 12 | ． 00 | 2.91 |
| （2） | ． 28 | ． 33 | ． 33 | ． 21 | ． 31 | ． 12 | ． 24 | ． 07 | ． 17 | ． 09 | ． 09 | ． 14 | ． 17 | ． 07 | ． 17 | ． 12 | ． 00 | 2.91 |
| 1．6－2．0 | 20 | 35 | 16 | 20 | 22 | 7 | 12 | 7 | 8 | 3 | 15 | 8 | 7 | 9 | 9 | 14 | 0 | 212 |
| （1） | ． 47 | ． 83 | ． 38 | ． 47 | ． 52 | ． 17 | ． 28 | ． 17 | ． 19 | ． 07 | ． 35 | ． 19 | ． 17 | ． 21 | ． 21 | ． 33 | ． 00 | 5.02 |
| （2） | ． 47 | ． 83 | ． 38 | ． 47 | ． 52 | ． 17 | ． 28 | ． 17 | ． 19 | ． 07 | ． 35 | ． 19 | ． 17 | ． 21 | ． 21 | ． 33 | ． 00 | 5.02 |
| 2．1－3．0 | 57 | 103 | 35 | 49 | 77 | 36 | 36 | 37 | 34 | 23 | 16 | 12 | 24 | 17 | 11 | 24 | 0 | 591 |
| （1） | 1.35 | 2.44 | ． 83 | 1.16 | 1.82 | ． 85 | ． 85 | ． 88 | ． 80 | ． 54 | ． 38 | ． 28 | ． 57 | ． 40 | ． 26 | ． 57 | ． 00 | 13.98 |
| （2） | 1.35 | 2.44 | ． 83 | 1.16 | 1.82 | ． 85 | ． 85 | ． 88 | ． 80 | ． 54 | ． 38 | ． 28 | ． 57 | ． 40 | ． 26 | ． 57 | ． 00 | 13.98 |
| 3．1－4．0 | 118 | 88 | 22 | 48 | 34 | 58 | 49 | 49 | 51 | 39 | 47 | 24 | 31 | 36 | 19 | 32 | 0 | 745 |
| （1） | 2.79 | 2.08 | ． 52 | 1.14 | ． 80 | 1.37 | 1.16 | 1.16 | 1.21 | ． 92 | 1.11 | ． 57 | ． 73 | ． 85 | ． 45 | ． 76 | ． 00 | 17.63 |
| （2） | 2.79 | 2.08 | ． 52 | 1.14 | ． 80 | 1.37 | 1.16 | 1.16 | 1.21 | ． 92 | 1.11 | ． 57 | ． 73 | ． 85 | ． 45 | ． 76 | ． 00 | 17.63 |
| 4．1－5．0 | 93 | 63 | 42 | 29 | 44 | 40 | 58 | 90 | 71 | 75 | 62 | 24 | 15 | 34 | 30 | 59 | 0 | 829 |
| （1） | 2.20 | 1.49 | ． 99 | ． 69 | 1.04 | ． 95 | 1.37 | 2.13 | 1.68 | 1.77 | 1.47 | ． 57 | ． 35 | ． 80 | ． 71 | 1.40 | ． 00 | 19.62 |
| （2） | 2.20 | 1.49 | ． 99 | ． 69 | 1.04 | ． 95 | 1.37 | 2.13 | 1.68 | 1.77 | 1.47 | ． 57 | ． 35 | ． 80 | ． 71 | 1.40 | ． 00 | 19.62 |
| 5．1－6．0 | 51 | 36 | 50 | 26 | 18 | 6 | 19 | 86 | 81 | 50 | 55 | 28 | 18 | 32 | 48 | 70 | 0 | 674 |
| （1） | 1.21 | ． 85 | 1.18 | ． 62 | ． 43 | ． 14 | ． 45 | 2.04 | 1.92 | 1.18 | 1.30 | ． 66 | ． 43 | ． 76 | 1.14 | 1.66 | ． 00 | 15.95 |
| （2） | 1.21 | ． 85 | 1.18 | ． 62 | ． 43 | ． 14 | ． 45 | 2.04 | 1.92 | 1.18 | 1.30 | ． 66 | ． 43 | ． 76 | 1.14 | 1.66 | ． 00 | 15.95 |
| 6．1－8．0 | 41 | 46 | 89 | 40 | 2 | 5 | 12 | 40 | 42 | 74 | 59 | 11 | 10 | 20 | 47 | 42 | 0 | 580 |
| （1） | ． 97 | 1.09 | 2.11 | ． 95 | ． 05 | ． 12 | ． 28 | ． 95 | ． 99 | 1.75 | 1.40 | ． 26 | ． 24 | ． 47 | 1.11 | ． 99 | ． 00 | 13.72 |
| （2） | ． 97 | 1.09 | 2.11 | ． 95 | ． 05 | ． 12 | ． 28 | ． 95 | ． 99 | 1.75 | 1.40 | ． 26 | ． 24 | ． 47 | 1.11 | ． 99 | ． 00 | 13.72 |
| 8．1－10．0 | 32 | 44 | 70 | 11 | 0 | 0 | 12 | 11 | 11 | 16 | 7 | 1 | 2 | 2 | 12 | 8 | 0 | 239 |
| （1） | ． 76 | 1.04 | 1.66 | ． 26 | ． 00 | ． 00 | ． 28 | ． 26 | ． 26 | ． 38 | ． 17 | ． 02 | ． 05 | ． 05 | ． 28 | ． 19 | ． 00 | 5.66 |
| （2） | ． 76 | 1.04 | 1.66 | ． 26 | ． 00 | ． 00 | ． 28 | ． 26 | ． 26 | ． 38 | ． 17 | ． 02 | ． 05 | ． 05 | ． 28 | ． 19 | ． 00 | 5.66 |
| 10．1－89．5 | 17 | 64 | 33 | 2 | 3 | 3 | 3 | 4 | 5 | 1 | 1 | 0 | 0 | 0 | 0 | 6 | 0 | 142 |
| （1） | ． 40 | 1.51 | ． 78 | ． 05 | ． 07 | ． 07 | ． 07 | ． 09 | ． 12 | ． 02 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 14 | ． 00 | 3.36 |
| （2） | ． 40 | 1.51 | ． 78 | ． 05 | ． 07 | ． 07 | ． 07 | ． 09 | ． 12 | ． 02 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 14 | ． 00 | 3.36 |
| ALL SPEEDS | 448 | 498 | 380 | 242 | 225 | 166 | 216 | 333 | 311 | 290 | 273 | 121 | 116 | 156 | 188 | 263 | 0 | 4226 |
| （1） | 10.60 | 11.78 | 8.99 | 5.73 | 5.32 | 3.93 | 5.11 | 7.88 | 7.36 | 6.86 | 6.46 | 2.86 | 2.74 | 3.69 | 4.45 | 6.22 | ． 00 | 100.00 |
| （2） | 10.60 | 11.78 | 8.99 | 5.73 | 5.32 | 3.93 | 5.11 | 7.88 | 7.36 | 6.86 | 6.46 | 2.86 | 2.74 | 3.69 | 4.45 | 6.22 | ． 00 | 100.00 |

（2）＝PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
To
$\stackrel{0}{0}$
$i$

Table 2.3-39—\{CCNPP 197 ft ( 60 m) October JFD (2000-2005)\}

## (Page 1 of 8)

CC OCTOBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS A CLASS FREQUENCY (PERCENT) = 12.84

|  | WIND DIRECTION FROM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 18 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 18 |
| (2) | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| 1.1-1.5 | 0 | 0 | 0 | 1 | 4 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| (1) | . 00 | . 00 | . 00 | . 18 | . 70 | . 35 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.23 |
| (2) | . 00 | . 00 | . 00 | . 02 | . 09 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 16 |
| 1.6-2.0 | 5 | 3 | 2 | 1 | 3 | 0 | 0 | 0 | 0 | 1 | 2 | 2 | 1 | 0 | 0 | 1 | 0 | 21 |
| (1) | . 88 | . 53 | . 35 | . 18 | . 53 | . 00 | . 00 | . 00 | . 00 | . 18 | . 35 | . 35 | . 18 | . 00 | . 00 | . 18 | . 00 | 3.70 |
| (2) | . 11 | . 07 | . 05 | . 02 | . 07 | . 00 | . 00 | . 00 | . 00 | . 02 | . 05 | . 05 | . 02 | . 00 | . 00 | . 02 | . 00 | . 47 |
| 2.1-3.0 | 16 | 5 | 2 | 2 | 8 | 7 | 2 | 5 | 1 | 1 | 2 | 3 | 4 | 1 | 2 | 4 | 0 | 65 |
| (1) | 2.82 | . 88 | . 35 | . 35 | 1.41 | 1.23 | . 35 | . 88 | . 18 | . 18 | . 35 | . 53 | . 70 | . 18 | . 35 | . 70 | . 00 | 11.44 |
| (2) | . 36 | . 11 | . 05 | . 05 | . 18 | . 16 | . 05 | . 11 | . 02 | . 02 | . 05 | . 07 | . 09 | . 02 | . 05 | . 09 | . 00 | 1.47 |
| 3.1-4.0 | 12 | 6 | 1 | 0 | 0 | 2 | 6 | 11 | 4 | 7 | 10 | 7 | 6 | 6 | 0 | 4 | 0 | 82 |
| (1) | 2.11 | 1.06 | . 18 | . 00 | . 00 | . 35 | 1.06 | 1.94 | . 70 | 1.23 | 1.76 | 1.23 | 1.06 | 1.06 | . 00 | . 70 | . 00 | 14.44 |
| (2) | . 27 | . 14 | . 02 | . 00 | . 00 | . 05 | . 14 | . 25 | . 09 | . 16 | . 23 | . 16 | . 14 | . 14 | . 00 | . 09 | . 00 | 1.85 |
| 4.1-5.0 | 30 | 9 | 2 | 0 | 0 | 0 | 1 | 9 | 4 | 13 | 12 | 9 | 4 | 7 | 18 | 4 | 0 | 122 |
| (1) | 5.28 | 1.58 | . 35 | . 00 | . 00 | . 00 | . 18 | 1.58 | . 70 | 2.29 | 2.11 | 1.58 | . 70 | 1.23 | 3.17 | . 70 | . 00 | 21.48 |
| (2) | . 68 | . 20 | . 05 | . 00 | . 00 | . 00 | . 02 | . 20 | . 09 | . 29 | . 27 | . 20 | . 09 | . 16 | . 41 | . 09 | . 00 | 2.76 |
| 5.1-6.0 | 28 | 8 | 1 | 0 | 3 | 0 | 2 | 7 | 5 | 5 | 14 | 6 | 1 | 10 | 7 | 12 | 0 | 109 |
| (1) | 4.93 | 1.41 | . 18 | . 00 | . 53 | . 00 | . 35 | 1.23 | . 88 | . 88 | 2.46 | 1.06 | . 18 | 1.76 | 1.23 | 2.11 | . 00 | 19.19 |
| (2) | . 63 | . 18 | . 02 | . 00 | . 07 | . 00 | . 05 | . 16 | . 11 | . 11 | . 32 | . 14 | . 02 | . 23 | . 16 | . 27 | . 00 | 2.46 |
| 6.1-8.0 | 17 | 7 | 1 | 1 | 1 | 0 | 0 | 5 | 0 | 4 | 8 | 8 | 9 | 23 | 18 | 4 | 0 | 106 |
| (1) | 2.99 | 1.23 | . 18 | . 18 | . 18 | . 00 | . 00 | . 88 | . 00 | . 70 | 1.41 | 1.41 | 1.58 | 4.05 | 3.17 | . 70 | . 00 | 18.66 |
| (2) | . 38 | . 16 | . 02 | . 02 | . 02 | . 00 | . 00 | . 11 | . 00 | . 09 | . 18 | . 18 | . 20 | . 52 | . 41 | . 09 | . 00 | 2.40 |
| 8.1-10.0 | 3 | 6 | 1 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 7 | 6 | 2 | 6 | 8 | 1 | 0 | 43 |
| (1) | . 53 | 1.06 | . 18 | . 18 | . 00 | . 00 | . 00 | . 35 | . 00 | . 00 | 1.23 | 1.06 | . 35 | 1.06 | 1.41 | . 18 | . 00 | 7.57 |
| (2) | . 07 | . 14 | . 02 | . 02 | . 00 | . 00 | . 00 | . 05 | . 00 | . 00 | . 16 | . 14 | . 05 | . 14 | . 18 | . 02 | . 00 | . 97 |
| 10.1-89.5 | 1 | 1 | 2 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 3 | 0 | 0 | 0 | 12 |
| (1) | . 18 | . 18 | . 35 | . 18 | . 00 | . 00 | . 00 | . 35 | . 00 | . 00 | . 00 | . 35 | . 00 | . 53 | . 00 | . 00 | . 00 | 2.11 |
| (2) | . 02 | . 02 | . 05 | . 02 | . 00 | . 00 | . 00 | . 05 | . 00 | . 00 | . 00 | . 05 | . 00 | . 07 | . 00 | . 00 | . 00 | . 27 |
| ALL SPEEDS | 112 | 45 | 13 | 7 | 19 | 11 | 11 | 41 | 14 | 31 | 55 | 43 | 27 | 56 | 53 | 30 | 0 | 568 |
| (1) | 19.72 | 7.92 | 2.29 | 1.23 | 3.35 | 1.94 | 1.94 | 7.22 | 2.46 | 5.46 | 9.68 | 7.57 | 4.75 | 9.86 | 9.33 | 5.28 | . 00 | 100.00 |
| (2) | 2.53 | 1.02 | . 29 | . 16 | . 43 | . 25 | . 25 | . 93 | . 32 | . 70 | 1.24 | . 97 | . 61 | 1.27 | 1.20 | . 68 | . 00 | 12.84 |

(1) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAG
(2) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD


CC OCTOBER MET DATA TOTNT FREQUENCY DTSTRTBUTION (60-METER TOWR)
197.0 FT WIND DATA STABILITY CLASS B CLASS FREQUENCY (PERCENT) = 3.98

(1) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
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| CC OCTOBER MET DATA JOINT | FREQUENCY DISTRIBUTION | (60-METER TOWER) |  |
| :---: | :---: | :---: | :---: |
| $197.0 ~ F T ~ W I N D ~ D A T A ~$ | STABILITY CLASS C | CLASS FREQUENCY | (PERCENT) $=4.36$ |


(1) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
P
$\stackrel{0}{0}$
$i=1$
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$$
\begin{array}{ccc}
\text { CC OCTOBER MET DATA JOINT FREQUENCY DISTRIBUTION } & (60-\mathrm{METER} \mathrm{TOWER)} \\
197.0 \text { FT WIND DATA } & \text { STABILITY CLASS D } & \text { CLASS FREQUENCY (PERCENT) }=33.92
\end{array}
$$


To
$\stackrel{0}{0}$
$i$
$i$

Table 2.3-39—\{CCNPP 197 ft ( 60 m ) October JFD (2000-2005)\}
(Page 5 of 8)
CC OCTOBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS E CLASS FREQUENCY (PERCENT) = 20.23

|  |  |  |  |  |  |  |  | IND DI | RECTIO | N FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 11 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 11 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| . $2-.4$ | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 11 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 11 |
| (2) | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| .5-1.0 | 0 | 0 | 3 | 1 | 1 | 3 | 2 | 6 | 0 | 1 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 20 |
| (1) | . 00 | . 00 | . 34 | . 11 | . 11 | . 34 | . 22 | . 67 | . 00 | . 11 | . 00 | . 00 | . 11 | . 11 | . 11 | . 00 | . 00 | 2.23 |
| (2) | . 00 | . 00 | . 07 | . 02 | . 02 | . 07 | . 05 | . 14 | . 00 | . 02 | . 00 | . 00 | . 02 | . 02 | . 02 | . 00 | . 00 | . 45 |
| 1.1-1.5 | 3 | 2 | 2 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 2 | 0 | 14 |
| (1) | . 34 | . 22 | . 22 | . 00 | . 11 | . 00 | . 11 | . 11 | . 00 | . 00 | . 11 | . 00 | . 00 | . 11 | . 00 | . 22 | . 00 | 1.56 |
| (2) | . 07 | . 05 | . 05 | . 00 | . 02 | . 00 | . 02 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 05 | . 00 | . 32 |
| 1.6-2.0 | 1 | 3 | 0 | 0 | 3 | 1 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 14 |
| (1) | . 11 | . 34 | . 00 | . 00 | . 34 | . 11 | . 00 | . 00 | . 22 | . 11 | . 00 | . 00 | . 00 | . 11 | . 11 | . 11 | . 00 | 1.56 |
| (2) | . 02 | . 07 | . 00 | . 00 | . 07 | . 02 | . 00 | . 00 | . 05 | . 02 | . 00 | . 00 | . 00 | . 02 | . 02 | . 02 | . 00 | . 32 |
| 2.1-3.0 | 6 | 3 | 5 | 10 | 16 | 6 | 1 | 4 | 2 | 2 | 2 | 1 | 1 | 2 | 5 | 7 | 0 | 73 |
| (1) | . 67 | . 34 | . 56 | 1.12 | 1.79 | . 67 | . 11 | . 45 | . 22 | . 22 | . 22 | . 11 | . 11 | . 22 | . 56 | . 78 | . 00 | 8.16 |
| (2) | . 14 | . 07 | . 11 | . 23 | . 36 | . 14 | . 02 | . 09 | . 05 | . 05 | . 05 | . 02 | . 02 | . 05 | . 11 | . 16 | . 00 | 1.65 |
| $3.1-4.0$ | 8 | 7 | 9 | 17 | 20 | 8 | 3 | 8 | 5 | 4 | 5 | 5 | 0 | 7 | 4 | 10 | 0 | 120 |
| (1) | . 89 | . 78 | 1.01 | 1.90 | 2.23 | . 89 | . 34 | . 89 | . 56 | . 45 | . 56 | . 56 | . 00 | . 78 | . 45 | 1.12 | . 00 | 13.41 |
| (2) | . 18 | . 16 | . 20 | . 38 | . 45 | . 18 | . 07 | . 18 | . 11 | . 09 | . 11 | . 11 | . 00 | . 16 | . 09 | . 23 | . 00 | 2.71 |
| 4.1-5.0 | 14 | 8 | 7 | 9 | 3 | 3 | 4 | 21 | 18 | 4 | 6 | 5 | 10 | 12 | 21 | 17 | 0 | 162 |
| (1) | 1.56 | . 89 | . 78 | 1.01 | . 34 | . 34 | . 45 | 2.35 | 2.01 | . 45 | . 67 | . 56 | 1.12 | 1.34 | 2.35 | 1.90 | . 00 | 18.10 |
| (2) | . 32 | . 18 | . 16 | . 20 | . 07 | . 07 | . 09 | . 47 | . 41 | . 09 | . 14 | . 11 | . 23 | . 27 | . 47 | . 38 | . 00 | 3.66 |
| 5.1-6.0 | 4 | 8 | 4 | 0 | 0 | 3 | 2 | 25 | 18 | 10 | 17 | 16 | 13 | 25 | 18 | 19 | 0 | 182 |
| (1) | . 45 | . 89 | . 45 | . 00 | . 00 | . 34 | . 22 | 2.79 | 2.01 | 1.12 | 1.90 | 1.79 | 1.45 | 2.79 | 2.01 | 2.12 | . 00 | 20.34 |
| (2) | . 09 | . 18 | . 09 | . 00 | . 00 | . 07 | . 05 | . 56 | . 41 | . 23 | . 38 | . 36 | . 29 | . 56 | . 41 | . 43 | . 00 | 4.11 |
| 6.1-8.0 | 9 | 12 | 1 | 0 | 0 | 0 | 0 | 10 | 27 | 51 | 37 | 15 | 9 | 22 | 43 | 38 | 0 | 274 |
| (1) | 1.01 | 1.34 | . 11 | . 00 | . 00 | . 00 | . 00 | 1.12 | 3.02 | 5.70 | 4.13 | 1.68 | 1.01 | 2.46 | 4.80 | 4.25 | . 00 | 30.61 |
| (2) | . 20 | . 27 | . 02 | . 00 | . 00 | . 00 | . 00 | . 23 | . 61 | 1.15 | . 84 | . 34 | . 20 | . 50 | . 97 | . 86 | . 00 | 6.19 |
| 8.1-10.0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 15 | 6 | 1 | 0 | 0 | 1 | 2 | 0 | 30 |
| (1) | . 11 | . 11 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 34 | 1.68 | . 67 | . 11 | . 00 | . 00 | . 11 | . 22 | . 00 | 3.35 |
| (2) | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 | . 34 | . 14 | . 02 | . 00 | . 00 | . 02 | . 05 | . 00 | . 68 |
| 10.1-89.5 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| (1) | . 00 | . 00 | . 11 | . 00 | . 00 | . 00 | . 00 | . 11 | . 00 | . 11 | . 11 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 45 |
| (2) | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 09 |
| ALL SPEEDS | 46 | 44 | 33 | 37 | 45 | 24 | 13 | 76 | 75 | 89 | 75 | 43 | 34 | 71 | 94 | 96 | 0 | 895 |
| (1) | 5.14 | 4.92 | 3.69 | 4.13 | 5.03 | 2.68 | 1.45 | 8.49 | 8.38 | 9.94 | 8.38 | 4.80 | 3.80 | 7.93 | 10.50 | 10.73 | . 00 | 100.00 |
| (2) | 1.04 | . 99 | . 75 | . 84 | 1.02 | . 54 | . 29 | 1.72 | 1.69 | 2.01 | 1.69 | . 97 | . 77 | 1.60 | 2.12 | 2.17 | . 00 | 20.23 |



Table 2.3-39—\{CCNPP 197 ft (60 m) October JFD (2000-2005)\}

C OCTOBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)

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Table 2.3-39—\{CCNPP 197 ft (60 m) October JFD (2000-2005)\} (Page 8 of 8)
CC OCTOBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS ALL CLASS FREQUENCY (PERCENT) = 100.00

| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 3 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 |
| . $2-.4$ | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 7 |
| (1) | . 02 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 16 |
| (2) | . 02 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 16 |
| .5-1.0 | 3 | 2 | 6 | 4 | 3 | 7 | 4 | 8 | 2 | 1 | 0 | 7 | 3 | 4 | 3 | 2 | 0 | 59 |
| (1) | . 07 | . 05 | . 14 | . 09 | . 07 | . 16 | . 09 | . 18 | . 05 | . 02 | . 00 | . 16 | . 07 | . 09 | . 07 | . 05 | . 00 | 1.33 |
| (2) | . 07 | . 05 | . 14 | . 09 | . 07 | . 16 | . 09 | . 18 | . 05 | . 02 | . 00 | . 16 | . 07 | . 09 | . 07 | . 05 | . 00 | 1.33 |
| 1.1-1.5 | 10 | 10 | 12 | 7 | 12 | 8 | 5 | 4 | 1 | 1 | 8 | 4 | 6 | 8 | 5 | 9 | 0 | 110 |
| (1) | . 23 | . 23 | . 27 | . 16 | . 27 | . 18 | . 11 | . 09 | . 02 | . 02 | . 18 | . 09 | . 14 | . 18 | . 11 | . 20 | . 00 | 2.49 |
| (2) | . 23 | . 23 | . 27 | . 16 | . 27 | . 18 | . 11 | . 09 | . 02 | . 02 | . 18 | . 09 | . 14 | . 18 | . 11 | . 20 | . 00 | 2.49 |
| 1.6-2.0 | 13 | 19 | 13 | 9 | 18 | 9 | 8 | 10 | 7 | 10 | 7 | 7 | 5 | 5 | 4 | 11 | 0 | 155 |
| (1) | . 29 | . 43 | . 29 | . 20 | . 41 | . 20 | . 18 | . 23 | . 16 | . 23 | . 16 | . 16 | . 11 | . 11 | . 09 | . 25 | . 00 | 3.50 |
| (2) | . 29 | . 43 | . 29 | . 20 | . 41 | . 20 | . 18 | . 23 | . 16 | . 23 | . 16 | . 16 | . 11 | . 11 | . 09 | . 25 | . 00 | 3.50 |
| 2.1-3.0 | 66 | 51 | 26 | 47 | 50 | 40 | 18 | 24 | 23 | 27 | 22 | 19 | 11 | 12 | 17 | 30 | 0 | 483 |
| (1) | 1.49 | 1.15 | . 59 | 1.06 | 1.13 | . 90 | . 41 | . 54 | . 52 | . 61 | . 50 | . 43 | . 25 | . 27 | . 38 | . 68 | . 00 | 10.92 |
| (2) | 1.49 | 1.15 | . 59 | 1.06 | 1.13 | . 90 | . 41 | . 54 | . 52 | . 61 | . 50 | . 43 | . 25 | . 27 | . 38 | . 68 | . 00 | 10.92 |
| 3.1-4.0 | 68 | 46 | 31 | 41 | 51 | 26 | 31 | 43 | 34 | 32 | 48 | 29 | 15 | 29 | 34 | 50 | 0 | 608 |
| (1) | 1.54 | 1.04 | . 70 | . 93 | 1.15 | . 59 | . 70 | . 97 | . 77 | . 72 | 1.08 | . 66 | . 34 | . 66 | . 77 | 1.13 | . 00 | 13.74 |
| (2) | 1.54 | 1.04 | . 70 | . 93 | 1.15 | . 59 | . 70 | . 97 | . 77 | . 72 | 1.08 | . 66 | . 34 | . 66 | . 77 | 1.13 | . 00 | 13.74 |
| 4.1-5.0 | 79 | 62 | 46 | 47 | 14 | 9 | 23 | 59 | 50 | 54 | 50 | 50 | 33 | 41 | 85 | 79 | 0 | 781 |
| (1) | 1.79 | 1.40 | 1.04 | 1.06 | . 32 | . 20 | . 52 | 1.33 | 1.13 | 1.22 | 1.13 | 1.13 | . 75 | . 93 | 1.92 | 1.79 | . 00 | 17.65 |
| (2) | 1.79 | 1.40 | 1.04 | 1.06 | . 32 | . 20 | . 52 | 1.33 | 1.13 | 1.22 | 1.13 | 1.13 | . 75 | . 93 | 1.92 | 1.79 | . 00 | 17.65 |
| 5.1-6.0 | 53 | 56 | 57 | 17 | 6 | 9 | 10 | 63 | 69 | 61 | 67 | 53 | 43 | 78 | 80 | 87 | 0 | 809 |
| (1) | 1.20 | 1.27 | 1.29 | . 38 | . 14 | . 20 | . 23 | 1.42 | 1.56 | 1.38 | 1.51 | 1.20 | . 97 | 1.76 | 1.81 | 1.97 | . 00 | 18.28 |
| (2) | 1.20 | 1.27 | 1.29 | . 38 | . 14 | . 20 | . 23 | 1.42 | 1.56 | 1.38 | 1.51 | 1.20 | . 97 | 1.76 | 1.81 | 1.97 | . 00 | 18.28 |
| 6.1-8.0 | 73 | 116 | 60 | 12 | 2 | 2 | 6 | 67 | 93 | 106 | 106 | 60 | 46 | 84 | 137 | 101 | 0 | 1071 |
| (1) | 1.65 | 2.62 | 1.36 | . 27 | . 05 | . 05 | . 14 | 1.51 | 2.10 | 2.40 | 2.40 | 1.36 | 1.04 | 1.90 | 3.10 | 2.28 | . 00 | 24.20 |
| (2) | 1.65 | 2.62 | 1.36 | . 27 | . 05 | . 05 | . 14 | 1.51 | 2.10 | 2.40 | 2.40 | 1.36 | 1.04 | 1.90 | 3.10 | 2.28 | . 00 | 24.20 |
| 8.1-10.0 | 40 | 55 | 29 | 3 | 0 | 0 | 1 | 17 | 10 | 25 | 23 | 15 | 8 | 14 | 18 | 18 | 0 | 276 |
| (1) | . 90 | 1.24 | . 66 | . 07 | . 00 | . 00 | . 02 | . 38 | . 23 | . 56 | . 52 | . 34 | . 18 | . 32 | . 41 | . 41 | . 00 | 6.24 |
| (2) | . 90 | 1.24 | . 66 | . 07 | . 00 | . 00 | . 02 | . 38 | . 23 | . 56 | . 52 | . 34 | . 18 | . 32 | . 41 | . 41 | . 00 | 6.24 |
| 10.1-89.5 | 25 | 13 | 9 | 1 | 0 | 0 | 0 | 3 | 1 | 2 | 2 | 2 | 0 | 4 | 0 | 1 | 0 | 63 |
| (1) | . 56 | . 29 | . 20 | . 02 | . 00 | . 00 | . 00 | . 07 | . 02 | . 05 | . 05 | . 05 | . 00 | . 09 | . 00 | . 02 | . 00 | 1.42 |
| (2) | . 56 | . 29 | . 20 | . 02 | . 00 | . 00 | . 00 | . 07 | . 02 | . 05 | . 05 | . 05 | . 00 | . 09 | . 00 | . 02 | . 00 | 1.42 |
| ALL SPEEDS | 431 | 430 | 290 | 188 | 158 | 111 | 106 | 299 | 291 | 319 | 333 | 247 | 171 | 279 | 383 | 389 | 0 | 4425 |
| (1) | 9.74 | 9.72 | 6.55 | 4.25 | 3.57 | 2.51 | 2.40 | 6.76 | 6.58 | 7.21 | 7.53 | 5.58 | 3.86 | 6.31 | 8.66 | 8.79 | . 00 | 100.00 |
| (2) | 9.74 | 9.72 | 6.55 | 4.25 | 3.57 | 2.51 | 2.40 | 6.76 | 6.58 | 7.21 | 7.53 | 5.58 | 3.86 | 6.31 | 8.66 | 8.79 | . 00 | 100.00 |
| (1) = PERCENT | OF ALI | GOOD | OBSERV | TIONS | FOR | HIS PA |  |  |  |  |  |  |  |  |  |  |  |  |

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$i$

Table 2.3-40—\{CCNPP 197 ft ( 60 m) November JFD (2000-2005)\}

## (Page 1 of 8)

CC NOVEMBER MET DATA JOINT FREQUENCY DISTRIBUTION ( 60 -METER TOWER)
197.0 FT WIND DATA STABILITY CLASS A CLASS FREQUENCY (PERCENT) = 13.19

(1) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) =Percent of all good observations for this period
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| CC NOVEMBER MET DATA JOINT FREQUENCY DISTRIBUTION | ( 60 -METER TOWER) |  |  |
| :---: | :---: | :---: | :---: | :---: |
| 197.0 FT WIND DATA | STABILITY CLASS B | CLASS FREQUENCY | (PERCENT) $=\quad 3.59$ |


(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD


Table 2.3-40—\{CCNPP 197 ft ( 60 m) November JFD (2000-2005)\}

## (Page 3 of 8)

CC NOVEMBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS C CLASS FREQUENCY (PERCENT) = 3.69

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD


Table 2.3-40—\{CCNPP 197 ft ( 60 m) November JFD (2000-2005) \}

## (Page 4 of 8)

CC NOVEMBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS D CLASS FREQUENCY (PERCENT) = 30.35

| $\begin{aligned} & \text { SPEED } \\ & \text { mps } \end{aligned}$ | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $5-1.0$ | 2 | 2 | 1 | 1 | 2 | 0 | 0 | 2 | 1 | 0 | 1 | 0 | 0 | 2 | 0 | 2 | 0 | 16 |
| (1) | . 15 | . 15 | . 08 | . 08 | . 15 | . 00 | . 00 | . 15 | . 08 | . 00 | . 08 | . 00 | . 00 | . 15 | . 00 | . 15 | . 00 | 1.22 |
| (2) | . 05 | . 05 | . 02 | . 02 | . 05 | . 00 | . 00 | . 05 | . 02 | . 00 | . 02 | . 00 | . 00 | . 05 | . 00 | . 05 | . 00 | . 37 |
| 1.1-1.5 | 1 | 4 | 1 | 3 | 2 | 0 | 2 | 1 | 0 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 0 | 21 |
| (1) | . 08 | . 31 | . 08 | . 23 | . 15 | . 00 | . 15 | . 08 | . 00 | . 00 | . 08 | . 15 | . 08 | . 00 | . 08 | . 15 | . 00 | 1.60 |
| (2) | . 02 | . 09 | . 02 | . 07 | . 05 | . 00 | . 05 | . 02 | . 00 | . 00 | . 02 | . 05 | . 02 | . 00 | . 02 | . 05 | . 00 | . 49 |
| 1.6-2.0 | 5 | 4 | 3 | 7 | 5 | 3 | 1 | 2 | 2 | 1 | 2 | 0 | 2 | 1 | 2 | 3 | 0 | 43 |
| (1) | . 38 | . 31 | . 23 | . 53 | . 38 | . 23 | . 08 | . 15 | . 15 | . 08 | . 15 | . 00 | . 15 | . 08 | . 15 | . 23 | . 00 | 3.28 |
| (2) | . 12 | . 09 | . 07 | . 16 | . 12 | . 07 | . 02 | . 05 | . 05 | . 02 | . 05 | . 00 | . 05 | . 02 | . 05 | . 07 | . 00 | 1.00 |
| 2.1-3.0 | 9 | 6 | 13 | 5 | 11 | 12 | 15 | 15 | 12 | 5 | 4 | 4 | 2 | 2 | 3 | 2 | 0 | 120 |
| (1) | . 69 | . 46 | . 99 | . 38 | . 84 | . 92 | 1.15 | 1.15 | . 92 | . 38 | . 31 | . 31 | . 15 | . 15 | . 23 | . 15 | . 00 | 9.17 |
| (2) | . 21 | . 14 | . 30 | . 12 | . 26 | . 28 | . 35 | . 35 | . 28 | . 12 | . 09 | . 09 | . 05 | . 05 | . 07 | . 05 | . 00 | 2.78 |
| 3.1-4.0 | 10 | 6 | 8 | 10 | 13 | 12 | 22 | 23 | 13 | 12 | 5 | 8 | 8 | 2 | 7 | 13 | 0 | 172 |
| (1) | . 76 | . 46 | . 61 | . 76 | . 99 | . 92 | 1.68 | 1.76 | . 99 | . 92 | . 38 | . 61 | . 61 | . 15 | . 53 | . 99 | . 00 | 13.14 |
| (2) | . 23 | . 14 | . 19 | . 23 | . 30 | . 28 | . 51 | . 53 | . 30 | . 28 | . 12 | . 19 | . 19 | . 05 | . 16 | . 30 | . 00 | 3.99 |
| 4.1-5.0 | 11 | 4 | 7 | 9 | 17 | 13 | 17 | 21 | 13 | 8 | 10 | 7 | 5 | 9 | 10 | 13 | 0 | 174 |
| (1) | . 84 | . 31 | . 53 | . 69 | 1.30 | . 99 | 1.30 | 1.60 | . 99 | . 61 | . 76 | . 53 | . 38 | . 69 | . 76 | . 99 | . 00 | 13.29 |
| (2) | . 26 | . 09 | . 16 | . 21 | . 39 | . 30 | . 39 | . 49 | . 30 | . 19 | . 23 | . 16 | . 12 | . 21 | . 23 | . 30 | . 00 | 4.03 |
| 5.1-6.0 | 12 | 2 | 4 | 7 | 4 | 6 | 12 | 32 | 7 | 11 | 10 | 13 | 3 | 4 | 16 | 30 | 0 | 173 |
| (1) | . 92 | . 15 | . 31 | . 53 | . 31 | . 46 | . 92 | 2.44 | . 53 | . 84 | . 76 | . 99 | . 23 | . 31 | 1.22 | 2.29 | . 00 | 13.22 |
| (2) | . 28 | . 05 | . 09 | . 16 | . 09 | . 14 | . 28 | . 74 | . 16 | . 26 | . 23 | . 30 | . 07 | . 09 | . 37 | . 70 | . 00 | 4.01 |
| 6.1-8.0 | 19 | 19 | 9 | 2 | 5 | 8 | 5 | 50 | 20 | 19 | 30 | 11 | 12 | 34 | 43 | 49 | 0 | 335 |
| (1) | 1.45 | 1.45 | . 69 | . 15 | . 38 | . 61 | . 38 | 3.82 | 1.53 | 1.45 | 2.29 | . 84 | . 92 | 2.60 | 3.28 | 3.74 | . 00 | 25.59 |
| (2) | . 44 | . 44 | . 21 | . 05 | . 12 | . 19 | . 12 | 1.16 | . 46 | . 44 | . 70 | . 26 | . 28 | . 79 | 1.00 | 1.14 | . 00 | 7.77 |
| 8.1-10.0 | 27 | 15 | 8 | 0 | 0 | 0 | 0 | 23 | 8 | 8 | 13 | 3 | 4 | 31 | 23 | 21 | 0 | 184 |
| (1) | 2.06 | 1.15 | . 61 | . 00 | . 00 | . 00 | . 00 | 1.76 | . 61 | . 61 | . 99 | . 23 | . 31 | 2.37 | 1.76 | 1.60 | . 00 | 14.06 |
| (2) | . 63 | . 35 | . 19 | . 00 | . 00 | . 00 | . 00 | . 53 | . 19 | . 19 | . 30 | . 07 | . 09 | . 72 | . 53 | . 49 | . 00 | 4.27 |
| 10.1-89.5 | 21 | 10 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 0 | 0 | 1 | 3 | 18 | 6 | 3 | 0 | 71 |
| (1) | 1.60 | . 76 | . 00 | . 00 | . 00 | . 00 | . 00 | . 69 | . 00 | . 00 | . 00 | . 08 | . 23 | 1.38 | . 46 | . 23 | . 00 | 5.42 |
| (2) | . 49 | . 23 | . 00 | . 00 | . 00 | . 00 | . 00 | . 21 | . 00 | . 00 | . 00 | . 02 | . 07 | . 42 | . 14 | . 07 | . 00 | 1.65 |
| ALL SPEEDS | 117 | 72 | 54 | 44 | 59 | 54 | 74 | 178 | 76 | 64 | 76 | 49 | 40 | 103 | 111 | 138 | 0 | 1309 |
| (1) | 8.94 | 5.50 | 4.13 | 3.36 | 4.51 | 4.13 | 5.65 | 13.60 | 5.81 | 4.89 | 5.81 | 3.74 | 3.06 | 7.87 | 8.48 | 10.54 | . 00 | 100.00 |
| (2) | 2.71 | 1.67 | 1.25 | 1.02 | 1.37 | 1.25 | 1.72 | 4.13 | 1.76 | 1.48 | 1.76 | 1.14 | . 93 | 2.39 | 2.57 | 3.20 | . 00 | 30.35 |
| (1) = PERCENT | OF ALL | GOOD | OBSERV | ATIONS | FOR | HIS PA |  |  |  |  |  |  |  |  |  |  |  |  |

Table 2.3-40—\{CCNPP 197 ft (60 m) November JFD (2000-2005)\}

## (Page 5 of 8)

CC NOVEMBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS E CLASS FREQUENCY (PERCENT) = 28.61

|  |  |  |  |  |  |  |  | IND D | ECIIO | N FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| (1) | . 16 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 16 |
| (2) | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 |
| .5-1.0 | 1 | 2 | 0 | 0 | 1 | 2 | 1 | 2 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 0 | 14 |
| (1) | . 08 | . 16 | . 00 | . 00 | . 08 | . 16 | . 08 | . 16 | . 00 | . 00 | . 00 | . 00 | . 08 | . 08 | . 08 | . 16 | . 00 | 1.13 |
| (2) | . 02 | . 05 | . 00 | . 00 | . 02 | . 05 | . 02 | . 05 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 02 | . 05 | . 00 | . 32 |
| 1.1-1.5 | 3 | 0 | 1 | 2 | 2 | 4 | 0 | 1 | 2 | 1 | 0 | 1 | 1 | 1 | 1 | 2 | 0 | 22 |
| (1) | . 24 | . 00 | . 08 | . 16 | . 16 | . 32 | . 00 | . 08 | . 16 | . 08 | . 00 | . 08 | . 08 | . 08 | . 08 | . 16 | . 00 | 1.78 |
| (2) | . 07 | . 00 | . 02 | . 05 | . 05 | . 09 | . 00 | . 02 | . 05 | . 02 | . 00 | . 02 | . 02 | . 02 | . 02 | . 05 | . 00 | . 51 |
| 1.6-2.0 | 2 | 1 | 3 | 1 | 4 | 3 | 2 | 2 | 1 | 2 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 24 |
| (1) | . 16 | . 08 | . 24 | . 08 | . 32 | . 24 | . 16 | . 16 | . 08 | . 16 | . 00 | . 00 | . 00 | . 00 | . 08 | . 16 | . 00 | 1.94 |
| (2) | . 05 | . 02 | . 07 | . 02 | . 09 | . 07 | . 05 | . 05 | . 02 | . 05 | . 00 | . 00 | . 00 | . 00 | . 02 | . 05 | . 00 | . 56 |
| 2.1-3.0 | 4 | 0 | 9 | 11 | 11 | 12 | 6 | 7 | 8 | 5 | 2 | 2 | 2 | 6 | 10 | 6 | 0 | 101 |
| (1) | . 32 | . 00 | . 73 | . 89 | . 89 | . 97 | . 49 | . 57 | . 65 | . 41 | . 16 | . 16 | . 16 | . 49 | . 81 | . 49 | . 00 | 8.18 |
| (2) | . 09 | . 00 | . 21 | . 26 | . 26 | . 28 | . 14 | . 16 | . 19 | . 12 | . 05 | . 05 | . 05 | . 14 | . 23 | . 14 | . 00 | 2.34 |
| 3.1-4.0 | 8 | 5 | 7 | 6 | 12 | 12 | 6 | 9 | 10 | 16 | 13 | 9 | 8 | 11 | 9 | 7 | 0 | 148 |
| (1) | . 65 | . 41 | . 57 | . 49 | . 97 | . 97 | . 49 | . 73 | . 81 | 1.30 | 1.05 | . 73 | . 65 | . 89 | . 73 | . 57 | . 00 | 11.99 |
| (2) | . 19 | . 12 | . 16 | . 14 | . 28 | . 28 | . 14 | . 21 | . 23 | . 37 | . 30 | . 21 | . 19 | . 26 | . 21 | . 16 | . 00 | 3.43 |
| 4.1-5.0 | 11 | 4 | 3 | 2 | 2 | 13 | 8 | 13 | 9 | 14 | 21 | 17 | 10 | 24 | 29 | 34 | 0 | 214 |
| (1) | . 89 | . 32 | . 24 | . 16 | . 16 | 1.05 | . 65 | 1.05 | . 73 | 1.13 | 1.70 | 1.38 | . 81 | 1.94 | 2.35 | 2.76 | . 00 | 17.34 |
| (2) | . 26 | . 09 | . 07 | . 05 | . 05 | . 30 | . 19 | . 30 | . 21 | . 32 | . 49 | . 39 | . 23 | . 56 | . 67 | . 79 | . 00 | 4.96 |
| 5.1-6.0 | 7 | 4 | 3 | 2 | 2 | 1 | 5 | 14 | 25 | 35 | 20 | 13 | 15 | 20 | 45 | 49 | 0 | 260 |
| (1) | . 57 | . 32 | . 24 | . 16 | . 16 | . 08 | . 41 | 1.13 | 2.03 | 2.84 | 1.62 | 1.05 | 1.22 | 1.62 | 3.65 | 3.97 | . 00 | 21.07 |
| (2) | . 16 | . 09 | . 07 | . 05 | . 05 | . 02 | . 12 | . 32 | . 58 | . 81 | . 46 | . 30 | . 35 | . 46 | 1.04 | 1.14 | . 00 | 6.03 |
| 6.1-8.0 | 7 | 4 | 0 | 0 | 1 | 0 | 2 | 12 | 56 | 76 | 54 | 19 | 15 | 19 | 34 | 38 | 0 | 337 |
| (1) | . 57 | . 32 | . 00 | . 00 | . 08 | . 00 | . 16 | . 97 | 4.54 | 6.16 | 4.38 | 1.54 | 1.22 | 1.54 | 2.76 | 3.08 | . 00 | 27.31 |
| (2) | . 16 | . 09 | . 00 | . 00 | . 02 | . 00 | . 05 | . 28 | 1.30 | 1.76 | 1.25 | . 44 | . 35 | . 44 | . 79 | . 88 | . 00 | 7.81 |
| 8.1-10.0 | 4 | 0 | 0 | 0 | 1 | 0 | 0 | 8 | 8 | 32 | 31 | 3 | 3 | 7 | 6 | 1 | 0 | 104 |
| (1) | . 32 | . 00 | . 00 | . 00 | . 08 | . 00 | . 00 | . 65 | . 65 | 2.59 | 2.51 | . 24 | . 24 | . 57 | . 49 | . 08 | . 00 | 8.43 |
| (2) | . 09 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 19 | . 19 | . 74 | . 72 | . 07 | . 07 | . 16 | . 14 | . 02 | . 00 | 2.41 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 5 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 8 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 08 | . 00 | . 41 | . 08 | . 00 | . 00 | . 08 | . 00 | . 00 | . 00 | . 65 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 12 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 19 |
| ALL SPEEDS | 49 | 20 | 26 | 24 | 36 | 47 | 30 | 69 | 119 | 186 | 142 | 64 | 55 | 90 | 136 | 141 | 0 | 1234 |
| (1) | 3.97 | 1.62 | 2.11 | 1.94 | 2.92 | 3.81 | 2.43 | 5.59 | 9.64 | 15.07 | 11.51 | 5.19 | 4.46 | 7.29 | 11.02 | 11.43 | . 00 | 100.00 |
| (2) | 1.14 | . 46 | . 60 | . 56 | . 83 | 1.09 | . 70 | 1.60 | 2.76 | 4.31 | 3.29 | 1.48 | 1.28 | 2.09 | 3.15 | 3.27 | . 00 | 28.61 |

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CC NOVEMBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS F CLASS FREQUENCY (PERCENT) = 11.62


| CC NOVEMBER MET DATA JOINT FREQUENCY DISTRIBUTION | (60-METER TOWER) |  |  |
| :---: | :---: | :---: | :---: | :---: |
| 197.0 FT WIND DATA | STABILITY CLASS G | CLASS FREQUENCY | (PERCENT) $=8.95$ |



Table 2．3－40—\｛CCNPP 197 ft（60 m）November JFD（2000－2005）\}

## （Page 8 of 8）

CC NOVEMBER MET DATA JOINT FREQUENCY DISTRIBUTION（60－METER TOWER）
197．0 FT WIND DATA STABILITY CLASS ALL CLASS FREQUENCY（PERCENT）$=100.00$


Table 2.3-41—\{CCNPP 197 ft (60 m) December JFD (2000-2005)\}

## (Page 1 of 8)

CC DECEMBER MET DATA JOINT FREQUENCY DISTRIBUTION ( 60 -METER TOWER
197.0 FT WIND DATA STABILITY CLASS A CLASS FREQUENCY (PERCENT) = 8.34

(1) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
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$$
\begin{aligned}
& \text { CC DECEMBER MET DATA JOINT FREQUENCY DISTRIBUTION } \\
& \text { (60-METER TOWER) } \\
& 197.0 \text { FT WIND DATA }
\end{aligned} \text { STABILITY CLASS B } \quad \text { CLASS FREQUENCY (PERCENT) = } 4.20
$$

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { SPEED } \\ & \text { mps } \end{aligned}$ | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 1.1-1.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 1.6-2.0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 3 |
| (1) | . 00 | . 55 | . 55 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 55 | . 00 | . 00 | 1.66 |
| (2) | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 07 |
| 2.1-3.0 | 3 | 5 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 0 | 4 | 0 | 1 | 0 | 1 | 0 | 17 |
| (1) | 1.66 | 2.76 | . 00 | . 00 | . 55 | . 55 | . 00 | . 00 | . 00 | . 55 | . 00 | 2.21 | . 00 | . 55 | . 00 | . 55 | . 00 | 9.39 |
| (2) | . 07 | . 12 | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 02 | . 00 | . 09 | . 00 | . 02 | . 00 | . 02 | . 00 | . 39 |
| 3.1-4.0 | 2 | 5 | 2 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 1 | 0 | 2 | 2 | 3 | 3 | 0 | 23 |
| (1) | 1.10 | 2.76 | 1.10 | . 00 | . 55 | . 00 | . 55 | . 55 | . 00 | . 00 | . 55 | . 00 | 1.10 | 1.10 | 1.66 | 1.66 | . 00 | 12.71 |
| (2) | . 05 | . 12 | . 05 | . 00 | . 02 | . 00 | . 02 | . 02 | . 00 | . 00 | . 02 | . 00 | . 05 | . 05 | . 07 | . 07 | . 00 | . 53 |
| 4.1-5.0 | 5 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 3 | 6 | 4 | 1 | 3 | 2 | 1 | 0 | 30 |
| (1) | 2.76 | 1.10 | . 00 | . 00 | . 00 | . 00 | . 00 | . 55 | 1.10 | 1.66 | 3.31 | 2.21 | . 55 | 1.66 | 1.10 | . 55 | . 00 | 16.57 |
| (2) | . 12 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 05 | . 07 | . 14 | . 09 | . 02 | . 07 | . 05 | . 02 | . 00 | . 70 |
| 5.1-6.0 | 5 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 1 | 0 | 2 | 4 | 4 | 2 | 0 | 28 |
| (1) | 2.76 | 1.10 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 55 | 3.87 | . 55 | . 00 | 1.10 | 2.21 | 2.21 | 1.10 | . 00 | 15.47 |
| (2) | . 12 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 16 | . 02 | . 00 | . 05 | . 09 | . 09 | . 05 | . 00 | . 65 |
| 6.1-8.0 | 4 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 4 | 3 | 6 | 5 | 9 | 5 | 0 | 44 |
| (1) | 2.21 | 1.10 | . 55 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 2.76 | 2.21 | 1.66 | 3.31 | 2.76 | 4.97 | 2.76 | . 00 | 24.31 |
| (2) | . 09 | . 05 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 12 | . 09 | . 07 | . 14 | . 12 | . 21 | . 12 | . 00 | 1.02 |
| 8.1-10.0 | 2 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 1 | 8 | 7 | 1 | 0 | 25 |
| (1) | 1.10 | 1.10 | . 55 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 55 | 1.10 | . 00 | . 55 | 4.42 | 3.87 | . 55 | . 00 | 13.81 |
| (2) | . 05 | . 05 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 05 | . 00 | . 02 | . 19 | . 16 | . 02 | . 00 | . 58 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 8 | 0 | 0 | 11 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 55 | . 00 | . 00 | . 55 | . 00 | . 55 | 4.42 | . 00 | . 00 | 6.08 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 02 | . 19 | . 00 | . 00 | . 25 |
| ALL SPEEDS | 21 | 19 | 5 | 0 | 2 | 1 | 1 | 2 | 4 | 17 | 14 | 12 | 12 | 24 | 34 | 13 | 0 | 181 |
| (1) | 11.60 | 10.50 | 2.76 | . 00 | 1.10 | . 55 | . 55 | 1.10 | 2.21 | 9.39 | 7.73 | 6.63 | 6.63 | 13.26 | 18.78 | 7.18 | . 00 | 100.00 |
| (2) | . 49 | . 44 | . 12 | . 00 | . 05 | . 02 | . 02 | . 05 | . 09 | . 39 | . 32 | . 28 | . 28 | . 56 | . 79 | . 30 | . 00 | 4.20 |

[^1]CC DECEMBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS C CLASS FREQUENCY (PERCENT) = 4.36

| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 53 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 53 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |
| 1.1-1.5 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| (1) | . 53 | . 00 | . 53 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.06 |
| (2) | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 |
| 1.6-2.0 | 1 | 2 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 9 |
| (1) | . 53 | 1.06 | . 53 | 1.06 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 53 | . 53 | . 00 | . 53 | . 00 | . 00 | 4.79 |
| (2) | . 02 | . 05 | . 02 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 02 | . 00 | . 00 | . 21 |
| 2.1-3.0 | 0 | 2 | 1 | 0 | 2 | 3 | 1 | 1 | 0 | 1 | 1 | 2 | 2 | 4 | 2 | 1 | 0 | 23 |
| (1) | . 00 | 1.06 | . 53 | . 00 | 1.06 | 1.60 | . 53 | . 53 | . 00 | . 53 | . 53 | 1.06 | 1.06 | 2.13 | 1.06 | . 53 | . 00 | 12.23 |
| (2) | . 00 | . 05 | . 02 | . 00 | . 05 | . 07 | . 02 | . 02 | . 00 | . 02 | . 02 | . 05 | . 05 | . 09 | . 05 | . 02 | . 00 | . 53 |
| 3.1-4.0 | 2 | 2 | 1 | 0 | 0 | 1 | 0 | 1 | 2 | 1 | 2 | 2 | 3 | 2 | 2 | 4 | 0 | 25 |
| (1) | 1.06 | 1.06 | . 53 | . 00 | . 00 | . 53 | . 00 | . 53 | 1.06 | . 53 | 1.06 | 1.06 | 1.60 | 1.06 | 1.06 | 2.13 | . 00 | 13.30 |
| (2) | . 05 | . 05 | . 02 | . 00 | . 00 | . 02 | . 00 | . 02 | . 05 | . 02 | . 05 | . 05 | . 07 | . 05 | . 05 | . 09 | . 00 | . 58 |
| 4.1-5.0 | 3 | 3 | 0 | 0 | 0 | 1 | 1 | 3 | 1 | 0 | 0 | 3 | 3 | 4 | 3 | 7 | 0 | 32 |
| (1) | 1.60 | 1.60 | . 00 | . 00 | . 00 | . 53 | . 53 | 1.60 | . 53 | . 00 | . 00 | 1.60 | 1.60 | 2.13 | 1.60 | 3.72 | . 00 | 17.02 |
| (2) | . 07 | . 07 | . 00 | . 00 | . 00 | . 02 | . 02 | . 07 | . 02 | . 00 | . 00 | . 07 | . 07 | . 09 | . 07 | . 16 | . 00 | . 74 |
| 5.1-6.0 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 4 | 7 | 5 | 1 | 3 | 2 | 1 | 1 | 0 | 27 |
| (1) | 1.06 | . 00 | . 53 | . 00 | . 00 | . 00 | . 00 | . 00 | 2.13 | 3.72 | 2.66 | . 53 | 1.60 | 1.06 | . 53 | . 53 | . 00 | 14.36 |
| (2) | . 05 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 09 | . 16 | . 12 | . 02 | . 07 | . 05 | . 02 | . 02 | . 00 | . 63 |
| 6.1-8.0 | 3 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 3 | 3 | 5 | 9 | 8 | 2 | 0 | 42 |
| (1) | 1.60 | 1.60 | 1.06 | . 00 | . 00 | . 00 | . 00 | . 00 | . 53 | 1.60 | 1.60 | 1.60 | 2.66 | 4.79 | 4.26 | 1.06 | . 00 | 22.34 |
| (2) | . 07 | . 07 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 07 | . 07 | . 07 | . 12 | . 21 | . 19 | . 05 | . 00 | . 97 |
| 8.1-10.0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 6 | 8 | 1 | 0 | 18 |
| (1) | . 00 | . 53 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.06 | . 00 | . 00 | 3.19 | 4.26 | . 53 | . 00 | 9.57 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 00 | . 14 | . 19 | . 02 | . 00 | . 42 |
| 10.1-89.5 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 4 | 0 | 0 | 9 |
| (1) | . 00 | . 53 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.06 | . 00 | . 00 | 1.06 | 2.13 | . 00 | . 00 | 4.79 |
| (2) | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 00 | . 05 | . 09 | . 00 | . 00 | . 21 |
| ALL SPEEDS | 12 | 14 | 7 | 2 | 2 | 5 | 2 | 5 | 9 | 12 | 15 | 12 | 17 | 29 | 29 | 16 | 0 | 188 |
| (1) | 6.38 | 7.45 | 3.72 | 1.06 | 1.06 | 2.66 | 1.06 | 2.66 | 4.79 | 6.38 | 7.98 | 6.38 | 9.04 | 15.43 | 15.43 | 8.51 | . 00 | 100.00 |
| (2) | . 28 | . 32 | . 16 | . 05 | . 05 | . 12 | . 05 | . 12 | . 21 | . 28 | . 35 | . 28 | . 39 | . 67 | . 67 | . 37 | . 00 | 4.36 |

(1) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
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## Table 2.3-41—\{CCNPP 197 ft (60 m) December JFD (2000-2005)\}

## (Page 4 of 8)

CC DECEMBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS D CLASS FREQUENCY (PERCENT) = 35.33

|  |  |  |  |  |  |  |  | IND DIR | RECTIO | FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT $\begin{array}{r}\text {. } 2 \\ \\ \\ \\ \\ \\ (1) \\ (2)\end{array}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
|  | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-\quad .4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
|  | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $5-1.0$ | 0 | 4 | 2 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 2 | 0 | 11 |
|  | . 00 | . 26 | . 13 | . 07 | . 00 | . 00 | . 00 | . 07 | . 00 | . 00 | . 07 | . 00 | . 00 | . 00 | . 00 | . 13 | . 00 | . 72 |
|  | . 00 | . 09 | . 05 | . 02 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 25 |
| 1.1-1.5 | 3 | 2 | 1 | 2 | 2 | 0 | 1 | 1 | 0 | 0 | 1 | 1 | 2 | 2 | 2 | 1 | 0 | 21 |
| (1) | . 20 | . 13 | . 07 | . 13 | . 13 | . 00 | . 07 | . 07 | . 00 | . 00 | . 07 | . 07 | . 13 | . 13 | . 13 | . 07 | . 00 | 1.38 |
| $\begin{array}{r} (2) \\ 1.6-\quad 2.0 \end{array}$ | . 07 | . 05 | . 02 | . 05 | . 05 | . 00 | . 02 | . 02 | . 00 | . 00 | . 02 | . 02 | . 05 | . 05 | . 05 | . 02 | . 00 | . 49 |
|  | 5 | 3 | 5 | 4 | 5 | 3 | 1 | 1 | 2 | 1 | 1 | 3 | 1 | 4 | 1 | 5 | 0 | 45 |
| (1) | . 33 | . 20 | . 33 | . 26 | . 33 | . 20 | . 07 | . 07 | . 13 | . 07 | . 07 | . 20 | . 07 | . 26 | . 07 | . 33 | . 00 | 2.95 |
| (2) | . 12 | . 07 | . 12 | . 09 | . 12 | . 07 | . 02 | . 02 | . 05 | . 02 | . 02 | . 07 | . 02 | . 09 | . 02 | . 12 | . 00 | 1.04 |
| $2.1-3.0$ | 17 | 14 | 5 | 9 | 4 | 7 | 4 | 6 | 7 | 4 | 2 | 12 | 13 | 8 | 11 | 3 | 0 | 126 |
| $\begin{array}{r} 2.1-3.0 \\ (1) \end{array}$ | 1.12 | . 92 | . 33 | . 59 | . 26 | . 46 | . 26 | . 39 | . 46 | . 26 | . 13 | . 79 | . 85 | . 52 | . 72 | . 20 | . 00 | 8.27 |
| $\begin{array}{r} \text { (2) } \\ 3.1-4.0 \end{array}$ | . 39 | . 32 | . 12 | . 21 | . 09 | . 16 | . 09 | . 14 | . 16 | . 09 | . 05 | . 28 | . 30 | . 19 | . 25 | . 07 | . 00 | 2.92 |
|  | 23 | 12 | 15 | 18 | 7 | 7 | 10 | 10 | 14 | 9 | 5 | 10 | 11 | 15 | 22 | 29 | 0 | 217 |
| $3.1-4.0$ <br> (1) | 1.51 | . 79 | . 98 | 1.18 | . 46 | . 46 | . 66 | . 66 | . 92 | . 59 | . 33 | . 66 | . 72 | . 98 | 1.44 | 1.90 | . 00 | 14.24 |
| (2) | . 53 | . 28 | . 35 | . 42 | . 16 | . 16 | . 23 | . 23 | . 32 | . 21 | . 12 | . 23 | . 25 | . 35 | . 51 | . 67 | . 00 | 5.03 |
|  | 19 | 15 | 19 | 15 | 5 | 7 | 10 | 12 | 14 | 15 | 12 | 9 | 7 | 16 | 20 | 33 | 0 | 228 |
| $\begin{array}{r} 4.1-5.0 \\ (1) \end{array}$ | 1.25 | . 98 | 1.25 | . 98 | . 33 | . 46 | . 66 | . 79 | . 92 | . 98 | . 79 | . 59 | . 46 | 1.05 | 1.31 | 2.17 | . 00 | 14.96 |
| (2) | . 44 | . 35 | . 44 | . 35 | . 12 | . 16 | . 23 | . 28 | . 32 | . 35 | . 28 | . 21 | . 16 | . 37 | . 46 | . 76 | . 00 | 5.29 |
|  | 22 | 22 | 19 | 12 | 3 | 2 | 3 | 6 | 8 | 13 | 12 | 13 | 12 | 19 | 28 | 28 | 0 | 222 |
| $\begin{array}{r} 5.1-6.0 \\ (1) \end{array}$ | 1.44 | 1.44 | 1.25 | . 79 | . 20 | . 13 | . 20 | . 39 | . 52 | . 85 | . 79 | . 85 | . 79 | 1.25 | 1.84 | 1.84 | . 00 | 14.57 |
| (2) | . 51 | . 51 | . 44 | . 28 | . 07 | . 05 | . 07 | . 14 | . 19 | . 30 | . 28 | . 30 | . 28 | . 44 | . 65 | . 65 | . 00 | 5.15 |
| $6.1-8.0$ | 53 | 54 | 27 | 7 | 0 | 0 | 2 | 15 | 13 | 16 | 25 | 15 | 17 | 37 | 73 | 41 | 0 | 395 |
| (1) | 3.48 | 3.54 | 1.77 | . 46 | . 00 | . 00 | . 13 | . 98 | . 85 | 1.05 | 1.64 | . 98 | 1.12 | 2.43 | 4.79 | 2.69 | . 00 | 25.92 |
| 8.1-10.0 | 1.23 | 1.25 | . 63 | . 16 | . 00 | . 00 | . 05 | . 35 | . 30 | . 37 | . 58 | . 35 | . 39 | . 86 | 1.69 | . 95 | . 00 | 9.16 |
|  | 29 | 25 | 14 | 1 | 0 | 0 | 2 | 9 | 5 | 6 | 12 | 1 | 9 | 30 | 34 | 14 | 0 | 191 |
| (1) | 1.90 | 1.64 | . 92 | . 07 | . 00 | . 00 | . 13 | . 59 | . 33 | . 39 | . 79 | . 07 | . 59 | 1.97 | 2.23 | . 92 | . 00 | 12.53 |
| (2) | . 67 | . 58 | . 32 | . 02 | . 00 | . 00 | . 05 | . 21 | . 12 | . 14 | . 28 | . 02 | . 21 | . 70 | . 79 | . 32 | . 00 | 4.43 |
| 10.1-89.5 | 9 | 6 | 9 | 0 | 0 | 0 | 5 | 3 | 2 | 0 | 1 | 3 | 3 | 14 | 10 | 3 | 0 | 68 |
| (1) <br> (2) | . 59 | . 39 | . 59 | . 00 | . 00 | . 00 | . 33 | . 20 | . 13 | . 00 | . 07 | . 20 | . 20 | . 92 | . 66 | . 20 | . 00 | 4.46 |
|  | . 21 | . 14 | . 21 | . 00 | . 00 | . 00 | . 12 | . 07 | . 05 | . 00 | . 02 | . 07 | . 07 | . 32 | . 23 | . 07 | . 00 | 1.58 |
| ALL SPEEDS | 180 | 157 | 116 | 69 | 26 | 26 | 38 | 64 | 65 | 64 | 72 | 67 | 75 | 145 | 201 | 159 | 0 | 1524 |
| (1) <br> (2) | 11.81 | 10.30 | 7.61 | 4.53 | 1.71 | 1.71 | 2.49 | 4.20 | 4.27 | 4.20 | 4.72 | 4.40 | 4.92 | 9.51 | 13.19 | 10.43 | . 00 | 100.00 |
|  | 4.17 | 3.64 | 2.69 | 1.60 | . 60 | . 60 | . 88 | 1.48 | 1.51 | 1.48 | 1.67 | 1.55 | 1.74 | 3.36 | 4.66 | 3.69 | . 00 | 35.33 |
| (1) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE(2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Table 2.3-41—\{CCNPP 197 ft (60 m) December JFD (2000-2005)\} (Page 5 of 8)
CC DECEMBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS E CLASS FREQUENCY (PERCENT) = 36.07

|  | WIND DIRECTION FROM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 1 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 2 | 3 | 0 | 0 | 2 | 0 | 14 |
| (1) | . 06 | . 06 | . 06 | . 00 | . 00 | . 06 | . 00 | . 00 | . 00 | . 19 | . 00 | . 13 | . 19 | . 00 | . 00 | . 13 | . 00 | . 90 |
| (2) | . 02 | . 02 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 07 | . 00 | . 05 | . 07 | . 00 | . 00 | . 05 | . 00 | . 32 |
| 1.1-1.5 | 2 | 0 | 1 | 1 | 2 | 0 | 1 | 1 | 1 | 2 | 0 | 2 | 0 | 1 | 3 | 0 | 0 | 17 |
| (1) | . 13 | . 00 | . 06 | . 06 | . 13 | . 00 | . 06 | . 06 | . 06 | . 13 | . 00 | . 13 | . 00 | . 06 | . 19 | . 00 | . 00 | 1.09 |
| (2) | . 05 | . 00 | . 02 | . 02 | . 05 | . 00 | . 02 | . 02 | . 02 | . 05 | . 00 | . 05 | . 00 | . 02 | . 07 | . 00 | . 00 | . 39 |
| 1.6-2.0 | 3 | 3 | 1 | 2 | 2 | 0 | 1 | 3 | 1 | 0 | 3 | 1 | 2 | 2 | 0 | 2 | 0 | 26 |
| (1) | . 19 | . 19 | . 06 | . 13 | . 13 | . 00 | . 06 | . 19 | . 06 | . 00 | . 19 | . 06 | . 13 | . 13 | . 00 | . 13 | . 00 | 1.67 |
| (2) | . 07 | . 07 | . 02 | . 05 | . 05 | . 00 | . 02 | . 07 | . 02 | . 00 | . 07 | . 02 | . 05 | . 05 | . 00 | . 05 | . 00 | . 60 |
| 2.1-3.0 | 6 | 6 | 8 | 6 | 2 | 6 | 9 | 4 | 6 | 4 | 5 | 3 | 9 | 9 | 16 | 11 | 0 | 110 |
| (1) | . 39 | . 39 | . 51 | . 39 | . 13 | . 39 | . 58 | . 26 | . 39 | . 26 | . 32 | . 19 | . 58 | . 58 | 1.03 | . 71 | . 00 | 7.07 |
| (2) | . 14 | . 14 | . 19 | . 14 | . 05 | . 14 | . 21 | . 09 | . 14 | . 09 | . 12 | . 07 | . 21 | . 21 | . 37 | . 25 | . 00 | 2.55 |
| 3.1-4.0 | 16 | 9 | 12 | 6 | 6 | 6 | 4 | 16 | 14 | 13 | 3 | 12 | 16 | 35 | 27 | 19 | 0 | 214 |
| (1) | 1.03 | . 58 | . 77 | . 39 | . 39 | . 39 | . 26 | 1.03 | . 90 | . 84 | . 19 | . 77 | 1.03 | 2.25 | 1.74 | 1.22 | . 00 | 13.75 |
| (2) | . 37 | . 21 | . 28 | . 14 | . 14 | . 14 | . 09 | . 37 | . 32 | . 30 | . 07 | . 28 | . 37 | . 81 | . 63 | . 44 | . 00 | 4.96 |
| 4.1-5.0 | 13 | 14 | 7 | 5 | 0 | 8 | 21 | 7 | 19 | 11 | 8 | 12 | 24 | 57 | 69 | 57 | 0 | 332 |
| (1) | . 84 | . 90 | . 45 | . 32 | . 00 | . 51 | 1.35 | . 45 | 1.22 | . 71 | . 51 | . 77 | 1.54 | 3.66 | 4.43 | 3.66 | . 00 | 21.34 |
| (2) | . 30 | . 32 | . 16 | . 12 | . 00 | . 19 | . 49 | . 16 | . 44 | . 25 | . 19 | . 28 | . 56 | 1.32 | 1.60 | 1.32 | . 00 | 7.70 |
| 5.1-6.0 | 14 | 3 | 1 | 0 | 0 | 2 | 7 | 22 | 26 | 20 | 23 | 16 | 24 | 51 | 55 | 50 | 0 | 314 |
| (1) | . 90 | . 19 | . 06 | . 00 | . 00 | . 13 | . 45 | 1.41 | 1.67 | 1.29 | 1.48 | 1.03 | 1.54 | 3.28 | 3.53 | 3.21 | . 00 | 20.18 |
| (2) | . 32 | . 07 | . 02 | . 00 | . 00 | . 05 | . 16 | . 51 | . 60 | . 46 | . 53 | . 37 | . 56 | 1.18 | 1.27 | 1.16 | . 00 | 7.28 |
| 6.1-8.0 | 8 | 7 | 1 | 0 | 0 | 0 | 3 | 20 | 31 | 70 | 90 | 20 | 27 | 57 | 39 | 25 | 0 | 398 |
| (1) | . 51 | . 45 | . 06 | . 00 | . 00 | . 00 | . 19 | 1.29 | 1.99 | 4.50 | 5.78 | 1.29 | 1.74 | 3.66 | 2.51 | 1.61 | . 00 | 25.58 |
| (2) | . 19 | . 16 | . 02 | . 00 | . 00 | . 00 | . 07 | . 46 | . 72 | 1.62 | 2.09 | . 46 | . 63 | 1.32 | . 90 | . 58 | . 00 | 9.23 |
| 8.1-10.0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 9 | 8 | 30 | 43 | 2 | 3 | 17 | 2 | 0 | 0 | 117 |
| (1) | . 06 | . 06 | . 00 | . 00 | . 00 | . 00 | . 06 | . 58 | . 51 | 1.93 | 2.76 | . 13 | . 19 | 1.09 | . 13 | . 00 | . 00 | 7.52 |
| (2) | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 | . 21 | . 19 | . 70 | 1.00 | . 05 | . 07 | . 39 | . 05 | . 00 | . 00 | 2.71 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 6 | 0 | 2 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 14 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 19 | . 39 | . 00 | . 13 | . 13 | . 00 | . 00 | . 06 | . 00 | . 00 | . 00 | . 90 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 | . 14 | . 00 | . 05 | . 05 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 32 |
| ALL SPEEDS | 64 | 44 | 32 | 20 | 12 | 23 | 50 | 88 | 106 | 155 | 177 | 70 | 108 | 230 | 211 | 166 | 0 | 1556 |
| (1) | 4.11 | 2.83 | 2.06 | 1.29 | . 77 | 1.48 | 3.21 | 5.66 | 6.81 | 9.96 | 11.38 | 4.50 | 6.94 | 14.78 | 13.56 | 10.67 | . 00 | 100.00 |
| (2) | 1.48 | 1.02 | . 74 | . 46 | . 28 | . 53 | 1.16 | 2.04 | 2.46 | 3.59 | 4.10 | 1.62 | 2.50 | 5.33 | 4.89 | 3.85 | . 00 | 36.07 |

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| CC DECEMBER MET DATA JOINT FREQUENCY DISTRIBUTION | ( $60-$ METER TOWER) |  |  |
| :---: | :---: | :---: | :---: | :---: |
| 197.0 FT WIND DATA | STABILITY CLASS F | CLASS FREQUENCY | (PERCENT) $=8.81$ | 197.0 FT WIND DATA

Table 2.3-41—\{CCNPP 197 ft ( 60 m ) December JFD (2000-2005)\}

## (Page 6 of 8)

|  |  |  |  |  |  |  |  | D | IRECTIO | N FROM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 0 | 0 | 1 | 1 | 2 | 1 | 1 | 1 | 0 | 1 | 1 | 0 | 1 | 2 | 1 | 2 | 0 | 15 |
| (1) | . 00 | . 00 | . 26 | . 26 | . 53 | . 26 | . 26 | . 26 | . 00 | . 26 | . 26 | . 00 | . 26 | . 53 | . 26 | . 53 | . 00 | 3.95 |
| (2) | . 00 | . 00 | . 02 | . 02 | . 05 | . 02 | . 02 | . 02 | . 00 | . 02 | . 02 | . 00 | . 02 | . 05 | . 02 | . 05 | . 00 | . 35 |
| 1.1-1.5 | 1 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 0 | 2 | 0 | 3 | 1 | 0 | 15 |
| (1) | . 26 | . 53 | . 26 | . 00 | . 00 | . 00 | . 00 | . 26 | . 26 | . 26 | . 53 | . 00 | . 53 | . 00 | . 79 | . 26 | . 00 | 3.95 |
| (2) | . 02 | . 05 | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 02 | . 05 | . 00 | . 05 | . 00 | . 07 | . 02 | . 00 | . 35 |
| 1.6-2.0 | 0 | 0 | 2 | 0 | 2 | 3 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 14 |
| (1) | . 00 | . 00 | . 53 | . 00 | . 53 | . 79 | . 26 | . 00 | . 26 | . 26 | . 00 | . 00 | . 00 | . 00 | . 26 | . 79 | . 00 | 3.68 |
| (2) | . 00 | . 00 | . 05 | . 00 | . 05 | . 07 | . 02 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 02 | . 07 | . 00 | . 32 |
| 2.1-3.0 | 7 | 3 | 1 | 1 | 2 | 0 | 1 | 8 | 2 | 3 | 5 | 1 | 4 | 8 | 4 | 7 | 0 | 57 |
| (1) | 1.84 | . 79 | . 26 | . 26 | . 53 | . 00 | . 26 | 2.11 | . 53 | . 79 | 1.32 | . 26 | 1.05 | 2.11 | 1.05 | 1.84 | . 00 | 15.00 |
| (2) | . 16 | . 07 | . 02 | . 02 | . 05 | . 00 | . 02 | . 19 | . 05 | . 07 | . 12 | . 02 | . 09 | . 19 | . 09 | . 16 | . 00 | 1.32 |
| 3.1-4.0 | 2 | 1 | 1 | 0 | 2 | 1 | 1 | 1 | 2 | 4 | 10 | 7 | 4 | 5 | 11 | 9 | 0 | 61 |
| (1) | . 53 | . 26 | . 26 | . 00 | . 53 | . 26 | . 26 | . 26 | . 53 | 1.05 | 2.63 | 1.84 | 1.05 | 1.32 | 2.89 | 2.37 | . 00 | 16.05 |
| (2) | . 05 | . 02 | . 02 | . 00 | . 05 | . 02 | . 02 | . 02 | . 05 | . 09 | . 23 | . 16 | . 09 | . 12 | . 25 | . 21 | . 00 | 1.41 |
| 4.1-5.0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 3 | 3 | 5 | 8 | 8 | 3 | 14 | 11 | 5 | 0 | 62 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 53 | . 79 | . 79 | 1.32 | 2.11 | 2.11 | . 79 | 3.68 | 2.89 | 1.32 | . 00 | 16.32 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 | . 07 | . 07 | . 12 | . 19 | . 19 | . 07 | . 32 | . 25 | . 12 | . 00 | 1.44 |
| 5.1-6.0 | 1 | 0 | 0 | 0 | 0 | 0 | 4 | 2 | 13 | 18 | 8 | 4 | 6 | 4 | 10 | 2 | 0 | 72 |
| (1) | . 26 | . 00 | . 00 | . 00 | . 00 | . 00 | 1.05 | . 53 | 3.42 | 4.74 | 2.11 | 1.05 | 1.58 | 1.05 | 2.63 | . 53 | . 00 | 18.95 |
| (2) | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 09 | . 05 | . 30 | . 42 | . 19 | . 09 | . 14 | . 09 | . 23 | . 05 | . 00 | 1.67 |
| 6.1-8.0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 18 | 29 | 19 | 8 | 1 | 3 | 0 | 0 | 0 | 81 |
| (1) | . 53 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 26 | 4.74 | 7.63 | 5.00 | 2.11 | . 26 | . 79 | . 00 | . 00 | . 00 | 21.32 |
| (2) | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 42 | . 67 | . 44 | . 19 | . 02 | . 07 | . 00 | . 00 | . 00 | 1.88 |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 26 | . 26 | . 26 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 79 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| ALL SPEEDS | 13 | 6 | 6 | 2 | 8 | 5 | 10 | 17 | 41 | 63 | 54 | 28 | 21 | 36 | 41 | 29 | 0 | 380 |
| (1) | 3.42 | 1.58 | 1.58 | . 53 | 2.11 | 1.32 | 2.63 | 4.47 | 10.79 | 16.58 | 14.21 | 7.37 | 5.53 | 9.47 | 10.79 | 7.63 | .00 | 100.00 |
| (2) | . 30 | . 14 | . 14 | . 05 | . 19 | . 12 | . 23 | . 39 | . 95 | 1.46 | 1.25 | . 65 | . 49 | . 83 | . 95 | . 67 | . 00 | 8.81 |

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| CC DECEMBER MET DATA JOINT | FREQUENCY DISTRIBUTION | (60-METER TOWER) |  |
| :---: | :---: | :---: | :---: | :---: |
| 197.0 FT WIND DATA | STABILITY CLASS G | CLASS FREQUENCY | (PERCENT) $=2.90$ |



Table 2.3-41—\{CCNPP 197 ft (60 m) December JFD (2000-2005)\} (Page 8 of 8)
CC DECEMBER MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS ALL CLASS FREQUENCY (PERCENT) = 100.00

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| .5-1.0 | 4 | 5 | 4 | 2 | 3 | 3 | 1 | 2 | 1 | 6 | 2 | 2 | 4 | 2 | 2 | 7 | 0 | 50 |
| (1) | . 09 | . 12 | . 09 | . 05 | . 07 | . 07 | . 02 | . 05 | . 02 | . 14 | . 05 | . 05 | . 09 | . 05 | . 05 | . 16 | . 00 | 1.16 |
| (2) | . 09 | . 12 | . 09 | . 05 | . 07 | . 07 | . 02 | . 05 | . 02 | . 14 | . 05 | . 05 | . 09 | . 05 | . 05 | . 16 | . 00 | 1.16 |
| 1.1-1.5 | 7 | 6 | 5 | 3 | 4 | 0 | 3 | 3 | 2 | 4 | 3 | 3 | 4 | 4 | 9 | 2 | 0 | 62 |
| (1) | . 16 | . 14 | . 12 | . 07 | . 09 | . 00 | . 07 | . 07 | . 05 | . 09 | . 07 | . 07 | . 09 | . 09 | . 21 | . 05 | . 00 | 1.44 |
| (2) | . 16 | . 14 | . 12 | . 07 | . 09 | . 00 | . 07 | . 07 | . 05 | . 09 | . 07 | . 07 | . 09 | . 09 | . 21 | . 05 | . 00 | 1.44 |
| 1.6-2.0 | 9 | 9 | 12 | 9 | 11 | 6 | 5 | 4 | 6 | 7 | 6 | 5 | 4 | 6 | 5 | 11 | 0 | 115 |
| (1) | . 21 | . 21 | . 28 | . 21 | . 25 | . 14 | . 12 | . 09 | . 14 | . 16 | . 14 | . 12 | . 09 | . 14 | . 12 | . 25 | . 00 | 2.67 |
| (2) | . 21 | . 21 | . 28 | . 21 | . 25 | . 14 | . 12 | . 09 | . 14 | . 16 | . 14 | . 12 | . 09 | . 14 | . 12 | . 25 | . 00 | 2.67 |
| 2.1-3.0 | 35 | 34 | 17 | 18 | 13 | 17 | 16 | 21 | 16 | 17 | 16 | 27 | 33 | 31 | 41 | 26 | 0 | 378 |
| (1) | . 81 | . 79 | . 39 | . 42 | . 30 | . 39 | . 37 | . 49 | . 37 | . 39 | . 37 | . 63 | . 76 | . 72 | . 95 | . 60 | . 00 | 8.76 |
| (2) | . 81 | . 79 | . 39 | . 42 | . 30 | . 39 | . 37 | . 49 | . 37 | . 39 | . 37 | . 63 | . 76 | . 72 | . 95 | . 60 | . 00 | 8.76 |
| 3.1-4.0 | 54 | 34 | 34 | 24 | 17 | 15 | 16 | 31 | 34 | 35 | 30 | 35 | 40 | 67 | 67 | 66 | 0 | 599 |
| (1) | 1.25 | . 79 | . 79 | . 56 | . 39 | . 35 | . 37 | . 72 | . 79 | . 81 | . 70 | . 81 | . 93 | 1.55 | 1.55 | 1.53 | . 00 | 13.89 |
| (2) | 1.25 | . 79 | . 79 | . 56 | . 39 | . 35 | . 37 | . 72 | . 79 | . 81 | . 70 | . 81 | . 93 | 1.55 | 1.55 | 1.53 | . 00 | 13.89 |
| 4.1-5.0 | 50 | 36 | 27 | 20 | 5 | 16 | 35 | 30 | 41 | 41 | 43 | 47 | 42 | 101 | 112 | 106 | 0 | 752 |
| (1) | 1.16 | . 83 | . 63 | . 46 | . 12 | . 37 | . 81 | . 70 | . 95 | . 95 | 1.00 | 1.09 | . 97 | 2.34 | 2.60 | 2.46 | . 00 | 17.43 |
| (2) | 1.16 | . 83 | . 63 | . 46 | . 12 | . 37 | . 81 | . 70 | . 95 | . 95 | 1.00 | 1.09 | . 97 | 2.34 | 2.60 | 2.46 | . 00 | 17.43 |
| 5.1-6.0 | 50 | 29 | 22 | 13 | 3 | 4 | 14 | 34 | 56 | 81 | 64 | 45 | 54 | 90 | 105 | 88 | 0 | 752 |
| (1) | 1.16 | . 67 | . 51 | . 30 | . 07 | . 09 | . 32 | . 79 | 1.30 | 1.88 | 1.48 | 1.04 | 1.25 | 2.09 | 2.43 | 2.04 | . 00 | 17.43 |
| (2) | 1.16 | . 67 | . 51 | . 30 | . 07 | . 09 | . 32 | . 79 | 1.30 | 1.88 | 1.48 | 1.04 | 1.25 | 2.09 | 2.43 | 2.04 | . 00 | 17.43 |
| 6.1-8.0 | 85 | 70 | 33 | 9 | 0 | 0 | 5 | 39 | 71 | 143 | 155 | 63 | 66 | 127 | 145 | 74 | 0 | 1085 |
| (1) | 1.97 | 1.62 | . 76 | . 21 | . 00 | . 00 | . 12 | . 90 | 1.65 | 3.31 | 3.59 | 1.46 | 1.53 | 2.94 | 3.36 | 1.72 | . 00 | 25.15 |
| (2) | 1.97 | 1.62 | . 76 | . 21 | . 00 | . 00 | . 12 | . 90 | 1.65 | 3.31 | 3.59 | 1.46 | 1.53 | 2.94 | 3.36 | 1.72 | . 00 | 25.15 |
| 8.1-10.0 | 35 | 30 | 16 | 1 | 0 | 0 | 3 | 18 | 15 | 41 | 65 | 4 | 16 | 80 | 69 | 17 | 0 | 410 |
| (1) | . 81 | . 70 | . 37 | . 02 | . 00 | . 00 | . 07 | . 42 | . 35 | . 95 | 1.51 | . 09 | . 37 | 1.85 | 1.60 | . 39 | . 00 | 9.50 |
| (2) | . 81 | . 70 | . 37 | . 02 | . 00 | . 00 | . 07 | . 42 | . 35 | . 95 | 1.51 | . 09 | . 37 | 1.85 | 1.60 | . 39 | . 00 | 9.50 |
| 10.1-89.5 | 9 | 7 | 9 | 0 | 0 | 0 | 8 | 9 | 3 | 3 | 5 | 4 | 3 | 22 | 26 | 3 | 0 | 111 |
| (1) | . 21 | . 16 | . 21 | . 00 | . 00 | . 00 | . 19 | . 21 | . 07 | . 07 | . 12 | . 09 | . 07 | . 51 | . 60 | . 07 | . 00 | 2.57 |
| (2) | . 21 | . 16 | . 21 | . 00 | . 00 | . 00 | . 19 | . 21 | . 07 | . 07 | . 12 | . 09 | . 07 | . 51 | . 60 | . 07 | . 00 | 2.57 |
| ALL SPEEDS | 338 | 260 | 179 | 99 | 56 | 61 | 106 | 191 | 245 | 378 | 389 | 235 | 266 | 530 | 581 | 400 | 0 | 4314 |
| (1) | 7.83 | 6.03 | 4.15 | 2.29 | 1.30 | 1.41 | 2.46 | 4.43 | 5.68 | 8.76 | 9.02 | 5.45 | 6.17 | 12.29 | 13.47 | 9.27 | . 00 | 100.00 |
| (2) | 7.83 | 6.03 | 4.15 | 2.29 | 1.30 | 1.41 | 2.46 | 4.43 | 5.68 | 8.76 | 9.02 | 5.45 | 6.17 | 12.29 | 13.47 | 9.27 | . 00 | 100.00 |


| $\begin{gathered} \underset{\lambda}{\lambda} \\ \underset{0}{0} \\ \underset{\sim}{c} \\ \underset{\omega}{\omega} \end{gathered}$ | Table 2.3-42—\{CCNPP 33 Feet Wind Direction Persistence Summary for Year 2000\} <br> (Page 1 of 2) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SECTOR | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | Direction Persistence (Hours)/Percent |  |  |  |  |  |  | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
|  |  |  |  |  |  |  |  |  |  |  | 10 | 11 | 12 | 13 | 14 | 15 | 16 |  |  |  |  |  |  |  |  |  |  |
|  | N | 158 | 55 | 22 | 15 | 14 | 9 | 2 | 2 | 1 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 282 |
|  |  | 56 | 76 | 83 | 89 | 94 | 97 | 98 | 98 | 99 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | NNE | 176 | 63 | 35 | 13 | 12 | 4 | 2 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 308 |
|  |  | 57 | 78 | 89 | 93 | 97 | 98 | 99 | 99 | 99 | 99 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | NE | 159 | 54 | 25 | 8 | 4 | 3 | 3 | 4 | 3 | 1 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 267 |
|  |  | 60 | 80 | 89 | 92 | 94 | 95 | 96 | 97 | 99 | 99 | 99 | 99 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | ENE | 156 | 33 | 17 | 9 | 2 | 4 | 2 | 1 | 0 | 2 | 1 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 230 |
|  |  | 68 | 82 | 90 | 93 | 94 | 96 | 97 | 97 | 97 | 98 | 99 | 99 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | E | 112 | 35 | 12 | 7 | 2 | 2 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 172 |
|  |  | 65 | 85 | 92 | 97 | 98 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | ESE | 76 | 26 | 4 | 2 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 112 |
|  |  | 68 | 91 | 95 | 96 | 96 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | SE | 110 | 19 | 7 | 2 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 141 |
|  |  | 78 | 91 | 96 | 98 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | SSE | 139 | 41 | 27 | 15 | 6 | 1 | 4 | 1 | 1 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 238 |
|  |  | 58 | 76 | 87 | 93 | 96 | 96 | 98 | 98 | 99 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\begin{aligned} & \text { R } \\ & \stackrel{0}{2} \\ & i \end{aligned}$ | S | 192 | 49 | 25 | 14 | 5 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 287 |


|  | Table 2.3-42—\{CCNPP 33 Feet Wind Direction Persistence Summary for Year 2000\} <br> (Page 2 of 2) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SECTOR | $\frac{1}{67}$ | $\frac{2}{84}$ | $\frac{3}{93}$ | $\begin{gathered} 4 \\ \hline 98 \end{gathered}$ | $\frac{5}{99}$ | $\begin{gathered} 6 \\ \hline 99 \end{gathered}$ | $\frac{7}{100}$ | $\frac{8}{100}$ | $\frac{9}{100}$ | $\begin{gathered} \text { Direc } \\ \mathbf{1 0} \\ \hline 0 \end{gathered}$ | ion P <br> 11 <br> 0 | rsiste <br> 12 <br> 0 | a130 | crs)/ <br> 14 <br> 0 | $\begin{gathered} \\ \hline 15 \\ \hline 0 \end{gathered}$ | $\frac{16}{0}$ | $\begin{gathered} 17 \\ \hline 0 \end{gathered}$ | $\begin{gathered} 18 \\ \hline 0 \end{gathered}$ | $\begin{gathered} 19 \\ \hline 0 \end{gathered}$ | $\frac{20}{0}$ | $\frac{21}{0}$ | $\frac{22}{0}$ | $\frac{23}{0}$ |  |  | TOTAL |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\frac{24}{0}$ | $\begin{gathered} \text { GT. } 24 \\ 0 \end{gathered}$ |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | SSW | 227 | 86 | 36 | 16 | 11 | 8 | 0 | 2 | 5 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 394 |
|  |  | 58 | 79 | 89 | 93 | 95 | 97 | 97 | 98 | 99 | 99 | 99 | 99 | 99 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | SW | 234 | 103 | 45 | 23 | 22 | 17 | 8 | 10 | 4 | 4 | 1 | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 477 |
|  |  | 49 | 71 | 80 | 85 | 90 | 93 | 95 | 97 | 98 | 99 | 99 | 99 | 99 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 |  |
|  | WSW | 216 | 82 | 23 | 20 | 9 | 5 | 3 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 359 |
|  |  | 60 | 83 | 89 | 95 | 97 | 99 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | W | 198 | 53 | 29 | 3 | 6 | 2 | 0 | 2 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 295 |
|  |  | 67 | 85 | 95 | 96 | 98 | 99 | 99 | 99 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | WNW | 203 | 66 | 32 | 10 | 8 | 3 | 3 | 3 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 332 |
|  |  | 61 | 81 | 91 | 94 | 96 | 97 | 98 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 |  |
|  | NW | 202 | 58 | 36 | 15 | 13 | 11 | 5 | 4 | 4 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 350 |
|  |  | 58 | 74 | 85 | 89 | 93 | 96 | 97 | 98 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | NNW | 157 | 50 | 18 | 8 | 2 | 0 | 2 | 1 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 241 |
|  |  | 65 | 86 | 93 | 97 | 98 | 98 | 98 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | TOTAL | 2715 | 873 | 393 | 180 | 118 | 73 | 36 | 31 | 24 | 16 | 5 | 6 | 3 | 3 | 0 | 4 | 2 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 4485 |

Table 2．3－43—\｛CCNPP 33 Feet Wind Direction Persistence Summary for Year 2001\}
（Page 1 of 2）
Direction Persistence（Hours）／Percent

| SECTOR | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT． 24 | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N | 143 | 60 | 35 | 26 | 9 | 5 | 5 | 8 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 292 |
|  | 49 | 70 | 82 | 90 | 93 | 95 | 97 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |


| NNE | 183 | 65 | 33 | 7 | 4 | 4 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 300 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 61 | 83 | 94 | 96 | 97 | 99 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |


| NE | 159 | 41 | 17 | 10 | 7 | 5 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 242 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 66 | 83 | 90 | 94 | 97 | 99 | 99 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |



| E | 116 | 31 | 16 | 2 | 2 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 171 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 68 | 86 | 95 | 96 | 98 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |




ऽ＾＾әу

|  | Table 2.3-43—\{CCNPP 33 Feet Wind Direction Persistence Summary for Year 2001\} <br> (Page 2 of 2) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Direction Persistence (Hours)/Percent |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | SECTOR | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
|  |  | 61 | 80 | 89 | 93 | 97 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | SSW | 253 | 75 | 59 | 31 | 15 | 4 | 3 | 6 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 449 |
|  |  | 56 | 73 | 86 | 93 | 96 | 97 | 98 | 99 | 99 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | SW | 258 | 104 | 42 | 27 | 24 | 16 | 10 | 2 | 11 | 3 | 0 | 2 | 2 | 2 | 0 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 506 |
|  |  | 51 | 72 | 80 | 85 | 90 | 93 | 95 | 95 | 98 | 98 | 98 | 99 | 99 | 99 | 99 | 99 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 |  |
|  | WSW | 240 | 66 | 39 | 16 | 6 | 5 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 376 |
|  |  | 64 | 81 | 92 | 96 | 98 | 99 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | W | 175 | 51 | 17 | 6 | 3 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 254 |
|  |  | 69 | 89 | 96 | 98 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | WNW | 194 | 58 | 26 | 8 | 10 | 4 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 301 |
|  |  | 64 | 84 | 92 | 95 | 98 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | NW | 179 | 59 | 26 | 20 | 13 | 8 | 4 | 3 | 2 | 2 | 1 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 320 |
|  |  | 56 | 74 | 83 | 89 | 93 | 95 | 97 | 98 | 98 | 99 | 99 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | NNW | 162 | 45 | 20 | 13 | 6 | 4 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 254 |
|  |  | 64 | 81 | 89 | 94 | 97 | 98 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | TOTAL | 2705 | 881 | 426 | 205 | 127 | 73 | 39 | 30 | 21 | 6 | 5 | 3 | 6 | 3 | 1 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 4534 |


Table 2.3-44—\{CCNPP 33 Feet Wind Direction Persistence Summary for Year 2002\}
(Page 1 of 2)

|  | Direction Persistence (Hours)/Percent |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SECTOR | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
|  | N | 145 | 70 | 37 | 15 | 13 | 6 | 5 | 7 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 300 |
|  |  | 48 | 72 | 84 | 89 | 93 | 95 | 97 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | NNE | 165 | 73 | 27 | 19 | 7 | 4 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 299 |
|  |  | 55 | 80 | 89 | 95 | 97 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | NE | 144 | 51 | 26 | 11 | 9 | 2 | 1 | 3 | 1 | 3 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 254 |
|  |  | 57 | 77 | 87 | 91 | 95 | 96 | 96 | 97 | 98 | 99 | 99 | 99 | 99 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | ENE | 124 | 37 | 21 | 9 | 5 | 5 | 1 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 206 |
|  |  | 60 | 78 | 88 | 93 | 95 | 98 | 98 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | E | 95 | 30 | 15 | 0 | 2 | 1 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 145 |
|  |  | 66 | 86 | 97 | 97 | 98 | 99 | 99 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | ESE | 94 | 24 | 3 | 2 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 128 |
|  |  | 73 | 92 | 95 | 96 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  |  | 124 | 36 | 12 | 3 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 178 |
|  |  | 70 | 90 | 97 | 98 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\stackrel{7}{\sim}$ | SSE | 127 | 49 | 20 | 12 | 11 | 7 | 1 | 2 | 4 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 237 |
|  |  | 54 | 74 | 83 | 88 | 92 | 95 | 96 | 97 | 98 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | S | 149 | 62 | 24 | 13 | 8 | 6 | 3 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 267 |


|  | Table 2.3-44—\{CCNPP 33 Feet Wind Direction Persistence Summary for Year 2002\} <br> (Page 2 of 2) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SECTOR | $\frac{\mathbf{1}}{56}$ | $\frac{\mathbf{2}}{79}$ | $\frac{3}{88}$ | $\begin{gathered} \mathbf{4} \\ \hline 93 \end{gathered}$ | $\frac{5}{96}$ | $\begin{gathered} 6 \\ \hline 98 \end{gathered}$ | $\begin{gathered} 7 \\ \hline 99 \end{gathered}$ | $\frac{8}{99}$ | $\frac{9}{100}$ | $\begin{gathered} \hline \text { Direc } \\ \mathbf{1 0} \\ \hline 100 \end{gathered}$ | ion P <br> $\mathbf{1 1}$ <br> 100 | rsist12100 | 13 | Hours <br> 14 <br> 0 | $\begin{gathered} / \text { Per } \\ \mathbf{1 5} \\ \hline 0 \end{gathered}$ | $\begin{gathered} \text { nt } \\ 16 \\ \hline 0 \end{gathered}$ | $\begin{gathered} 17 \\ \hline 0 \end{gathered}$ | $\frac{18}{0}$ | $\frac{19}{0}$ | $\begin{gathered} 20 \\ \hline 0 \end{gathered}$ | $\frac{21}{0}$ | $\frac{22}{0}$ | $\frac{23}{0}$ | $\frac{\mathbf{2 4}}{0}$ | $\begin{gathered} \text { GT. } 24 \\ \hline 0 \end{gathered}$ | TOTAL |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | SSW | 213 | 85 | 41 | 20 | 11 | 10 | 5 | 2 | 4 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 392 |
|  |  | 54 | 76 | 86 | 92 | 94 | 97 | 98 | 99 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | SW | 238 | 95 | 54 | 20 | 19 | 12 | 8 | 8 | 8 | 8 | 3 | 4 | 2 | 0 | 0 | 2 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 484 |
|  |  | 49 | 69 | 80 | 84 | 88 | 90 | 92 | 94 | 95 | 97 | 98 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |  |
|  | WSW | 214 | 67 | 26 | 17 | 11 | 4 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 342 |
|  |  | 63 | 82 | 90 | 95 | 98 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | W | 177 | 44 | 20 | 12 | 3 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 259 |
|  |  | 68 | 85 | 93 | 98 | 99 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | WNW | 170 | 51 | 7 | 12 | 8 | 3 | 1 | 3 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 257 |
|  |  | 66 | 86 | 89 | 93 | 96 | 98 | 98 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | NW | 144 | 68 | 34 | 18 | 10 | 3 | 3 | 3 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 286 |
|  |  | 50 | 74 | 86 | 92 | 96 | 97 | 98 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | NNW | 147 | 60 | 23 | 19 | 11 | 4 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 267 |
|  |  | 55 | 78 | 86 | 93 | 97 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | TOTAL | 2470 | 902 | 390 | 202 | 134 | 71 | 31 | 37 | 24 | 16 | 8 | 7 | 2 | 0 | 1 | 2 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 4301 |

Table 2.3-45—\{CCNPP 33 Feet Wind Direction Persistence Summary for Year 2003\} (Page 1 of 2)

| Direction Persistence (Hours)/Percent |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SECTOR | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
| N | 145 | 73 | 34 | 13 | 10 | 9 | 4 | 4 | 1 | 2 | 3 | 1 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 301 |
|  | 48 | 72 | 84 | 88 | 91 | 94 | 96 | 97 | 97 | 98 | 99 | 99 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| NNE | 180 | 68 | 36 | 18 | 6 | 5 | 3 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 320 |
|  | 56 | 78 | 89 | 94 | 96 | 98 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| NE | 161 | 57 | 21 | 13 | 7 | 7 | 2 | 1 | 2 | 1 | 2 | 1 | 2 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 280 |
|  | 58 | 78 | 85 | 90 | 93 | 95 | 96 | 96 | 97 | 97 | 98 | 98 | 99 | 99 | 99 | 99 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 0 | 0 |  |
| ENE | 114 | 40 | 17 | 12 | 2 | 3 | 4 | 0 | 3 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 198 |
|  | 58 | 78 | 86 | 92 | 93 | 95 | 97 | 97 | 98 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 100 |  |
| E | 111 | 26 | 12 | 7 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 159 |
|  | 70 | 86 | 94 | 98 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| ESE | 110 | 22 | 8 | 3 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 146 |
|  | 75 | 90 | 96 | 98 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| SE | 134 | 30 | 16 | 8 | 4 | 2 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 197 |
|  | 68 | 83 | 91 | 95 | 97 | 98 | 99 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| SSE | 139 | 56 | 33 | 11 | 6 | 11 | 3 | 4 | 1 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 267 |
|  | 52 | 73 | 85 | 90 | 92 | 96 | 97 | 99 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| S | 173 | 68 | 28 | 15 | 13 | 2 | 1 | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 304 |


|  | Table 2.3-45—\{CCNPP 33 Feet Wind Direction Persistence Summary for Year 2003\} <br> (Page 2 of 2 ) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SECTOR | 1 |  |  |  | 5 |  | 7 |  |  | Direction Persistence (Hours)/Percent |  |  |  |  |  |  | 17 | 18 | 19 | 20 | 21 | 22 | 23 |  |  | TOTAL |
|  |  |  |  |  |  |  |  |  |  |  | 10 | 11 | 12 | 13 | 14 | 15 | 16 |  |  |  |  |  |  |  |  |  |  |
|  |  | 57 | 79 | 88 | 93 | 98 | 98 | 99 | 99 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | SSW | 220 | 75 | 32 | 22 | 7 | 7 | 0 | 4 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 371 |
|  |  | 59 | 80 | 88 | 94 | 96 | 98 | 98 | 99 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | SW | 248 | 77 | 40 | 30 | 12 | 8 | 9 | 5 | 4 | 4 | 4 | 0 | 1 | 1 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 446 |
|  |  | 56 | 73 | 82 | 89 | 91 | 93 | 95 | 96 | 97 | 98 | 99 | 99 | 99 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | WSW | 214 | 69 | 29 | 13 | 6 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 335 |
|  |  | 64 | 84 | 93 | 97 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | W | 202 | 43 | 17 | 11 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 280 |
|  |  | 72 | 88 | 94 | 98 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | WNW | 202 | 60 | 26 | 9 | 4 | 7 | 1 | 2 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 314 |
|  |  | 64 | 83 | 92 | 95 | 96 | 98 | 98 | 99 | 99 | 99 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | NW | 198 | 63 | 38 | 21 | 6 | 6 | 5 | 2 | 0 | 2 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 343 |
|  |  | 58 | 76 | 87 | 93 | 95 | 97 | 98 | 99 | 99 | 99 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | NNW | 148 | 56 | 14 | 13 | 4 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 239 |
|  |  | 62 | 85 | 91 | 97 | 98 | 98 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | TOTAL | 2699 | 883 | 401 | 219 | 99 | 71 | 38 | 26 | 16 | 15 | 13 | 5 | 3 | 4 | 2 | 2 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 4500 |

Table 2．3－46—\｛CCNPP 33 Feet Wind Direction Persistence Summary for Year 2004\}
（Page 1 of 2）

| Direction Persistence（Hours）／Percent |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SECTOR | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT． 24 | TOTAL |
| N | 151 | 61 | 39 | 23 | 10 | 2 | 2 | 4 | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 295 |
|  | 51 | 72 | 85 | 93 | 96 | 97 | 98 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| NNE | 185 | 59 | 34 | 13 | 9 | 1 | 5 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 309 |
|  | 60 | 79 | 90 | 94 | 97 | 97 | 99 | 99 | 99 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| NE | 156 | 54 | 19 | 8 | 10 | 5 | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 258 |
|  | 60 | 81 | 89 | 92 | 96 | 98 | 98 | 98 | 98 | 98 | 99 | 99 | 99 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| ENE | 142 | 46 | 21 | 8 | 5 | 3 | 0 | 1 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 229 |
|  | 62 | 82 | 91 | 95 | 97 | 98 | 98 | 99 | 99 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| E | 145 | 31 | 15 | 5 | 3 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 201 |
|  | 72 | 88 | 95 | 98 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| ESE | 128 | 18 | 10 | 3 | 5 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 168 |
|  | 76 | 87 | 93 | 95 | 98 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| SE | 121 | 41 | 15 | 4 | 2 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 187 |
|  | 65 | 87 | 95 | 97 | 98 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| SSE | 136 | 42 | 23 | 16 | 11 | 5 | 9 | 4 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 248 |
|  | 55 | 72 | 81 | 88 | 92 | 94 | 98 | 99 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| S | 194 | 65 | 33 | 15 | 10 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 321 |



| $\begin{gathered} \underset{\lambda}{\lambda} \\ \underset{0}{0} \\ \stackrel{c}{c} \\ \underset{\omega}{\omega} \end{gathered}$ | Table 2.3-47—\{CCNPP 33 Feet Wind Direction Persistence Summary for Year 2005\} <br> (Page 1 of 2) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SECTOR | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |  | ection <br> 11 | Persi12 | 13 | (Hour14 |  |  | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | N | 157 | 69 | 35 | 15 | 10 | 13 | 6 | 1 | 6 | 0 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 315 |
|  |  | 50 | 72 | 83 | 88 | 91 | 95 | 97 | 97 | 99 | 99 | 99 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | NNE | 199 | 67 | 26 | 14 | 7 | 6 | 2 | 4 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 327 |
|  |  | 61 | 81 | 89 | 94 | 96 | 98 | 98 | 99 | 99 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | NE | 151 | 45 | 29 | 13 | 8 | 7 | 2 | 4 | 3 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 264 |
|  |  | 57 | 74 | 85 | 90 | 93 | 96 | 97 | 98 | 99 | 99 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | ENE | 142 | 49 | 15 | 7 | 6 | 4 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 226 |
|  |  | 63 | 85 | 91 | 94 | 97 | 99 | 99 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | E | 116 | 37 | 17 | 8 | 6 | 5 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 191 |
|  |  | 61 | 80 | 89 | 93 | 96 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | ESE | 122 | 22 | 11 | 4 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 162 |
|  |  | 75 | 89 | 96 | 98 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | SE | 135 | 37 | 4 | 6 | 4 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 189 |
|  |  | 71 | 91 | 93 | 96 | 98 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | SSE | 129 | 49 | 31 | 15 | 9 | 9 | 5 | 4 | 1 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 254 |
|  |  | 51 | 70 | 82 | 88 | 92 | 95 | 97 | 99 | 99 | 99 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\left.\begin{aligned} & \underset{N}{0} \\ & \stackrel{N}{i} \\ & i \end{aligned} \right\rvert\,$ | S | 176 | 47 | 37 | 16 | 2 | 9 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 290 |


|  | Table 2.3-47—\{CCNPP 33 Feet Wind Direction Persistence Summary for Year 2005\} <br> (Page 2 of 2) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Direction Persistence (Hours)/Percent |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | SECTOR | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
|  |  | 61 | 77 | 90 | 95 | 96 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | SSW | 208 | 71 | 31 | 17 | 10 | 5 | 4 | 0 | 2 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 351 |
|  |  | 59 | 79 | 88 | 93 | 96 | 97 | 99 | 99 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | SW | 232 | 75 | 45 | 23 | 24 | 9 | 11 | 4 | 2 | 4 | 2 | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 436 |
|  |  | 53 | 70 | 81 | 86 | 92 | 94 | 96 | 97 | 97 | 98 | 99 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 |  |
|  | WSW | 222 | 65 | 36 | 12 | 8 | 4 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 350 |
|  |  | 63 | 82 | 92 | 96 | 98 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | W | 210 | 62 | 22 | 5 | 3 | 2 | 1 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 308 |
|  |  | 68 | 88 | 95 | 97 | 98 | 99 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | WNW | 189 | 56 | 17 | 14 | 4 | 3 | 1 | 2 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 291 |
|  |  | 65 | 84 | 90 | 95 | 96 | 97 | 98 | 98 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | NW | 160 | 72 | 23 | 16 | 11 | 4 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 291 |
|  |  | 55 | 80 | 88 | 93 | 97 | 98 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 100 | 100 | 100 | 100 | 100 |  |
|  | NNW | 133 | 35 | 19 | 5 | 3 | 2 | 2 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 204 |
|  |  | 65 | 82 | 92 | 94 | 96 | 97 | 98 | 98 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | TOTAL | 2681 | 858 | 398 | 190 | 118 | 83 | 40 | 26 | 19 | 12 | 3 | 5 | 1 | 6 | 3 | 2 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 4449 |

Table 2.3-48—\{CCNPP 33 Feet Average Wind Direction Persistence Summary for Years 2000-2005\}
(Page 1 of 2)
Direction Persistence (Hours)/Percent

| SECTOR | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | Direction Persistence (Hours)/Percent |  |  |  |  |  |  | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  | 9 | 10 | 11 | 12 | 13 | 14 | 15 |  |  |  |  |  |  |  |  |  |  |  |
| N | 150 | 65 | 34 | 18 | 11 | 7 | 4 | 4 | 2 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 298 |
|  | 50 | 72 | 84 | 90 | 93 | 96 | 97 | 98 | 99 | 83 | 83 | 66 | 66 | 67 | 50 | 33 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| NNE | 181 | 66 | 32 | 14 | 8 | 4 | 3 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 311 |
|  | 58 | 80 | 90 | 94 | 97 | 98 | 99 | 99 | 83 | 66 | 50 | 50 | 50 | 33 | 17 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| NE | 155 | 50 | 23 | 11 | 8 | 5 | 2 | 2 | 2 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 261 |
|  | 60 | 79 | 88 | 92 | 95 | 97 | 97 | 98 | 99 | 99 | 99 | 82 | 83 | 83 | 67 | 67 | 50 | 17 | 17 | 17 | 17 | 17 | 17 | 0 | 0 | 0 |
| ENE | 132 | 42 | 18 | 8 | 4 | 4 | 2 | 2 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 213 |
|  | 62 | 82 | 90 | 94 | 95 | 97 | 98 | 98 | 82 | 83 | 66 | 66 | 33 | 33 | 33 | 33 | 17 | 17 | 17 | 17 | 17 | 17 | 17 | 17 | 17 | 0 |
| E | 116 | 32 | 15 | 5 | 3 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 173 |
|  | 67 | 85 | 94 | 97 | 98 | 83 | 83 | 83 | 50 | 33 | 33 | 17 | 17 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| ESE | 107 | 24 | 7 | 3 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 145 |
|  | 73 | 90 | 95 | 97 | 99 | 83 | 17 | 17 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| SE | 121 | 33 | 12 | 4 | 3 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 175 |
|  | 69 | 88 | 95 | 97 | 99 | 83 | 66 | 66 | 33 | 33 | 33 | 17 | 17 | 17 | 17 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| SSE | 133 | 48 | 27 | 14 | 9 | 6 | 5 | 3 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 249 |
|  | 54 | 73 | 84 | 89 | 93 | 95 | 97 | 99 | 99 | 100 | 100 | 67 | 50 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |


| SECTOR | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | Direction Persistence (Hours)/Percent |  |  |  |  |  |  | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  | 9 | 10 | 11 | 12 | 13 | 14 | 15 |  |  |  |  |  |  |  |  |  |  |  |
| N | 150 | 65 | 34 | 18 | 11 | 7 | 4 | 4 | 2 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 298 |
|  | 50 | 72 | 84 | 90 | 93 | 96 | 97 | 98 | 99 | 83 | 83 | 66 | 66 | 67 | 50 | 33 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| NNE | 181 | 66 | 32 | 14 | 8 | 4 | 3 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 311 |
|  | 58 | 80 | 90 | 94 | 97 | 98 | 99 | 99 | 83 | 66 | 50 | 50 | 50 | 33 | 17 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| NE | 155 | 50 | 23 | 11 | 8 | 5 | 2 | 2 | 2 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 261 |
|  | 60 | 79 | 88 | 92 | 95 | 97 | 97 | 98 | 99 | 99 | 99 | 82 | 83 | 83 | 67 | 67 | 50 | 17 | 17 | 17 | 17 | 17 | 17 | 0 | 0 | 0 |
| ENE | 132 | 42 | 18 | 8 | 4 | 4 | 2 | 2 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 213 |
|  | 62 | 82 | 90 | 94 | 95 | 97 | 98 | 98 | 82 | 83 | 66 | 66 | 33 | 33 | 33 | 33 | 17 | 17 | 17 | 17 | 17 | 17 | 17 | 17 | 17 | 0 |
| E | 116 | 32 | 15 | 5 | 3 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 173 |
|  | 67 | 85 | 94 | 97 | 98 | 83 | 83 | 83 | 50 | 33 | 33 | 17 | 17 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| ESE | 107 | 24 | 7 | 3 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 145 |
|  | 73 | 90 | 95 | 97 | 99 | 83 | 17 | 17 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| SE | 121 | 33 | 12 | 4 | 3 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 175 |
|  | 69 | 88 | 95 | 97 | 99 | 83 | 66 | 66 | 33 | 33 | 33 | 17 | 17 | 17 | 17 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| SSE | 133 | 48 | 27 | 14 | 9 | 6 | 5 | 3 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 249 |
|  | 54 | 73 | 84 | 89 | 93 | 95 | 97 | 99 | 99 | 100 | 100 | 67 | 50 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

$\begin{array}{lcccccccccccccccccccccccccccccccccccc}\text { E } & 116 & 32 & 15 & 5 & 3 & 2 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 173 \\ & 67 & 85 & 94 & 97 & 98 & 83 & 83 & 83 & 50 & 33 & 33 & 17 & 17 & 17 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0\end{array}$
$\begin{array}{lccccccccccccccccccccccccccccccccccccc}\text { ESE } & 107 & 24 & 7 & 3 & 3 & 2 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 145 \\ & 73 & 90 & 95 & 97 & 99 & 83 & 17 & 17 & 17 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0\end{array}$
$\begin{array}{llllllllllllllllllllllllllllllllll}\text { SE } & 121 & 33 & 12 & 4 & 3 & 1 & 1 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 175 \\ & 69 & 88 & 95 & 97 & 99 & 83 & 66 & 66 & 33 & 33 & 33 & 17 & 17 & 17 & 17 & 17 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0\end{array}$

s ^^əy
Table 2.3-48—\{CCNPP 33 Feet Average Wind Direction Persistence Summary for Years 2000-2005\}
(Page 2 of 2)

| SECTOR | Direction Persistence (Hours)/Percent |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
|  | 60 | 80 | 90 | 95 | 98 | 99 | 100 | 100 | 83 | 50 | 50 | 50 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| SSW | 225 | 79 | 42 | 21 | 12 | 7 | 3 | 3 | 3 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 395 |
|  | 57 | 77 | 87 | 93 | 96 | 97 | 98 | 99 | 99 | 100 | 100 | 83 | 50 | 17 | 17 | 17 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| SW | 242 | 90 | 45 | 25 | 20 | 11 | 9 | 6 | 6 | 5 | 3 | 2 | 1 | 1 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 469 |
|  | 52 | 71 | 81 | 86 | 90 | 92 | 94 | 96 | 97 | 98 | 99 | 99 | 99 | 99 | 100 | 100 | 83 | 83 | 83 | 83 | 17 | 17 | 17 | 17 | 17 | 0 |
| WSW | 226 | 69 | 31 | 15 | 8 | 5 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 356 |
|  | 64 | 83 | 92 | 96 | 98 | 99 | 99 | 83 | 83 | 50 | 33 | 33 | 17 | 17 | 17 | 17 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| W | 192 | 51 | 20 | 7 | 4 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 277 |
|  | 69 | 88 | 95 | 98 | 99 | 83 | 83 | 67 | 50 | 17 | 17 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| WNW | 189 | 59 | 22 | 11 | 6 | 4 | 1 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 296 |
|  | 64 | 84 | 91 | 95 | 97 | 98 | 99 | 99 | 100 | 83 | 50 | 50 | 50 | 50 | 33 | 33 | 33 | 33 | 17 | 17 | 17 | 0 | 0 | 0 | 0 | 0 |
| NW | 175 | 64 | 32 | 19 | 10 | 6 | 3 | 3 | 2 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 316 |
|  | 55 | 76 | 86 | 91 | 95 | 96 | 98 | 98 | 99 | 99 | 83 | 83 | 66 | 66 | 50 | 33 | 17 | 17 | 17 | 17 | 17 | 17 | 17 | 17 | 17 | 0 |
| NNW | 154 | 47 | 19 | 11 | 5 | 2 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 242 |
|  | 64 | 83 | 91 | 95 | 97 | 98 | 99 | 99 | 83 | 50 | 33 | 33 | 17 | 17 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL | 2675 | 877 | 406 | 200 | 119 | 71 | 37 | 30 | 20 | 13 | 8 | 6 | 3 | 3 | 1 | 2 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 4474 |

Direction Persistence (Hours)/Percent

| $\begin{gathered} \underset{\lambda}{\lambda} \\ \underset{0}{0} \\ \underset{\sim}{c} \\ \underset{\omega}{\omega} \end{gathered}$ | Table 2.3-49—\{CCNPP 197 Feet Wind Direction Persistence Summary for Year 2000\} <br> (Page 1 of 2) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SECTOR | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | Direction Persistence (Hours)/Percent |  |  |  |  |  |  | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
|  |  |  |  |  |  |  |  |  |  |  | 10 | 11 | 12 | 13 | 14 | 15 | 16 |  |  |  |  |  |  |  |  |  |  |
|  | $N$ | 146 | 60 | 37 | 19 | 12 | 17 | 2 | 3 | 1 | 3 | 2 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 305 |
|  |  | 48 | 68 | 80 | 86 | 90 | 95 | 96 | 97 | 97 | 98 | 99 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | NNE | 165 | 70 | 22 | 18 | 13 | 3 | 4 | 3 | 2 | 3 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 305 |
|  |  | 54 | 77 | 84 | 90 | 94 | 95 | 97 | 98 | 98 | 99 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | NE | 141 | 53 | 25 | 8 | 4 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 237 |
|  |  | 59 | 82 | 92 | 96 | 97 | 98 | 98 | 98 | 98 | 99 | 99 | 99 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | ENE | 115 | 42 | 15 | 12 | 2 | 5 | 3 | 3 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 199 |
|  |  | 58 | 79 | 86 | 92 | 93 | 96 | 97 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | E | 103 | 30 | 9 | 5 | 2 | 4 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 157 |
|  |  | 66 | 85 | 90 | 94 | 95 | 97 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | ESE | 77 | 21 | 9 | 1 | 1 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 112 |
|  |  | 69 | 88 | 96 | 96 | 97 | 98 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | SE | 96 | 29 | 21 | 5 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 154 |
|  |  | 62 | 81 | 95 | 98 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | SSE | 112 | 35 | 28 | 19 | 4 | 11 | 5 | 2 | 3 | 1 | 1 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 224 |
|  |  | 50 | 66 | 78 | 87 | 88 | 93 | 96 | 96 | 98 | 98 | 99 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\begin{aligned} & \text { R } \\ & \stackrel{0}{2} \\ & i \end{aligned}$ | S | 154 | 41 | 28 | 16 | 7 | 6 | 2 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 258 |


Table 2.3-50—\{CCNPP 197 Feet Wind Direction Persistence Summary for Year 2001\}
(Page 1 of 2)

| SECTOR | Direction Persistence (Hours)/Percent |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
| N | 133 | 62 | 39 | 18 | 16 | 6 | 6 | 1 | 2 | 2 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 286 |
|  | 47 | 68 | 82 | 88 | 94 | 96 | 98 | 98 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| NNE | 149 | 52 | 29 | 17 | 9 | 6 | 4 | 4 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 271 |
|  | 55 | 74 | 85 | 91 | 94 | 97 | 98 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| NE | 136 | 34 | 20 | 9 | 4 | 3 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 210 |
|  | 65 | 81 | 90 | 95 | 97 | 98 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| ENE | 122 | 32 | 17 | 7 | 1 | 4 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 185 |
|  | 66 | 83 | 92 | 96 | 97 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| E | 125 | 44 | 16 | 5 | 2 | 2 | 1 | 1 | 0 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 200 |
|  | 63 | 85 | 93 | 95 | 96 | 97 | 98 | 98 | 98 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| ESE | 93 | 32 | 14 | 3 | 6 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 151 |
|  | 62 | 83 | 92 | 94 | 98 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| SE | 119 | 33 | 11 | 8 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 173 |
|  | 69 | 88 | 94 | 99 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| SSE | 118 | 43 | 35 | 27 | 15 | 6 | 5 | 5 | 1 | 1 | 1 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 261 |
|  | 45 | 62 | 75 | 85 | 91 | 93 | 95 | 97 | 98 | 98 | 98 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 |  |
| S | 176 | 51 | 33 | 19 | 9 | 12 | 4 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 308 |



SE $\begin{array}{rlcccccccccccccccccccccccccccc}119 & 33 & 11 & 8 & 1 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ & 69 & 88 & 94 & 99 & 99 & 99 & 99 & 100 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0\end{array}$

-^əу
S 1
Table 2．3－50—\｛CCNPP 197 Feet Wind Direction Persistence Summary for Year 2001\}
（Page 2 of 2）

| SECTOR | Direction Persistence（Hours）／Percent |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT． 24 | TOTAL |
|  | 57 | 74 | 84 | 91 | 94 | 97 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| SSW | 174 | 72 | 43 | 35 | 17 | 13 | 5 | 3 | 4 | 3 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 372 |
|  | 47 | 66 | 78 | 87 | 92 | 95 | 97 | 97 | 98 | 99 | 99 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| SW | 165 | 73 | 37 | 25 | 25 | 10 | 2 | 6 | 1 | 3 | 3 | 3 | 2 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 357 |
|  | 46 | 67 | 77 | 84 | 91 | 94 | 94 | 96 | 96 | 97 | 98 | 99 | 99 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| WSW | 155 | 64 | 34 | 7 | 10 | 3 | 3 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 279 |
|  | 56 | 78 | 91 | 93 | 97 | 98 | 99 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| W | 123 | 49 | 23 | 7 | 2 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 208 |
|  | 59 | 83 | 94 | 97 | 98 | 98 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| WNW | 139 | 39 | 23 | 10 | 2 | 7 | 0 | 2 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 225 |
|  | 62 | 79 | 89 | 94 | 95 | 98 | 98 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| NW | 178 | 55 | 32 | 18 | 13 | 8 | 6 | 2 | 0 | 4 | 2 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 323 |
|  | 55 | 72 | 82 | 88 | 92 | 94 | 96 | 97 | 97 | 98 | 98 | 99 | 99 | 99 | 99 | 99 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| NNW | 136 | 64 | 18 | 24 | 9 | 8 | 12 | 5 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 281 |
|  | 48 | 71 | 78 | 86 | 89 | 92 | 96 | 98 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| TOTAL | 2241 | 799 | 424 | 239 | 141 | 90 | 52 | 40 | 12 | 21 | 7 | 9 | 2 | 4 | 4 | 1 | 1 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 4090 |


| $\begin{gathered} \underset{\lambda}{\lambda} \\ \underset{0}{0} \\ \stackrel{c}{c} \\ \underset{\omega}{\omega} \end{gathered}$ | Table 2.3-51—\{CCNPP 197 Feet Wind Direction Persistence Summary for Year 2002\} <br> (Page 1 of 2) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SECTOR | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | Direction Persistence (Hours)/Percent |  |  |  |  |  |  | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |  | TOTAL |
|  |  |  |  |  |  |  |  |  |  |  | 10 | 11 | 12 | 13 | 14 | 15 | 16 |  |  |  |  |  |  |  |  |  |  |
|  | N | 125 | 61 | 42 | 30 | 14 | 7 | 5 | 1 | 4 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 292 |
|  |  | 43 | 64 | 78 | 88 | 93 | 96 | 97 | 98 | 99 | 99 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | NNE | 149 | 62 | 30 | 18 | 13 | 11 | 5 | 3 | 5 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 299 |
|  |  | 50 | 71 | 81 | 87 | 91 | 95 | 96 | 97 | 99 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | NE | 139 | 51 | 20 | 6 | 5 | 2 | 1 | 1 | 1 | 1 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 231 |
|  |  | 60 | 82 | 91 | 94 | 96 | 97 | 97 | 97 | 98 | 98 | 98 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 |  |
|  | ENE | 124 | 24 | 13 | 5 | 4 | 2 | 2 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 177 |
|  |  | 70 | 84 | 91 | 94 | 96 | 97 | 98 | 99 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | E | 81 | 34 | 13 | 4 | 2 | 1 | 2 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 139 |
|  |  | 58 | 83 | 92 | 95 | 96 | 97 | 99 | 99 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | ESE | 86 | 28 | 13 | 3 | 1 | 2 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 135 |
|  |  | 64 | 84 | 94 | 96 | 97 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | SE | 101 | 36 | 11 | 10 | 1 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 162 |
|  |  | 62 | 85 | 91 | 98 | 98 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | SSE | 94 | 50 | 26 | 17 | 11 | 9 | 5 | 3 | 2 | 5 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 226 |
|  |  | 42 | 64 | 75 | 83 | 88 | 92 | 94 | 95 | 96 | 98 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\left.\begin{aligned} & \underset{N}{0} \\ & \stackrel{N}{i} \\ & i \end{aligned} \right\rvert\,$ | S | 126 | 57 | 39 | 21 | 10 | 9 | 1 | 3 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 269 |

Table 2.3-51—\{CCNPP 197 Feet Wind Direction Persistence Summary for Year 2002\}
(Page 2 of 2)
Direction Persistence (Hours)/Percent

| SECTOR | Direction Persistence (Hours)/Percent |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
|  | 47 | 68 | 83 | 90 | 94 | 97 | 98 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| SSW | 153 | 78 | 53 | 26 | 15 | 8 | 5 | 1 | 5 | 2 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 349 |
|  | 44 | 66 | 81 | 89 | 93 | 95 | 97 | 97 | 99 | 99 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| SW | 163 | 60 | 34 | 36 | 16 | 4 | 5 | 7 | 5 | 5 | 4 | 3 | 2 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 348 |
|  | 47 | 64 | 74 | 84 | 89 | 90 | 91 | 93 | 95 | 96 | 97 | 98 | 99 | 99 | 99 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |  |
| WSW | 164 | 52 | 16 | 9 | 11 | 7 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 263 |
|  | 62 | 82 | 88 | 92 | 96 | 98 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| W | 126 | 33 | 22 | 11 | 2 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 197 |
|  | 64 | 81 | 92 | 97 | 98 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |


| WNW | 147 | 50 | 18 | 15 | 12 | 4 | 3 | 1 | 1 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 25 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 58 | 78 | 85 | 91 | 95 | 97 | 98 | 98 | 99 | 99 | 99 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |


| NW | 145 | 57 | 30 | 14 | 13 | 7 | 7 | 1 | 1 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 280 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 52 | 72 | 83 | 88 | 93 | 95 | 98 | 98 | 98 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |


| NNW | 114 | 50 | 36 | 18 | 18 | 7 | 7 | 0 | 6 | 1 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 260 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 44 | 63 | 77 | 84 | 91 | 93 | 96 | 96 | 98 | 99 | 99 | 99 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |


Table 2.3-52—\{CCNPP 197 Feet Wind Direction Persistence Summary for Year 2003\}
Direction Persistence (Hours)/Percent

|  |  |  |  |  |  |  |  |  |  | irect | n P | iste | (H) | urs)/ | ercen |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SECTOR | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| N | 124 | 61 | 39 | 15 | 13 | 13 | 8 | 8 | 2 | 1 | 3 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 290 |
|  | 43 | 64 | 77 | 82 | 87 | 91 | 94 | 97 | 98 | 98 | 99 | 99 | 99 | 99 | 99 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| NNE | 161 | 65 | 36 | 20 | 4 | 8 | 2 | 1 | 1 | 3 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 305 |
|  | 53 | 74 | 86 | 92 | 94 | 96 | 97 | 97 | 98 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| NE | 137 | 50 | 22 | 8 | 5 | 3 | 3 | 3 | 1 | 4 | 2 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 242 |
|  | 57 | 77 | 86 | 90 | 92 | 93 | 94 | 95 | 96 | 98 | 98 | 99 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| ENE | 138 | 34 | 12 | 4 | 4 | 1 | 6 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 202 |
|  | 68 | 85 | 91 | 93 | 95 | 96 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| E | 99 | 26 | 14 | 13 | 0 | 2 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 156 |
|  | 63 | 80 | 89 | 97 | 97 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| ESE | 99 | 30 | 14 | 1 | 2 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 149 |
|  | 66 | 87 | 96 | 97 | 98 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| SE | 134 | 42 | 14 | 10 | 3 | 3 | 2 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 209 |
|  | 64 | 84 | 91 | 96 | 97 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| SSE | 124 | 56 | 37 | 15 | 16 | 5 | 5 | 5 | 1 | 3 | 3 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 271 |
|  | 46 | 66 | 80 | 86 | 92 | 93 | 95 | 97 | 97 | 99 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| S | 162 | 54 | 32 | 21 | 12 | 8 | 1 | 1 | 3 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 295 |


|  |  |  |  |  |  |  |  |  |  | irect | n P | iste | (H) | urs)/ | ercen |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SECTOR | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| N | 124 | 61 | 39 | 15 | 13 | 13 | 8 | 8 | 2 | 1 | 3 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 290 |
|  | 43 | 64 | 77 | 82 | 87 | 91 | 94 | 97 | 98 | 98 | 99 | 99 | 99 | 99 | 99 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| NNE | 161 | 65 | 36 | 20 | 4 | 8 | 2 | 1 | 1 | 3 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 305 |
|  | 53 | 74 | 86 | 92 | 94 | 96 | 97 | 97 | 98 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| NE | 137 | 50 | 22 | 8 | 5 | 3 | 3 | 3 | 1 | 4 | 2 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 242 |
|  | 57 | 77 | 86 | 90 | 92 | 93 | 94 | 95 | 96 | 98 | 98 | 99 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| ENE | 138 | 34 | 12 | 4 | 4 | 1 | 6 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 202 |
|  | 68 | 85 | 91 | 93 | 95 | 96 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| E | 99 | 26 | 14 | 13 | 0 | 2 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 156 |
|  | 63 | 80 | 89 | 97 | 97 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| ESE | 99 | 30 | 14 | 1 | 2 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 149 |
|  | 66 | 87 | 96 | 97 | 98 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| SE | 134 | 42 | 14 | 10 | 3 | 3 | 2 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 209 |
|  | 64 | 84 | 91 | 96 | 97 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| SSE | 124 | 56 | 37 | 15 | 16 | 5 | 5 | 5 | 1 | 3 | 3 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 271 |
|  | 46 | 66 | 80 | 86 | 92 | 93 | 95 | 97 | 97 | 99 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| S | 162 | 54 | 32 | 21 | 12 | 8 | 1 | 1 | 3 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 295 |



$\begin{array}{llllllcccccccccccccccccccccccccc}\text { SSE } & 124 & 56 & 37 & 15 & 16 & 5 & 5 & 5 & 1 & 3 & 3 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 271 \\ & 46 & 66 & 80 & 86 & 92 & 93 & 95 & 97 & 97 & 99 & 100 & 100 & 100 & 100 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & \end{array}$

## (Page 1 of 2)

| $\begin{gathered} \underset{\sim}{\lambda} \\ \underset{0}{0} \\ 0 \\ \stackrel{\rightharpoonup}{7} \\ \omega \end{gathered}$ | Table 2.3-52—\{CCNPP 197 Feet Wind Direction Persistence Summary for Year 2003\} <br> (Page 2 of 2) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SECTOR | 1 | $\frac{2}{73}$ | $\begin{gathered} \mathbf{3} \\ \hline 84 \end{gathered}$ | $\frac{4}{91}$ | $\frac{5}{95}$ | $\begin{gathered} 6 \\ \hline 98 \end{gathered}$ | $\begin{gathered} 7 \\ \hline 98 \end{gathered}$ | $\begin{gathered} \mathbf{8} \\ \hline 99 \end{gathered}$ | $\frac{9}{100}$ | $\begin{array}{r} \hline \text { Direc } \\ \mathbf{1 0} \\ \hline 100 \end{array}$ | on Pe <br> 11 <br> 100 | sisten12100 | (H) <br> 13 <br> 100 | urs)/P <br> $\mathbf{1 4}$ <br> 100 | $\begin{aligned} & \text { rent } \\ & \hline 15 \\ & \hline 0 \end{aligned}$ | $\frac{16}{0}$ | $\frac{17}{0}$ | $\frac{18}{0}$ | $\frac{19}{0}$ | $\frac{20}{0}$ | $\frac{21}{0}$ | $\frac{22}{0}$ | $\frac{23}{0}$ |  |  | TOTAL |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\frac{\mathbf{2 4}}{0}$ | $\frac{\text { GT. } 24}{0}$ |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | SSW | 159 | 58 | 28 | 21 | 9 | 11 | 7 | 2 | 4 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 302 |
|  |  | 53 | 72 | 81 | 88 | 91 | 95 | 97 | 98 | 99 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | SW | 177 | 75 | 22 | 26 | 6 | 7 | 7 | 9 | 3 | 3 | 2 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 340 |
|  |  | 52 | 74 | 81 | 88 | 90 | 92 | 94 | 97 | 98 | 99 | 99 | 99 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | WSW | 146 | 48 | 23 | 12 | 4 | 3 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 239 |
|  |  | 61 | 81 | 91 | 96 | 97 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | W | 141 | 47 | 22 | 6 | 5 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 223 |
|  |  | 63 | 84 | 94 | 97 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | WNW | 145 | 65 | 22 | 17 | 4 | 4 | 2 | 0 | 4 | 0 | 1 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 267 |
|  |  | 54 | 79 | 87 | 93 | 95 | 96 | 97 | 97 | 99 | 99 | 99 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | NW | 138 | 62 | 39 | 17 | 7 | 14 | 2 | 1 | 3 | 2 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 290 |
|  |  | 48 | 69 | 82 | 88 | 91 | 96 | 96 | 97 | 98 | 98 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | NNW | 122 | 58 | 20 | 14 | 8 | 6 | 6 | 1 | 2 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 240 |
|  |  | 51 | 75 | 83 | 89 | 93 | 95 | 98 | 98 | 99 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | TOTAL | 2206 | 831 | 396 | 220 | 102 | 91 | 56 | 32 | 26 | 18 | 16 | 8 | 4 | 5 | 2 | 2 | 1 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 4020 |


| $\begin{gathered} \underset{\lambda}{\lambda} \\ \underset{0}{0} \\ \stackrel{c}{c} \\ \underset{\omega}{\omega} \end{gathered}$ | Table 2.3-53—\{CCNPP 197 Feet Wind Direction Persistence Summary for Year 2004\} <br> (Page 1 of 2) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SECTOR | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |  | 11 | $12$ | 13 | Hours |  | ent16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | N | 145 | 49 | 37 | 21 | 23 | 10 | 6 | 5 | 2 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 301 |
|  |  | 48 | 64 | 77 | 84 | 91 | 95 | 97 | 98 | 99 | 99 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | NNE | 156 | 59 | 21 | 14 | 12 | 4 | 7 | 3 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 284 |
|  |  | 55 | 76 | 83 | 88 | 92 | 94 | 96 | 97 | 98 | 98 | 98 | 99 | 99 | 99 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 0 | 0 |  |
|  | NE | 133 | 44 | 23 | 16 | 3 | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 223 |
|  |  | 60 | 79 | 90 | 97 | 98 | 98 | 99 | 99 | 99 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 |  |
|  | ENE | 129 | 37 | 17 | 11 | 5 | 4 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 205 |
|  |  | 63 | 81 | 89 | 95 | 97 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | E | 115 | 30 | 9 | 12 | 3 | 1 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 173 |
|  |  | 66 | 84 | 89 | 96 | 98 | 98 | 98 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | ESE | 111 | 30 | 10 | 5 | 4 | 2 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 165 |
|  |  | 67 | 85 | 92 | 95 | 97 | 98 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | SE | 134 | 36 | 18 | 8 | 6 | 2 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 208 |
|  |  | 64 | 82 | 90 | 94 | 97 | 98 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | SSE | 131 | 46 | 36 | 20 | 9 | 7 | 6 | 1 | 3 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 263 |
|  |  | 50 | 67 | 81 | 89 | 92 | 95 | 97 | 97 | 98 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 0 |  |
| $\left.\begin{aligned} & \underset{N}{0} \\ & \stackrel{N}{i} \\ & i \end{aligned} \right\rvert\,$ | S | 159 | 62 | 35 | 11 | 14 | 8 | 2 | 3 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 297 |


Table 2.3-54—\{CCNPP 197 Feet Wind Direction Persistence Summary for Year 2005\}
(Page 1 of 2)

## Direction Persistence (Hours)/Percent

| Direction Persistence (Hours)/Percent |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SECTOR | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
| N | 134 | 69 | 43 | 19 | 17 | 7 | 13 | 2 | 1 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 310 |
|  | 43 | 65 | 79 | 85 | 91 | 93 | 97 | 98 | 98 | 98 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 |  |
| NNE | 158 | 66 | 33 | 19 | 13 | 13 | 4 | 4 | 1 | 2 | 1 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 318 |
|  | 50 | 70 | 81 | 87 | 91 | 95 | 96 | 97 | 98 | 98 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| NE | 147 | 46 | 17 | 11 | 4 | 6 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 235 |
|  | 63 | 82 | 89 | 94 | 96 | 98 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| ENE | 131 | 56 | 10 | 7 | 2 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 211 |
|  | 62 | 89 | 93 | 97 | 98 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| E | 129 | 38 | 14 | 12 | 7 | 5 | 3 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 209 |
|  | 62 | 80 | 87 | 92 | 96 | 98 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |


| SECTOR | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | Direction Persistence (Hours)/Percent |  |  |  |  |  |  | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  | 10 | 11 | 12 | 13 | 14 | 15 | 16 |  |  |  |  |  |  |  |  |  |  |
| N | 134 | 69 | 43 | 19 | 17 | 7 | 13 | 2 | 1 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 310 |
|  | 43 | 65 | 79 | 85 | 91 | 93 | 97 | 98 | 98 | 98 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 |  |
| NNE | 158 | 66 | 33 | 19 | 13 | 13 | 4 | 4 | 1 | 2 | 1 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 318 |
|  | 50 | 70 | 81 | 87 | 91 | 95 | 96 | 97 | 98 | 98 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| NE | 147 | 46 | 17 | 11 | 4 | 6 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 235 |
|  | 63 | 82 | 89 | 94 | 96 | 98 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| ENE | 131 | 56 | 10 | 7 | 2 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 211 |
|  | 62 | 89 | 93 | 97 | 98 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| E | 129 | 38 | 14 | 12 | 7 | 5 | 3 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 209 |
|  | 62 | 80 | 87 | 92 | 96 | 98 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |


|  |
| :---: |


| ESE | 115 | 39 | 14 | 3 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 65 | 88 | 95 | 97 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |


| SE | 143 | 48 | 19 | 7 | 3 | 0 | 0 | 1 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 225 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 64 | 85 | 93 | 96 | 98 | 98 | 98 | 98 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |


| SSE | 143 | 59 | 35 | 15 | 14 | 7 | 5 | 2 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 284 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 50 | 71 | 83 | 89 | 94 | 96 | 98 | 99 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |  |


| s | 154 | 45 | 29 | 16 | 11 | 10 | 3 | 4 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 275 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| $\left.\begin{gathered} \underset{\sim}{\hat{2}} \\ \underset{0}{0} \\ 0 \\ \stackrel{\rightharpoonup}{7} \\ \omega \end{gathered} \right\rvert\,$ | Table 2.3-54—\{CCNPP 197 Feet Wind Direction Persistence Summary for Year 2005\} <br> (Page 2 of 2) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SECTOR | $\frac{\mathbf{1}}{56}$ | $\frac{\mathbf{2}}{72}$ | $\begin{gathered} \mathbf{3} \\ \hline 83 \end{gathered}$ | $\begin{gathered} 4 \\ \hline 89 \end{gathered}$ | $\begin{gathered} 5 \\ \hline 93 \end{gathered}$ | $\frac{6}{96}$ | $\begin{gathered} 7 \\ \hline 97 \end{gathered}$ | $\begin{gathered} 8 \\ \hline 99 \end{gathered}$ | $\begin{gathered} 9 \\ \hline 99 \end{gathered}$ | $\begin{gathered} \text { Dire } \\ \mathbf{1 0} \\ \hline 100 \end{gathered}$ | ction <br> 11 <br> 100 | Persis12100 | ence13100 | Hours <br> 14 <br> 0 | $\begin{gathered} \hline \text { JPerc } \\ 15 \\ \hline 0 \end{gathered}$ | $\begin{aligned} & \text { ent } \\ & \mathbf{1 6} \\ & \hline 0 \end{aligned}$ | $\frac{17}{0}$ | $\frac{18}{0}$ | $\frac{19}{0}$ | $\frac{20}{0}$ | $\begin{gathered} 21 \\ \hline 0 \end{gathered}$ | $\frac{22}{0}$ | 23 | $\frac{\mathbf{2 4}}{0}$ | $\begin{gathered} \text { GT. } 24 \\ \hline 0 \end{gathered}$ | TOTAL |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | SSW | 152 | 65 | 38 | 18 | 12 | 7 | 3 | 2 | 1 | 2 | 0 | 0 | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 304 |
|  |  | 50 | 71 | 84 | 90 | 94 | 96 | 97 | 98 | 98 | 99 | 99 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | SW | 167 | 64 | 34 | 15 | 15 | 8 | 5 | 3 | 3 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 317 |
|  |  | 53 | 73 | 84 | 88 | 93 | 96 | 97 | 98 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | WSW | 152 | 46 | 31 | 15 | 12 | 2 | 2 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 263 |
|  |  | 58 | 75 | 87 | 93 | 97 | 98 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | W | 133 | 48 | 19 | 6 | 0 | 4 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 212 |
|  |  | 63 | 85 | 94 | 97 | 97 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | WNW | 182 | 45 | 16 | 10 | 9 | 3 | 3 | 1 | 2 | 1 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 277 |
|  |  | 66 | 82 | 88 | 91 | 95 | 96 | 97 | 97 | 98 | 98 | 98 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 100 |  |
|  | NW | 161 | 50 | 30 | 19 | 11 | 5 | 5 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 285 |
|  |  | 56 | 74 | 85 | 91 | 95 | 97 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | NNW | 144 | 40 | 24 | 12 | 11 | 5 | 2 | 4 | 2 | 1 | 4 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 250 |
|  |  | 58 | 74 | 83 | 88 | 92 | 94 | 95 | 97 | 98 | 98 | 100 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | TOTAL | 2345 | 824 | 406 | 204 | 145 | 85 | 53 | 30 | 16 | 12 | 9 | 5 | 4 | 2 | 4 | 1 | 2 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 2 | 4151 |


| $\begin{gathered} \underset{\lambda}{\lambda} \\ \underset{0}{0} \\ \stackrel{c}{c} \\ \underset{\omega}{\omega} \end{gathered}$ | Table 2.3-55—\{CCNPP 197 Feet Average Wind Direction Persistence Summary for Years 2000-2005\} <br> (Page 1 of 2 ) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SECTOR | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | Direction Persistence (Hours)/Percent |  |  |  |  |  |  | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
|  |  |  |  |  |  |  |  |  |  | 9 | 10 | 11 | 12 | 13 | 14 | 15 |  |  |  |  |  |  |  |  |  |  |  |
|  | N | 135 | 60 | 40 | 20 | 16 | 10 | 7 | 3 | 2 | 1 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 297 |
|  |  | 45 | 66 | 79 | 86 | 91 | 94 | 97 | 98 | 98 | 99 | 99 | 100 | 100 | 83 | 50 | 33 | 33 | 33 | 33 | 17 | 17 | 0 | 0 | 0 | 0 | 0 |
|  | NNE | 156 | 62 | 29 | 18 | 11 | 8 | 4 | 3 | 2 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 297 |
|  |  | 53 | 74 | 83 | 89 | 93 | 95 | 97 | 98 | 99 | 99 | 83 | 83 | 67 | 50 | 50 | 33 | 33 | 33 | 33 | 17 | 17 | 17 | 17 | 0 | 0 | 0 |
|  | NE | 139 | 46 | 21 | 10 | 4 | 3 | 2 | 1 | 0 | 1 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 230 |
|  |  | 61 | 81 | 90 | 94 | 96 | 97 | 98 | 98 | 82 | 82 | 82 | 83 | 83 | 83 | 67 | 67 | 50 | 50 | 50 | 33 | 17 | 17 | 0 | 0 | 0 | 0 |
|  | ENE | 127 | 38 | 14 | 8 | 3 | 3 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 197 |
|  |  | 65 | 84 | 90 | 95 | 96 | 98 | 99 | 100 | 83 | 83 | 83 | 67 | 33 | 33 | 17 | 17 | 17 | 17 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | E | 109 | 34 | 13 | 9 | 3 | 3 | 2 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 172 |
|  |  | 63 | 83 | 90 | 95 | 96 | 98 | 99 | 99 | 83 | 66 | 33 | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | ESE | 97 | 30 | 12 | 3 | 3 | 2 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 148 |
|  |  | 66 | 86 | 94 | 96 | 98 | 99 | 83 | 66 | 50 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | SE | 121 | 37 | 16 | 8 | 3 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 189 |
|  |  | 64 | 84 | 92 | 97 | 98 | 99 | 99 | 100 | 50 | 33 | 33 | 33 | 17 | 17 | 17 | 17 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | SSE | 120 | 48 | 33 | 19 | 12 | 8 | 5 | 3 | 2 | 2 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 255 |
|  |  | 47 | 66 | 79 | 87 | 91 | 94 | 96 | 97 | 98 | 99 | 99 | 100 | 83 | 83 | 67 | 67 | 50 | 50 | 50 | 50 | 50 | 33 | 33 | 33 | 17 | 0 |
| $\left.\begin{aligned} & 刀_{0}^{0} \\ & \stackrel{i}{i} \end{aligned} \right\rvert\,$ | S | 155 | 52 | 33 | 17 | 11 | 9 | 2 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 284 |


| (1) |  |
| :---: | :---: |

Table 2.3-55—\{CCNPP 197 Feet Average Wind Direction Persistence Summary for Years 2000-2005\}

| SECTOR | Direction Persistence (Hours)/Percent |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
|  | 55 | 73 | 84 | 91 | 94 | 97 | 98 | 99 | 100 | 100 | 67 | 50 | 50 | 33 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| SSW | 167 | 69 | 41 | 24 | 13 | 9 | 5 | 4 | 3 | 2 | 0 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 341 |
|  | 49 | 70 | 82 | 89 | 93 | 95 | 97 | 98 | 99 | 99 | 99 | 100 | 83 | 67 | 50 | 17 | 17 | 17 | 17 | 17 | 0 | 0 | 0 | 0 | 0 | 0 |
| SW | 170 | 72 | 34 | 23 | 14 | 8 | 6 | 6 | 4 | 3 | 2 | 2 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 347 |
|  | 49 | 70 | 80 | 86 | 90 | 93 | 94 | 96 | 97 | 98 | 99 | 99 | 83 | 83 | 83 | 66 | 67 | 50 | 33 | 33 | 33 | 17 | 17 | 17 | 17 | 0 |
| WSW | 155 | 51 | 26 | 12 | 9 | 4 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 261 |
|  | 60 | 79 | 89 | 94 | 97 | 98 | 99 | 66 | 66 | 33 | 33 | 33 | 33 | 33 | 33 | 17 | 17 | 17 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| W | 134 | 44 | 21 | 7 | 3 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 213 |
|  | 63 | 84 | 94 | 97 | 98 | 99 | 100 | 67 | 33 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| WNW | 156 | 52 | 22 | 13 | 8 | 4 | 2 | 1 | 2 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 263 |
|  | 59 | 79 | 88 | 93 | 96 | 97 | 98 | 98 | 99 | 99 | 83 | 83 | 83 | 67 | 33 | 33 | 33 | 33 | 33 | 17 | 17 | 17 | 17 | 17 | 17 | 0 |
| NW | 156 | 55 | 33 | 18 | 12 | 8 | 5 | 3 | 2 | 2 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 296 |
|  | 52 | 71 | 82 | 89 | 93 | 95 | 97 | 98 | 98 | 99 | 99 | 83 | 83 | 66 | 50 | 50 | 50 | 33 | 33 | 17 | 17 | 17 | 17 | 17 | 17 | 0 |
| NNW | 135 | 54 | 25 | 17 | 11 | 7 | 6 | 2 | 3 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 263 |
|  | 51 | 72 | 82 | 88 | 92 | 94 | 96 | 97 | 98 | 99 | 100 | 83 | 67 | 33 | 33 | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL | 2231 | 805 | 412 | 225 | 133 | 86 | 51 | 34 | 23 | 17 | 11 | 8 | 5 | 3 | 2 | 2 | 2 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 1 | 4051 |

Table 2.3-56—\{CCNPP Monthly Mean Temperatures (2000-2005)\}

|  | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\circ} \mathrm{F}$ | 34.3 | 38.1 | 45.1 | 55.0 | 63.4 | 71.6 | 75.1 | 75.0 | 69.0 | 58.5 | 51.6 | 38.4 |
| ${ }^{\circ} \mathrm{C}$ | 1.3 | 3.4 | 7.3 | 12.8 | 17.4 | 22.0 | 23.9 | 23.9 | 20.6 | 14.7 | 10.9 | 3.6 |

Table 2.3-57—\{CCNPP Monthly Mean Extreme Maximum Temperatures (2000-2005)\}

|  | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\circ} \mathrm{F}$ | 40.9 | 41.6 | 52.0 | 57.1 | 69.4 | 72.8 | 78.3 | 77.5 | 72.1 | 60.4 | 59.5 | 45.0 |
| ${ }^{\circ} \mathrm{C}$ | 4.9 | 5.3 | 11.1 | 13.9 | 20.8 | 22.7 | 25.7 | 25.3 | 22.3 | 15.8 | 15.3 | 7.2 |

Table 2.3-58_\{CCNPP Monthly Mean Extreme Minimum Temperatures (2000-2005)\}

|  | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\circ} \mathrm{F}$ | 29.5 | 33.1 | 40.3 | 53.2 | 58.8 | 69.1 | 72.0 | 72.4 | 65.9 | 57.2 | 45.4 | 31.4 |
| ${ }^{\circ} \mathrm{C}$ | -1.4 | 0.6 | 4.6 | 11.8 | 14.9 | 20.6 | 22.2 | 22.4 | 18.8 | 14.0 | 7.4 | -0.3 |

Table 2.3-59— \{CCNPP Monthly Mean Daily Maximum Temperatures (2000-2005)\}

|  | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\circ} \mathrm{F}$ | 40.6 | 45.4 | 52.7 | 63.3 | 70.8 | 78.8 | 81.8 | 81.4 | 75.2 | 65.3 | 58.9 | 44.7 |
| ${ }^{\circ} \mathrm{C}$ | 4.8 | 7.4 | 11.5 | 17.4 | 21.6 | 26.0 | 27.7 | 27.4 | 24.0 | 18.5 | 14.9 | 7.1 |

Table 2.3-60—\{CCNPP Monthly Mean Daily Minimum Temperatures (2000-2005)\}

|  | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\circ} \mathrm{F}$ | 28.5 | 31.7 | 38.1 | 47.4 | 56.3 | 64.8 | 68.7 | 69.3 | 63.1 | 51.7 | 44.5 |
| ${ }^{\circ} \mathrm{C}$ | -1.9 | -0.2 | 3.4 | 8.6 | 13.5 | 18.2 | 20.4 | 20.7 | 17.3 | 10.9 | 6.9 |

Table 2.3-61—\{CCNPP Maximum Hourly Temperatures (2000-2005)\}

|  | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\circ} \mathrm{F}$ | 77.2 | 75.6 | 84.0 | 90.7 | 89.8 | 91.4 | 96.3 | 93.9 | 87.6 | 86.0 | 78.6 | 75.972 .9 |
| ${ }^{\circ} \mathrm{C}$ | 25.1 | 24.2 | 28.9 | 32.6 | 32.1 | 33.0 | 35.7 | 34.4 | 30.9 | 30.0 | 25.9 | 24.422 .7 |

Table 2.3-62— \{CCNPP Minimum Hourly Temperatures (2000-2005)\}

|  | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\circ} \mathrm{F}$ | 9.2 | 15.0 | 16.2 | 29.4 | 24.339 .9 | 51.8 | 55.6 | 55.0 | 43.3 | 32.7 | 22.0 | 8.5 |
| ${ }^{\circ} \mathrm{C}$ | -12.7 | -9.4 | -8.8 | -1.4 | -4.34 .4 | 11.0 | 13.1 | 12.8 | 6.3 | 0.4 | -5.6 | -13.1 |

Table 2.3-63—\{CCNPP Number of Hourly Temperature Values Greater Than or Less Than Indicated Value (2000-2005)\}

| Value | Number of Hours of Occurrence | Percent Frequency of Occurrence |
| :---: | :---: | :---: |
| $95.0^{\circ} \mathrm{F}$ | 3 | 0.006 |
| $90.0^{\circ} \mathrm{F}$ | 137 | 0.262 |
| $32.0^{\circ} \mathrm{F}$ | 5062 | 9.663 |
| $00.0^{\circ} \mathrm{F}$ | 0 | 0.000 |

Table 2.3-64-\{Monthly Mean Temperatures (1971-2000) at Sites Around CCNPP\}

Table 2.3-65-\{Monthly Mean Maximum Temperatures (1971-2000) at Sites Around CCNPP $\}$

| SITE |  | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC | ANNUAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Baltimore/Washington International Airport | ${ }^{\circ} \mathrm{F}$ | 41.2 | 44.8 | 53.9 | 64.5 | 73.9 | 82.7 | 87.2 | 85.1 | 78.2 | 67.0 | 56.3 | 46.0 | 65.1 |
|  | ${ }^{\circ} \mathrm{C}$ | 5.1 | 7.1 | 12.2 | 18.1 | 23.3 | 28.2 | 30.7 | 29.5 | 25.7 | 19.4 | 13.5 | 7.8 | 18.4 |
| Annapolis, MD | ${ }^{\circ} \mathrm{F}$ | 41.8 | 45.0 | 54.3 | 65.1 | 74.8 | 83.2 | 87.7 | 85.3 | 78.0 | 66.9 | 55.7 | 46.8 | 65.4 |
|  | ${ }^{\circ} \mathrm{C}$ | 5.4 | 7.2 | 12.4 | 18.4 | 23.8 | 28.4 | 30.9 | 29.6 | 25.6 | 19.4 | 13.2 | 8.2 | 18.6 |
| Cambridge, MD | ${ }^{\circ} \mathrm{F}$ | 45.0 | 48.6 | 57.0 | 67.7 | 76.9 | 85.3 | 89.4 | 87.3 | 81.1 | 70.5 | 60.2 | 50.1 | 68.3 |
|  | ${ }^{\circ} \mathrm{C}$ | 7.2 | 9.2 | 13.9 | 19.8 | 24.9 | 29.6 | 31.9 | 30.7 | 27.3 | 21.4 | 15.7 | 10.1 | 20.2 |
| Princess Anne, MD | ${ }^{\circ} \mathrm{F}$ | 46.6 | 49.1 | 57.6 | 67.5 | 76.2 | 84.0 | 88.4 | 86.4 | 81.0 | 70.6 | 60.3 | 51.0 | 68.2 |
|  | ${ }^{\circ} \mathrm{C}$ | 8.1 | 9.5 | 14.2 | 19.7 | 24.6 | 28.9 | 31.3 | 30.2 | 27.2 | 21.4 | 15.7 | 10.6 | 20.1 |
| Patuxent River NAS | ${ }^{\circ} \mathrm{F}$ | 43.9 | 46.5 | 54.8 | 64.8 | 73.6 | 81.5 | 86.1 | 84.8 | 78.8 | 68.3 | 58.5 | 48.7 | 65.9 |
|  | ${ }^{\circ} \mathrm{C}$ | 6.6 | 8.1 | 12.7 | 18.2 | 23.1 | 27.5 | 30.1 | 29.3 | 26.0 | 20.2 | 14.7 | 9.3 | 18.8 |
| Mechanicsville, MD | ${ }^{\circ} \mathrm{F}$ | 43.5 | 47.2 | 56.7 | 66.8 | 74.3 | 82.0 | 86.1 | 84.0 | 77.4 | 66.3 | 57.8 | 48.4 | 65.9 |
|  | ${ }^{\circ} \mathrm{C}$ | 6.4 | 8.4 | 13.7 | 19.3 | 23.5 | 27.8 | 30.1 | 28.9 | 25.2 | 19.1 | 14.3 | 9.1 | 18.8 |

Table 2.3-66-\{Monthly Mean Minimum Temperatures (1971-2000) at Sites Around CCNPP $\}$

| SITE |  | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC | ANNUAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Baltimore/Washington International Airport | ${ }^{\circ} \mathrm{F}$ | 23.5 | 26.1 | 33.6 | 42.0 | 51.8 | 60.8 | 65.8 | 63.9 | 56.6 | 43.7 | 34.7 | 27.3 | 44.2 |
|  | ${ }^{\circ} \mathrm{C}$ | -4.7 | -3.3 | 0.9 | 5.6 | 11.0 | 16.0 | 18.8 | 17.7 | 13.7 | 6.5 | 1.5 | -2.6 | 6.8 |
| Annapolis, MD | ${ }^{\circ} \mathrm{F}$ | 23.8 | 25.1 | 32.8 | 42.1 | 52.3 | 61.6 | 67.3 | 65.8 | 58.5 | 46.3 | 36.2 | 28.6 | 45.0 |
|  | ${ }^{\circ} \mathrm{C}$ | -4.6 | -3.8 | 0.4 | 5.6 | 11.3 | 16.4 | 19.6 | 18.8 | 14.7 | 7.9 | 2.3 | -1.9 | 7.2 |
| Cambridge, MD | ${ }^{\circ} \mathrm{F}$ | 27.2 | 29.3 | 36.5 | 44.7 | 54.5 | 63.5 | 68.3 | 66.9 | 60.5 | 48.8 | 40.1 | 31.8 | 47.7 |
|  | ${ }^{\circ} \mathrm{C}$ | -2.7 | -1.5 | 2.5 | 7.1 | 12.5 | 17.5 | 20.2 | 19.4 | 15.8 | 9.3 | 4.5 | -0.1 | 8.7 |
| Princess Anne, MD | ${ }^{\circ} \mathrm{F}$ | 26.0 | 27.8 | 34.3 | 41.2 | 50.8 | 59.8 | 64.7 | 63.1 | 56.2 | 44.4 | 37.1 | 29.5 | 44.6 |
|  | ${ }^{\circ} \mathrm{C}$ | -3.3 | -2.3 | 1.3 | 5.1 | 10.4 | 15.4 | 18.2 | 17.3 | 13.4 | 6.9 | 2.8 | -1.4 | 7.0 |
| Patuxent River NAS | ${ }^{\circ} \mathrm{F}$ | 28.3 | 29.9 | 36.9 | 45.7 | 55.9 | 64.8 | 70.0 | 68.7 | 62.4 | 50.4 | 41.2 | 32.8 | 48.9 |
|  | ${ }^{\circ} \mathrm{C}$ | -2.1 | -1.2 | 2.7 | 7.6 | 13.3 | 18.2 | 21.1 | 20.4 | 16.9 | 10.2 | 5.1 | 0.4 | 9.4 |
| Mechanicsville, MD | ${ }^{\circ} \mathrm{F}$ | 26.3 | 28.5 | 35.6 | 43.7 | 53.4 | 61.9 | 67.0 | 65.5 | 59.1 | 47.0 | 38.0 | 30.6 | 46.4 |
|  | ${ }^{\circ} \mathrm{C}$ | -3.2 | -1.9 | 2.0 | 6.5 | 11.9 | 16.6 | 19.4 | 18.6 | 15.1 | 8.3 | 3.3 | -0.8 | 8.0 |

Table 2.3-67—\{Monthly Mean Wet Bulb Temperatures (1983-2000) at Sites Around CCNPP $\}$

Table 2.3-68_\{Monthly Mean Dew Point Temperatures (1983-2000) at Sites Around CCNPP\}

| SITE |  | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC | ANNUAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Baltimore/Washington International Airport | ${ }^{\circ} \mathrm{F}$ | 23.6 | 25.1 | 30.1 | 40.3 | 51.4 | 61.5 | 65.9 | 64.7 | 58.4 | 47.1 | 34.4 | 25.4 | 44.0 |
|  | ${ }^{\circ} \mathrm{C}$ | -4.7 | -3.8 | -1.1 | 4.6 | 10.8 | 16.4 | 18.8 | 18.2 | 14.7 | 8.4 | 1.3 | -3.7 | 6.7 |
| Norfolk, VA | ${ }^{\circ} \mathrm{F}$ | 31.0 | 32.5 | 37.2 | 45.7 | 55.1 | 64.5 | 65.9 | 68.7 | 59.8 | 52.5 | 43.0 | 34.5 | 49.2 |
|  | ${ }^{\circ} \mathrm{C}$ | -0.6 | 0.3 | 2.9 | 7.6 | 12.8 | 18.1 | 18.8 | 20.4 | 15.4 | 11.4 | 6.1 | 1.4 | 9.6 |
| Richmond, VA | ${ }^{\circ} \mathrm{F}$ | 27.3 | 28.9 | 33.9 | 43.3 | 54.3 | 63.2 | 68.0 | 63.2 | 60.1 | 49.0 | 38.7 | 29.9 | 46.7 |
|  | ${ }^{\circ} \mathrm{C}$ | -2.6 | -1.7 | 1.1 | 6.3 | 12.4 | 17.3 | 20.0 | 17.3 | 15.6 | 9.4 | 3.7 | -1.2 | 8.2 |

Table 2．3－69—\｛Number of Days with Maximum Hourly Temperature Value Greater Than or Equal to $9 \mathbf{0}^{\circ} \mathbf{F}$ at Sites Around CCNPP\}

| SITE | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC | ANNUAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Baltimore／Washington International Airport | 0.0 | 0.0 | 0.0 | 0.4 | 1.4 | 5.8 | 11.3 | 8.0 | 3.4 | 0.0 | 0.0 | 0.0 | 30.3 |
| Norfolk，VA | 0.0 | 0.0 | 0.0 | 0.4 | 1.5 | 5.9 | 10.9 | 8.6 | 2.8 | 0.1 | 0.0 | 0.0 | 30.2 |
| Richmond，VA | 0.0 | 0.0 | 0.1 | 0.8 | 2.3 | 8.7 | 13.8 | 11.0 | 4.1 | 0.3 | 0.0 | 0.0 | 41.1 |

Table 2.3-70—\{Number of Days with Maximum Hourly Temperature Value Less Than or Equal to $32^{\circ} \mathrm{F}$ at Sites Around CCNPP\}

| SITE | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC | ANNUAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Baltimore/Washington International Airport | 7.2 | 4.2 | 0.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 3.6 | 15.5 |
| Norfolk, VA | 3.3 | 1.3 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.0 | 5.7 |
| Richmond, VA | 4.3 | 1.7 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.5 | 7.6 |

Table 2.3-71—\{Number of Days with Minimum Hourly Temperature Value Less Than or Equal to $32^{\circ} \mathbf{F}$ at Sites Around CCNPP\}

| SITE | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC | ANNUAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Baltimore/Washington International Airport | 25.3 | 21.1 | 14.0 | 3.4 | * | 0.0 | 0.0 | 0.0 | 0.0 | 1.9 | 10.2 | 21.1 | 97.0 |
| Norfolk, VA | 18.0 | 15.5 | 6.0 | 0.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.2 | 3.0 | 13.1 | 56.2 |
| Richmond, VA | 23.0 | 19.5 | 10.8 | 2.3 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 2.1 | 9.4 | 19.2 | 86.4 |

Note:

* Denotes value is between 0.00 and 0.05
Table 2.3-72—\{Number of Days with Minimum Hourly Temperature Value Less Than or Equal to $0^{\circ}$ F at Sites Around CCNPP\}

| SITE | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC | ANNUAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Baltimore/Washington International Airport | 0.5 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | * | 0.6 |
| Norfolk, VA | * | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Richmond, VA | 0.3 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.4 |

Note:

* Denotes value is between 0.00 and 0.05
Table 2．3－73—\｛Monthly Mean Relative Humidity at Sites Around CCNPP\}

| SITE |  | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC | ANNUAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Baltimore／Washington International Airport | \％ | 63 | 61 | 59 | 59 | 66 | 68 | 69 | 71 | 71 | 70 | 66 | 66 | 66 |
| Norfolk，VA | \％ | 66 | 66 | 65 | 63 | 69 | 71 | 73 | 75 | 74 | 72 | 68 | 67 | 69 |
| Richmond，VA | \％ | 68 | 66 | 63 | 61 | 70 | 72 | 75 | 77 | 77 | 74 | 69 | 69 | 70 |

Table 2.3-74—\{Monthly Design Wet Bulb and Mean Coincident Dry Bulb Temperature Values for Patuxent River Naval Air Station, Maryland (1982-2001)\}

| \% | Jan |  | Feb |  | Mar |  | Apr |  | May |  | Jun |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | WB | MCDB | WB | MCDB | WB | MCDB | WB | MCDB | WB | MCDB | WB | MCDB |
|  | 19a | 19b | 19c | 19d | 19e | 19 f | 19g | 19h | 19i | 19j | 19k | 191 |
| 0.4\% | $60.2^{\circ} \mathrm{F}$ | $63.7^{\circ} \mathrm{F}$ | $61.3^{\circ} \mathrm{F}$ | $67.1^{\circ} \mathrm{F}$ | $65.1^{\circ} \mathrm{F}$ | $77.6^{\circ} \mathrm{F}$ | $68.8^{\circ} \mathrm{F}$ | $79.7^{\circ} \mathrm{F}$ | $76.0^{\circ} \mathrm{F}$ | $86.3^{\circ} \mathrm{F}$ | $79.5{ }^{\circ} \mathrm{F}$ | $88.4{ }^{\circ} \mathrm{F}$ |
|  | $15.7^{\circ} \mathrm{C}$ | $17.6^{\circ} \mathrm{C}$ | $16.3^{\circ} \mathrm{C}$ | $19.5{ }^{\circ} \mathrm{C}$ | $18.4{ }^{\circ} \mathrm{C}$ | $25.3^{\circ} \mathrm{C}$ | $20.4{ }^{\circ} \mathrm{C}$ | $26.5^{\circ} \mathrm{C}$ | $24.4{ }^{\circ} \mathrm{C}$ | $30.2^{\circ} \mathrm{C}$ | $26.4{ }^{\circ} \mathrm{C}$ | $31.3{ }^{\circ} \mathrm{C}$ |
| 1\% | $57.5^{\circ} \mathrm{F}$ | $61.8^{\circ} \mathrm{F}$ | $58.8{ }^{\circ} \mathrm{F}$ | $64.4^{\circ} \mathrm{F}$ | $63.0^{\circ} \mathrm{F}$ | $72.3{ }^{\circ} \mathrm{F}$ | $67.1^{\circ} \mathrm{F}$ | $76.9^{\circ} \mathrm{F}$ | $74.6{ }^{\circ} \mathrm{F}$ | $83.9^{\circ} \mathrm{F}$ | $78.2^{\circ} \mathrm{F}$ | $86.9^{\circ} \mathrm{F}$ |
|  | $14.2^{\circ} \mathrm{C}$ | $16.6^{\circ} \mathrm{C}$ | $14.9{ }^{\circ} \mathrm{C}$ | $18.0^{\circ} \mathrm{C}$ | $17.2^{\circ} \mathrm{C}$ | $22.4{ }^{\circ} \mathrm{C}$ | $19.5{ }^{\circ} \mathrm{C}$ | $24.9^{\circ} \mathrm{C}$ | $23.7^{\circ} \mathrm{C}$ | $28.8^{\circ} \mathrm{C}$ | $25.7^{\circ} \mathrm{C}$ | $30.5^{\circ} \mathrm{C}$ |
| 2\% | $55.0^{\circ} \mathrm{F}$ | $58.5{ }^{\circ} \mathrm{F}$ | $56.0^{\circ} \mathrm{F}$ | $61.9^{\circ} \mathrm{F}$ | $60.8^{\circ} \mathrm{F}$ | $68.7^{\circ} \mathrm{F}$ | $65.5^{\circ} \mathrm{F}$ | $74.3{ }^{\circ} \mathrm{F}$ | $73.0^{\circ} \mathrm{F}$ | $81.8^{\circ} \mathrm{F}$ | $77.4^{\circ} \mathrm{F}$ | $85.9{ }^{\circ} \mathrm{F}$ |
|  | $12.8{ }^{\circ} \mathrm{C}$ | $14.7^{\circ} \mathrm{C}$ | $13.3^{\circ} \mathrm{C}$ | $16.6^{\circ} \mathrm{C}$ | $16.0^{\circ} \mathrm{C}$ | $20.4{ }^{\circ} \mathrm{C}$ | $18.6^{\circ} \mathrm{C}$ | $23.5^{\circ} \mathrm{C}$ | $22.8{ }^{\circ} \mathrm{C}$ | $27.7^{\circ} \mathrm{C}$ | $25.2^{\circ} \mathrm{C}$ | $29.9^{\circ} \mathrm{C}$ |
| \% | Jul |  | Aug |  | Sep |  | Oct |  | Nov |  | Dec |  |
|  | WB | MCDB | WB | MCDB | WB | MCDB | WB | MCDB | WB | MCDB | WB | MCDB |
|  | 19m | 19n | 190 | 19p | 19q | 19r | 19s | 19t | 19u | 19v | 19w | 19x |
| 0.4\% | $81.3^{\circ} \mathrm{F}$ | $90.8^{\circ} \mathrm{F}$ | $80.9^{\circ} \mathrm{F}$ | $88.2^{\circ} \mathrm{F}$ | $78.4^{\circ} \mathrm{F}$ | $85.5^{\circ} \mathrm{F}$ | $72.8{ }^{\circ} \mathrm{F}$ | $80.0^{\circ} \mathrm{F}$ | $67.1^{\circ} \mathrm{F}$ | $72.0^{\circ} \mathrm{F}$ | $63.5^{\circ} \mathrm{F}$ | $68.9^{\circ} \mathrm{F}$ |
|  | $27.4^{\circ} \mathrm{C}$ | $32.7^{\circ} \mathrm{C}$ | $27.2^{\circ} \mathrm{C}$ | $31.2^{\circ} \mathrm{C}$ | $25.8^{\circ} \mathrm{C}$ | $29.7^{\circ} \mathrm{C}$ | $22.7^{\circ} \mathrm{C}$ | $26.7^{\circ} \mathrm{C}$ | $19.5{ }^{\circ} \mathrm{C}$ | $22.2^{\circ} \mathrm{C}$ | $17.5^{\circ} \mathrm{C}$ | $20.5^{\circ} \mathrm{C}$ |
| 1\% | $80.3^{\circ} \mathrm{F}$ | $89.9^{\circ} \mathrm{F}$ | $79.7^{\circ} \mathrm{F}$ | $88.4^{\circ} \mathrm{F}$ | $77.4^{\circ} \mathrm{F}$ | $84.6^{\circ} \mathrm{F}$ | $71.3^{\circ} \mathrm{F}$ | $78.6^{\circ} \mathrm{F}$ | $65.5^{\circ} \mathrm{F}$ | $69.9^{\circ} \mathrm{F}$ | $61.3^{\circ} \mathrm{F}$ | $65.9{ }^{\circ} \mathrm{F}$ |
|  | $26.8^{\circ} \mathrm{C}$ | $32.2^{\circ} \mathrm{C}$ | $26.5^{\circ} \mathrm{C}$ | $31.3^{\circ} \mathrm{C}$ | $25.2^{\circ} \mathrm{C}$ | $29.2^{\circ} \mathrm{C}$ | $21.8^{\circ} \mathrm{C}$ | $25.9^{\circ} \mathrm{C}$ | $18.6^{\circ} \mathrm{C}$ | $21.1^{\circ} \mathrm{C}$ | $16.3^{\circ} \mathrm{C}$ | $18.8^{\circ} \mathrm{C}$ |
| 2\% | $79.6{ }^{\circ} \mathrm{F}$ | $89.2^{\circ} \mathrm{F}$ | $78.6^{\circ} \mathrm{F}$ | $87.0^{\circ} \mathrm{F}$ | $76.4^{\circ} \mathrm{F}$ | $83.3^{\circ} \mathrm{F}$ | $70.2^{\circ} \mathrm{F}$ | $76.6^{\circ} \mathrm{F}$ | $64.0^{\circ} \mathrm{F}$ | $68.2^{\circ} \mathrm{F}$ | $59.4{ }^{\circ} \mathrm{F}$ | $64.2^{\circ} \mathrm{F}$ |
|  | $26.4^{\circ} \mathrm{C}$ | $31.8^{\circ} \mathrm{C}$ | $25.9^{\circ} \mathrm{C}$ | $30.6{ }^{\circ} \mathrm{C}$ | $24.7{ }^{\circ} \mathrm{C}$ | $28.5^{\circ} \mathrm{C}$ | $21.2^{\circ} \mathrm{C}$ | $24.8{ }^{\circ} \mathrm{C}$ | $17.8^{\circ} \mathrm{C}$ | $20.1^{\circ} \mathrm{C}$ | $15.2^{\circ} \mathrm{C}$ | $17.9^{\circ} \mathrm{C}$ |

Note:
WB = wet bulb
MCDB = mean coincident dry bulb

Table 2.3-75-\{Monthly Design Wet Bulb and Mean Coincident Dry Bulb Temperature Values for Salisbury Wicomico County Airport, Maryland (1982-2001)\}

|  | Jan |  | Feb |  | Mar |  | Apr |  | May |  | Jun |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \% | WB | MCDB | WB | MCDB | WB | MCDB | WB | MCDB | WB | MCDB | WB | MCDB |
|  | 19a | 19b | 19c | 19d | 19e | 19 f | 19g | 19h | 19i | 19j | 19k | 191 |
| 0.4\% | $63.6^{\circ} \mathrm{F}$ | $65.1^{\circ} \mathrm{F}$ | $63.0^{\circ} \mathrm{F}$ | $66.9^{\circ} \mathrm{F}$ | $65.9^{\circ} \mathrm{F}$ | $74.4{ }^{\circ} \mathrm{F}$ | $70.5^{\circ} \mathrm{F}$ | $82.3^{\circ} \mathrm{F}$ | $75.9^{\circ} \mathrm{F}$ | $85.2^{\circ} \mathrm{F}$ | $80.2^{\circ} \mathrm{F}$ | $88.1^{\circ} \mathrm{F}$ |
|  | $17.6^{\circ} \mathrm{C}$ | $18.4^{\circ} \mathrm{C}$ | $17.2^{\circ} \mathrm{C}$ | $19.4{ }^{\circ} \mathrm{C}$ | $18.8^{\circ} \mathrm{C}$ | $23.6^{\circ} \mathrm{C}$ | $21.4^{\circ} \mathrm{C}$ | $27.9^{\circ} \mathrm{C}$ | $24.4{ }^{\circ} \mathrm{C}$ | $29.6^{\circ} \mathrm{C}$ | $26.8^{\circ} \mathrm{C}$ | $31.2{ }^{\circ} \mathrm{C}$ |
| 1\% | $61.2^{\circ} \mathrm{F}$ | $63.4^{\circ} \mathrm{F}$ | $61.3^{\circ} \mathrm{F}$ | $65.1^{\circ} \mathrm{F}$ | $64.4{ }^{\circ} \mathrm{F}$ | $71.8^{\circ} \mathrm{F}$ | $68.6^{\circ} \mathrm{F}$ | $78.5^{\circ} \mathrm{F}$ | $74.7{ }^{\circ} \mathrm{F}$ | $83.9^{\circ} \mathrm{F}$ | $78.7^{\circ} \mathrm{F}$ | $87.0^{\circ} \mathrm{F}$ |
|  | $16.2^{\circ} \mathrm{C}$ | $17.4^{\circ} \mathrm{C}$ | $16.3^{\circ} \mathrm{C}$ | $18.4^{\circ} \mathrm{C}$ | $18.0^{\circ} \mathrm{C}$ | $22.1{ }^{\circ} \mathrm{C}$ | $20.3^{\circ} \mathrm{C}$ | $25.8^{\circ} \mathrm{C}$ | $23.7^{\circ} \mathrm{C}$ | $28.8^{\circ} \mathrm{C}$ | $25.9^{\circ} \mathrm{C}$ | $30.6^{\circ} \mathrm{C}$ |
| 2\% | $58.8{ }^{\circ} \mathrm{F}$ | $61.9^{\circ} \mathrm{F}$ | $59.1{ }^{\circ} \mathrm{F}$ | $62.7^{\circ} \mathrm{F}$ | $62.9^{\circ} \mathrm{F}$ | $69.2^{\circ} \mathrm{F}$ | $66.9^{\circ} \mathrm{F}$ | $75.7^{\circ} \mathrm{F}$ | $73.5{ }^{\circ} \mathrm{F}$ | $82.5^{\circ} \mathrm{F}$ | $77.8^{\circ} \mathrm{F}$ | $86.5^{\circ} \mathrm{F}$ |
|  | $14.9{ }^{\circ} \mathrm{C}$ | $16.6^{\circ} \mathrm{C}$ | $15.1^{\circ} \mathrm{C}$ | $17.1^{\circ} \mathrm{C}$ | $17.2^{\circ} \mathrm{C}$ | $20.7^{\circ} \mathrm{C}$ | $19.4{ }^{\circ} \mathrm{C}$ | $24.3{ }^{\circ} \mathrm{C}$ | $23.1{ }^{\circ} \mathrm{C}$ | $28.1{ }^{\circ} \mathrm{C}$ | $25.4^{\circ} \mathrm{C}$ | $30.3^{\circ} \mathrm{C}$ |
| \% | Jul |  | Aug |  | Sep |  | Oct |  | Nov |  | Dec |  |
|  | WB | MCDB | WB | MCDB | WB | MCDB | WB | MCDB | WB | MCDB | WB | MCDB |
|  | 19m | 19n | 190 | 19p | 19q | 19r | 19s | 19t | 19u | 19v | 19w | 19x |
| 0.4\% | $82.3^{\circ} \mathrm{F}$ | $91.4^{\circ} \mathrm{F}$ | $81.2^{\circ} \mathrm{F}$ | $88.9^{\circ} \mathrm{F}$ | $78.2^{\circ} \mathrm{F}$ | $86.0^{\circ} \mathrm{F}$ | $73.9^{\circ} \mathrm{F}$ | $78.9^{\circ} \mathrm{F}$ | $68.1^{\circ} \mathrm{F}$ | $71.5^{\circ} \mathrm{F}$ | $64.8{ }^{\circ} \mathrm{F}$ | $68.3^{\circ} \mathrm{F}$ |
|  | $27.9^{\circ} \mathrm{C}$ | $33.0{ }^{\circ} \mathrm{C}$ | $27.3^{\circ} \mathrm{C}$ | $31.6^{\circ} \mathrm{C}$ | $25.7^{\circ} \mathrm{C}$ | $30.0^{\circ} \mathrm{C}$ | $23.3^{\circ} \mathrm{C}$ | $26.1^{\circ} \mathrm{C}$ | $20.1{ }^{\circ} \mathrm{C}$ | $21.9^{\circ} \mathrm{C}$ | $18.2^{\circ} \mathrm{C}$ | $20.2^{\circ} \mathrm{C}$ |
| 1\% | $81.1^{\circ} \mathrm{F}$ | $90.3^{\circ} \mathrm{F}$ | $80.0^{\circ} \mathrm{F}$ | $88.1{ }^{\circ} \mathrm{F}$ | $77.3^{\circ} \mathrm{F}$ | $84.3^{\circ} \mathrm{F}$ | $72.5{ }^{\circ} \mathrm{F}$ | $78.4^{\circ} \mathrm{F}$ | $66.8^{\circ} \mathrm{F}$ | $70.0^{\circ} \mathrm{F}$ | $63.2^{\circ} \mathrm{F}$ | $65.8^{\circ} \mathrm{F}$ |
|  | $27.3^{\circ} \mathrm{C}$ | $32.4{ }^{\circ} \mathrm{C}$ | $26.7^{\circ} \mathrm{C}$ | $31.2^{\circ} \mathrm{C}$ | $25.2^{\circ} \mathrm{C}$ | $29.1{ }^{\circ} \mathrm{C}$ | $22.5{ }^{\circ} \mathrm{C}$ | $25.8^{\circ} \mathrm{C}$ | $19.3{ }^{\circ} \mathrm{C}$ | $21.1^{\circ} \mathrm{C}$ | $17.3^{\circ} \mathrm{C}$ | $18.8{ }^{\circ} \mathrm{C}$ |
| 2\% | $80.2^{\circ} \mathrm{F}$ | $89.1{ }^{\circ} \mathrm{F}$ | $79.0^{\circ} \mathrm{F}$ | $87.0^{\circ} \mathrm{F}$ | $76.4{ }^{\circ} \mathrm{F}$ | $82.9^{\circ} \mathrm{F}$ | $71.3^{\circ} \mathrm{F}$ | $77.4^{\circ} \mathrm{F}$ | $65.8^{\circ} \mathrm{F}$ | $69.2^{\circ} \mathrm{F}$ | $61.4^{\circ} \mathrm{F}$ | $64.1{ }^{\circ} \mathrm{F}$ |
|  | $26.8{ }^{\circ} \mathrm{C}$ | $31.7^{\circ} \mathrm{C}$ | $26.1{ }^{\circ} \mathrm{C}$ | $30.6{ }^{\circ} \mathrm{C}$ | $24.7^{\circ} \mathrm{C}$ | $28.3^{\circ} \mathrm{C}$ | $21.8^{\circ} \mathrm{C}$ | $25.2{ }^{\circ} \mathrm{C}$ | $18.8{ }^{\circ} \mathrm{C}$ | $20.7^{\circ} \mathrm{C}$ | $16.3{ }^{\circ} \mathrm{C}$ | $17.8^{\circ} \mathrm{C}$ |

Note:
WB = wet bulb
MCDB = mean coincident dry bulb

Table 2.3-76-\{Monthly Design Wet Bulb and Mean Coincident Dry Bulb Temperature Values for Baltimore, Maryland (1982-2001)\}

| \% | Jan |  | Feb |  | Mar |  | Apr |  | May |  | Jun |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | WB | MCDB | WB | MCDB | WB | MCDB | WB | MCDB | WB | MCDB | WB | MCDB |
|  | 19a | 19b | 19c | 19d | 19e | 19 f | 19g | 19h | 19i | 19j | 19k | 191 |
| 0.4\% | $60.2^{\circ} \mathrm{F}$ | $63.5^{\circ} \mathrm{F}$ | $60.0^{\circ} \mathrm{F}$ | $66.0^{\circ} \mathrm{F}$ | $64.8{ }^{\circ} \mathrm{F}$ | $77.7^{\circ} \mathrm{F}$ | $68.7^{\circ} \mathrm{F}$ | $80.2^{\circ} \mathrm{F}$ | $74.7^{\circ} \mathrm{F}$ | $85.5^{\circ} \mathrm{F}$ | $78.5^{\circ} \mathrm{F}$ | $88.2^{\circ} \mathrm{F}$ |
|  | $15.7^{\circ} \mathrm{C}$ | $17.5^{\circ} \mathrm{C}$ | $15.6^{\circ} \mathrm{C}$ | $18.9{ }^{\circ} \mathrm{C}$ | $18.2^{\circ} \mathrm{C}$ | $25.4^{\circ} \mathrm{C}$ | $20.4{ }^{\circ} \mathrm{C}$ | $26.8^{\circ} \mathrm{C}$ | $23.7{ }^{\circ} \mathrm{C}$ | $29.7^{\circ} \mathrm{C}$ | $25.8^{\circ} \mathrm{C}$ | $31.2{ }^{\circ} \mathrm{C}$ |
| 1\% | $57.5^{\circ} \mathrm{F}$ | $61.3^{\circ} \mathrm{F}$ | $57.4{ }^{\circ} \mathrm{F}$ | $62.7^{\circ} \mathrm{F}$ | $62.4{ }^{\circ} \mathrm{F}$ | $72.4{ }^{\circ} \mathrm{F}$ | $67.3^{\circ} \mathrm{F}$ | $78.4{ }^{\circ} \mathrm{F}$ | $73.3^{\circ} \mathrm{F}$ | $83.9^{\circ} \mathrm{F}$ | $77.3^{\circ} \mathrm{F}$ | $87.1^{\circ} \mathrm{F}$ |
|  | $14.2^{\circ} \mathrm{C}$ | $16.3^{\circ} \mathrm{C}$ | $14.1{ }^{\circ} \mathrm{C}$ | $17.1^{\circ} \mathrm{C}$ | $16.9^{\circ} \mathrm{C}$ | $22.4{ }^{\circ} \mathrm{C}$ | $19.6{ }^{\circ} \mathrm{C}$ | $25.8^{\circ} \mathrm{C}$ | $22.9{ }^{\circ} \mathrm{C}$ | $28.8^{\circ} \mathrm{C}$ | $25.2^{\circ} \mathrm{C}$ | $30.6{ }^{\circ} \mathrm{C}$ |
| 2\% | $54.4^{\circ} \mathrm{F}$ | $57.8^{\circ} \mathrm{F}$ | $54.4{ }^{\circ} \mathrm{F}$ | $60.0^{\circ} \mathrm{F}$ | $60.0^{\circ} \mathrm{F}$ | $68.6^{\circ} \mathrm{F}$ | $65.6^{\circ} \mathrm{F}$ | $75.9^{\circ} \mathrm{F}$ | $72.0^{\circ} \mathrm{F}$ | $81.7^{\circ} \mathrm{F}$ | $76.3^{\circ} \mathrm{F}$ | $85.8^{\circ} \mathrm{F}$ |
|  | $12.4{ }^{\circ} \mathrm{C}$ | $14.3{ }^{\circ} \mathrm{C}$ | $12.4{ }^{\circ} \mathrm{C}$ | $15.6^{\circ} \mathrm{C}$ | $15.6^{\circ} \mathrm{C}$ | $20.3^{\circ} \mathrm{C}$ | $18.7^{\circ} \mathrm{C}$ | $24.4{ }^{\circ} \mathrm{C}$ | $22.2{ }^{\circ} \mathrm{C}$ | $27.6^{\circ} \mathrm{C}$ | $24.6{ }^{\circ} \mathrm{C}$ | $29.9^{\circ} \mathrm{C}$ |
| \% | Jul |  | Aug |  | Sep |  | Oct |  | Nov |  | Dec |  |
|  | WB | MCDB | WB | MCDB | WB | MCDB | WB | MCDB | WB | MCDB | WB | MCDB |
|  | 19m | 19n | 190 | 19p | 19q | 19r | 19s | 19t | 19u | 19v | 19w | 19x |
| 0.4\% | $80.3^{\circ} \mathrm{F}$ | $91.2^{\circ} \mathrm{F}$ | $79.5^{\circ} \mathrm{F}$ | $89.0^{\circ} \mathrm{F}$ | $77.3^{\circ} \mathrm{F}$ | $86.2^{\circ} \mathrm{F}$ | $71.5{ }^{\circ} \mathrm{F}$ | $77.8^{\circ} \mathrm{F}$ | $66.5^{\circ} \mathrm{F}$ | $71.3^{\circ} \mathrm{F}$ | $61.7^{\circ} \mathrm{F}$ | $66.5^{\circ} \mathrm{F}$ |
|  | $26.8^{\circ} \mathrm{C}$ | $32.9^{\circ} \mathrm{C}$ | $26.4{ }^{\circ} \mathrm{C}$ | $31.7^{\circ} \mathrm{C}$ | $25.2^{\circ} \mathrm{C}$ | $30.1{ }^{\circ} \mathrm{C}$ | $21.9^{\circ} \mathrm{C}$ | $25.4^{\circ} \mathrm{C}$ | $19.2^{\circ} \mathrm{C}$ | $21.8^{\circ} \mathrm{C}$ | $16.5^{\circ} \mathrm{C}$ | $19.2{ }^{\circ} \mathrm{C}$ |
| 1\% | $79.3^{\circ} \mathrm{F}$ | $90.5^{\circ} \mathrm{F}$ | $78.4{ }^{\circ} \mathrm{F}$ | $88.1{ }^{\circ} \mathrm{F}$ | $76.3^{\circ} \mathrm{F}$ | $84.7^{\circ} \mathrm{F}$ | $70.5^{\circ} \mathrm{F}$ | $76.4^{\circ} \mathrm{F}$ | $64.7^{\circ} \mathrm{F}$ | $68.9^{\circ} \mathrm{F}$ | $59.5^{\circ} \mathrm{F}$ | $63.1^{\circ} \mathrm{F}$ |
|  | $26.3^{\circ} \mathrm{C}$ | $32.5{ }^{\circ} \mathrm{C}$ | $25.8^{\circ} \mathrm{C}$ | $31.2^{\circ} \mathrm{C}$ | $24.6{ }^{\circ} \mathrm{C}$ | $29.3{ }^{\circ} \mathrm{C}$ | $21.4^{\circ} \mathrm{C}$ | $24.7^{\circ} \mathrm{C}$ | $18.2^{\circ} \mathrm{C}$ | $20.5^{\circ} \mathrm{C}$ | $15.3^{\circ} \mathrm{C}$ | $17.3^{\circ} \mathrm{C}$ |
| 2\% | $78.4{ }^{\circ} \mathrm{F}$ | $89.2^{\circ} \mathrm{F}$ | $77.7^{\circ} \mathrm{F}$ | $87.5^{\circ} \mathrm{F}$ | $75.3^{\circ} \mathrm{F}$ | $83.2{ }^{\circ} \mathrm{F}$ | $69.1{ }^{\circ} \mathrm{F}$ | $74.7{ }^{\circ} \mathrm{F}$ | $63.4^{\circ} \mathrm{F}$ | $67.3^{\circ} \mathrm{F}$ | $56.9^{\circ} \mathrm{F}$ | $60.7^{\circ} \mathrm{F}$ |
|  | $25.8{ }^{\circ} \mathrm{C}$ | $31.8{ }^{\circ} \mathrm{C}$ | $25.4{ }^{\circ} \mathrm{C}$ | $30.8{ }^{\circ} \mathrm{C}$ | $24.1{ }^{\circ} \mathrm{C}$ | $28.4^{\circ} \mathrm{C}$ | $20.6{ }^{\circ} \mathrm{C}$ | $23.7^{\circ} \mathrm{C}$ | $17.4^{\circ} \mathrm{C}$ | $19.6{ }^{\circ} \mathrm{C}$ | $13.8{ }^{\circ} \mathrm{C}$ | $15.9^{\circ} \mathrm{C}$ |

Note:
WB = wet bulb
MCDB = mean coincident dry bulb
Table 2.3-77—\{CCNPP Monthly and Annual Precipitation (2000-2005)\}
Table 2．3－78—\｛CCNPP Monthly and Annual Percent Frequency of Precipitation Occurrence（2000－2005）\}

| JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC | ANNUAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5.19 | 4.93 | 6.41 | 7.87 | 6.17 | 4.30 | 5.13 | 4.57 | 4.26 | 6.32 | 5.30 | 6.46 | 5.58 |

Table 2.3-79—\{CCNPP Hourly Rainfall Rate Distribution (2000-2005)\}

| Rainfall Rate in $/ \mathbf{h r}$ $(\mathbf{m m} / \mathbf{h r})$ | $\begin{gathered} 0.0 \\ (0.0) \end{gathered}$ | $\begin{gathered} 0.0-0.1 \\ (0.0-2.5) \end{gathered}$ | $\begin{gathered} 0.1-0.2 \\ (2.5-5.1) \end{gathered}$ | $\begin{gathered} 0.2-0.3 \\ (5.1-7.6) \end{gathered}$ | $\begin{gathered} 0.3-0.4 \\ (7.6-10.2) \end{gathered}$ | $\begin{gathered} 0.4-0.5 \\ (10.2-12.7) \end{gathered}$ | $\begin{gathered} 0.5-0.6 \\ (12.7-15.2) \end{gathered}$ | $\begin{gathered} 0.6-0.7 \\ (15.2-17.8) \end{gathered}$ | $\begin{gathered} 0.7-0.8 \\ (17.8-20.3) \end{gathered}$ | $\begin{gathered} 0.8-0.9 \\ (20.3-22.9) \end{gathered}$ | $\begin{gathered} 0.9-1.0 \\ (22.9-25.4) \end{gathered}$ | $\begin{gathered} 1.0-2.0 \\ (25.4-50.8) \end{gathered}$ | $\begin{gathered} 2.0-3.0 \\ (50.8-76.2) \end{gathered}$ | Missing Data |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Number of hours | 48781 | 2374 | 306 | 73 | 87 | 18 | 10 | 9 | 6 | 1 | 1 | 2 | 1 | 939 |

Table 2.3-80—\{CCNPP Measured Extreme Precipitation Hourly Values (2000-2005)\}

| Rainfall Amount <br> (in (mm)) | 2.2 <br> $(55.9)$ | $\mathbf{1 . 5 9 ( 4 0 . 3 9 )}$ | $\mathbf{1 . 5 7}$ (39.88) |
| :---: | :---: | :---: | :---: |
| Dat Occurred | $4 / 15 / 2003$ | $5 / 21 / 2001$ | $6 / 30 / 2005)$ |

Date Occurred
Table 2.3-81-\{Mean Monthly and Annual Precipitation (1971-2000) At Sites Around CCNPP\}

Table 2.3-82—\{Mean Monthly and Annual Snowfall (1961-1990)At Sites Around CCNPP\}

| SITE |  | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC | ANNUAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Baltimore/Washington International Airport | in | 7.0 | 6.4 | 2.4 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.6 | 1.7 | 18.2 |
|  | mm | 177.80 | 162.56 | 60.96 | 2.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 15.24 | 43.18 | 462.28 |
| Norfolk, VA | in | 2.6 | 3.8 | 1.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.4 | 8.1 |
|  | mm | 66.04 | 96.52 | 33.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 10.16 | 205.74 |
| Richmond, VA | in | 4.3 | 4.8 | 1.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.3 | 1.6 | 12.4 |
|  | mm | 109.22 | 121.92 | 35.56 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 7.62 | 40.64 | 314.96 |

Table 2．3－83—\｛Monthly Mean Number of Days with Precipitation（1961－1990）At Sites Around CCNPP\}

| SITE | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC | ANNUAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Baltimore／Washington International Airport | 10.2 | 9.4 | 10.0 | 10.5 | 10.9 | 9.2 | 9.6 | 9.4 | 7.2 | 7.4 | 9.0 | 9.2 | 112.0 |
| Norfolk，VA | 10.7 | 10.3 | 10.4 | 9.8 | 9.9 | 9.7 | 11.1 | 10.1 | 7.7 | 7.4 | 7.7 | 9.5 | 114.3 |
| Richmond，VA | 10.4 | 9.4 | 10.2 | 9.0 | 10.7 | 9.6 | 10.4 | 9.5 | 7.6 | 7.0 | 8.0 | 9.1 | 110.9 |

Table 2．3－84—\｛Monthly Mean Number of Days with Heavy Fog（1971－2000）At Sites Around CCNPP\}

| SITE | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC | ANNUAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Baltimore／Washington International Airport | 3.1 | 3.2 | 2.5 | 1.8 | 1.6 | 0.9 | 0.8 | 1.0 | 1.3 | 2.5 | 2.6 | 3.1 | 24.4 |
| Norfolk，VA | 2.1 | 2.5 | 2.0 | 1.5 | 1.8 | 1.0 | 0.5 | 1.0 | 1.2 | 2.1 | 1.9 | 2.1 | 19.7 |
| Richmond，VA | 2.7 | 2.1 | 1.7 | 1.6 | 1.8 | 1.5 | 2.0 | 2.4 | 2.9 | 3.3 | 2.3 | 2.8 | 27.1 |

Note：
BWI period 1949－2002，Norfolk period 1948－2002，Richmond period 1928－2002

|  | Table 2.3-85—\{CCNPP 33 ft ( 10 m ) Annual Stability Persistence Summary for Year 2000 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | STABILITY PERSISTENCE (HOURS)/PERCENT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | STABILITY | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
|  | A | 113 | 62 | 35 | 39 | 28 | 26 | 19 | 8 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 334 |
|  |  | 34 | 52 | 63 | 75 | 83 | 91 | 96 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | B | 302 | 49 | 11 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 364 |
|  |  | 83 | 96 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | C | 300 | 55 | 12 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 371 |
|  |  | 81 | 96 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | D | 381 | 198 | 68 | 44 | 27 | 16 | 3 | 8 | 9 | 8 | 11 | 7 | 8 | 5 | 7 | 7 | 4 | 4 | 1 | 4 | 0 | 1 | 2 | 3 | 9 | 835 |
|  |  | 46 | 69 | 77 | 83 | 86 | 88 | 88 | 89 | 90 | 91 | 93 | 93 | 94 | 95 | 96 | 97 | 97 | 98 | 98 | 98 | 98 | 98 | 99 | 99 | 100 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | E | 273 | 133 | 70 | 47 | 32 | 30 | 23 | 20 | 11 | 19 | 8 | 11 | 6 | 5 | 1 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 693 |
|  |  | 39 | 59 | 69 | 75 | 80 | 84 | 88 | 91 | 92 | 95 | 96 | 98 | 99 | 99 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | F | 204 | 73 | 44 | 17 | 13 | 11 | 4 | 2 | 3 | 0 | 2 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 375 |
|  |  | 54 | 74 | 86 | 90 | 94 | 97 | 98 | 98 | 99 | 99 | 99 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | G | 58 | 27 | 21 | 12 | 9 | 14 | 3 | 4 | 3 | 7 | 2 | 1 | 2 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 168 |
|  |  | 35 | 51 | 63 | 70 | 76 | 84 | 86 | 88 | 90 | 94 | 95 | 96 | 97 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | TOTAL | 1631 | 597 | 261 | 163 | 109 | 99 | 52 | 42 | 29 | 35 | 23 | 19 | 17 | 14 | 10 | 10 | 4 | 5 | 1 | 4 | 0 | 1 | 2 | 3 | 9 | 3140 |


| $\begin{aligned} & \widehat{\lambda} \\ & \substack{0 \\ 0 \\ \underset{\sim}{c} \\ \underset{\omega}{c} \\ \hline} \end{aligned}$ | Table 2.3-86—\{CCNPP 33 ft (10m) Annual Stability Persistence Summary for Year 2001\} |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | STABILITY PERSISTENCE (HOURS)/PERCENT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | STABILITY | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
|  | A | 129 | 65 | 34 | 29 | 40 | 34 | 32 | 20 | 7 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 392 |
|  |  | 33 | 49 | 58 | 66 | 76 | 84 | 93 | 98 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | B | 305 | 46 | 10 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 363 |
| $\underset{O}{\circ}$ |  | 84 | 97 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\xlongequal{\beth}$ | C | 288 | 47 | 10 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 347 |
| $\begin{aligned} & \overline{\mathrm{O}} \\ & \underline{1} \end{aligned}$ |  | 83 | 97 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\underset{0}{2} \underset{ }{2}$ | D | 373 | 193 | 81 | 37 | 23 | 18 | 12 | 8 | 12 | 5 | 7 | 8 | 5 | 3 | 7 | 2 | 4 | 2 | 4 | 4 | 0 | 2 | 0 | 0 | 5 | 815 |
| 入 |  | 46 | 69 | 79 | 84 | 87 | 89 | 90 | 91 | 93 | 93 | 94 | 95 | 96 | 96 | 97 | 97 | 98 | 98 | 99 | 99 | 99 | 99 | 99 | 99 | 100 |  |
| - | E | 310 | 130 | 78 | 48 | 36 | 28 | 15 | 12 | 13 | 9 | 7 | 6 | 8 | 7 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 712 |
| $0$ |  | 44 | 62 | 73 | 79 | 85 | 88 | 91 | 92 | 94 | 95 | 96 | 97 | 98 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | F | 262 | 102 | 39 | 33 | 15 | 14 | 7 | 4 | 2 | 2 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 482 |
| $\stackrel{\text { ¢ }}{\substack{\text { I }}}$ |  | 54 | 76 | 84 | 90 | 94 | 96 | 98 | 99 | 99 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\stackrel{\pi}{n}$ | G | 79 | 35 | 23 | 19 | 11 | 7 | 9 | 5 | 4 | 6 | 4 | 3 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 209 |
| ¢ |  | 38 | 55 | 66 | 75 | 80 | 83 | 88 | 90 | 92 | 95 | 97 | 98 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\bigcirc$ | TOTAL | 1746 | 618 | 275 | 169 | 126 | 101 | 75 | 49 | 38 | 24 | 19 | 17 | 16 | 11 | 10 | 5 | 4 | 2 | 4 | 4 | 0 | 2 | 0 | 0 | 5 | 3320 |


|  | Table 2.3-87—\{CCNPP 33 ft (10m) Annual Stability Persistence Summary for Year 2002\} |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | STABILITY PERSISTENCE (HOURS)/PERCENT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | STABILITY | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
|  | A | 101 | 53 | 36 | 40 | 25 | 26 | 34 | 12 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 332 |
|  |  | 30 | 46 | 57 | 69 | 77 | 85 | 95 | 98 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | B | 275 | 47 | 8 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 331 |
|  |  | 83 | 97 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | C | 264 | 62 | 8 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 336 |
|  |  | 79 | 97 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | D | 348 | 186 | 99 | 32 | 26 | 17 | 16 | 10 | 9 | 7 | 7 | 3 | 5 | 6 | 1 | 3 | 3 | 2 | 1 | 3 | 1 | 1 | 1 | 0 | 13 | 800 |
|  |  | 44 | 67 | 79 | 83 | 86 | 89 | 91 | 92 | 93 | 94 | 95 | 95 | 96 | 96 | 97 | 97 | 97 | 98 | 98 | 98 | 98 | 98 | 98 | 98 | 100 |  |
|  | E | 291 | 126 | 61 | 47 | 42 | 28 | 22 | 28 | 12 | 8 | 9 | 12 | 8 | 3 | 4 | 4 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 706 |
|  |  | 41 | 59 | 68 | 74 | 80 | 84 | 87 | 91 | 93 | 94 | 95 | 97 | 98 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 |  |
|  | F | 217 | 84 | 40 | 34 | 25 | 8 | 7 | 0 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 420 |
|  |  | 52 | 72 | 81 | 89 | 95 | 97 | 99 | 99 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | G | 75 | 32 | 26 | 14 | 10 | 8 | 5 | 4 | 2 | 4 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 183 |
|  |  | 41 | 58 | 73 | 80 | 86 | 90 | 93 | 95 | 96 | 98 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | TOTAL | 1571 | 590 | 278 | 169 | 129 | 87 | 84 | 54 | 28 | 22 | 20 | 15 | 13 | 10 | 5 | 7 | 3 | 2 | 1 | 3 | 1 | 2 | 1 | 0 | 13 | 3108 |


|  | Table 2.3-88—\{CCNPP 33 ft (10m) Annual Stability Persistence Summary for Year 2003\} |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | STABILITY PERSISTENCE (HOURS)/PERCENT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | STABILITY | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
|  | A | 100 | 50 | 26 | 29 | 25 | 12 | 6 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 251 |
|  |  | 40 | 60 | 70 | 82 | 92 | 96 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| 1exs!un LOOZ © | B | 207 | 47 | 15 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 272 |
|  |  | 76 | 93 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | C | 287 | 49 | 10 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 348 |
|  |  | 82 | 97 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | D | 314 | 190 | 101 | 44 | 36 | 27 | 19 | 12 | 14 | 3 | 4 | 8 | 2 | 3 | 3 | 7 | 7 | 2 | 1 | 3 | 1 | 1 | 4 | 0 | 10 | 816 |
|  |  | 38 | 62 | 74 | 80 | 84 | 87 | 90 | 91 | 93 | 93 | 94 | 95 | 95 | 95 | 96 | 96 | 97 | 98 | 98 | 98 | 98 | 98 | 99 | 99 | 100 |  |
|  | E | 285 | 140 | 69 | 42 | 48 | 31 | 17 | 20 | 11 | 11 | 11 | 14 | 6 | 5 | 3 | 7 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 722 |
|  |  | 39 | 59 | 68 | 74 | 81 | 85 | 88 | 90 | 92 | 93 | 95 | 97 | 98 | 98 | 99 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 |  |
|  | F | 198 | 85 | 58 | 23 | 13 | 8 | 6 | 3 | 1 | 3 | 3 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 403 |
|  |  | 49 | 70 | 85 | 90 | 94 | 96 | 97 | 98 | 98 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | G | 73 | 31 | 17 | 16 | 12 | 9 | 4 | 2 | 2 | 4 | 4 | 2 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 179 |
|  |  | 41 | 58 | 68 | 77 | 83 | 88 | 91 | 92 | 93 | 95 | 97 | 98 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | TOTAL | 1464 | 592 | 296 | 158 | 135 | 87 | 52 | 40 | 28 | 21 | 22 | 25 | 10 | 9 | 7 | 14 | 7 | 3 | 1 | 4 | 1 | 1 | 4 | 0 | 10 | 2991 |


|  | Table 2.3-89— \{CCNPP 33 ft ( 10 m ) Annual Stability Persistence Summary for Year 2004\} |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | STABILITY PERSISTENCE (HOURS)/PERCENT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | STABILITY | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
|  | A | 106 | 46 | 35 | 22 | 25 | 24 | 21 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 285 |
|  |  | 37 | 53 | 66 | 73 | 82 | 91 | 98 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | B | 226 | 63 | 7 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 298 |
| $\underset{\sim}{\circ}$ |  | 76 | 97 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\subseteq .$ | C | 284 | 51 | 9 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 348 |
|  |  | 82 | 96 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\underset{O}{\circ} \underset{\sim}{2}$ | D | 289 | 191 | 103 | 52 | 30 | 24 | 18 | 28 | 10 | 13 | 12 | 6 | 5 | 3 | 7 | 2 | 5 | 4 | 2 | 1 | 2 | 3 | 0 | 3 | 12 | 825 |
| 증 멕 |  | 35 | 58 | 71 | 77 | 81 | 84 | 86 | 89 | 90 | 92 | 93 | 94 | 95 | 95 | 96 | 96 | 97 | 97 | 97 | 98 | 98 | 98 | 98 | 99 | 100 |  |
| - | E | 267 | 103 | 91 | 56 | 33 | 35 | 25 | 23 | 11 | 10 | 10 | 8 | 6 | 5 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 685 |
| $\mathcal{O}_{0}^{0} \hat{0}_{0}^{\infty}$ |  | 39 | 54 | 67 | 75 | 80 | 85 | 89 | 92 | 94 | 95 | 97 | 98 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\xrightarrow[\square]{\mathrm{h}}$ | F | 196 | 81 | 44 | 28 | 16 | 7 | 1 | 2 | 4 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 381 |
| $0$ |  | 51 | 73 | 84 | 92 | 96 | 98 | 98 | 98 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\stackrel{\sim}{5}$ | G | 52 | 34 | 11 | 14 | 10 | 3 | 6 | 5 | 1 | 2 | 4 | 0 | 4 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 149 |
| ¢ |  | 35 | 58 | 65 | 74 | 81 | 83 | 87 | 91 | 91 | 93 | 95 | 95 | 98 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\bigcirc$ | TOTAL | 1420 | 569 | 300 | 176 | 114 | 95 | 71 | 63 | 27 | 26 | 27 | 14 | 15 | 10 | 10 | 2 | 5 | 4 | 2 | 1 | 2 | 3 | 0 | 3 | 12 | 2971 |



|  | Table 2.3-91—\{CCNPP 33 ft (10m) Annual Stability Persistence Summary for Years 2000-2005\} |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | STABILITY PERSISTENCE (HOURS)/PERCENT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | STABILITY | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
|  | A | 108 | 53 | 33 | 29 | 27 | 24 | 22 | 13 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 313 |
|  |  | 35 | 52 | 63 | 72 | 80 | 88 | 95 | 98 | 83 | 50 | 17 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | B | 255 | 50 | 10 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 317 |
| N |  | 80 | 96 | 99 | 100 | 50 | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| $\subseteq$ | C | 283 | 53 | 11 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 349 |
| $\begin{aligned} & \cong \\ & \cong \end{aligned}$ |  | 81 | 96 | 99 | 100 | 67 | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| $\bigcirc \stackrel{\sum_{0}^{2}}{n}$ | D | 333 | 186 | 94 | 43 | 30 | 22 | 15 | 13 | 11 | 7 | 8 | 6 | 5 | 4 | 5 | 5 | 4 | 3 | 3 | 3 | 1 | 1 | 1 | 2 | 9 | 813 |
| 或 |  | 41 | 64 | 75 | 81 | 84 | 87 | 89 | 90 | 92 | 93 | 94 | 94 | 95 | 95 | 96 | 97 | 97 | 98 | 98 | 98 | 98 | 98 | 99 | 99 | 100 | 0 |
| $\begin{aligned} & 1 \\ & 7 \\ & 7 \end{aligned} \frac{10}{\leq}$ | E | 289 | 122 | 72 | 49 | 38 | 30 | 20 | 20 | 11 | 11 | 8 | 11 | 6 | 5 | 3 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 699 |
| $\mathcal{O}_{0} \hat{i}$ |  | 41 | 59 | 69 | 76 | 82 | 86 | 89 | 91 | 93 | 95 | 96 | 98 | 98 | 99 | 100 | 83 | 67 | 50 | 33 | 33 | 17 | 17 | 0 | 0 | 0 | 0 |
|  | F | 213 | 85 | 45 | 28 | 16 | 10 | 6 | 3 | 2 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 411 |
| $0 \underset{y}{\bar{Z}}$ |  | 52 | 73 | 84 | 90 | 94 | 97 | 98 | 99 | 99 | 100 | 100 | 50 | 50 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| $\overline{\vec{\omega}}$ | G | 68 | 30 | 20 | 16 | 9 | 9 | 6 | 4 | 2 | 4 | 4 | 2 | 2 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 178 |
| $\begin{aligned} & \text { No } \\ & \text { مِ } \end{aligned}$ |  | 38 | 55 | 66 | 75 | 80 | 85 | 89 | 91 | 92 | 94 | 96 | 97 | 98 | 99 | 83 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| $\stackrel{\circ}{\circ}$ | TOTAL | 1550 | 579 | 284 | 167 | 120 | 94 | 69 | 52 | 31 | 25 | 22 | 19 | 14 | 12 | 8 | 7 | 5 | 3 | 3 | 3 | 1 | 2 | 1 | 2 | 9 | 3080 |


| $\begin{aligned} & \widehat{\lambda} \\ & \substack{0 \\ 0 \\ \underset{\sim}{c} \\ \underset{\omega}{c} \\ \hline} \end{aligned}$ | Table 2.3-92—\{CCNPP 197 ft (60m) Annual Stability Persistence Summary for Year 2000 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | STABILITY PERSISTENCE (HOURS)/PERCENT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | STABILITY | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
|  | A | 113 | 62 | 36 | 39 | 28 | 26 | 19 | 8 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 335 |
|  |  | 34 | 52 | 63 | 75 | 83 | 91 | 96 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | B | 304 | 49 | 11 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 366 |
| $\underset{\sim}{\circ}$ |  | 83 | 96 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\xlongequal{\beth}$ | C | 300 | 55 | 12 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 371 |
| $\begin{aligned} & \overline{\mathrm{O}} \\ & \underline{1} \end{aligned}$ |  | 81 | 96 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | D | 383 | 197 | 68 | 42 | 26 | 16 | 3 | 9 | 9 | 8 | 11 | 7 | 8 | 5 | 7 | 7 | 4 | 4 | 1 | 4 | 0 | 1 | 2 | 3 | 9 | 834 |
| 끄엒 |  | 46 | 70 | 78 | 83 | 86 | 88 | 88 | 89 | 90 | 91 | 93 | 93 | 94 | 95 | 96 | 97 | 97 | 98 | 98 | 98 | 98 | 98 | 99 | 99 | 100 |  |
| - | E | 273 | 131 | 71 | 45 | 30 | 30 | 23 | 20 | 11 | 19 | 8 | 11 | 6 | 5 | 2 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 689 |
| OD |  | 40 | 59 | 69 | 75 | 80 | 84 | 88 | 90 | 92 | 95 | 96 | 98 | 98 | 99 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\bigcirc$ | F | 204 | 73 | 44 | 17 | 13 | 11 | 4 | 2 | 3 | 0 | 2 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 375 |
|  |  | 54 | 74 | 86 | 90 | 94 | 97 | 98 | 98 | 99 | 99 | 99 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\stackrel{\pi}{n}$ | G | 57 | 27 | 21 | 12 | 9 | 14 | 3 | 4 | 3 | 7 | 2 | 1 | 2 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 167 |
| ¢ |  | 34 | 50 | 63 | 70 | 75 | 84 | 86 | 88 | 90 | 94 | 95 | 96 | 97 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\bigcirc$ | TOTAL | 1634 | 594 | 263 | 159 | 106 | 99 | 52 | 43 | 29 | 35 | 23 | 19 | 17 | 14 | 11 | 10 | 4 | 5 | 1 | 4 | 0 | 1 | 2 | 3 | 9 | 3137 |


|  | Table 2.3-93—\{CCNPP 197 ft (60m) Annual Stability Persistence Summary for Year 2001\} |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | STABILITY PERSISTENCE (HOURS)/PERCENT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | STABILITY | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
|  | A | 130 | 65 | 34 | 29 | 40 | 34 | 32 | 20 | 7 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 393 |
|  |  | 33 | 50 | 58 | 66 | 76 | 84 | 93 | 98 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | B | 305 | 46 | 10 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 363 |
| $\underset{O}{\circ}$ |  | 84 | 97 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\xlongequal{\beth}$ | C | 288 | 47 | 10 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 347 |
| $\begin{aligned} & \overline{\mathrm{O}} \\ & \underline{1} \end{aligned}$ |  | 83 | 97 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\underset{0}{2} \underset{ }{2}$ | D | 375 | 194 | 80 | 37 | 23 | 18 | 12 | 8 | 12 | 5 | 7 | 8 | 5 | 3 | 7 | 2 | 4 | 2 | 4 | 4 | 0 | 2 | 0 | 0 | 5 | 817 |
| 入 |  | 46 | 70 | 79 | 84 | 87 | 89 | 90 | 91 | 93 | 94 | 94 | 95 | 96 | 96 | 97 | 97 | 98 | 98 | 99 | 99 | 99 | 99 | 99 | 99 | 100 |  |
| - ¢ | E | 310 | 131 | 78 | 48 | 36 | 28 | 15 | 12 | 13 | 9 | 7 | 6 | 8 | 8 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 714 |
| $\mathcal{O}_{0} \stackrel{\rightharpoonup}{\sim}$ |  | 43 | 62 | 73 | 79 | 84 | 88 | 90 | 92 | 94 | 95 | 96 | 97 | 98 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | F | 262 | 102 | 39 | 33 | 15 | 14 | 7 | 4 | 2 | 2 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 482 |
| $\stackrel{\text { ¢ }}{\substack{\text { I }}}$ |  | 54 | 76 | 84 | 90 | 94 | 96 | 98 | 99 | 99 | 100 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\stackrel{\pi}{n}$ | G | 77 | 36 | 24 | 19 | 11 | 7 | 9 | 5 | 5 | 6 | 4 | 2 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 209 |
| ¢ |  | 37 | 54 | 66 | 75 | 80 | 83 | 88 | 90 | 92 | 95 | 97 | 98 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\bigcirc$ | TOTAL | 1747 | 621 | 275 | 169 | 126 | 101 | 75 | 49 | 39 | 24 | 19 | 16 | 16 | 12 | 10 | 5 | 4 | 2 | 4 | 4 | 0 | 2 | 0 | 0 | 5 | 3325 |


|  | Table 2．3－94—\｛CCNPP 197 ft（60m）Annual Stability Persistence Summary for Year 2002\} |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | STABILITY PERSISTENCE（HOURS）／PERCENT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | STABILITY | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT． 24 | TOTAL |
|  | A | 100 | 53 | 36 | 40 | 27 | 27 | 33 | 14 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 335 |
|  |  | 30 | 46 | 56 | 68 | 76 | 84 | 94 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | B | 281 | 47 | 8 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 337 |
| $\bigcirc$ |  | 83 | 97 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\bigcirc$ | C | 270 | 62 | 8 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 342 |
| $\xlongequal{\beth}$ |  | 79 | 97 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\stackrel{\cong}{Z}$ | D | 352 | 189 | 98 | 32 | 26 | 17 | 15 | 10 | 9 | 8 | 7 | 3 | 5 | 6 | 1 | 3 | 3 | 3 | 1 | 3 | 1 | 1 | 1 | 0 | 13 | 807 |
| 웅 |  | 44 | 67 | 79 | 83 | 86 | 88 | 90 | 92 | 93 | 94 | 95 | 95 | 96 | 96 | 96 | 97 | 97 | 98 | 98 | 98 | 98 | 98 | 98 | 98 | 100 |  |
| Q | E | 287 | 127 | 59 | 47 | 44 | 28 | 22 | 29 | 12 | 9 | 9 | 12 | 8 | 3 | 4 | 4 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 705 |
| 궁 |  | 41 | 59 | 67 | 74 | 80 | 84 | 87 | 91 | 93 | 94 | 95 | 97 | 98 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 0 | 0 | 0 |  |
| 而下 | F | 219 | 83 | 41 | 32 | 25 | 8 | 7 | 0 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 420 |
| 令 |  | 52 | 72 | 82 | 89 | 95 | 97 | 99 | 99 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\frac{\mathbf{1}}{\mathbf{0}}$ | G | 71 | 32 | 26 | 15 | 10 | 10 | 4 | 5 | 2 | 4 | 3 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 183 |
| $\frac{\stackrel{4}{\infty}}{\infty}$ |  | 39 | 56 | 70 | 79 | 84 | 90 | 92 | 95 | 96 | 98 | 99 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | TOTAL | 1580 | 593 | 276 | 168 | 133 | 90 | 81 | 58 | 28 | 24 | 21 | 15 | 13 | 10 | 5 | 7 | 3 | 3 | 1 | 3 | 1 | 2 | 1 | 0 | 13 | 3129 |


|  | Table 2.3-95- \{CCNPP 197 ft ( 60 m ) Annual Stability Persistence Summary for Year 2003\} |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | STABILITY PERSISTENCE (HOURS)/PERCENT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | STABILITY | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
|  | A | 100 | 50 | 26 | 29 | 25 | 12 | 6 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 251 |
|  |  | 40 | 60 | 70 | 82 | 92 | 96 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | B | 208 | 47 | 15 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 273 |
| $\underset{\sim}{\circ}$ |  | 76 | 93 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\xlongequal{\beth}$ | C | 289 | 49 | 10 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 350 |
| $\begin{aligned} & \overline{\mathrm{O}} \\ & \underline{1} \end{aligned}$ |  | 83 | 97 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\bigcirc{ }^{\text {O }}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\bigcirc$ | D | 310 | 190 | 99 | 46 | 36 | 27 | 19 | 12 | 14 | 3 | 4 | 8 | 2 | 3 | 3 | 7 | 7 | 2 | 1 | 3 | 1 | 1 | 4 | 0 | 10 | 812 |
| 入 |  | 38 | 62 | 74 | 79 | 84 | 87 | 90 | 91 | 93 | 93 | 94 | 95 | 95 | 95 | 96 | 96 | 97 | 98 | 98 | 98 | 98 | 98 | 99 | 99 | 100 |  |
| - | E | 287 | 137 | 69 | 41 | 47 | 30 | 17 | 20 | 11 | 11 | 11 | 15 | 6 | 5 | 3 | 7 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 718 |
| $\bigcirc \bigcirc$ |  | 40 | 59 | 69 | 74 | 81 | 85 | 87 | 90 | 92 | 93 | 95 | 97 | 98 | 98 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | F | 194 | 83 | 58 | 23 | 13 | 7 | 6 | 3 | 1 | 2 | 4 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 396 |
| $0 \underset{\substack{2 \\ \hline}}{ }$ |  | 49 | 70 | 85 | 90 | 94 | 95 | 97 | 98 | 98 | 98 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\stackrel{\pi}{n}$ | G | 71 | 32 | 17 | 16 | 12 | 9 | 4 | 2 | 2 | 4 | 4 | 2 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 178 |
| ¢ |  | 40 | 58 | 67 | 76 | 83 | 88 | 90 | 92 | 93 | 95 | 97 | 98 | 99 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\bigcirc$ | TOTAL | 1459 | 588 | 294 | 159 | 134 | 85 | 52 | 40 | 28 | 20 | 23 | 26 | 10 | 9 | 7 | 14 | 7 | 3 | 1 | 3 | 1 | 1 | 4 | 0 | 10 | 2978 |


|  | Table 2.3-96— \{CCNPP 197 ft (60m) Annual Stability Persistence Summary for Year 2004\} |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | STABILITY PERSISTENCE (HOURS)/PERCENT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | STABILITY | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
|  | A | 106 | 46 | 35 | 21 | 25 | 24 | 21 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 284 |
|  |  | 37 | 54 | 66 | 73 | 82 | 90 | 98 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | B | 225 | 63 | 7 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 297 |
| N |  | 76 | 97 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\bigcirc$ | C | 284 | 51 | 9 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 348 |
| $\begin{aligned} & \bar{W} \\ & \underline{\cong} \end{aligned}$ |  | 82 | 96 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\bigcirc \hat{O}$ | D | 289 | 191 | 104 | 52 | 30 | 24 | 18 | 28 | 10 | 13 | 12 | 6 | 5 | 3 | 7 | 2 | 4 | 4 | 3 | 1 | 2 | 3 | 0 | 3 | 12 | 826 |
| 予 |  | 35 | 58 | 71 | 77 | 81 | 84 | 86 | 89 | 90 | 92 | 93 | 94 | 95 | 95 | 96 | 96 | 97 | 97 | 97 | 98 | 98 | 98 | 98 | 99 | 100 |  |
| $\underset{0}{\frac{1}{7}} \stackrel{10}{\Sigma}$ | E | 267 | 105 | 91 | 56 | 33 | 35 | 25 | 23 | 11 | 10 | 10 | 8 | 6 | 5 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 687 |
| $\mathcal{O D}_{0} \hat{D}$ |  | 39 | 54 | 67 | 76 | 80 | 85 | 89 | 92 | 94 | 95 | 97 | 98 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\xrightarrow[\square]{\mathrm{h}}$ | F | 197 | 82 | 44 | 28 | 15 | 7 | 1 | 2 | 4 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 382 |
| $\underset{\sim}{\square}$ |  | 52 | 73 | 85 | 92 | 96 | 98 | 98 | 98 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\stackrel{\rightharpoonup}{\mathrm{N}}$ | G | 53 | 34 | 11 | 13 | 10 | 3 | 6 | 5 | 1 | 2 | 4 | 0 | 4 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 149 |
| $\begin{aligned} & \stackrel{\otimes}{\infty} \\ & \underset{\sim}{0} \end{aligned}$ |  | 36 | 58 | 66 | 74 | 81 | 83 | 87 | 91 | 91 | 93 | 95 | 95 | 98 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\bigcirc$ | TOTAL | 1421 | 572 | 301 | 174 | 113 | 95 | 71 | 63 | 27 | 26 | 27 | 14 | 15 | 10 | 10 | 2 | 4 | 4 | 3 | 1 | 2 | 3 | 0 | 3 | 12 | 2973 |


|  | Table 2.3-97—\{CCNPP 197 ft ( 60 m ) Annual Stability Persistence Summary for Year 2005\} |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | STABILITY PERSISTENCE (HOURS)/PERCENT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | STABILITY | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | GT. 24 | TOTAL |
|  | A | 101 | 42 | 30 | 13 | 18 | 20 | 21 | 27 | 11 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 285 |
|  |  | 35 | 50 | 61 | 65 | 72 | 79 | 86 | 95 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | B | 214 | 47 | 8 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 271 |
| $\underset{\sim}{0}$ |  | 79 | 96 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\subseteq$ | C | 273 | 54 | 15 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 343 |
| $\underset{\sim}{\mathrm{O}}$ |  | 80 | 95 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\bigcirc \hat{O}$ | D | 293 | 158 | 109 | 48 | 37 | 24 | 19 | 11 | 14 | 9 | 9 | 5 | 7 | 4 | 2 | 6 | 3 | 4 | 8 | 4 | 1 | 0 | 0 | 3 | 7 | 785 |
| 〇 |  | 37 | 57 | 71 | 77 | 82 | 85 | 88 | 89 | 91 | 92 | 93 | 94 | 95 | 95 | 95 | 96 | 97 | 97 | 98 | 99 | 99 | 99 | 99 | 99 | 100 |  |
| $\begin{array}{ll} -1 \\ 7 & 1 \\ \hline \end{array}$ | E | 308 | 98 | 65 | 52 | 37 | 26 | 20 | 16 | 8 | 11 | 5 | 14 | 2 | 7 | 5 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 675 |
| or |  | 46 | 60 | 70 | 77 | 83 | 87 | 90 | 92 | 93 | 95 | 96 | 98 | 98 | 99 | 100 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | F | 205 | 86 | 45 | 32 | 13 | 10 | 8 | 4 | 2 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 408 |
|  |  | 50 | 71 | 82 | 90 | 93 | 96 | 98 | 99 | 99 | 100 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\overrightarrow{\stackrel{\rightharpoonup}{\omega}}$ | G | 73 | 19 | 21 | 20 | 4 | 12 | 9 | 6 | 1 | 1 | 5 | 6 | 2 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 184 |
| D/ |  | 40 | 50 | 61 | 72 | 74 | 81 | 86 | 89 | 90 | 90 | 93 | 96 | 97 | 99 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $\bigcirc$ | TOTAL | 1467 | 504 | 293 | 168 | 109 | 92 | 77 | 64 | 36 | 24 | 20 | 26 | 11 | 15 | 8 | 6 | 4 | 4 | 8 | 4 | 1 | 0 | 0 | 3 | 7 | 2951 |


Table 2.3-99—\{Monthly and Annual Average Mixing Height Values (m)\}
(Page 1 of 2)

| MONTH | YEAR |  |  |  |  |  |  |  |  |  | Monthly Average | Annual Average |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1996 | 1997 | 1998 | 1999 | 2000 | 2001 | 2002 | 2003 | 2004 | 2005 |  |  |
| JAN | 601 |  | 593 | 465 | 645 | 611 | 468 | 733 | 756 | 558 | 603 | 748 |
| FEB | 736 |  | 640 | 637 | 653 | 607 | 637 | 476 | 646 | 561 | 621 |  |
| MAR | 833 |  | 834 | 829 | 771 | 909 | 641 | 574 | 759 | 815 | 774 |  |
| APR | 873 |  | 932 | 855 | 878 | 597 | 829 | 723 | 812 | 809 | 812 |  |
| MAY | 997 |  | 729 |  | 810 | 701 | 949 | 633 | 762 | 878 | 807 |  |
| JUN | 824 |  |  | 973 | 756 | 864 | 953 | 762 | 837 | 896 | 858 |  |
| JUL |  |  | 889 | 938 | 858 | 990 | 1020 | 873 | 834 | 815 | 902 |  |
| AUG |  |  | 1069 | 1010 | 748 | 808 | 919 | 789 | 863 | 880 | 886 |  |
| SEP |  |  | 940 | 747 | 700 | 821 | 714 | 745 | 677 | 971 | 789 |  |
| OCT |  | 721 | 865 | 634 | 733 | 801 | 699 | 718 | 623 | 708 | 723 |  |
| NOV |  | 713 | 529 | 614 | 691 | 467 | 807 | 585 | 603 | 581 | 621 |  |
| DEC |  | 570 | 502 | 599 | 565 | 554 | 564 | 649 | 597 | 560 | 573 |  |

## 


Table 2.3-99—\{Monthly and Annual Average Mixing Height Values (m)\}

## (Page 2 of 2)

| $\bigcirc$ |  | YEAR |  |  |  |  |  |  |  |  |  | Monthly Average | Annual <br> Average |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\underset{\mp}{\rightleftharpoons}$ | MONTH | 1996 | 1997 | 1998 | 1999 | 2000 | $\underline{2001}$ | $\underline{2002}$ | $\underline{2003}$ | $\underline{2004}$ | $\underline{2005}$ |  |  |
|  | JAN | 1971 |  | 1944 | 1525 | $\underline{2115}$ | $\underline{2003}$ | 1535 | $\underline{2404}$ | $\underline{2480}$ | 1830 | 1979 | $\underline{2452}$ |
|  | FEB | 2414 |  | 2099 | 2088 | 2141 | 1991 | 2090 | 1560 | $\underline{2118}$ | 1841 | 2038 |  |
|  | MAR | $\underline{2731}$ |  | $\underline{2736}$ | $\underline{2719}$ | $\underline{2529}$ | $\underline{2983}$ | $\underline{2104}$ | 1883 | $\underline{2489}$ | $\underline{2673}$ | $\underline{2539}$ |  |
|  | APR | 2863 |  | 3056 | 2804 | 2879 | 1959 | 2718 | 2372 | 2662 | 2652 | 2663 |  |
|  | MAY | 3269 |  | $\underline{2390}$ |  | $\underline{2658}$ | $\underline{2301}$ | 3111 | $\underline{2077}$ | $\underline{2498}$ | $\underline{2879}$ | $\underline{2648}$ |  |
|  | JUN | $\underline{2701}$ |  |  | 3192 | $\underline{2480}$ | $\underline{2835}$ | 3127 | $\underline{2500}$ | $\underline{2747}$ | $\underline{2937}$ | $\underline{2815}$ |  |
|  | JUL |  |  | $\underline{2917}$ | 3075 | $\underline{2814}$ | 3247 | 3347 | $\underline{2862}$ | $\underline{2737}$ | $\underline{2672}$ | $\underline{2959}$ |  |
|  | AUG |  |  | 3506 | 3312 | $\underline{2452}$ | $\underline{2651}$ | $\underline{3015}$ | $\underline{2589}$ | $\underline{2829}$ | $\underline{2886}$ | $\underline{2905}$ |  |
|  | SEP |  |  | 3085 | $\underline{2450}$ | 2296 | $\underline{2694}$ | 2342 | $\underline{2445}$ | 2221 | 3183 | $\underline{2589}$ |  |
|  | OCT |  | $\underline{2365}$ | $\underline{2836}$ | $\underline{2081}$ | $\underline{2405}$ | $\underline{2627}$ | $\underline{2294}$ | $\underline{2355}$ | $\underline{2045}$ | $\underline{2322}$ | 2370 |  |
|  | NOV |  | 2340 | 1734 | 2014 | 2266 | 1533 | 2647 | 1918 | 1979 | 1904 | 2037 |  |
|  | DEC |  | 1869 | 1647 | 1966 | 1853 | $\underline{1817}$ | 1849 | $\underline{2129}$ | 1959 | 1837 | 1881 |  |

Table 2.3-100—\{Monthly and Annual Average Mixing Height Values (ft) Not Used\}

|  | YEAR |  |  |  |  |  |  |  |  |  | Monthly Average | Annual Average |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MONTH | 1996 | 1997 | 1998 | 1999 | 2000 | 2001 | 2002 | 2003 | 2004 | 2005 |  |  |
| JAN | 1971 |  | 1944 | 1525 | 2115 | 2003 | 1535 | 2404 | 2480 | 1830 | 1979 | 2452 |
| FEB | 2414 |  | 2099 | 2088 | 2141 | 1991 | 2090 | 1560 | 2118 | 1841 | 2038 |  |
| MAR | 2731 |  | 2736 | 2719 | 2529 | 2983 | 2104 | 1883 | 2489 | 2673 | 2539 |  |
| APR | 2863 |  | 3056 | 2804 | 2879 | 1959 | 2718 | 2372 | 2662 | 2652 | 2663 |  |
| MAY | 3269 |  | 2390 |  | 2658 | 2301 | 3111 | 2077 | 2498 | 2879 | 2648 |  |
| UN | 2707 |  |  | 3192 | 2480 | 2835 | 3127 | 2500 | 2747 | 2937 | 2815 |  |
| Ut |  |  | 2917 | 3075 | 2814 | 3247 | 3347 | 2862 | 2737 | 2672 | 2959 |  |
| AUG |  |  | 3506 | 3312 | 2452 | 2651 | 3015 | 2589 | 2829 | 2886 | 2905 |  |
| SEP |  |  | 3085 | 2450 | 2296 | 2694 | 2342 | 2445 | 2221 | 3183 | 2589 |  |
| OCT |  | 2365 | 2836 | 2081 | 2405 | 2627 | 2294 | 2355 | 2045 | 2322 | 2370 |  |
| NOV |  | 2340 | 1734 | 2014 | 2266 | 1533 | 2647 | 1918 | 1979 | 1904 | 2037 |  |
| DEC |  | 1869 | 1647 | 1966 | 1853 | 1817 | 1849 | 2129 | 1959 | 1837 | 1881 |  |

Note: Empty cells denote no valid data.

Table 2.3-101—\{Temperature Inversion Frequency and Persistence, Year 2000\}

| DURATION (HOURS) | NUMBER OF OBSERVATIONS | PERCENT PROBABILITY |
| :---: | :---: | :---: |
| 1 | 96 | 22.91 |
| 2 | 53 | 35.56 |
| 3 | 33 | 43.44 |
| 4 | 32 | 51.07 |
| 5 | 17 | 55.13 |
| 6 | 18 | 59.43 |
| 7 | 15 | 63.01 |
| 8 | 13 | 66.11 |
| 9 | 13 | 69.21 |
| 10 | 16 | 73.03 |
| 11 | 20 | 77.80 |
| 12 | 27 | 84.25 |
| 13 | 23 | 89.74 |
| 14 | 19 | 94.27 |
| 15 | 12 | 97.14 |
| 16 | 7 | 98.81 |
| 17 | 4 | 99.76 |
| 18 | 0 | 99.76 |
| 19 | 0 | 99.76 |
| 20 | 1 | 100.00 |

THE LONGEST INVERSION LASTED 20 HOURS
OF THE LONGEST INVERSIONS, NUMBER 1 STARTED 14 HOURS INTO DAY 1.
THIRD COLUMN DEFINES THE PERCENT PROBABILITY THAT IF AN INVERSION OCCURS, ITS DURATION WILL BE LESS THAN THE NUMBER OF HOURS SPECIFIED

Table 2.3-102—\{Temperature Inversion Frequency and Persistence, Year 2001\}

| DURATION (HOURS) | NUMBER OF OBSERVATIONS | PERCENT PROBABILITY |
| :---: | :---: | :---: |
| 1 | 82 | 18.51 |
| 2 | 56 | 31.15 |
| 3 | 36 | 39.28 |
| 4 | 28 | 45.60 |
| 5 | 20 | 50.11 |
| 6 | 19 | 54.40 |
| 7 | 17 | 58.24 |
| 8 | 26 | 64.11 |
| 9 | 16 | 67.72 |
| 10 | 13 | 70.65 |
| 11 | 14 | 73.81 |
| 12 | 35 | 81.72 |
| 13 | 31 | 88.71 |
| 14 | 24 | 94.13 |
| 15 | 20 | 98.65 |
| 16 | 3 | 99.32 |
| 17 | 1 | 99.55 |
| 18 | 1 | 99.77 |
| 19 | 1100.00 |  |
| The longest inversion lasted 19 hours. <br> Of the longest inversions, number 1 started 16 hours into day 10 <br> Third column defines the percent probability that if an inversion occurs, its duration will be less than the number of hours specified |  |  |

Table 2.3-103-\{Temperature Inversion Frequency and Persistence, Year 2002\}

| DURATION (HOURS) | NUMBER OF OBSERVATIONS | PERCENT PROBABILITY |
| :---: | :---: | :---: |
| 1 | 92 | 21.80 |
| 2 | 38 | 30.81 |
| 3 | 41 | 40.52 |
| 4 | 25 | 46.45 |
| 5 | 19 | 50.95 |
| 6 | 14 | 54.27 |
| 7 | 21 | 59.24 |
| 8 | 19 | 63.74 |
| 9 | 16 | 67.54 |
| 10 | 21 | 72.51 |
| 11 | 24 | 78.20 |
| 12 | 34 | 86.26 |
| 13 | 12 | 89.10 |
| 14 | 13 | 92.18 |
| 15 | 25 | 98.10 |
| 16 | 7 | 99.76 |
| 17 | 1 | 100.00 |

The longest inversion lasted 17 hours.
Of the longest inversions, number 1 started 18 hours into day 323.
Third column defines the percent probability that if an inversion occurs, its duration will be less than the number of hours specified

Table 2.3-104—\{Temperature Inversion Frequency and Persistence, Year 2003\}

| DURATION (HOURS) | NUMBER OF OBSERVATIONS | PERCENT PROBABILITY |
| :---: | :---: | :---: |
| 1 | 113 | 24.30 |
| 2 | 72 | 39.78 |
| 3 | 33 | 46.88 |
| 4 | 42 | 55.91 |
| 5 | 14 | 58.92 |
| 6 | 22 | 63.66 |
| 7 | 17 | 67.31 |
| 8 | 14 | 70.32 |
| 9 | 11 | 72.69 |
| 10 | 14 | 75.70 |
| 11 | 13 | 78.49 |
| 12 | 19 | 82.58 |
| 13 | 20 | 86.88 |
| 14 | 26 | 92.47 |
| 15 | 23 | 97.42 |
| 16 | 8 | 99.14 |
| 17 | 1 | 99.35 |
| 18 | 1 | 99.57 |
| 19 | 1 | 99.78 |
| 20 | 1 | 100.00 |

The longest inversion lasted 20 hours.
Of the longest inversions, number 1 started 15 hours into day 76 .
Third column defines the percent probability that if an inversion occurs, its duration will be less than the number of hours specified.

Table 2.3-105—\{Temperature Inversion Frequency and Persistence, Year 2004\}

|  | DURATION <br> (HOURS) | NUMBER OF <br> OBSERVATIONS | PERCENT <br> PROBABILITY |
| :--- | :--- | :--- | :--- |
| 1 | 94 | 22.98 |  |
| 2 | 54 | 36.19 |  |
| 3 | 34 | 44.50 |  |
|  | 4 | 29 | 51.59 |
|  | 12 | 54.52 |  |
|  | 6 | 18 | 58.92 |
|  | 7 | 21 | 64.06 |
| 8 | 18 | 68.46 |  |
|  | 14 | 71.88 |  |
| 10 | 13 | 75.06 |  |
| 11 | 25 | 81.17 |  |
| 12 | 21 | 86.31 |  |
| 13 | 21 | 91.44 |  |
| 14 | 13 | 94.62 |  |
| 15 | 13 | 97.80 |  |
| 16 | 6 | 99.27 |  |
|  |  | 2 | 99.76 |
|  | 17 | 1 | 100.00 |

The longest inversion lasted 18 hours.
Of the longest inversions, number 1 started 18 hours into day 286.
Third column defines the percent probability that if an inversion occurs, its duration will be less than the number of hours specified

Table 2.3-106-\{Temperature Inversion Frequency and Persistence, Year 2005\}

| DURATION (HOURS) | NUMBER OF OBSERVATIONS | PERCENT PROBABILITY |
| :---: | :---: | :---: |
| 1 | 83 | 20.39 |
| 2 | 47 | 31.94 |
| 3 | 36 | 40.79 |
| 4 | 31 | 48.40 |
| 5 | 18 | 52.83 |
| 6 | 15 | 56.51 |
| 7 | 15 | 60.20 |
| 8 | 9 | 62.41 |
| 9 | 5 | 63.64 |
| 10 | 20 | 68.55 |
| 11 | 20 | 73.46 |
| 12 | 27 | 80.10 |
| 13 | 28 | 86.98 |
| 14 | 26 | 93.37 |
| 15 | 17 | 97.54 |
| 16 | 6 | 99.02 |
| 17 | 1 | 99.26 |
| 18 | 1 | 99.51 |
| 19 | 0 | 99.51 |
| 20 | 0 | 99.51 |
| 21 | 1 | 99.75 |
| 22 | 0 | 99.75 |
| 23 | 0 | 99.75 |
| 24 | 0 | 99.75 |
| 25 | 0 | 99.75 |
| 26 | 0 | 99.75 |
| 27 | 0 | 99.75 |
| 28 | 0 | 99.75 |
| 29 | 0 | 99.75 |
| 30 | 0 | 99.75 |
| 31 | 1 | 100.00 |
| The longest inversion lasted 31 hours. <br> Of the longest inversions, number 1 started 1 hours into day 12 <br> Third column defines the percent probability that if an inversion occurs, its duration will be less than the number of hours specified |  |  |

## Table 2.3-107—\{National Ambient Air Quality Standards\}

| Pollutant | Primary Stds. | Averaging Times | Secondary Stds. |
| :---: | :---: | :---: | :---: |
| Carbon Monoxide | $\begin{gathered} 9 \mathrm{ppm} \\ \left(10 \mathrm{mg} / \mathrm{m}^{3}\right) \end{gathered}$ | 8-hour(1) | None |
|  | $\begin{gathered} 35 \mathrm{ppm} \\ \left(40 \mathrm{mg} / \mathrm{m}^{3}\right) \end{gathered}$ | 1-hour(1) | None |
| Lead | $1.5 \mu \mathrm{~g} / \mathrm{m}^{3}$ | Quarterly Average | Same as Primary |
| Nitrogen Dioxide | $\begin{gathered} 0.053 \mathrm{ppm} \\ \left(100 \mu \mathrm{~g} / \mathrm{m}^{3}\right) \end{gathered}$ | Annual (Arithmetic Mean) | Same as Primary |
| Particulate Matter ( $\mathrm{PM}_{10}$ ) | Revoked(2) | Annual(2) (Arith. Mean) |  |
|  | $150 \mu \mathrm{~g} / \mathrm{m}^{3}$ | 24-hour(3) |  |
| Particulate Matter ( $\mathrm{PM}_{2.5}$ ) | $15.0 \mu \mathrm{~g} / \mathrm{m}^{3}$ | Annual(4) (Arith. Mean) | Same as Primary |
|  | $35 \mu \mathrm{~g} / \mathrm{m}^{3}$ | 24-hour(5) |  |
| Ozone | 0.08 ppm | 8-hour(6) | Same as Primary |
|  | 0.12 ppm | 1-hour(7) (Applies only in limited areas) | Same as Primary |
| Sulfur Oxides | 0.03 ppm | Annual (Arith. Mean) | ------- |
|  | 0.14 ppm | 24-hour(1) | ---- |
|  | ------- | 3-hour(1) | $\begin{gathered} 0.5 \mathrm{ppm} \\ \left(1300 \mu \mathrm{~g} / \mathrm{m}^{3}\right) \end{gathered}$ |

Notes:
(1)Not to be exceeded more than once per year.
(2)Due to a lack of evidence linking health problems to long-term exposure to coarse particle pollution, the agency revoked the annual PM10 standard in 2006 (effective December 17, 2006).
(3)Not to be exceeded more than once per year on average over 3 years.
(4)To attain this standard, the 3-year average of the weighted annual mean PM2.5 concentrations from single or multiple community-oriented monitors must not exceed $15.0 \mu \mathrm{~g} / \mathrm{m} 3$.
(5)To attain this standard, the 3-year average of the 98th percentile of 24-hour concentrations at each population-oriented monitor within an area must not exceed $35 \mu \mathrm{~g} / \mathrm{m} 3$ (effective December 17, 2006).
(6)To attain this standard, the 3-year average of the fourth-highest daily maximum 8 -hour average ozone concentrations measured at each monitor within an area over each year must not exceed 0.08 ppm .
(7)(a)The standard is attained when the expected number of days per calendar year with maximum hourly average concentrations above 0.12 ppm is $<1$, as determined by appendix H .
(b)As of June 15, 2005 EPA revoked the 1-hour ozone standard in all areas except the fourteen 8-hour ozone nonattainment Early Action Compact (EAC) Areas

## Table 2.3-108-\{Tower Instrument Specifications and Accuracies for Meteorological Monitoring Program (Preoperational and Operational)\}

| Characteristics | Requirements* | Specifications |
| :---: | :---: | :---: |
| Wind Speed Sensor |  |  |
| Accuracy | $\begin{gathered} \pm 0.2 \mathrm{~m} / \mathrm{s}( \pm 0.45 \mathrm{mph}) \\ \text { OR } \\ \pm 5 \% \text { of observed wind speed } \end{gathered}$ | $\pm 1 \%$ |
| Resolution | $0.1 \mathrm{~m} / \mathrm{s}$ ( 0.1 mph ) | 0.1 m/s |
| Wind Direction Sensor |  |  |
| Accuracy | $\pm 5$ degrees | $\pm 1.5$ degrees |
| Resolution | 1.0 degree | 1.0 degree |
| Temperature Sensors |  |  |
| Accuracy (ambient) | $\pm 0.5^{\circ} \mathrm{C}\left( \pm 0.9^{\circ} \mathrm{F}\right)$ | $\pm 0.05^{\circ} \mathrm{C}$ |
| Resolution (ambient) | $0.1^{\circ} \mathrm{C}\left(0.1^{\circ} \mathrm{F}\right)$ | $0.1{ }^{\circ} \mathrm{C}$ |
| Accuracy (vertical temperature difference) | $\pm 0.1^{\circ} \mathrm{C}\left( \pm 0.18^{\circ} \mathrm{F}\right)$ | $\pm 0.05^{\circ} \mathrm{C}$ |
| Resolution (vertical temperature difference) | $0.01^{\circ} \mathrm{C}\left(0.01^{\circ} \mathrm{F}\right)$ | $0.01{ }^{\circ} \mathrm{C}$ |
| Precipitation Sensor |  |  |
| Accuracy | $\pm 10 \%$ for a volume equivalent to 2.54 mm ( 0.1 in ) of precipitation at a rate $<50 \mathrm{~mm} / \mathrm{hr}(<2 \mathrm{in} / \mathrm{hr}$ ) | $\pm 1 \%$ |
| Resolution | 0.25 mm ( 0.01 in ) | 0.25 mm |
| Time |  |  |
| Accuracy | $\pm 5 \mathrm{~min}$ | $\pm 5 \mathrm{~min}$ |
| Resolution | 1 min | 1 min |
| Note: <br> * Accuracy and resolution criteria from Regulatory Guide 1.23, Revision 1 |  |  |

Table 2.3-109—\{Distances from Meteorological Tower to Nearby Obstructions to Air Flow\}

| Downwind Sector* | Approximate Distance miles (meters) |
| :---: | :---: |
| N | $0.25(402)$ |
| NNE | $0.33(531)$ |
| NE | $\mathrm{N} / \mathrm{A}^{* *}$ |
| ENE | $\mathrm{N} / \mathrm{A}^{* *}$ |
| E | $\mathrm{N} / \mathrm{A}^{* *}$ |
| ESE | $1(1609)$ |
| SE | $0.1(161)$ |
| SSE | $0.1(161)$ |
| S | $0.1(161)$ |
| SSW | $0.25(402)$ |
| SW | $0.33(531)$ |
| WSW | $0.1(161)$ |
| W | $0.25(402)$ |
| WNW | $0.33(531)$ |
| NW | $0.25(402)$ |
| NNW | $0.25(402)$ |

Notes:

* With respect to True North
** Lower than tower base elevation and therefore no possible obstructions

Table 2.3-110—\{Site-Specific EAB/LPZ Accident $\chi$ /Q Values for Ground Level Release\}

| Distance <br> Downwind <br> $(\mathbf{m i l e s})$ | $\mathbf{0 - 2}$ hours <br> $\chi / \mathbf{Q}$ <br> $\left(\mathbf{s e c} / \mathbf{m}^{\mathbf{3}}\right)$ | $\mathbf{2 - 8}$ hours <br> $\chi / \mathbf{Q}$ <br> $\left(\mathbf{s e c} / \mathbf{m}^{\mathbf{3}}\right)$ | $\mathbf{8 - 2 4}$ hours <br> $\chi / \mathbf{Q}$ <br> $\left(\mathbf{s e c} / \mathbf{m}^{\mathbf{3}}\right)$ | $\mathbf{1 - 4}$ days <br> $\left(\mathbf{s e c} / \mathbf{m}^{3}\right)$ | $\mathbf{4 - 3 0}$ days <br> $\chi / \mathbf{Q}$ <br> $\left(\mathbf{s e c} / \mathbf{m}^{3}\right)$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $0.5(\mathrm{EAB})$ | $6.914 \mathrm{E}-04$ | $4.131 \mathrm{E}-04$ | $2.609 \mathrm{E}-04$ | $1.289 \mathrm{E}-04$ | $4.686 \mathrm{E}-05$ |
| $1.5(\mathbf{L P Z})$ | $2.151 \mathrm{E}-04$ | $1.176 \mathrm{E}-04$ | $6.865 \mathrm{E}-05$ | $3.005 \mathrm{E}-05$ | $9.179 \mathrm{E}-06$ |

Table 2.3-111—\{Control Room/TSC $\chi /$ Q Values for Vent Stack Release $\}$

| Stack <br> Release | Wind Direction $=$ 0 $(\mathrm{~N})$ | Wind Direction $=$ 23 <br> (NNE) | Wind Direction $=$ 45 (NE) | Wind Direction $=$ 68 $(E N E)$ | Wind Direction $=$ 90 (E) | ```Wind Direction \(=\) 113 (ESE)``` | Wind Direction $=$ 135 (SE) | $\begin{gathered} \hline \text { Wind } \\ \text { Direction = } \\ 158 \\ \text { (SSE) } \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time Period | $\chi / \mathbf{Q}\left(\mathrm{sec} / \mathrm{m}^{\mathbf{3}}\right.$ ) | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \end{gathered}$ | $\chi / \mathbf{Q}\left(\mathbf{s e c} / \mathrm{m}^{3}\right)$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \end{gathered}$ |
| 0 to 2 hours | $1.43 \mathrm{E}-03$ | $1.40 \mathrm{E}-03$ | $1.38 \mathrm{E}-03$ | $1.35 \mathrm{E}-03$ | $1.29 \mathrm{E}-03$ | $1.28 \mathrm{E}-03$ | $1.36 \mathrm{E}-03$ | $1.47 \mathrm{E}-03$ |
| 2 to 8 hours | $1.20 \mathrm{E}-03$ | $1.16 \mathrm{E}-03$ | $1.14 \mathrm{E}-03$ | $1.03 \mathrm{E}-03$ | 7.85E-04 | 6.96E-04 | $8.60 \mathrm{E}-04$ | $1.11 \mathrm{E}-03$ |
| 8 to 24 hours | $4.64 \mathrm{E}-04$ | $4.84 \mathrm{E}-04$ | $4.64 \mathrm{E}-04$ | $3.74 \mathrm{E}-04$ | 3.00E-04 | $2.73 \mathrm{E}-04$ | $2.88 \mathrm{E}-04$ | $3.74 \mathrm{E}-04$ |
| 1 to 4 days | $3.16 \mathrm{E}-04$ | $3.23 \mathrm{E}-04$ | $3.11 \mathrm{E}-04$ | $2.62 \mathrm{E}-04$ | $2.08 \mathrm{E}-04$ | $1.99 \mathrm{E}-04$ | $2.19 \mathrm{E}-04$ | $2.64 \mathrm{E}-04$ |
| 4 to 30 days | $2.82 \mathrm{E}-04$ | $2.44 \mathrm{E}-04$ | $2.21 \mathrm{E}-04$ | $1.85 \mathrm{E}-04$ | $1.52 \mathrm{E}-04$ | $1.36 \mathrm{E}-04$ | $1.52 \mathrm{E}-04$ | $2.01 \mathrm{E}-04$ |
| Stack <br> Release | Wind Direction $=$ 180 $(\mathbf{S})$ | Wind Direction $=$ 203 $(S S W)$ | Wind Direction $=$ 225 $(S W)$ | Wind Direction $=$ 248 (WSW) | Wind Direction $=$ 270 $(W)$ | Wind Direction $=$ 293 (WNW) | Wind Direction $=$ 315 $(N W)$ | Wind Direction $=$ 338 (NNW) |
| Time Period | $\chi / \mathrm{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right)$ | $\chi / \mathrm{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right)$ | $\chi / \mathrm{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right)$ | $\chi / \mathrm{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right)$ | $\chi / \mathrm{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right)$ | $\chi / \mathrm{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right)$ | $\chi / \mathrm{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right)$ | $\chi / \mathrm{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right)$ |
| 0-2 hours | $1.73 \mathrm{E}-03$ | $1.81 \mathrm{E}-03$ | $1.81 \mathrm{E}-03$ | $1.80 \mathrm{E}-03$ | $1.72 \mathrm{E}-03$ | $1.62 \mathrm{E}-03$ | $1.60 \mathrm{E}-03$ | $1.54 \mathrm{E}-03$ |
| 2-8 hours | $1.38 \mathrm{E}-03$ | 1.55E-03 | $1.54 \mathrm{E}-03$ | $1.46 \mathrm{E}-03$ | $1.27 \mathrm{E}-03$ | $1.26 \mathrm{E}-03$ | $1.29 \mathrm{E}-03$ | $1.24 \mathrm{E}-03$ |
| 8-24 hours | $5.13 \mathrm{E}-04$ | 5.60E-04 | $5.38 \mathrm{E}-04$ | $4.97 \mathrm{E}-04$ | $4.58 \mathrm{E}-04$ | $4.88 \mathrm{E}-04$ | $4.93 \mathrm{E}-04$ | $4.75 \mathrm{E}-04$ |
| 1-4 days | $4.14 \mathrm{E}-04$ | 4.95E-04 | $4.77 \mathrm{E}-04$ | $4.50 \mathrm{E}-04$ | $3.71 \mathrm{E}-04$ | $3.49 \mathrm{E}-04$ | $3.46 \mathrm{E}-04$ | 3.32E-04 |
| 4-30 days | 3.19E-04 | 3.87E-04 | 3.77E-04 | $3.42 \mathrm{E}-04$ | 2.98E-04 | 2.93E-04 | 3.00E-04 | $3.06 \mathrm{E}-04$ |

Note:Bold entries identify maximum values in this table. SSW is the critical downwind sector.

Table 2.3-112—\{Control Room/TSC $\chi / \mathbf{Q}$ Values for Main Steam Relief Valve Release\}

| Main Steam Relief Valve Release | SG-4 to Div. 3 Air Intake Wind Direction = 203 (SSW) | SG-1 to Div. 3 Air Intake Wind Direction = 203 (SSW) | SG-3 to Div. 3 Air Intake Wind Direction = 203 (SSW) | SG-2 to Div. 3 Air Intake Wind Direction = 203 (SSW) |
| :---: | :---: | :---: | :---: | :---: |
| Time Period | $\chi / \mathrm{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right)$ | $\chi / \mathrm{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right)$ | $\chi / \mathrm{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right)$ | $\chi / \mathrm{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right)$ |
| 0-2 hours | $2.97 \mathrm{E}-03$ | $1.42 \mathrm{E}-03$ | $3.90 \mathrm{E}-03$ | $1.71 \mathrm{E}-03$ |
| 2-8 hours | $2.61 \mathrm{E}-03$ | $1.26 \mathrm{E}-03$ | 3.41E-03 | $1.50 \mathrm{E}-03$ |
| 8-24 hours | $9.41 \mathrm{E}-04$ | $4.53 \mathrm{E}-04$ | 1.23E-03 | $1.42 \mathrm{E}-04$ |
| 1-4 days | $8.18 \mathrm{E}-04$ | $3.94 \mathrm{E}-04$ | 1.07E-03 | $1.70 \mathrm{E}-04$ |
| 4-30 days | $6.42 \mathrm{E}-04$ | $3.11 \mathrm{E}-04$ | 8.39E-04 | $1.70 \mathrm{E}-04$ |

Note:Bold entries identify maximum values in this table. The critical wind direction sector was based on the stack releases in Table 2.3-110.

## Table 2.3-113-\{Control Room/TSC $\chi$ /Q Values for Safeguards Building Roof Release (via Safeguards Building Canopies)\}

| Safeguards Building Roof Release | Pt. 1 Wind Direction $=203$ (SSW) | Pt. 2 Wind Direction $=203$ (SSW) |
| :---: | :---: | :---: |
| Time Period | $\chi / \mathrm{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right)$ | $\chi / \mathrm{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right)$ |
| 0-2 hours | 5.88E-03 | $1.48 \mathrm{E}-03$ |
| 2-8 hours | 4.99E-03 | $1.29 \mathrm{E}-03$ |
| 8-24 hours | 1.95E-03 | $5.14 \mathrm{E}-04$ |
| 1-4 days | $1.60 \mathrm{E}-03$ | $4.09 \mathrm{E}-04$ |
| 4-30 days | $1.23 \mathrm{E}-03$ | $3.16 \mathrm{E}-04$ |

Notes:Bold entries identify maximum values in this table. The critical wind direction sector was based on the stack releases in Table 2.3-110.

Table 2.3-114—\{Control Room/TSC $\chi /$ Q Values for Equipment Hatch Release\}

| Equip. Hatch Release | Wind Direction $=\mathbf{2 0 3}$ <br> $(\mathbf{S S W})$ |
| :---: | :---: |
| Time Period | $\chi / \mathrm{Q}\left(\mathrm{sec} / \mathrm{m}^{\mathbf{3}}\right)$ |
| $0-2$ hours | $9.42 \mathrm{E}-04$ |
| $2-8$ hours | $8.10 \mathrm{E}-04$ |
| $8-24$ hours | $2.94 \mathrm{E}-04$ |
| $1-4$ days | $2.58 \mathrm{E}-04$ |
| $4-30$ days | $2.03 \mathrm{E}-04$ |

Note:The critical wind direction sector was based on the stack releases in Table 2.3-110

Table 2.3-115-\{Control Room/TSC $\chi$ /Q Values for Safeguards Building Depressurization Shaft Release\}

| Safeguards Building Depressurization Shaft Release | Wind Direction $=\mathbf{2 0 3}$ <br> $(\mathbf{S S W})$ |
| :---: | :---: |
| Time Period | $\chi / \mathrm{Q}\left(\mathrm{sec} / \mathrm{m}^{\mathbf{3}}\right)$ |
| $0-2$ hours | $3.98 \mathrm{E}-03$ |
| $2-8$ hours | $3.45 \mathrm{E}-03$ |
| $8-24$ hours | $1.37 \mathrm{E}-03$ |
| $1-4$ days | $1.09 \mathrm{E}-03$ |
| $4-30$ days | $8.32 \mathrm{E}-04$ |

Note:The critical wind direction sector was based on the stack releases in Table 2.3-110.

Table 2.3-116—\{50 ${ }^{\text {th }}$ Percentile $\chi / Q$ Values $\}$

| Time Period | $\chi / \mathbf{Q}\left(\mathbf{s e c} / \mathbf{m}^{\mathbf{3}}\right)$ | Receptor |
| :---: | :---: | :---: |
| $0-2$ hours | $8.079 \mathrm{E}-05$ | EAB |
| $0-2$ hours | $1.527 \mathrm{E}-05$ | LPZ |
| $2-8$ hours | $1.181 \mathrm{E}-05$ | LPZ |
| $8-24$ hours | $9.391 \mathrm{E}-06$ | LPZ |
| $24-96$ hours (1-4 days) | $6.607 \mathrm{E}-06$ | LPZ |
| $96-720$ hours (4-30 days) | $3.987 \mathrm{E}-06$ | LPZ |
| annual average | $2.150 \mathrm{E}-06$ | LPZ |

## Table 2.3-117—\{AEOLUS3 Design Input\}

| Parameter | Value(s) |
| :---: | :---: |
| Wind speed group upper limits for AEOLUS3 | $0.234,0.75,1.0,1.5,2.0,3.0,5.0,7.0,10.0,13.0,18.0,50.0$ meters/second |
| AEOLUS3 wind speed assigned to calms | 0.25 mph |
| Anemometer starting speed for the AEOLUS3 runs | 0.5 mph |
| The annual average mixing layer height at CC | 900 meters for accident analysis, 748 meters for normal effluent analysis <br> (Both are conservative, low values; 748 was used after purchase of data for one station from the National Climatic Data Center. The 900 meter value was determined by interpolation of data from many stations and may therefore be considered more accurate for the site.) |
| Temperature sensor separation | 50 meters |
| Wind instrument heights | 10 meters and 60 meters |
| CCNPP Unit 3 meteorological channel units of measure | Wind speed - miles per hour <br> Wind direction - degrees from True North <br> Delta Temperature - degrees Fahrenheit per sensor separation in feet |
| Stack flow rate for normal operations | 242,458 cfm |
| Stack inner diameter | 3.8 meters |
| Stack height | 62 meters (2 meters above assumed Reactor Building) |
| Reactor Building height and cross sectional area | 60 meters (used for cross sectional area for building wake - smaller height gives a lower credit for building wake; actual $=62.3$ meter) and $2940 \mathrm{~m}^{2}$ |
| Maximum Terrain Heights | Values in meters above plant grade |
| 0.5 miles | $0.0,0.0,0.0,0.0,16.8,19.8,22.9,22.9,19.8,29.0,29.0,25.9,32.0,22.9,22.9,19.8$ |
| 0.62 miles | $0.0,0.0,0.0,0.0,16.8,19.8,22.9,22.9,19.8,29.0,29.0,25.9,32.0,22.9,22.9,19.8$ |
| 1.5 miles | 0.0, 0.0, 0.0, 0.0, 16.8, 19.8, 25.9, 22.9, 25.9, 29.0, 29.0, 25.9,32.0, 25.9, 25.9, 19.8 |
| 2.5 miles | $0.0,0.0,0.0,0.0,16.8,19.8,25.9,25.9,25.9,29.0,29.0,25.9,32.0,25.9,25.9,19.8$ |
| 3.5 miles | $0.0,0.0,0.0,0.0,16.8,19.8,25.9,25.9,26.8,29.0,29.0,25.9,32.0,25.9,25.9,19.8$ |
| 4.5 miles | 0.0, 0.0, 0.0, 0.0, 16.8, 19.8, 25.9, 25.9, 26.8, 29.0, 29.0, 25.9, 32.0, 29.6, 25.9, 19.8 |
| 7.5 miles | $0.0,0.0,0.0,0.0,16.8,19.8,25.9,25.9,26.8,29.0,29.0,25.9,32.0,32.0,26.3,26.3$ |
| 15 miles | $0.0,0.0,0.0,0.0,16.8,19.8,25.9,25.9,26.8,29.0,29.0,26.3,44.3,32.0,27.3,43.3$ |
| 25 miles | $0.0,0.0,6.3,6.3,19.1,22.4,28.9,28.9,29.9,32.2,31.3,26.3,45.3,49.3,52.3,61.3$ |
| 35 miles | $6.3,1.3,6.3,6.3,19.1,22.4,28.9,28.9,29.9,32.2,39.3,46.3,45.3,51.3,66.3,61.3$ |
| 45 miles | $6.3,6.3,6.3,6.3,19.1,22.4,28.9,28.9,29.9,32.2,46.3,52.3,45.3,78.3,78.3,61.3$ |

Table 2.3-118—\{ARCON96 Design Inputs\}

| Minimum wind speed value | $0.5 \mathrm{~m} / \mathrm{sec}$ |
| :---: | :---: |
| Surface roughness | 0.2 |
| Sector averaging constant | 4.3 |
| Wind direction window | 90 degrees |
| Control Room air intake location employed in analysis | Intake closest to stack. |
| Control Room air intake elevation | 32.1 meters (Mid-point of intake) |
| Control Room air intake horizontal distance to stack base | 69.0 meters (scaled) |
| Control Room air intake horizontal distance to Main Steam Relief Train, via Silencer (referred to as the Silencer release point in the present application): |  |
| SG-4 Silencer to MCR Div. 3 Air Intake (AI) | 53.0 meters |
| SG-3 Silencer to MCR Div. 3 AI | 46.0 meters |
| SG-1 Silencer to MCR Div. 3 AI | 78.0 meters |
| SG-2 Silencer to MCR Div. 3 AI | 71.0 meters |
| Control Room air intake horizontal distances to Canopy exhausts (referred to as the Canopy release point in the present application) |  |
| 1) Near depressurization shaft (Safeguard Building Div. 4) | 30.1 meters (scaled) |
| 2) Southeast side of SAB Div. 4 | 65.3 meters (scaled) |
| Control Room air intake horizontal distance to Material Lock (for the Equipment Hatch release) | 97.5 meters (scaled) |
| Control Room air intake horizontal distance to the depressurization shaft of Safeguard Building Div. 4 (referred to as the depressurization shaft release point in the present application) | 31.4 meters (scaled) |
| Site grade elevation | 0 meters |
| Release heights used |  |
| Silencer | 33.9 meters |
| Stack | 32.1 meters |
| Canopy Pt. 1 | 15.5 meters |
| Canopy Pt. 2 | 11.5 meters elevation |
| Material Lock (for Equipment Hatch release) | 23.2 meters <br> (release height employed in analysis = 32.1 meters, conservative) |
| Depressurization Shaft | 7 meters |

Table 2．3－119—\｛Normal Effluent Annual Average，Undecayed，Undepleted $\chi$／Q Values for Mixed Mode Release Using 242，458 cfm Flow Rate for Grid Receptors\}
（Page 1 of 2）

| Downwind Sector | $\begin{gathered} \hline \chi / \mathrm{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 0.5 \text { miles } \end{gathered}$ | $\begin{gathered} \hline \chi / \mathrm{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 0.75 \text { miles } \end{gathered}$ | $\begin{gathered} \chi / \mathrm{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 1.0 \text { mile } \end{gathered}$ | $\begin{gathered} \chi / Q\left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 1.5 \text { miles } \end{gathered}$ | $\begin{gathered} \chi / \mathrm{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 2.0 \text { miles } \end{gathered}$ | $\begin{gathered} \hline \chi / \mathrm{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 2.5 \text { miles } \end{gathered}$ | $\begin{gathered} \hline \chi / \mathrm{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 3.0 \text { miles } \end{gathered}$ | $\begin{gathered} \hline \chi / \mathrm{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 3.5 \text { miles } \end{gathered}$ | $\begin{gathered} \hline \chi / Q\left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 4.0 \text { miles } \end{gathered}$ | $\begin{gathered} \hline \chi / \mathrm{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 4.5 \text { miles } \end{gathered}$ | $\begin{gathered} \hline \chi / \mathbf{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 5.0 \text { miles } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N | 1．923E－06 | 1．065E－06 | $5.811 \mathrm{E}-07$ | $2.571 \mathrm{E}-07$ | $1.538 \mathrm{E}-07$ | $1.055 \mathrm{E}-07$ | $8.046 \mathrm{E}-08$ | $6.401 \mathrm{E}-08$ | $5.261 \mathrm{E}-08$ | $4.482 \mathrm{E}-08$ | $3.881 \mathrm{E}-08$ |
| NNE | 3．287E－06 | $1.754 \mathrm{E}-06$ | $9.348 \mathrm{E}-07$ | 3．980E－07 | $2.333 \mathrm{E}-07$ | $1.584 \mathrm{E}-07$ | $1.201 \mathrm{E}-07$ | $9.528 \mathrm{E}-08$ | 7．821E－08 | $6.663 \mathrm{E}-08$ | 5．773E－08 |
| NE | $5.039 \mathrm{E}-06$ | $2.711 \mathrm{E}-06$ | $1.443 \mathrm{E}-06$ | $6.059 \mathrm{E}-07$ | $3.491 \mathrm{E}-07$ | $2.334 \mathrm{E}-07$ | $1.748 \mathrm{E}-07$ | $1.372 \mathrm{E}-07$ | $1.117 \mathrm{E}-07$ | $9.446 \mathrm{E}-08$ | 8．134E－08 |
| ENE | $2.038 \mathrm{E}-06$ | $1.090 \mathrm{E}-06$ | 5．855E－07 | $2.525 \mathrm{E}-07$ | $1.491 \mathrm{E}-07$ | $1.017 \mathrm{E}-07$ | $7.731 \mathrm{E}-08$ | $6.142 \mathrm{E}-08$ | $5.048 \mathrm{E}-08$ | $4.303 \mathrm{E}-08$ | $3.731 \mathrm{E}-08$ |
| E | $1.516 \mathrm{E}-06$ | $8.448 \mathrm{E}-07$ | $4.715 \mathrm{E}-07$ | $2.135 \mathrm{E}-07$ | $1.287 \mathrm{E}-07$ | $8.848 \mathrm{E}-08$ | $6.751 \mathrm{E}-08$ | $5.374 \mathrm{E}-08$ | $4.421 \mathrm{E}-08$ | $3.773 \mathrm{E}-08$ | $3.273 \mathrm{E}-08$ |
| ESE | 1．987E－06 | $1.123 \mathrm{E}-06$ | 6．238E－07 | $2.761 \mathrm{E}-07$ | $1.627 \mathrm{E}-07$ | $1.099 \mathrm{E}-07$ | 8．269E－08 | $6.509 \mathrm{E}-08$ | $5.305 \mathrm{E}-08$ | $4.489 \mathrm{E}-08$ | $3.866 \mathrm{E}-08$ |
| SE | $2.416 \mathrm{E}-06$ | $1.464 \mathrm{E}-06$ | $8.347 \mathrm{E}-07$ | 3．833E－07 | $2.214 \mathrm{E}-07$ | $1.458 \mathrm{E}-07$ | $1.072 \mathrm{E}-07$ | $8.261 \mathrm{E}-08$ | $6.606 \mathrm{E}-08$ | $5.495 \mathrm{E}-08$ | $4.660 \mathrm{E}-08$ |
| SSE | $1.381 \mathrm{E}-06$ | $8.911 \mathrm{E}-07$ | 5．240E－07 | $2.393 \mathrm{E}-07$ | $1.396 \mathrm{E}-07$ | $9.489 \mathrm{E}-08$ | $6.969 \mathrm{E}-08$ | $5.363 \mathrm{E}-08$ | $4.280 \mathrm{E}-08$ | 3．554E－08 | 3．008E－08 |
| S | $1.815 \mathrm{E}-06$ | $1.127 \mathrm{E}-06$ | $6.501 \mathrm{E}-07$ | 3．095E－07 | $1.771 \mathrm{E}-07$ | $1.155 \mathrm{E}-07$ | $8.420 \mathrm{E}-08$ | $6.481 \mathrm{E}-08$ | $5.148 \mathrm{E}-08$ | $4.256 \mathrm{E}-08$ | $3.589 \mathrm{E}-08$ |
| SSW | 1．599E－06 | 1．050E－06 | $6.224 \mathrm{E}-07$ | 2．824E－07 | 1．628E－07 | $1.066 \mathrm{E}-07$ | $7.786 \mathrm{E}-08$ | 5．963E－08 | $4.741 \mathrm{E}-08$ | 3．922E－08 | $3.308 \mathrm{E}-08$ |
| SW | $1.557 \mathrm{E}-06$ | $1.013 \mathrm{E}-06$ | 5．897E－07 | $2.619 \mathrm{E}-07$ | $1.496 \mathrm{E}-07$ | $9.750 \mathrm{E}-08$ | 7．102E－08 | $5.432 \mathrm{E}-08$ | $4.314 \mathrm{E}-08$ | $3.568 \mathrm{E}-08$ | $3.009 \mathrm{E}-08$ |
| WSW | $1.053 \mathrm{E}-06$ | 7．219E－07 | $4.396 \mathrm{E}-07$ | $2.056 \mathrm{E}-07$ | $1.204 \mathrm{E}-07$ | $7.956 \mathrm{E}-08$ | $5.843 \mathrm{E}-08$ | $4.492 \mathrm{E}-08$ | 3．580E－08 | $2.968 \mathrm{E}-08$ | $2.508 \mathrm{E}-08$ |
| W | $6.742 \mathrm{E}-07$ | $5.085 \mathrm{E}-07$ | 3．282E－07 | $1.627 \mathrm{E}-07$ | 9．803E－08 | $6.584 \mathrm{E}-08$ | $4.888 \mathrm{E}-08$ | 3．787E－08 | $3.036 \mathrm{E}-08$ | $2.528 \mathrm{E}-08$ | $2.143 \mathrm{E}-08$ |
| WNW | $4.529 \mathrm{E}-07$ | 3．122E－07 | 2．012E－07 | $1.108 \mathrm{E}-07$ | $6.956 \mathrm{E}-08$ | $4.823 \mathrm{E}-08$ | $3.671 \mathrm{E}-08$ | $2.902 \mathrm{E}-08$ | $2.365 \mathrm{E}-08$ | $2.079 \mathrm{E}-08$ | $1.781 \mathrm{E}-08$ |
| NW | 6．608E－07 | $4.337 \mathrm{E}-07$ | $2.685 \mathrm{E}-07$ | $1.399 \mathrm{E}-07$ | 8．563E－08 | $5.846 \mathrm{E}-08$ | $4.403 \mathrm{E}-08$ | 3．454E－08 | $2.799 \mathrm{E}-08$ | $2.353 \mathrm{E}-08$ | $2.012 \mathrm{E}-08$ |
| NNW | $1.586 \mathrm{E}-06$ | $9.808 \mathrm{E}-07$ | 5．737E－07 | $2.658 \mathrm{E}-07$ | $1.580 \mathrm{E}-07$ | 1．062E－07 | 7．933E－08 | $6.190 \mathrm{E}-08$ | $4.999 \mathrm{E}-08$ | $4.193 \mathrm{E}-08$ | $3.580 \mathrm{E}-08$ |

Table 2.3-119—\{Normal Effluent Annual Average, Undecayed, Undepleted $\epsilon / \mathbb{Q} /$ /Q Values for Mixed Mode Release Using 242,458 cfm Flow Rate for Grid Receptors\}
(Page 2 of 2)

| Downwind Sector | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 7.5 \mathrm{miles}^{2} \end{gathered}$ | $\begin{gathered} \chi / \mathrm{Q} \\ \left(\mathrm{sec}^{3} / \mathrm{m}^{3}\right) \\ 10 \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \end{gathered}$ $15 \text { mile }$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 20 \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 25 \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 30 \text { miles } \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 35 \text { miles } \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 40 \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 45 \text { miles } \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 50 \mathrm{miles} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N | 2.217E-08 | $1.608 \mathrm{E}-08$ | $1.013 \mathrm{E}-08$ | $7.265 \mathrm{E}-09$ | 5.602E-09 | $4.526 \mathrm{E}-09$ | $3.937 \mathrm{E}-09$ | $3.363 \mathrm{E}-09$ | $2.926 \mathrm{E}-09$ | $2.584 \mathrm{E}-09$ |
| NNE | $3.321 \mathrm{E}-08$ | $2.429 \mathrm{E}-08$ | $1.555 \mathrm{E}-08$ | 1.129E-08 | 8.797E-09 | 7.170E-09 | 6.090E-09 | 5.239E-09 | $4.773 \mathrm{E}-09$ | $4.236 \mathrm{E}-09$ |
| NE | $4.586 \mathrm{E}-08$ | $3.318 \mathrm{E}-08$ | $2.099 \mathrm{E}-08$ | $1.515 \mathrm{E}-08$ | $1.236 \mathrm{E}-08$ | $1.005 \mathrm{E}-08$ | $8.434 \mathrm{E}-09$ | 7.247E-09 | $6.340 \mathrm{E}-09$ | $5.625 \mathrm{E}-09$ |
| ENE | $2.152 \mathrm{E}-08$ | $1.580 \mathrm{E}-08$ | $1.018 \mathrm{E}-08$ | $7.445 \mathrm{E}-09$ | 6.198E-09 | 5.078E-09 | $4.290 \mathrm{E}-09$ | 3.706E-09 | 3.258E-09 | 2.903E-09 |
| E | $1.892 \mathrm{E}-08$ | $1.390 \mathrm{E}-08$ | 8.963E-09 | 6.547E-09 | 5.263E-09 | $4.304 \mathrm{E}-09$ | 3.629E-09 | 3.129E-09 | $2.746 \mathrm{E}-09$ | $2.443 \mathrm{E}-09$ |
| ESE | $2.176 \mathrm{E}-08$ | $1.570 \mathrm{E}-08$ | 9.870E-09 | 7.089E-09 | 5.615E-09 | $4.546 \mathrm{E}-09$ | $3.802 \mathrm{E}-09$ | $3.257 \mathrm{E}-09$ | $2.841 \mathrm{E}-09$ | $2.514 \mathrm{E}-09$ |
| SE | $2.468 \mathrm{E}-08$ | $1.706 \mathrm{E}-08$ | $1.011 \mathrm{E}-08$ | 6.975E-09 | 5.294E-09 | 4.183E-09 | $3.429 \mathrm{E}-09$ | 2.888E-09 | 2.482E-09 | $2.169 \mathrm{E}-09$ |
| SSE | $1.578 \mathrm{E}-08$ | $1.081 \mathrm{E}-08$ | $6.328 \mathrm{E}-09$ | $4.322 \mathrm{E}-09$ | 3.249E-09 | 2.550E-09 | $2.079 \mathrm{E}-09$ | $1.743 \mathrm{E}-09$ | $1.492 \mathrm{E}-09$ | $1.299 \mathrm{E}-09$ |
| S | $1.862 \mathrm{E}-08$ | $1.270 \mathrm{E}-08$ | 7.407E-09 | 5.053E-09 | 3.791E-09 | 2.977E-09 | $2.429 \mathrm{E}-09$ | 2.037E-09 | $1.746 \mathrm{E}-09$ | 1.522E-09 |
| SSW | $1.716 \mathrm{E}-08$ | $1.170 \mathrm{E}-08$ | 6.808E-09 | $4.636 \mathrm{E}-09$ | $3.470 \mathrm{E}-09$ | 2.721E-09 | $2.217 \mathrm{E}-09$ | 1.857E-09 | $1.590 \mathrm{E}-09$ | $1.385 \mathrm{E}-09$ |
| SW | $1.562 \mathrm{E}-08$ | $1.065 \mathrm{E}-08$ | 6.206E-09 | $4.230 \mathrm{E}-09$ | 3.169E-09 | 2.487E-09 | $2.078 \mathrm{E}-09$ | $1.741 \mathrm{E}-09$ | $1.519 \mathrm{E}-09$ | $1.322 \mathrm{E}-09$ |
| WSW | $1.306 \mathrm{E}-08$ | 8.908E-09 | 5.187E-09 | 3.526E-09 | $2.614 \mathrm{E}-09$ | 2.048E-09 | $1.779 \mathrm{E}-09$ | $1.486 \mathrm{E}-09$ | $1.290 \mathrm{E}-09$ | $1.120 \mathrm{E}-09$ |
| W | $1.128 \mathrm{E}-08$ | $7.736 \mathrm{E}-09$ | 4.767E-09 | $3.231 \mathrm{E}-09$ | 2.399E-09 | 1.876E-09 | $1.525 \mathrm{E}-09$ | $1.275 \mathrm{E}-09$ | 1.089E-09 | $9.469 \mathrm{E}-10$ |
| WNW | $9.934 \mathrm{E}-09$ | 6.957E-09 | $4.180 \mathrm{E}-09$ | 2.903E-09 | $2.411 \mathrm{E}-09$ | $1.901 \mathrm{E}-09$ | $1.571 \mathrm{E}-09$ | $1.321 \mathrm{E}-09$ | $1.234 \mathrm{E}-09$ | $1.074 \mathrm{E}-09$ |
| NW | $1.095 \mathrm{E}-08$ | 7.658E-09 | 4.619E-09 | $3.201 \mathrm{E}-09$ | $2.677 \mathrm{E}-09$ | $2.106 \mathrm{E}-09$ | $1.789 \mathrm{E}-09$ | $1.499 \mathrm{E}-09$ | $1.309 \mathrm{E}-09$ | $1.139 \mathrm{E}-09$ |
| NNW | $2.036 \mathrm{E}-08$ | $1.421 \mathrm{E}-08$ | 9.444E-09 | $6.507 \mathrm{E}-09$ | 5.273E-09 | $4.148 \mathrm{E}-09$ | 3.389E-09 | 2.847E-09 | 2.442E-09 | 2.130E-09 |

Table 2.3-120-\{Normal Effluent Annual Average, Undecayed, UnDdepleted $\epsilon / Q_{\chi} / \mathrm{Q}$
Values for Mixed Mode Release Using 242,458 cfm Flow Rate for Special and Additional Receptors\}

| Downwind <br> Sector | $\chi / \mathbf{Q}\left(\mathbf{s e c} / \mathbf{m}^{\mathbf{3}}\right)$ <br> Site Boundary | $\chi / \mathbf{Q}\left(\mathbf{s e c} / \mathbf{m}^{\mathbf{3}}\right)$ <br> Nearest Residents | $\chi / \mathbf{Q}\left(\mathbf{s e c} / \mathbf{m}^{\mathbf{3}}\right)$ <br> Nearest Gardens |
| :---: | :---: | :---: | :---: |
| N | $2.885 \mathrm{E}-06$ | $\mathrm{~N} / \mathrm{A}$ | $\mathrm{N} / \mathrm{A}$ |
| NNE | $9.558 \mathrm{E}-06$ | $\mathrm{~N} / \mathrm{A}$ | $\mathrm{N} / \mathrm{A}$ |
| NE | $1.379 \mathrm{E}-05$ | $\mathrm{~N} / \mathrm{A}$ | $\mathrm{N} / \mathrm{A}$ |
| ENE | $4.991 \mathrm{E}-06$ | $\mathrm{~N} / \mathrm{A}$ | $\mathrm{N} / \mathrm{A}$ |
| E | $2.778 \mathrm{E}-06$ | $\mathrm{~N} / \mathrm{A}$ | $\mathrm{N} / \mathrm{A}$ |
| ESE | $2.486 \mathrm{E}-06$ | $\mathrm{~N} / \mathrm{A}$ | $\mathrm{N} / \mathrm{A}$ |
| SE | $1.076 \mathrm{E}-06$ | $3.0228 .707 \mathrm{E}-07$ | $3.0228 .707 \mathrm{E}-07$ |
| SSE | $5.252 \mathrm{E}-07$ | $3.1593 .545 \mathrm{E}-07$ | $3.1593 .054 \mathrm{E}-07$ |
| S | $8.681 \mathrm{E}-07$ | $2.1803 .717 \mathrm{E}-07$ | $2.1803 .717 \mathrm{E}-07$ |
| SSW | $8.366 \mathrm{E}-07$ | $2.824 \mathrm{E}-07 \mathrm{~N} / \mathrm{A}$ | $2.228 \mathrm{E}-07 \underline{\mathrm{~N} / \mathrm{A}}$ |
| SW | $4.960 \mathrm{E}-07$ | $4.8994 .040 \mathrm{E}-07$ | $4.899 \mathrm{E}-073.009 \mathrm{E}-07$ |
| WSW | $4.1523 .802 \mathrm{E}-07$ | $3.1374 .279 \mathrm{E}-07$ | $2.0564 .279 \mathrm{E}-07$ |
| W | $2.914 \mathrm{E}-07$ | $2.0982 .129 \mathrm{E}-07$ | $7.6271 .495 \mathrm{E}-07$ |
| WNW | $1.127 \mathrm{E}-07$ | $4.823 \mathrm{E}-081.053 \mathrm{E}-07$ | $4.8238 .776 \mathrm{E}-08$ |
| NW | $2.545 \mathrm{E}-07$ | $7.9005 .686 \mathrm{E}-08$ | $7.9005 .686 \mathrm{E}-08$ |
| NNW | $1.699 \mathrm{E}-06$ |  | $\mathrm{~N} / \mathrm{A}$ |

Table 2.3-121—\{Normal Effluent Annual Average, Depleted $\epsilon / Q \chi / Q$ Values for Mixed Mode Release Using 242,458 cfm Flow Rate for Grid Receptors\}

| Downwind Sector | $\begin{gathered} \chi / \mathrm{Q} \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 0.5 \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / \mathrm{Q} \\ \left(\mathrm{sec}^{3} / \mathrm{m}^{3}\right) \\ \mathbf{0 . 7 5} \mathbf{~ m i l e s} \end{gathered}$ | $\begin{gathered} \chi / \mathrm{Q} \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ \mathbf{1 . 0} \mathrm{mile} \end{gathered}$ | $\begin{gathered} \chi / \mathrm{Q} \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ \mathbf{1 . 5} \mathbf{~ m i l e s} \end{gathered}$ | $\begin{gathered} \chi / \mathrm{Q} \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ \mathbf{2 . 0} \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / \mathrm{Q} \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 2.5 \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / \mathrm{Q} \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 3.0 \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 3.5 \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / \mathrm{Q} \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 4.0 \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / \mathrm{Q} \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 4.5 \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / \mathrm{Q} \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 5.0 \mathrm{miles} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N | 1.760E-06 | $9.545 \mathrm{E}-07$ | $5.149 \mathrm{E}-07$ | $2.253 \mathrm{E}-07$ | $1.340 \mathrm{E}-07$ | $9.153 \mathrm{E}-08$ | $6.951 \mathrm{E}-08$ | $5.510 \mathrm{E}-08$ | $4.513 \mathrm{E}-08$ | 3.833E-08 | $3.308 \mathrm{E}-08$ |
| NNE | 3.008E-06 | 1.570E-06 | 8.255E-07 | 3.458E-07 | 2.007E-07 | $1.353 \mathrm{E}-07$ | $1.020 \mathrm{E}-07$ | 8.050E-08 | $6.579 \mathrm{E}-08$ | 5.582E-08 | $4.818 \mathrm{E}-08$ |
| NE | $4.614 \mathrm{E}-06$ | $2.427 \mathrm{E}-06$ | $1.274 \mathrm{E}-06$ | 5.254E-07 | $2.990 \mathrm{E}-07$ | $1.980 \mathrm{E}-07$ | $1.470 \mathrm{E}-07$ | $1.146 \mathrm{E}-07$ | $9.272 \mathrm{E}-08$ | 7.798E-08 | $6.680 \mathrm{E}-08$ |
| ENE | 1.870E-06 | $9.791 \mathrm{E}-07$ | 5.199E-07 | 2.212E-07 | $1.295 \mathrm{E}-07$ | $8.772 \mathrm{E}-08$ | $6.629 \mathrm{E}-08$ | $5.240 \mathrm{E}-08$ | $4.287 \mathrm{E}-08$ | 3.639E-08 | 3.142E-08 |
| E | $1.392 \mathrm{E}-06$ | 7.627E-07 | $4.229 \mathrm{E}-07$ | $1.902 \mathrm{E}-07$ | $1.141 \mathrm{E}-07$ | 7.811E-08 | 5.935E-08 | $4.707 \mathrm{E}-08$ | 3.860E-08 | 3.283E-08 | 2.839E-08 |
| ESE | $1.823 \mathrm{E}-06$ | 1.013E-06 | 5.585E-07 | $2.449 \mathrm{E}-07$ | $1.433 \mathrm{E}-07$ | $9.622 \mathrm{E}-08$ | 7.202E-08 | $5.641 \mathrm{E}-08$ | $4.578 \mathrm{E}-08$ | 3.859E-08 | $3.311 \mathrm{E}-08$ |
| SE | $2.220 \mathrm{E}-06$ | 1.328E-06 | 7.531E-07 | 3.439E-07 | $1.970 \mathrm{E}-07$ | $1.287 \mathrm{E}-07$ | $9.395 \mathrm{E}-08$ | 7.192E-08 | $5.715 \mathrm{E}-08$ | $4.727 \mathrm{E}-08$ | $3.986 \mathrm{E}-08$ |
| SSE | $1.272 \mathrm{E}-06$ | $8.145 \mathrm{E}-07$ | $4.778 \mathrm{E}-07$ | $2.168 \mathrm{E}-07$ | $1.255 \mathrm{E}-07$ | 8.487E-08 | 6.189E-08 | $4.730 \mathrm{E}-08$ | 3.752E-08 | 3.097E-08 | $2.606 \mathrm{E}-08$ |
| S | $1.680 \mathrm{E}-06$ | 1.033E-06 | 5.933E-07 | $2.816 \mathrm{E}-07$ | $1.596 \mathrm{E}-07$ | $1.032 \mathrm{E}-07$ | $7.458 \mathrm{E}-08$ | $5.698 \mathrm{E}-08$ | $4.493 \mathrm{E}-08$ | 3.689E-08 | $3.091 \mathrm{E}-08$ |
| SSW | $1.491 \mathrm{E}-06$ | $9.745 \mathrm{E}-07$ | $5.766 \mathrm{E}-07$ | 2.596E-07 | $1.484 \mathrm{E}-07$ | 9.633E-08 | $6.978 \mathrm{E}-08$ | 5.303E-08 | $4.186 \mathrm{E}-08$ | 3.439E-08 | 2.883E-08 |
| SW | $1.449 \mathrm{E}-06$ | $9.378 \mathrm{E}-07$ | $5.444 \mathrm{E}-07$ | $2.396 \mathrm{E}-07$ | $1.356 \mathrm{E}-07$ | $8.756 \mathrm{E}-08$ | $6.325 \mathrm{E}-08$ | $4.799 \mathrm{E}-08$ | 3.784E-08 | 3.108E-08 | $2.604 \mathrm{E}-08$ |
| WSW | $9.797 \mathrm{E}-07$ | $6.711 \mathrm{E}-07$ | 4.089E-07 | $1.901 \mathrm{E}-07$ | $1.104 \mathrm{E}-07$ | 7.237E-08 | 5.272E-08 | $4.022 \mathrm{E}-08$ | 3.183E-08 | $2.621 \mathrm{E}-08$ | $2.201 \mathrm{E}-08$ |
| W | $6.324 \mathrm{E}-07$ | $4.789 \mathrm{E}-07$ | $3.101 \mathrm{E}-07$ | $1.533 \mathrm{E}-07$ | $9.180 \mathrm{E}-08$ | $6.126 \mathrm{E}-08$ | $4.520 \mathrm{E}-08$ | $3.480 \mathrm{E}-08$ | $2.774 \mathrm{E}-08$ | $2.297 \mathrm{E}-08$ | $1.938 \mathrm{E}-08$ |
| WNW | $4.205 \mathrm{E}-07$ | 2.897E-07 | $1.876 \mathrm{E}-07$ | $1.039 \mathrm{E}-07$ | 6.502E-08 | $4.490 \mathrm{E}-08$ | $3.403 \mathrm{E}-08$ | $2.678 \mathrm{E}-08$ | $2.174 \mathrm{E}-08$ | 1.909E-08 | $1.629 \mathrm{E}-08$ |
| NW | $6.130 \mathrm{E}-07$ | $4.005 \mathrm{E}-07$ | $2.485 \mathrm{E}-07$ | $1.299 \mathrm{E}-07$ | 7.919E-08 | $5.382 \mathrm{E}-08$ | $4.035 \mathrm{E}-08$ | 3.151E-08 | 2.542E-08 | $2.128 \mathrm{E}-08$ | $1.812 \mathrm{E}-08$ |
| NNW | $1.462 \mathrm{E}-06$ | 8.954E-07 | $5.225 \mathrm{E}-07$ | $2.408 \mathrm{E}-07$ | $1.423 \mathrm{E}-07$ | 9.513E-08 | 7.063E-08 | $5.481 \mathrm{E}-08$ | $4.404 \mathrm{E}-08$ | 3.676E-08 | 3.125E-08 |

Table 2.3-122—\{Normal Effluent Annual Average, Depleted $\epsilon / Q \chi / Q$ Values for Mixed Mode Release Using 242,458 cfm Flow Rate for Grid Receptors 7.5 mi to 50 mi

| Downwind Sector | $\begin{gathered} \chi / \mathrm{Q} \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ \mathbf{7 . 5} \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 10 \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 15 \mathrm{mile} \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 20 \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 25 \text { miles } \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 30 \text { miles } \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 35 \text { miles } \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 40 \text { miles } \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 45 \text { miles } \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 50 \mathrm{miles} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N | $1.868 \mathrm{E}-08$ | $1.340 \mathrm{E}-08$ | $8.305 \mathrm{E}-09$ | $5.878 \mathrm{E}-09$ | $4.485 \mathrm{E}-09$ | $3.591 \mathrm{E}-09$ | $3.132 \mathrm{E}-09$ | $2.657 \mathrm{E}-09$ | $2.298 \mathrm{E}-09$ | $2.017 \mathrm{E}-09$ |
| NNE | $2.736 \mathrm{E}-08$ | $1.978 \mathrm{E}-08$ | $1.244 \mathrm{E}-08$ | 8.912E-09 | 6.869E-09 | 5.547E-09 | $4.687 \mathrm{E}-09$ | $4.003 \mathrm{E}-09$ | 3.668E-09 | 3.235E-09 |
| NE | 3.698E-08 | $2.634 \mathrm{E}-08$ | $1.628 \mathrm{E}-08$ | $1.156 \mathrm{E}-08$ | 9.443E-09 | 7.597E-09 | $6.315 \mathrm{E}-09$ | $5.381 \mathrm{E}-09$ | $4.672 \mathrm{E}-09$ | $4.115 \mathrm{E}-09$ |
| ENE | $1.788 \mathrm{E}-08$ | $1.297 \mathrm{E}-08$ | $8.214 \mathrm{E}-09$ | $5.928 \mathrm{E}-09$ | $4.961 \mathrm{E}-09$ | $4.034 \mathrm{E}-09$ | $3.383 \mathrm{E}-09$ | 2.904E-09 | 2.539E-09 | 2.250E-09 |
| E | $1.625 \mathrm{E}-08$ | $1.183 \mathrm{E}-08$ | 7.532E-09 | $5.449 \mathrm{E}-09$ | $4.371 \mathrm{E}-09$ | 3.552E-09 | $2.977 \mathrm{E}-09$ | $2.554 \mathrm{E}-09$ | $2.231 \mathrm{E}-09$ | $1.975 \mathrm{E}-09$ |
| ESE | $1.839 \mathrm{E}-08$ | $1.311 \mathrm{E}-08$ | 8.101E-09 | $5.743 \mathrm{E}-09$ | 4.529E-09 | 3.635E-09 | $3.016 \mathrm{E}-09$ | $2.565 \mathrm{E}-09$ | 2.224E-09 | $1.957 \mathrm{E}-09$ |
| SE | 2.067E-08 | $1.403 \mathrm{E}-08$ | 8.084E-09 | $5.456 \mathrm{E}-09$ | $4.081 \mathrm{E}-09$ | $3.176 \mathrm{E}-09$ | $2.567 \mathrm{E}-09$ | 2.135E-09 | $1.815 \mathrm{E}-09$ | $1.569 \mathrm{E}-09$ |
| SSE | $1.337 \mathrm{E}-08$ | 8.997E-09 | $5.116 \mathrm{E}-09$ | 3.418E-09 | 2.529E-09 | $1.956 \mathrm{E}-09$ | $1.572 \mathrm{E}-09$ | $1.302 \mathrm{E}-09$ | $1.102 \mathrm{E}-09$ | $9.494 \mathrm{E}-10$ |
| S | 1.562E-08 | $1.041 \mathrm{E}-08$ | 5.855E-09 | 3.883E-09 | 2.851E-09 | 2.195E-09 | $1.755 \mathrm{E}-09$ | $1.446 \mathrm{E}-09$ | $1.219 \mathrm{E}-09$ | 1.046E-09 |
| SSW | $1.457 \mathrm{E}-08$ | 9.706E-09 | 5.448E-09 | 3.606E-09 | 2.639E-09 | 2.027E-09 | $1.617 \mathrm{E}-09$ | 1.330E-09 | $1.120 \mathrm{E}-09$ | $9.590 \mathrm{E}-10$ |
| SW | $1.317 \mathrm{E}-08$ | 8.790E-09 | 4.952E-09 | 3.289E-09 | 2.415E-09 | $1.861 \mathrm{E}-09$ | 1.537E-09 | $1.268 \mathrm{E}-09$ | $1.093 \mathrm{E}-09$ | $9.369 \mathrm{E}-10$ |
| WSW | $1.117 \mathrm{E}-08$ | 7.458E-09 | 4.203E-09 | $2.785 \mathrm{E}-09$ | 2.022E-09 | $1.556 \mathrm{E}-09$ | $1.345 \mathrm{E}-09$ | $1.106 \mathrm{E}-09$ | $9.432 \mathrm{E}-10$ | $8.070 \mathrm{E}-10$ |
| W | 9.991E-09 | 6.734E-09 | $4.058 \mathrm{E}-09$ | 2.695E-09 | $1.968 \mathrm{E}-09$ | 1.517E-09 | $1.216 \mathrm{E}-09$ | 1.004E-09 | $8.487 \mathrm{E}-10$ | 7.291E-10 |
| WNW | 8.964E-09 | 6.202E-09 | 3.658E-09 | $2.505 \mathrm{E}-09$ | 2.078E-09 | $1.624 \mathrm{E}-09$ | $1.329 \mathrm{E}-09$ | $1.107 \mathrm{E}-09$ | $9.486 \mathrm{E}-10$ | 8.114E-10 |
| NW | 9.709E-09 | $6.696 \mathrm{E}-09$ | 3.954E-09 | $2.695 \mathrm{E}-09$ | 2.244E-09 | 1.742E-09 | $1.426 \mathrm{E}-09$ | 1.175E-09 | $9.615 \mathrm{E}-10$ | $8.199 \mathrm{E}-10$ |
| NNW | 1.757E-08 | $1.208 \mathrm{E}-08$ | 7.968E-09 | 5.395E-09 | 4.271E-09 | 3.304E-09 | $2.657 \mathrm{E}-09$ | 2.194E-09 | 1.853E-09 | 1.592E-09 |

Table 2.3-123-\{Normal Effluent Annual Average, Depleted $\epsilon / Q \chi / Q$ Values for Mixed Mode Release Using 242,458 cfm Flow Rate for Special and Additional Receptors\}

| Downwind Sector | $\chi / \mathrm{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right)$ <br> Site Boundary | $\chi / Q\left(\sec / \mathbf{m}^{3}\right)$ <br> Nearest Residents | $\chi / \mathbf{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right)$ <br> Nearest Gardens |
| :---: | :---: | :---: | :---: |
| N | $2.677 \mathrm{E}-06$ | N/A | N/A |
| NNE | $9.030 \mathrm{E}-06$ | N/A | N/A |
| NE | $1.301 \mathrm{E}-05$ | N/A | N/A |
| ENE | $4.701 \mathrm{E}-06$ | N/A | N/A |
| E | $2.597 \mathrm{E}-06$ | N/A | N/A |
| ESE | $2.298 \mathrm{E}-06$ | N/A | N/A |
| SE | $9.733 \mathrm{E}-07$ | 2.7027.859E-07 | 2.7027.859E-07 |
| SSE | $4.789 \mathrm{E}-07$ | $2.8693 .223 \mathrm{E}-07$ | $2.8692 .773 \mathrm{E}-07$ |
| S | $7.939 \mathrm{E}-07$ | $1.9723 .389 \mathrm{E}-07$ | $1.9723 .389 \mathrm{E}-07$ |
| SSW | $7.759 \mathrm{E}-07$ | 2.596E-07N/A | $2.041 \mathrm{E}-07 \mathrm{~N} / \mathrm{A}$ |
| SW | $4.573 \mathrm{E}-07$ | $4.5163 .717 \mathrm{E}-07$ | $4.5162 .758 \mathrm{E}-07$ |
| WSW | $3.8613 .534 \mathrm{E}-07$ | $2.9133 .980 \mathrm{E}-07$ | 1.9013.980E-07 |
| W | $2.753 \mathrm{E}-07$ | 1.9802.009E-07 | 1.5331.407E-07 |
| WNW | $1.054 \mathrm{E}-07$ | 4.4909.872E-08 | $4.4908 .218 \mathrm{E}-08$ |
| NW | $2.356 \mathrm{E}-07$ | $7.3005 .233 \mathrm{E}-08$ | $7.3005 .233 \mathrm{E}-08$ |
| NNW | $1.570 \mathrm{E}-06$ | N/A | N/A |

Table 2．3－124—\｛CCNPP Unit 3 Normal Effluent Annual Average，Gamma $\epsilon / Q \chi / Q$ Values for Mixed Mode Release Using 242，458 cfm Flow Rate for Grid Receptors\}

| Downwind Sector | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 0.5 \mathrm{miles} \end{gathered}$ | $\chi / \mathrm{Q}$ $\left(\mathrm{sec} / \mathrm{m}^{3}\right)$ $\mathbf{0 . 7 5}$ miles | $\begin{gathered} \chi / \mathrm{Q} \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 1.0 \mathrm{mile} \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ \mathbf{1 . 5} \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ \mathbf{2 . 0} \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 2.5 \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 3.0 \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / \mathrm{Q} \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 3.5 \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / \mathrm{Q} \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 4.0 \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 4.5 \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 5.0 \mathrm{miles} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N | $1.415 \mathrm{E}-06$ | 9．137E－07 | $5.319 \mathrm{E}-07$ | $2.442 \mathrm{E}-07$ | $1.460 \mathrm{E}-07$ | $9.939 \mathrm{E}-08$ | 7．527E－08 | 5．957E－08 | $4.877 \mathrm{E}-08$ | $4.143 \mathrm{E}-08$ | $3.580 \mathrm{E}-08$ |
| NNE | $2.160 \mathrm{E}-06$ | 1．379E－06 | 7．991E－07 | 3．647E－07 | 2．176E－07 | $1.481 \mathrm{E}-07$ | $1.123 \mathrm{E}-07$ | 8．900E－08 | 7．299E－08 | 6．212E－08 | 5．377E－08 |
| NE | 3．100E－06 | 1．968E－06 | $1.135 \mathrm{E}-06$ | 5．133E－07 | 3．040E－07 | 2．057E－07 | $1.552 \mathrm{E}-07$ | $1.226 \mathrm{E}-07$ | 1．002E－07 | 8．505E－08 | 7．345E－08 |
| ENE | $1.504 \mathrm{E}-06$ | 9．617E－07 | 5．580E－07 | $2.548 \mathrm{E}-07$ | 1．519E－07 | $1.034 \mathrm{E}-07$ | 7．835E－08 | $6.210 \mathrm{E}-08$ | 5．093E－08 | $4.335 \mathrm{E}-08$ | 3．752E－08 |
| E | $1.270 \mathrm{E}-06$ | $8.198 \mathrm{E}-07$ | 4．771E－07 | 2．182E－07 | $1.299 \mathrm{E}-07$ | $8.814 \mathrm{E}-08$ | $6.661 \mathrm{E}-08$ | $5.265 \mathrm{E}-08$ | $4.308 \mathrm{E}-08$ | 3．659E－08 | 3．162E－08 |
| ESE | $1.470 \mathrm{E}-06$ | $9.407 \mathrm{E}-07$ | $5.436 \mathrm{E}-07$ | 2．457E－07 | $1.449 \mathrm{E}-07$ | $9.760 \mathrm{E}-08$ | $7.331 \mathrm{E}-08$ | $5.765 \mathrm{E}-08$ | $4.696 \mathrm{E}-08$ | 3．972E－08 | 3．420E－08 |
| SE | $1.716 \mathrm{E}-06$ | 1．100E－06 | $6.334 \mathrm{E}-07$ | $2.878 \mathrm{E}-07$ | $1.671 \mathrm{E}-07$ | $1.109 \mathrm{E}-07$ | $8.221 \mathrm{E}-08$ | 6．389E－08 | 5．150E－08 | $4.315 \mathrm{E}-08$ | $3.683 \mathrm{E}-08$ |
| SSE | $1.113 \mathrm{E}-06$ | $7.248 \mathrm{E}-07$ | $4.199 \mathrm{E}-07$ | $1.884 \mathrm{E}-07$ | $1.097 \mathrm{E}-07$ | 7．407E－08 | $5.484 \mathrm{E}-08$ | $4.255 \mathrm{E}-08$ | $3.424 \mathrm{E}-08$ | $2.864 \mathrm{E}-08$ | $2.440 \mathrm{E}-08$ |
| S | $1.453 \mathrm{E}-06$ | $9.258 \mathrm{E}-07$ | 5．304E－07 | $2.428 \mathrm{E}-07$ | $1.394 \mathrm{E}-07$ | $9.163 \mathrm{E}-08$ | $6.741 \mathrm{E}-08$ | $5.224 \mathrm{E}-08$ | $4.188 \mathrm{E}-08$ | 3．490E－08 | $2.965 \mathrm{E}-08$ |
| SSW | $1.370 \mathrm{E}-06$ | 8．780E－07 | $5.041 \mathrm{E}-07$ | $2.225 \mathrm{E}-07$ | $1.279 \mathrm{E}-07$ | $8.412 \mathrm{E}-08$ | 6．187E－08 | $4.777 \mathrm{E}-08$ | $3.828 \mathrm{E}-08$ | $3.190 \mathrm{E}-08$ | 2．709E－08 |
| SW | $1.286 \mathrm{E}-06$ | $8.259 \mathrm{E}-07$ | 4．729E－07 | 2．081E－07 | $1.194 \mathrm{E}-07$ | 7．843E－08 | $5.763 \mathrm{E}-08$ | $4.445 \mathrm{E}-08$ | 3．559E－08 | 2．964E－08 | $2.516 \mathrm{E}-08$ |
| WSW | $1.004 \mathrm{E}-06$ | $6.576 \mathrm{E}-07$ | 3．815E－07 | $1.707 \mathrm{E}-07$ | 9．890E－08 | $6.536 \mathrm{E}-08$ | $4.821 \mathrm{E}-08$ | $3.728 \mathrm{E}-08$ | $2.990 \mathrm{E}-08$ | $2.493 \mathrm{E}-08$ | $2.118 \mathrm{E}-08$ |
| W | $8.038 \mathrm{E}-07$ | 5．327E－07 | 3．119E－07 | $1.414 \mathrm{E}-07$ | $8.256 \mathrm{E}-08$ | 5．487E－08 | $4.065 \mathrm{E}-08$ | 3．154E－08 | $2.537 \mathrm{E}-08$ | $2.120 \mathrm{E}-08$ | $1.805 \mathrm{E}-08$ |
| WNW | 5．959E－07 | 3．950E－07 | $2.331 \mathrm{E}-07$ | $1.108 \mathrm{E}-07$ | 6．573E－08 | $4.426 \mathrm{E}-08$ | $3.315 \mathrm{E}-08$ | 2．597E－08 | $2.105 \mathrm{E}-08$ | $1.811 \mathrm{E}-08$ | $1.550 \mathrm{E}-08$ |
| NW | 7．179E－07 | 4．689E－07 | 2．742E－07 | $1.283 \mathrm{E}-07$ | 7．546E－08 | $5.053 \mathrm{E}-08$ | $3.771 \mathrm{E}-08$ | $2.945 \mathrm{E}-08$ | $2.383 \mathrm{E}-08$ | 2．003E－08 | $1.714 \mathrm{E}-08$ |
| NNW | $1.365 \mathrm{E}-06$ | 8．820E－07 | $5.114 \mathrm{E}-07$ | $2.308 \mathrm{E}-07$ | $1.352 \mathrm{E}-07$ | $9.033 \mathrm{E}-08$ | $6.731 \mathrm{E}-08$ | 5．253E－08 | $4.249 \mathrm{E}-08$ | 3．570E－08 | 3．054E－08 |

Table 2.3-125—\{CCNPP Unit 3 Normal Effluent Annual Average, Gamma $\epsilon / Q \chi / Q$ Values for Mixed Mode Release Using 242,458 cfm Flow Rate for Grid Receptors\}

| Downwind Sector | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 7.5 \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / \mathrm{Q} \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 10 \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 15 \mathrm{mile} \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 20 \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 25 \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 30 \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 35 \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec}^{3} / \mathrm{m}^{3}\right) \\ 40 \mathrm{miles} \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 45 \text { miles } \end{gathered}$ | $\begin{gathered} \chi / Q \\ \left(\mathrm{sec} / \mathrm{m}^{3}\right) \\ 50 \mathrm{miles} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N | $2.036 \mathrm{E}-08$ | $1.475 \mathrm{E}-08$ | $9.307 \mathrm{E}-09$ | $6.685 \mathrm{E}-09$ | 5.162E-09 | $4.175 \mathrm{E}-09$ | $3.577 \mathrm{E}-09$ | 3.058E-09 | $2.663 \mathrm{E}-09$ | $2.353 \mathrm{E}-09$ |
| NNE | 3.084E-08 | 2.253E-08 | $1.439 \mathrm{E}-08$ | $1.044 \mathrm{E}-08$ | 8.122E-09 | 6.613E-09 | 5.590E-09 | $4.805 \mathrm{E}-09$ | $4.301 \mathrm{E}-09$ | 3.815E-09 |
| NE | $4.181 \mathrm{E}-08$ | 3.040E-08 | $1.933 \mathrm{E}-08$ | $1.398 \mathrm{E}-08$ | $1.119 \mathrm{E}-08$ | 9.095E-09 | $7.631 \mathrm{E}-09$ | $6.554 \mathrm{E}-09$ | 5.730E-09 | 5.082E-09 |
| ENE | $2.155 \mathrm{E}-08$ | $1.577 \mathrm{E}-08$ | $1.011 \mathrm{E}-08$ | 7.357E-09 | 5.953E-09 | 4.856E-09 | 4.087E-09 | 3.519E-09 | 3.084E-09 | $2.741 \mathrm{E}-09$ |
| E | $1.803 \mathrm{E}-08$ | $1.313 \mathrm{E}-08$ | $8.360 \mathrm{E}-09$ | $6.056 \mathrm{E}-09$ | $4.773 \mathrm{E}-09$ | 3.885E-09 | $3.264 \mathrm{E}-09$ | 2.806E-09 | $2.456 \mathrm{E}-09$ | 2.180E-09 |
| ESE | $1.924 \mathrm{E}-08$ | $1.387 \mathrm{E}-08$ | $8.715 \mathrm{E}-09$ | 6.254E-09 | $4.890 \mathrm{E}-09$ | 3.957E-09 | 3.308E-09 | 2.833E-09 | $2.471 \mathrm{E}-09$ | $2.186 \mathrm{E}-09$ |
| SE | $2.001 \mathrm{E}-08$ | $1.407 \mathrm{E}-08$ | 8.532E-09 | 5.968E-09 | $4.548 \mathrm{E}-09$ | 3.620E-09 | 2.985E-09 | $2.526 \mathrm{E}-09$ | 2.179E-09 | $1.911 \mathrm{E}-09$ |
| SSE | $1.314 \mathrm{E}-08$ | 9.172E-09 | 5.492E-09 | 3.804E-09 | 2.874E-09 | 2.273E-09 | $1.864 \mathrm{E}-09$ | $1.569 \mathrm{E}-09$ | $1.348 \mathrm{E}-09$ | $1.178 \mathrm{E}-09$ |
| S | $1.582 \mathrm{E}-08$ | $1.099 \mathrm{E}-08$ | 6.561E-09 | $4.538 \mathrm{E}-09$ | 3.423E-09 | 2.707E-09 | $2.220 \mathrm{E}-09$ | $1.870 \mathrm{E}-09$ | $1.608 \mathrm{E}-09$ | $1.405 \mathrm{E}-09$ |
| SSW | $1.443 \mathrm{E}-08$ | $1.001 \mathrm{E}-08$ | 5.965E-09 | 4.119E-09 | 3.102E-09 | 2.450E-09 | 2.007E-09 | $1.689 \mathrm{E}-09$ | $1.452 \mathrm{E}-09$ | $1.268 \mathrm{E}-09$ |
| SW | $1.337 \mathrm{E}-08$ | $9.260 \mathrm{E}-09$ | 5.497E-09 | 3.787E-09 | 2.846E-09 | $2.246 \mathrm{E}-09$ | $1.861 \mathrm{E}-09$ | $1.564 \mathrm{E}-09$ | $1.355 \mathrm{E}-09$ | $1.183 \mathrm{E}-09$ |
| WSW | $1.127 \mathrm{E}-08$ | 7.797E-09 | 4.617E-09 | $3.171 \mathrm{E}-09$ | 2.366E-09 | 1.862E-09 | $1.570 \mathrm{E}-09$ | $1.316 \mathrm{E}-09$ | $1.136 \mathrm{E}-09$ | 9.889E-10 |
| W | 9.675E-09 | 6.726E-09 | $4.121 \mathrm{E}-09$ | $2.832 \mathrm{E}-09$ | 2.118E-09 | $1.668 \mathrm{E}-09$ | $1.363 \mathrm{E}-09$ | $1.144 \mathrm{E}-09$ | $9.811 \mathrm{E}-10$ | 8.553E-10 |
| WNW | 8.582E-09 | $6.046 \mathrm{E}-09$ | 3.667E-09 | $2.563 \mathrm{E}-09$ | 2.033E-09 | $1.614 \mathrm{E}-09$ | $1.333 \mathrm{E}-09$ | $1.125 \mathrm{E}-09$ | $1.007 \mathrm{E}-09$ | 8.809E-10 |
| NW | $9.389 \mathrm{E}-09$ | 6.622E-09 | 4.036E-09 | $2.823 \mathrm{E}-09$ | 2.258E-09 | 1.791E-09 | $1.501 \mathrm{E}-09$ | $1.266 \mathrm{E}-09$ | $1.100 \mathrm{E}-09$ | $9.619 \mathrm{E}-10$ |
| NNW | $1.718 \mathrm{E}-08$ | $1.212 \mathrm{E}-08$ | 7.752E-09 | $5.412 \mathrm{E}-09$ | 4.238E-09 | 3.366E-09 | $2.772 \mathrm{E}-09$ | $2.343 \mathrm{E}-09$ | 2.020E-09 | 1.770E-09 |

Table 2.3-126-\{Normal Effluent Annual Average, Gamma $\epsilon / \mathbb{Q} \chi / Q$ Values for Mixed Mode Release Using 242,458 cfm Flow Rate for Special and Additional Receptors\}

| Downwind Sector | $\chi / \mathbf{Q}\left(\mathbf{s e c} / \mathrm{m}^{3}\right)$ Site Boundary | $\chi / \mathbf{Q}\left(\mathbf{s e c} / \mathbf{m}^{3}\right)$ <br> Nearest Residents | $\chi / \mathbf{Q}\left(\mathrm{sec} / \mathrm{m}^{3}\right)$ <br> Nearest Gardens |
| :---: | :---: | :---: | :---: |
| N | 1.872E-06 | N/A | N/A |
| NNE | $4.043 \mathrm{E}-06$ | N/A | N/A |
| NE | $5.769 \mathrm{E}-06$ | N/A | N/A |
| ENE | $2.580 \mathrm{E}-06$ | N/A | N/A |
| E | $1.905 \mathrm{E}-06$ | N/A | N/A |
| ESE | $1.733 \mathrm{E}-06$ | N/A | N/A |
| SE | $8.150 \mathrm{E}-07$ | $2.2736 .605 \mathrm{E}-07$ | 2.2736.605E-07 |
| SSE | $4.208 \mathrm{E}-07$ | 2.4982.810E-07 | 2.4982.413E-07 |
| S | $7.118 \mathrm{E}-07$ | 1.7122.919E-07 | 1.7122.919E-07 |
| SSW | $6.895 \mathrm{E}-07$ | $2.225 \mathrm{E}-07 \mathrm{~N} / \mathrm{A}$ | $2.225 \mathrm{E}-07 \mathrm{~N} / \mathrm{A}$ |
| SW | $3.963 \mathrm{E}-07$ | $3.9143 .218 \mathrm{E}-07$ | $3.9142 .391 \mathrm{E}-07$ |
| WSW | 3.5863.261E-07 | $2.6573 .705 \mathrm{E}-07$ | $2.6573 .705 \mathrm{E}-07$ |
| W | $2.712 \mathrm{E}-07$ | 1.8691.900E-07 | 1.8691.290E-07 |
| WNW | $1.171 \mathrm{E}-07$ | $4.426 \mathrm{E}-081.046 \mathrm{E}-07$ | $4.4268 .503 \mathrm{E}-08$ |
| NW | $2.580 \mathrm{E}-07$ | $6.9274 .910 \mathrm{E}-08$ | $6.9274 .910 \mathrm{E}-08$ |
| NNW | $1.447 \mathrm{E}-06$ | N/A | N/A |

Table 2.3-127—\{Normal Effluent Annual Average, D/Q Values for Mixed Mode Release Using 242,458 cfm Flow Rate for Grid Receptors\}

| Downwind Sector | D/Q $\left(1 / \mathrm{m}^{2}\right)$ 0.5 miles | $\begin{gathered} \hline \text { D/Q } \\ \left(1 / \mathrm{m}^{2}\right) \\ 0.75 \text { miles } \end{gathered}$ | $\begin{gathered} \text { D/Q } \\ \left(1 / \mathrm{m}^{2}\right) \\ 1.0 \mathrm{mile} \end{gathered}$ | D/Q $\left(1 / \mathrm{m}^{2}\right)$ 1.5 miles | D/Q $\left(1 / \mathrm{m}^{2}\right)$ 2.0 miles | $\begin{gathered} \hline \text { D/Q } \\ \left(1 / \mathrm{m}^{2}\right) \\ 2.5 \text { miles } \end{gathered}$ | $\begin{gathered} \hline \text { D/Q } \\ \left(1 / \mathrm{m}^{2}\right) \\ 3.0 \text { miles } \end{gathered}$ | $\begin{gathered} \hline \text { D/Q } \\ \left(1 / \mathrm{m}^{2}\right) \\ 3.5 \text { miles } \end{gathered}$ | $\begin{gathered} \hline \text { D/Q } \\ \left(1 / \mathrm{m}^{2}\right) \\ 4.0 \text { miles } \end{gathered}$ | $\begin{gathered} \mathrm{D} / \mathrm{Q} \\ \left(1 / \mathrm{m}^{2}\right) \\ 4.5 \text { miles } \end{gathered}$ | $\begin{gathered} \mathrm{D} / \mathrm{Q} \\ \left(1 / \mathrm{m}^{2}\right) \\ 5.0 \text { miles } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N | 1.322E-08 | $7.391 \mathrm{E}-09$ | 3.875E-09 | 1.472E-09 | 7.661E-10 | $4.653 \mathrm{E}-10$ | $3.197 \mathrm{E}-10$ | $2.322 \mathrm{E}-10$ | $1.759 \mathrm{E}-10$ | $1.390 \mathrm{E}-10$ | $1.123 \mathrm{E}-10$ |
| NNE | $2.145 \mathrm{E}-08$ | $1.177 \mathrm{E}-08$ | 6.016E-09 | 2.219E-09 | $1.135 \mathrm{E}-09$ | 6.822E-10 | 4.657E-10 | $3.368 \mathrm{E}-10$ | $2.545 \mathrm{E}-10$ | $2.008 \mathrm{E}-10$ | $1.622 \mathrm{E}-10$ |
| NE | 3.792E-08 | $2.075 \mathrm{E}-08$ | 1.057E-08 | 3.879E-09 | 1.977E-09 | $1.184 \mathrm{E}-09$ | $8.068 \mathrm{E}-10$ | $5.829 \mathrm{E}-10$ | $4.402 \mathrm{E}-10$ | $3.472 \mathrm{E}-10$ | 2.804E-10 |
| ENE | $1.588 \mathrm{E}-08$ | $8.994 \mathrm{E}-09$ | 4.695E-09 | $1.763 \mathrm{E}-09$ | 9.143E-10 | $5.545 \mathrm{E}-10$ | $3.812 \mathrm{E}-10$ | $2.773 \mathrm{E}-10$ | $2.105 \mathrm{E}-10$ | 1.666E-10 | 1.349E-10 |
| E | $1.203 \mathrm{E}-08$ | $6.702 \mathrm{E}-09$ | 3.472E-09 | $1.305 \mathrm{E}-09$ | $6.721 \mathrm{E}-10$ | 4.053E-10 | $2.774 \mathrm{E}-10$ | $2.010 \mathrm{E}-10$ | $1.522 \mathrm{E}-10$ | 1.202E-10 | $9.720 \mathrm{E}-11$ |
| ESE | $1.987 \mathrm{E}-08$ | $1.081 \mathrm{E}-08$ | 5.498E-09 | 2.033E-09 | 1.032E-09 | $6.158 \mathrm{E}-10$ | $4.181 \mathrm{E}-10$ | $3.012 \mathrm{E}-10$ | $2.270 \mathrm{E}-10$ | 1.787E-10 | $1.441 \mathrm{E}-10$ |
| SE | 2.758E-08 | $1.520 \mathrm{E}-08$ | 7.823E-09 | 2.943E-09 | $1.496 \mathrm{E}-09$ | 8.920E-10 | $6.051 \mathrm{E}-10$ | $4.355 \mathrm{E}-10$ | $3.280 \mathrm{E}-10$ | $2.582 \mathrm{E}-10$ | $2.081 \mathrm{E}-10$ |
| SSE | 1.508E-08 | 8.770E-09 | 4.717E-09 | $1.846 \mathrm{E}-09$ | 9.593E-10 | 5.823E-10 | 3.982E-10 | 2.882E-10 | $2.179 \mathrm{E}-10$ | $1.721 \mathrm{E}-10$ | 1.390E-10 |
| S | 2.818E-08 | $1.604 \mathrm{E}-08$ | 8.446E-09 | 3.275E-09 | 1.690E-09 | 1.018E-09 | $6.966 \mathrm{E}-10$ | $5.050 \mathrm{E}-10$ | 3.822E-10 | $3.021 \mathrm{E}-10$ | $2.443 \mathrm{E}-10$ |
| SSW | $2.181 \mathrm{E}-08$ | $1.271 \mathrm{E}-08$ | 6.802E-09 | 2.649E-09 | $1.380 \mathrm{E}-09$ | $8.371 \mathrm{E}-10$ | $5.751 \mathrm{E}-10$ | $4.180 \mathrm{E}-10$ | $3.172 \mathrm{E}-10$ | $2.511 \mathrm{E}-10$ | 2.033E-10 |
| SW | $2.151 \mathrm{E}-08$ | $1.255 \mathrm{E}-08$ | 6.719E-09 | $2.616 \mathrm{E}-09$ | 1.357E-09 | 8.192E-10 | 5.607E-10 | $4.063 \mathrm{E}-10$ | $3.075 \mathrm{E}-10$ | $2.431 \mathrm{E}-10$ | 1.966E-10 |
| WSW | $1.199 \mathrm{E}-08$ | 7.502E-09 | 4.250E-09 | 1.740E-09 | $9.261 \mathrm{E}-10$ | 5.680E-10 | $3.929 \mathrm{E}-10$ | 2.867E-10 | $2.179 \mathrm{E}-10$ | $1.729 \mathrm{E}-10$ | 1.400E-10 |
| W | 6.673E-09 | $4.317 \mathrm{E}-09$ | $2.510 \mathrm{E}-09$ | 1.053E-09 | 5.700E-10 | 3.537E-10 | $2.466 \mathrm{E}-10$ | $1.810 \mathrm{E}-10$ | 1.382E-10 | 1.098E-10 | $8.910 \mathrm{E}-11$ |
| WNW | 4.775E-09 | $3.015 \mathrm{E}-09$ | 1.737E-09 | 7.306E-10 | 3.965E-10 | $2.468 \mathrm{E}-10$ | $1.724 \mathrm{E}-10$ | $1.267 \mathrm{E}-10$ | $9.681 \mathrm{E}-11$ | $7.725 \mathrm{E}-11$ | 6.266E-11 |
| NW | 8.120E-09 | $4.833 \mathrm{E}-09$ | 2.646E-09 | $1.061 \mathrm{E}-09$ | 5.619E-10 | 3.445E-10 | $2.384 \mathrm{E}-10$ | $1.741 \mathrm{E}-10$ | $1.326 \mathrm{E}-10$ | 1.052E-10 | 8.525E-11 |
| NNW | $1.920 \mathrm{E}-08$ | $1.103 \mathrm{E}-08$ | 5.871E-09 | 2.275E-09 | 1.184E-09 | 7.177E-10 | 4.927E-10 | $3.578 \mathrm{E}-10$ | $2.712 \mathrm{E}-10$ | $2.145 \mathrm{E}-10$ | $1.735 \mathrm{E}-10$ |

Table 2．3－128－\｛Normal Effluent Annual Average，D／Q Values for Mixed Mode Release Using 242，458 cfm Flow Rate for Grid Receptors\}

| Downwind Sector | D／Q $\left(1 / \mathrm{m}^{2}\right)$ 7.5 miles | D／Q $\left(1 / \mathrm{m}^{2}\right)$ 10 miles | D／Q $\left(1 / \mathrm{m}^{2}\right)$ 15 mile | $\begin{gathered} \hline \text { D/Q } \\ \left(1 / \mathrm{m}^{2}\right) \\ 20 \mathrm{miles} \end{gathered}$ | $\begin{gathered} \hline \text { D/Q } \\ \left(1 / \mathrm{m}^{2}\right) \\ 25 \text { miles } \end{gathered}$ | D／Q $\left(1 / \mathrm{m}^{2}\right)$ 30 miles | $\begin{gathered} \text { D/Q } \\ \left(1 / \mathrm{m}^{2}\right) \\ 35 \text { miles } \end{gathered}$ | D／Q $\left(1 / \mathrm{m}^{2}\right)$ 40 miles | D／Q $\left(1 / \mathrm{m}^{2}\right)$ 45 miles | D／Q $\left(1 / \mathrm{m}^{2}\right)$ 50 miles |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N | $5.031 \mathrm{E}-11$ | $3.161 \mathrm{E}-11$ | 1．627E－11 | $1.009 \mathrm{E}-11$ | $7.011 \mathrm{E}-12$ | 5．187E－12 | 3．990E－12 | 3．183E－12 | $2.596 \mathrm{E}-12$ | $2.156 \mathrm{E}-12$ |
| NNE | 7．259E－11 | 4．579E－11 | $2.373 \mathrm{E}-11$ | $1.478 \mathrm{E}-11$ | $1.034 \mathrm{E}-11$ | 7．696E－12 | 5．956E－12 | 4．767E－12 | 3．888E－12 | 3．234E－12 |
| NE | $1.254 \mathrm{E}-10$ | 7．906E－11 | $4.100 \mathrm{E}-11$ | $2.555 \mathrm{E}-11$ | $1.786 \mathrm{E}-11$ | $1.329 \mathrm{E}-11$ | $1.030 \mathrm{E}-11$ | 8．249E－12 | $6.744 \mathrm{E}-12$ | $5.611 \mathrm{E}-12$ |
| ENE | $6.088 \mathrm{E}-11$ | 3．847E－11 | 2．012E－11 | $1.265 \mathrm{E}-11$ | 8．954E－12 | 6．734E－12 | 5．259E－12 | 4．245E－12 | $3.491 \mathrm{E}-12$ | 2．917E－12 |
| E | $4.350 \mathrm{E}-11$ | $2.735 \mathrm{E}-11$ | $1.418 \mathrm{E}-11$ | $8.878 \mathrm{E}-12$ | $6.223 \mathrm{E}-12$ | $4.649 \mathrm{E}-12$ | $3.614 \mathrm{E}-12$ | 2．909E－12 | $2.388 \mathrm{E}-12$ | $1.994 \mathrm{E}-12$ |
| ESE | $6.385 \mathrm{E}-11$ | 4．000E－11 | 2．053E－11 | $1.272 \mathrm{E}-11$ | $8.795 \mathrm{E}-12$ | $6.499 \mathrm{E}-12$ | 5．015E－12 | $4.011 \mathrm{E}-12$ | $3.279 \mathrm{E}-12$ | 2．733E－12 |
| SE | $9.188 \mathrm{E}-11$ | 5．720E－11 | $2.906 \mathrm{E}-11$ | 1．793E－11 | $1.243 \mathrm{E}-11$ | 9．273E－12 | 7．278E－12 | 5．937E－12 | $4.959 \mathrm{E}-12$ | $4.244 \mathrm{E}-12$ |
| SSE | 6．157E－11 | 3．806E－11 | $1.920 \mathrm{E}-11$ | $1.183 \mathrm{E}-11$ | $8.188 \mathrm{E}-12$ | 6．096E－12 | $4.774 \mathrm{E}-12$ | 3．884E－12 | 3．236E－12 | $2.763 \mathrm{E}-12$ |
| S | 1．089E－10 | $6.795 \mathrm{E}-11$ | 3．500E－11 | 2．193E－11 | 1．539E－11 | $1.158 \mathrm{E}-11$ | $9.095 \mathrm{E}-12$ | 7．412E－12 | $6.162 \mathrm{E}-12$ | 5．223E－12 |
| SSW | 9．094E－11 | $5.673 \mathrm{E}-11$ | $2.926 \mathrm{E}-11$ | 1．839E－11 | $1.298 \mathrm{E}-11$ | $9.821 \mathrm{E}-12$ | 7．758E－12 | $6.356 \mathrm{E}-12$ | $5.308 \mathrm{E}-12$ | 4．519E－12 |
| SW | $8.744 \mathrm{E}-11$ | 5．427E－11 | $2.766 \mathrm{E}-11$ | $1.720 \mathrm{E}-11$ | $1.198 \mathrm{E}-11$ | 8．950E－12 | 7．656E－12 | $6.425 \mathrm{E}-12$ | 6．883E－12 | $6.214 \mathrm{E}-12$ |
| WSW | $6.255 \mathrm{E}-11$ | 3．862E－11 | 1．952E－11 | 1．208E－11 | $8.370 \mathrm{E}-12$ | 6．195E－12 | 5．790E－12 | $4.968 \mathrm{E}-12$ | 5．869E－12 | 5．485E－12 |
| W | 4．009E－11 | $2.485 \mathrm{E}-11$ | $1.266 \mathrm{E}-11$ | 7．985E－12 | $5.745 \mathrm{E}-12$ | $4.473 \mathrm{E}-12$ | $3.663 \mathrm{E}-12$ | 3．106E－12 | $2.678 \mathrm{E}-12$ | 2．365E－12 |
| WNW | $2.827 \mathrm{E}-11$ | 1．757E－11 | $9.012 \mathrm{E}-12$ | $5.644 \mathrm{E}-12$ | $4.309 \mathrm{E}-12$ | 3．511E－12 | $3.334 \mathrm{E}-12$ | 3．048E－12 | $4.026 \mathrm{E}-11$ | 3．979E－11 |
| NW | 3．833E－11 | $2.395 \mathrm{E}-11$ | $1.238 \mathrm{E}-11$ | 7．785E－12 | $6.691 \mathrm{E}-12$ | 5．943E－12 | 2．517E－11 | 2．703E－11 | 5．502E－11 | 5．402E－11 |
| NNW | 7．758E－11 | 4．832E－11 | 2．489E－11 | $1.618 \mathrm{E}-11$ | $2.645 \mathrm{E}-11$ | 3．090E－11 | 3．475E－11 | 3．701E－11 | $3.749 \mathrm{E}-11$ | $3.831 \mathrm{E}-11$ |

Table 2.3-129—\{Normal Effluent Annual Average, D/Q Values for Mixed Mode Release Using 242,458 cfm Flow Rate for Special and Additional Receptors\}

| Downwind Sector | D/Q $\left(1 / \mathbf{m}^{2}\right)$ Site Boundary | $\mathrm{D} / \mathrm{Q}$ $\left(1 / \mathrm{m}^{2}\right)$ Nearest Residents | $\mathrm{D} / \mathrm{Q}$ $\left(1 / \mathbf{m}^{2}\right)$ Nearest Gardens |
| :---: | :---: | :---: | :---: |
| N | $1.895 \mathrm{E}-08$ | N/A | N/A |
| NNE | $5.101 \mathrm{E}-08$ | N/A | N/A |
| NE | $8.617 \mathrm{E}-08$ | N/A | N/A |
| ENE | $3.134 \mathrm{E}-08$ | N/A | N/A |
| E | $1.978 \mathrm{E}-08$ | N/A | N/A |
| ESE | $2.465 \mathrm{E}-08$ | N/A | N/A |
| SE | $1.060 \mathrm{E}-08$ | 2.1938.234E-09 | 2.1938.234E-09 |
| SSE | $4.730 \mathrm{E}-09$ | $2.5782 .960 \mathrm{E}-09$ | $2.5782 .475 \mathrm{E}-09$ |
| S | $1.186 \mathrm{E}-08$ | $2.1504 .068 \mathrm{E}-09$ | $2.1504 .068 \mathrm{E}-09$ |
| SSW | $9.686 \mathrm{E}-09$ | 2.649E-09N/A | $1.992 \mathrm{E}-09 \mathrm{~N} / \mathrm{A}$ |
| SW | $5.493 \mathrm{E}-09$ | $5.4154 .333 \mathrm{E}-09$ | $5.4153 .074 \mathrm{E}-09$ |
| WSW | $3.9713 .580 \mathrm{E}-09$ | 2.8604.115E-09 | 1.7404.115E-09 |
| W | $2.159 \mathrm{E}-09$ | 1.4381.465E-09 | 1.053E-099.487E-10 |
| WNW | 7.963E-10 | $2.4686 .835 \mathrm{E}-10$ | $2.4685 .336 \mathrm{E}-10$ |
| NW | $2.465 \mathrm{E}-09$ | 5.0603.322E-10 | 5.0603.322E-10 |
| NNW | $2.064 \mathrm{E}-08$ | N/A | N/A |

Table 2.3-130—\{Specific Locations of Receptors of Interest\}

| Receptor | Distance Downwind m (ft) | Sector |
| :---: | :---: | :---: |
| Site Boundary | 623.4 (2045.3) | N |
| Site Boundary | 429.4 (1408.8) | NNE |
| Site Boundary | 443.3 (1454.4) | NE |
| Site Boundary | 471.0 (1545.3) | ENE |
| Site Boundary | 554.1 (1817.9) | E |
| Site Boundary | 692.7 (2272.6) | ESE |
| Site Boundary | 1413.0 (4635.8) | SE |
| Site Boundary | 1607.0 (5272.3) | SSE |
| Site Boundary | 1385.0 (4544.0) | S |
| Site Boundary | 1371.0 (4498).0(4498.0) | SSW |
| Site Boundary | 1759.0 (5771.0) | SW |
| Site Boundary | 1662.01745 .0 (5452.85725.1) | WSW |
| Site Boundary | 1732.0 (5682.4) | W |
| Site Boundary | 2313.0 (7588.6) | WNW |
| Site Boundary | 1662.0 (5452.8) | NW |
| Site Boundary | 761.9 (2499.7) | NNW |
| Nearest Resident | 2735.01574 .0 (8973.15164.0) | SE |
| Nearest Resident | 2092.01969 .0 (6863.56460.0) | SSE |
| Nearest Resident | 2896.02206 .0 (9501.37237.5) | S |
| Nearest Resident | 1770.01945 .0 (5807.16381.2) | SW |
| Nearest Resident | 1931.01634 .0 (6335.35360.9) | WSW |
| Nearest Resident | 2092.02074 .0 (6863.56804.5) | W |
| Nearest Resident | 4023.02485 .0 (13199.08152.9) | WNW |
| Nearest Resident | 3379.04097 .0 (71086.013441.6) | NW |
| Nearest Garden | 2735.01574 .0 (8973.15164.0) | SE |
| Nearest Garden | 2092.02130 .0 (6863.56988.2) | SSE |
| Nearest Garden | z896.02206.0 (9501.37237.5) | S |
| Nearest Garden | 2735.0 (8973.1) | SSW |
| Nearest Garden | 1770.02256 .0 (5807.17401.6) | SW |
| Nearest Garden | 2414.01634 .0 (7919.95360.9) | WSW |
| Nearest Garden | 2414.02529.0 (7919.98297.2) | W |
| Nearest Garden | 4023.02795 .0 (13198.89169.9) | WNW |
| Nearest Garden | 3379.04097 .0 (11086.013441.6) | NW |

Table 2.3-131—Calvert Cliffs Nuclear Power Station Monthly Mean Temperatures (1987-2006)

|  | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC | ANNUAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\circ} \mathrm{F}$ | 36.5 | 38.3 | 44.7 | 54.8 | 63.2 | 71.7 | 76.5 | 75.3 | 68.9 | 58.2 | 50.2 | 39.9 | 56.5 |
| ${ }^{\circ} \mathrm{C}$ | 2.5 | 3.5 | 7.1 | 12.7 | 17.3 | 22.1 | 24.7 | 24.1 | 20.5 | 14.6 | 10.1 | 4.4 | 13.6 |

Table 2.3-132—Calvert Cliffs Nuclear Power Station Monthly and Annual Precipitation (1992-2006)

|  | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC | ANNUAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | 2.11 | $\underline{2.16}$ | 3.58 | 2.90 | 2.87 | 2.82 | 3.04 | 1.95 | 2.80 | 2.42 | $\underline{2.74}$ | 2.20 | 31.58 |
| mm | 53.59 | 54.86 | $\underline{90.93}$ | 73.66 | 72.90 | $\underline{71.63}$ | 77.22 | 49.53 | 71.12 | 61.47 | 69.60 | 55.88 | 802.13 |

## 

## 

Table 2.3-133—Monthly Atmospheric Stability Summary (2000 through 2005)

Table 2.3-134—\{CCNPP 33' (10-m) 2000-2006 Annual Joint Frequency Distribution Table\} (Page 1 of 8)
CC JANOO-DEC06 MET DATA JOINT FREQUENCY DISTRIBUTION ( 60 -METER TOWER)
33.0 FT WIND DATA STABILITY CLASS A CLASS FREQUENCY (PERCENT) $=10.89$
WIND DIRECTION FROM

## 

| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | wNW | NW | nNW | VRBL | total | SPEED |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | MPH |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | LT . 4 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |

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| $(2)$ | .00 | .00 | .00 | .00 | .00 | .00 | .00 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $.2-$ | .4 | 0 | 0 | 0 | 0 | 0 | 0 |
| $(1)$ | .00 | .00 | .00 | .00 | .00 | .00 | .00 |



| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| . $5-1.0$ | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 6 | $1.0-2.2$ |
| (1) | . 00 | . 00 | . 00 | . 00 | . 03 | . 00 | . 00 | . 02 | . 00 | . 02 | . 02 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 09 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 |  |
| 1.1-1.5 | 3 | 3 | 4 | 8 | 4 | 0 | 5 | 2 | 3 | 12 | 9 | 6 | 8 | 4 | 1 | 1 | 0 | 73 | $2.3-3.4$ |


| (1) | 2.12 | 2.72 | 1.85 | 1.08 | 1.27 | 1.02 | 1.10 | 1.28 | 1.28 | 2.95 | 4.53 | 2.72 | 1.01 | . 58 | . 44 | . 29 | . 00 | 26.24 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (2) | . 23 | . 30 | . 20 | . 12 | . 14 | . 11 | . 12 | . 14 | . 14 | . 32 | . 49 | . 30 | . 11 | . 06 | . 05 | . 03 | . 00 | 2.86 |  |
| $3.1-4.0$ | 317 | 280 | 120 | 21 | 31 | 39 | 112 | 168 | 73 | 152 | 329 | 215 | 99 | 92 | 76 | 60 | 0 | 2184 | 6.8-8.9 |
| (1) | 4.84 | 4.27 | 1.83 | . 32 | . 47 | . 60 | 1.71 | 2.56 | 1.11 | 2.32 | 5.02 | 3.28 | 1.51 | 1.40 | 1.16 | . 92 | . 00 | 33.34 |  |
| (2) | . 53 | . 47 | . 20 | . 03 | . 05 | . 06 | . 19 | . 28 | . 12 | . 25 | . 55 | . 36 | . 16 | . 15 | . 13 | . 10 | . 00 | 3.63 |  |
| 4.1-5.0 | 179 | 105 | 49 | 9 | 5 | 10 | 54 | 110 | 36 | 88 | 183 | 84 | 76 | 117 | 136 | 49 | 0 | 1290 | 9.0-11.2 |
| (1) | 2.73 | 1.60 | . 75 | . 14 | . 08 | . 15 | . 82 | 1.68 | . 55 | 1.34 | 2.79 | 1.28 | 1.16 | 1.79 | 2.08 | . 75 | . 00 | 19.69 |  |
| (2) | . 30 | . 17 | . 08 | . 01 | . 01 | . 02 | . 09 | . 18 | . 06 | . 15 | . 30 | . 14 | . 13 | . 19 | . 23 | . 08 | . 00 | 2.14 |  |
| 5.1-6.0 | 70 | 24 | 28 | 1 | 0 | 1 | 12 | 53 | 6 | 35 | 72 | 26 | 40 | 120 | 122 | 31 | 0 | 641 | 11.3-13.4 |
| (1) | 1.07 | . 37 | . 43 | . 02 | . 00 | . 02 | . 18 | . 81 | . 09 | . 53 | 1.10 | . 40 | . 61 | 1.83 | 1.86 | . 47 | . 00 | 9.78 |  |
| (2) | . 12 | . 04 | . 05 | . 00 | . 00 | . 00 | . 02 | . 09 | . 01 | . 06 | . 12 | . 04 | . 07 | . 20 | . 20 | . 05 | . 00 | 1.07 |  |
| 6.1-8.0 | 16 | 1 | 15 | 3 | 0 | 0 | 0 | 28 | 1 | 9 | 19 | 13 | 17 | 80 | 106 | 16 | 0 | 324 | 13.5-17.9 |
| (1) | . 24 | . 02 | . 23 | . 05 | . 00 | . 00 | . 00 | . 43 | . 02 | . 14 | . 29 | . 20 | . 26 | 1.22 | 1.62 | . 24 | . 00 | 4.95 |  |
| (2) | . 03 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 05 | . 00 | . 01 | . 03 | . 02 | . 03 | . 13 | . 18 | . 03 | . 00 | . 54 |  |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 13 | 8 | 0 | 0 | 25 | 18.0-22.4 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 03 | . 00 | . 00 | . 03 | . 20 | . 12 | . 00 | . 00 | . 38 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 01 | . 00 | . 00 | . 04 |  |
| 10.1-89.5 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 2 | 22.5-200.2 |
| (1) | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 03 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| ALL SPEEDS | 734 | 620 | 358 | 135 | 139 | 130 | 262 | 459 | 214 | 528 | 964 | 549 | 323 | 470 | 483 | 183 | 0 | 6551 |  |
| (1) | 11.20 | 9.46 | 5.46 | 2.06 | 2.12 | 1.98 | 4.00 | 7.01 | 3.27 | 8.06 | 14.72 | 8.38 | 4.93 | 7.17 | 7.37 | 2.79 | . 00 | 100.00 |  |
| (2) | 1.22 | 1.03 | . 60 | . 22 | . 23 | . 22 | . 44 | . 76 | . 36 | . 88 | 1.60 | . 91 | . 54 | . 78 | . 80 | . 30 | . 00 | 10.89 |  |

[^2](2) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
Table 2.3-134—\{CCNPP 33' (10-m) 2000-2006 Annual Joint Frequency Distribution Table\} (Page 2 of 8)

CLASS FREQU

## 

| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL | SPEED |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | MPH |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | LT . 4 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 04 | . 00 | . 00 | . 00 | . 00 | . 00 | . 04 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| .2- . 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | . $4-.9$ |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| .5-1.0 | 1 | 0 | 1 | 0 | 2 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 8 | 1.0-2.2 |
| (1) | . 04 | . 00 | . 04 | . 00 | . 07 | . 00 | . 04 | . 04 | . 04 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 04 | . 00 | . 30 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 |  |
| 1.1-1.5 | 3 | 4 | 3 | 2 | 9 | 1 | 4 | 2 | 3 | 5 | 7 | 3 | 4 | 3 | 0 | 0 | 0 | 53 | 2.3-3.4 |
| (1) | . 11 | . 15 | . 11 | . 07 | . 33 | . 04 | . 15 | . 07 | . 11 | . 18 | . 26 | . 11 | . 15 | . 11 | . 00 | . 00 | . 00 | 1.96 |  |
| (2) | . 00 | . 01 | . 00 | . 00 | . 01 | . 00 | . 01 | . 00 | . 00 | . 01 | . 01 | . 00 | . 01 | . 00 | . 00 | . 00 | . 00 | . 09 |  |
| 1.6-2.0 | 12 | 12 | 27 | 24 | 13 | 20 | 13 | 3 | 13 | 10 | 24 | 20 | 10 | 6 | 4 | 6 | 0 | 217 | 3.5-4.5 |
| (1) | . 44 | . 44 | 1.00 | . 89 | . 48 | . 74 | . 48 | . 11 | . 48 | . 37 | . 89 | . 74 | . 37 | . 22 | . 15 | . 22 | . 00 | 8.01 |  |
| (2) | . 02 | . 02 | . 04 | . 04 | . 02 | . 03 | . 02 | . 00 | . 02 | . 02 | . 04 | . 03 | . 02 | . 01 | . 01 | . 01 | . 00 | . 36 |  |
| 2.1-3.0 | 103 | 132 | 74 | 70 | 53 | 36 | 48 | 44 | 40 | 58 | 69 | 70 | 46 | 31 | 17 | 15 | 0 | 906 | 4.6-6.7 |
| (1) | 3.80 | 4.87 | 2.73 | 2.58 | 1.96 | 1.33 | 1.77 | 1.62 | 1.48 | 2.14 | 2.55 | 2.58 | 1.70 | 1.14 | . 63 | . 55 | . 00 | 33.44 |  |
| (2) | . 17 | . 22 | . 12 | . 12 | . 09 | . 06 | . 08 | . 07 | . 07 | . 10 | . 11 | . 12 | . 08 | . 05 | . 03 | . 02 | . 00 | 1.51 |  |
| 3.1-4.0 | 122 | 92 | 49 | 16 | 8 | 12 | 53 | 86 | 16 | 44 | 86 | 58 | 33 | 34 | 33 | 18 | 0 | 760 | 6.8-8.9 |
| (1) | 4.50 | 3.40 | 1.81 | . 59 | . 30 | . 44 | 1.96 | 3.17 | . 59 | 1.62 | 3.17 | 2.14 | 1.22 | 1.26 | 1.22 | . 66 | . 00 | 28.05 |  |
| (2) | . 20 | . 15 | . 08 | . 03 | . 01 | . 02 | . 09 | . 14 | . 03 | . 07 | . 14 | . 10 | . 05 | . 06 | . 05 | . 03 | . 00 | 1.26 |  |
| 4.1- 5.0 | 58 | 18 | 31 | 3 | 1 | 3 | 15 | 31 | 10 | 22 | 42 | 23 | 26 | 27 | 45 | 29 | 0 | 384 | 9.0-11.2 |
| (1) | 2.14 | . 66 | 1.14 | . 11 | . 04 | . 11 | . 55 | 1.14 | . 37 | . 81 | 1.55 | . 85 | . 96 | 1.00 | 1.66 | 1.07 | . 00 | 14.17 |  |
| (2) | . 10 | . 03 | . 05 | . 00 | . 00 | . 00 | . 02 | . 05 | . 02 | . 04 | . 07 | . 04 | . 04 | . 04 | . 07 | . 05 | . 00 | . 64 |  |
| 5.1- 6.0 | 43 | 10 | 17 | 4 | 0 | 1 | 4 | 21 | 3 | 5 | 17 | 4 | 14 | 26 | 44 | 15 | 0 | 228 | 11.3-13.4 |
| (1) | 1.59 | . 37 | . 63 | . 15 | . 00 | . 04 | . 15 | . 78 | . 11 | . 18 | . 63 | . 15 | . 52 | . 96 | 1.62 | . 55 | . 00 | 8.42 |  |
| (2) | . 07 | . 02 | . 03 | . 01 | . 00 | . 00 | . 01 | . 03 | . 00 | . 01 | . 03 | . 01 | . 02 | . 04 | . 07 | . 02 | . 00 | . 38 |  |
| 6.1-8.0 | 10 | 2 | 4 | 4 | 0 | 0 | 2 | 12 | 1 | 4 | 6 | 5 | 5 | 38 | 38 | 10 | 0 | 141 | 13.5-17.9 |
| (1) | . 37 | . 07 | . 15 | . 15 | . 00 | . 00 | . 07 | . 44 | . 04 | . 15 | . 22 | . 18 | . 18 | 1.40 | 1.40 | . 37 | . 00 | 5.20 |  |
| (2) | . 02 | . 00 | . 01 | . 01 | . 00 | . 00 | . 00 | . 02 | . 00 | . 01 | . 01 | . 01 | . 01 | . 06 | . 06 | . 02 | . 00 | . 23 |  |
| 8.1-10.0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 0 | 0 | 10 | 18.0-22.4 |
| (1) | . 04 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 04 | . 00 | . 00 | . 00 | . 00 | . 00 | . 04 | . 26 | . 00 | . 00 | . 37 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 00 | . 00 | . 02 |  |
| 10.1-89.5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 22.5-200.2 |
| (1) | . 04 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 04 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| ALL SPEEDS | 354 | 270 | 206 | 123 | 86 | 73 | 140 | 201 | 87 | 148 | 251 | 184 | 138 | 166 | 188 | 94 | 0 | 2709 |  |
| (1) | 13.07 | 9.97 | 7.60 | 4.54 | 3.17 | 2.69 | 5.17 | 7.42 | 3.21 | 5.46 | 9.27 | 6.79 | 5.09 | 6.13 | 6.94 | 3.47 | . 00 | 100.00 |  |
| (2) | . 59 |  | . 34 | . 20 |  |  | . 23 | . 33 | . 14 | . 25 | . 42 | . 31 | . 23 | . 28 | . 31 | . 16 | . 00 | 4.50 |  |
| (1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| (2)=PERCENT | OF ALL | GOOD | OBSERV | ATIONS | FOR | HIS PE | RIOD |  |  |  |  |  |  |  |  |  |  |  |  |

Table 2.3-134—\{CCNPP $33^{\prime}(10-m)$ 2000-2006 Annual Joint Frequency Distribution Table\} (Page 3 of 8)
CC JANOO-DEC06 MET DATA JOINT FREQUENCY DISTRIBUTION ( 60 -METER TOWER)

| CC |  |  |
| :---: | :---: | :---: |
| 33.0 FT WIND DATA | STABILITY CLASS C | CLASS FREQUENCY (PERCENT) $=$ | WIND DIRECTION FROM

## 

| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL | SPEED |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | MPH |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | LT . 4 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | . $4-.9$ |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 03 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 03 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| . $5-1.0$ | 1 | 1 | 1 | 0 | 3 | 0 | 2 | 1 | 2 | 1 | 3 | 2 | 3 | 1 | 1 | 1 | 0 | 23 | 1.0-2.2 |
| (1) | . 03 | . 03 | . 03 | . 00 | . 10 | . 00 | . 07 | . 03 | . 07 | . 03 | . 10 | . 07 | . 10 | . 03 | . 03 | . 03 | . 00 | . 75 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 04 |  |
| 1.1-1.5 | 5 | 14 | 8 | 13 | 11 | 7 | 6 | 5 | 3 | 8 | 11 | 12 | 8 | 6 | 2 | 4 | 0 | 123 | $2.3-3.4$ |
| (1) | . 16 | . 46 | . 26 | . 42 | . 36 | . 23 | . 20 | . 16 | . 10 | . 26 | . 36 | . 39 | . 26 | . 20 | . 07 | . 13 | . 00 | 4.02 |  |
| (2) | . 01 | . 02 | . 01 | . 02 | . 02 | . 01 | . 01 | . 01 | . 00 | . 01 | . 02 | . 02 | . 01 | . 01 | . 00 | . 01 | . 00 | . 20 |  |
| 1.6-2.0 | 18 | 41 | 23 | 30 | 39 | 21 | 19 | 16 | 16 | 11 | 31 | 24 | 16 | 7 | 8 | 4 | 0 | 324 | $3.5-4.5$ |
| (1) | . 59 | 1.34 | . 75 | . 98 | 1.27 | . 69 | . 62 | . 52 | . 52 | . 36 | 1.01 | . 78 | . 52 | . 23 | . 26 | . 13 | . 00 | 10.58 |  |
| (2) | . 03 | . 07 | . 04 | . 05 | . 06 | . 03 | . 03 | . 03 | . 03 | . 02 | . 05 | . 04 | . 03 | . 01 | . 01 | . 01 | . 00 | . 54 |  |
| 2.1-3.0 | 132 | 163 | 107 | 79 | 58 | 44 | 56 | 63 | 39 | 60 | 108 | 76 | 48 | 38 | 36 | 25 | 0 | 1132 | 4.6-6.7 |
| (1) | 4.31 | 5.32 | 3.49 | 2.58 | 1.89 | 1.44 | 1.83 | 2.06 | 1.27 | 1.96 | 3.53 | 2.48 | 1.57 | 1.24 | 1.18 | . 82 | . 00 | 36.97 |  |
| (2) | . 22 | . 27 | . 18 | . 13 | . 10 | . 07 | . 09 | . 10 | . 06 | . 10 | . 18 | . 13 | . 08 | . 06 | . 06 | . 04 | . 00 | 1.88 |  |
| 3.1-4.0 | 126 | 71 | 76 | 19 | 13 | 8 | 18 | 92 | 26 | 32 | 75 | 56 | 43 | 32 | 47 | 30 | 0 | 764 | $6.8-8.9$ |
| (1) | 4.11 | 2.32 | 2.48 | . 62 | . 42 | . 26 | . 59 | 3.00 | . 85 | 1.05 | 2.45 | 1.83 | 1.40 | 1.05 | 1.53 | . 98 | . 00 | 24.95 |  |
| (2) | . 21 | . 12 | . 13 | . 03 | . 02 | . 01 | . 03 | . 15 | . 04 | . 05 | . 12 | . 09 | . 07 | . 05 | . 08 | . 05 | . 00 | 1.27 |  |
| 4.1-5.0 | 56 | 22 | 35 | 7 | 3 | 2 | 9 | 44 | 8 | 18 | 35 | 27 | 15 | 33 | 46 | 26 | 0 | 386 | 9.0-11.2 |
| (1) | 1.83 | . 72 | 1.14 | . 23 | . 10 | . 07 | . 29 | 1.44 | . 26 | . 59 | 1.14 | . 88 | . 49 | 1.08 | 1.50 | . 85 | . 00 | 12.61 |  |
| (2) | . 09 | . 04 | . 06 | . 01 | . 00 | . 00 | . 01 | . 07 | . 01 | . 03 | . 06 | . 04 | . 02 | . 05 | . 08 | . 04 | . 00 | . 64 |  |
| 5.1-6.0 | 15 | 10 | 18 | 9 | 0 | 0 | 3 | 15 | 2 | 2 | 19 | 5 | 8 | 24 | 31 | 10 | 0 | 171 | 11.3-13.4 |
| (1) | . 49 | . 33 | . 59 | . 29 | . 00 | . 00 | . 10 | . 49 | . 07 | . 07 | . 62 | . 16 | . 26 | . 78 | 1.01 | . 33 | . 00 | 5.58 |  |
| (2) | . 02 | . 02 | . 03 | . 01 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 03 | . 01 | . 01 | . 04 | . 05 | . 02 | . 00 | . 28 |  |
| 6.1-8.0 | 18 | 4 | 7 | 5 | 0 | 0 | 0 | 5 | 0 | 2 | 4 | 0 | 5 | 27 | 41 | 9 | 0 | 127 | 13.5-17.9 |
| (1) | . 59 | . 13 | . 23 | . 16 | . 00 | . 00 | . 00 | . 16 | . 00 | . 07 | . 13 | . 00 | . 16 | . 88 | 1.34 | . 29 | . 00 | 4.15 |  |
| (2) | . 03 | . 01 | . 01 | . 01 | . 00 | . 00 | . 00 | . 01 | . 00 | . 00 | . 01 | . 00 | . 01 | . 04 | . 07 | . 01 | . 00 | . 21 |  |
| 8.1-10.0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 3 | 1 | 0 | 11 | 18.0-22.4 |
| (1) | . 07 | . 00 | . 07 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 10 | . 10 | . 03 | . 00 | . 36 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |  |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $22.5-200.2$ |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| ALL SPEEDS | 373 | 326 | 277 | 162 | 127 | 83 | 113 | 241 | 96 | 134 | 286 | 202 | 146 | 171 | 215 | 110 | 0 | 3062 |  |
| (1) | 12.18 | 10.65 | 9.05 | 5.29 | 4.15 | 2.71 | 3.69 | 7.87 | 3.14 | 4.38 | 9.34 | 6.60 | 4.77 | 5.58 | 7.02 | 3.59 | . 00 | 100.00 |  |
| (2) | . 62 | . 54 | . 46 | . 27 | . 21 | . 14 | . 19 | . 40 | . 16 | . 22 | . 48 | . 34 | . 24 | . 28 | . 36 | . 18 | . 00 | 5.09 |  |
| (1) =PERCENT | OF ALI | GOOD | OBSERV | ATIONS | FOR | HIS PA |  |  |  |  |  |  |  |  |  |  |  |  |  |
| (2) =PERCENT | OF ALI | GOOD | OBSERV | ATIONS | FOR | HIS PER | RIOD |  |  |  |  |  |  |  |  |  |  |  |  |

Table 2．3－134—\｛CCNPP $33^{\prime}(10-m)$ 2000－2006 Annual Joint Frequency Distribution Table\} （Page 4 of 8）
CC JANOO－DEC06 MET DATA JOINT FREQUENCY DISTRIBUTION（ 60 －METER TOWER）

| 33.0 | FT WIND DATA STABILITY CLASS D $\quad 33.91$ |
| ---: | ---: | ---: | ---: | $\longrightarrow$ WIND DIRECTION FROM


| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL | SPEED |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | MPH |
| LT ． 2 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 2 | 3 | 0 | 0 | 1 | 2 | 1 | 0 | 10 | LT ． 4 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 01 | ． 01 | ． 00 | ． 00 | ． 00 | ． 01 | ． 00 | ． 00 | ． 05 |  |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 |  |
| ． $2-.4$ | 1 | 1 | 0 | 2 | 0 | 0 | 1 | 1 | 2 | 2 | 2 | 2 | 4 | 5 | 0 | 1 | 0 | 24 | ． $4-.9$ |
| （1） | ． 00 | ． 00 | ． 00 | ． 01 | ． 00 | ． 00 | ． 00 | ． 00 | ． 01 | ． 01 | ． 01 | ． 01 | ． 02 | ． 02 | ． 00 | ． 00 | ． 00 | ． 12 |  |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 01 | ． 01 | ． 00 | ． 00 | ． 00 | ． 04 |  |
| ． $5-1.0$ | 33 | 35 | 41 | 26 | 41 | 46 | 34 | 33 | 36 | 50 | 57 | 35 | 26 | 40 | 23 | 36 | 0 | 592 | 1．0－2．2 |
| （1） | ． 16 | ． 17 | ． 20 | ． 13 | ． 20 | ． 23 | ． 17 | ． 16 | ． 18 | ． 25 | ． 28 | ． 17 | ． 13 | ． 20 | ． 11 | ． 18 | ． 00 | 2.90 |  |
| （2） | ． 05 | ． 06 | ． 07 | ． 04 | ． 07 | ． 08 | ． 06 | ． 05 | ． 06 | ． 08 | ． 09 | ． 06 | ． 04 | ． 07 | ． 04 | ． 06 | ． 00 | ． 98 |  |
| 1．1－1．5 | 89 | 92 | 88 | 100 | 152 | 101 | 75 | 79 | 72 | 85 | 109 | 69 | 66 | 46 | 51 | 50 | 0 | 1324 | $2.3-3.4$ |
| （1） | ． 44 | ． 45 | ． 43 | ． 49 | ． 75 | ． 50 | ． 37 | ． 39 | ． 35 | ． 42 | ． 53 | ． 34 | ． 32 | ． 23 | ． 25 | ． 25 | ． 00 | 6.49 |  |
| （2） | ． 15 | ． 15 | ． 15 | ． 17 | ． 25 | ． 17 | ． 12 | ． 13 | ． 12 | ． 14 | ． 18 | ． 11 | ． 11 | ． 08 | ． 08 | ． 08 | ． 00 | 2.20 |  |
| 1．6－2．0 | 173 | 244 | 172 | 219 | 225 | 159 | 144 | 137 | 138 | 139 | 158 | 108 | 81 | 64 | 88 | 84 | 0 | 2333 | $3.5-4.5$ |
| （1） | ． 85 | 1.20 | ． 84 | 1.07 | 1.10 | ． 78 | ． 71 | ． 67 | ． 68 | ． 68 | ． 77 | ． 53 | ． 40 | ． 31 | ． 43 | ． 41 | ． 00 | 11.44 |  |
| （2） | ． 29 | ． 41 | ． 29 | ． 36 | ． 37 | ． 26 | ． 24 | ． 23 | ． 23 | ． 23 | ． 26 | ． 18 | ． 13 | ． 11 | ． 15 | ． 14 | ． 00 | 3.88 |  |
| 2．1－3．0 | 487 | 577 | 448 | 573 | 434 | 274 | 304 | 463 | 284 | 242 | 375 | 282 | 184 | 171 | 287 | 303 | 0 | 5688 | 4．6－6．7 |
| （1） | 2.39 | 2.83 | 2.20 | 2.81 | 2.13 | 1.34 | 1.49 | 2.27 | 1.39 | 1.19 | 1.84 | 1.38 | ． 90 | ． 84 | 1.41 | 1.49 | ． 00 | 27.89 |  |
| （2） | ． 81 | ． 96 | ． 74 | ． 95 | ． 72 | ． 46 | ． 51 | ． 77 | ． 47 | ． 40 | ． 62 | ． 47 | ． 31 | ． 28 | ． 48 | ． 50 | ． 00 | 9.45 |  |
| 3．1－4．0 | 470 | 352 | 470 | 445 | 186 | 116 | 153 | 406 | 179 | 154 | 294 | 191 | 114 | 150 | 374 | 452 | 0 | 4506 | 6．8－8．9 |
| （1） | 2.30 | 1.73 | 2.30 | 2.18 | ． 91 | ． 57 | ． 75 | 1.99 | ． 88 | ． 76 | 1.44 | ． 94 | ． 56 | ． 74 | 1.83 | 2.22 | ． 00 | 22.09 |  |
| （2） | ． 78 | ． 59 | ． 78 | ． 74 | ． 31 | ． 19 | ． 25 | ． 67 | ． 30 | ． 26 | ． 49 | ． 32 | ． 19 | ． 25 | ． 62 | ． 75 | ． 00 | 7.49 |  |
| 4．1－5．0 | 384 | 285 | 403 | 243 | 48 | 19 | 53 | 221 | 80 | 80 | 188 | 80 | 65 | 144 | 334 | 324 | 0 | 2951 | 9．0－11．2 |
| （1） | 1.88 | 1.40 | 1.98 | 1.19 | ． 24 | ． 09 | ． 26 | 1.08 | ． 39 | ． 39 | ． 92 | ． 39 | ． 32 | ． 71 | 1.64 | 1.59 | ． 00 | 14.47 |  |
| （2） | ． 64 | ． 47 | ． 67 | ． 40 | ． 08 | ． 03 | ． 09 | ． 37 | ． 13 | ． 13 | ． 31 | ． 13 | ． 11 | ． 24 | ． 56 | ． 54 | ． 00 | 4.91 |  |
| 5．1－6．0 | 265 | 187 | 267 | 122 | 1 | 4 | 19 | 118 | 22 | 32 | 85 | 23 | 31 | 118 | 267 | 135 | 0 | 1696 | 11．3－13．4 |
| （1） | 1.30 | ． 92 | 1.31 | ． 60 | ． 00 | ． 02 | ． 09 | ． 58 | ． 11 | ． 16 | ． 42 | ． 11 | ． 15 | ． 58 | 1.31 | ． 66 | ． 00 | 8.31 |  |
| （2） | ． 44 | ． 31 | ． 44 | ． 20 | ． 00 | ． 01 | ． 03 | ． 20 | ． 04 | ． 05 | ． 14 | ． 04 | ． 05 | ． 20 | ． 44 | ． 22 | ． 00 | 2.82 |  |
| 6．1－8．0 | 204 | 110 | 211 | 53 | 3 | 2 | 13 | 62 | 17 | 17 | 15 | 12 | 15 | 133 | 162 | 49 | 0 | 1078 | 13．5－17．9 |
| （1） | 1.00 | ． 54 | 1.03 | ． 26 | ． 01 | ． 01 | ． 06 | ． 30 | ． 08 | ． 08 | ． 07 | ． 06 | ． 07 | ． 65 | ． 79 | ． 24 | ． 00 | 5.29 |  |
| （2） | ． 34 | ． 18 | ． 35 | ． 09 | ． 00 | ． 00 | ． 02 | ． 10 | ． 03 | ． 03 | ． 02 | ． 02 | ． 02 | ． 22 | ． 27 | ． 08 | ． 00 | 1.79 |  |
| 8．1－10．0 | 34 | 11 | 45 | 10 | 1 | 0 | 3 | 9 | 1 | 2 | 1 | 1 | 4 | 22 | 21 | 3 | 0 | 168 | 18．0－22．4 |
| （1） | ． 17 | ． 05 | ． 22 | ． 05 | ． 00 | ． 00 | ． 01 | ． 04 | ． 00 | ． 01 | ． 00 | ． 00 | ． 02 | ． 11 | ． 10 | ． 01 | ． 00 | ． 82 |  |
| （2） | ． 06 | ． 02 | ． 07 | ． 02 | ． 00 | ． 00 | ． 00 | ． 01 | ． 00 | ． 00 | ． 00 | ． 00 | ． 01 | ． 04 | ． 03 | ． 00 | ． 00 | ． 28 |  |
| 10．1－89．5 | 4 | 2 | 13 | 3 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 27 | $22.5-200.2$ |
| （1） | ． 02 | ． 01 | ． 06 | ． 01 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 13 |  |
| （2） | ． 01 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 04 |  |
| ALL SPEEDS | 2144 | 1896 | 2158 | 1796 | 1093 | 721 | 800 | 1530 | 831 | 805 | 1287 | 803 | 590 | 895 | 1610 | 1438 | 0 | 20397 |  |
| （1） | 10.51 | 9.30 | 10.58 | 8.81 | 5.36 | 3.53 | 3.92 | 7.50 | 4.07 | 3.95 | 6.31 | 3.94 | 2.89 | 4.39 | 7.89 | 7.05 | ． 00 | 100.00 |  |
| （2） | 3.56 | 3.15 | 3.59 | 2.99 | 1.82 | 1.20 | 1.33 | 2.54 | 1.38 | 1.34 | 2.14 | 1.33 | ． 98 | 1.49 | 2.68 | 2.39 | ． 00 | 33.91 |  |
| （1）＝PERCENT | OF ALL | GOOD | OBSERV | ATIONS | FOR | HIS PA |  |  |  |  |  |  |  |  |  |  |  |  |  |
| （2）＝PERCENT | OF ALL | GOOD | OBSERV | ATIONS | FOR | HIS PER | RIOD |  |  |  |  |  |  |  |  |  |  |  |  |

Table 2.3-134—\{CCNPP $33^{\prime}(10-m)$ 2000-2006 Annual Joint Frequency Distribution Table\} (Page 5 of 8)
CC JANOO-DEC06 MET DATA JOINT FREQUENCY DISTRIBUTION ( 60 -METER TOWER)

| CC |  |  |
| :---: | :---: | :---: | :---: |
| 33.0 FT WIND DATA | STABILITY CLASS E | CLASS FREQUENCY (PERCENT) $=27.57$ | WIND DIRECTION FROM


| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL | SPEED |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | MPH |
| LT . 2 | 3 | 3 | 0 | 0 | 2 | 1 | 4 | 6 | 7 | 3 | 12 | 8 | 5 | 1 | 2 | 1 | 0 | 58 | LT . 4 |
| (1) | . 02 | . 02 | . 00 | . 00 | . 01 | . 01 | . 02 | . 04 | . 04 | . 02 | . 07 | . 05 | . 03 | . 01 | . 01 | . 01 | . 00 | . 35 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 01 | . 01 | . 00 | . 02 | . 01 | . 01 | . 00 | . 00 | . 00 | . 00 | . 10 |  |
| . $2-.4$ | 3 | 2 | 7 | 2 | 4 | 7 | 8 | 10 | 17 | 19 | 10 | 13 | 15 | 7 | 8 | 1 | 0 | 133 | . $4-.9$ |
| (1) | . 02 | . 01 | . 04 | . 01 | . 02 | . 04 | . 05 | . 06 | . 10 | . 11 | . 06 | . 08 | . 09 | . 04 | . 05 | . 01 | . 00 | . 80 |  |
| (2) | . 00 | . 00 | . 01 | . 00 | . 01 | . 01 | . 01 | . 02 | . 03 | . 03 | . 02 | . 02 | . 02 | . 01 | . 01 | . 00 | . 00 | . 22 |  |
| .5-1.0 | 54 | 42 | 35 | 40 | 59 | 65 | 67 | 83 | 120 | 132 | 137 | 100 | 81 | 52 | 63 | 63 | 0 | 1193 | 1.0-2.2 |
| (1) | . 33 | . 25 | . 21 | . 24 | . 36 | . 39 | . 40 | . 50 | . 72 | . 80 | . 83 | . 60 | . 49 | . 31 | . 38 | . 38 | . 00 | 7.19 |  |
| (2) | . 09 | . 07 | . 06 | . 07 | . 10 | . 11 | . 11 | . 14 | . 20 | . 22 | . 23 | . 17 | . 13 | . 09 | . 10 | . 10 | . 00 | 1.98 |  |
| 1.1-1.5 | 110 | 107 | 75 | 64 | 68 | 81 | 98 | 144 | 235 | 299 | 278 | 165 | 134 | 127 | 152 | 84 | 0 | 2221 | $2.3-3.4$ |
| (1) | . 66 | . 65 | . 45 | . 39 | . 41 | . 49 | . 59 | . 87 | 1.42 | 1.80 | 1.68 | . 99 | . 81 | . 77 | . 92 | . 51 | . 00 | 13.39 |  |
| (2) | . 18 | . 18 | . 12 | . 11 | . 11 | . 13 | . 16 | . 24 | . 39 | . 50 | . 46 | . 27 | . 22 | . 21 | . 25 | . 14 | . 00 | 3.69 |  |
| 1.6-2.0 | 137 | 141 | 63 | 76 | 99 | 70 | 115 | 184 | 296 | 309 | 319 | 204 | 178 | 214 | 233 | 175 | 0 | 2813 | $3.5-4.5$ |
| (1) | . 83 | . 85 | . 38 | . 46 | . 60 | . 42 | . 69 | 1.11 | 1.78 | 1.86 | 1.92 | 1.23 | 1.07 | 1.29 | 1.40 | 1.05 | . 00 | 16.96 |  |
| (2) | . 23 | . 23 | . 10 | . 13 | . 16 | . 12 | . 19 | . 31 | . 49 | . 51 | . 53 | . 34 | . 30 | . 36 | . 39 | . 29 | . 00 | 4.68 |  |
| 2.1-3.0 | 244 | 213 | 134 | 101 | 105 | 71 | 102 | 270 | 566 | 630 | 871 | 364 | 281 | 354 | 657 | 365 | 0 | 5328 | 4.6-6.7 |
| (1) | 1.47 | 1.28 | . 81 | . 61 | . 63 | . 43 | . 61 | 1.63 | 3.41 | 3.80 | 5.25 | 2.19 | 1.69 | 2.13 | 3.96 | 2.20 | . 00 | 32.12 |  |
| (2) | . 41 | . 35 | . 22 | . 17 | . 17 | . 12 | . 17 | . 45 | . 94 | 1.05 | 1.45 | . 61 | . 47 | . 59 | 1.09 | . 61 | . 00 | 8.86 |  |
| 3.1-4.0 | 162 | 100 | 88 | 38 | 16 | 16 | 36 | 157 | 234 | 360 | 775 | 162 | 123 | 182 | 393 | 221 | 0 | 3063 | 6.8-8.9 |
| (1) | . 98 | . 60 | . 53 | . 23 | . 10 | . 10 | . 22 | . 95 | 1.41 | 2.17 | 4.67 | . 98 | . 74 | 1.10 | 2.37 | 1.33 | . 00 | 18.47 |  |
| (2) | . 27 | . 17 | . 15 | . 06 | . 03 | . 03 | . 06 | . 26 | . 39 | . 60 | 1.29 | . 27 | . 20 | . 30 | . 65 | . 37 | . 00 | 5.09 |  |
| 4.1-5.0 | 78 | 36 | 33 | 6 | 8 | 5 | 11 | 78 | 77 | 163 | 292 | 54 | 47 | 110 | 119 | 78 | 0 | 1195 | 9.0-11.2 |
| (1) | . 47 | . 22 | . 20 | . 04 | . 05 | . 03 | . 07 | . 47 | . 46 | . 98 | 1.76 | . 33 | . 28 | . 66 | . 72 | . 47 | . 00 | 7.20 |  |
| (2) | . 13 | . 06 | . 05 | . 01 | . 01 | . 01 | . 02 | . 13 | . 13 | . 27 | . 49 | . 09 | . 08 | . 18 | . 20 | . 13 | . 00 | 1.99 |  |
| 5.1-6.0 | 34 | 15 | 7 | 0 | 2 | 1 | 5 | 30 | 23 | 56 | 94 | 12 | 18 | 48 | 44 | 18 | 0 | 407 | 11.3-13.4 |
| (1) | . 20 | . 09 | . 04 | . 00 | . 01 | . 01 | . 03 | . 18 | . 14 | . 34 | . 57 | . 07 | . 11 | . 29 | . 27 | . 11 | . 00 | 2.45 |  |
| (2) | . 06 | . 02 | . 01 | . 00 | . 00 | . 00 | . 01 | . 05 | . 04 | . 09 | . 16 | . 02 | . 03 | . 08 | . 07 | . 03 | . 00 | . 68 |  |
| $6.1-8.0$ | 13 | 1 | 2 | 2 | 0 | 1 | 4 | 25 | 9 | 12 | 16 | 3 | 6 | 22 | 14 | 4 | 0 | 134 | 13.5-17.9 |
| (1) | . 08 | . 01 | . 01 | . 01 | . 00 | . 01 | . 02 | . 15 | . 05 | . 07 | . 10 | . 02 | . 04 | . 13 | . 08 | . 02 | . 00 | . 81 |  |
| (2) | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 04 | . 01 | . 02 | . 03 | . 00 | . 01 | . 04 | . 02 | . 01 | . 00 | . 22 |  |
| 8.1-10.0 | 7 | 1 | 0 | 0 | 0 | 0 | 1 | 5 | 0 | 0 | 0 | 2 | 0 | 6 | 2 | 4 | 0 | 28 | 18.0-22.4 |
| (1) | . 04 | . 01 | . 00 | . 00 | . 00 | . 00 | . 01 | . 03 | . 00 | . 00 | . 00 | . 01 | . 00 | . 04 | . 01 | . 02 | . 00 | . 17 |  |
| (2) | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 00 | . 01 | . 00 | . 05 |  |
| 10.1-89.5 | 0 | 0 | 8 | 2 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 15 | $22.5-200.2$ |
| (1) | . 00 | . 00 | . 05 | . 01 | . 00 | . 01 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 00 | . 00 | . 00 | . 09 |  |
| (2) | . 00 | . 00 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |  |
| ALL SPEEDS | 845 | 661 | 452 | 331 | 363 | 320 | 453 | 992 | 1584 | 1983 | 2804 | 1087 | 888 | 1124 | 1687 | 1014 | 0 | 16588 |  |
| (1) | 5.09 | 3.98 | 2.72 | 2.00 | 2.19 | 1.93 | 2.73 | 5.98 | 9.55 | 11.95 | 16.90 | 6.55 | 5.35 | 6.78 | 10.17 | 6.11 | . 00 | 100.00 |  |
| (2) | 1.40 | 1.10 | . 75 | . 55 | . 60 | . 53 | . 75 | 1.65 | 2.63 | 3.30 | 4.66 | 1.81 | 1.48 | 1.87 | 2.80 | 1.69 | . 00 | 27.57 |  |
| (1) =PERCENT | OF ALL | GOOD | OBSERV | ATIONS | FOR | HIS PA |  |  |  |  |  |  |  |  |  |  |  |  |  |
| (2) =PERCENT | OF ALL | GOOD | OBSERV | ATIONS | FOR | HIS PER | RIOD |  |  |  |  |  |  |  |  |  |  |  |  |

Table 2.3-134—\{CCNPP 33' (10-m) 2000-2006 Annual Joint Frequency Distribution Table\} (Page 6 of 8)

## CC JANOO-DEC06 MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER) <br> 33.0 FT WIND DATA <br> STABILITY CLASS F <br> WIND DIRECTION FROM

| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL | SPEED |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | MPH |
| LT . 2 | 0 | 4 | 2 | 2 | 2 | 2 | 3 | 2 | 8 | 9 | 9 | 9 | 3 | 4 | 4 | 1 | 0 | 64 | LT. 4 |
| (1) | . 00 | . 06 | . 03 | . 03 | . 03 | . 03 | . 05 | . 03 | . 13 | . 14 | . 14 | . 14 | . 05 | . 06 | . 06 | . 02 | . 00 | 1.01 |  |
| (2) | . 00 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 01 | . 01 | . 01 | . 00 | . 01 | . 01 | . 00 | . 00 | . 11 |  |
| . $2-.4$ | 0 | 2 | 6 | 2 | 9 | 8 | 8 | 12 | 11 | 19 | 11 | 5 | 7 | 10 | 1 | 6 | 0 | 117 | . $4-.9$ |
| (1) | . 00 | . 03 | . 09 | . 03 | . 14 | . 13 | . 13 | . 19 | . 17 | . 30 | . 17 | . 08 | . 11 | . 16 | . 02 | . 09 | . 00 | 1.85 |  |
| (2) | . 00 | . 00 | . 01 | . 00 | . 01 | . 01 | . 01 | . 02 | . 02 | . 03 | . 02 | . 01 | . 01 | . 02 | . 00 | . 01 | . 00 | . 19 |  |
| .5-1.0 | 31 | 29 | 41 | 27 | 22 | 41 | 30 | 55 | 104 | 150 | 179 | 110 | 82 | 71 | 28 | 32 | 0 | 1032 | 1.0-2.2 |
| (1) | . 49 | . 46 | . 65 | . 43 | . 35 | . 65 | . 47 | . 87 | 1.64 | 2.37 | 2.83 | 1.74 | 1.30 | 1.12 | . 44 | . 51 | . 00 | 16.31 |  |
| (2) | . 05 | . 05 | . 07 | . 04 | . 04 | . 07 | . 05 | . 09 | . 17 | . 25 | . 30 | . 18 | . 14 | . 12 | . 05 | . 05 | . 00 | 1.72 |  |
| 1.1-1.5 | 25 | 27 | 24 | 16 | 15 | 24 | 36 | 83 | 216 | 373 | 342 | 177 | 104 | 127 | 71 | 30 | 0 | 1690 | $2.3-3.4$ |
| (1) | . 40 | . 43 | . 38 | . 25 | . 24 | . 38 | . 57 | 1.31 | 3.41 | 5.89 | 5.40 | 2.80 | 1.64 | 2.01 | 1.12 | . 47 | . 00 | 26.71 |  |
| (2) | . 04 | . 04 | . 04 | . 03 | . 02 | . 04 | . 06 | . 14 | . 36 | . 62 | . 57 | . 29 | . 17 | . 21 | . 12 | . 05 | . 00 | 2.81 |  |
| 1.6-2.0 | 20 | 26 | 13 | 18 | 6 | 6 | 27 | 85 | 187 | 344 | 374 | 190 | 135 | 154 | 107 | 24 | 0 | 1716 | $3.5-4.5$ |
| (1) | . 32 | . 41 | . 21 | . 28 | . 09 | . 09 | . 43 | 1.34 | 2.96 | 5.44 | 5.91 | 3.00 | 2.13 | 2.43 | 1.69 | . 38 | . 00 | 27.12 |  |
| (2) | . 03 | . 04 | . 02 | . 03 | . 01 | . 01 | . 04 | . 14 | . 31 | . 57 | . 62 | . 32 | . 22 | . 26 | . 18 | . 04 | . 00 | 2.85 |  |
| 2.1-3.0 | 23 | 37 | 12 | 9 | 5 | 1 | 15 | 38 | 104 | 229 | 458 | 172 | 92 | 135 | 132 | 11 | 0 | 1473 | 4.6-6.7 |
| (1) | . 36 | . 58 | . 19 | . 14 | . 08 | . 02 | . 24 | . 60 | 1.64 | 3.62 | 7.24 | 2.72 | 1.45 | 2.13 | 2.09 | . 17 | . 00 | 23.28 |  |
| (2) | . 04 | . 06 | . 02 | . 01 | . 01 | . 00 | . 02 | . 06 | . 17 | . 38 | . 76 | . 29 | . 15 | . 22 | . 22 | . 02 | . 00 | 2.45 |  |
| $3.1-4.0$ | 2 | 9 | 2 | 2 | 0 | 0 | 0 | 1 | 12 | 25 | 81 | 16 | 6 | 5 | 12 | 1 | 0 | 174 | 6.8-8.9 |
| (1) | . 03 | . 14 | . 03 | . 03 | . 00 | . 00 | . 00 | . 02 | . 19 | . 40 | 1.28 | . 25 | . 09 | . 08 | . 19 | . 02 | . 00 | 2.75 |  |
| (2) | . 00 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 04 | . 13 | . 03 | . 01 | . 01 | . 02 | . 00 | . 00 | . 29 |  |
| 4.1-5.0 | 3 | 4 | 3 | 8 | 2 | 0 | 0 | 0 | 1 | 2 | 11 | 0 | 1 | 0 | 2 | 0 | 0 | 37 | 9.0-11.2 |
| (1) | . 05 | . 06 | . 05 | . 13 | . 03 | . 00 | . 00 | . 00 | . 02 | . 03 | . 17 | . 00 | . 02 | . 00 | . 03 | . 00 | . 00 | . 58 |  |
| (2) | . 00 | . 01 | . 00 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 06 |  |
| 5.1-6.0 | 5 | 1 | 2 | 6 | 2 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 2 | 0 | 21 | 11.3-13.4 |
| (1) | . 08 | . 02 | . 03 | . 09 | . 03 | . 00 | . 00 | . 00 | . 00 | . 00 | . 03 | . 00 | . 02 | . 00 | . 00 | . 03 | . 00 | . 33 |  |
| (2) | . 01 | . 00 | . 00 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 03 |  |
| $6.1-8.0$ | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 13.5-17.9 |
| (1) | . 02 | . 02 | . 03 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 06 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 |  |
| 8.1-10.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 18.0-22.4 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $22.5-200.2$ |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| ALL SPEEDS | 110 | 140 | 107 | 90 | 63 | 82 | 119 | 276 | 643 | 1151 | 1467 | 679 | 431 | 506 | 357 | 107 | 0 | 6328 |  |
| (1) | 1.74 | 2.21 | 1.69 | 1.42 | 1.00 | 1.30 | 1.88 | 4.36 | 10.16 | 18.19 | 23.18 | 10.73 | 6.81 | 8.00 | 5.64 | 1.69 | . 00 | 100.00 |  |
| (2) | . 18 | . 23 | . 18 | . 15 | . 10 | . 14 | . 20 | . 46 | 1.07 | 1.91 | 2.44 | 1.13 | . 72 | . 84 | . 59 | . 18 | . 00 | 10.52 |  |
| (1) = PERCENT | OF ALL | GOOD | OBSERV | ATIONS | FOR | HIS PA |  |  |  |  |  |  |  |  |  |  |  |  |  |
| (2) =PERCENT | OF ALL | GOOD | OBSERV | ATIONS | FOR | HIS PER | RIOD |  |  |  |  |  |  |  |  |  |  |  |  |

Table 2.3-134—\{CCNPP $33^{\prime}(10-m)$ 2000-2006 Annual Joint Frequency Distribution Table\} (Page 7 of 8)
CC JANOO-DECO6 MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
 WIND DIRECTION FROM

| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL | SPEED |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | MPH |
| LT . 2 | 0 | 1 | 1 | 2 | 2 | 1 | 2 | 3 | 9 | 5 | 12 | 15 | 3 | 1 | 2 | 2 | 0 | 61 | LT . 4 |
| (1) | . 00 | . 02 | . 02 | . 04 | . 04 | . 02 | . 04 | . 07 | . 20 | . 11 | . 27 | . 33 | . 07 | . 02 | . 04 | . 04 | . 00 | 1.35 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 01 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 10 |  |
| . $2-.4$ | 2 | 0 | 2 | 3 | 1 | 7 | 3 | 6 | 16 | 23 | 24 | 18 | 18 | 7 | 7 | 3 | 0 | 140 | . $4-.9$ |
| (1) | . 04 | . 00 | . 04 | . 07 | . 02 | . 15 | . 07 | . 13 | . 35 | . 51 | . 53 | . 40 | . 40 | . 15 | . 15 | . 07 | . 00 | 3.09 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 00 | . 01 | . 03 | . 04 | . 04 | . 03 | . 03 | . 01 | . 01 | . 00 | . 00 | . 23 |  |
| . $5-1.0$ | 15 | 4 | 9 | 12 | 9 | 12 | 9 | 30 | 64 | 119 | 193 | 196 | 162 | 108 | 21 | 12 | 0 | 975 | 1.0-2.2 |
| (1) | . 33 | . 09 | . 20 | . 27 | . 20 | . 27 | . 20 | . 66 | 1.41 | 2.63 | 4.27 | 4.33 | 3.58 | 2.39 | . 46 | . 27 | . 00 | 21.55 |  |
| (2) | . 02 | . 01 | . 01 | . 02 | . 01 | . 02 | . 01 | . 05 | . 11 | . 20 | . 32 | . 33 | . 27 | . 18 | . 03 | . 02 | . 00 | 1.62 |  |
| 1.1-1.5 | 6 | 6 | 9 | 8 | 2 | 6 | 7 | 23 | 119 | 393 | 488 | 270 | 167 | 126 | 18 | 3 | 0 | 1651 | $2.3-3.4$ |
| (1) | . 13 | . 13 | . 20 | . 18 | . 04 | . 13 | . 15 | . 51 | 2.63 | 8.69 | 10.79 | 5.97 | 3.69 | 2.79 | . 40 | . 07 | . 00 | 36.49 |  |
| (2) | . 01 | . 01 | . 01 | . 01 | . 00 | . 01 | . 01 | . 04 | . 20 | . 65 | . 81 | . 45 | . 28 | . 21 | . 03 | . 00 | . 00 | 2.74 |  |
| 1.6-2.0 | 1 | 8 | 2 | 9 | 0 | 8 | 4 | 22 | 82 | 263 | 378 | 138 | 108 | 126 | 26 | 5 | 0 | 1180 | $3.5-4.5$ |
| (1) | . 02 | . 18 | . 04 | . 20 | . 00 | . 18 | . 09 | . 49 | 1.81 | 5.81 | 8.36 | 3.05 | 2.39 | 2.79 | . 57 | . 11 | . 00 | 26.08 |  |
| (2) | . 00 | . 01 | . 00 | . 01 | . 00 | . 01 | . 01 | . 04 | . 14 | . 44 | . 63 | . 23 | . 18 | . 21 | . 04 | . 01 | . 00 | 1.96 |  |
| 2.1-3.0 | 1 | 4 | 3 | 0 | 0 | 2 | 2 | 7 | 22 | 64 | 160 | 72 | 55 | 51 | 21 | 2 | 0 | 466 | 4.6-6.7 |
| (1) | . 02 | . 09 | . 07 | . 00 | . 00 | . 04 | . 04 | . 15 | . 49 | 1.41 | 3.54 | 1.59 | 1.22 | 1.13 | . 46 | . 04 | . 00 | 10.30 |  |
| (2) | . 00 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 04 | . 11 | . 27 | . 12 | . 09 | . 08 | . 03 | . 00 | . 00 | . 77 |  |
| $3.1-4.0$ | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 3 | 3 | 1 | 3 | 0 | 2 | 0 | 0 | 14 | 6.8-8.9 |
| (1) | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 07 | . 07 | . 02 | . 07 | . 00 | . 04 | . 00 | . 00 | . 31 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |  |
| 4.1-5.0 | 0 | 1 | 2 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 5 | 0 | 0 | 16 | 9.0-11.2 |
| (1) | . 00 | . 02 | . 04 | . 11 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 02 | . 11 | . 00 | . 00 | . 35 |  |
| (2) | . 00 | . 00 | . 00 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 00 | . 00 | . 03 |  |
| 5.1-6.0 | 0 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 7 | 11.3-13.4 |
| (1) | . 00 | . 00 | . 07 | . 04 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 15 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 |  |
| $6.1-8.0$ | 0 | 0 | 8 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 13.5-17.9 |
| (1) | . 00 | . 00 | . 18 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 20 |  |
| (2) | . 00 | . 00 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 |  |
| 8.1-10.0 | 0 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 18.0-22.4 |
| (1) | . 00 | . 00 | . 07 | . 04 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 11 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 |  |
| 10.1-89.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $22.5-200.2$ |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| ALL SPEEDS | 25 | 25 | 42 | 44 | 15 | 36 | 27 | 92 | 312 | 870 | 1259 | 710 | 516 | 421 | 103 | 27 | 0 | 4524 |  |
| (1) | . 55 | . 55 | . 93 | . 97 | . 33 | . 80 | . 60 | 2.03 | 6.90 | 19.23 | 27.83 | 15.69 | 11.41 | 9.31 | 2.28 | . 60 | . 00 | 100.00 |  |
| (2) | . 04 | . 04 | . 07 | . 07 | . 02 | . 06 | . 04 | . 15 | . 52 | 1.45 | 2.09 | 1.18 | . 86 | . 70 | . 17 | . 04 | . 00 | 7.52 |  |
| (1) = PERCENT | ALL | GOOD | BSERV | TIONS | OR I | IS PA |  |  |  |  |  |  |  |  |  |  |  |  |  |
| (2) =PERCENT | ALL | GOOD | SERV | TIONS | OR I | IS PE | IOD |  |  |  |  |  |  |  |  |  |  |  |  |

Table 2.3-134—\{CCNPP $33^{\prime}(10-m)$ 2000-2006 Annual Joint Frequency Distribution Table\} (Page 8 of 8)
CC JANOO-DEC06 MET DATA JOINT FREQUENCY DISTRIBUTION ( 60 -METER TOWER)

| 33.0 FT WIND DATA STABILITY CLASS ALL $\quad$ CLASS FREQUENCY (PERCENT) $=100.00$ |
| :---: | :---: | :---: | WIND DIRECTION FROM


| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL | SPEED |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | MPH |
| LT . 2 | 3 | 8 | 3 | 4 | 7 | 4 | 9 | 11 | 24 | 19 | 36 | 33 | 11 | 7 | 10 | 5 | 0 | 194 | LT . 4 |
| (1) | . 00 | . 01 | . 00 | . 01 | . 01 | . 01 | . 01 | . 02 | . 04 | . 03 | . 06 | . 05 | . 02 | . 01 | . 02 | . 01 | . 00 | . 32 |  |
| (2) | . 00 | . 01 | . 00 | . 01 | . 01 | . 01 | . 01 | . 02 | . 04 | . 03 | . 06 | . 05 | . 02 | . 01 | . 02 | . 01 | . 00 | . 32 |  |
| . $2-.4$ | 6 | 5 | 15 | 9 | 14 | 23 | 20 | 29 | 46 | 63 | 47 | 38 | 44 | 29 | 16 | 11 | 0 | 415 | . $4-.9$ |
| (1) | . 01 | . 01 | . 02 | . 01 | . 02 | . 04 | . 03 | . 05 | . 08 | . 10 | . 08 | . 06 | . 07 | . 05 | . 03 | . 02 | . 00 | . 69 |  |
| (2) | . 01 | . 01 | . 02 | . 01 | . 02 | . 04 | . 03 | . 05 | . 08 | . 10 | . 08 | . 06 | . 07 | . 05 | . 03 | . 02 | . 00 | . 69 |  |
| . $5-1.0$ | 135 | 111 | 128 | 105 | 138 | 164 | 143 | 204 | 327 | 453 | 570 | 443 | 354 | 273 | 136 | 145 | 0 | 3829 | 1.0-2.2 |
| (1) | . 22 | . 18 | . 21 | . 17 | . 23 | . 27 | . 24 | . 34 | . 54 | . 75 | . 95 | . 74 | . 59 | . 45 | . 23 | . 24 | . 00 | 6.36 |  |
| (2) | . 22 | . 18 | . 21 | . 17 | . 23 | . 27 | . 24 | . 34 | . 54 | . 75 | . 95 | . 74 | . 59 | . 45 | . 23 | . 24 | . 00 | 6.36 |  |
| 1.1-1.5 | 241 | 253 | 211 | 211 | 261 | 220 | 231 | 338 | 651 | 1175 | 1244 | 702 | 491 | 439 | 295 | 172 | 0 | 7135 | $2.3-3.4$ |
| (1) | . 40 | . 42 | . 35 | . 35 | . 43 | . 37 | . 38 | . 56 | 1.08 | 1.95 | 2.07 | 1.17 | . 82 | . 73 | . 49 | . 29 | . 00 | 11.86 |  |
| (2) | . 40 | . 42 | . 35 | . 35 | . 43 | . 37 | . 38 | . 56 | 1.08 | 1.95 | 2.07 | 1.17 | . 82 | . 73 | . 49 | . 29 | . 00 | 11.86 |  |
| 1.6-2.0 | 371 | 501 | 320 | 398 | 396 | 297 | 329 | 460 | 743 | 1112 | 1338 | 711 | 542 | 576 | 471 | 305 | 0 | 8870 | $3.5-4.5$ |
| (1) | . 62 | . 83 | . 53 | . 66 | . 66 | . 49 | . 55 | . 76 | 1.24 | 1.85 | 2.22 | 1.18 | . 90 | . 96 | . 78 | . 51 | . 00 | 14.74 |  |
| (2) | . 62 | . 83 | . 53 | . 66 | . 66 | . 49 | . 55 | . 76 | 1.24 | 1.85 | 2.22 | 1.18 | . 90 | . 96 | . 78 | . 51 | . 00 | 14.74 |  |
| 2.1-3.0 | 1129 | 1304 | 899 | 903 | 738 | 495 | 599 | 969 | 1139 | 1476 | 2338 | 1214 | 772 | 818 | 1179 | 740 | 0 | 16712 | 4.6-6.7 |
| (1) | 1.88 | 2.17 | 1.49 | 1.50 | 1.23 | . 82 | 1.00 | 1.61 | 1.89 | 2.45 | 3.89 | 2.02 | 1.28 | 1.36 | 1.96 | 1.23 | . 00 | 27.78 |  |
| (2) | 1.88 | 2.17 | 1.49 | 1.50 | 1.23 | . 82 | 1.00 | 1.61 | 1.89 | 2.45 | 3.89 | 2.02 | 1.28 | 1.36 | 1.96 | 1.23 | . 00 | 27.78 |  |
| 3.1-4.0 | 1199 | 905 | 805 | 541 | 254 | 191 | 372 | 911 | 540 | 770 | 1643 | 699 | 421 | 495 | 937 | 782 | 0 | 11465 | 6.8-8.9 |
| (1) | 1.99 | 1.50 | 1.34 | . 90 | . 42 | . 32 | . 62 | 1.51 | . 90 | 1.28 | 2.73 | 1.16 | . 70 | . 82 | 1.56 | 1.30 | . 00 | 19.06 |  |
| (2) | 1.99 | 1.50 | 1.34 | . 90 | . 42 | . 32 | . 62 | 1.51 | . 90 | 1.28 | 2.73 | 1.16 | . 70 | . 82 | 1.56 | 1.30 | . 00 | 19.06 |  |
| 4.1-5.0 | 758 | 471 | 556 | 281 | 68 | 39 | 142 | 484 | 212 | 373 | 752 | 268 | 230 | 432 | 687 | 506 | 0 | 6259 | 9.0-11.2 |
| (1) | 1.26 | . 78 | . 92 | . 47 | . 11 | . 06 | . 24 | . 80 | . 35 | . 62 | 1.25 | . 45 | . 38 | . 72 | 1.14 | . 84 | . 00 | 10.40 |  |
| (2) | 1.26 | . 78 | . 92 | . 47 | . 11 | . 06 | . 24 | . 80 | . 35 | . 62 | 1.25 | . 45 | . 38 | . 72 | 1.14 | . 84 | . 00 | 10.40 |  |
| 5.1-6.0 | 432 | 247 | 342 | 144 | 5 | 7 | 43 | 237 | 56 | 130 | 289 | 70 | 112 | 337 | 509 | 211 | 0 | 3171 | 11.3-13.4 |
| (1) | . 72 | . 41 | . 57 | . 24 | . 01 | . 01 | . 07 | . 39 | . 09 | . 22 | . 48 | . 12 | . 19 | . 56 | . 85 | . 35 | . 00 | 5.27 |  |
| (2) | . 72 | . 41 | . 57 | . 24 | . 01 | . 01 | . 07 | . 39 | . 09 | . 22 | . 48 | . 12 | . 19 | . 56 | . 85 | . 35 | . 00 | 5.27 |  |
| 6.1-8.0 | 262 | 119 | 249 | 68 | 3 | 3 | 19 | 132 | 28 | 44 | 60 | 33 | 48 | 300 | 361 | 88 | 0 | 1817 | 13.5-17.9 |
| (1) | . 44 | . 20 | . 41 | . 11 | . 00 | . 00 | . 03 | . 22 | . 05 | . 07 | . 10 | . 05 | . 08 | . 50 | . 60 | . 15 | . 00 | 3.02 |  |
| (2) | . 44 | . 20 | . 41 | . 11 | . 00 | . 00 | . 03 | . 22 | . 05 | . 07 | . 10 | . 05 | . 08 | . 50 | . 60 | . 15 | . 00 | 3.02 |  |
| 8.1-10.0 | 44 | 12 | 50 | 12 | 1 | 0 | 4 | 15 | 1 | 4 | 1 | 3 | 6 | 45 | 41 | 8 | 0 | 247 | 18.0-22.4 |
| (1) | . 07 | . 02 | . 08 | . 02 | . 00 | . 00 | . 01 | . 02 | . 00 | . 01 | . 00 | . 00 | . 01 | . 07 | . 07 | . 01 | . 00 | . 41 |  |
| (2) | . 07 | . 02 | . 08 | . 02 | . 00 | . 00 | . 01 | . 02 | . 00 | . 01 | . 00 | . 00 | . 01 | . 07 | . 07 | . 01 | . 00 | . 41 |  |
| 10.1-89.5 | 5 | 2 | 22 | 5 | 1 | 2 | 3 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 1 | 0 | 0 | 45 | $22.5-200.2$ |
| (1) | . 01 | . 00 | . 04 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 |  |
| (2) | . 01 | . 00 | . 04 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 |  |
| ALL SPEEDS | 4585 | 3938 | 3600 | 2681 | 1886 | 1445 | 1914 | 3791 | 3767 | 5619 | 8318 | 4214 | 3032 | 3753 | 4643 | 2973 | 0 | 60159 |  |
| (1) | 7.62 | 6.55 | 5.98 | 4.46 | 3.14 | 2.40 | 3.18 | 6.30 | 6.26 | 9.34 | 13.83 | 7.00 | 5.04 | 6.24 | 7.72 | 4.94 | . 00 | 100.00 |  |
| (2) | 7.62 | 6.55 | 5.98 | 4.46 | 3.14 | 2.40 | 3.18 | 6.30 | 6.26 | 9.34 | 13.83 | 7.00 | 5.04 | 6.24 | 7.72 | 4.94 | . 00 | 100.00 |  |
| (1) =PERCENT | OF ALL | GOOD | OBSERV | ATIONS | FOR I | HIS PA |  |  |  |  |  |  |  |  |  |  |  |  |  |
| (2) =PERCENT | OF ALL | GOOD | OBSERV | ATIONS | FOR T | HIS P | RIOD |  |  |  |  |  |  |  |  |  |  |  |  |

Table 2．3－135—\｛CCNPP $197^{\prime}(60-m)$ 2000－2006 Annual Joint Frequency Distribution Table\}
（Page 1 of 8）
CC JANOO－DEC06 MET DATA JOINT EREQUENCY DISTRIBUTION（ $60-$－METER TOWER）197．0 FT WIND DATA STABILITY CLASS A CLASS FREQUENCY（PERCENT）$=10.94$



| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ．2－． 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | ． $4-.9$ |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |  |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |  |
| ． $5-1.0$ | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1．0－2．2 |
| （1） | ． 00 | ． 00 | ． 02 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 03 |  |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 |  |
| 1．1－1．5 | 2 | 3 | 2 | 3 | 4 | 2 | 1 | 1 | 0 | 1 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 22 | $2.3-3.4$ |
| （1） | ． 03 | ． 05 | ． 03 | ． 05 | ． 06 | ． 03 | ． 02 | ． 02 | ． 00 | ． 02 | ． 00 | ． 02 | ． 02 | ． 02 | ． 00 | ． 00 | ． 00 | ． 34 |  |
| （2） | ． 00 | ． 01 | ． 00 | ． 01 | ． 01 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 04 |  |
| 1．6－2．0 | 12 | 13 | 9 | 12 | 20 | 1 | 1 | 1 | 2 | 4 | 12 | 11 | 6 | 0 | 1 | 6 | 0 | 111 | $3.5-4.5$ |
| （1） | ． 18 | ． 20 | ． 14 | ． 18 | ． 31 | ． 02 | ． 02 | ． 02 | ． 03 | ． 06 | ． 18 | ． 17 | ． 09 | ． 00 | ． 02 | ． 09 | ． 00 | 1.70 |  |
| （2） | ． 02 | ． 02 | ． 02 | ． 02 | ． 03 | ． 00 | ． 00 | ． 00 | ． 00 | ． 01 | ． 02 | ． 02 | ． 01 | ． 00 | ． 00 | ． 01 | ． 00 | ． 19 |  |
| 2．1－3．0 | 75 | 91 | 58 | 55 | 76 | 48 | 26 | 22 | 29 | 48 | 77 | 33 | 17 | 10 | 10 | 15 | 0 | 690 | 4．6－6．7 |
| （1） | 1.15 | 1.39 | ． 89 | ． 84 | 1.16 | ． 73 | ． 40 | ． 34 | ． 44 | ． 73 | 1.18 | ． 51 | ． 26 | ． 15 | ． 15 | ． 23 | ． 00 | 10.56 |  |
| （2） | ． 13 | ． 15 | ． 10 | ． 09 | ． 13 | ． 08 | ． 04 | ． 04 | ． 05 | ． 08 | ． 13 | ． 06 | ． 03 | ． 02 | ． 02 | ． 03 | ． 00 | 1.16 |  |
| 3．1－4．0 | 166 | 181 | 38 | 18 | 30 | 54 | 63 | 91 | 54 | 120 | 157 | 93 | 42 | 27 | 18 | 22 | 0 | 1174 | $6.8-8.9$ |
| （1） | 2.54 | 2.77 | ． 58 | ． 28 | ． 46 | ． 83 | ． 96 | 1.39 | ． 83 | 1.84 | 2.40 | 1.42 | ． 64 | ． 41 | ． 28 | ． 34 | ． 00 | 17.97 |  |
| （2） | ． 28 | ． 30 | ． 06 | ． 03 | ． 05 | ． 09 | ． 11 | ． 15 | ． 09 | ． 20 | ． 26 | ． 16 | ． 07 | ． 05 | ． 03 | ． 04 | ． 00 | 1.97 |  |
| 4．1－5．0 | 246 | 132 | 20 | 6 | 14 | 32 | 79 | 112 | 52 | 150 | 222 | 112 | 64 | 50 | 59 | 42 | 0 | 1392 | 9．0－11．2 |
| （1） | 3.77 | 2.02 | ． 31 | ． 09 | ． 21 | ． 49 | 1.21 | 1.71 | ． 80 | 2.30 | 3.40 | 1.71 | ． 98 | ． 77 | ． 90 | ． 64 | ． 00 | 21.31 |  |
| （2） | ． 41 | ． 22 | ． 03 | ． 01 | ． 02 | ． 05 | ． 13 | ． 19 | ． 09 | ． 25 | ． 37 | ． 19 | ． 11 | ． 08 | ． 10 | ． 07 | ． 00 | 2.33 |  |
| 5．1－6．0 | 154 | 93 | 14 | 1 | 7 | 6 | 55 | 91 | 39 | 108 | 203 | 89 | 62 | 75 | 72 | 56 | 0 | 1125 | 11．3－13．4 |
| （1） | 2.36 | 1.42 | ． 21 | ． 02 | ． 11 | ． 09 | ． 84 | 1.39 | ． 60 | 1.65 | 3.11 | 1.36 | ． 95 | 1.15 | 1.10 | ． 86 | ． 00 | 17.22 |  |
| （2） | ． 26 | ． 16 | ． 02 | ． 00 | ． 01 | ． 01 | ． 09 | ． 15 | ． 07 | ． 18 | ． 34 | ． 15 | ． 10 | ． 13 | ． 12 | ． 09 | ． 00 | 1.88 |  |
| 6．1－8．0 | 141 | 78 | 22 | 5 | 6 | 6 | 39 | 89 | 28 | 152 | 244 | 87 | 78 | 180 | 168 | 64 | 0 | 1387 | 13．5－17．9 |
| （1） | 2.16 | 1.19 | ． 34 | ． 08 | ． 09 | ． 09 | ． 60 | 1.36 | ． 43 | 2.33 | 3.74 | 1.33 | 1.19 | 2.76 | 2.57 | ． 98 | ． 00 | 21.23 |  |
| （2） | ． 24 | ． 13 | ． 04 | ． 01 | ． 01 | ． 01 | ． 07 | ． 15 | ． 05 | ． 25 | ． 41 | ． 15 | ． 13 | ． 30 | ． 28 | ． 11 | ． 00 | 2.32 |  |
| 8．1－10．0 | 35 | 33 | 11 | 2 | 0 | 0 | 7 | 23 | 3 | 47 | 62 | 19 | 16 | 107 | 110 | 13 | 0 | 488 | 18．0－22．4 |
| （1） | ． 54 | ． 51 | ． 17 | ． 03 | ． 00 | ． 00 | ． 11 | ． 35 | ． 05 | ． 72 | ． 95 | ． 29 | ． 24 | 1.64 | 1.68 | ． 20 | ． 00 | 7.47 |  |
| （2） | ． 06 | ． 06 | ． 02 | ． 00 | ． 00 | ． 00 | ． 01 | ． 04 | ． 01 | ． 08 | ． 10 | ． 03 | ． 03 | ． 18 | ． 18 | ． 02 | ． 00 | ． 82 |  |
| 10．1－89．5 | 4 | 6 | 9 | 1 | 0 | 0 | 0 | 6 | 1 | 12 | 9 | 5 | 10 | 35 | 38 | 5 | 0 | 141 | $22.5-200.2$ |
| （1） | ． 06 | ． 09 | ． 14 | ． 02 | ． 00 | ． 00 | ． 00 | ． 09 | ． 02 | ． 18 | ． 14 | ． 08 | ． 15 | ． 54 | ． 58 | ． 08 | ． 00 | 2.16 |  |
| （2） | ． 01 | ． 01 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 01 | ． 00 | ． 02 | ． 02 | ． 01 | ． 02 | ． 06 | ． 06 | ． 01 | ． 00 | ． 24 |  |
| ALL SPEEDS | 835 | 630 | 184 | 103 | 158 | 149 | 271 | 436 | 208 | 642 | 986 | 450 | 296 | 485 | 476 | 223 | 0 | 6532 |  |
| （1） | 12.78 | 9.64 | 2.82 | 1.58 | 2.42 | 2.28 | 4.15 | 6.67 | 3.18 | 9.83 | 15.09 | 6.89 | 4.53 | 7.42 | 7.29 | 3.41 | ． 00 | 100.00 |  |
| （2） | 1.40 | 1.06 | ． 31 | ． 17 | ． 26 | ． 25 | ． 45 | ． 73 | ． 35 | 1.08 | 1.65 | ． 75 | ． 50 | ． 81 | ． 80 | ． 37 | ． 00 | 10.94 |  |

[^3]Table 2.3-135—\{CCNPP 197' (60-m) 2000-2006 Annual Joint Frequency Distribution Table\} (Page 2 of 8 )
CC JANOO-DECO6 MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS B ( LIASS FREQUENCY (PERCENT) $=4.50$ WIND DIRECTION FROM

## 

| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL | SPEED |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | MPH |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | LT . 4 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | . $4-.9$ |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| .5-1.0 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 7 | 1.0-2.2 |
| (1) | . 00 | . 04 | . 04 | . 00 | . 04 | . 00 | . 00 | . 04 | . 00 | . 00 | . 00 | . 00 | . 04 | . 00 | . 07 | . 00 | . 00 | . 26 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 |  |
| 1.1-1.5 | 2 | 4 | 2 | 5 | 3 | 3 | 3 | 1 | 0 | 0 | 4 | 2 | 1 | 0 | 0 | 0 | 0 | 30 | $2.3-3.4$ |
| (1) | . 07 | . 15 | . 07 | . 19 | . 11 | . 11 | . 11 | . 04 | . 00 | . 00 | . 15 | . 07 | . 04 | . 00 | . 00 | . 00 | . 00 | 1.12 |  |
| (2) | . 00 | . 01 | . 00 | . 01 | . 01 | . 01 | . 01 | . 00 | . 00 | . 00 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 |  |
| 1.6-2.0 | 6 | 10 | 14 | 20 | 10 | 11 | 3 | 1 | 4 | 3 | 7 | 5 | 1 | 1 | 3 | 3 | 0 | 102 | $3.5-4.5$ |
| (1) | . 22 | . 37 | . 52 | . 74 | . 37 | . 41 | . 11 | . 04 | . 15 | . 11 | . 26 | . 19 | . 04 | . 04 | . 11 | . 11 | . 00 | 3.79 |  |
| (2) | . 01 | . 02 | . 02 | . 03 | . 02 | . 02 | . 01 | . 00 | . 01 | . 01 | . 01 | . 01 | . 00 | . 00 | . 01 | . 01 | . 00 | . 17 |  |
| 2.1-3.0 | 66 | 81 | 48 | 38 | 68 | 30 | 22 | 17 | 12 | 26 | 25 | 33 | 14 | 9 | 4 | 13 | 0 | 506 | 4.6-6.7 |
| (1) | 2.45 | 3.01 | 1.79 | 1.41 | 2.53 | 1.12 | . 82 | . 63 | . 45 | . 97 | . 93 | 1.23 | . 52 | . 33 | . 15 | . 48 | . 00 | 18.82 |  |
| (2) | . 11 | . 14 | . 08 | . 06 | . 11 | . 05 | . 04 | . 03 | . 02 | . 04 | . 04 | . 06 | . 02 | . 02 | . 01 | . 02 | . 00 | . 85 |  |
| 3.1-4.0 | 94 | 87 | 16 | 12 | 13 | 22 | 37 | 42 | 20 | 26 | 46 | 38 | 29 | 24 | 13 | 17 | 0 | 536 | 6.8-8.9 |
| (1) | 3.50 | 3.24 | . 60 | . 45 | . 48 | . 82 | 1.38 | 1.56 | . 74 | . 97 | 1.71 | 1.41 | 1.08 | . 89 | . 48 | . 63 | . 00 | 19.93 |  |
| (2) | . 16 | . 15 | . 03 | . 02 | . 02 | . 04 | . 06 | . 07 | . 03 | . 04 | . 08 | . 06 | . 05 | . 04 | . 02 | . 03 | . 00 | . 90 |  |
| 4.1-5.0 | 78 | 46 | 8 | 4 | 5 | 11 | 30 | 56 | 17 | 33 | 51 | 38 | 22 | 20 | 20 | 20 | 0 | 459 | 9.0-11.2 |
| (1) | 2.90 | 1.71 | . 30 | . 15 | . 19 | . 41 | 1.12 | 2.08 | . 63 | 1.23 | 1.90 | 1.41 | . 82 | . 74 | . 74 | . 74 | . 00 | 17.07 |  |
| (2) | . 13 | . 08 | . 01 | . 01 | . 01 | . 02 | . 05 | . 09 | . 03 | . 06 | . 09 | . 06 | . 04 | . 03 | . 03 | . 03 | . 00 | . 77 |  |
| 5.1-6.0 | 49 | 26 | 9 | 1 | 3 | 1 | 25 | 42 | 8 | 37 | 59 | 22 | 20 | 22 | 29 | 21 | 0 | 374 | 11.3-13.4 |
| (1) | 1.82 | . 97 | . 33 | . 04 | . 11 | . 04 | . 93 | 1.56 | . 30 | 1.38 | 2.19 | . 82 | . 74 | . 82 | 1.08 | . 78 | . 00 | 13.91 |  |
| (2) | . 08 | . 04 | . 02 | . 00 | . 01 | . 00 | . 04 | . 07 | . 01 | . 06 | . 10 | . 04 | . 03 | . 04 | . 05 | . 04 | . 00 | . 63 |  |
| 6.1-8.0 | 43 | 18 | 16 | 3 | 2 | 3 | 7 | 28 | 9 | 38 | 53 | 20 | 27 | 42 | 57 | 33 | 0 | 399 | 13.5-17.9 |
| (1) | 1.60 | . 67 | . 60 | . 11 | . 07 | . 11 | . 26 | 1.04 | . 33 | 1.41 | 1.97 | . 74 | 1.00 | 1.56 | 2.12 | 1.23 | . 00 | 14.84 |  |
| (2) | . 07 | . 03 | . 03 | . 01 | . 00 | . 01 | . 01 | . 05 | . 02 | . 06 | . 09 | . 03 | . 05 | . 07 | . 10 | . 06 | . 00 | . 67 |  |
| 8.1-10.0 | 25 | 12 | 10 | 3 | 0 | 0 | 2 | 19 | 3 | 17 | 13 | 5 | 9 | 39 | 41 | 15 | 0 | 213 | 18.0-22.4 |
| (1) | . 93 | . 45 | . 37 | . 11 | . 00 | . 00 | . 07 | . 71 | . 11 | . 63 | . 48 | . 19 | . 33 | 1.45 | 1.52 | . 56 | . 00 | 7.92 |  |
| (2) | . 04 | . 02 | . 02 | . 01 | . 00 | . 00 | . 00 | . 03 | . 01 | . 03 | . 02 | . 01 | . 02 | . 07 | . 07 | . 03 | . 00 | . 36 |  |
| 10.1-89.5 | 5 | 7 | 2 | 1 | 0 | 0 | 0 | 3 | 3 | 0 | 3 | 3 | 1 | 13 | 17 | 5 | 0 | 63 | $22.5-200.2$ |
| (1) | . 19 | . 26 | . 07 | . 04 | . 00 | . 00 | . 00 | . 11 | . 11 | . 00 | . 11 | . 11 | . 04 | . 48 | . 63 | . 19 | . 00 | 2.34 |  |
| (2) | . 01 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 01 | . 00 | . 01 | . 01 | . 00 | . 02 | . 03 | . 01 | . 00 | . 11 |  |
| ALL SPEEDS | 368 | 292 | 126 | 87 | 105 | 81 | 129 | 210 | 76 | 180 | 261 | 166 | 125 | 170 | 186 | 127 | 0 | 2689 |  |
| (1) | 13.69 | 10.86 | 4.69 | 3.24 | 3.90 | 3.01 | 4.80 | 7.81 | 2.83 | 6.69 | 9.71 | 6.17 | 4.65 | 6.32 | 6.92 | 4.72 | . 00 | 100.00 |  |
| (2) | . 62 | . 49 | . 21 | . 15 | . 18 | . 14 | . 22 | . 35 | . 13 | . 30 | . 44 | . 28 | . 21 | . 28 | . 31 | . 21 | . 00 | 4.50 |  |
| (1) =PERCENT | OF ALI | GOOD | OBSERV | ATIONS | FOR | HIS PA |  |  |  |  |  |  |  |  |  |  |  |  |  |
| (2) =PERCENT | OF ALI | GOOD | OBSERV | ATIONS | FOR | HIS PER | RIOD |  |  |  |  |  |  |  |  |  |  |  |  |

Table 2.3-135—\{CCNPP 197' (60-m) 2000-2006 Annual Joint Frequency Distribution Table\} (Page 3 of 8 )
CC JANOO-DEC06 MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS C $\quad$ CLASS FREQUENCY (PERCENT) $=5.10$ 197.0 FT WIND DATA STABILITY CLASS C CLASS FREQUE

| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL | SPEED |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | MPH |
| LT . 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | LT. 4 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| . $2-.4$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | . $4-.9$ |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| . $5-1.0$ | 1 | 1 | 1 | 0 | 0 | 2 | 1 | 1 | 1 | 1 | 0 | 4 | 0 | 1 | 0 | 0 | 0 | 14 | 1.0-2.2 |
| (1) | . 03 | . 03 | . 03 | . 00 | . 00 | . 07 | . 03 | . 03 | . 03 | . 03 | . 00 | . 13 | . 00 | . 03 | . 00 | . 00 | . 00 | . 46 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |  |
| 1.1-1.5 | 3 | 7 | 9 | 8 | 8 | 1 | 3 | 1 | 2 | 1 | 4 | 4 | 3 | 1 | 3 | 3 | 0 | 61 | $2.3-3.4$ |
| (1) | . 10 | . 23 | . 30 | . 26 | . 26 | . 03 | . 10 | . 03 | . 07 | . 03 | . 13 | . 13 | . 10 | . 03 | . 10 | . 10 | . 00 | 2.00 |  |
| (2) | . 01 | . 01 | . 02 | . 01 | . 01 | . 00 | . 01 | . 00 | . 00 | . 00 | . 01 | . 01 | . 01 | . 00 | . 01 | . 01 | . 00 | . 10 |  |
| 1.6-2.0 | 15 | 33 | 22 | 26 | 27 | 13 | 6 | 6 | 2 | 4 | 16 | 10 | 8 | 5 | 4 | 4 | 0 | 201 | $3.5-4.5$ |
| (1) | . 49 | 1.08 | . 72 | . 85 | . 89 | . 43 | . 20 | . 20 | . 07 | . 13 | . 53 | . 33 | . 26 | . 16 | . 13 | . 13 | . 00 | 6.61 |  |
| (2) | . 03 | . 06 | . 04 | . 04 | . 05 | . 02 | . 01 | . 01 | . 00 | . 01 | . 03 | . 02 | . 01 | . 01 | . 01 | . 01 | . 00 | . 34 |  |
| 2.1-3.0 | 67 | 103 | 54 | 65 | 56 | 40 | 35 | 27 | 21 | 17 | 43 | 29 | 20 | 19 | 6 | 12 | 0 | 614 | 4.6-6.7 |
| (1) | 2.20 | 3.38 | 1.77 | 2.14 | 1.84 | 1.31 | 1.15 | . 89 | . 69 | . 56 | 1.41 | . 95 | . 66 | . 62 | . 20 | . 39 | . 00 | 20.18 |  |
| (2) | . 11 | . 17 | . 09 | . 11 | . 09 | . 07 | . 06 | . 05 | . 04 | . 03 | . 07 | . 05 | . 03 | . 03 | . 01 | . 02 | . 00 | 1.03 |  |
| 3.1-4.0 | 118 | 95 | 32 | 14 | 18 | 24 | 33 | 39 | 26 | 26 | 58 | 47 | 31 | 21 | 30 | 32 | 0 | 644 | $6.8-8.9$ |
| (1) | 3.88 | 3.12 | 1.05 | . 46 | . 59 | . 79 | 1.08 | 1.28 | . 85 | . 85 | 1.91 | 1.54 | 1.02 | . 69 | . 99 | 1.05 | . 00 | 21.16 |  |
| (2) | . 20 | . 16 | . 05 | . 02 | . 03 | . 04 | . 06 | . 07 | . 04 | . 04 | . 10 | . 08 | . 05 | . 04 | . 05 | . 05 | . 00 | 1.08 |  |
| 4.1-5.0 | 72 | 49 | 11 | 3 | 11 | 9 | 20 | 68 | 18 | 38 | 54 | 37 | 24 | 22 | 37 | 35 | 0 | 508 | 9.0-11.2 |
| (1) | 2.37 | 1.61 | . 36 | . 10 | . 36 | . 30 | . 66 | 2.23 | . 59 | 1.25 | 1.77 | 1.22 | . 79 | . 72 | 1.22 | 1.15 | . 00 | 16.69 |  |
| (2) | . 12 | . 08 | . 02 | . 01 | . 02 | . 02 | . 03 | . 11 | . 03 | . 06 | . 09 | . 06 | . 04 | . 04 | . 06 | . 06 | . 00 | . 85 |  |
| 5.1-6.0 | 48 | 27 | 8 | 6 | 1 | 2 | 6 | 41 | 10 | 27 | 48 | 31 | 17 | 23 | 26 | 27 | 0 | 348 | 11.3-13.4 |
| (1) | 1.58 | . 89 | . 26 | . 20 | . 03 | . 07 | . 20 | 1.35 | . 33 | . 89 | 1.58 | 1.02 | . 56 | . 76 | . 85 | . 89 | . 00 | 11.44 |  |
| (2) | . 08 | . 05 | . 01 | . 01 | . 00 | . 00 | . 01 | . 07 | . 02 | . 05 | . 08 | . 05 | . 03 | . 04 | . 04 | . 05 | . 00 | . 58 |  |
| $6.1-8.0$ | 36 | 31 | 19 | 5 | 1 | 2 | 9 | 39 | 12 | 38 | 45 | 25 | 21 | 32 | 63 | 30 | 0 | 408 | 13.5-17.9 |
| (1) | 1.18 | 1.02 | . 62 | . 16 | . 03 | . 07 | . 30 | 1.28 | . 39 | 1.25 | 1.48 | . 82 | . 69 | 1.05 | 2.07 | . 99 | . 00 | 13.41 |  |
| (2) | . 06 | . 05 | . 03 | . 01 | . 00 | . 00 | . 02 | . 07 | . 02 | . 06 | . 08 | . 04 | . 04 | . 05 | . 11 | . 05 | . 00 | . 68 |  |
| 8.1-10.0 | 13 | 26 | 9 | 3 | 1 | 0 | 2 | 10 | 2 | 8 | 18 | 3 | 5 | 33 | 34 | 7 | 0 | 174 | 18.0-22.4 |
| (1) | . 43 | . 85 | . 30 | . 10 | . 03 | . 00 | . 07 | . 33 | . 07 | . 26 | . 59 | . 10 | . 16 | 1.08 | 1.12 | . 23 | . 00 | 5.72 |  |
| (2) | . 02 | . 04 | . 02 | . 01 | . 00 | . 00 | . 00 | . 02 | . 00 | . 01 | . 03 | . 01 | . 01 | . 06 | . 06 | . 01 | . 00 | . 29 |  |
| 10.1-89.5 | 10 | 8 | 6 | 2 | 0 | 0 | 0 | 0 | 0 | 2 | 3 | 0 | 2 | 12 | 25 | 1 | 0 | 71 | 22.5-200.2 |
| (1) | . 33 | . 26 | . 20 | . 07 | . 00 | . 00 | . 00 | . 00 | . 00 | . 07 | . 10 | . 00 | . 07 | . 39 | . 82 | . 03 | . 00 | 2.33 |  |
| (2) | . 02 | . 01 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 00 | . 00 | . 02 | . 04 | . 00 | . 00 | . 12 |  |
| ALL SPEEDS | 383 | 380 | 171 | 132 | 123 | 93 | 115 | 232 | 94 | 162 | 289 | 190 | 131 | 169 | 228 | 151 | 0 | 3043 |  |
| (1) | 12.59 | 12.49 | 5.62 | 4.34 | 4.04 | 3.06 | 3.78 | 7.62 | 3.09 | 5.32 | 9.50 | 6.24 | 4.30 | 5.55 | 7.49 | 4.96 | . 00 | 100.00 |  |
| (2) | . 64 | . 64 | . 29 | . 22 | . 21 | . 16 | . 19 | . 39 | . 16 | . 27 | . 48 | . 32 | . 22 | . 28 | . 38 | . 25 | . 00 | 5.10 |  |
| (1) =PERCENT | OF ALI | GOOD | OBSERV | ATIONS | FOR | HIS PA |  |  |  |  |  |  |  |  |  |  |  |  |  |
| (2) =PERCENT | OF ALI | GOOD | OBSERV | ATIONS | FOR | HIS PER | RIOD |  |  |  |  |  |  |  |  |  |  |  |  |

Table 2.3-135—\{CCNPP 197' (60-m) 2000-2006 Annual Joint Frequency Distribution Table\} (Page 4 of 8)
CC JANOO-DEC06 MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA
ATABILITY CLASS D
WIND DIRECTION FROM


| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL | SPEED |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | MPH |
| LT . 2 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | LT . 4 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |  |
| . $2-.4$ | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 1 | 1 | 0 | 9 | . $4-.9$ |
| (1) | . 00 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 00 | . 00 | . 00 | . 04 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |  |
| . $5-1.0$ | 18 | 18 | 26 | 21 | 28 | 13 | 11 | 12 | 11 | 12 | 12 | 9 | 8 | 11 | 8 | 17 | 0 | 235 | 1.0-2.2 |
| (1) | . 09 | . 09 | . 13 | . 10 | . 14 | . 06 | . 05 | . 06 | . 05 | . 06 | . 06 | . 04 | . 04 | . 05 | . 04 | . 08 | . 00 | 1.16 |  |
| (2) | . 03 | . 03 | . 04 | . 04 | . 05 | . 02 | . 02 | . 02 | . 02 | . 02 | . 02 | . 02 | . 01 | . 02 | . 01 | . 03 | . 00 | . 39 |  |
| 1.1-1.5 | 45 | 52 | 47 | 55 | 57 | 41 | 24 | 15 | 16 | 17 | 22 | 22 | 24 | 19 | 20 | 21 | 0 | 497 | $2.3-3.4$ |
| (1) | . 22 | . 26 | . 23 | . 27 | . 28 | . 20 | . 12 | . 07 | . 08 | . 08 | . 11 | . 11 | . 12 | . 09 | . 10 | . 10 | . 00 | 2.45 |  |
| (2) | . 08 | . 09 | . 08 | . 09 | . 10 | . 07 | . 04 | . 03 | . 03 | . 03 | . 04 | . 04 | . 04 | . 03 | . 03 | . 04 | . 00 | . 83 |  |
| 1.6-2.0 | 72 | 106 | 77 | 99 | 119 | 59 | 36 | 22 | 32 | 25 | 57 | 36 | 35 | 27 | 29 | 52 | 0 | 883 | $3.5-4.5$ |
| (1) | . 36 | . 52 | . 38 | . 49 | . 59 | . 29 | . 18 | . 11 | . 16 | . 12 | . 28 | . 18 | . 17 | . 13 | . 14 | . 26 | . 00 | 4.36 |  |
| (2) | . 12 | . 18 | . 13 | . 17 | . 20 | . 10 | . 06 | . 04 | . 05 | . 04 | . 10 | . 06 | . 06 | . 05 | . 05 | . 09 | . 00 | 1.48 |  |
| 2.1-3.0 | 306 | 347 | 188 | 256 | 258 | 152 | 164 | 165 | 107 | 112 | 109 | 110 | 83 | 66 | 91 | 106 | 0 | 2620 | 4.6-6.7 |
| (1) | 1.51 | 1.71 | . 93 | 1.26 | 1.27 | . 75 | . 81 | . 81 | . 53 | . 55 | . 54 | . 54 | . 41 | . 33 | . 45 | . 52 | . 00 | 12.93 |  |
| (2) | . 51 | . 58 | . 31 | . 43 | . 43 | . 25 | . 27 | . 28 | . 18 | . 19 | . 18 | . 18 | . 14 | . 11 | . 15 | . 18 | . 00 | 4.39 |  |
| 3.1-4.0 | 279 | 282 | 174 | 287 | 230 | 194 | 198 | 240 | 167 | 144 | 174 | 148 | 109 | 101 | 143 | 206 | 0 | 3076 | 6.8-8.9 |
| (1) | 1.38 | 1.39 | . 86 | 1.42 | 1.14 | . 96 | . 98 | 1.18 | . 82 | . 71 | . 86 | . 73 | . 54 | . 50 | . 71 | 1.02 | . 00 | 15.19 |  |
| (2) | . 47 | . 47 | . 29 | . 48 | . 39 | . 32 | . 33 | . 40 | . 28 | . 24 | . 29 | . 25 | . 18 | . 17 | . 24 | . 35 | . 00 | 5.15 |  |
| 4.1-5.0 | 277 | 225 | 243 | 283 | 209 | 122 | 170 | 319 | 153 | 158 | 160 | 134 | 81 | 106 | 188 | 261 | 0 | 3089 | 9.0-11.2 |
| (1) | 1.37 | 1.11 | 1.20 | 1.40 | 1.03 | . 60 | . 84 | 1.57 | . 76 | . 78 | . 79 | . 66 | . 40 | . 52 | . 93 | 1.29 | . 00 | 15.25 |  |
| (2) | . 46 | . 38 | . 41 | . 47 | . 35 | . 20 | . 28 | . 53 | . 26 | . 26 | . 27 | . 22 | . 14 | . 18 | . 31 | . 44 | . 00 | 5.17 |  |
| 5.1-6.0 | 258 | 227 | 254 | 224 | 95 | 72 | 117 | 295 | 99 | 131 | 175 | 123 | 68 | 124 | 279 | 324 | 0 | 2865 | 11.3-13.4 |
| (1) | 1.27 | 1.12 | 1.25 | 1.11 | . 47 | . 36 | . 58 | 1.46 | . 49 | . 65 | . 86 | . 61 | . 34 | . 61 | 1.38 | 1.60 | . 00 | 14.14 |  |
| (2) | . 43 | . 38 | . 43 | . 38 | . 16 | . 12 | . 20 | . 49 | . 17 | . 22 | . 29 | . 21 | . 11 | . 21 | . 47 | . 54 | . 00 | 4.80 |  |
| 6.1-8.0 | 443 | 480 | 411 | 211 | 63 | 46 | 92 | 333 | 126 | 180 | 303 | 126 | 81 | 218 | 502 | 479 | 0 | 4094 | 13.5-17.9 |
| (1) | 2.19 | 2.37 | 2.03 | 1.04 | . 31 | . 23 | . 45 | 1.64 | . 62 | . 89 | 1.50 | . 62 | . 40 | 1.08 | 2.48 | 2.36 | . 00 | 20.21 |  |
| (2) | . 74 | . 80 | . 69 | . 35 | . 11 | . 08 | . 15 | . 56 | . 21 | . 30 | . 51 | . 21 | . 14 | . 37 | . 84 | . 80 | . 00 | 6.86 |  |
| 8.1-10.0 | 301 | 328 | 240 | 47 | 4 | 4 | 35 | 117 | 38 | 89 | 127 | 18 | 27 | 162 | 259 | 181 | 0 | 1977 | 18.0-22.4 |
| (1) | 1.49 | 1.62 | 1.18 | . 23 | . 02 | . 02 | . 17 | . 58 | . 19 | . 44 | . 63 | . 09 | . 13 | . 80 | 1.28 | . 89 | . 00 | 9.76 |  |
| (2) | . 50 | . 55 | . 40 | . 08 | . 01 | . 01 | . 06 | . 20 | . 06 | . 15 | . 21 | . 03 | . 05 | . 27 | . 43 | . 30 | . 00 | 3.31 |  |
| 10.1-89.5 | 173 | 238 | 131 | 21 | 2 | 2 | 12 | 35 | 11 | 23 | 15 | 9 | 12 | 86 | 91 | 48 | 0 | 909 | $22.5-200.2$ |
| (1) | . 85 | 1.17 | . 65 | . 10 | . 01 | . 01 | . 06 | . 17 | . 05 | . 11 | . 07 | . 04 | . 06 | . 42 | . 45 | . 24 | . 00 | 4.49 |  |
| (2) | . 29 | . 40 | . 22 | . 04 | . 00 | . 00 | . 02 | . 06 | . 02 | . 04 | . 03 | . 02 | . 02 | . 14 | . 15 | . 08 | . 00 | 1.52 |  |
| ALL SPEEDS | 2172 | 2306 | 1791 | 1504 | 1066 | 706 | 859 | 1554 | 760 | 891 | 1154 | 735 | 529 | 922 | 1611 | 1696 | 0 | 20256 |  |
| (1) | 10.72 | 11.38 | 8.84 | 7.42 | 5.26 | 3.49 | 4.24 | 7.67 | 3.75 | 4.40 | 5.70 | 3.63 | 2.61 | 4.55 | 7.95 | 8.37 | . 00 | 100.00 |  |
| (2) | 3.64 | 3.86 | 3.00 | 2.52 | 1.79 | 1.18 | 1.44 | 2.60 | 1.27 | 1.49 | 1.93 | 1.23 | . 89 | 1.54 | 2.70 | 2.84 | . 00 | 33.93 |  |
| (1) = PERCENT | OF ALL | GOOD | OBSERV | ATIONS | FOR T | HIS PA |  |  |  |  |  |  |  |  |  |  |  |  |  |
| (2) =PERCENT | OF ALL | GOOD | OBSERV | ATIONS | FOR T | HIS PER | RIOD |  |  |  |  |  |  |  |  |  |  |  |  |

Table 2．3－135—\｛CCNPP $197^{\prime}(60-m)$ 2000－2006 Annual Joint Frequency Distribution Table\} （Page 5 of 8）
CC JANOO－DEC06 MET DATA JOINT FREQUENCY DISTRIBUTION（60－METER TOWER）
197．0 FT WIND DATA STABILITY CLASS E CLASS FREQUENCY（PERCENT）$=27.60$ WIND DIRECTION FROM

| SPeed | N | NNE | NE | ene | E | ESE | SE | SSE | s | SSW | SW | WSW | W | WNW | NW | nNW | VRBL | TOTAL | Speed |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | MPH |
| LT ． 2 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 4 | LT ． 4 |
| （1） | ． 00 | ． 00 | ． 01 | ． 00 | ． 01 | ． 00 | ． 00 | ． 00 | ． 00 | ． 01 | ． 00 | ． 00 | ． 01 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 |  |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 01 |  |
| ． $2-.4$ | 2 |  | 2 | 1 | 1 | 0 | 1 | 1 | 2 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 12 | ． $4-.9$ |
| （1） | ． 01 | ． 00 | ． 01 | ． 01 | ． 01 | ． 00 | ． 01 | ． 01 | ． 01 | ． 00 | ． 00 | ． 00 | ． 01 | ． 00 | ． 01 | ． 00 | ． 00 | ． 07 |  |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 |  |
| ．5－1．0 | 12 | 8 | 21 | 13 | 25 | 18 | 13 | 21 | 7 | 14 | 7 |  | 8 | 8 | 12 | 11 | 0 | 206 | 1．0－2．2 |
| （1） | ． 07 | ． 05 | ． 13 | ． 08 | ． 15 | ． 11 | ． 08 | ． 13 | ． 04 | ． 08 | ． 04 | ． 05 | ． 05 | ． 05 | ． 07 | ． 07 | ． 00 | 1.25 |  |
| （2） | ． 02 | ． 01 | ． 04 | ． 02 | ． 04 | ． 03 | ． 02 | ． 04 | ． 01 | ． 02 | ． 01 | ． 01 | ． 01 | ． 01 | ． 02 | ． 02 | ． 00 | ． 35 |  |
| 1．1－1．5 | 19 | 21 | 19 | 21 | 18 | 14 | 22 | 17 | 15 | 14 | 13 | 8 | 9 | 13 | 13 | 13 | 0 | 249 | 2．3－3．4 |
| （1） | ． 12 | ． 13 | ． 12 | ． 13 | ． 11 | ． 08 | ． 13 | ． 10 | ． 09 | ． 08 | ． 08 | ． 05 | ． 05 | ． 08 | ． 08 | ． 08 | ． 00 | 1.51 |  |
| （2） | ． 03 | ． 04 | ． 03 | ． 04 | ． 03 | ． 02 | ． 04 | ． 03 | ． 03 | ． 02 | ． 02 | ． 01 | ． 02 | ． 02 | ． 02 | ． 02 | ． 00 | ． 42 |  |
| 1．6－2．0 | 25 | 41 | 36 | 35 | 51 | 26 | 20 | 29 | 29 | 21 | 21 | 19 | 12 | 20 | 14 | 15 | 0 | 414 | 3．5－4．5 |
| （1） | ． 15 | ． 25 | ． 22 | ． 21 | ． 31 | ． 16 | ． 12 | ． 18 | ． 18 | ． 13 | ． 13 | ． 12 | ． 07 | ． 12 | ． 08 | ． 09 | ． 00 | 2.51 |  |
| （2） | ． 04 | ． 07 | ． 06 | ． 06 | ． 09 | ． 04 | ． 03 | ． 05 | ． 05 | ． 04 | ． 04 | ． 03 | ． 02 | ． 03 | ． 02 | ． 03 | ． 00 | ． 69 |  |
| 2．1－3．0 | 92 | 89 | 91 | 98 | 116 | 80 | 79 | 86 | 84 | 62 | 95 | 60 | 67 | 78 | 88 | 94 | 0 | 1359 | 4．6－6．7 |
| （1） | ． 56 | ． 54 | ． 55 | ． 59 | ． 70 | ． 49 | ． 48 | ． 52 | ． 51 | ． 38 | ． 58 | ． 36 | ． 41 | ． 47 | ． 53 | ． 57 | ． 00 | 8.25 |  |
| （2） | ． 15 | ． 15 | ． 15 | ． 16 | ． 19 | ． 13 | ． 13 | ． 14 | ． 14 | ． 10 | ． 16 | ． 10 | ． 11 | ． 13 | ． 15 | ． 16 | ． 00 | 2.28 |  |
| 3．1－4．0 | 175 | 113 | 101 | 82 | 126 | 102 | 97 | 175 | 162 | 139 | 158 | 133 | 121 | 172 | 176 | 206 |  | 2238 | 6．8－8．9 |
| （1） | 1.06 | ． 69 | ． 61 | ． 50 | ． 76 | ． 62 | ． 59 | 1.06 | ． 98 | ． 84 | ． 96 | ． 81 | ． 73 | 1.04 | 1.07 | 1.25 | ． 00 | 13.59 |  |
| （2） | ． 29 | ． 19 | ． 17 | ． 14 | ． 21 | ． 17 | ． 16 | ． 29 | ． 27 | ． 23 | ． 26 | ． 22 | ． 20 | ． 29 | ． 29 | ． 35 | ． 00 | 3.75 |  |
| 4．1－5．0 | 192 | 125 | 96 | 50 | 44 | 103 | 142 | 305 | 325 | 231 | 219 | 193 | 161 | 298 | 401 | 377 | 0 | 3262 | 9．0－11．2 |
| （1） | 1.17 | ． 76 | ． 58 | ． 30 | ． 27 | ． 63 | ． 86 | 1.85 | 1.97 | 1.40 | 1.33 | 1.17 | ． 98 | 1.81 | 2.43 | 2.29 | ． 00 | 19.80 |  |
| （2） | ． 32 | ． 21 | ． 16 | ． 08 | ． 07 | ． 17 | ． 24 | ． 51 | ． 54 | ． 39 | ． 37 | ． 32 | ． 27 | ． 50 | ． 67 | ． 63 | ． 00 | 5.46 |  |
| 5．1－6．0 | 164 | 99 | 49 | 18 | 26 | 26 | 68 | 334 | 423 | 371 | 329 | 224 | 151 | 302 | 447 | 391 | 0 | 3422 | $11.3-13.4$ |
| （1） | 1.00 | ． 60 | ． 30 | ． 11 | ． 16 | ． 16 | ． 41 | 2.03 | 2.57 | 2.25 | 2.00 | 1.36 | ． 92 | 1.83 | 2.71 | 2.37 | ． 00 | 20.77 |  |
| （2） | ． 27 | ． 17 | ． 08 | ． 03 | ． 04 | ． 04 | ． 11 | ． 56 | ． 71 | ． 62 | ． 55 | ． 38 | ． 25 | ． 51 | ． 75 | ． 66 | ． 00 | 5.73 |  |
| 6．1－8．0 | 128 | 131 | 32 | T | 7 | 19 | 41 | 251 | 453 | 930 | 865 | 191 | 118 | 272 | 351 | 302 | 0 | 4098 | 13．5－17．9 |
| （1） | ． 78 | ． 80 | ． 19 | ． 04 | ． 04 | ． 12 | ． 25 | 1.52 | 2.75 | 5.65 | 5.25 | 1.16 | ． 72 | 1.65 | 2.13 | 1.83 | ． 00 | 24.88 |  |
| （2） | ． 21 | ． 22 | ． 05 | ． 01 | ． 01 | ． 03 | ． 07 | ． 42 | ． 76 | 1.56 | 1.45 | ． 32 | ． 20 | ． 46 | ． 59 | ． 51 | ． 00 | 6.87 |  |
| 8．1－10．0 | 56 | 27 | 8 | 2 | 3 | 4 | 7 | 65 | 84 | 274 | 273 | 28 | 20 | 70 | 47 | 37 | 0 | 1005 | 18．0－22．4 |
| （1） | ． 34 | ． 16 | ． 05 | ． 01 | ． 02 | ． 02 | ． 04 | ． 39 | ． 51 | 1.66 | 1.66 | ． 17 | ． 12 | ． 42 | ． 29 | ． 22 | ． 00 | 6.10 |  |
| （2） | ． 09 | ． 05 | ． 01 | ． 00 | ． 01 | ． 01 | ． 01 | ． 11 | ． 14 | ． 46 | ． 46 | ． 05 | ． 03 | ． 12 | ． 08 | ． 06 | ． 00 | 1.68 |  |
| 10．1－89．5 | 18 | 17 | 12 | 2 | 1 | 4 | 8 | 27 | 10 | 44 | 27 | 3 | 4 | 15 | 6 | 7 | 0 | 205 | 22．5－200．2 |
| （1） | ． 11 | ． 10 | ． 07 | ． 01 | ． 01 | ． 02 | ． 05 | ． 16 | ． 06 | ． 27 | ． 16 | ． 02 | ． 02 | ． 09 | ． 04 | ． 04 | ． 00 | 1.24 |  |
| （2） | ． 03 | ． 03 | ． 02 | ． 00 | ． 00 | ． 01 | ． 01 | ． 05 | ． 02 | ． 07 | ． 05 | ． 01 | ． 01 | ． 03 | ． 01 | ． 01 | ． 00 | ． 34 |  |
| ALL SPEEDS | 883 | 671 | 468 | 329 | 419 | 396 | 498 | 1311 | 1594 | 2101 | 2007 | 867 | 673 | 1248 | 1556 | 1453 | 0 | 16474 |  |
| （1） | 5.36 | 4.07 | 2.84 | 2.00 | 2.54 | 2.40 | 3.02 | 7.96 | 9.68 | 12.75 | 12.18 | 5.26 | 4.09 | 7.58 | 9.45 | 8.82 | ． 00 | 100.00 |  |
| （2） | 1.48 | 1.12 | ． 78 | ． 55 |  | ． 66 | ． 83 | 2.20 | 2.67 | 3.52 | 3.36 | 1.45 | 1.13 | 2.09 | 2.61 | 2.43 | ． 00 | 27.60 |  |
| （1）＝PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| （2）＝PERCENT | OF ALL | GOOD | OBSERV | ATIONS | FOR | HIS PE | RIOD |  |  |  |  |  |  |  |  |  |  |  |  |

Table 2.3-135—\{CCNPP $197^{\prime}(60-m)$ 2000-2006 Annual Joint Frequency Distribution Table\} (Page 6 of 8)
CC JANOO-DECO6 MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA STABILITY CLASS F ( LLASS FREQUENCY (PERCENT) $=10.44$ WIND DIRECTION FROM

## 

| SPEED | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | VRBL | TOTAL | SPEED |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | MPH |
| LT . 2 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 3 | LT. 4 |
| (1) | . 00 | . 00 | . 00 | . 02 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 05 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 |  |
| .2- . 4 | 2 | 1 | 0 | 0 | 0 | 1 | 1 | 2 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 10 | . $4-.9$ |
| (1) | . 03 | . 02 | . 00 | . 00 | . 00 | . 02 | . 02 | . 03 | . 02 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 16 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |  |
| . $5-1.0$ | 6 | 5 | 7 | 10 | 12 | 13 | 7 | 8 | 6 | 12 | 10 | 5 | 6 | 5 | 7 | 6 | 0 | 125 | 1.0-2.2 |
| (1) | . 10 | . 08 | . 11 | . 16 | . 19 | . 21 | . 11 | . 13 | . 10 | . 19 | . 16 | . 08 | . 10 | . 08 | . 11 | . 10 | . 00 | 2.01 |  |
| (2) | . 01 | . 01 | . 01 | . 02 | . 02 | . 02 | . 01 | . 01 | . 01 | . 02 | . 02 | . 01 | . 01 | . 01 | . 01 | . 01 | . 00 | . 21 |  |
| 1.1-1.5 | 8 | 10 | 9 | 8 | 18 | 7 | 9 | 12 | 11 | 7 | 7 | 4 | 9 | 9 | 9 | 8 | 0 | 145 | $2.3-3.4$ |
| (1) | . 13 | . 16 | . 14 | . 13 | . 29 | . 11 | . 14 | . 19 | . 18 | . 11 | . 11 | . 06 | . 14 | . 14 | . 14 | . 13 | . 00 | 2.33 |  |
| (2) | . 01 | . 02 | . 02 | . 01 | . 03 | . 01 | . 02 | . 02 | . 02 | . 01 | . 01 | . 01 | . 02 | . 02 | . 02 | . 01 | . 00 | . 24 |  |
| 1.6-2.0 | 11 | 7 | 13 | 20 | 17 | 16 | 17 | 11 | 13 | 15 | 14 | 11 | 11 | 10 | 12 | 11 | 0 | 209 | $3.5-4.5$ |
| (1) | . 18 | . 11 | . 21 | . 32 | . 27 | . 26 | . 27 | . 18 | . 21 | . 24 | . 22 | . 18 | . 18 | . 16 | . 19 | . 18 | . 00 | 3.35 |  |
| (2) | . 02 | . 01 | . 02 | . 03 | . 03 | . 03 | . 03 | . 02 | . 02 | . 03 | . 02 | . 02 | . 02 | . 02 | . 02 | . 02 | . 00 | . 35 |  |
| 2.1-3.0 | 48 | 41 | 29 | 26 | 36 | 29 | 30 | 36 | 45 | 45 | 44 | 39 | 34 | 50 | 29 | 40 | 0 | 601 | 4.6-6.7 |
| (1) | . 77 | . 66 | . 47 | . 42 | . 58 | . 47 | . 48 | . 58 | . 72 | . 72 | . 71 | . 63 | . 55 | . 80 | . 47 | . 64 | . 00 | 9.64 |  |
| (2) | . 08 | . 07 | . 05 | . 04 | . 06 | . 05 | . 05 | . 06 | . 08 | . 08 | . 07 | . 07 | . 06 | . 08 | . 05 | . 07 | . 00 | 1.01 |  |
| 3.1-4.0 | 43 | 24 | 28 | 19 | 20 | 31 | 57 | 64 | 105 | 92 | 89 | 81 | 60 | 62 | 55 | 61 | 0 | 891 | 6.8-8.9 |
| (1) | . 69 | . 38 | . 45 | . 30 | . 32 | . 50 | . 91 | 1.03 | 1.68 | 1.48 | 1.43 | 1.30 | . 96 | . 99 | . 88 | . 98 | . 00 | 14.29 |  |
| (2) | . 07 | . 04 | . 05 | . 03 | . 03 | . 05 | . 10 | . 11 | . 18 | . 15 | . 15 | . 14 | . 10 | . 10 | . 09 | . 10 | . 00 | 1.49 |  |
| 4.1-5.0 | 42 | 22 | 11 | 6 | 4 | 13 | 46 | 100 | 155 | 165 | 142 | 118 | 102 | 104 | 97 | 97 | 0 | 1224 | 9.0-11.2 |
| (1) | . 67 | . 35 | . 18 | . 10 | . 06 | . 21 | . 74 | 1.60 | 2.49 | 2.65 | 2.28 | 1.89 | 1.64 | 1.67 | 1.56 | 1.56 | . 00 | 19.63 |  |
| (2) | . 07 | . 04 | . 02 | . 01 | . 01 | . 02 | . 08 | . 17 | . 26 | . 28 | . 24 | . 20 | . 17 | . 17 | . 16 | . 16 | . 00 | 2.05 |  |
| 5.1-6.0 | 18 | 13 | 8 | 4 | 0 | 5 | 32 | 108 | 306 | 277 | 191 | 129 | 112 | 110 | 130 | 76 | 0 | 1519 | 11.3-13.4 |
| (1) | . 29 | . 21 | . 13 | . 06 | . 00 | . 08 | . 51 | 1.73 | 4.91 | 4.44 | 3.06 | 2.07 | 1.80 | 1.76 | 2.09 | 1.22 | . 00 | 24.37 |  |
| (2) | . 03 | . 02 | . 01 | . 01 | . 00 | . 01 | . 05 | . 18 | . 51 | . 46 | . 32 | . 22 | . 19 | . 18 | . 22 | . 13 | . 00 | 2.54 |  |
| 6.1-8.0 | 10 | 14 | 11 | 8 | 3 | 1 | 8 | 72 | 241 | 377 | 286 | 121 | 53 | 59 | 137 | 18 | 0 | 1419 | 13.5-17.9 |
| (1) | . 16 | . 22 | . 18 | . 13 | . 05 | . 02 | . 13 | 1.15 | 3.87 | 6.05 | 4.59 | 1.94 | . 85 | . 95 | 2.20 | . 29 | . 00 | 22.76 |  |
| (2) | . 02 | . 02 | . 02 | . 01 | . 01 | . 00 | . 01 | . 12 | . 40 | . 63 | . 48 | . 20 | . 09 | . 10 | . 23 | . 03 | . 00 | 2.38 |  |
| 8.1-10.0 | 5 | 2 | 1 | 3 | 0 | 0 | 0 | 0 | 6 | 24 | 32 | 2 | 1 | 1 | 1 | 0 | 0 | 78 | 18.0-22.4 |
| (1) | . 08 | . 03 | . 02 | . 05 | . 00 | . 00 | . 00 | . 00 | . 10 | . 38 | . 51 | . 03 | . 02 | . 02 | . 02 | . 00 | . 00 | 1.25 |  |
| (2) | . 01 | . 00 | . 00 | . 01 | . 00 | . 00 | . 00 | . 00 | . 01 | . 04 | . 05 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 13 |  |
| 10.1-89.5 | 4 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 22.5-200.2 |
| (1) | . 06 | . 05 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 02 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 16 |  |
| (2) | . 01 | . 01 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 |  |
| ALL SPEEDS | 197 | 142 | 118 | 105 | 110 | 117 | 207 | 413 | 889 | 1015 | 817 | 512 | 388 | 410 | 477 | 317 | 0 | 6234 |  |
| (1) | 3.16 | 2.28 | 1.89 | 1.68 | 1.76 | 1.88 | 3.32 | 6.62 | 14.26 | 16.28 | 13.11 | 8.21 | 6.22 | 6.58 | 7.65 | 5.09 | . 00 | 100.00 |  |
| (2) | . 33 | . 24 | . 20 | . 18 | . 18 | . 20 | . 35 | . 69 | 1.49 | 1.70 | 1.37 | . 86 | . 65 | . 69 | . 80 | . 53 | . 00 | 10.44 |  |
| (1) = PERCENT | OF ALL | GOOD | OBSERV | ATIONS | FOR | HIS PA |  |  |  |  |  |  |  |  |  |  |  |  |  |
| (2) = PERCENT | OF ALL | GOOD | OBSERV | ATIONS | FOR | HIS PER | RIOD |  |  |  |  |  |  |  |  |  |  |  |  |

Table 2．3－135—\｛CCNPP 197＇（60－m）2000－2006 Annual Joint Frequency Distribution Table\} （Page 7 of 8）
CC JANOO－DEC06 MET DATA JOINT FREQUENCY DISTRIBUTION（60－METER TOWER）
197．0 FT WIND DATA STABILITY CLASS G CLASS FREQUENCY（PERCENT）$=7.48$ 197．0 FT WIND DATA STABILITY CLASS G WIND DIRECTION FROM

| SPEed | N | NNE | NE | Ene | E | ESE | SE | SSE | S | SSW | SW | WSW | W | wnw | NW | nNw | VRBL | TOTAL | SPEED |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | MPH |
| LT ． 2 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 3 | 0 | 2 | 0 | 0 | 9 | LT ． 4 |
| （1） | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 04 | ． 02 | ． 07 | ． 00 | ． 04 | ． 00 | ． 00 | ． 20 |  |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 01 | ． 00 | ． 00 | ． 00 | ． 00 | ． 02 |  |
| ．2－． 4 | 2 | 1 | 1 | 0 | 2 | 1 | 3 | 0 | 1 | 2 | 0 | 1 | 2 | 0 | 1 | 1 | 0 | 18 | ． $4-.9$ |
| （1） | ． 04 | ． 02 | ． 02 | ． 00 | ． 04 | ． 02 | ． 07 | ． 00 | ． 02 | ． 04 | ． 00 | ． 02 | ． 04 | ． 00 | ． 02 | ． 02 | ． 00 | ． 40 |  |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 01 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 03 |  |
| ．5－1．0 | 11 | 9 | 10 | 5 | 15 | 9 | 12 | 13 | 4 | 11 | 12 | 11 | 6 | 10 | 13 | 12 | 0 | 163 | 1．0－2．2 |
| （1） | ． 25 | ． 20 | ． 22 | ． 11 | ． 34 | ． 20 | ． 27 | ． 29 | ． 09 | ． 25 | ． 27 | ． 25 | ． 13 | ． 22 | ． 29 | ． 27 | ． 00 | 3.65 |  |
| （2） | ． 02 | ． 02 | ． 02 | ． 01 | ． 03 | ． 02 | ． 02 | ． 02 | ． 01 | ． 02 | ． 02 | ． 02 | ． 01 | ． 02 | ． 02 | ． 02 | ． 00 | ． 27 |  |
| 1．1－1．5 | 19 | 11 | 20 | 11 | 22 | 13 | 15 | 15 | 13 | 10 | 15 | 20 | 12 | 10 | 12 | 10 | 0 | 228 | $2.3-3.4$ |
| （1） | ． 43 | ． 25 | ． 45 | ． 25 | ． 49 | ． 29 | ． 34 | ． 34 | ． 29 | ． 22 | ． 34 | ． 45 | ． 27 | ． 22 | ． 27 | ． 22 | ． 00 | 5.11 |  |
| （2） | ． 03 | ． 02 | ． 03 | ． 02 | ． 04 | ． 02 | ． 03 | ． 03 | ． 02 | ． 02 | ． 03 | ． 03 | ． 02 | ． 02 | ． 02 | ． 02 | ． 00 | ． 38 |  |
| 1．6－2．0 | 17 | 16 | 12 | 16 | 18 | 8 | 25 | 16 | 29 | 26 | 19 | 17 | 19 | 9 | 14 | 14 | 0 | 275 | $3.5-4.5$ |
| （1） | ． 38 | ． 36 | ． 27 | ． 36 | ． 40 | ． 18 | ． 56 | ． 36 | ． 65 | ． 58 | ． 43 | ． 38 | ． 43 | ． 20 | ． 31 | ． 31 | ． 00 | 6.16 |  |
| （2） | ． 03 | ． 03 | ． 02 | ． 03 | ． 03 | ． 01 | ． 04 | ． 03 | ． 05 | ． 04 | ． 03 | ． 03 | ． 03 | ． 02 | ． 02 | ． 02 | ． 00 | ． 46 |  |
| 2．1－3．0 | 41 | 35 | 18 | 24 | 22 | 26 | 26 | 35 | 48 | 66 | 41 | 54 | 54 | 39 | 40 | 34 | 0 | 603 | 4．6－6．7 |
| （1） | ． 92 | ． 78 | ． 40 | ． 54 | ． 49 | ． 58 | ． 58 | ． 78 | 1.08 | 1.48 | ． 92 | 1.21 | 1.21 | ． 87 | ． 90 | ． 76 | ． 00 | 13.51 |  |
| （2） | ． 07 | ． 06 | ． 03 | ． 04 | ． 04 | ． 04 | ． 04 | ． 06 | ． 08 | ． 11 | ． 07 | ． 09 | ． 09 | ． 07 | ． 07 | ． 06 | ． 00 | 1.01 |  |
| 3．1－4．0 | 34 | 13 | 4 | 3 | 7 | 8 | 33 | 49 | 71 | 78 | 92 | 95 | 64 | 62 | 41 | 62 | 0 | 716 | $6.8-8.9$ |
| （1） | ． 76 | ． 29 | ． 09 | ． 07 | ． 16 | ． 18 | ． 74 | 1.10 | 1.59 | 1.75 | 2.06 | 2.13 | 1.43 | 1.39 | ． 92 | 1.39 | ． 00 | 16.04 |  |
| （2） | ． 06 | ． 02 | ． 01 | ． 01 | ． 01 | ． 01 | ． 06 | ． 08 | ． 12 | ． 13 | ． 15 | ． 16 | ． 11 | ． 10 | ． 07 | ． 10 | ． 00 | 1.20 |  |
| 4．1－5．0 | 11 | 1 | 2 | 2 | 1 | 6 | 12 | 51 | 113 | 154 | 164 | 125 | 72 | 68 | 61 | 64 | 0 | 907 | 9．0－11．2 |
| （1） | ． 25 | ． 02 | ． 04 | ． 04 | ． 02 | ． 13 | ． 27 | 1.14 | 2.53 | 3.45 | 3.67 | 2.80 | 1.61 | 1.52 | 1.37 | 1.43 | ． 00 | 20.31 |  |
| （2） | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 01 | ． 02 | ． 09 | ． 19 | ． 26 | ． 27 | ． 21 | ． 12 | ． 11 | ． 10 | ． 11 | ． 00 | 1.52 |  |
| 5．1－ 6.0 | 3 | 3 | 1 | 1 | 0 | 5 | 7 | 32 | 138 | 171 | 145 | 85 | 67 | 50 | 57 | 41 | 0 | 806 | 11．3－13．4 |
| （1） | ． 07 | ． 07 | ． 02 | ． 02 | ． 00 | ． 11 | ． 16 | ． 72 | 3.09 | 3.83 | 3.25 | 1.90 | 1.50 | 1.12 | 1.28 | ． 92 | ． 00 | 18.05 |  |
| （2） | ． 01 | ． 01 | ． 00 | ． 00 | ． 00 | ． 01 | ． 01 | ． 05 | ． 23 | ． 29 | ． 24 | ． 14 | ． 11 | ． 08 | ． 10 | ． 07 | ． 00 | 1.35 |  |
| $6.1-8.0$ | 2 | 4 | 7 | 2 | 0 | 4 | 3 | 39 | 128 | 151 | 96 | 65 | 62 | 50 | 67 | 4 | 0 | 684 | 13．5－17．9 |
| （1） | ． 04 | ． 09 | ． 16 | ． 04 | ． 00 | ． 09 | ． 07 | ． 87 | 2.87 | 3.38 | 2.15 | 1.46 | 1.39 | 1.12 | 1.50 | ． 09 | ． 00 | 15.32 |  |
| （2） | ． 00 | ． 01 | ． 01 | ． 00 | ． 00 | ． 01 | ． 01 | ． 07 | ． 21 | ． 25 | ． 16 | ． 11 | ． 10 | ． 08 | ． 11 | ． 01 | ． 00 | 1.15 |  |
| 8．1－10．0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 1 | 2 | 8 | 4 | 11 | 3 | 5 | 3 | 0 | 0 | 41 | 18．0－22．4 |
| （1） | ． 00 | ． 00 | ． 04 | ． 04 | ． 00 | ． 00 | ． 00 | ． 02 | ． 04 | ． 18 | ． 09 | ． 25 | ． 07 | ． 11 | ． 07 | ． 00 | ． 00 | ． 92 |  |
| （2） | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 01 | ． 01 | ． 02 | ． 01 | ． 01 | ． 01 | ． 00 | ． 00 | ． 07 |  |
| 10．1－89．5 | 0 | 3 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15 | 22．5－200．2 |
| （1） | ． 00 | ． 07 | ． 27 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 34 |  |
| （2） | ． 00 | ． 01 | ． 02 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 00 | ． 03 |  |
| ALL SPEEDS | 140 | 96 | 89 | 66 | 88 | 80 | 136 | 251 | 547 | 677 | 590 | 485 | 364 | 303 | 311 | 242 | 0 | 4465 |  |
| （1） | 3.14 | 2.15 | 1.99 | 1.48 | 1.97 | 1.79 | 3.05 | 5.62 | 12.25 | 15.16 | 13.21 |  | 8.15 | 6.79 | 6.97 | 5.42 | ． 00 | 100.00 |  |
| （2） | ． 23 |  | ． 15 | ． 11 | ． 15 | ． 13 | ． 23 | ． 42 | ． 92 | 1.13 | ． 99 | ． 81 | ． 61 | ． 51 | ． 52 | ． 41 | ． 00 | 7.48 |  |
| （1）＝PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| （2）＝PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Table 2.3-135—\{CCNPP 197' (60-m) 2000-2006 Annual Joint Frequency Distribution Table\} (Page 8 of 8)
CC JANOO-DEC06 MET DATA JOINT FREQUENCY DISTRIBUTION (60-METER TOWER)
197.0 FT WIND DATA
STABILITY CLASS ALL
CLASS FREQUE


| SPeed | N | NNE | NE | ene | E | ESE | SE | SSE | S | SSW | SW | wSW | W | wnw | NW | NNW | VRBL | TOTAL | SPEED |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | MPH |
| LT . 2 | 0 | 1 | 1 | 1 | 2 | 2 | 0 | 0 | 0 | 1 | 2 | 2 | 4 | 0 | 2 | 0 | 0 | 18 | LT . 4 |
| (1) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 00 | . 00 | . 00 | . 00 | . 03 |  |
| (2) | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 00 | . 00 | . 00 | . 00 | . 03 |  |
| .2- . 4 | 6 | 4 | 3 | 1 | 4 | 2 | 5 | 4 | 4 | 2 | 1 | 2 | 4 | 2 | 3 | 2 | 0 | 49 | . 4 - . 9 |
| (1) | . 01 | . 01 | . 01 | . 00 | . 01 | . 00 | . 01 | . 01 | . 01 | . 00 | . 00 | . 00 | . 01 | . 00 | . 01 | . 00 | . 00 | . 08 |  |
| (2) | . 01 | . 01 | . 01 | . 00 | . 01 | . 00 | . 01 | . 01 | . 01 | . 00 | . 00 | . 00 | . 01 | . 00 | . 01 | . 00 | . 00 | . 08 |  |
| .5-1.0 | 48 | 42 | 67 | 49 | 82 | 55 | 44 | 56 | 29 | 50 | 41 | 37 | 29 | 35 | 42 | 46 | 0 | 752 | $1.0-2.2$ |
| (1) | . 08 | . 07 | . 11 | . 08 | . 14 | . 09 | . 07 | . 09 | . 05 | . 08 | . 07 | . 06 | . 05 | . 06 | . 07 | . 08 | . 00 | 1.26 |  |
| (2) | . 08 | . 07 | . 11 | . 08 | . 14 | . 09 | . 07 | . 09 | . 05 | . 08 | . 07 | . 06 | . 05 | . 06 | . 07 | . 08 | . 00 | 1.26 |  |
| 1.1-1.5 | 98 | 108 | 108 | 111 | 130 | 81 | 77 | 62 | 57 | 50 | 65 | 61 | 59 | 53 | 57 | 55 | 0 | 1232 | $2.3-3.4$ |
| (1) | . 16 | . 18 | . 18 | . 19 | . 22 | . 14 | . 13 | . 10 | . 10 | . 08 | . 11 | . 10 | . 10 | . 09 | . 10 | . 09 | . 00 | 2.06 |  |
| (2) | . 16 | . 18 | . 18 | . 19 | . 22 | . 14 | . 13 | . 10 | . 10 | . 08 | . 11 | . 10 | . 10 | . 09 | . 10 | . 09 | . 00 | 2.06 |  |
| 1.6-2.0 | 158 | 226 | 183 | 228 | 262 | 134 | 108 | 86 | 111 | 98 | 146 | 109 | 92 | 72 | 77 | 105 | 0 | 2195 | $3.5-4.5$ |
| (1) | . 26 | . 38 | . 31 | . 38 | . 44 | . 22 | . 18 | . 14 | . 19 | . 16 | . 24 | . 18 | . 15 | . 12 | . 13 | . 18 | . 00 | 3.68 |  |
| (2) | . 26 | . 38 | . 31 | . 38 | . 44 | . 22 | . 18 | . 14 | . 19 | . 16 | . 24 | . 18 | . 15 | . 12 | . 13 | . 18 | . 00 | 3.68 |  |
| 2.1-3.0 | 695 | 787 | 486 | 562 | 632 | 405 | 382 | 388 | 346 | 376 | 434 | 358 | 289 | 271 | 268 | 314 | 0 | 6993 | 4.6-6.7 |
| (1) | 1.16 | 1.32 | . 81 | . 94 | 1.06 | . 68 | . 64 | . 65 | . 58 | . 63 | . 73 | . 60 | . 48 | . 45 | . 45 | . 53 | . 00 | 11.71 |  |
| (2) | 1.16 | 1.32 | . 81 | . 94 | 1.06 | . 68 | . 64 | . 65 | . 58 | . 63 | . 73 | . 60 | . 48 | . 45 | . 45 | . 53 | . 00 | 11.71 |  |
| 3.1-4.0 | 909 | 795 | 393 | 435 | 444 | 435 | 518 | 700 | 605 | 625 | 774 | 635 | 456 | 469 | 476 | 606 | 0 | 9275 | $6.8-8.9$ |
| (1) | 1.52 | 1.33 | . 66 | . 73 | . 74 | . 73 | . 87 | 1.17 | 1.01 | 1.05 | 1.30 | 1.06 | . 76 | . 79 | . 80 | 1.02 | . 00 | 15.54 |  |
| (2) | 1.52 | 1.33 | . 66 | . 73 | . 74 | . 73 | . 87 | 1.17 | 1.01 | 1.05 | 1.30 | 1.06 | . 76 | . 79 | . 80 | 1.02 | . 00 | 15.54 |  |
| 4.1- 5.0 | 918 | 600 | 391 | 354 | 288 | 296 | 499 | 1011 | 833 | 929 | 1012 | 757 | 526 | 668 | 863 | 896 | 0 | 10841 | 9.0-11.2 |
| (1) | 1.54 | 1.01 | 66 | . 59 | 48 | . 50 | . 84 | 1.69 | 1.40 | 1.56 | 1.70 | 1.27 | . 88 | 1.12 | 1.45 | 1.50 | . 00 | 18.16 |  |
| (2) | 1.54 | 1.01 | 66 | . 59 | 48 | . 50 | . 84 | 1.69 | 1.40 | 1.56 | 1.70 | 1.27 | . 88 | 1.12 | 1.45 | 1.50 | . 00 | 18.16 |  |
| 5.1- 6.0 | 694 | 488 | 343 | 255 | 132 | 117 | 310 | 943 | 1023 | 1122 | 1150 | 703 | 497 | 706 | 1040 | 936 | 0 | 10459 | 11.3-13.4 |
| (1) | 1.16 | . 82 | . 57 | . 43 | . 22 | . 20 | . 52 | 1.58 | 1.71 | 1.88 | 1.93 | 1.18 | . 83 | 1.18 | 1.74 | 1.57 | . 00 | 17.52 |  |
| (2) | 1.16 | . 82 | . 57 | . 43 | . 22 | . 20 | . 52 | 1.58 | 1.71 | 1.88 | 1.93 | 1.18 | . 83 | 1.18 | 1.74 | 1.57 | . 00 | 17.52 |  |
| 6.1-8.0 | 803 | 756 | 518 | 241 | 82 | 81 | 199 | 851 | 997 | 1866 | 1892 | 635 | 440 | 853 | 1345 | 930 | 0 | 12489 | 13.5-17.9 |
| (1) | 1.35 | 1.27 | . 87 | . 40 | . 14 | . 14 | . 33 | 1.43 | 1.67 | 3.13 | 3.17 | 1.06 | . 74 | 1.43 | 2.25 | 1.56 | . 00 | 20.92 |  |
| (2) | 1.35 | 1.27 | . 87 | . 40 | . 14 | . 14 | . 33 | 1.43 | 1.67 | 3.13 | 3.17 | 1.06 | . 74 | 1.43 | 2.25 | 1.56 | . 00 | 20.92 |  |
| 8.1-10.0 | 435 | 428 | 281 | 62 | 8 | 8 | 53 | 235 | 138 | 467 | 529 | 86 | 81 | 417 | 495 | 253 | - | 3976 | 18.0-22.4 |
| (1) | . 73 | . 72 | . 47 | . 10 | . 01 | . 01 | . 09 | . 39 | . 23 | . 78 | . 89 | . 14 | . 14 | . 70 | . 83 | . 42 | . 00 | 6.66 |  |
| (2) | . 73 | . 72 | . 47 | . 10 | . 01 | . 01 | . 09 | . 39 | . 23 | . 78 | . 89 | . 14 | . 14 | . 70 | . 83 | . 42 | . 00 | 6.66 |  |
| 10.1-89.5 | 214 | 282 | 173 | 27 | 3 | 6 | 20 | 71 | 25 | 82 | 58 | 20 | 29 | 161 | 177 | 66 | - | 1414 | 22.5-200.2 |
| (1) | . 36 | . 47 | . 29 | . 05 | . 01 | . 01 | . 03 | . 12 | . 04 | . 14 | . 10 | . 03 | . 05 | . 27 | . 30 | . 11 | . 00 | 2.37 |  |
| (2) | . 36 | . 47 | . 29 | . 05 | . 01 | . 01 | . 03 | . 12 | . 04 | . 14 | . 10 | . 03 | . 05 | . 27 | . 30 | . 11 | . 00 | 2.37 |  |
| ALL SPEEDS | 4978 | 4517 | 2947 | 2326 | 2069 | 1622 | 2215 | 4407 | 4168 | 5668 | 6104 | 3405 | 2506 | 3707 | 4845 | 4209 | - | 59693 |  |
| (1) | 8.34 | 7.57 | 4.94 | 3.90 | 3.47 | 2.72 | 3.71 | 7.38 | 6.98 | 9.50 | 10.23 | 5.70 | 4.20 | 6.21 | 8.12 | 7.05 | . 00 | 100.00 |  |
| (2) | 8.34 | 7.57 | 4.94 | 3.90 | 3.47 | 2.72 | 3.71 | 7.38 | 6.98 | 9.50 | 10.23 | 5.70 | 4.20 | 6.21 | 8.12 | 7.05 | . 00 | 100.00 |  |
| (1) =PERCENT | OF ALL | GOOD | OBSERV | ATIONS | FOR | HIS P |  |  |  |  |  |  |  |  |  |  |  |  |  |
| (2) =PERCENT | OF ALL | GOOD | OBSERV | ATIONS | FOR | HIS P | RIOD |  |  |  |  |  |  |  |  |  |  |  |  |

Figure 2.3-1—\{Not Used $\}$

Figure 2.3-2—\{Not Used\}

Figure 2.3-3—\{Not Used\}

Figure 2.3-4—\{Not Used\}

Figure 2.3-5—\{Not Used\}

Figure 2.3-6-\{Not Used\}

Figure 2.3-7-\{Not Used\}



Figure 2.3-11-\{Date of Maximum Tornado Threat\}



Figure 2.3-13-\{Ozone Concentration for Maryland Counties\}

Ozone 4th highest 8 -hour average concentration


4th highest 8 -hour overoge concentrotion (ppm) in 2006


Figure 2.3-14—\{CCNPP 33' (10 m) Annual Wind Rose (2000-2005)\}

CCNPP JAN 2000 - DEC 2005
33-FOOT WIND DATA


STABILITY CLASS AL
CALM WINDS $0.33 \%$
$\begin{aligned} & \text { NOTE: Frequencies indicate } \\ & \text { direction from which } \\ & \text { the wind is blowing. }\end{aligned}$


Figure 2.3-15—\{CCNPP 197' (60 m) Annual Wind Rose (2000-2005)\}

CCNPP JAN 2000 - DEC 2005

197-FOOT WIND DATA


Figure 2.3-16—\{CCNPP 33' (10 m) January Wind Rose (2000-2005)\}

## CC STATION JAN

## 33-FOOT WIND DATA



STABILITY CLASS ALL


Figure 2.3-17—\{CCNPP 33' (10 m) February Wind Rose (2000-2005)\}

## CC STATION FEB



Figure 2.3-18—\{CCNPP 33' (10 m) March Wind Rose (2000-2005)\}

## CC STATION MAR

## 33-FOOT WIND DATA



STABILITY CLASS ALL
CALM WINDS 0.32\%

NOTE: Frequencies indicate
direction from which the wind is blowing.


Figure 2.3-19—\{CCNPP 33' (10 m) April Wind Rose (2000-2005)\}

## CC STATION APR

## 33-FOOT WIND DATA



STABILITY CLASS ALL
CALM WINDS $0.15 \%$

NOTE: Frequencies indicate direction from which the wind is blowing.


Figure 2.3-20—\{CCNPP 33' (10 m) May Wind Rose (2000-2005)\}

## CC STATION MAY

33-FOOT WIND DATA


STABILITY CLASS ALL
CALM WINDS $0.25 \%$

NOTE: Frequencles Indicate direction from which the wind is blowing.


Figure 2.3-21—\{CCNPP 33' (10 m) June Wind Rose (2000-2005) \}
CC STATION JUN

## 33-FOOT WIND DATA



STABILITY CLASS ALL
CALM WINDS $0.42 \%$

NOTE: Frequencies indicate
direction from which the wind is tlowing.


Figure 2.3-22—\{CCNPP 33' (10 m) July Wind Rose (2000-2005)\}
CC STATION JUL

## 33-FOOT WIND DATA



Figure 2.3-23—\{CCNPP 33' (10 m) August Wind Rose (2000-2005)\}

## CC STATION AUG

## 33-FOOT WIND DATA



Figure 2.3-24—\{CCNPP 33' (10 m) September Wind Rose (2000-2005)\}
CC STATION SEP

## 33-FOOT WIND DATA



S
STABILITY CLASS ALL
CALM WINDS $0.52 \%$

NOTE: Frequencies indicate direction from which the wind is blowing.


Figure 2.3-25—\{CCNPP 33' (10 m) October Wind Rose (2000-2005)\}

## CC STATION OCT

## 33-FOOT WIND DATA



STABILITY CLASS ALL


Figure 2.3-26—\{CCNPP 33' (10 m) November Wind Rose (2000-2005)\}

## CC STATION NOV

## 33-FOOT WIND DATA



STABILITY CLASS ALL


Figure 2.3-27—\{CCNPP 33' (10 m) December Wind Rose (2000-2005)\} CC STATION DEC

## 33-FOOT WIND DATA



STABILITY CLASS ALL


Figure 2.3-28—\{CCNPP 197' (60 m) January Wind Rose (2000-2005)\}
CC STATION JAN

197-FOOT WIND DATA


STABILITY CLASS ALL
CALM WINDS $0.02 \%$

NOTE: Frequencies indicate
direction from which
the wind is blowing.

$\begin{array}{rrrrrrrrrr}.2-.4 & .5-1.0 & 1.1-1.5 & 1.6-2.0 & 2.1-3.0 & 3.1-4.0 & 4.1-5.0 & 5.1-6.0 & 6.1-8.0 & 8.1-10.0 \\ 10.1-89.5\end{array}$

Figure 2.3-29—\{CCNPP 197' (60 m) February Wind Rose (2000-2005)\}
CC STATION FEB

197-FOOT WIND DATA


STABILITY CLASS ALL

.2-.4 $4-1.0 \quad 1.1-1.5 \quad 1.6-2.0 \quad 2.1-3.0 \quad 3.1-4.0 \quad 4.1-5.0 \quad 5.1-6.0 \quad 6.1-8.0 \quad 8.1-10.010 .1-89.5$

Figure 2.3-30—\{CCNPP 197 ' ( 60 m ) March Wind Rose (2000-2005) \}
CC STATION MAR

197-FOOT WIND DATA


STABILITY CLASS ALL
CALM WINDS $0.00 \%$

NOTE: Frequencies indicate direction from which the wind is blowing.


Figure 2.3-31—\{CCNPP 197' (60m) April Wind Rose (2000-2005)\} CC STATION APR

## 197-FOOT WIND DATA



Figure 2.3-32—\{CCNPP 197' (60 m) May Wind Rose (2000-2005)\}
CC STATION MAY

197-FOOT WIND DATA


STABILITY CLASS ALL


Figure 2.3-33—\{CCNPP 197' (60 m) June Wind Rose (2000-2005)\}

## CC STATION JUN

197-FOOT WIND DATA


STABILITY CLASS ALL
CALM WINDS $0.02 \%$

NOTE: Frequencles Indicate
direction from which the wind is blowing


Figure 2.3-34—\{CCNPP 197' (60 m) July Wind Rose (2000-2005)\}
CC STATION JUL

197-FOOT WIND DATA


STABILITY CLASS ALL
CALM WINDS $0.02 \%$

NOTE: Frequencies indicate
direction from which
the wind is blowing.


Figure 2.3-35—\{CCNPP 197' (60 m) August Wind Rose (2000-2005)\}
CC STATION AUG

197-FOOT WIND DATA


STABILITY CLASS ALL
CALM WINDS $0.09 \%$

NOTE: Frequencies indicate direction from which the wind is blowing.


Figure 2.3-36—\{CCNPP 197' (60 m) September Wind Rose (2000-2005)\}
CC STATION SEP

197-FOOT WIND DATA


STABILITY CLASS ALL


Figure 2.3-37—\{CCNPP 197' (60 m) October Wind Rose (2000-2005)\}
CC STATION OCT

## 197-FOOT WIND DATA



STABILITY CLASS ALL


Figure 2.3-38-\{CCNPP 197' ( 60 m) November Wind Rose (2000-2005)\}
CC STATION NOV

197-FOOT WIND DATA


STABILITY CLASS ALL
CALM WINDS $0.05 \%$

NOTE: Frequencies indicate direction from which
the wind is blowing.


Figure 2.3-39—\{CCNPP 197' ( 60 m) December Wind Rose (2000-2005)\}

## CC STATION DEC

197-FOOT WIND DATA


STABILITY CLASS ALL


Figure 2.3-40-\{BWI Annual Wind Rose\}

WIND ROSE PLOT:
Station \#93721

## BALTIMORE/BLT-WASHINGTON INT'L, MD

DISPLAY:
Wind Speed Dir ection (blowing from)

DATA PERIOD:

| 1984,1985,1986,1987,1988,1990,1991,1992 |
| :--- |
| Jan 1 - Dec 31 (00:00-23:00) |
| CALM WINDS: |
| $4.12 \%$ |
| TOTAL COUNT: |
| 70152 hrs | | AVG. WIND SPEED: |
| :--- |

Figure 2.3-41— $\{$ Norfolk Annual Wind Rose $\}$

WIND ROSE PLOT:
Station \#13737
NORFOLK INT'L AIRPORT, VA

DISPLAY:
Wind Speed Direction (blowing from)


Calms: $5.27 \%$
DATA PERIOD:

| 1984,1985,1986,1987,1988,1989,1990,19 |
| :--- |
| Jan 1 - Dec 31 (00:00-23:00) |
| CALM WINDS: |
| $5.27 \%$ |
| TOTAL COUNT: |
| 78912 hrs |$|$| AVG. WIND SIEED: |
| :--- |

Figure 2.3-42-\{Richmond Annual Wind Rose\}

WIND ROSE PLOT:
Station \#13740
RICHMOND/R E BYRD INT'L AIRPORT, VA

DISPLAY:
Wind Speed Direction (blowing from)


WIND SPEED ( $\mathrm{m} / \mathrm{s}$ )


Calms: $7.35 \%$

| DATA PERIOD: |
| :--- |
| $1984,1985,1986,1987,1988,1989,1990,1991,1992$ |
| Jan $1 \quad$ Dec $31(00: 00-23: 00)$ |
| CALM WINDS: |
| $7.35 \%$ |
| TOTAL COUNT: |
| 78912 hrs |

Figure 2.3-43—\{CCNPP 33' (10 m) Annual Precipitation Wind Rose (2000-2005)\}
CCNPP JAN 2000 - DEC 2005

33-FOOT WIND DATA


STABILITY CLASS ALL


Figure 2.3-44—\{CCNPP 197' (60 m) Annual Precipitation Wind Rose (2000-2005)\} CCNPP JAN 2000 - DEC 2005

197-FOOT WIND DATA


STABILITY CLASS ALL CALM WINDS $0.04 \%$

NOTE: Frequencies indicate direction from which the wrind is blowing.


Figure 2.3-45—\{CCNPP 33' ( 10 m) January Precipitation Wind Rose for Rate Class 0.0-0.1 in/hr\}

## CC STATION JAN

## 33-FOOT WIND DATA



PRECIP RATE CLASS 0.0-0.1 IN/HR


Figure 2.3-46—\{CCNPP 33' (10 m) January Precipitation Wind Rose for Rate Class
0.1-0.2 in/hr\}

## CCNPP JAN

## 33-FOOT WIND DATA



PRECIP RATE CLASS 0.1-0.2 IN/HR


Figure 2.3-47—\{CCNPP 33' (10 m) January Precipitation Wind Rose for Rate Class 0.2-0.3 in/hr\}

CCNPP JAN

33-FOOT WIND DATA


PRECIP RATE CLASS 0.2-0.3 IN/HR

$\begin{array}{lllllllllllll}.2-.4 & .5-1.0 & 1.1-1.5 & 1.0-2.0 & 2.1-3.0 & 3.1-4.0 & 4.1-5.0 & 5.1-6.0 & 6.1-6.0 & 8.1-10.0 & 10.1-69.5\end{array}$

Figure 2.3-48—\{CCNPP 33' (10 m) January Precipitation Wind Rose for Rate Class 0.3-0.4 in/hr\}

CCNPP JAN


Figure 2.3-49—\{CCNPP 33' (10 m) January Precipitation Wind Rose for Rate Class 0.4-0.5 in/hr\}

## CCNPP JAN

## 33-FOOT WIND DATA



Figure 2.3-50—\{CCNPP 33' ( 10 m ) January Precipitation Wind Rose for All Rate classes\}

## CCNPP JAN

## 33-FOOT WIND DATA



S


Figure 2.3-51—\{CCNPP 33' (10 m) February Precipitation Wind Rose for Rate Class 0.0-0.1 in/hr\}

## CCNPP FEB

## 33-FOOT WIND DATA



PRECIP RATE CLASS 0.0-0.1 IN/HR


Figure 2.3-52- \{CCNPP 33' (10 m) February Precipitation Wind Rose for Rate Class 0.1-0.2 in/hr\}

CCNPP FEB

## 33-FOOT WIND DATA



PRECIP RATE CLASS 0.1-0.2 IN/HR


Figure 2.3-53- \{CCNPP 33' (10 m) February Precipitation Wind Rose for Rate Class 0.2-0.3 in/hr\}

CCNPP FEB

## 33-FOOT WIND DATA



PRECIP RATE CLASS 0.2-0.3 IN/HR


Figure 2.3-54- \{CCNPP 33' (10 m) February Precipitation Wind Rose for Rate Class 0.3-0.4 n/hr\}

## CCNPP FEB

## 33-FOOT WIND DATA



PRECIP RATE CLASS 0.3-0.4 IN/HR
CALM WINDS $0.00 \%$

NOTE: Frequencies indicate direction from which the wind is blowing.

.2-. 4 .5-1.0 1.1-1.5 1.6-2.0 2.1-3.0 3.1-4.0 $4.1-5.0 \quad 5.1-6.0 \quad 6.1-8.0 \quad 8.1-10.010 .1-69.5$

Figure 2.3-55—\{CCNPP 33' (10 m) February Precipitation Wind Rose for All Rate classes

CCNPP FEB

## 33-FOOT WIND DATA



Figure 2.3-56—\{CCNPP 33' (10 m) March Precipitation Wind Rose for Rate Class 0.0-0.1 in/hr\}

CCNPP MAR

## 33-FOOT WIND DATA



Figure 2.3-57—\{CCNPP 33' ( 10 m ) March Precipitation Wind Rose for Rate Class 0.1-0.2 in/hr\}

## CCNPP MAR

## 33-FOOT WIND DATA



PRECIP RATE CLASS 0.1-0.2 IN/HR


Figure 2.3-58-\{CCNPP 33' ( 10 m) March Precipitation Wind Rose for Rate Class 0.2-0.3 in/hr\}

## CCNPP MAR

33-FOOT WIND DATA


Figure 2.3-59—\{CCNPP 33' (10 m) March Precipitation Wind Rose for Rate Class 0.3-0.4 in/hr\}

CCNPP MAR

33-FOOT WIND DATA


PRECIP RATE CLASS 0.3-0.4 IN/HR CALM WINDS 0.00\%

NOTE: Frequencles Indicate direction from which the wind is blowing


Figure 2.3-60— \{CCNPP 33' (10 m) March Precipitation Wind Rose for Rate Class $0.4-0.5 \mathrm{in} / \mathrm{hr}\}$

CCNPP MAR

## 33-FOOT WIND DATA



PRECIP RATE CLASS 0.4-0.5 IN/HR


Figure 2.3-61—\{CCNPP 33' (10 m) March Precipitation Wind Rose for All Rate classes\}
CCNPP MAR

## 33-FOOT WIND DATA



PRECIP RATE CLASS ALLRATES IN/HR


Figure 2.3-62—\{CCNPP 33' (10 m) April Precipitation Wind Rose for Rate Class 0.0-0.1 in/hr\}

## CCNPP APR

33-FOOT WIND DATA


Figure 2.3-63—\{CCNPP33' (10 m) April Precipitation Wind Rose for Rate Class 0.1-0.2 in/hr\}

## CCNPP APR

## 33-FOOT WIND DATA



PRECIP RATE CLASS 0.1-0.2 IN/HR
CALM WINDS $0.00 \%$

NOTE: Frequencies indicate direction from which the wind is blowing.


Figure 2.3-64—\{CCNPP 33' (10 m) April Precipitation Wind Rose for Rate Class 0.2-0.3 in/hr\}

CCNPP APR

## 33-FOOT WIND DATA



S
PRECIP RATE CLASS 0.2-0.3 IN/HR

$2-.4 \quad .5-1.0 \quad 1.1-1.5 \quad 1.6-2.0 \quad 2.1-3.0 \quad 3.1-4.0 \quad 4.1-5.0 \quad 5.1-6.0 \quad 6.1-8.0 \quad 8.1-10.010 .1-89.5$

Figure 2.3-65—\{CCNPP 33' (10 m) April Precipitation Wind Rose for Rate Class 0.3-0.4 in/hr\}


PRECIP RATE CLASS 0.3-0.4 IN/HR


Figure 2.3-66—\{CCNPP 33' (10 m) April Precipitation Wind Rose for Rate Class 0.4-0.5 in/hr\}

CCNPP APR

33-FOOT WIND DATA


PRECIP RATE CLASS 0.4-0.5 IN/HR
CALM WINDS $0.00 \%$

NOTE: Frequencles Indlcate direction from which the wind is blowing.


Figure 2.3-67—\{CCNPP 33' (10 m) April Precipitation Wind Rose for Rate Class 0.7-0.8 in/hr\}

## CCNPP APR

## 33-FOOT WIND DATA



PRECIP RATE CLASS 0.7-0.8 IN/HR


Figure 2.3-68-\{CCNPP 33' ( 10 m ) April Precipitation Wind Rose for All Rate classes\}
CCNPP APR

## 33-FOOT WIND DATA



S


Figure 2.3-69—\{CCNPP 33' (10 m) May Precipitation Wind Rose for Rate Class 0.0-0.1 in/hr\}

CCNPP MAY

## 33-FOOT WIND DATA



PRECIP RATE CLASS 0.0-0.1 IN/HR


Figure 2.3-70—\{CCNPP 33' (10 m) May Precipitation Wind Rose for Rate Class 0.1-0.2 in/hr\}

## CCNPP MAY

## 33-FOOT WIND DATA



PRECIP RATE CLASS 0.1-0.2 IN/HR


Figure 2.3-71—\{CCNPP 33' (10 m) May Precipitation Wind Rose for Rate Class 0.2-0.3 in/hr\}

CCNPP MAY

33-FOOT WIND DATA


S
PRECIP RATE CLASS 0.2-0.3 IN/HR


Figure 2.3-72—\{CCNPP 33' (10 m) May Precipitation Wind Rose for Rate Class 0.3-0.4 in/hr\}

## CCNPP MAY

33-FOOT WIND DATA


S
PRECIP RATE CLASS 0.3-0.4 IN/HR


Figure 2.3-73—\{CCNPP 33' (10 m) May Precipitation Wind Rose for Rate Class 0.5-0.6 in/hr\}

## CCNPP MAY

## 33-FOOT WIND DATA



S
PRECIP RATE CLASS 0.5-0.6 IN/HR


Figure 2.3-74—\{CCNPP 33' (10 m) May Precipitation Wind Rose for Rate Class 0.6-0.7 in/hr\}

## CCNPP MAY

33-FOOT WIND DATA


PRECIP RATE CLASS 0.6-0.7 IN/HR



[^0]:    (1) =PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAG

[^1]:    (2) = PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

[^2]:    (1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE

[^3]:    （1）＝PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE（2）＝PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD

