



July 24, 2009  
NRC:09:078

Document Control Desk  
U.S. Nuclear Regulatory Commission  
Washington, D.C. 20555-0001

**Response to Request for Comment on Draft SER for EMF-2209(P) Revision 2, Addendum 1 and ANP-10249(P) Revision 0, Supplement 1**

Ref. 1: Letter, Stacey L. Rosenberg (NRC) to Ronnie L. Gardner (AREVA NP Inc.), "Draft Safety Evaluation for AREVA NP Inc. (AREVA) Topical Reports (TR) EMF-2209(P), Revision 2, Addendum 1, "SPCB Additive Constants for Atrium-10 Fuel" And ANP-10249(P), Revision 0, Supplement 1, "ACE Additive Constants for Atrium-10 Fuel" (TAC Nos. MD8754 and MEO162), "July 6, 2009.

Ref. 2: Letter, Ronnie L. Gardner, (AREVA NP Inc.) to Document Control Desk (NRC), "Request for Review and Approval of EMF-2209(P), Revision 2, Addendum 1, 'SPCB Additive Constants for ATRIUM-10 Fuel'," NRC:08:028, May 1, 2008.

Ref. 3: Letter, Ronnie L. Gardner, (AREVA NP Inc.) to Document Control Desk (NRC), "Request for Review and Approval of ANP-10249P, Revision 0, Supplement 1, Revision 0, 'ACE Additive Constants for ATRIUM-10 Fuel'," NRC:08:054, July 31, 2008.

In Reference 1 the NRC requested comments on the combined Draft SER pursuant to the Reference 2 and 3 topical report reviews. The combined draft SER has been evaluated and proprietary markings have been added to the Draft SER. One set of proprietary markings (brackets) have been added to the Draft SER beginning on Line 20 of Page 3 and ending on line 24 of the same page. Proprietary and non-proprietary versions of the Draft SER are attached.

Note that AREVA NP has also provided editorial comments regarding the citing of References 1 and 2 in Section 5 of the Draft SER.

If you have any questions related to this proprietary submittal, please contact Mr. Alan B. Meginnis, Product Licensing Manager at 509-375-8266 or by e-mail at [alan.meginnis@areva.com](mailto:alan.meginnis@areva.com).

Sincerely,

A handwritten signature in cursive script that reads "Ronnie L. Gardner".

Ronnie L. Gardner, Manager  
Corporate Regulatory Affairs  
AREVA NP Inc.

**AREVA NP INC.**  
An AREVA and Siemens company

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T007  
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Enclosures

cc: H. D. Cruz  
R. Subbaratnam  
Project 728



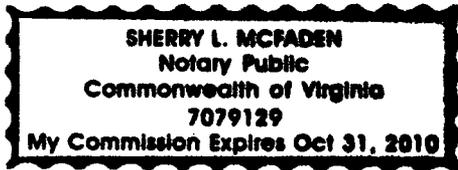
9. The foregoing statements are true and correct to the best of my knowledge, information, and belief.

Alan B. Meyer

SUBSCRIBED before me this 24<sup>th</sup>  
day of July, 2009.

Sherry L. McFaden

Sherry L. McFaden  
NOTARY PUBLIC, COMMONWEALTH OF VIRGINIA  
MY COMMISSION EXPIRES: 10/31/10  
Reg. # 7079129



DRAFT SAFETY EVALUATION BY THE OFFICE OF NUCLEAR REACTOR REGULATION

AREVA NP, INC. (AREVA) TOPICAL REPORTS

EMF-2209(P), REVISION 2, ADDENDUM 1

"SPCB ADDITIVE CONSTANTS FOR ATRIUM-10 FUEL," AND

ANP-10249 (P), REVISION 0, SUPPLEMENT 1

"ACE ADDITIVE CONSTANTS FOR ATRIUM-10 FUEL"

AREVA NP, INC.

PROJECT NO. 728

1 1.0 INTRODUCTION AND BACKGROUND

2

3 AREVA NP, INC. (AREVA) submitted, by letters dated, May 1, 2008, and July 31, 2008, the  
4 following topical reports (TRs): EMF-2209(P), Revision 2, Addendum 1, "SPCB Additive  
5 Constants for ATRIUM-10 Fuel" and ANP-10249 (P), Revision 0, Supplement 1, "ACE Additive  
6 Constants for ATRIUM-10 Fuel," for U.S. Nuclear Regulatory Commission (NRC) staff review  
7 and approval. These submittals are in response to the 10 CFR Part 21 notification, dated  
8 October 8, 2007.

9

10 The above stated AREVA submittals document revisions made to the ACE and SPCB critical  
11 power correlations additive constants for ATRIUM-10 fuel for boiling water reactors (BWRs).  
12 The additive constants were revised in response to an error discovered in the evaluation of the  
13 laboratory data when accounting for the power distribution and the power contained in the part  
14 length fuel rods. Evaluations have confirmed that the SPCB critical power correlation  
15 coefficients do not require revision as a result of the error.

16

17 The SPCB correlation was developed for two fuel types, the ATRIUM-10 and the ATRIUM-9 fuel  
18 designs. However, application of the SPCB correlation to ATRIUM-9 fuel does not require  
19 revision as this fuel design does not contain part-length fuel rods. AREVA also noted that the  
20 error discussed in these reports is restricted to critical heat flux (CHF) testing of the ATRIUM-10  
21 fuel. Application of the ACE and SPCB additive constant correlation to co-resident BWR fuel  
22 containing part-length fuel rods using the NRC approved method described in References 1 and  
23 2, do not require revision.

ENCLOSURE

1   2.0   REGULATORY EVALUATION

2  
3   In its review of EMF-2209 (P), Addendum 1 and ANP-10249 (P) Revision 0, Supplement 1, the  
4   staff utilized the guidance of Standard Review Plan 4.4 "Thermal and Hydraulic Design." SRP  
5   4.4 implements the requirements of General Design Criterion 10 which is found in Appendix A to  
6   10CFR50 to the Commissions regulations. GDC-10 states the following:

7  
8   The reactor core and associated coolant, control, and protection systems shall be designed with  
9   the appropriate margin to assure that specified acceptable fuel design limits are not exceeded  
10   during any condition of normal operation, including the effects of anticipated operational  
11   occurrences.

12  
13   The guidance from SRP - 4.4 which is applicable to the review of EMF-2209 (P), Addendum 1  
14   and ANP-10249 (P) Revision 0, Supplement 1, is Acceptance Criterion 1.b, which states that for  
15   correlations used to predict critical power, the limiting (minimum) value should be established so  
16   that at least 99.9% of the fuel rods in the core will not be expected to experience departure from  
17   nucleate boiling or boiling transition during normal operation or anticipated operational  
18   occupations.

19  
20   3.0   TECHNICAL EVALUATION

21  
22   3.1   Test Data Modifications

23  
24   The AREVA test facility uses electrically heated rods to simulate the behavior of the fuel bundle  
25   in the reactor core. The electrical power generated in the individual rods is readily calculated by  
26   knowing the voltage, current, and/or the resistance of the various components. The surface of  
27   the simulated rods serves as the electrical conductor for the full length rods. The part length  
28   rods carry the current on the surface of the rod in one direction and then through an inner  
29   copper conductor in the other direction. Consequently, the power for the part-length rods  
30   should account for the power associated with current at the surface of the rod and in the portion  
31   of the inner copper conductor that is contained within the heated length. The initial method for  
32   determining the power distribution within the bundle did not properly account for the power of  
33   the inner copper conductor of the part-length rods in the test bundle. The test data power  
34   distributions and the total power generated in a bundle were modified to properly account for the  
35   power present in the inner copper conductor in the part-length rods.

36  
37   3.2   Power Distributions

38  
39   AREVA assessed the impact of the modified additive constants on all the pertinent power  
40   distributions. AREVA recalculated lattice peaking powers and noted that, when the power  
41   carried in the inner copper conductor of the part length rods is included, the relative power  
42   delivered by the part-length rods in the lower end of the lattice (in the fully rodDED region below  
43   the end of the part-length rods) of the bundle, increased compared to the previously reported  
44   powers. Consequently, on a normalized relative power basis, the radial peaking factors of the  
45   part-length rods increase, and the radial peaking factors of the full-length rods decrease in the  
46   fully rodDED region of the bundle. See Figures 3.1 and 3.2 of References 1 and 2.

47  
48   The inclusion of the power associated with the inner copper conductor of the part-length heater  
49   rods impacts the axial power shape of the part length rods, and consequently impacts the

1 bundle average axial power. However, because the power associated with the inner copper  
2 conductor is such a small fraction of the overall bundle power (much less than 1 percent), the  
3 impact is small.  
4

5 The development of the ACE and SPCB correlations was based on selected axial power  
6 shapes. The adjustment to the additive constants included the axial power shapes from  
7 measurements of the individual rod axial shapes for both, full-length rods and part-length rods.  
8 The part-length heater rods accounted for the incorporation of the inner copper conductor. An  
9 example comparing the bundle average axial power shape for the bundle STS 17.1 is shown in  
10 Figure 3.3 of References 1 and 2. The calculations show that the impact is small, and that the  
11 impact on the bundle axial power shape was included in the revised additive constant  
12 calculations.  
13

### 14 3.3 Additive Constants

15 Having corrected the respective power distributions, both the lattice power and the bundle  
16 power, AREVA performed calculations to determine the boiling transition values of f-effective  
17 (SPCB), and the K-factors (ACE), respectively, for each test in the data base. The boiling  
18 transition values of f-effective are those values that result in a critical power ratio of 1.0 at the  
19 measured operating condition. [  
20  
21

22  
23  
24 ] A detailed description of the determination of the new  
25 additive constants is provided in responses to requests for additional information (RAIs) in  
26 Reference 3. The newly derived additive constants supersede the additive constants that were  
27 presented in Reference 4 and 5.  
28

### 29 3.4 Evaluation of Transient Critical Power Data

30  
31 AREVA re-analyzed the transient critical power tests presented in References 4 and 5 using the  
32 revised initial bundle powers, axial power shapes, f-effective and K-factors values. The  
33 repeated analysis was performed consistent with Reference 4 and 5. The calculated time of  
34 boiling transition of each test for the repeat analysis are presented in Table 6.1 of References 1  
35 and 2, and Table 7.1 in Reference 2.  
36

37 Table 7.1 of Reference 2 indicates that two of the tests listed in 7.1 are slightly non-  
38 conservative. The explanation for the minor non-conservatism provided by AREVA is that in  
39 one of the tests (Test STS-17.8-u6.2), simulating a flow decay event along with a correspondent  
40 power decay, the power decay was delayed by nearly a full second after the initiation of the flow  
41 decay. Typically, an event of this kind experiences an instantaneous power decrease during a  
42 flow decay transient. Consequently, the test is considered "atypical", and thus is not a true  
43 representation of a realistic plant event. The other test that indicates a minor non-conservatism  
44 is Test STS-29.5-H100.1. For this test, AREVA pointed out that Test STS-29.5-H100.4 had  
45 very similar initial boundary conditions, but that Test STS-29.5-H100.4 had a lower bundle  
46 power, and is representative of how the transient calculation is performed in a licensing  
47 procedure. But, in Test STS-29.5-H100.1, the initial bundle power was too high and thus not  
48 representative of realistic licensing event. Also, the higher power case would not be analyzed  
49 because boiling transition is to happen at a lower bundle power.

1 The analysis conducted by AREVA in support of this issue indicated that the changes to initial  
2 bundle powers, axial power shapes, f-effective and K-factors values, did not impact conclusions  
3 in References 4 and 5. The repeated analysis for each of these parameters demonstrated that  
4 the ACE and SPCB steady-state "Dry-out" correlations continue to be appropriate for use in  
5 evaluating transient events.

6  
7 **4.0 CONCLUSION**

8  
9 The NRC staff finds that the revisions AREVA provided in the submittal regarding the  
10 uncertainties associated with the additive constants are acceptable. The revised additive  
11 constants will supersede the additive constants for the ATRIUM-10 that is presented in  
12 Reference 4 and 5.

13  
14 The additive constants were revised in response to an error discovered in the evaluation of the  
15 laboratory data when accounting for the power distribution and the power contained in the part-  
16 length fuel rods.

17  
18 Application of SPCB to ATRIUM-9 fuel does not require revision, as this fuel design does not  
19 contain part-length fuel rods. Since the error discussed in this report is restricted to CHF testing  
20 of the ATRIUM-10 fuel, applications of ACE and SPCB to co-resident BWR fuel containing part-  
21 length fuel rods using the NRC approved method described in Reference 1 do not require  
22 revision.

23  
24 The NRC staff acknowledges that AREVA will combine this safety evaluation with the previously  
25 approved TRs, to issue Revision 3 of TR EMF-2209, and Revision 1 of TR ANP-10249 . All  
26 parts of the latest revisions have been approved by the NRC staff. Therefore, Revision 3 of TR  
27 EMF-2209, and Revision 1 of TR ANP-10249, can be submitted as the approved versions of the  
28 TRs. This will allow use of current plant technical specification (TS) references without  
29 modifications to the standard TSs.

30  
31 **5.0 REFERENCES**

32  
33 1. Letter, Ronnie L. Gardner, Manager, Site operations and Corporate Regulatory Affairs,  
34 AREVA, to the U.S. Nuclear Regulatory Commission, requesting review and approval of  
35 EMF-2209 (P), Revision 2, Addendum 1, "SPVB Additive Constants for Atrium-10 Fuel,"  
36 dated May 1, 2008, .....

Deleted: September 2003.

37  
38 2. Letter, Ronnie L. Gardner, Manager, Site operations and Corporate Regulatory Affairs,  
39 AERVA, to the U.S. Nuclear Regulatory Commission, requesting review and approval of  
40 ANP-10249 (P), Revision 0, Supplement 1, Revision 0, ACE Additive Constants for  
41 ATRIUM-10 Fuel," dated July 31, 2008, .....

Deleted: September 26, 2007

