# PAT-1 SAR Addendum Structural Analysis Overview for the NRC 

David Harding

Lili Akin
Bob Kalan
Jason Petti

Sandia National Labs
June 11, 2009

## Methodology

- The PAT-1 package has been certified by the NRC (since 1978) for air transport of 2 kg powdered $\mathrm{PuO}_{2}$.
- SAR Addendum is to add solid metal to the contents list.
- The only new requirement is dynamic crush.
- NCT analyses establish the initial position of contents for accident simulations.
- The integrity of a thin eutectic barrier is shown to be maintained using an empirically-based analytical failure criterion called "Tearing Parameter".
- Staying below critical Tearing Parameter avoids even the initiation of a ductile tear in the Ti-6AI-4V eutectic barrier.


## Requirements and Acceptance Criteria

- Overall Program-Defined Package Constraints:
- PAT-1 already meets all regulatory criteria (except dynamic crush) for the same mass with oxide contents.
- AQ-1 overpack to remain the same; same TB-1 provides containment throughout NCT, HAC, air transport environments.
- Total contents mass within TB-1 (fissile and structure) not to exceed $4.4 \mathrm{lb} ; 25$ watts heat generation.
- Contents subcritical; radiation limits on container.
- T-Ampoule is a eutectic barrier only (not for Pu containment) and maintains integrity.


## Materials to be Shipped

- Electro-refined Pu bulk material
- Machined hollow cylinder form
- Pu metal samples of varying age
- Samples are typically in disc, strip, or cylinder form

- Pu-Be Composite samples
- Samples are machined into disc (or other) forms from extracted samples


## TB-1 Containment Vessel

(Shown with T-Ampoule)

## Attributes:

- PH13-8Mo stainless steel
- 12 fasteners
- Copper gasket and O-ring
- 25 watts decay heat
- $4.6 \mathrm{lbs}(2.1 \mathrm{~kg})$ content weight
- $41.6 \mathrm{lbs}(18.9 \mathrm{~kg})$ maximum gross weight
- Maximum $1080^{\circ} \mathbf{F}\left(582^{\circ} \mathrm{C}\right)$ during air accident fire test
- TB-1 design unchanged for plutonium metals transport



## Focus on T-Ampoule

## Attributes:

- Eutectic prevention barrier
- Titanium alloy (Ti-6Al-4V)
- 2-piece construction
- Machined from solid bar stock
- No welding processes
- Threaded closure bore seal w/ elastomeric O-ring
- Minimum 0.060" wall thickness
- Contents include bulk Pu metal and sample containers supported by titanium structure
- Maximum gross weight of 4.6 lbs (2.1 kg)



## TB-1 and T-Ampoule PRONTO Model


?40,000 TB-1 :lements



Sandia National
Laboratories

## Sample Containers (SC)

## Attributes:

- Titanium alloy (Ti-6Al-4V)
- 2-piece construction
- Machined from solid bar stock
- No welding processes
- Threaded closure w/ elastomeric O-ring
- Minimum 0.060" wall thickness
- Provides convenience container for single or multiple samples
- Samples placed in tantalum foil



## Sample Container Configuration

## Attributes:

- 3 individual SC-1 per T-Ampoule
- Pu Metal Allowances:
- $\leq 174$ grams per SC-1
- $\leq 522$ grams for 3 SC-1
- 2 individual SC-2 per T-Ampoule
- Pu metal allowances:
- $\leq 338$ grams per SC-2
- $\leq 676$ grams for 2 SC-2
- Titanium legs and bowl end supports serve as a position control component


Three SC-1 Sample Containers in T-Ampoule

## Sample Containers Cradle

## Attributes:

- Sharp titanium legs and asymmetric edges can unfortunately cause localized stress risers in contact with TAmpoule
- Ti-6AI-4V construction (~0.061
- No welding



## Three SC-1 Lumped Pu Contents Models



## Two SC-2 Lumped Pu Contents Models



Note larger Pu cylinders with higher mass

## Electro-Refined Plutonium Cylinder

## Attributes:

- Hollow Pu cylindrical shape allows softer deformable configuration to mitigate impact stresses
- Allowable Pu mass is $\mathbf{8 3 1}$ and 731 grams
- Pu metal cylinder wrapped in tantalum foil, no other supports are required.


3 to $3.5 \mathrm{~kg}, 102 \mathrm{~mm}$ dia. $\times 13 \mathrm{~mm}$ wall $x 51 \mathrm{~mm}$ length

831 gm Hollow Cylinder

## 831 g ER Cylinder Models



## LANL-Defined Composite Sample Configuration 1: Small Pu Cylinders

One configuration:
The individual cylinders (at 1.7 grams each) are combined into a single cylinder of 16.85 mm dia $\times 16.85 \mathrm{~mm}$ height weighing 60 grams using the strength of Be metal.
Up to 35 individual 1.7 gram cylinders ( 59.5 grams) could be packaged in each sample container.


## LANL-Defined Composite Sample Configuration 2: Composite Disk

Two configurations:
a) $\mathbf{1 2} \mathbf{~ m m}$ dia $\times 6 \mathrm{~mm}$ thick (weighing $\mathbf{1 0 . 8} \mathrm{g}$ using Pu density) with beryllium metal strength.
b) b) $\mathbf{4 5} \mathbf{~ m m}$ dia $\times 2.37 \mathrm{~mm}$ thick (weighing 59.9 g using Pu density) with beryllium metal strength.
b)


## LANL-Defined Composite Sample Configuration 3: Flat Composite Plate

Two Configurations:
a) 50 mm length $\times 6 \mathrm{~mm}$ thick $\times 12.5 \mathrm{~mm}$ wide composite plate (weighing 59.6 g using Pu density) with beryllium metal strength.
b) b) 30 mm length $\times 6 \mathrm{~mm}$ thick $\times 12.5 \mathrm{~mm}$ wide composite plate (weighing 35.8 g using Pu density) with beryllium metal strength.


## LANL-Defined Composite Sample Configuration 4: Long Pu Cylinders

## Two Configurations:

a) 8.9 mm dia $\times 60 \mathrm{~mm}$ length (weighing 59.3 grams using Pu density) with beryllium strength.
b) b) 7.62 mm dia $\times 26 \mathrm{~mm}$ length (weighing 18.9 grams using Pu density) with beryllium strength.


## "Bounding" Composite

A single cylinder of 16.85 mm dia $\times 16.85 \mathrm{~mm}$ height weighing 60 grams (density of Pu ) using the strength of Be metal.
This compact and strong shape maximizes net impact velocity and provides a conservatively sharp impact edge.
Cylinders always rotated to impact CGOC (sharpest).


## Full Package Analysis: Overpack Calculation Has Been Validated with Certification Tests



## FEA Model Conservatisms

- Always assume contents in most damage-inducing location/orientation (velocity/sharpness).
- Ignore Ta foil slight energy absorber/load spreader.
- Pu, Be assumed infinitely plastic.
- Be composite shape is bounding.
- ER cylinders assume strongest dimensions.
- Ductile crack propagation is not modeled; assume "failure" at ductile crack initiation.


## Acceptance Criteria

- TB-1 containment vessel must
- be "essentially leak tight" in air transport accidents ( $<\mathrm{A}_{2} / \mathrm{wk}$ )
- meet thru-wall ASME stress limits for NCT and HAC
- NCT and HAC limits already accepted via certification tests
- HAC dynamic crush is new requirement since original SAR
- T-Ampoule eutectic barrier must maintain integrity.


## Tearing Parameter Failure Criterion

- Over the last 40+ years, improvements to failure criteria have been made. The most successful criterion matching test data (including notched) very well is Tearing Parameter:

$$
T P=\int_{0}^{\bar{\varepsilon}_{p f}}\left\langle\frac{2 \sigma_{1}}{3\left(\sigma_{1}-\sigma_{H}\right)}\right\rangle^{4} d \bar{\varepsilon}_{p}
$$

- This ductile Tearing Parameter has been successfully used for many years at Sandia to simulate ductile failure.
- References: Bridgman, 1964; Brozzo, et al., 1972; Johnson \& Cook, 1985; Wellman, et al., 1993; Dawson, et. al., 1998; Bao \& Weirzbicki, 2003; Wellman, 2007.


## Critical Tearing Parameter

- The critical value of TP is determined from the analysis of a tensile test to failure, for the Ti-6Al-4V T-Ampoule material.
- TP is evaluated using the computed stress state, with the EQPS at failure used as the upper integration limit.
- $\mathbf{T P}_{\text {crit }}=1.012$ for Ti-6Al-4V based on the tensile tests.
- TP can be computed for elements in the T-Ampoule and compared to the critical value of $\mathbf{1 . 0 1 2}$.


## Analysis of Ti-6AI-4V Tensile Test




Sandia
National
Laboratories

## Combined Model Results

- Example of Full Models for High Speed and HAC.
- Sample Runs (only 5 chosen out of total 53 analyses)
- High Speed 2 Amp ( 45 deg) Side Impact
- High Speed 831 g ER Cylinder Angled for End Impact
- High Speed 831 g ER Cylinder CGOC Impact
- Be Composite High Speed 3 Amp ( 45 deg) Side Impact
- HAC 2 Amp (45 deg) CGOC Impact
- In no case does the impact of the contents induce ductile tearing of the eutectic barrier.


## Example of Full Models (Approximately 2,000,000 Elements)



HAC and NCT


High Speed

## High Speed 2A (45 deg) Side Impact



## High Speed 2A (45 deg) Side Impact



## High Speed 2A (45 deg) Side Impact



## High Speed 2A (45 deg) Side Impact



0 Elements Exceed the Critical Tearing Parameter

## Friction Variation

- Plus or minus 33\% on friction coefficient (from referenced 0.30 ) were analyzed for the 2 Ampoule side impact 45-degree rotated case:
- 0.40 dynamic friction yielded very similar results for both T-Ampoule Tearing Parameter and TB-1 EQPS
- 0.20 dynamic friction also yielded similar results for TB-1 EQPS, but much reduced T-Ampoule Tearing Parameter (peaking around $<0.2$ vs. 0.5 )


## Cylinder - 831 g (Angled End Impact)



## Cylinder - 831 g (Angled End Impact)



## Cylinder - 831 g (Angled End Impact)



## Cylinder - 831 g (Angled End Impact)



0 Elements Exceed the Critical Tearing Parameter

## Cylinder - 831 g (CGOC Impact)



## Cylinder - 831 g (CGOC Impact)



## Cylinder - 831 g (CGOC Impact)



## Cylinder - 831 g (CGOC Impact)



## Cylinder - 831 g (CGOC Impact)



0 Elements Exceed the Critical Tearing Parameter

## Be Composite Cylinder (45 deg) Side Impact



## Be Composite Cylinder (45 deg) Side Impact



## Be Composite Cylinder (45 deg) Side Impact

Comparison Graph Tearing Parameter
Titanium Impact Test and High Speed 3A (45deg) Full Model
Composite Plugs and Side Impact


0 Elements Exceed the Critical Tearing Parameter

## HAC - 2A (45 deg) CGOC Impact



No Elements Extend Beyond the B-W Locus
0 Elements Exceed ASME Stress Limits in the TB1

## HAC - 2A (45 deg) CGOC Impact



0 Elements Exceed Thru-Thickness
ASME Stress Limits (107 ksi) in the TB1

## HAC - 2A (45 deg) CGOC Impact



- No elements violate ASME thru-thickness allowables for HAC: $0.7 \mathrm{~S}_{\mathrm{u}}=107 \mathrm{ksi}$
- Similar results for end and side HAC dynamic crush impacts


## Conclusions

- FEA results show that ductile tearing will NOT be initiated in the T-Ampoule eutectic barrier, based on the Tearing Parameter failure criterion
- No leakage or seal area (or any other visible) deformation occurred in the original PAT-1 certification tests, and based on analyses, none occur with the new metal contents (except minimal localized denting)
- Thru-thickness TB-1 stresses well below ASME allowables for dynamic crush
- The analyses performed provide sufficient evidence that the PAT- 1 container can safely transport the proposed solid metal contents

