

## 1.0 OBJECTIVE

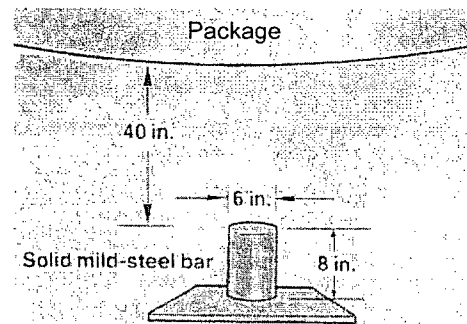
Evaluation of the 3-60B Cask (Reference 1) under:

- Regulatory puncture drop-test
- Hypothetical drop test when the trunnions are orientated in the vertical plane.

## 2.0 INTRODUCTION

In order to get the 3-60B Cask certified as a Type-B package, it must demonstrate the requirements of the 10 CFR Part 71 (Reference 2) code. One of the requirements listed in the code is for the cask to meet a puncture drop test of § 71.73(c)(3), which states:

“A free drop test of the specimen through a distance of 1 m (40 in) in a position for which maximum damage is expected, onto the upper end of a solid, vertical, cylindrical, mild steel bar mounted on an essentially unyielding, horizontal surface. The bar must be 15 cm (6 in) in diameter, with the top horizontal and its edge rounded to a radius of not more than 6 mm (0.25 in) and of a length as to cause maximum damage to the package, but not less than 20 cm (8 in) long. The long axis of the bar must be vertical.”



This test is required to be conducted after the hypothetical drop tests.

In order to assess the package performance an analytical evaluation is accepted means. This document presents the analyses performed for the 3-60B Cask to meet the requirement of the puncture test.

Two scenarios are identified that could cause the maximum damage to a particular component of the cask. In one, the cask is assumed to be dropped on the puncture bar in a horizontal orientation such that the puncture bar impacts the sidewall of the cask. In this case the outer shell is evaluated against the puncture bar piercing through it. In the other, the cask is assumed to be dropped in a vertical orientation such that its lid impacts the puncture bar. In this case the cask lid is evaluated. The closure bolts are separately evaluated for this condition using NUREG-6007 methodology in the SAR.

For the puncture drop on the sidewall a nonlinear inelastic analysis of the cask wall has been performed using ANSYS (Reference 3) finite element model to show that the entire amount of the potential energy may be converted into mechanical work done, without exceeding the allowable stresses in the cask outer shell.

For the evaluation of the puncture drop on the cask lid, analysis is performed using the linear elastic finite element model that has been used in other evaluations, e.g. NCT conditions (Reference 4). The effect of cold and hot conditions is included in the analyses.

The results of the analyses show that the 3-60B Cask can withstand the drop on the puncture bar, without rupture. Therefore, the requirements of § 71.73(c)(3) are satisfied.

The analyses performed here are also utilized to evaluate the 3-60B Cask under the hypothetical drop tests scenario in which the trunnions are located in the vertical plane. Under such drop scenarios the impact limiters may deform enough so that the trunnions could impact the rigid plane before the cask comes to rest. It has been shown that under all the drop orientations, except the slapdown, the impact limiters provide enough protection that the trunnions will not impact the rigid target plane. Under the slapdown conditions the impact limiters absorb enough energy such that the remaining energy can be safely absorbed by the cask, without damage to the outer shell. Hence the package will meet the requirements of § 71.73(c)(3) for the hypothetical drop test in this orientation.

### 3.0 REFERENCES

1. *EnergySolutions* Drawing No. C-002-165024-001, Rev.0, 3-60B Cask General Arrangement and Details.
2. Code of Federal Regulations, Title 10, Part 71, Packaging and Transportation of Radioactive Material, January 2003.
3. ANSYS, Rev. 11.0, Computer Software, ANSYS Inc., Canonsburg, PA, 2007.
4. *EnergySolutions* Document No. ST-501, Rev.1, Structural Analyses of the 3-60B Cask under Normal Conditions of Transport.
5. ASME Boiler & Pressure Vessel Code, Section II, Part D, Materials, The American Society of Mechanical Engineers, New York, NY, 2005.
6. NUREG 0481/SAND77-1872, An Assessment of Stress-Strain Data Suitable for Finite Element Elastic-Plastic Analysis of Shipping Containers, Sandia National Laboratories, 1978.
7. U.S. NRC Regulatory Guide 7.6, Revision 1, Design Criteria for the Structural Analysis of Shipping Cask Containment Vessels, 1978.
8. *EnergySolutions* Proprietary Document ST-557, Drop Analyses of the 3-60B Cask Package Using LS-DYNA Program.

**4.0 MATERIAL PROPERTIES**

Material	Temp. (°F)	Strength (ksi)			Young's Modulus (10 <sup>6</sup> psi)	Coefficient of Thermal Expansion (10 <sup>-6</sup> in/in)
		Yield (S <sub>y</sub> )	Ultimate (S <sub>u</sub> )	Membrane Allowable (S <sub>m</sub> )		
ASTM A240 Type 304L		(1)	(1)	(1)	(1)	(1)
	-20	25.0	70.0	16.7	28.8	-
	70	25.0	70.0	16.7	28.3	8.5
	100	25.0	70.0	16.7	-	8.6
	200	21.4	66.1	16.7	27.5	8.9
	300	19.2	61.2	16.7	27.0	9.2
	400	17.5	58.7	15.8	26.4	9.5
500	16.4	57.5	14.7	25.9	9.7	
ASTM A240 Gr. 45 & ASTM A182 Gr. F45		(1)	(1)	(1)	(1)	(1)
	-20	45.0	87.0	24.9	28.8	-
	70	45.0	87.0	24.9	28.3	8.5
	100	45.0	87.0	24.9	-	8.6
	200	37.5	86.4	24.7	27.5	8.9
	300	33.0	81.6	23.3	27.0	9.2
	400	29.9	78.5	22.4	26.4	9.5
500	27.8	76.4	21.8	25.9	9.7	
ASTM A354 Gr. BD (Lid Bolts)		(1)	(1)	(1)	(1)	(1)
	-20	130	150	30	29.7	-
	70	130	150	30	29.2	6.4
	100	130	150	30	-	6.5
	200	119.1	150	30	28.6	6.7
	300	115	150	30	28.1	6.9
	400	111	150	30	27.7	7.1
500	105.9	150	30	27.1	7.3	
ASTM B29 Lead		(2)			(2)	(2)
	-20	-	-	-	2.43	15.65
	70	5	-	-	2.27	16.06
	100	-	-	-	2.21	16.22
	200	-	-	-	2.01	16.70
	300	-	-	-	1.85	17.33
	400	-	-	-	1.70	18.16
500	-	-	-	1.52	19.12	

Notes:

- (1) From ASME B&PV Code 2004, Section II, Part D (Reference 5).
- (2) From NUREG/CR 0481 (Reference 6)

**5.0 ALLOWABLE STRESSES**

Material →		ASTM A240 Type 304L	ASTM A182 Gr.F45 & A240 Gr. 45	ASTM A354 Gr. BD
Yield Stress, $S_y$	(psi)	25,000 <sup>(1)</sup>	45,000 <sup>(1)</sup>	130,000 <sup>(1)</sup>
Ultimate Stress, $S_u$	(psi)	70,000 <sup>(1)</sup>	87,000 <sup>(1)</sup>	150,000 <sup>(1)</sup>
Design Stress Intensity, $S_m$	(psi)	16,700 <sup>(1)</sup>	24,900 <sup>(1)</sup>	30,000 <sup>(1)</sup>
Normal Conditions	Membrane Stress	16,700 <sup>(2)</sup>	24,900 <sup>(2)</sup>	60,000 <sup>(2)</sup>
	Mem. + Bending Stress	25,050 <sup>(2)</sup>	37,350 <sup>(2)</sup>	90,000 <sup>(2)</sup>
	Peak Stress	50,100 <sup>(3)</sup>	74,700 <sup>(3)</sup>	150,000 <sup>(3)</sup>
Hypothetical Accident Conditions	Membrane Stress	40,080 <sup>(4)</sup>	59,760 <sup>(4)</sup>	105,000 <sup>(4)</sup>
	Mem. + Bending Stress	60,120 <sup>(4)</sup>	87,000 <sup>(4)</sup>	150,000 <sup>(4)</sup>
	Peak Stress	140,000 <sup>(5)</sup>	174,000 <sup>(5)</sup>	300,000 <sup>(5)</sup>

Notes:

- (1) From ASME B&PV Code 2004, Section II, Part D (Reference 5).
- (2) Established from Regulatory Guide 7.6 (Reference 7).
- (3) Established from Regulatory Guide 7.6, Regulatory Position 4, and ASME, Section III, Division 3, WB-3200 criteria. The limit on this stress component is  $3S_m$ .
- (4) Regulatory Guide 7.6 (Reference 7) does not provide any criteria. ASME B&PV Code, Section III, Appendix F has been used to establish these criteria.
- (5) Regulatory Guide 7.6, Regulatory Position 7 and ASME Section III, Division 3, WB-3221.9 criteria of limiting these stresses to  $2S_a @ 10$  cycles results in higher than  $2S_u$  allowable values. The limits for peak stresses are conservatively set to be  $2S_u$ .

**6.0 MODEL DESCRIPTION**

The structural analyses of the 3-60B Cask under puncture drop conditions have been performed using finite element modeling techniques. ANSYS finite element analysis code

(Reference 3) has been employed to perform the analyses. Two different models have been employed to address two puncture drop scenarios.

### **6.1 Scenario 1: Puncture Drop on the Sidewall**

The puncture drop on the sidewall causes high local stresses at the point of contact. The magnitude of these stresses attenuates quickly with distance. Thus for the evaluation of the stresses in the cask under this loading a finite element model representing the sidewall in the vicinity of the impact has been employed. Since the cylindrical cask-to-the cylindrical pin impact provides two planes of symmetry, the model uses two vertical symmetry planes. In the horizontal plane there is no plane of symmetry. However, since the stresses resulting from the impact are highly local, based on St. Venant's principle, approximate boundary conditions on the horizontal plane will have little effects on the stresses at the point of impact. Symmetry boundary conditions on this plane, in fact will result in a conservative stress prediction. Thus the FEM used in the analysis has three planes of symmetry. This model is shown in Figure 1.

### **6.2 Scenario 2: Puncture Drop on the Lid**

For the puncture drop on the lid, the cyclic symmetry of the cask has been utilized. Since the lid of the cask is attached to the body using 16 bolts, the cask geometry has a cyclic symmetry every 11.25° of the circumference. Therefore, an 11.25° model of the cask is made using 3-dimensional 8-node structural solid elements (ANSYS SOLID185) to represent the major components of the cask, the cask body, the lid, and the bolts. The fire shield does not provide any structural strength to the cask. Therefore, it is not included in the model.

The poured lead in the body of the cask is not bonded to the steel. It is free to slide over the steel surface. Therefore, the interface between the lead and the steel is modeled by a pair of contact (CONTA174) and target (TARGE170) elements. These elements allow the lead to slide over the steel at the same time prevent it from penetrating the steel surface.

Figure 2 shows the finite element model of the cask used for the puncture drop analysis of 3-60B on its lid.

## **7.0 RESULTS & CONCLUSIONS**

### **7.1 Scenario 1: Puncture Drop on the Sidewall**

Analyses using the FEM described in Section 6.1 are performed for obtaining the force-deflection plot. A known amount of load is applied in form of surface pressure at the end of the puncture bar. The deflection of the bar is obtained from the analysis of the FEM. Figure 3 shows the force-deflection plot at the end of the rod. The area under this plot gives the work done versus deflection relation. Using Microsoft Excel spreadsheet program the force-deflection curve is integrated to obtain the work done versus deflection plot shown in Figure 4. Energy versus deflection diagram also created as follows:

Mass of the package = 80,000 lb

Height of the package = 40 in

Assuming that the package travels an additional distance  $\delta$  before it comes to stop, the total potential energy is:

$$PE(\delta) = 80,000 \times (40 + \delta)$$

This curve is also plotted in Figure 4. The intersection of the potential energy curve and the work done curve represent the energy balance point. Any loading larger than that at the intersection point, applied to the FEM can be used to conservatively calculate the stresses in the structure. A loading much larger than the balance point loading is used to compute the stresses. This loading point is shown in Figure 4. Its selection is based on the fact that it envelopes the puncture drop loading and the cask drop on the trunnion loading covered in Section 7.3 of this document.

Figure 5 shows the maximum stress intensity in the inner and outer shells of the cask under this loading. Figure 6 shows the maximum stress intensity in the lead and Figure 7 shows the stress intensity in the outer shell of the cask under this loading.

From Figures 5 to 7, the maximum stress intensity in the lead is small (6,507 psi) and the maximum stress intensity in the outer shell is 63,084 psi. This stress intensity is compared to the ultimate tensile strength of the shell material, i.e. 70,000 psi. It is, therefore, concluded that the 3-60B Cask can safely withstand the regulatory puncture drop on its sidewall.

## 7.2 Scenario 2: Puncture Drop on the Lid

The puncture bar has 6" diameter and it is made of mild steel. Conservatively assuming a flow stress of 45,000 psi for the mild steel, the corresponding load is:

$$F = \pi/4 \times 6^2 \times 45,000 = 1.272 \times 10^6 \text{ lb}$$

This load is applied over a circle of 3.333 in. The equivalent pressure is therefore,

$$p = 1.272 \times 10^6 / (\pi \times 3.333^2) = 36,447 \text{ psi}$$

This load is applied as a surface pressure on the model described in Section 6.2. Both cold and hot environments have been analyzed for this loading.

The stresses in the cask under this loading are shown in Figures 8 through 10. From these figures it is observed that the maximum stress intensity occurs in the lid at the point of impact and its value is 41,568 psi. This stress intensity is compared to the ultimate tensile strength of the lid material, i.e. 70,000 psi. It is, therefore, concluded that the 3-60B Cask can safely withstand the regulatory puncture drop on its sidewall.

**7.3 Impact on Trunnion during HAC Testing**

Analyses of the 3-60B Cask have been performed in Reference 8 for the HAC drop test loading conditions. These analyses were performed using finite element models of the package with its major components. Since the objective of these analyses was to obtain the impact limiter reactions, detailed modeling of the cask was not necessary. However, from these analyses the complete deformation of the package can be obtained. These deformations could be used to establish whether the trunnions of the cask will contact the rigid target surface if the cask were to be dropped in an orientation such that the trunnions were located in the vertical plane as shown in Figure 11.

From the geometry of the package shown in Figure 11, the vertical distance between the lowest point of the impact limiter to the lowest point of the trunnions is 8 in. From the results of the Reference 8 analyses the maximum crush of the impact limiters during various drop scenarios is as follows:

Drop Orientation	Environment	Max. Crush
Side	Cold	6.50
	Hot	8.02
Slapdown-1	Cold	7.44
	Hot	9.04
Slapdown-2	Cold	7.23
	Hot	8.86

It can be seen that for most drop orientations the impact limiter crush is less than the minimum foam thickness available, i.e. 8 in. The largest crush of the impact limiter occurs during the slapdown-1 orientation (7½° from the horizontal) in the hot environment. Figure 12 shows a pictorial depiction of the deformation of the package at the instant of maximum tail impact limiter crush. Figure 13 shows the time-history of this crush. The internal energy time-history of the package is shown in Figure 14.

Figures 13 and 14 are used to establish the amount of energy that has been absorbed by the impact limiters before the tail-end trunnion could impact the rigid surface. The foam of the tail-end impact limiter crushes by 8" at time instant 0.057 second (see Figure 13). Figure 14 shows that at this time instant  $12.2 \times 10^6$  in-lb energy has been absorbed by the impact limiters. Since the result is for ½ model. The energy absorbed is  $2 \times 12.2 \times 10^6 = 24.4 \times 10^6$  in-lb.

The maximum potential energy of the package is obtained from its initial to final (resting) positions. Figure 15 shows these orientations. The distances of the C.G. for the two positions are also marked in this figure. The potential energy of the system is:

$$PE = 80,000 \times (360 + 51.418 - 35.025) = 30.1 \times 10^6 \text{ in-lb}$$

Since  $24.4 \times 10^6$  in-lb energy has already been absorbed in the impact limiters, the rest of the energy, i.e.  $(30.1 - 24.4) \times 10^6 = 5.7 \times 10^6$  in-lb must be accounted for between the crush of the trunnion and that of the tail-end impact limiter. Let us conservatively assume that this energy is totally absorbed by the cask body by the trunnion crush. The minimum diameter of the trunnion body is 8". Therefore, during the trunnion crush the load on the cask sidewall will be distributed over 8" circular area. Let us further conservatively assume that the bearing area on the cask is a circle of 6" diameter which is equal to the diameter of the puncture bar. Therefore, the evaluation performed for the puncture bar drop can be conservatively used to envelope the stresses in the package sidewall for direct impact on the trunnion during the HAC drop tests. Figure 4 annotates  $5.7 \times 10^6$  in-lb location on the energy-deflection plot curve.

In Section 7.2 stresses are evaluated in the cask sidewall for a loading level that envelopes both the puncture drop loading and the cask drop on the trunnion loading. It is shown that the maximum stress intensity of 63,084 psi will result in the cask sidewall under these loading conditions (see Figure 7). This stress intensity is compared to the ultimate tensile strength of the shell material, i.e. 70,000 psi. It is, therefore, concluded that the 3-60B Cask can safely withstand the regulatory HAC drop tests, with its trunnions oriented in the vertical plane, without exceeding the allowable stress value.

## 8.0 ANSYS PRINTOUT AND DATA FILES

The printout of the pertinent model quantities is included in Appendix 1. The printout of the important data from the program is included in electronic form as Appendix 2.

### APPENDICES

Appendix 1 Print-out of the ANSYS model data input

Appendix 2 Electronic data on CDROM



**Title** 3-60B Cask Analyses under Puncture Drop & Impact on Trunnions During HAC Testing

**Calc. No.** ST-505 **Rev.** 1

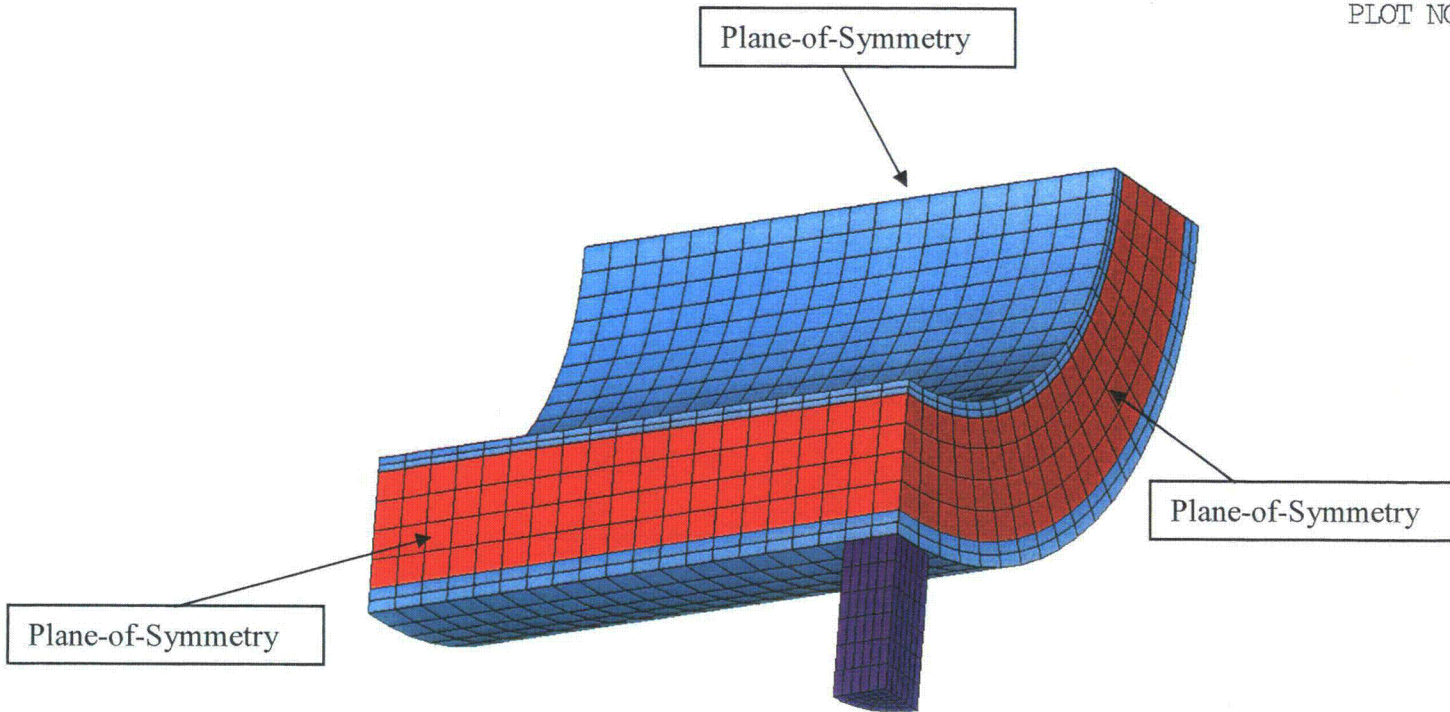
**Sheet** 9 **of** 11

**Figures**

(15 Pages)

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MAT NUM

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PLOT NO. 1



Puncture Drop on Cask Sidewall

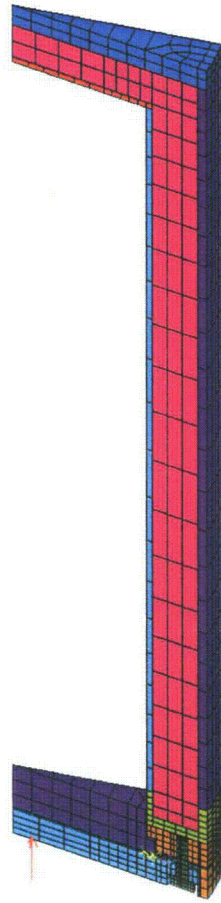
Figure 1

Finite Element Model of the 3-60B Cask for Puncture Drop on the Sidewall Analysis

**Title** 3-60B Cask Analyses under Puncture Drop & Impact on Trunnions during HAC Testing  
**Calc. No.** ST-505 (Figures) \_\_\_\_\_ **Rev.** 1 \_\_\_\_\_ **Sheet** 1 of 15 \_\_\_\_\_

ELEMENTS  
REAL NUM  
PRES-NORM  
36447

**ANSYS**  
JUN 16 2009  
16:05:04  
PLOT NO. 1



Puncture Drop on the Lid (Hot)

Title 3-60B Cask Analyses under Puncture Drop & Impact on Trunnions during HAC Testing  
Calc. No. ST-505 (Figures) Rev. 1 Sheet 2 of 15

Figure 2  
Finite Element Model of the 3-60B Cask for Puncture Drop on the Lid Analysis

3-60B Cask Puncture Drop

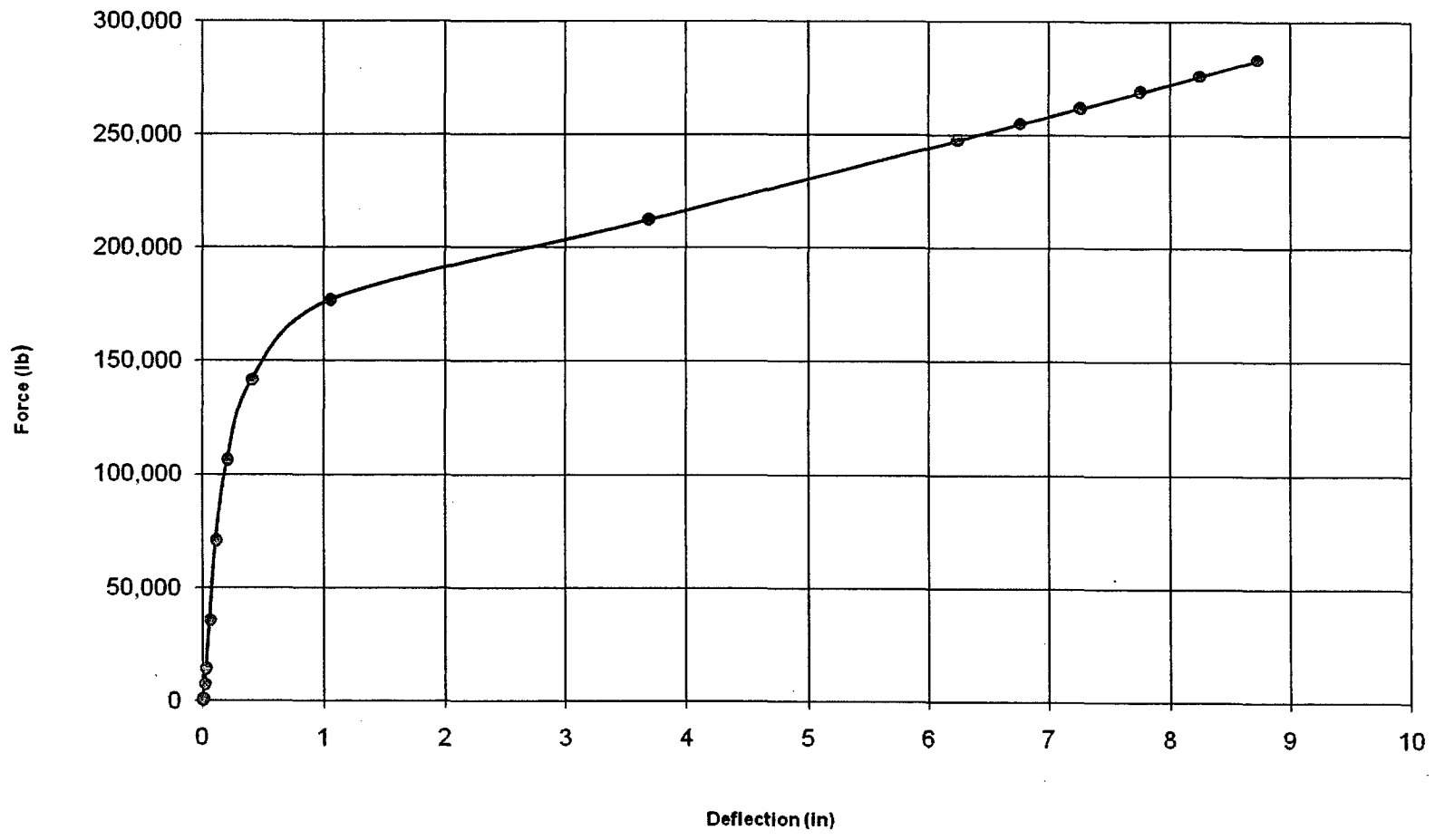


Figure 3  
Force-Deflection Plot at the Point of Impact

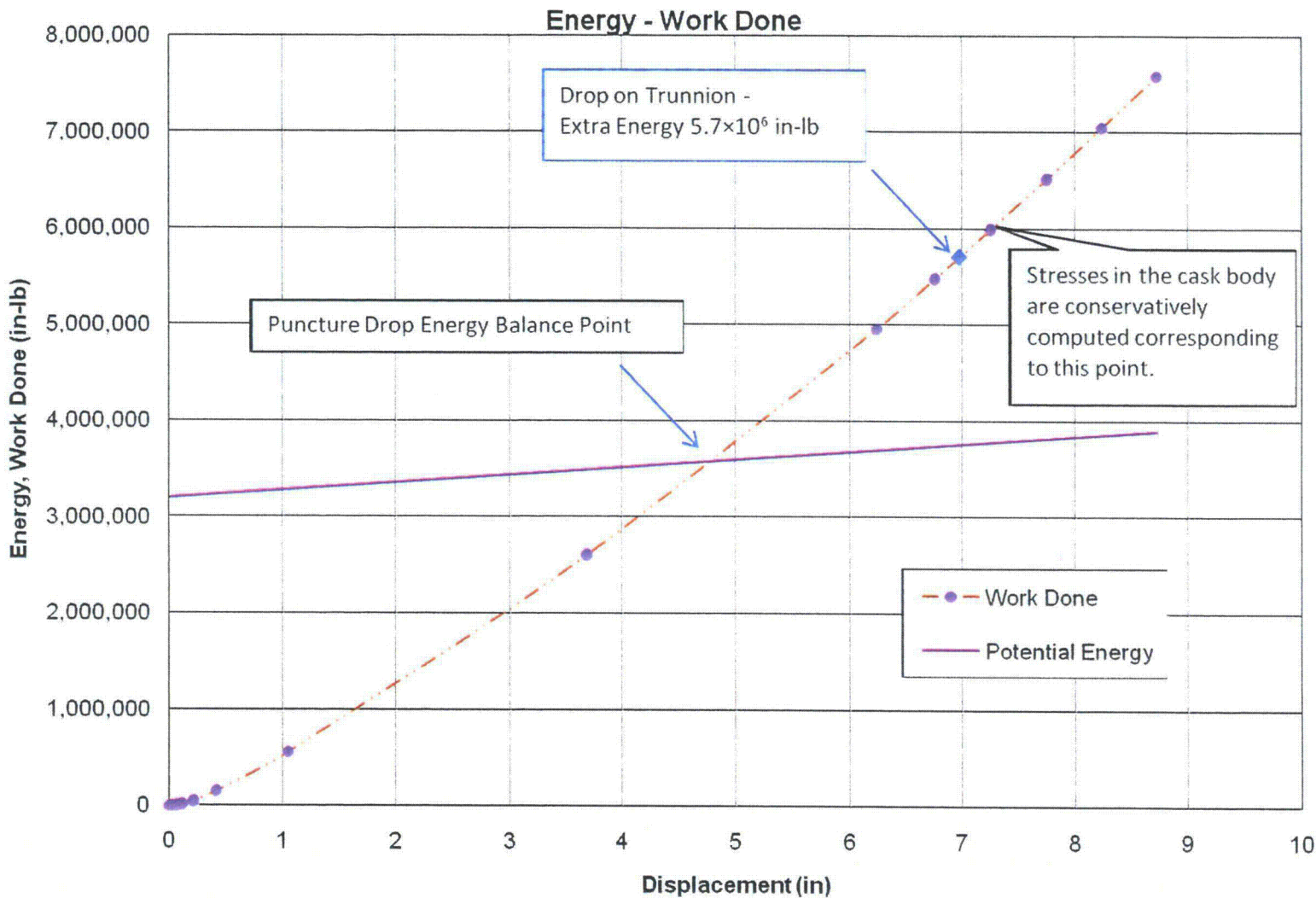


Figure 4  
Energy versus Deflection Plot



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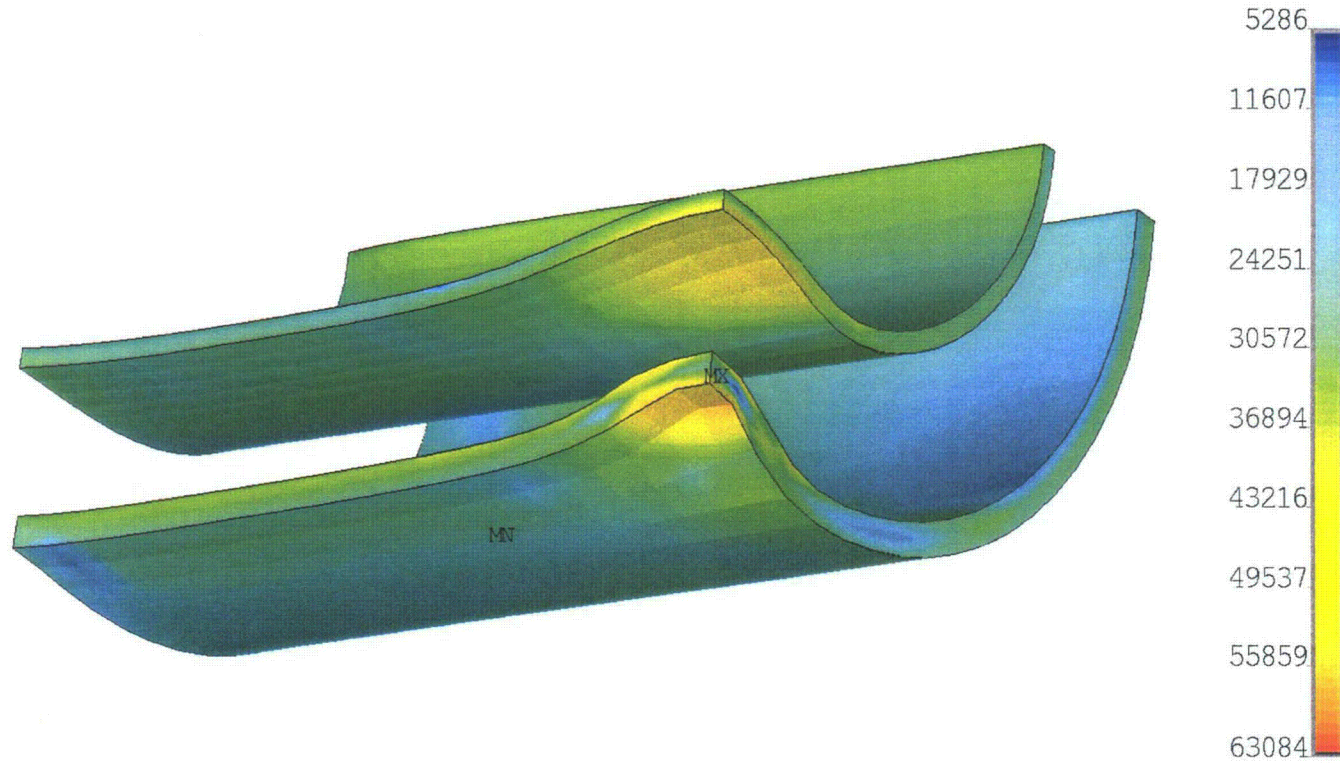
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ANSYS

JUN 15 2009

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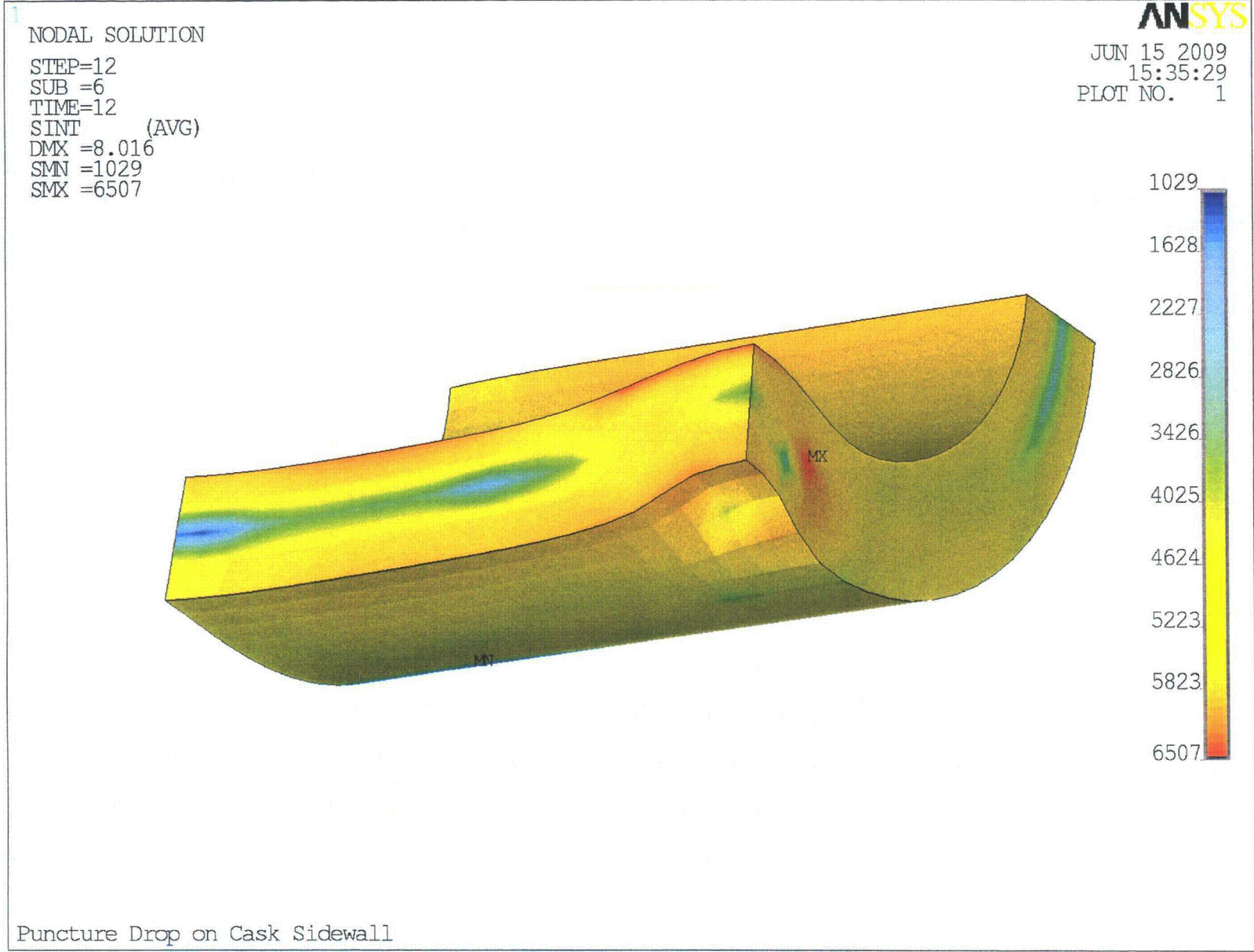
PLOT NO. 1



Puncture Drop on Cask Sidewall

Title 3-60B Cask Analyses under Puncture Drop & Impact on Trunnions during HAC Testing  
Calc. No. ST-505 (Figures) Rev. 1 Sheet 5 of 15

Figure 5  
Maximum Stress Intensity in the Inner & Outer Shells of the Cask under Puncture Drop



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Calc. No. ST-505 (Figures) \_\_\_\_\_ Rev. 1 \_\_\_\_\_ Sheet 6 of 15 \_\_\_\_\_

Figure 6  
Maximum Stress Intensity in the Lead under Puncture Drop



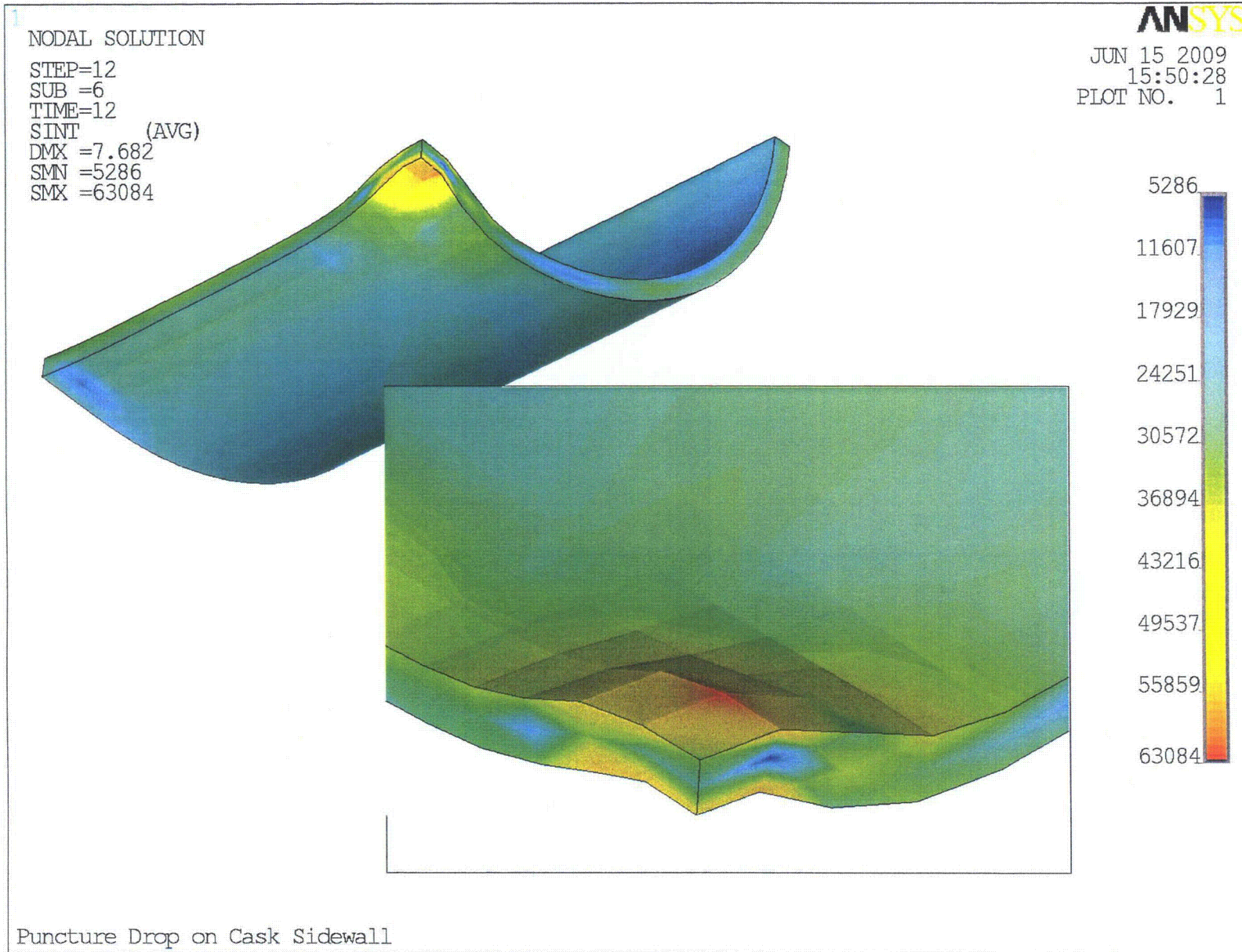


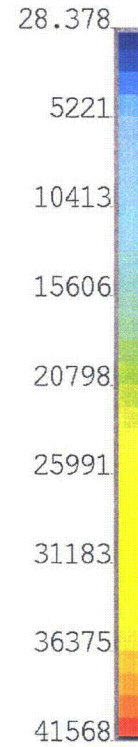
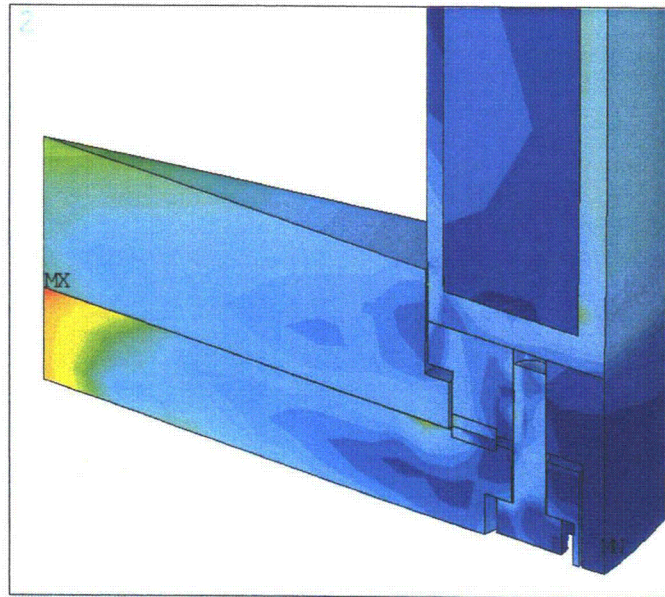
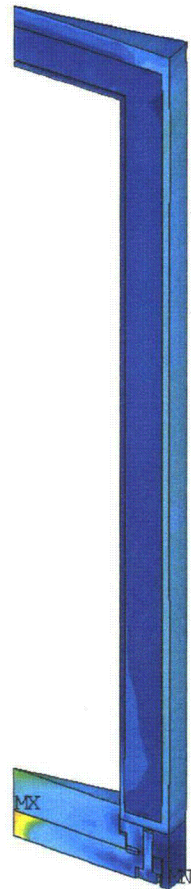
Figure 7  
 Maximum Stress Intensity in the Outer Shells of the Cask under Puncture Drop



NODAL SOLUTION

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SMN =28.378  
SMX =41568

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PLOT NO. 1



Puncture Drop on the Lid (Hot)

Figure 8  
Maximum Stress Intensity in the Cask under Puncture Drop on the Lid

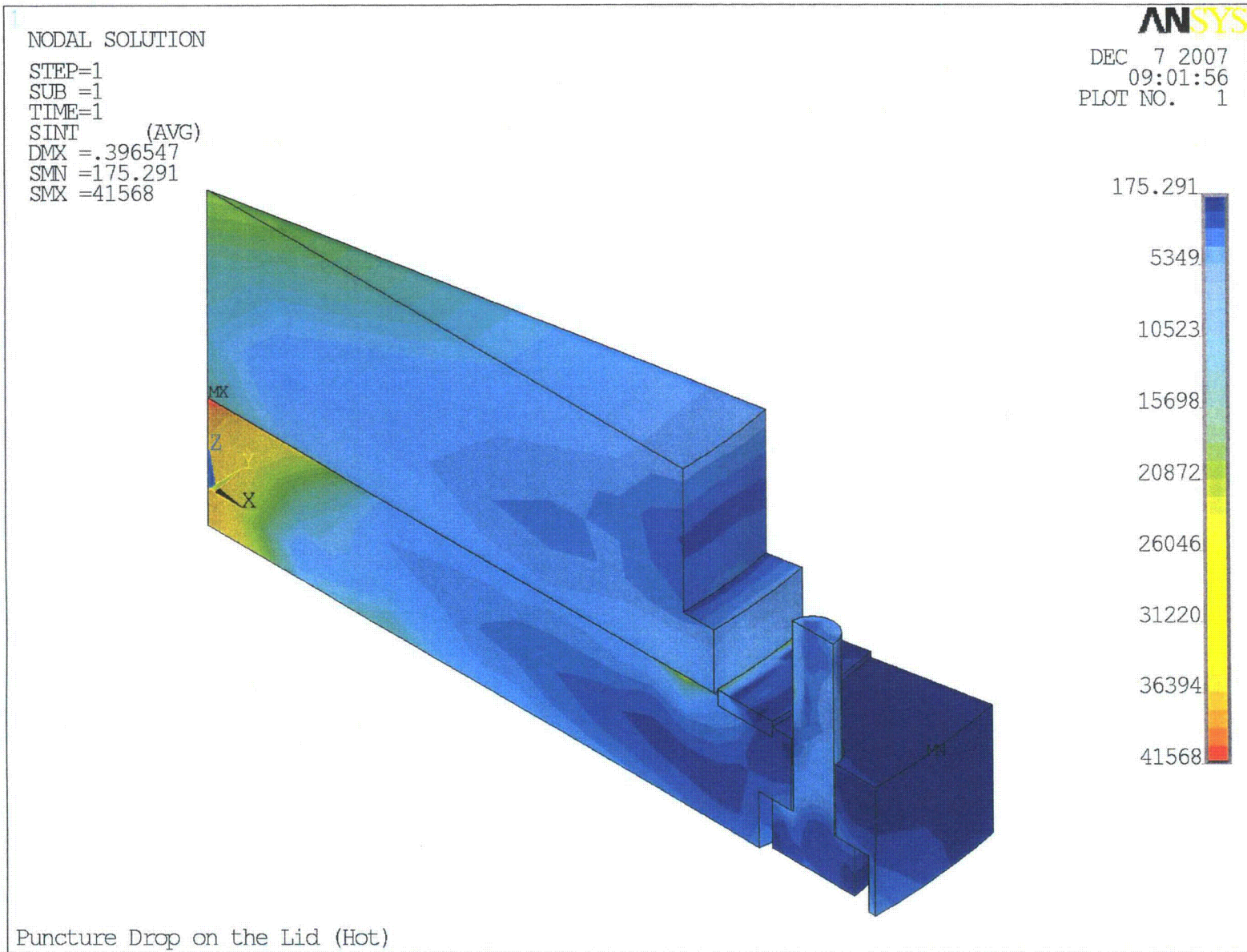
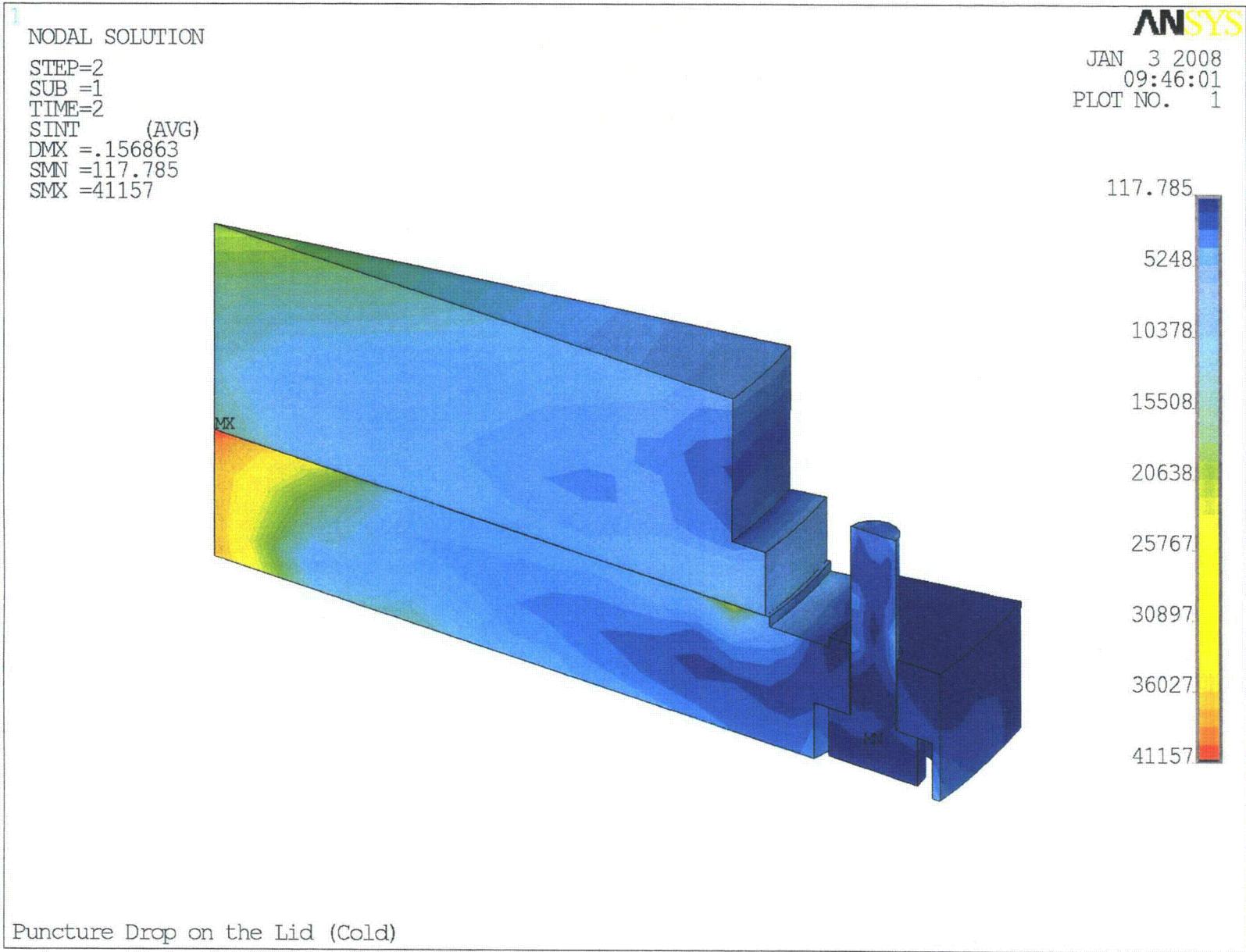


Figure 9  
 Maximum Stress Intensity in the Lid under Puncture Drop (Hot Conditions)





Title 3-60B Cask Analyses under Puncture Drop & Impact on Trunnions during HAC Testing  
 Calc. No. ST-505 (Figures) Rev. 1 Sheet 10 of 15

Figure 10  
 Maximum Stress Intensity in the Lid under Puncture Drop (Cold Conditions)

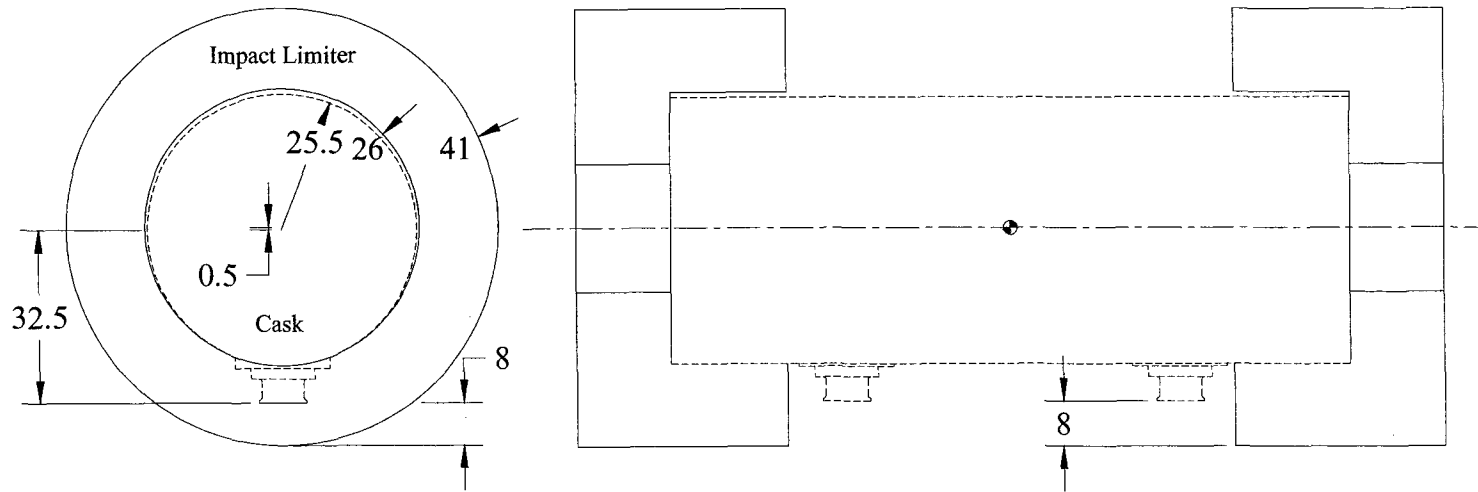


Figure 11  
Package Geometry with Trunnions in the Vertical Plane

30-FT SLAP DOWN-1 - HOT CONDITION

Time = 0.063

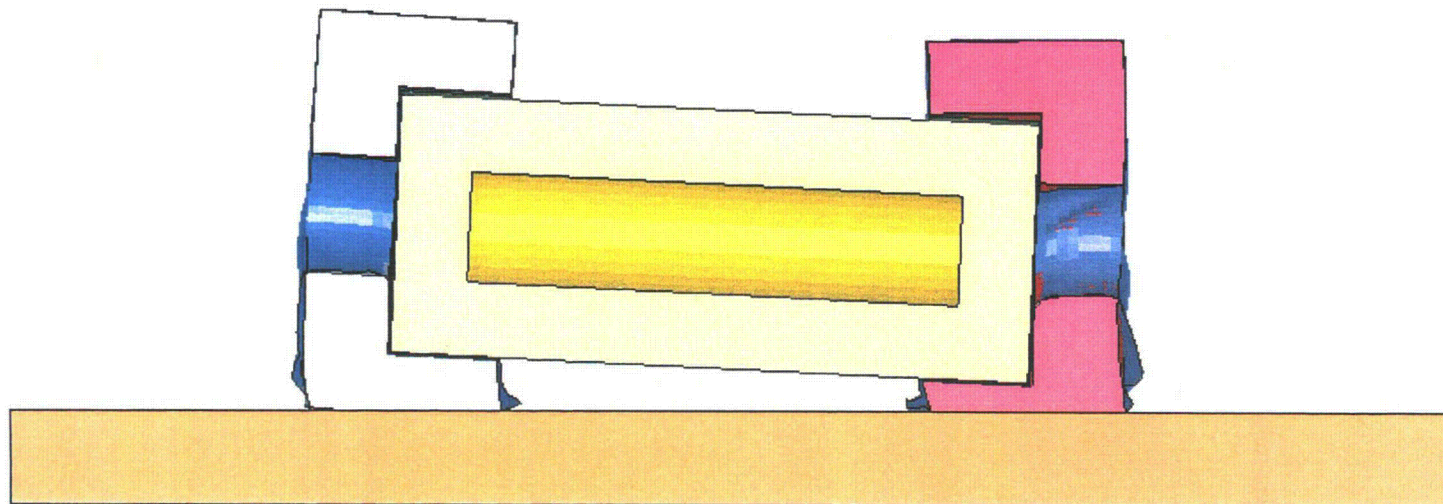


Figure 12  
Deformation of the Impact Limiters with 8" Foam Crush at the Tail End  
(Reference 8 Analysis)

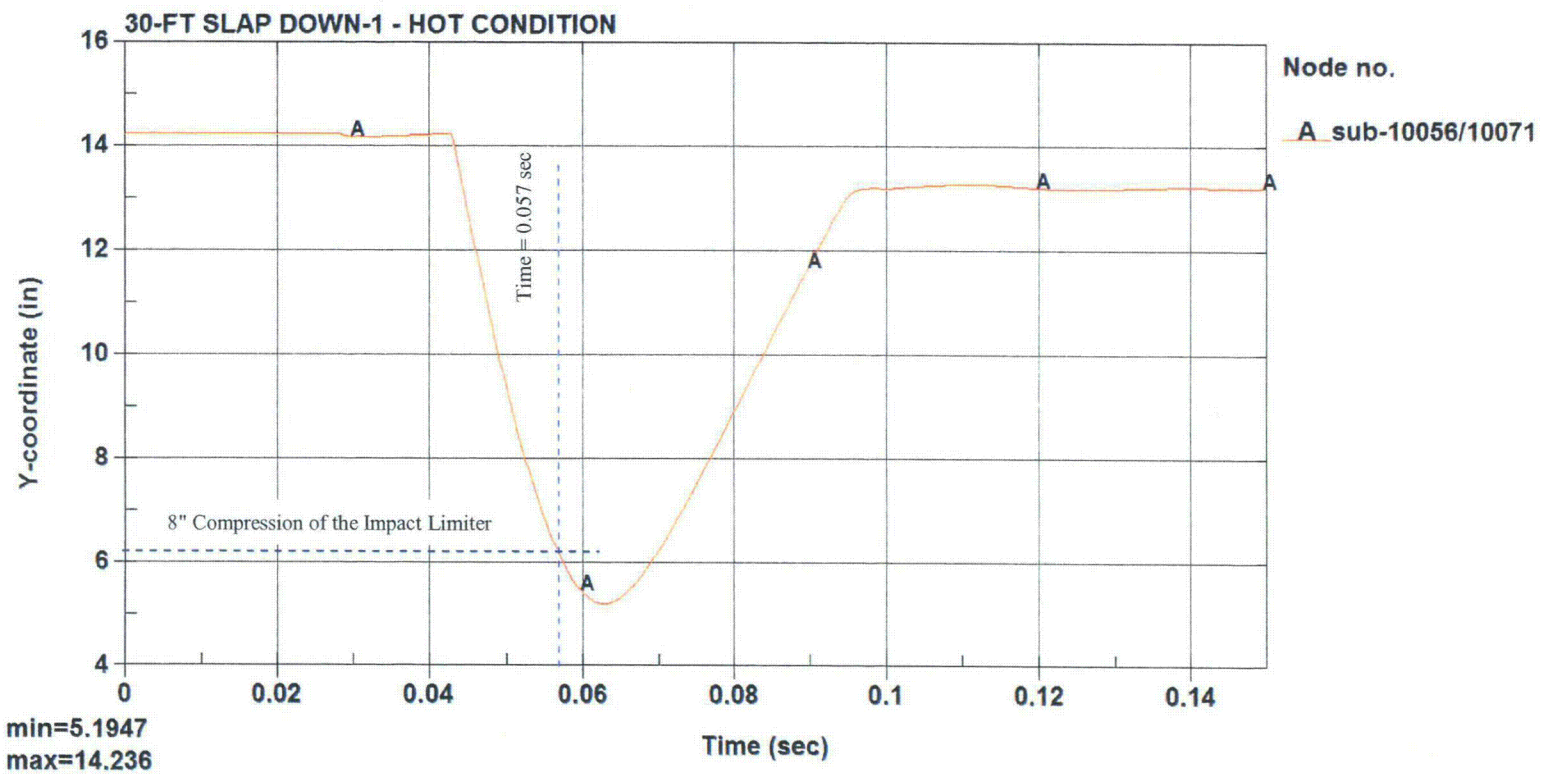


Figure 13  
Impact Limiter Deformation Time-History for Slapdown-1 in Hot Environment  
 (ST-557 Reference 8, Figure 95)



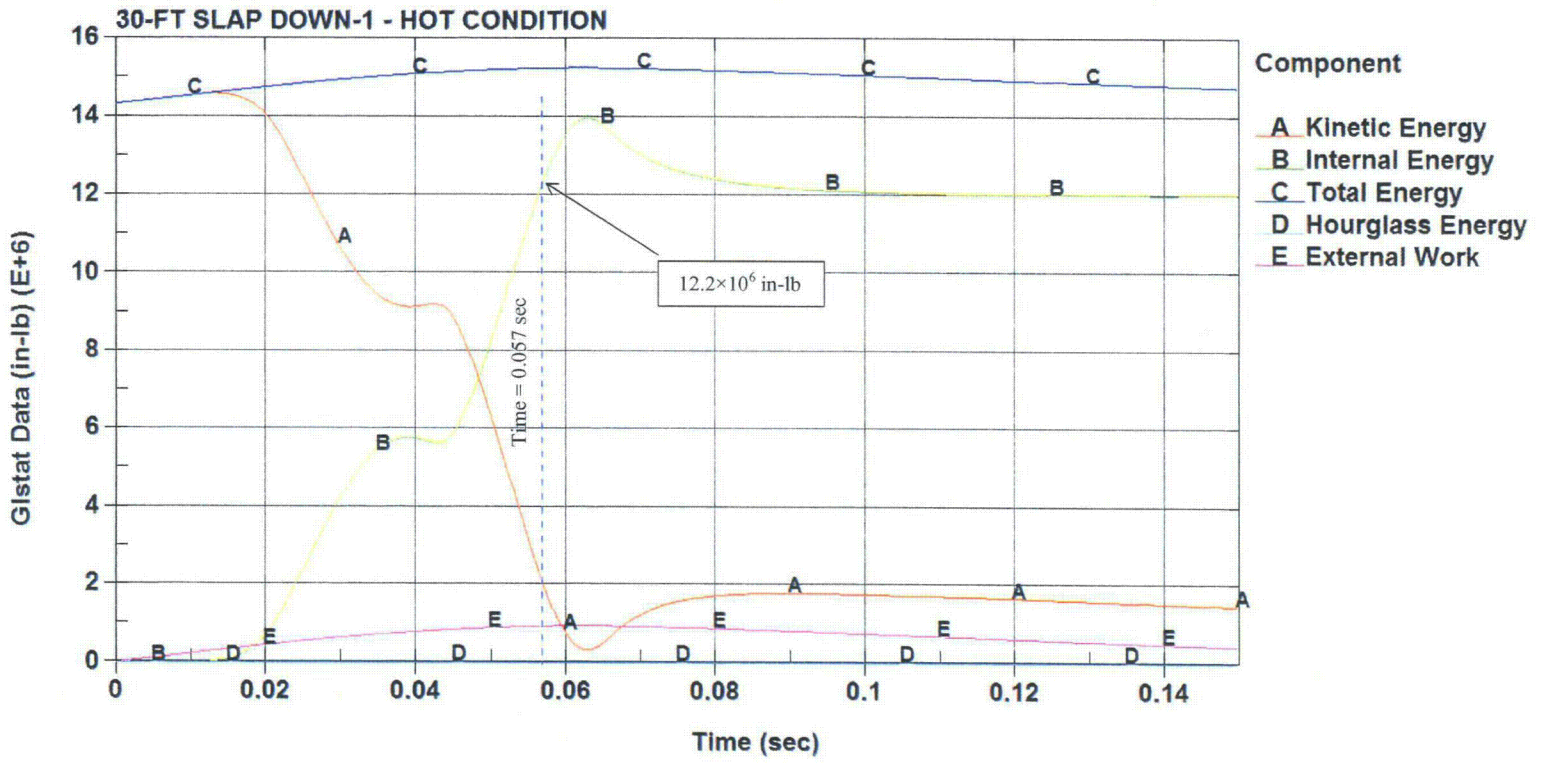
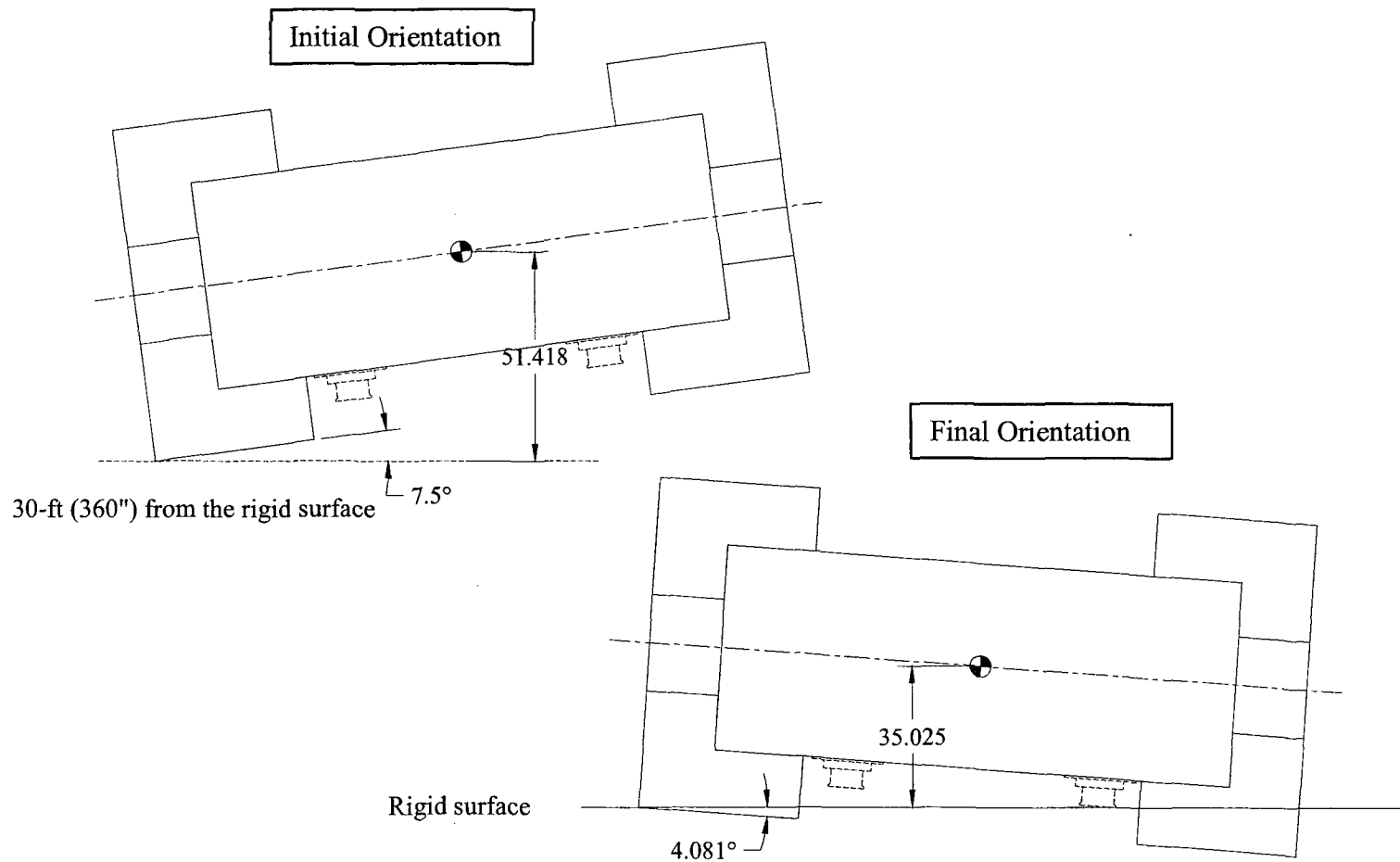


Figure 14  
Impact Limiter Internal Energy Time-History for Slapdown-1 in Hot Environment  
 (ST-557 Reference 8, Figure 92)



**Figure 15**  
C.G. Location of the Package Before and After the Slapdown-1 Drop Test



**Title** 3-60B Cask Analyses under Puncture Drop & Impact on Trunnions During HAC Testing

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**Sheet** 10 of 11

**Appendix 1**

Printout of the ANSYS Model Data

(18 Pages)

**ANSYS Model Sample Print-Out**

**Scenario 1: Puncture Drop on the Sidewall**

\*\*\*\*\* TITLES \*\*\*\*\*

\*\*\* YOU ARE IN ANSYS - ENGINEERING ANALYSIS SYSTEM \*\*\*  
 ANSYS Mechanical/Emag  
 RELEASE 11.0SP1 UPDATE 20070830 CUSTOMER 00222442

INITIAL JOBNAME = file  
 CURRENT JOBNAME = file

Current Working Directory: D:\Ansys Analyses\3-60B\Puncture Drop on Wall

TITLE= Puncture Drop on Cask Sidewall

MENULIST File: C:\Program Files\ANSYS Inc\v110\ANSYS\gui\en-us\UIDL\menulist110.ans

G L O B A L S T A T U S

ANSYS - Engineering Analysis System Jun 17, 2009 08:48  
 Release 11.0SP1 00222442 WINDOWS x64 Version

Current working directory: D:\Ansys Analyses\3-60B\Puncture Drop on Wall

MENULIST File: C:\Program Files\ANSYS Inc\v110\ANSYS\gui\en-us\UIDL\menulist110.ans

Product(s) enabled: ANSYS Mechanical/Emag

Total connect time. . . . . 0 hours : 1 minutes  
 Total CP usage. . . . . 0 hours 0 minutes 2.4 seconds

J O B I N F O R M A T I O N -----

Puncture Drop on Cask Sidewall

Current jobname . . . . .file  
 Initial jobname . . . . .file

Units . . . . .unknown

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Database space . . . . .	1048572.000 mb	29.115 mb ( 0.0%)

User menu file in use . . .C:\Program Files\ANSYS Inc\v110\ANSYS\gui\en-us\uidl\UIMENU.GRN  
 User menu file in use . . .C:\Program Files\ANSYS Inc\v110\ANSYS\gui\en-us\uidl\UIFUNC1.GRN  
 User menu file in use . . .C:\Program Files\ANSYS Inc\v110\ANSYS\gui\en-us\uidl\UIFUNC2.GRN  
 User menu file in use . . .C:\Program Files\ANSYS Inc\v110\ANSYS\gui\en-us\uidl\MECHTOOL.AUI  
 Beta features . . . . .are not shown in the user interface

M O D E L I N F O R M A T I O N -----

Solid model summary:

	Largest Number	Number Defined	Number Selected
Keypoints . . . . .	33	33	15

Lines . . . . .	47	47	22
Areas . . . . .	23	23	11
Volumes . . . . .	4	4	2

Finite element model summary:

	Largest Number	Number Defined	Number Selected
Nodes . . . . .	25932	18541	4725
Elements . . . . .	5250	5019	800
Element types . . . . .	9	9	n.a.
Real constant sets . . . . .	14	10	n.a.
Material property sets . . . . .	3	3	n.a.
Coupling . . . . .	0	0	n.a.
Constraint equations . . . . .	0	0	n.a.
Master DOFs . . . . .	0	0	n.a.
Dynamic gap conditions . . . . .	0	0	n.a.

BOUNDARY CONDITION INFORMATION -----

	Number Defined		
Constraints on nodes . . . . .	2123		
Constraints on keypoints . . . . .	0		
Constraints on lines . . . . .	0		
Constraints on areas . . . . .	0		
Forces on nodes . . . . .	0		
Forces on keypoints . . . . .	0		
Surface loads on elements . . . . .	27		
Number of element flagged surfaces . . . . .	0		
Surface loads on lines . . . . .	0		
Surface loads on areas . . . . .	0		
Body loads on elements . . . . .	0		
Body loads on nodes . . . . .	0		
Body loads on keypoints . . . . .	0		
Temperatures			
Uniform temperature . . . . .	0.000		
Reference temperature . . . . .	0.000		
Offset from absolute scale . . . . .	0.000		
	X	Y	Z
Linear acceleration . . . . .	0.0000	0.0000	0.0000
Angular velocity (about global CS) . . . . .	0.0000	0.0000	0.0000
Angular acceleration (about global CS) . . . . .	0.0000	0.0000	0.0000
Location of reference CS . . . . .	0.0000	0.0000	0.0000
Angular velocity (about reference CS) . . . . .	0.0000	0.0000	0.0000
Angular acceleration (about reference CS) . . . . .	0.0000	0.0000	0.0000

ROUTINE INFORMATION -----

Current routine . . . . . None (BEGIN level)

Active coordinate system . . . . . 1 (Cylindrical)

Display coordinate system . . . . . 0 (Cartesian)

Analysis type . . . . . Static (steady-state)

Active options for this analysis type:  
 Large deformation effects . . . . .Not included  
 Plasticity. . . . .Included  
 Creep . . . . .Not included  
 Equation solver to use. . . . .Sparse

Results file . . . . .file.rst

Load step number . . . . . 13

Number of substeps:  
 Starting number of substeps . . . . . 10  
 Maximum number of substeps. . . . . 100  
 Minimum number of substeps. . . . . 1  
 Step change boundary conditions . .No

S O L U T I O N O P T I O N S

PROBLEM DIMENSIONALITY. . . . .3-D  
 DEGREES OF FREEDOM. . . . . UX UY UZ  
 ANALYSIS TYPE . . . . .STATIC (STEADY-STATE)  
 EQUATION SOLVER OPTION. . . . .SPARSE  
 PLASTIC MATERIAL PROPERTIES INCLUDED. . . . .YES  
 NEWTON-RAPHSON OPTION . . . . .PROGRAM CHOSEN  
 GLOBALLY ASSEMBLED MATRIX . . . . .SYMMETRIC

L O A D S T E P O P T I O N S

LOAD STEP NUMBER. . . . . 13  
 TIME AT END OF THE LOAD STEP. . . . . 16.000  
 AUTOMATIC TIME STEPPING . . . . . ON  
 INITIAL NUMBER OF SUBSTEPS . . . . . 10  
 MAXIMUM NUMBER OF SUBSTEPS . . . . . 100  
 MINIMUM NUMBER OF SUBSTEPS . . . . . 1  
 MAXIMUM NUMBER OF EQUILIBRIUM ITERATIONS. . . . . 15  
 STEP CHANGE BOUNDARY CONDITIONS . . . . . NO  
 TERMINATE ANALYSIS IF NOT CONVERGED . . . . .YES (EXIT)  
 CONVERGENCE CONTROLS. . . . .USE DEFAULTS  
 COPY INTEGRATION POINT VALUES TO NODE . . . . .YES, FOR ELEMENTS WITH  
 ACTIVE MAT. NONLINEARITIES  
 PRINT OUTPUT CONTROLS . . . . .NO PRINTOUT  
 DATABASE OUTPUT CONTROLS  
 ITEM FREQUENCY COMPONENT  
 ALL ALL

LIST ELEMENT TYPES FROM 1 TO 9 BY 1

\*\*\*\*\* ANSYS - ENGINEERING ANALYSIS SYSTEM RELEASE 11.0SP1 \*\*\*\*\*  
 ANSYS Mechanical/Emag  
 00222442 VERSION=WINDOWS x64 08:48:42 JUN 17, 2009 CP= 2.406

Puncture Drop on Cask Sidewall

ELEMENT TYPE 1 IS SOLID186 3-D 20-NODE STRUCTURAL SOLID INOPR  
 KEYOPT(1-12)= 0 0 0 0 0 0 0 0 0 0 0 0  
 ELEMENT TYPE 2 IS TARGE170 3-D TARGET SEGMENT INOPR  
 KEYOPT(1-12)= 0 0 0 0 0 0 0 0 0 0 0 0  
 ELEMENT TYPE 3 IS CONTA174 3D 8-NODE SURF-SURF CONTACT INOPR

```

KEYOPT(1-12) = 0 0 0 0 1 0 0 0 0 1 0 0 0
ELEMENT TYPE 4 IS TARGE170 3-D TARGET SEGMENT INOPR
KEYOPT(1-12) = 0 0 0 0 0 0 0 0 0 0 0 0 0
ELEMENT TYPE 5 IS CONTA174 3D 8-NODE SURF-SURF CONTACT INOPR
KEYOPT(1-12) = 0 0 0 0 1 0 0 0 0 1 0 0 0
ELEMENT TYPE 6 IS TARGE170 3-D TARGET SEGMENT INOPR
KEYOPT(1-12) = 0 0 0 0 0 0 0 0 0 0 0 0 0
ELEMENT TYPE 7 IS CONTA174 3D 8-NODE SURF-SURF CONTACT INOPR
KEYOPT(1-12) = 0 0 0 0 1 0 0 0 0 1 0 0 0
ELEMENT TYPE 8 IS TARGE170 3-D TARGET SEGMENT INOPR
KEYOPT(1-12) = 0 0 0 0 0 0 0 0 0 0 0 0 0
ELEMENT TYPE 9 IS CONTA174 3D 8-NODE SURF-SURF CONTACT INOPR
KEYOPT(1-12) = 0 0 0 0 1 0 0 0 1 1 0 0 0

```

```

CURRENT NODAL DOF SET IS UX UY UZ
THREE-DIMENSIONAL MODEL

```

```

LIST REAL SETS 1 TO 14 BY 1

```

```

REAL CONSTANT SET 3 ITEMS 1 TO 6
0.0000 0.0000 1.0000 0.10000 0.0000 0.0000
REAL CONSTANT SET 3 ITEMS 7 TO 12
0.0000 0.0000 0.10000E+21 0.0000 1.0000 0.0000
REAL CONSTANT SET 3 ITEMS 13 TO 18
0.0000 0.0000 1.0000 0.0000 1.0000 0.50000
REAL CONSTANT SET 3 ITEMS 19 TO 24
0.0000 1.0000 1.0000 0.0000 0.0000 1.0000
REAL CONSTANT SET 4 ITEMS 1 TO 6
0.0000 0.0000 1.0000 0.10000 0.0000 0.0000
REAL CONSTANT SET 4 ITEMS 7 TO 12
0.0000 0.0000 0.10000E+21 0.0000 1.0000 0.0000
REAL CONSTANT SET 4 ITEMS 13 TO 18
0.0000 0.0000 1.0000 0.0000 1.0000 0.50000
REAL CONSTANT SET 4 ITEMS 19 TO 24
0.0000 1.0000 1.0000 0.0000 0.0000 1.0000
REAL CONSTANT SET 5 ITEMS 1 TO 6
0.0000 0.0000 1.0000 0.10000 0.0000 0.0000
REAL CONSTANT SET 5 ITEMS 7 TO 12
0.0000 0.0000 0.10000E+21 0.0000 1.0000 0.0000
REAL CONSTANT SET 5 ITEMS 13 TO 18
0.0000 0.0000 1.0000 0.0000 1.0000 0.50000
REAL CONSTANT SET 5 ITEMS 19 TO 24
0.0000 1.0000 1.0000 0.0000 0.0000 1.0000
REAL CONSTANT SET 6 ITEMS 1 TO 6
0.0000 0.0000 1.0000 0.10000 0.0000 0.0000

```

REAL CONSTANT SET	6	ITEMS 7 TO 12	0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000
REAL CONSTANT SET	6	ITEMS 13 TO 18	0.0000	0.0000	1.0000	0.0000	1.0000	0.50000
REAL CONSTANT SET	6	ITEMS 19 TO 24	0.0000	1.0000	1.0000	0.0000	0.0000	1.0000
REAL CONSTANT SET	7	ITEMS 1 TO 6	0.0000	0.0000	1.0000	0.10000	0.0000	0.0000
REAL CONSTANT SET	7	ITEMS 7 TO 12	0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000
REAL CONSTANT SET	7	ITEMS 13 TO 18	0.0000	0.0000	1.0000	0.0000	1.0000	0.50000
REAL CONSTANT SET	7	ITEMS 19 TO 24	0.0000	1.0000	1.0000	0.0000	0.0000	1.0000
REAL CONSTANT SET	8	ITEMS 1 TO 6	0.0000	0.0000	1.0000	0.10000	0.0000	0.0000
REAL CONSTANT SET	8	ITEMS 7 TO 12	0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000
REAL CONSTANT SET	8	ITEMS 13 TO 18	0.0000	0.0000	1.0000	0.0000	1.0000	0.50000
REAL CONSTANT SET	8	ITEMS 19 TO 24	0.0000	1.0000	1.0000	0.0000	0.0000	1.0000
REAL CONSTANT SET	11	ITEMS 1 TO 6	0.0000	0.0000	1.0000	0.10000	0.0000	0.0000
REAL CONSTANT SET	11	ITEMS 7 TO 12	0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000
REAL CONSTANT SET	11	ITEMS 13 TO 18	0.0000	0.0000	1.0000	0.0000	1.0000	0.50000
REAL CONSTANT SET	11	ITEMS 19 TO 24	0.0000	1.0000	1.0000	0.0000	0.0000	1.0000
REAL CONSTANT SET	12	ITEMS 1 TO 6	0.0000	0.0000	1.0000	0.10000	0.0000	0.0000
REAL CONSTANT SET	12	ITEMS 7 TO 12	0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000
REAL CONSTANT SET	12	ITEMS 13 TO 18	0.0000	0.0000	1.0000	0.0000	1.0000	0.50000
REAL CONSTANT SET	12	ITEMS 19 TO 24	0.0000	1.0000	1.0000	0.0000	0.0000	1.0000
REAL CONSTANT SET	13	ITEMS 1 TO 6	0.0000	0.0000	1.0000	0.10000	0.0000	0.0000
REAL CONSTANT SET	13	ITEMS 7 TO 12	0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000

```

REAL CONSTANT SET      13  ITEMS 13 TO 18
  0.0000    0.0000    1.0000    0.0000    1.0000    0.50000

REAL CONSTANT SET      13  ITEMS 19 TO 24
  0.0000    1.0000    1.0000    0.0000    0.0000    1.0000

REAL CONSTANT SET      14  ITEMS  1 TO  6
  0.0000    0.0000    1.0000    0.10000    0.0000    0.0000

REAL CONSTANT SET      14  ITEMS  7 TO 12
  0.0000    0.0000    0.10000E+21  0.0000    1.0000    0.0000

REAL CONSTANT SET      14  ITEMS 13 TO 18
  0.0000    0.0000    1.0000    0.0000    1.0000    0.50000

REAL CONSTANT SET      14  ITEMS 19 TO 24
  0.0000    1.0000    1.0000    0.0000    0.0000    1.0000
    
```

```

LIST MATERIALS      1 TO      3 BY      1
PROPERTY= ALL
    
```

```

PROPERTY TABLE EX      MAT=      1  NUM. POINTS= 6
  TEMPERATURE      DATA      TEMPERATURE      DATA      TEMPERATURE      DATA
  70.000    0.28300E+08    100.00    0.28100E+08    200.00    0.27600E+08
  300.00    0.27000E+08    400.00    0.26500E+08    500.00    0.25800E+08
    
```

```

PROPERTY TABLE NUXY MAT=      1  NUM. POINTS= 6
  TEMPERATURE      DATA      TEMPERATURE      DATA      TEMPERATURE      DATA
  70.000    0.30000    100.00    0.30000    200.00    0.30000
  300.00    0.30000    400.00    0.30000    500.00    0.30000
    
```

```

PROPERTY TABLE ALPX MAT=      1  NUM. POINTS= 6  REFERENCE TEMP. = 0.00
  TEMPERATURE      DATA      TEMPERATURE      DATA      TEMPERATURE      DATA
  70.000    0.85000E-05    100.00    0.86000E-05    200.00    0.89000E-05
  300.00    0.92000E-05    400.00    0.95000E-05    500.00    0.97000E-05
    
```

```

PROPERTY TABLE DENS MAT=      1  NUM. POINTS= 1
  TEMPERATURE      DATA      TEMPERATURE      DATA      TEMPERATURE      DATA
  0.0000    0.28300
    
```

```

PROPERTY TABLE MU      MAT=      1  NUM. POINTS= 1
  TEMPERATURE      DATA      TEMPERATURE      DATA      TEMPERATURE      DATA
  0.0000    0.0000
    
```

```

PROPERTY TABLE EMIS MAT=      1  NUM. POINTS= 1
  TEMPERATURE      DATA      TEMPERATURE      DATA      TEMPERATURE      DATA
  0.0000    0.78886E-30
    
```

```

PROPERTY TABLE EX      MAT=      2  NUM. POINTS= 6
  TEMPERATURE      DATA      TEMPERATURE      DATA      TEMPERATURE      DATA
  70.000    0.29900E+08    100.00    0.29900E+08    200.00    0.29900E+08
  300.00    0.29900E+08    400.00    0.29900E+08    500.00    0.29900E+08
    
```

```

PROPERTY TABLE NUXY MAT=      2  NUM. POINTS= 6
  TEMPERATURE      DATA      TEMPERATURE      DATA      TEMPERATURE      DATA
  70.000    0.30000    100.00    0.30000    200.00    0.30000
  300.00    0.30000    400.00    0.30000    500.00    0.30000
    
```

```

PROPERTY TABLE ALPX MAT=      2  NUM. POINTS= 6  REFERENCE TEMP. = 0.00
  TEMPERATURE      DATA      TEMPERATURE      DATA      TEMPERATURE      DATA
  70.000    0.65000E-05    100.00    0.65000E-05    200.00    0.65000E-05
  300.00    0.65000E-05    400.00    0.65000E-05    500.00    0.65000E-05
    
```

PROPERTY TABLE DENS MAT= 2 NUM. POINTS= 1  
 TEMPERATURE DATA TEMPERATURE DATA TEMPERATURE DATA  
 0.0000 0.28300

PROPERTY TABLE EX MAT= 3 NUM. POINTS= 8  
 TEMPERATURE DATA TEMPERATURE DATA TEMPERATURE DATA  
 -40.000 0.24600E+07 -20.000 0.24300E+07 70.000 0.22700E+07  
 100.00 0.22100E+07 200.00 0.20100E+07 300.00 0.18500E+07  
 400.00 0.17000E+07 500.00 0.15200E+07

PROPERTY TABLE NUXY MAT= 3 NUM. POINTS= 6  
 TEMPERATURE DATA TEMPERATURE DATA TEMPERATURE DATA  
 81.000 0.40000 212.00 0.40000 302.00 0.40000  
 392.00 0.40000 513.00 0.40000 621.00 0.40000

PROPERTY TABLE ALPX MAT= 3 NUM. POINTS= 8 REFERENCE TEMP. = 0.00  
 TEMPERATURE DATA TEMPERATURE DATA TEMPERATURE DATA  
 -40.000 0.15560E-04 -20.000 0.15650E-04 70.000 0.16060E-04  
 100.00 0.16220E-04 200.00 0.16700E-04 300.00 0.17330E-04  
 400.00 0.18160E-04 500.00 0.19120E-04

PROPERTY TABLE DENS MAT= 3 NUM. POINTS= 1  
 TEMPERATURE DATA TEMPERATURE DATA TEMPERATURE DATA  
 0.0000 0.41000

LIST DATA TABLE ALL FOR ALL MATERIALS

BiKin Pl (BKIN) Table For Material 1

1  
 Temps 0.0000  
 Yld Strs 25000.  
 Tang Mod 0.13406E+06

BiKin Pl (BKIN) Table For Material 3

1  
 Temps 0.0000  
 Yld Strs 4300.0  
 Tang Mod 4200.0

LIST NODAL SURFACE LOAD PRES FOR ALL SELECTED NODES



**Scenario 2: Puncture Drop on the Lid**

\*\*\*\*\* TITLES \*\*\*\*\*

\*\*\* YOU ARE IN ANSYS - ENGINEERING ANALYSIS SYSTEM \*\*\*  
 ANSYS Mechanical/Emag  
 RELEASE 11.0SP1 UPDATE 20070830 CUSTOMER 00222442

INITIAL JOBNAME = file  
 CURRENT JOBNAME = file

Current Working Directory: G:\3-60B Rev 2\Puncture

TITLE= Puncture Drop on the Lid (Hot)

MENULIST File: C:\Program Files\ANSYS Inc\v110\ANSYS\gui\en-us\UIDL\menulist110.ans

G L O B A L S T A T U S

ANSYS - Engineering Analysis System Dec 07, 2007 10:10  
 Release 11.0SP1 00222442 INTEL NT Version

Current working directory: G:\3-60B Rev 2\Puncture

MENULIST File: C:\Program Files\ANSYS Inc\v110\ANSYS\gui\en-us\UIDL\menulist110.ans

Product(s) enabled: ANSYS Mechanical/Emag

Total connect time. . . . . 0 hours 1 minutes  
 Total CP usage. . . . . 0 hours 0 minutes 2.3 seconds

J O B I N F O R M A T I O N -----

Puncture Drop on the Lid (Hot)

Current jobname . . . . .file  
 Initial jobname . . . . .file

Units . . . . .unknown

	Available	Used
Scratch Memory Space. . . . .	256.000 mb	4.598 mb ( 1.8%)
Database space . . . . .	65535.750 mb	8.777 mb ( 0.0%)

User menu file in use . . .C:\Program Files\ANSYS Inc\v110\ANSYS\gui\en-us\uidl\UIMENU.GRN  
 User menu file in use . . .C:\Program Files\ANSYS Inc\v110\ANSYS\gui\en-us\uidl\UIFUNC1.GRN  
 User menu file in use . . .C:\Program Files\ANSYS Inc\v110\ANSYS\gui\en-us\uidl\UIFUNC2.GRN  
 User menu file in use . . .C:\Program Files\ANSYS Inc\v110\ANSYS\gui\en-us\uidl\MECHTOOL.AUI  
 Beta features . . . . .are not shown in the user interface

M O D E L I N F O R M A T I O N -----

Solid model summary:

	Largest Number	Number Defined	Number Selected
Keypoints . . . . .	0	0	0
Lines . . . . .	0	0	0
Areas . . . . .	0	0	0
Volumes . . . . .	0	0	0

Finite element model summary:

	Largest Number	Number Defined	Number Selected
Nodes . . . . .	3001	2879	2878
Elements. . . . .	3946	2369	1522
Element types . . . . .	71	36	n.a.
Real constant sets. . . . .	71	29	n.a.
Material property sets. . . . .	3	3	n.a.
Coupling. . . . .	82	30	n.a.
Constraint equations. . . . .	0	0	n.a.
Master DOFs . . . . .	0	0	n.a.
Dynamic gap conditions. . . . .	0	0	n.a.

BOUNDARY CONDITION INFORMATION -----

	Number Defined	X	Y	Z
Constraints on nodes. . . . .	1196			
Constraints on keypoints. . . . .	0			
Constraints on lines. . . . .	0			
Constraints on areas. . . . .	0			
Forces on nodes . . . . .	0			
Forces on keypoints . . . . .	0			
Surface loads on elements . . . . .	1			
Number of element flagged surfaces . . . . .	0			
Surface loads on lines. . . . .	0			
Surface loads on areas. . . . .	0			
Body loads on elements. . . . .	0			
Body loads on nodes . . . . .	2878			
Body loads on keypoints . . . . .	0			
Temperatures				
Uniform temperature. . . . .	-20.000			
Reference temperature. . . . .	70.000			
Offset from absolute scale . . . . .	460.000			
Linear acceleration . . . . .	0.0000	0.0000	0.0000	22.390
Angular velocity (about global CS). . . . .	0.0000	0.0000	0.0000	0.0000
Angular acceleration (about global CS). . . . .	0.0000	0.0000	0.0000	0.0000
Location of reference CS. . . . .	0.0000	0.0000	0.0000	0.0000
Angular velocity (about reference CS) . . . . .	0.0000	0.0000	0.0000	0.0000
Angular acceleration (about reference CS) . . . . .	0.0000	0.0000	0.0000	0.0000

ROUTINE INFORMATION -----

Current routine. . . . .	Preprocessing (PREP7)
Active coordinate system . . . . .	1 (Cylindrical)
Display coordinate system. . . . .	0 (Cartesian)
Current element attributes:	
Type number . . . . .	71 (COMBIN14)
Real number . . . . .	71
Material number . . . . .	1

```

Element coordinate system number. . . . . 0

Current mesher type. . . . .based on default element shape

Current element meshing shape 2D . . .use default element shape.

Current element meshing shape 3D . . .use default element shape.

SmrtSize Level . . . . . OFF

Global element size. . . . . 0 divisions per line

Active coordinate system . . . . . 1 (Cylindrical)

Display coordinate system. . . . . 0 (Cartesian)

Analysis type. . . . .Static (steady-state)

Active options for this analysis type:
  Large deformation effects . . . .Not included
  Plasticity. . . . .Not included
  Creep . . . . .Not included
  Equation solver to use. . . . .Program Chosen

Results file . . . . .file.rst

Load step number . . . . . 2

Number of substeps . . . . . 1
  Step change boundary conditions . .No
  
```

S O L U T I O N O P T I O N S

```

PROBLEM DIMENSIONALITY. . . . .3-D
DEGREES OF FREEDOM. . . . . UX  UY  UZ  TEMP
ANALYSIS TYPE . . . . .STATIC (STEADY-STATE)
OFFSET TEMPERATURE FROM ABSOLUTE ZERO . . . . 460.00
NEWTON-RAPHSON OPTION . . . . .PROGRAM CHOSEN
GLOBALLY ASSEMBLED MATRIX . . . . .SYMMETRIC
  
```

L O A D S T E P O P T I O N S

```

LOAD STEP NUMBER. . . . . 2
TIME AT END OF THE LOAD STEP. . . . . 3.0000
NUMBER OF SUBSTEPS. . . . . 1
MAXIMUM NUMBER OF EQUILIBRIUM ITERATIONS. . . . 15
STEP CHANGE BOUNDARY CONDITIONS . . . . . NO
TERMINATE ANALYSIS IF NOT CONVERGED . . . . .YES (EXIT)
CONVERGENCE CONTROLS
  LABEL  REFERENCE  TOLERANCE  NORM  MINREF
  F      0.1000    0.1000E-02  2     -1.000
INERTIA LOADS
  ACEL . . . . . 0.0000    0.0000    22.390
PRINT OUTPUT CONTROLS . . . . .NO PRINTOUT
DATABASE OUTPUT CONTROLS
  ITEM  FREQUENCY  COMPONENT
  BASI  ALL
  
```

LIST ELEMENT TYPES FROM 1 TO 71 BY 1

```

ELEMENT TYPE      1 IS SOLID185      3-D 8-NODE STRUCTURAL SOLID  INOPR
KEYOPT(1-12)=    0 0 0 0 0 0 0 0 0 0 0 0
  
```



ELEMENT TYPE	54	IS	CONTA175		NODE-TO-SURFACE CONTACT		INOPR
KEYOPT(1-12) =	0	2	0	0	3	0	0
						0	0
						1	2
						0	5
							0
ELEMENT TYPE	57	IS	TARGE170		3-D TARGET SEGMENT		INOPR
KEYOPT(1-12) =	0	0	0	0	0	0	0
						0	0
						0	0
						0	0
						0	0
						0	0
ELEMENT TYPE	58	IS	CONTA174		3D 8-NODE SURF-SURF CONTACT		INOPR
KEYOPT(1-12) =	0	0	0	2	3	0	0
						0	0
						1	2
						0	1
							0
							0
ELEMENT TYPE	61	IS	TARGE170		3-D TARGET SEGMENT		INOPR
KEYOPT(1-12) =	0	0	0	0	0	0	0
						0	0
						0	0
						0	0
						0	0
ELEMENT TYPE	62	IS	CONTA174		3D 8-NODE SURF-SURF CONTACT		INOPR
KEYOPT(1-12) =	0	0	0	2	3	0	0
						0	0
						1	2
						0	0
							0
							0
ELEMENT TYPE	63	IS	TARGE170		3-D TARGET SEGMENT		INOPR
KEYOPT(1-12) =	0	0	0	0	0	0	0
						0	0
						0	0
						0	0
						0	0
ELEMENT TYPE	64	IS	CONTA174		3D 8-NODE SURF-SURF CONTACT		INOPR
KEYOPT(1-12) =	0	0	0	0	3	0	0
						0	0
						1	2
						0	0
							0
							0
ELEMENT TYPE	65	IS	TARGE170		3-D TARGET SEGMENT		INOPR
KEYOPT(1-12) =	0	0	0	0	0	0	0
						0	0
						0	0
						0	0
						0	0
ELEMENT TYPE	66	IS	CONTA175		NODE-TO-SURFACE CONTACT		INOPR
KEYOPT(1-12) =	0	0	0	0	3	0	0
						0	0
						1	2
						0	0
							0
							0
ELEMENT TYPE	67	IS	TARGE170		3-D TARGET SEGMENT		INOPR
KEYOPT(1-12) =	0	0	0	0	0	0	0
						0	0
						0	0
						0	0
						0	0
ELEMENT TYPE	68	IS	CONTA175		NODE-TO-SURFACE CONTACT		INOPR
KEYOPT(1-12) =	0	0	0	0	3	0	0
						0	0
						1	2
						0	0
							0
							0
ELEMENT TYPE	69	IS	TARGE170		3-D TARGET SEGMENT		INOPR
KEYOPT(1-12) =	0	0	0	0	0	0	0
						0	0
						0	0
						0	0
						0	0
ELEMENT TYPE	70	IS	CONTA175		NODE-TO-SURFACE CONTACT		INOPR
KEYOPT(1-12) =	0	0	0	0	3	0	0
						0	0
						1	2
						0	0
							0
							0
ELEMENT TYPE	71	IS	COMBIN14		SPRING-DAMPER		INOPR
KEYOPT(1-12) =	0	3	0	0	0	0	0
						0	0
						0	0
						0	0
						0	0

CURRENT NODAL DOF SET IS UX UY UZ TEMP  
THREE-DIMENSIONAL MODEL

LIST REAL SETS 1 TO 71 BY 1

REAL CONSTANT SET	23	ITEMS	1 TO	6		
1.0000	0.33056E-14	0.0000	0.0000	0.0000	0.0000	0.0000
REAL CONSTANT SET	24	ITEMS	1 TO	6		
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
REAL CONSTANT SET	24	ITEMS	7 TO	12		
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
REAL CONSTANT SET	24	ITEMS	13 TO	13		
0.33300						
REAL CONSTANT SET	27	ITEMS	1 TO	6		
1.0000	0.33056E-14	0.0000	0.0000	0.0000	0.0000	0.0000

REAL CONSTANT SET	28	ITEMS 1 TO	6			
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
REAL CONSTANT SET	28	ITEMS 7 TO	12			
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
REAL CONSTANT SET	28	ITEMS 13 TO	13			
0.33300						
REAL CONSTANT SET	32	ITEMS 1 TO	6			
0.0000	0.0000	1.0000	0.10000	0.0000	0.0000	0.0000
REAL CONSTANT SET	32	ITEMS 7 TO	12			
0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000	0.0000
REAL CONSTANT SET	32	ITEMS 13 TO	18			
0.0000	0.0000	1.0000	0.0000	1.0000	0.50000	
REAL CONSTANT SET	32	ITEMS 19 TO	24			
0.0000	1.0000	1.0000	0.0000	0.0000	1.0000	
REAL CONSTANT SET	33	ITEMS 1 TO	6			
0.0000	0.0000	1.0000	0.10000	0.0000	0.0000	0.0000
REAL CONSTANT SET	33	ITEMS 7 TO	12			
0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000	0.0000
REAL CONSTANT SET	33	ITEMS 13 TO	18			
0.0000	0.0000	1.0000	0.0000	1.0000	0.50000	
REAL CONSTANT SET	33	ITEMS 19 TO	24			
0.0000	1.0000	1.0000	0.0000	0.0000	1.0000	
REAL CONSTANT SET	34	ITEMS 1 TO	6			
0.0000	0.0000	1.0000	0.10000	0.0000	0.0000	0.0000
REAL CONSTANT SET	34	ITEMS 7 TO	12			
0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000	0.0000
REAL CONSTANT SET	34	ITEMS 13 TO	18			
0.0000	0.0000	1.0000	0.0000	1.0000	0.50000	
REAL CONSTANT SET	34	ITEMS 19 TO	24			
0.0000	1.0000	1.0000	0.0000	0.0000	1.0000	
REAL CONSTANT SET	35	ITEMS 1 TO	6			
0.0000	0.0000	1.0000	0.10000	0.0000	0.0000	0.0000
REAL CONSTANT SET	35	ITEMS 7 TO	12			
0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000	0.0000
REAL CONSTANT SET	35	ITEMS 13 TO	18			
0.0000	0.0000	1.0000	0.0000	1.0000	0.50000	
REAL CONSTANT SET	35	ITEMS 19 TO	24			
0.0000	1.0000	1.0000	0.0000	0.0000	1.0000	
REAL CONSTANT SET	36	ITEMS 1 TO	6			
0.0000	0.0000	1.0000	0.10000	0.0000	0.0000	0.0000
REAL CONSTANT SET	36	ITEMS 7 TO	12			
0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000	0.0000

REAL CONSTANT SET	36	ITEMS 13 TO 18	0.0000	0.0000	1.0000	0.0000	1.0000	0.50000
REAL CONSTANT SET	36	ITEMS 19 TO 24	0.0000	1.0000	1.0000	0.0000	0.0000	1.0000
REAL CONSTANT SET	37	ITEMS 1 TO 6	0.0000	0.0000	1.0000	0.10000	0.0000	0.0000
REAL CONSTANT SET	37	ITEMS 7 TO 12	0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000
REAL CONSTANT SET	37	ITEMS 13 TO 18	0.0000	0.0000	1.0000	0.0000	1.0000	0.50000
REAL CONSTANT SET	37	ITEMS 19 TO 24	0.0000	1.0000	1.0000	0.0000	0.0000	1.0000
REAL CONSTANT SET	38	ITEMS 1 TO 6	0.0000	0.0000	1.0000	0.10000	0.0000	0.0000
REAL CONSTANT SET	38	ITEMS 7 TO 12	0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000
REAL CONSTANT SET	38	ITEMS 13 TO 18	0.0000	0.0000	1.0000	0.0000	1.0000	0.50000
REAL CONSTANT SET	38	ITEMS 19 TO 24	0.0000	1.0000	1.0000	0.0000	0.0000	1.0000
REAL CONSTANT SET	39	ITEMS 1 TO 6	0.0000	0.0000	1.0000	0.10000	0.0000	0.0000
REAL CONSTANT SET	39	ITEMS 7 TO 12	0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000
REAL CONSTANT SET	39	ITEMS 13 TO 18	0.0000	0.0000	1.0000	0.0000	1.0000	0.50000
REAL CONSTANT SET	39	ITEMS 19 TO 24	0.0000	1.0000	1.0000	0.0000	0.0000	1.0000
REAL CONSTANT SET	40	ITEMS 1 TO 6	0.0000	0.0000	1.0000	0.10000	0.0000	0.0000
REAL CONSTANT SET	40	ITEMS 7 TO 12	0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000
REAL CONSTANT SET	40	ITEMS 13 TO 18	0.0000	0.0000	1.0000	0.0000	1.0000	0.50000
REAL CONSTANT SET	40	ITEMS 19 TO 24	0.0000	1.0000	1.0000	0.0000	0.0000	1.0000
REAL CONSTANT SET	42	ITEMS 1 TO 6	0.0000	0.0000	1.0000	0.10000	0.0000	0.0000
REAL CONSTANT SET	42	ITEMS 7 TO 12	0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000
REAL CONSTANT SET	42	ITEMS 13 TO 18	0.0000	0.0000	1.0000	0.0000	1.0000	0.50000

REAL CONSTANT SET	42	ITEMS 19 TO	24			
0.0000	1.0000	1.0000	0.0000	0.0000	1.0000	
REAL CONSTANT SET	43	ITEMS 1 TO	6			
0.0000	0.0000	1.0000	0.10000	0.0000	0.0000	
REAL CONSTANT SET	43	ITEMS 7 TO	12			
0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000	
REAL CONSTANT SET	43	ITEMS 13 TO	18			
0.0000	0.0000	1.0000	0.0000	1.0000	0.50000	
REAL CONSTANT SET	43	ITEMS 19 TO	24			
0.0000	1.0000	1.0000	0.0000	0.0000	1.0000	
REAL CONSTANT SET	44	ITEMS 1 TO	6			
0.0000	0.0000	1.0000	0.10000	0.0000	0.0000	
REAL CONSTANT SET	44	ITEMS 7 TO	12			
0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000	
REAL CONSTANT SET	44	ITEMS 13 TO	18			
0.0000	0.0000	1.0000	0.0000	1.0000	0.50000	
REAL CONSTANT SET	44	ITEMS 19 TO	24			
0.0000	1.0000	1.0000	0.0000	0.0000	1.0000	
REAL CONSTANT SET	45	ITEMS 1 TO	6			
0.0000	0.0000	1.0000	0.10000	0.0000	0.0000	
REAL CONSTANT SET	45	ITEMS 7 TO	12			
0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000	
REAL CONSTANT SET	45	ITEMS 13 TO	18			
0.0000	0.0000	1.0000	0.0000	1.0000	0.50000	
REAL CONSTANT SET	45	ITEMS 19 TO	24			
0.0000	1.0000	1.0000	0.0000	0.0000	1.0000	
REAL CONSTANT SET	46	ITEMS 1 TO	6			
0.0000	0.0000	1.0000	0.10000	0.0000	0.0000	
REAL CONSTANT SET	46	ITEMS 7 TO	12			
0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000	
REAL CONSTANT SET	46	ITEMS 13 TO	18			
0.0000	0.0000	1.0000	0.0000	1.0000	0.50000	
REAL CONSTANT SET	46	ITEMS 19 TO	24			
0.0000	1.0000	1.0000	0.0000	0.0000	1.0000	
REAL CONSTANT SET	47	ITEMS 1 TO	6			
0.0000	0.0000	1.0000	0.10000	0.0000	0.0000	
REAL CONSTANT SET	47	ITEMS 7 TO	12			
0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000	
REAL CONSTANT SET	47	ITEMS 13 TO	18			
0.0000	0.0000	1.0000	0.0000	1.0000	0.50000	
REAL CONSTANT SET	47	ITEMS 19 TO	24			
0.0000	1.0000	1.0000	0.0000	0.0000	1.0000	



REAL CONSTANT SET	48	ITEMS 1 TO	6			
0.0000	0.0000	1.0000	0.10000	0.0000	0.0000	
REAL CONSTANT SET	48	ITEMS 7 TO	12			
0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000	
REAL CONSTANT SET	48	ITEMS 13 TO	18			
0.0000	0.0000	1.0000	0.0000	1.0000	0.50000	
REAL CONSTANT SET	48	ITEMS 19 TO	24			
0.0000	1.0000	1.0000	0.0000	0.0000	1.0000	
REAL CONSTANT SET	50	ITEMS 1 TO	6			
0.0000	0.0000	1.0000	0.10000	0.0000	0.0000	
REAL CONSTANT SET	50	ITEMS 7 TO	12			
0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000	
REAL CONSTANT SET	50	ITEMS 13 TO	18			
0.0000	0.0000	1.0000	0.0000	1.0000	0.50000	
REAL CONSTANT SET	50	ITEMS 19 TO	24			
0.0000	1.0000	1.0000	0.0000	0.0000	1.0000	
REAL CONSTANT SET	51	ITEMS 1 TO	6			
0.0000	0.0000	1.0000	0.10000	0.0000	0.0000	
REAL CONSTANT SET	51	ITEMS 7 TO	12			
0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000	
REAL CONSTANT SET	51	ITEMS 13 TO	18			
0.0000	0.0000	1.0000	0.0000	1.0000	0.50000	
REAL CONSTANT SET	51	ITEMS 19 TO	24			
0.0000	1.0000	1.0000	0.0000	0.0000	1.0000	
REAL CONSTANT SET	52	ITEMS 1 TO	6			
0.0000	0.0000	1.0000	0.10000	0.0000	0.0000	
REAL CONSTANT SET	52	ITEMS 7 TO	12			
0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000	
REAL CONSTANT SET	52	ITEMS 13 TO	18			
0.0000	0.0000	1.0000	0.0000	1.0000	0.50000	
REAL CONSTANT SET	52	ITEMS 19 TO	24			
0.0000	1.0000	1.0000	0.0000	0.0000	1.0000	
REAL CONSTANT SET	53	ITEMS 1 TO	6			
0.0000	0.0000	1.0000	0.10000	0.0000	0.0000	
REAL CONSTANT SET	53	ITEMS 7 TO	12			
0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000	
REAL CONSTANT SET	53	ITEMS 13 TO	18			
0.0000	0.0000	1.0000	0.0000	1.0000	0.50000	
REAL CONSTANT SET	53	ITEMS 19 TO	24			
0.0000	1.0000	1.0000	0.0000	0.0000	1.0000	
REAL CONSTANT SET	54	ITEMS 1 TO	6			
0.0000	0.0000	1.0000	0.10000	0.0000	0.0000	

REAL CONSTANT SET	54	ITEMS 7 TO	12			
0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000	
REAL CONSTANT SET	54	ITEMS 13 TO	18			
0.0000	0.0000	1.0000	0.0000	1.0000	0.50000	
REAL CONSTANT SET	54	ITEMS 19 TO	24			
0.0000	1.0000	1.0000	0.0000	0.0000	1.0000	
REAL CONSTANT SET	55	ITEMS 1 TO	6			
0.0000	0.0000	1.0000	0.10000	0.0000	0.0000	
REAL CONSTANT SET	55	ITEMS 7 TO	12			
0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000	
REAL CONSTANT SET	55	ITEMS 13 TO	18			
0.0000	0.0000	1.0000	0.0000	1.0000	0.50000	
REAL CONSTANT SET	55	ITEMS 19 TO	24			
0.0000	1.0000	1.0000	0.0000	0.0000	1.0000	
REAL CONSTANT SET	55	ITEMS 25 TO	25			
10.000						
REAL CONSTANT SET	56	ITEMS 1 TO	6			
0.0000	0.0000	1.0000	0.10000	0.0000	0.0000	
REAL CONSTANT SET	56	ITEMS 7 TO	12			
0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000	
REAL CONSTANT SET	56	ITEMS 13 TO	18			
0.0000	0.0000	1.0000	0.0000	1.0000	0.50000	
REAL CONSTANT SET	56	ITEMS 19 TO	24			
0.0000	1.0000	1.0000	0.0000	0.0000	1.0000	
REAL CONSTANT SET	56	ITEMS 25 TO	25			
10.000						
REAL CONSTANT SET	57	ITEMS 1 TO	6			
0.0000	0.0000	1.0000	0.10000	0.0000	0.0000	
REAL CONSTANT SET	57	ITEMS 7 TO	12			
0.0000	0.0000	0.10000E+21	0.0000	1.0000	0.0000	
REAL CONSTANT SET	57	ITEMS 13 TO	18			
0.0000	0.0000	1.0000	0.0000	1.0000	0.50000	
REAL CONSTANT SET	57	ITEMS 19 TO	24			
0.0000	1.0000	1.0000	0.0000	0.0000	1.0000	
REAL CONSTANT SET	57	ITEMS 25 TO	25			
10.000						
REAL CONSTANT SET	71	ITEMS 1 TO	6			
1000.0	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
LIST MATERIALS	1 TO	3 BY	1			
PROPERTY= ALL						
PROPERTY TABLE EX	MAT=	1	NUM. POINTS=	6		
TEMPERATURE	DATA	TEMPERATURE	DATA	TEMPERATURE	DATA	
70.000	0.28300E+08	100.00	0.28100E+08	200.00	0.27600E+08	

300.00	0.27000E+08	400.00	0.26500E+08	500.00	0.25800E+08
PROPERTY TABLE NUXY MAT= 1 NUM. POINTS= 6					
TEMPERATURE	DATA	TEMPERATURE	DATA	TEMPERATURE	DATA
70.000	0.30000	100.00	0.30000	200.00	0.30000
300.00	0.30000	400.00	0.30000	500.00	0.30000
PROPERTY TABLE ALPX MAT= 1 NUM. POINTS= 6 REFERENCE TEMP. = 70.00					
TEMPERATURE	DATA	TEMPERATURE	DATA	TEMPERATURE	DATA
70.000	0.85000E-05	100.00	0.86000E-05	200.00	0.89000E-05
300.00	0.92000E-05	400.00	0.95000E-05	500.00	0.97000E-05
PROPERTY TABLE DENS MAT= 1 NUM. POINTS= 1					
TEMPERATURE	DATA	TEMPERATURE	DATA	TEMPERATURE	DATA
0.0000	0.28300				
PROPERTY TABLE MU MAT= 1 NUM. POINTS= 1					
TEMPERATURE	DATA	TEMPERATURE	DATA	TEMPERATURE	DATA
0.0000	0.0000				
PROPERTY TABLE EMIS MAT= 1 NUM. POINTS= 1					
TEMPERATURE	DATA	TEMPERATURE	DATA	TEMPERATURE	DATA
0.0000	0.0000				
PROPERTY TABLE EX MAT= 2 NUM. POINTS= 6					
TEMPERATURE	DATA	TEMPERATURE	DATA	TEMPERATURE	DATA
70.000	0.29900E+08	100.00	0.29900E+08	200.00	0.29900E+08
300.00	0.29900E+08	400.00	0.29900E+08	500.00	0.29900E+08
PROPERTY TABLE NUXY MAT= 2 NUM. POINTS= 6					
TEMPERATURE	DATA	TEMPERATURE	DATA	TEMPERATURE	DATA
70.000	0.30000	100.00	0.30000	200.00	0.30000
300.00	0.30000	400.00	0.30000	500.00	0.30000
PROPERTY TABLE ALPX MAT= 2 NUM. POINTS= 6 REFERENCE TEMP. = 70.00					
TEMPERATURE	DATA	TEMPERATURE	DATA	TEMPERATURE	DATA
70.000	0.65000E-05	100.00	0.65000E-05	200.00	0.65000E-05
300.00	0.65000E-05	400.00	0.65000E-05	500.00	0.65000E-05
PROPERTY TABLE DENS MAT= 2 NUM. POINTS= 1					
TEMPERATURE	DATA	TEMPERATURE	DATA	TEMPERATURE	DATA
0.0000	0.28300				
PROPERTY TABLE EX MAT= 3 NUM. POINTS= 8					
TEMPERATURE	DATA	TEMPERATURE	DATA	TEMPERATURE	DATA
-40.000	0.24600E+07	-20.000	0.24300E+07	70.000	0.22700E+07
100.00	0.22100E+07	200.00	0.20100E+07	300.00	0.18500E+07
400.00	0.17000E+07	500.00	0.15200E+07		
PROPERTY TABLE NUXY MAT= 3 NUM. POINTS= 6					
TEMPERATURE	DATA	TEMPERATURE	DATA	TEMPERATURE	DATA
81.000	0.40000	212.00	0.40000	302.00	0.40000
392.00	0.40000	513.00	0.40000	621.00	0.40000
PROPERTY TABLE ALPX MAT= 3 NUM. POINTS= 8 REFERENCE TEMP. = 70.00					
TEMPERATURE	DATA	TEMPERATURE	DATA	TEMPERATURE	DATA
-40.000	0.15560E-04	-20.000	0.15650E-04	70.000	0.16060E-04
100.00	0.16220E-04	200.00	0.16700E-04	300.00	0.17330E-04
400.00	0.18160E-04	500.00	0.19120E-04		
PROPERTY TABLE DENS MAT= 3 NUM. POINTS= 1					
TEMPERATURE	DATA	TEMPERATURE	DATA	TEMPERATURE	DATA
0.0000	0.41000				

**Title** 3-60B Cask Analyses under Puncture Drop & Impact on Trunnions During HAC Testing

**Calc. No.** ST-505 **Rev.** 1

**Sheet** 11 **of** 11

**Appendix 2**

Electronic Data on CDROM

(1 Page & 1 CDROM)