

Radon Emissions From Tailings Ponds

Presented To:

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/Nuclear Regulatory Commission (NRC)
Uranium Recovery Workshop**

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Today's Discussion

- ☐ Subpart W
- ☐ Radon
- ☐ Radon diffusion
- ☐ Radon flux from tailings
- ☐ Radon from water cover
- ☐ EPA's proposed method of monitoring
- ☐ Summary observations

Subpart W

NESHAP for Radon Emissions from Operating Mill Tailings

- ❑ ***Uranium byproduct material or tailings*** means waste produced by the extraction or concentration of uranium from any ore processed primarily for its source material content.
- ❑ Rn-222 flux from **existing** uranium mill tailings pile of less than 20 pCi/m² · s

Subpart W ...(cont'd)

NESHAP for Radon Emissions from Operating Mill Tailings

- ❑ **New** tailings impoundments must meet one of two work practices
 - ❖ For **phased disposal**, no more than two 40 acre cells (including existing impoundments can be in operation at any single time
 - ❖ For **continuous disposal**, tailings are dewatered and immediately disposed with no more than 10 acres in operation at any one time
- ❑ **Annual radon flux testing required**

Nominal Radon Flux

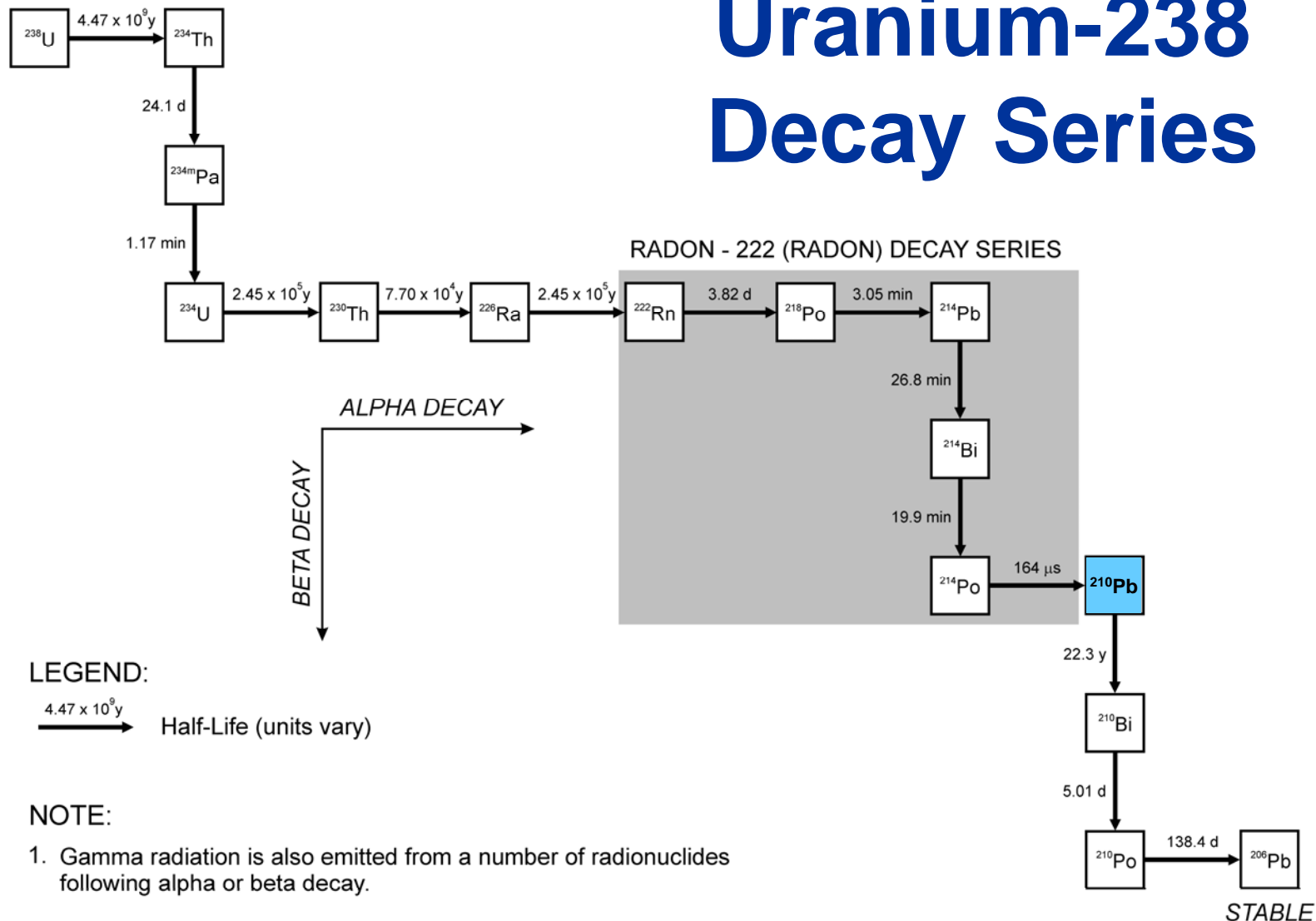
(BID – Final Rule for Radon, EPA 1986)

- ❑ **Dry Tailings (soil)** **1 pCi Rn-222/m²s per pCi Ra-226/g**
- ❑ **Saturated** **0.3 pCi Rn-222/m²s per pCi Ra-226/g**
- ❑ **Water Cover** **0 pCi Rn-222/m²s per pCi Ra-226/g**

Radon

- ❑ Radon is everywhere
- ❑ Produced through radioactive decay of Ra-226
- ❑ Half-life of 3.82 days
- ❑ EPA has raised issue with ISR evaporation ponds
- ❑ EPA has raised issue with Pb-210

Uranium-238 Decay Series



Radon Production Rate

The radon production rate (q) in a porous radium-bearing material can be expressed as:

$$q = [Ra] \times \rho \times \frac{E}{P} \times \lambda$$

$$= \frac{\beta \times E}{P} = \frac{\beta}{P}$$

Where:

$[Ra]$ = radium-226 concentration

ρ = bulk density (g/cm³)

E = emanation coefficient

P = porosity (void fraction)

λ = radon decay constant

β = emanating power (pCi/s-cm³)

Diffusion Length

Where:

L = diffusion length

= distance to which concentration
decreases by factor of e ($= 2.718$)

D = bulk diffusion coefficient (cm^2/s)

λ = radon decay constant

$= 2.1 \times 10^{-6}/\text{s}$

P = porosity (void volume/total volume)

$$L = \sqrt{\frac{D}{\lambda P}}$$

Diffusion of Radon Across a Medium

In general, when radon is covered by inert material, diffusive flux (J) can be expressed (approximately) as:

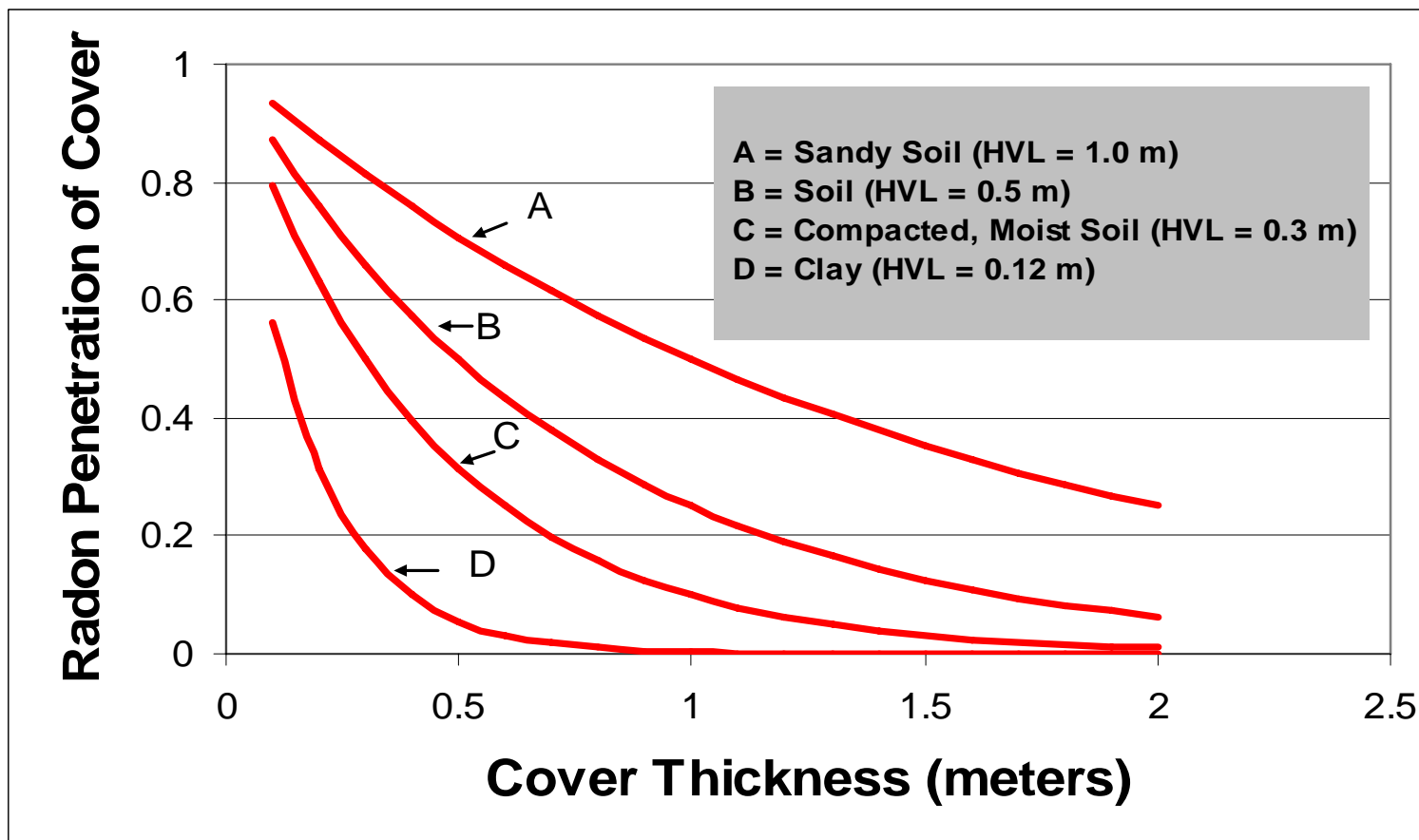
$$J = e^{-\frac{Z}{L}}$$

Where:

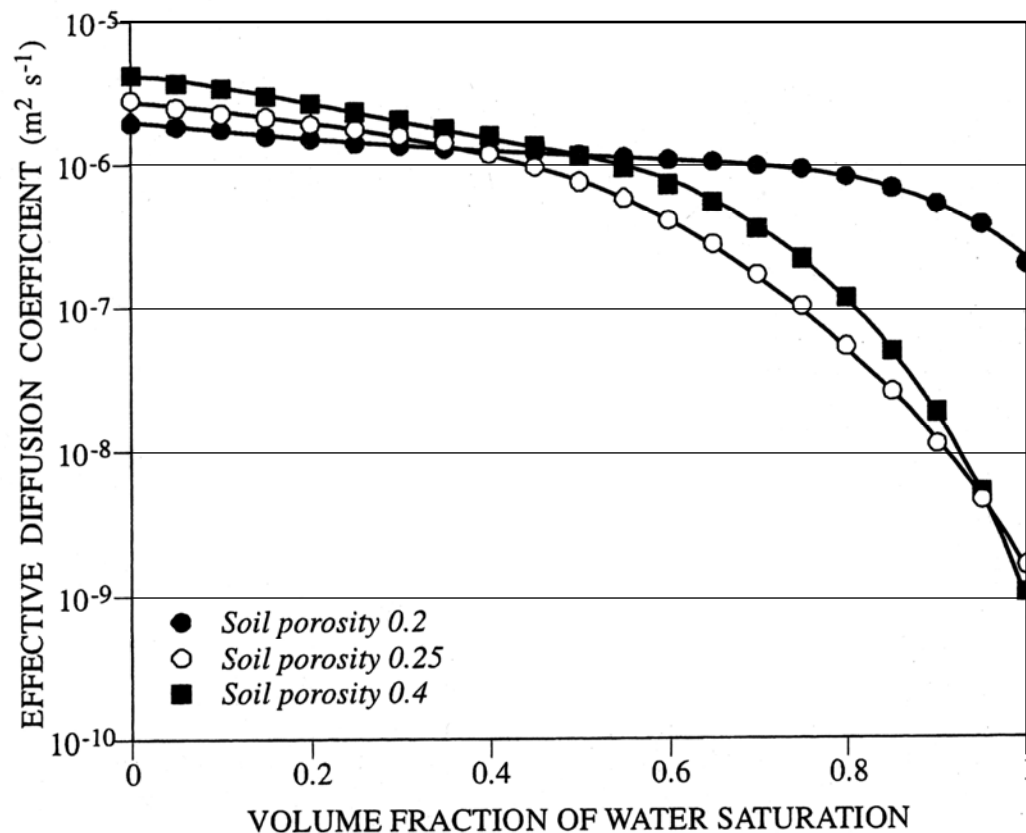
Z = “Cover” thickness

L = diffusion length

Diffusion of Radon Across a Medium

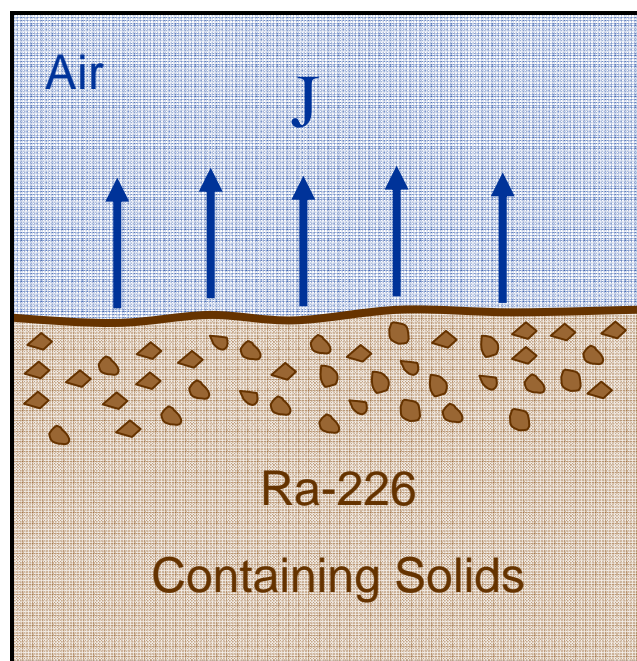


Experimental Diffusion Coefficients (UNSCEAR 2000)



SOURCE: After UNSCEAR 2000

Radon Flux



Based on Fick's Laws:

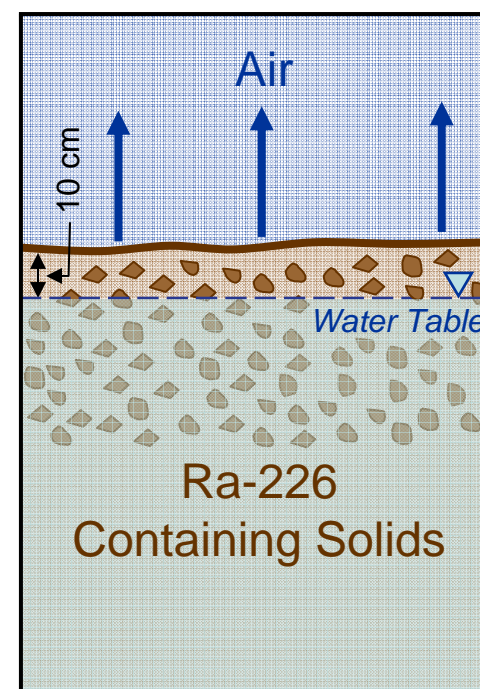
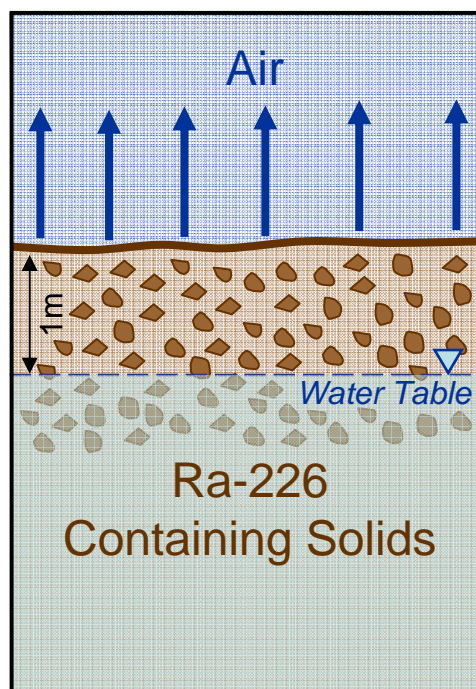
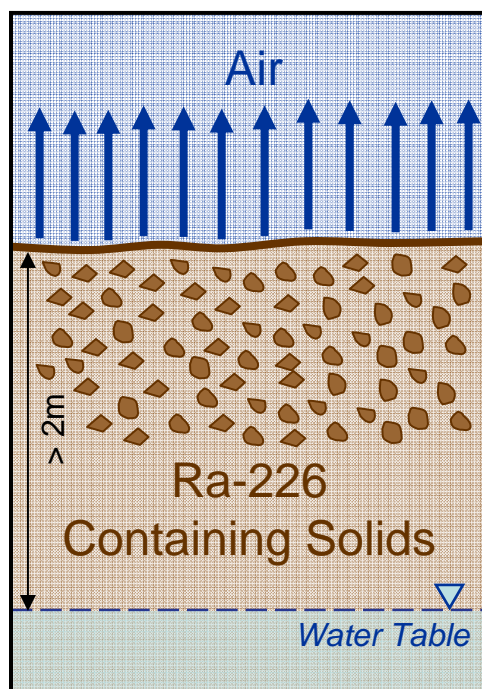
$$J = \beta \times L \text{ (pCi/m}^2 \cdot \text{s)}$$

Where:

β = emanating power (pCi/m³ · s)

L = diffusion length

Effects of Depth to Water Table



Radon From Water Cover (1)

- **Two Mechanisms**
 - ❖ **Diffusion**
 - ❖ **Turbulent transfer**

Radon From Water Cover (2)

□ Diffusion

- ❖ Diffusion coefficient in water << diffusion coefficient in air (1/100th)
- ❖ Rn-222 gas exchange via diffusion from surface of small lake has been measured (Experimental lakes, Ontario)

$$F \text{ (pCi/m}^2 \cdot \text{d)} \cong k_{\text{Rn}} \text{ (m/d)} \times [C - C_o] \text{ (pCi/m}^3\text{)}$$

$$\cong k_{\text{Rn}} \times C$$

- ❖ For $k_{\text{Rn}} \sim 0.5\text{m/d}$

C (pCi/L)	F (pCi/m ² ·s)
10	5.8×10^{-5}
100	5.8×10^{-4}
1000	5.8×10^{-3}

Radon From Water Cover (3)

□ Turbulence (wave action)

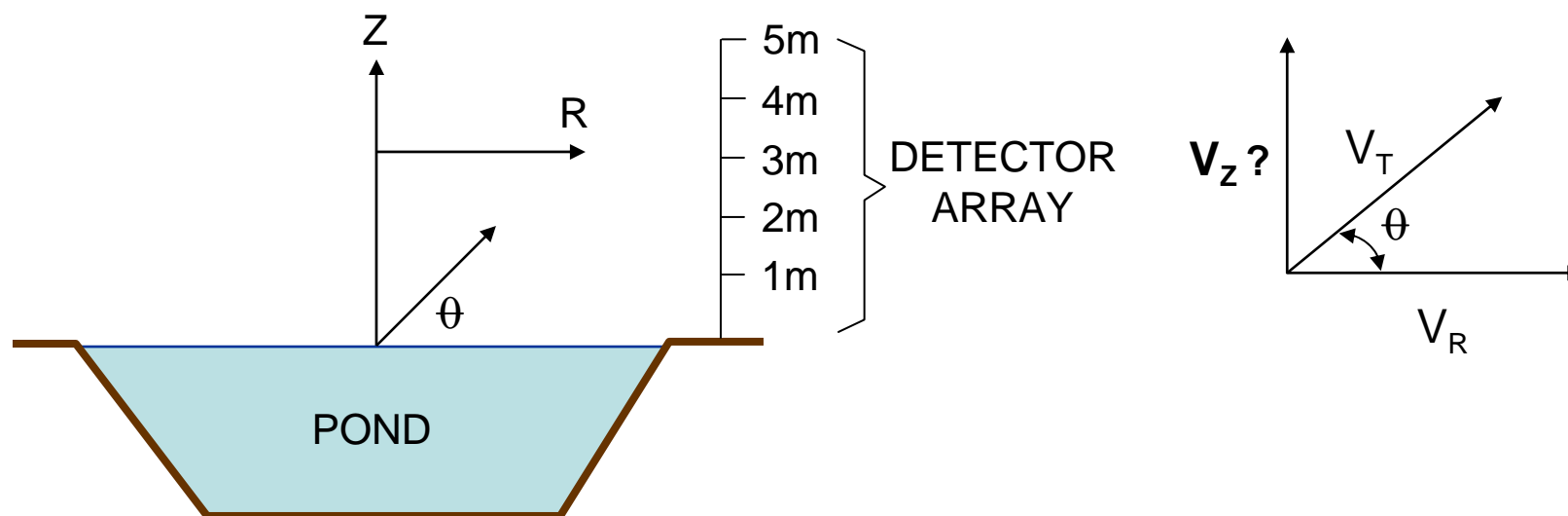
- ❖ Rn-222 is produced at the rate of $2.1 \times 10^{-6}/s$ from Ra-226
- ❖ Assumes radon released at surface as it is produced from Ra-226 within “turbulent” layer

Ra-226 (pCi/L)	Depth of Turbulent Mixing (cm)	Rn-222 (pCi/m ² ·s)
10	10	0.002
	50	0.01
100	10	0.02
	50	0.1
1000	10	0.2
	50	1

Can We Measure Radon Flux From Water Covered Tailings ?

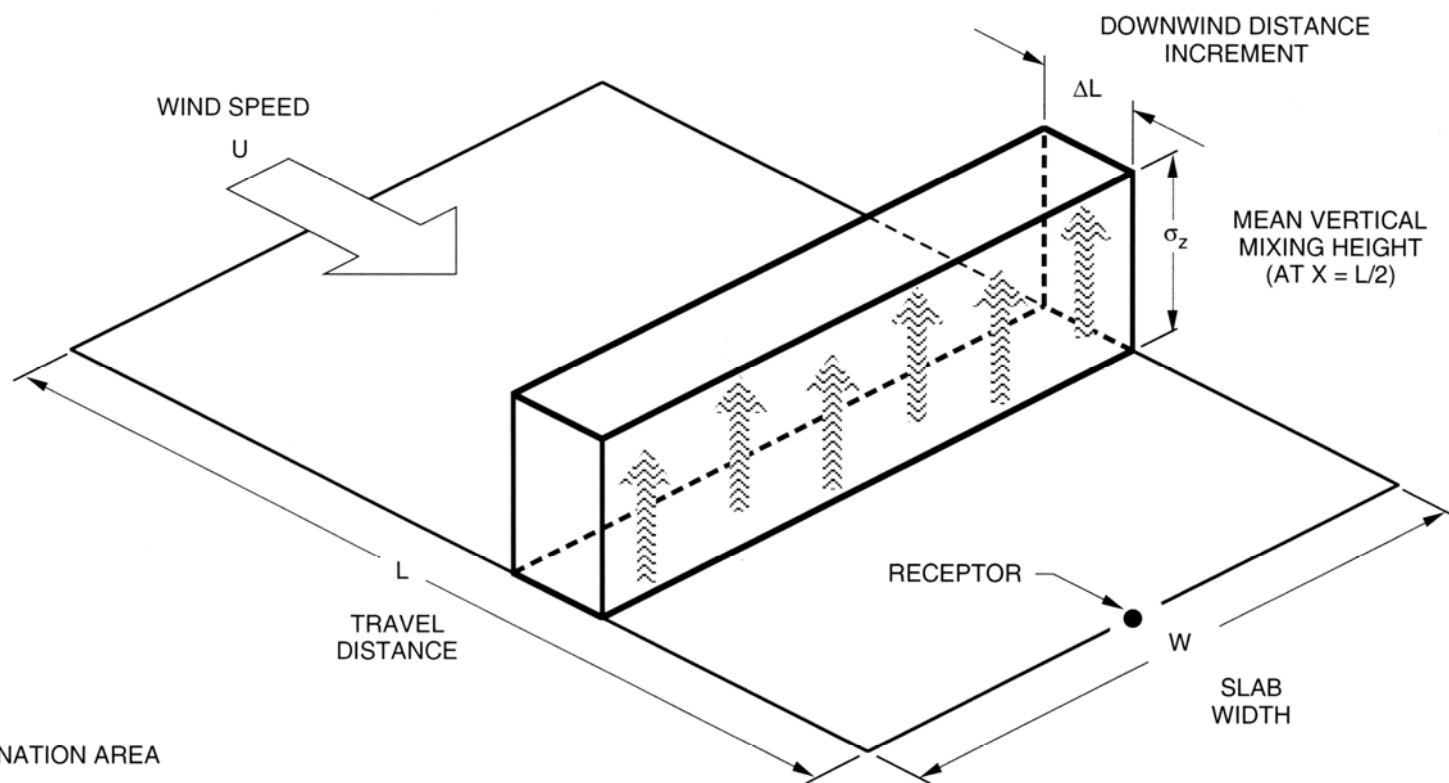
- ❑ EPA's proposal
- ❑ Schiager's method
- ❑ Diurnal variation
- ❑ Rn-222 with distance
- ❑ Pb-210 with distance

Pond Showing Z & R Directions and Detector Array



SOURCE: After EPA, 2009

Schiager's Box Model



NOTE:

$W\Delta L$ = EMANATION AREA

$\sigma_z W\Delta L$ = DILUTION VOLUME

$$C_x \text{ (pCi / m}^3\text{)} = \frac{[\text{FLUX, } \Phi] [\text{AREA, } W\Delta L] [\text{TIME, } L/U]}{[\text{VOLUME, } \sigma_z W\Delta L]} = \frac{\Phi L}{U \sigma_z}$$

σ_z defined by stability class

SOURCE: After Schiager, 1974

Incremental Radon

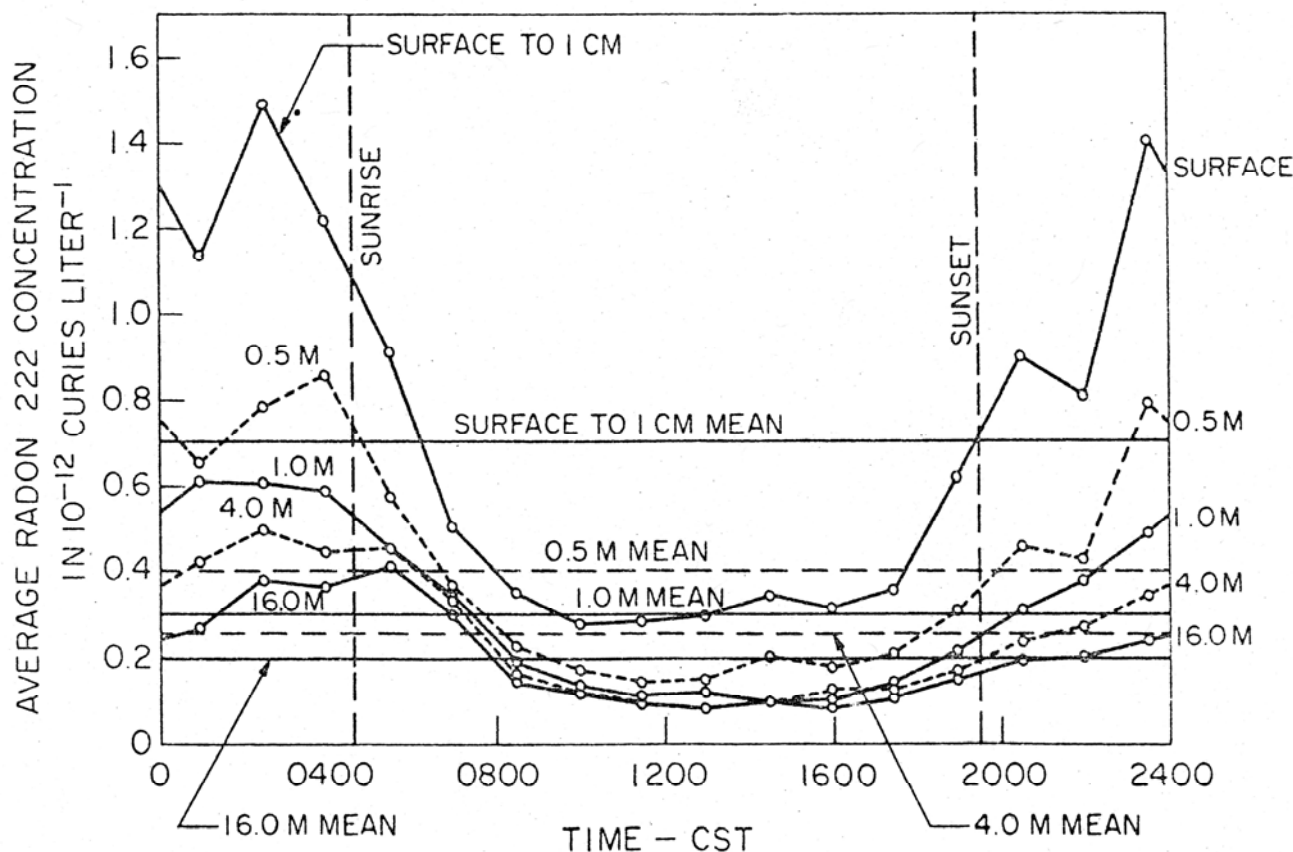
❑ Using Schiager model

- ❖ 80 acres of pond
- ❖ Radon flux of $1 \text{ pCi/m}^2 \cdot \text{S}$
- ❖ $L = 600 \text{ m}$
- ❖ Sigma z from Turner workbook of (about) 24m
- ❖ Assume $u = 3 \text{ m/s}$

❑ Radon concentration at edge of cell

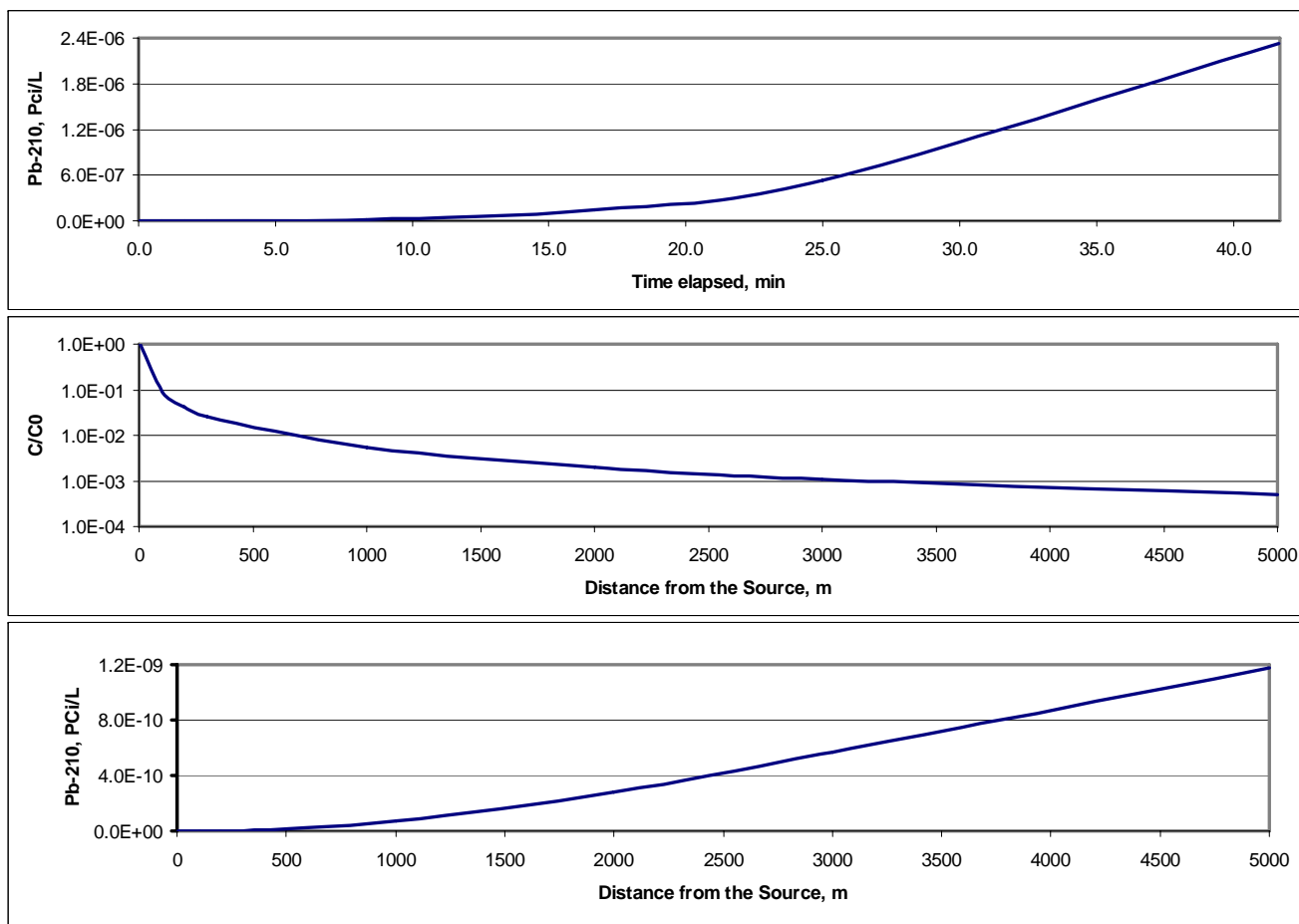
$$\begin{aligned} C &= (1 \times 600) / (3 \times 24) \text{ pCi/m}^3 \times 1 \text{ m}^3 / 1000\text{L} \\ &= 0.08 \text{ pCi/L} \end{aligned}$$

Rn-222 Concentration Diurnal Variation



SOURCE: After Pearson, U.S. Department of Health & Welfare, 1967

Pb-210 with Distance*



- * Denver Windrose, 80 acre source at $1\text{pCi/m}^2\text{s}$, direction of maximum concentration
- ** Background Pb-210 ranges from $3 \times 10^{-6} \text{ pCi/L}$ to $30 \times 10^{-6} \text{ pCi/L}$ (UNSCEAR 2000)

Key Observations

- ❑ Rn-222 is everywhere
- ❑ Concentrations of Rn-222 vary with location, time of day, meteorological conditions
- ❑ Rn-222 flux from ponded areas << dry areas
- ❑ Practical limits on ability to measure Rn-222 (or Pb-210) from pond areas
- ❑ Suggest feasibility assessment (DQO process) prior to implementation of proposed monitoring practices