

Irradiation Embrittlement Mechanical Properties and Irradiated Assisted Stress Corrosion Cracking

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Outline

- □ NRC Research Activities
- SSRT Testing
- □ Fracture Toughness Testing
- □ Results
- □ Summary
- □ Future Work



NRC Research

□ NRC IASCC research focused on the following areas

- Evaluate effectiveness of SCC mitigations
 - Hydrogen Water Chemistry
 - Grain Boundary Engineering
- Evaluate CGR models for BWRs and PWRs
- Evaluate the causes, mechanisms and effects of EAC on BWR internals
- Effect of cold work on crack growth rates
- Review and evaluation of EAC in vessel internal components and emerging aging degradation issues
- Radiation embrittlement at relevant to PWR conditions
- Radiation and thermal embrittlement of cast austenitic stainless steels



Alloys for SSRT

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	Heat ID	Description	Objectives		
	333	Type 304 SS from ABB GBE Type 304 SS			
	GBE304				
	304L	Type 304L SS.			
	GBE304L	GBE Type 304L SS		Effect of GBE	
	GBE316	GBE Type 316 SS			
	690	Alloy 690			
	GBE690	GBE Alloy 690)		
	623	Type 316LN SS	}	Effect of Ti	
	625	Type 316LN SS, Ti-doped	5	Ellect of TI	
Common Materials in Halden & BOR-60 Irr.	327	327High-purity Type 304L SS with low O945High-purity Type 304L SS with high O		Effect of O	
	945				
	C1 (SA, CW)	Low S, Type 304 SS, high P			
	C3 (SA, CW)	Type 304L SS			
	C9	High S, Type 304 SS 2 Low S, Type 304 SS		Effect of S	
	C12				
	L5	304-like alloy with high Ni and Cr			



SSRT Specimens



Elongations are expected to be different between the Halden and BOR-60 specimens $(I/A^{0.5} \approx 1.8)$



Experimental – Irradiation

- □ Halden reactor a boiling heavy water reactor
 - Dry irradiation in He-sealed capsules
 - Irradiation temperature ~ 290°C
 - Dose rate ~ 10^{-7} dpa/s
 - He/dpa ratio for a Typical LWR: ~2-5 appm/dpa.
- □ BOR-60 reactor a sodium cooled fast breeder reactor
 - Samples exposed to sodium
 - Irradiation temperature ~ 320°C
 - Dose rate ~ $9x10^{-7}$ dpa/s
 - He/dpa ratio for a Typical fast reactor: < 0.5 appm/dpa



SSRT Testing

Loading grip for BOR-60 specimen







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Fractography – SSRT Specimens



BOR-60 specimen



Sectioned Halden specimen



Characterize fracture surface

- IG or TG area fractions
- Number of IG or TG areas



Fracture Toughness Testing

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□ Weldments

- 304L submerge arc (SA) weld -- a *double-V butt weld* on Type 304L hot-rolled plates (ASME SA240) using ER308L filler rods.
- 304 shield metal arc (SMA) weld -- a *single-V butt weld* on Type 304 plates using E308 filler rods.
- Post-weld thermal treatment -- 500°C for 24 hours (to simulate the effect of low-temperature sensitization).

Four materials

- 304L SA HAZ, as-welded
- 304L SA HAZ, thermally-treated
- 304 SMA HAZ, as welded
- 304 SMA HAZ, thermally-treated

Weld	Heat ID	Ni	Si	Р	S	Mn	С	Ν	Cr	Mo	0
304 SMA	10285	8.45	0.60	0.015	0.007	1.90	0.070	0.084	18.56	0.51	0.013
304L SA	GG Top Shell	9.05	0.53	0.027	0.016	1.84	0.013	0.064	18.23	0.44	0.010

Chemical composition of the weld HAZ materials



Fracture Toughness Specimens

- 3.00 ^{+.05} 2 THRU HOLES Specimen geometry – 1/4T-CT || A .02 15.00 6.50-12.00 ← 6.00 **∢**-3.25→ ⊥ A .02 ⊥ C .02 -.794 CENTERED 2.00 B ⊥ A .02 7.00 ۷ 3.30 20° 1.89 14.00 1.89 3.30 20° 7.00 || B .02 2.00 XXX-X ⊥ A .02 ⊥ C .02 -1.53 DIA 2 THRU HOLES 2.00 SPECIMEN ID 120 130 140 150 160 170 180 20 80 100 110 150 130 140 1 7 15 34 32 47 47 55 1 15 32 32 47 47 48 5 1 15 24 32 47 47 304 SMA weld 304L SA weld



Fracture Toughness Specimens - Irradiation

Irradiated in Halden reactor in helium-sealed capsules

Irradiation conditions for the weld HAZ compact tension specimens

Material	Heat Treatment	Fast Neutron Fluence E > 1 MeV $(x10^{21} \text{ n/cm}^2)$	Displacement Damage (dpa)	Irradiation Temperature (°C)
	As-welded	0.50	0.75	~290
GG 304L SA HAZ	As-welded	1.44	2.15	290-296
	24 h @ 500°C	1.63	2.43	~290
	As welded	0.50	0.75	~290
304 SS SMA HA7	As-welueu	1.44	2.15	290-296
JUT SS SIVIA HAZ	24 h @ 500°C	0.50	0.75	~290
	24 II @ 300 C	1.44	2.15	290-296



Fracture Toughness Test Conditions

Temp:	≈290°C
DO:	≈350 ppb with N_2 + 1% O_2 cover gas
	<30 ppb with 4% H ₂ cover gas
Flow rate:	15–25 mL/min
Conductivity:	0.08 - 0.12 μS/cm
K _{max} :	approximately constant by load shedding
K/size criterion:	B and (W-a) \geq 2.5*(K/ σ_{eff}) ² , where $\sigma_{eff} = (\sigma_y + \sigma_u)/2$ for
	nonirradiated specimens, $\sigma_{eff} = \sigma_{y-irr}$ for irradiated specimens
J-R curve tests:	constant extension rate of 0.43 μ m/s. Use a blunting line given by $\Delta a = J/(4\sigma_f)$.





Irradiation hardening and embitterment start to appear at dose <0.5 dpa.



U.S.NRC Effect of Irradiation Dose on **Total Elongation**



Irradiation hardening starts to saturate around 3-5 dpa, and loss of elongation reaches a minimum around 2 dpa.



U.S.NRC Effect of Irradiation Dose on Intergranular Fracture

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IG cracking starts to occur at a dose lower than that elongation reaches minimum.



SSRT Testing

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NUREG/CR-6965, Halden Phase-II, Alloys 304, 304L, 316L, 690



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Fracture Toughness Testing Results



- Fracture toughness data of as-welded and thermally-treated HAZs are within the scatter band.
- Thermal treatment may have improved the fracture toughness of irradiated 304 SMA HAZ at 0.75 dpa



Summary

- While irradiation hardening and embattlement starts to appears at very low doses, the dose dependence of IG cracking shows a "*threshold*" behavior. IG cracking start to appear before the dose for that elongations reach minimum.
- The post-irradiation strengths (YS and UTS) for the BOR-60 specimens were consistently lower than those of the corresponding Halden specimens. Likely related to Neutron spectrum and damage rate.
- Fracture toughness data for irradiated SA and SMA HAZs are within the scatter band. Thermal treatment may have improved the fracture toughness of irradiated 304 SMA HAZ at 0.75 dpa



Future Work

- □ High dose specimens
 - Simulate PWR end of life
 - Interest in samples from Zorita
- □ SSRT testing at 10 and 40 dpa
- □ TEM specimens up to 40 dpa

