Ref: 10 CFR 50.55a



Crystal River Nuclear Plant Docket No. 50-302 Operating License No. DPR-72

May 28, 2009 3F0509-08

U.S. Nuclear Regulatory Commission Attn: Document Control Desk Washington, DC 20555-0001

- Subject: Crystal River Unit 3 Third Ten-Year Inservice Inspection (ISI) Interval Relief Request #09-003-II, Revision 1 (TAC NO. ME0907)
- Reference: CR-3 to NRC letter dated March 20, 2009, "Crystal River Unit 3 Third Ten-Year Inservice Inspection (ISI) Interval Relief Requests #09-001-II, #09-002-II and #09-003-II"

Dear Sir:

Pursuant to 10 CFR 50.55a(g)(5)(iii), Florida Power Corporation (FPC), doing business as Progress Energy Florida, Inc., hereby submits Relief Request #09-003-II, Revision 1, for Inservice Inspection Impracticality. Relief Request #09-003-II, Revision 0, was initially submitted pursuant to 10 CFR 50.55a(g)(6)(ii)(A)(5) and 10 CFR 50.55a(a)(3)(i), for Reactor Pressure Vessel Shell Weld Examinations. The purpose of this relief request is to seek approval for limited volumetric examinations performed on the ASME Code Class 1 Reactor Pressure Vessel Shell during the Crystal River Unit 3 (CR-3) Third Ten-Year Inservice Inspection (ISI) Interval. The examinations covered less than 90 percent of the weld volume required to be examined by the ASME Boiler and Pressure Vessel Code, Section XI, 1989 Edition, no Addenda. The examinations were limited due to geometry or by interferences with other plant components.

This submittal also corrects a reference contained in the Precedent Section of Relief Request #09-003-II, Revision 0. NRC letter dated August 5, 1999, (TAC NO. MA1642) was referenced instead of NRC letter dated October 1, 1999, (TAC NO. MA3314).

No new regulatory commitments are made in this submittal.

If you have any questions regarding this submittal, please contact Mr. Dan Westcott, ... Supervisor, Licensing and Regulatory Programs at (352) 563-4796.

Sincerely, Klobemann for S.J. CAHILL Stephen J. Cahill

Stephen J. Cahill Manager, Engineering Crystal River Nuclear Plant

SJC/dwh

Enclosure: Relief Request #09-003-II; Revision 1

xc: NRR Project Manager Regional Administrator, NRC Region II Senior Resident Inspector

Progress Energy Florida, Inc. Crystal River Nuclear Plant 15760 W. Power Line Street Crystal River, FL 34428

PROGRESS ENERGY FLORIDA, INC.

CRYSTAL RIVER UNIT 3

DOCKET NUMBER 50 - 302 / LICENSE NUMBER DPR - 72

ENCLOSURE

INSERVICE INSPECTION RELIEF REQUEST #09-003-II, REVISION 1 THIRD TEN-YEAR ISI INTERVAL

10 CFR 50.55a Request #09-003-II, Revision 1

Relief Request in Accordance with 10 CFR 50.55a(g)(5)(iii)

--Inservice Inspection Impracticality--

1. ASME Code Component(s) Affected

Reactor Pressure Vessel Lower Shell-to-Transition Piece Weld, Unique Identifier B1.2.1

Reactor Pressure Vessel Nozzle Belt Intermediate Shell Weld, Unique Identifier B1.2.3

Reactor Pressure Vessel Lower Shell to Lower Head Weld, Unique Identifier B1.2.2

Reactor Pressure Vessel Long Seam at 247 degrees, Unique Identifier B1.1.5

Reactor Pressure Vessel Long Seam at 67 degrees, Unique Identifier B1.1.6

Reactor Pressure Vessel Outlet Nozzle-to-Shell Weld, Unique Identifier B1.4.7A

Reactor Pressure Vessel Outlet Nozzle-to-Shell Weld, Unique Identifier B1.4.8A

2. Applicable Code Edition and Addenda

American Society of Mechanical Engineers (ASME), Boiler and Pressure Vessel Code, Section XI, 1989 Edition, no addenda.

3. Applicable Code Requirement

ASME Code, Section XI, Sub-article IWB-2500 states, in part, "Components shall be examined and tested as specified in Table IWB-2500-1." Table IWB-2500-1 requires an examination of applicable Class 1 pressure retaining-welds, which includes essentially 100 percent of weld length once during the ten-year ISI interval for the following Code Categories:

Category B-A: Item Numbers B1.11 and B1.12 Category B-D: Item Number B3.90

10 CFR 50.55a(g)(6)(ii)(A)(2) requires licensees to implement the examination requirements of the 1989 Edition of ASME Section XI for reactor vessel shell welds. Subsection IWB, Table IWB-2500-1, "Examination Category B-A," Item B1.11, requires a 100 percent volumetric examination of all shell welds for the Third Ten-Year ISI Interval. As defined in 10 CFR 50.55a(g)(6)(ii)(A)(2), 100 percent, as used in Table IWB-2500-1, means more than 90 percent of the examination volume of each weld, where the reduction in coverage is due to interference by another component, or part geometry.

Code Case N-460 permits a reduction in examination coverage of Class 1 and Class 2 welds provided the coverage reduction is less than 10 percent. CR-3 has adopted Code Case N-460 in the Inservice Inspection (ISI) Program Plan, as permitted by NRC Regulatory Guide 1.147, Revision 15.

4. Determination of Limits of Weld Volume Examination

Examinations were performed using two Trans World System manipulators and AREVA's Automated Data Acquisition and Analysis System, ACCUSONEX. All ultrasonic examinations were performed using examination procedures and personnel qualified by demonstration in accordance with the requirements of Appendix VIII of the ASME Boiler and Pressure Vessel Code, Section XI, 1995 Edition with Editions up to and Addenda through 2000, as modified by the Performance Demonstration Initiative (PDI) program. These examinations were performed to the acceptance standards of ASME Boiler and Pressure Vessel Code, Section XI, 1989 edition, no addenda. These examinations were performed to the maximum extent possible.

Examinations of the reactor vessel circumferential, longitudinal, and nozzle-to-shell welds, scanned from the vessel shell, were performed using 45 degree shear wave, 45 degree longitudinal wave and 70 degree longitudinal wave transducers. The circumferential and longitudinal welds were examined by scanning from four opposing beam directions such that the sound energy from the angle beams pass through the weld material and adjacent base material from each direction to the maximum extent possible. The nozzles to shell welds (inlet and outlet) were scanned from the vessel shell using four opposing beam directions and from the bore with beams looking radially. The scans from the bore used 45 degree shear wave and 15 degree longitudinal wave transducers. The inside radius sections of the inlet and outlet nozzles were also examined by enhanced visual testing.

For each required scan, the amount of sound beam that passed though the required examination volume has been plotted on scaled cross sectional drawings of each component configuration (see Attachment B). The examination coverages reported in the following table have been determined by averaging the amount of coverage obtained from each of the required scans for the required examination volume. These examinations are limited by part geometry or interferences with other components, such that the reduction in coverage is greater than 10 percent.

ldentifier	Description	Category	ltem	Coverage	Limitation
B1.2.1	RPV Lower Shell to- Transition Piece	B-A	B1.11	46	The core guide lugs and flow distributors interfere with scan paths.
B1.2.3	RPV Nozzle Belt Intermediate Weld	B-A	B1.11	90	Inlet and outlet nozzles interfere with the scan paths.
B1.2.2	RPV Transition Piece to Bottom Head	B-A	B1.11	0	Core guide lugs and flow distributors prevent inspection
B1.1.5	RPV Long Seam, at 247 degrees	B-A	B1.12	88.1	Core guide lugs and flow stabilizers prevented full movement of the head

ldentifier	Description	Category	Item	Coverage	Limitation
B1.1.6	RPV Long Seam, at 67 degrees	B-A	B1.12	88.1	Core guide lugs and flow stabilizers prevented full movement of the head
B1.4.7A	A Outlet Nozzle to RPV Shell Weld	B-D	B3.90	69.8	Surface Geometry
B1.4.8A	B Outlet Nozzle to RPV Shell Weld	B-D	B3.90	69.8	Surface Geometry

Examination Details

Component B1.2.1: Reactor Pressure Vessel Lower Shell-to-Transition Piece Weld

The pre-service records reported the examination coverage as "best effort" due to the interferences with core guide lugs and flow stabilizer vanes (see Attachment A, FPC Drawing 135546E, for lug and vane locations). No preservice indications were recorded.

During the First Ten-Year ISI Interval examination, the core guide lugs and flow stabilizer vanes were reported as limitations and no indications were recorded.

During the Second Ten-Year ISI Interval examination, the average amount of coverage was calculated to be 29 percent.

During the Third Ten-Year ISI Interval examination, the average amount of coverage has been calculated to be 46 percent. Twelve (12) sections of the weld between the 12 lugs were accessible for examination. No unacceptable indications have been recorded.

Although the weld area beneath the lugs received no ultrasonic examination coverage, no flaws were identified during a remote VT-3 visual examination of the lug areas. This weld is located outside of the area of highest irradiation in the reactor vessel. (See Attachment B for coverage data.)

Component B1.2.3: Reactor Pressure Vessel Nozzle Belt Intermediate Weld

No limitation areas were reported during the pre-service examination of this component. The weld was examined to the maximum extent possible. No relevant pre-service indications were recorded.

During the First Ten-Year ISI Interval examination, only 5 percent of the weld length was examined to satisfy the requirements of Table IWB-2500 of the 1974 Edition of ASME Section XI through Summer 1975 Addenda. No indications were recorded.

During the Second Ten-Year ISI Interval examination, a total of 75 percent of the weld was examined. No unacceptable indications were recorded.

During the Third Ten-Year ISI Interval examination, a total of 90 percent of the weld was examined. The remaining ten percent was not accessible due to scanning interferences with the inlet nozzle openings and the outlet nozzle boss extensions. (See Attachment B for coverage data.)

Component B1.2.2: Reactor Vessel Transition Piece to Bottom Head Weld

The subject weld is the reactor vessel transition-piece-to-bottom-head-weld. This weld is located below the beltline region and is not subject to the majority of the neutron flux escaping from the core. An evaluation of neutron embrittlement as a potential damage mechanism has been performed with the conclusion that service induced degradation of the transition-piece-to-bottom-head-weld as a result of corrosion, fatigue, nuclear or thermal embrittlement mechanisms is extremely unlikely.

This weld has been visually and ultrasonically inspected once during pre-service inspection (essentially 100 percent coverage). The volumetric examination method utilized during the pre-service inspection was performed with the manual contact method. There were no reportable or recordable indications detected during this inspection.

During the First Ten-Year ISI Interval vessel inspection, the weld was partially inspected (approximately 5 percent) using the immersion method of ultrasonic inspection. This was acceptable as per the ASME Boiler and Pressure Vessel Code, Section XI, 1974 Edition through the Summer of 1975 Addenda, and Regulatory Guide 1.150. The extent of this examination was acceptable since the 1974 Edition of ASME Section XI, Table 2500-1, Category B-A, only required the examination of 5 percent of this weld. The examination was performed using the ARIS II remote scanner, a device that utilized immersion ultrasonic techniques. The examination revealed no baseline indications, no reportable indications.

Although the use of immersion testing allowed the weld to be inspected with inspection equipment at a distance of up to twenty inches away from the weld, access for examination of this weld was limited by the flow stabilizers, the core support lugs and the incore instrumentation nozzles.

Since that inspection was performed, improvements in volumetric examination methods have shown the contact method to be much more accurate and reliable than the immersion method. As a result, equipment designed to use the immersion technique has been abandoned and modern reactor vessel inspection equipment has been designed to utilize the contact examination method.

Relief was granted from this inspection during the Second Ten-Year ISI Interval under Relief Request #95-030 (TAC NO. M93755).

The Third Ten-Year ISI Interval volumetric inspections were not able to be performed using modern automated reactor vessel inspection equipment. The implementation of the requirements of Appendix VIII of the ASME Boiler and Pressure Vessel Code, Section XI, 1995 Edition with Editions up to and Addenda through 2000, as modified by the PDI program, place stringent controls on the methodology utilized in performing this inspection.

Access to the weld from the vessel exterior presents safety and As Low As Reasonably Achievable hazards. Access to the weld to perform the inspection from the outside using a manual contact ultrasonic method would require concrete removal in the cavity and suspension of an inspection team between the exterior of the vessel and inside the shield wall by harnesses.

The reactor vessel interior was subject to VT-1 and VT-3 inspections in Refueling Outage 15 during the Fall of 2007 which included all welds and interior attachments. VT-2 inspections on the exterior of the vessel were performed during the inservice leak test performed during start-up. No indications were identified during these inspections.

Components B1.1.5 and B1.1.6: RPV Long Seam

The Reactor Pressure Vessel (RPV) long seam welds on the lower head to lower shell section are limited by the geometry of the core positioning lugs and the flow stabilizers(see Attachment A, FPC Drawings 135544E and 135546E).

The location of the obstructions prevented the scanning head of the inspection tool to achieve required coverage. During the Second Ten-Year ISI Interval, 94 percent coverage was achieved using a different inspection methodology that was not approved through the PDI process.

Inspections performed as directed by Appendix VIII of the ASME Boiler and Pressure Vessel Code, Section XI, 1995 Edition with Editions up to and Addenda through 2000, as modified by the PDI program, are more stringent in transducer selection which allowed for 88.1 percent required coverage for these longitudinal welds. No unacceptable indications have been identified during the Pre-service, First Ten-Year ISI Interval, Second Ten-Year ISI Interval, or Third Ten-Year ISI Interval examinations of these longitudinal welds. (See Attachment B for coverage data.)

Components B1.4.7A and B1.4.8A: Reactor Pressure Vessel Outlet Nozzle to Shell Welds

The outlet nozzle extension geometry has provided the same limitation area during the Pre-service, First Ten-Year ISI Interval, and Second Ten-Year ISI Interval volumetric examinations of these nozzle welds (see Attachment A, FPC Drawing 135540E). The boss extension limits the circumferential scan coverage to 26 percent. However, 100 percent of the required weld volume and adjacent base material has received 2 axial angle beam scans from the nozzle bore. No unacceptable indications have been identified during the Pre-service, First Ten-Year ISI Interval, Second Ten-Year ISI Interval or Third Ten-Year ISI Interval examinations of these outlet nozzle-to-shell welds. (See Attachment B for coverage data.) U. S. Nuclear Regulatory Commission 3F0509-08

5. **Proposed Alternative and Basis for Use**

None. In lieu of the ASME Code requirement of essentially 100 percent volumetric examination, CR-3 proposes ultrasonic inspections of accessible areas to the maximum extent practical, given the design configuration of the Reactor Pressure Vessel Welds, and VT Inspections of all accessible areas sufficient for continued safe operation. Additionally, system leak rate limitations are imposed by Improved Technical Specification 3.4.12 and reactor building normal sump rate monitoring provides additional assurance that any leakage would be detected prior to gross failure of the component.

6. Duration of proposed Alternative

Relief is requested for the Third Ten-Year ISI Interval of the Inservice Inspection Program for CR-3 which was effective from August 14, 1998, ending August 13, 2008.

7. Precedents (Optional)

NRC granted relief for Augmented Reactor Vessel Shell Weld Examination under Relief Request #98-009-II on October 1, 1999 (TAC NO. MA3314).

NRC granted relief for RPV Lower Head to Bottom Shell Weld under Relief Request #95-030 on April 14, 1996 (TAC NO. M93755).

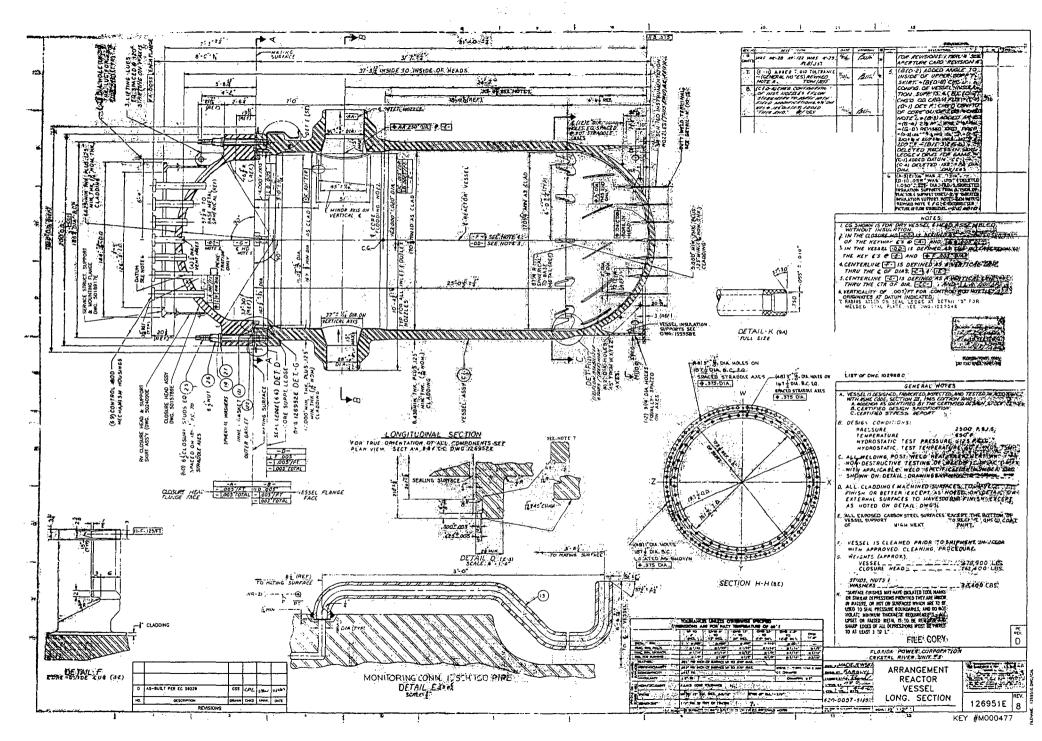
8. References (Optional)

ENCLOSURE ATTACHMENT A

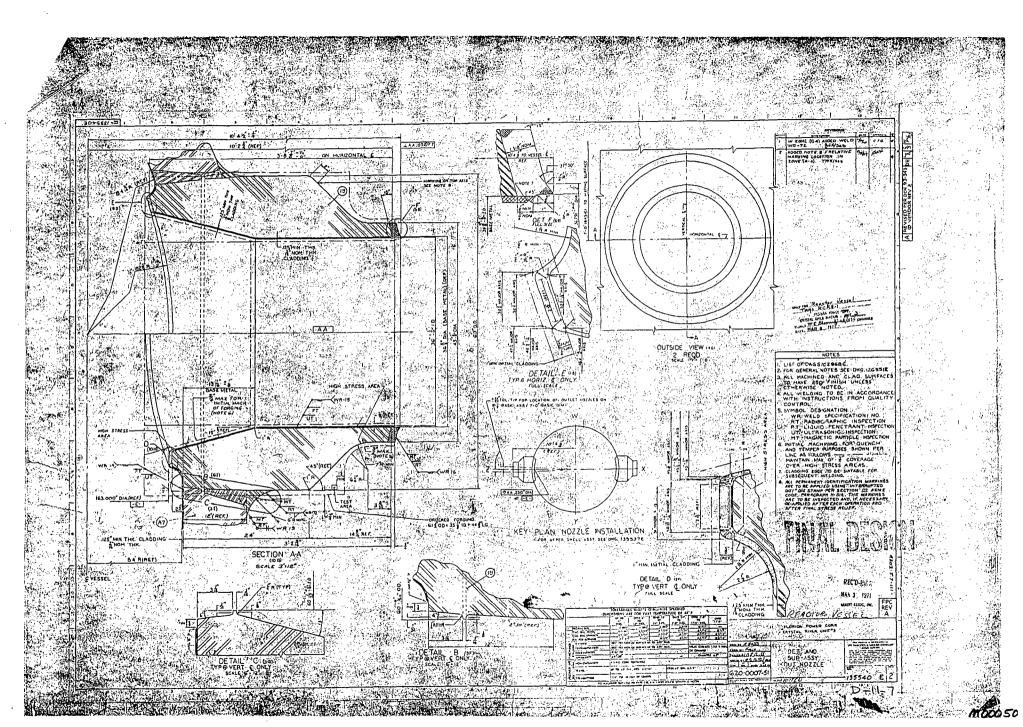
VESSEL DRAWINGS

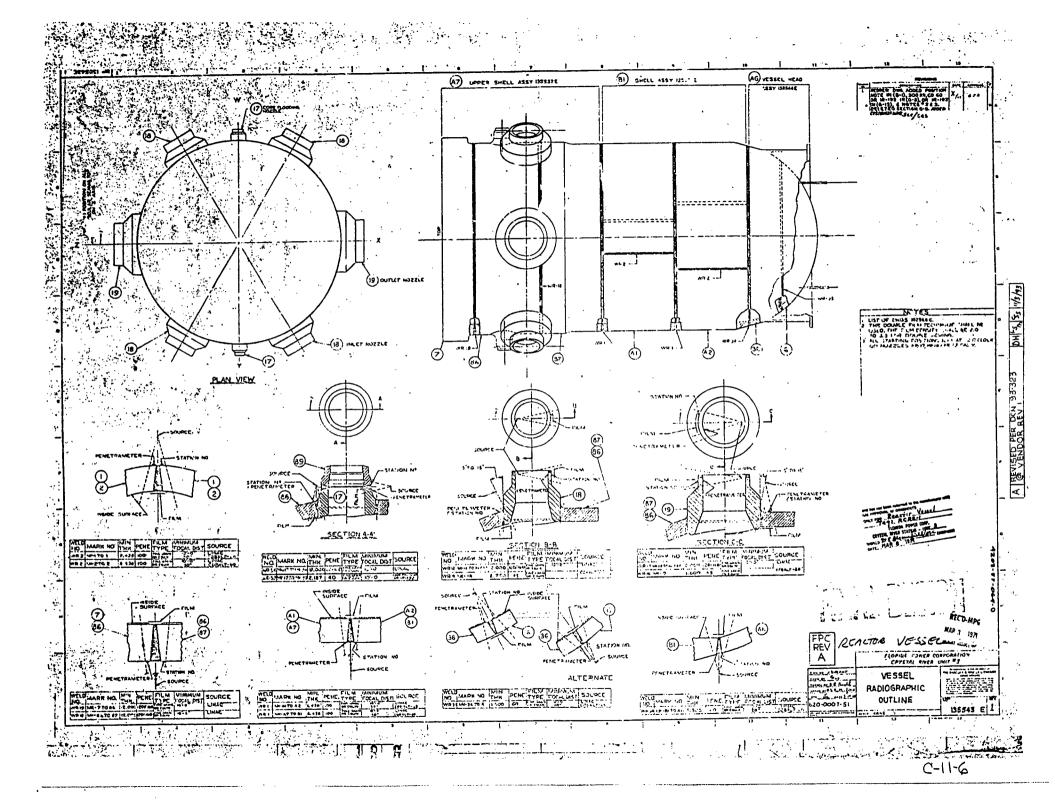
INSERVICE INSPECTION RELIEF REQUEST #09-003-II, REVISION 1 THIRD TEN-YEAR ISI INTERVAL

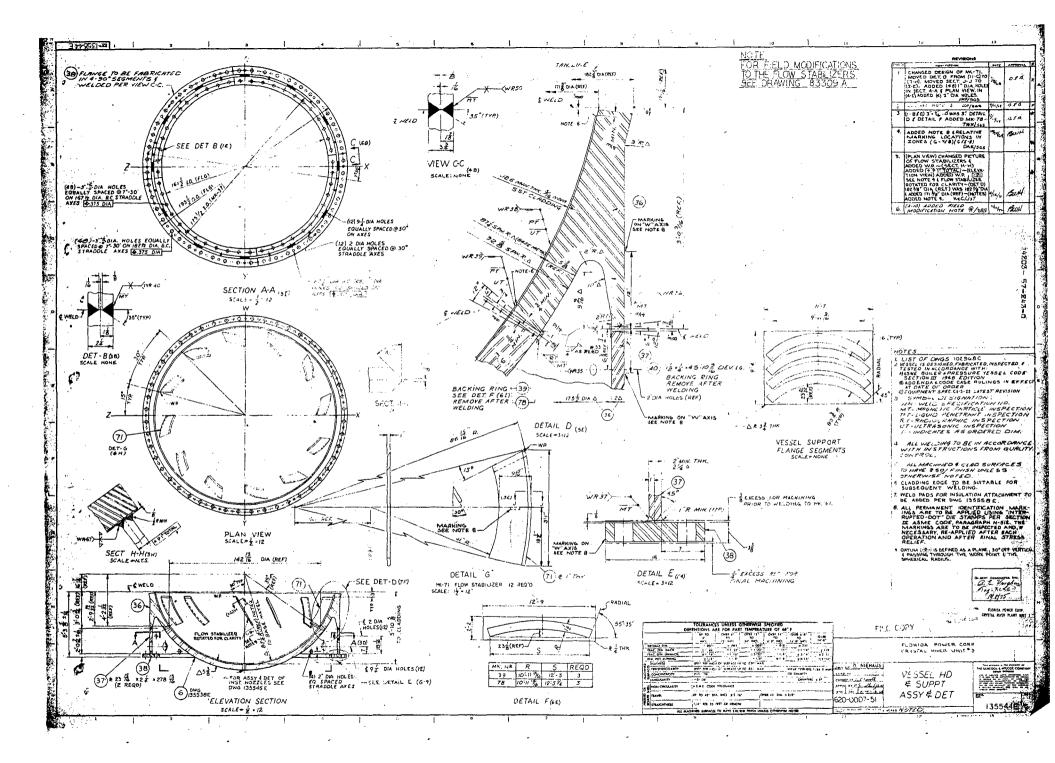
<u>126951E</u>	Arrangement Reactor Vessel Long Section
<u>135540E</u>	Reactor Vessel Detail and Sub-Assembly Outlet Nozzles
<u>135543E</u>	Vessel Radiographic Outline
<u>135544E</u>	Vessel Head and Support Assembly Detail
<u>135546E</u>	Vessel Assembly and Final Machining



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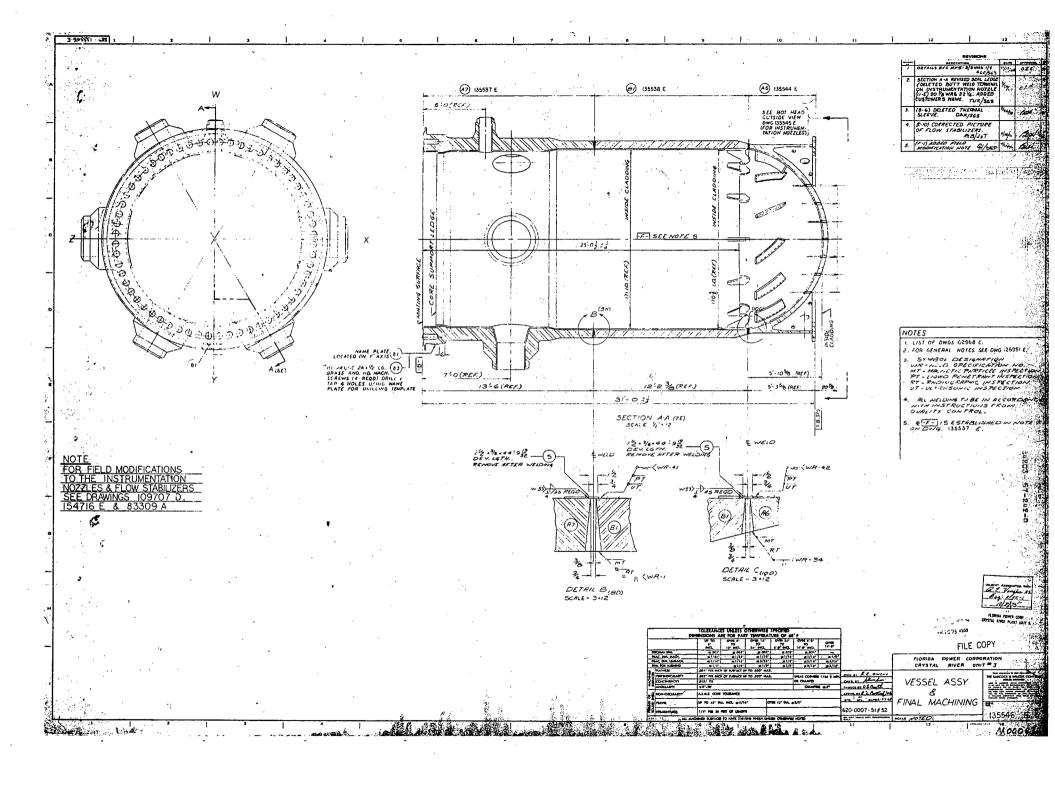






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ENCLOSURE

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ATTACHMENT B

COVERAGE DATA

INSERVICE INSPECTION RELIEF REQUEST #09-003-II, REVISION 1 THIRD TEN-YEAR ISI INTERVAL

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Coverage Layout & Calculations

Neld Description: Lower Shell to Lower Head ASME Code Item No.: B1.11 CR-3 Weld ID: B1.2.1 **TWS Weld Designator: W09**

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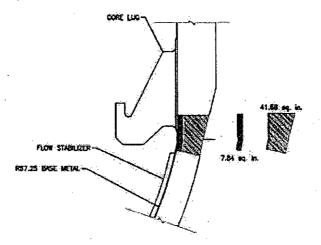
ASME Code Figure No.: IWB-2500-1 AREVA Drawing No.: 8019749

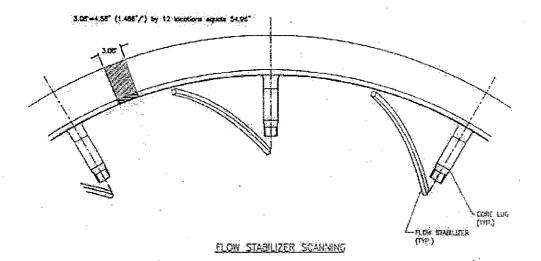
AGGREGATE COVERAGE: 46.0%

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	70L/45L	Down	7.84	54,95	430/9	4196.4	10.3%	Yes	Lugs & Flow Stabilizers
384	70L/45L	ew & cow	7.84	97.20	762.0	4196,4	18:2%	Yes	Lugs & Flow Stabilizers
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2	45U/455	Down	41,68	54,08	2290.7	22309.2	10.3%	Yes	Lugs & Flow Stabilizers
384	451/455	CW & CCW	41.68	160.32	6682.1	22309.2	30.0%	Yes	Lugs & Flow Stabilizers
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51-9065750-000





15% & 85%T Coverage Plot "Limited" Lower Scan in Axial "Z" Direction - Limited in Circumferential "e" Direction "MAP" Scan Not Possible Due to Tool Cable Bundle/Lug Interference (Axial Scan – Perpendicular to weld)

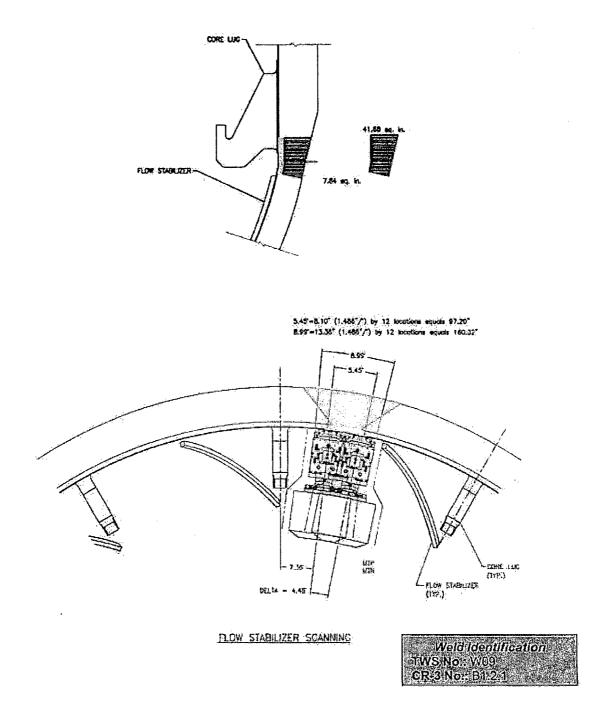
Weld Identification TWS No.: W09 CR-3 No.: B1.2:1

51-9065750-000

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Section E, Tab 2

Page 29 of 53



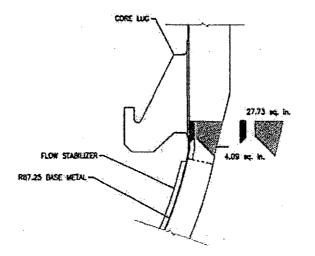
15% & 85%T Coverage Plot "Limited" Lower Scan in Axial "Z" Direction - Limited in Circumferential "e" Direction (Circ Scan – Parallel to weld)

Note: The circumferential extent of the MTP & MTN scons are derived by the average distance traveled by the respective Le., 45° or 70°) beam path. This is shown by the measurements taken from the midpoint of the beam paths.

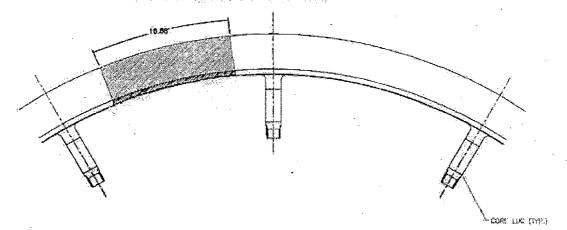
51-9065750-000

Section E, Tab 2

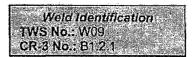
Page 30 of 53



15.85 =25.06" (1.486"/") by 12 locations equals 301.00"



CORE LUG SCANNING

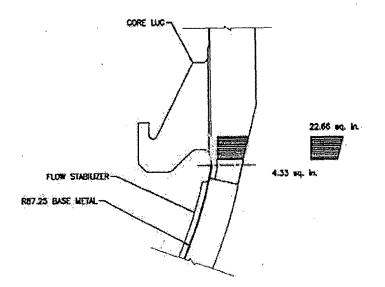


15% & 85%T Coverage Plot "Unlimited" Upper Scan in both Axial "Z" and Circumferential "e" Directions (Axial Scan – Perpendicular to weld)

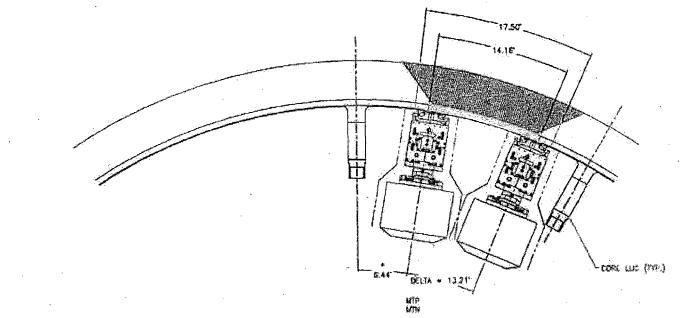
51-9065750-000

Section E, Tab 2

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14,16-21.07" (1.485"/) by 12 locations equals 252.64" 17.50"-26.00" (1.485"/) by 12 locations equals 312.0"



CORE LUG SCANNING

Weld Identification TWS No.: W09 CR-3 No.: B1/2/1

15% & 85%T Coverage Plot "Unlimited" Upper Scan in both Axial "Z" and Circumferential "e" Direction (Circ Scan – Parallel to weld)

Note: The circumferential extent of the MTP & MTP scans are derived by the average distance traveled by the respective i.e., 45° or 70°) beam path. This is shown by the measurements taken from the midpoint of the beam paths:

51-9065750-000

Section E, Tab 2

Page 32 of 53

Coverage Layout & Calculations

Weld Description: Nozzle Bell to Upper Shell ASME Code Item No.: B1.11 CR-3 Weld ID: B1.2.3 TWS Weld Designator: W02

ASME Code Figure No .: IWB-2500-1 AREVA Drawing No.: 8019749

AGGREGATE COVERAGE: 90.0%

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	Angle	Beam	Examined	Examined	Examined	Required	Percent		
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3	700451	CW	See	Notes	6090.9	7194.5	84.7%	Yes	Nozzies.
». 1 4	70L/45L	CCW	Sec	Notes	6090.9	7194.5	84.7%	Yes	Nozzles
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1:8 2	4512/465			Notes	37785.4	43643,6	86:6%	Yes	Nozzles
	45L/45S			Notes	43072.7	43643.6	98.7%	Yes	Nozzlès
	45U/45S			Notes	43072.7	43643.6	98:7%	100 100 100 100	Nozzles
	া অল চাইজি	ও জন্মপ্রাণ		Totals:	37785.4	43643.6	94.7%	Yes	S. C. Starter

Contraction of the second second

Support Charts for Area Examined:

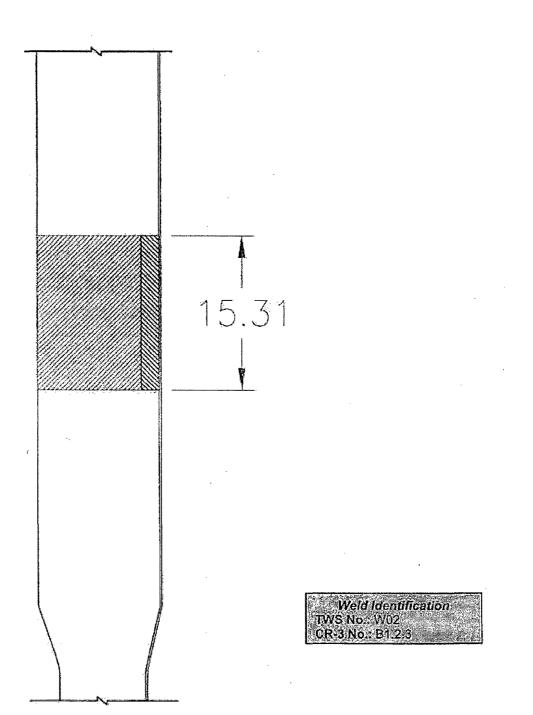
			otal Area to	be Examine	il . States
	· Verticali	Horizon	tal Area	Windotal	(dlamo t
Scan Area	Fleight	15%	A 85% H	2015%	85%
Z-W & W-X	15.31	86.98	527.62	1331.66	8077.86
OUT Z & Z-W	15.31	74.39	451.27	1138.91	6908.94
Y-Z & OUT Z	15,31	73.59	446,44	1126.66	6835.00
X-Y & Y-Z	15.31	86.98	527.62	1331,66	8077.86
OUT X & X-Y	15.31	73.59	446.44	1126.66	6835.00
W-X & OUT X	15.31	74.39	451.27	1138.91	6908.94
			Total	7194.5	43643.6

		STP & STN						
	Vertical	Horizon	tal Area 💦	Total	lolume 👘			
Scan Area 🛶 👘	Height	德洲15%和影	85%	45% 0	85%			
Z-W & W-X	15.31	77.76	524.67	1190-51	8032:70			
OUT Z & Z-W	15.31	60.58	440.12	927,48	6738:24			
Y-Z & OUT Z	15.31	60.58	434 30	927,48	6649.13			
X-Y & Y-Z	15.31	77 76	539.85	1190.51	8265.10			
OUT X & X-Y	15.31	60,58	434,32	927:48	6649.44			
W-X&OUTX	15.31	60.58	440,11	927 48	6738.08			
			Total	6090.9	43072 7			

otal 6090.9 43072.7

		SZP & SZŃ							
	Vertical	Horizon	tal Area	Total.	/olume				
Scan Area	Height	15%	85%	15%	85%				
Z-W & W-X	15.31	78.75	477.66	1205.66	7312.97				
OUT Z & 2-W	15.31	61/30	371.88	938.50	5693,48				
Y-Z & QUT Z	15.31	61.43	372.64	940.49	5705.12				
X-Y & Y-Z	15.81	83.64	501.32	1280.53	7675.21				
OUT X & X-Y	15.31	61.43	372.64	940.49	5705.12				
W-X & OUT X	15.31	61.30	371.88	938.50	5693.48				
			Total	6244.2	37785.4				

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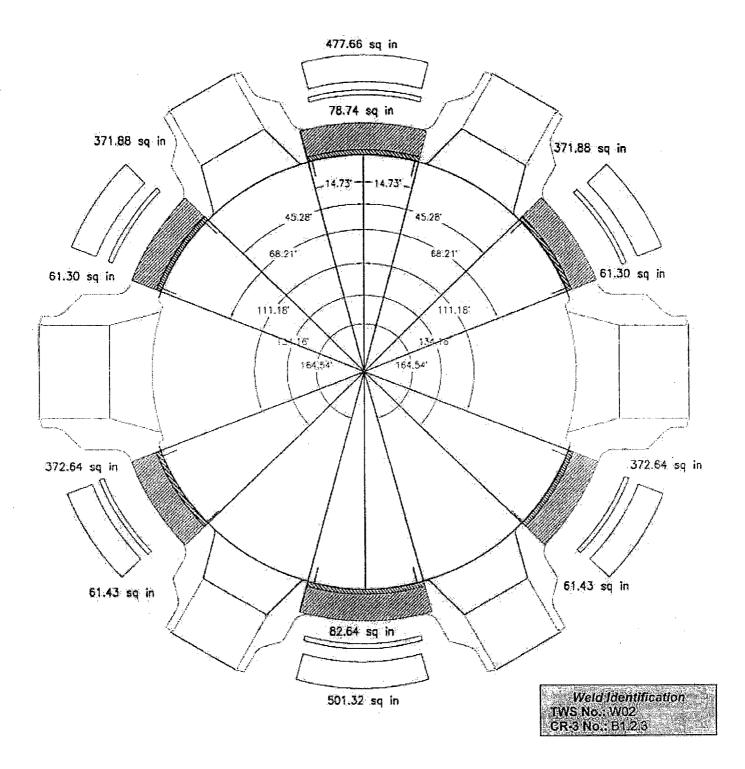
15% & 85%T Coverage Plot Typical Cross Section (Both Scans Axial & Circ)

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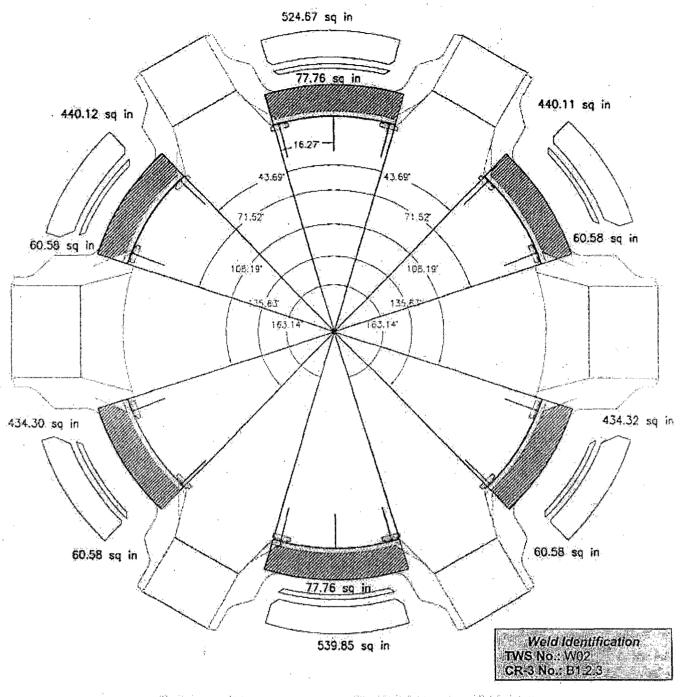


15% & 85%T Coverage Plot (Axial Scan - Perpendicular to weld)

View - Cross Section at Nozzle Centerline Elevation

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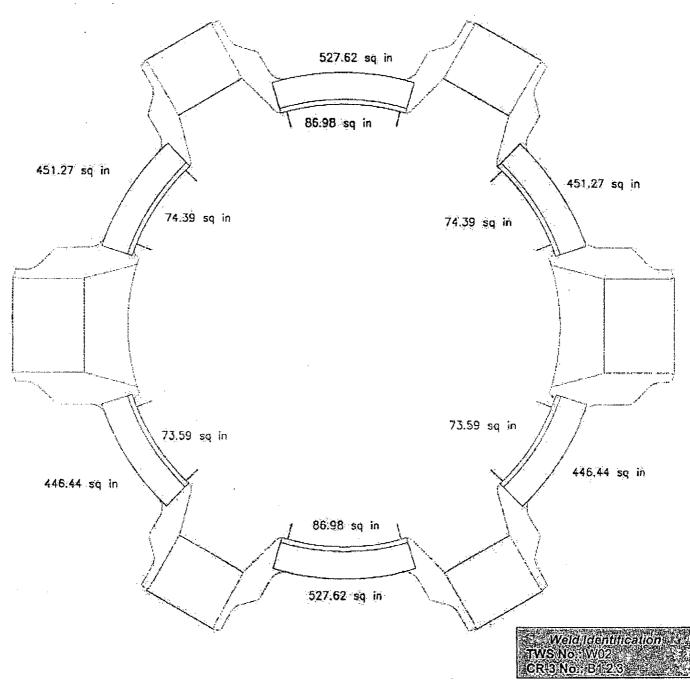
Section E, Tab 2



15% & 85%T Coverage Plot (Circumferential Scan - Parallel to weld)

View – Cross Section at Nozzle Centerline Elevation

Section E, Tab 2





View - Cross Section at Nozzle Centerline Elevation

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Coverage Layout & Calculations

Neld Description: Long Seam Weld CR-3 Weld ID: B1.1.5 & B1.1.6 TWS Weld Designator: W06 & W07

Γ

ASME Code Item No.: B1.12 ASME Code Figure No.: IWB-2500-2 AREVA Drawing No.: 8019749

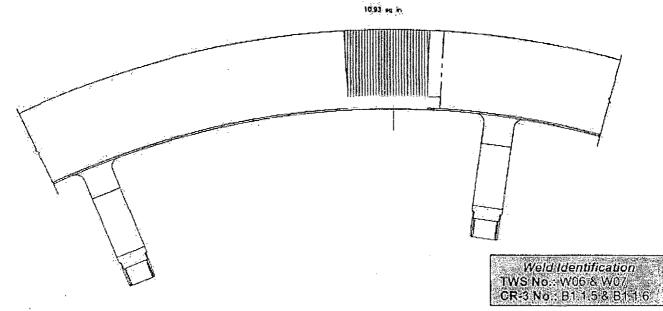
AGGREGATE COVERAGE: 88.1%

Zone Coverage Obtained

liner 1	9 (91:-)	87.2%			uter 85%T:			1	
		Model	Length:	Examina 73.12	tion Volum	Definition			
	Area	Measureme		1.9.14	Volume Ca	iculation	nun marin) ett. 1		
nner 15%T	ry Ea	meason sing		sg. in.	Inner 15%1			930 8	cu.in.
Dute: 85%T				sq. in,	Outer 85%			5531.5	
Limilat	lions	Lir	nits scan b		<u></u>	·	Comper	isation(s)	
Lugs & Flow	Stahilizers	Preventing !	iuli moveme	nt of Head	Ereakir	ng:oirc.sean			aximize scan coverage
								-	
		Examin	ation Cove	ragé Calci	ilations (Tre	ated as Duc	ll Sided Exam	inalion)	
NNER 15	5%T		a ma danin mara						· · ·
· · · · · · · · ·	Exam,		Area.	Length	Volume	Volume			
	Angie	Beam	Examined	Fxamilied	Examined	Required	Percent		
Entry #	(dea.)	Direction	(sq:in)	ansi '	(cu, ini)	(cu: jn:)	Exomities	Linited	Limitations
	70E/45L	Up	712.73		625.3	930.8	67.2%)	Yes	Lugs & Flow Stabilizen
4 <u>2</u> 	70L/45L	Down	12,73	49/12	625.3	930.8	67.2%	Yes	Lugs & Flow Stabilizer
्व बु	70Ê/45L	CW	-12,73	47.03	699.3	930.8	64 4 %	Yes	Lugs & Flow Stabilizer
	70L/45L	COW	12,73	97:08 Totals	599.3 2449.3	930.8 3723.3	64.4% 65.8%	THES:	Lugs & Flow Stabilizer
NHTED O	C0/ T	ardı, yele eşi n			in the state of t		U.S. 6 70	an aidean i an ann a	
OUTER 8	J 70 1								
			Area	น ซีเรียดนี้แก่	مر و المراجع . مراجع المراجع ال	Sandara as			
	Exam.	19 6 22 24		Longth	Volume	Yokime,	an a		
Entry #	Angle (dep.)	Beam Direction	(sq. in)	an.)	Examined (cu. in.)	Required (co. in.)	Percent Examined	Limited	Limitations
Contraction of the second s	450455	Up	75,65	40.12	3715.9	5531.5	67.2%	Yes	Lugs & Flow Stabilizer
	45L/45S	Down	75.65	19.12	3715.9	5531.5	67.2%	Yes	Lugs & Flow Stabilizer
3	451.455	CVI	75.65	47.08	3561.6	5531.5	64.4%	Yes	Lugs & Flow Stabilizer
4	456455	CÓŴ	75.66	47.08	3561.6	5531.5	64.4%	Yes	Lugs & Flow Stabilizer
n. En anter en		and the second secon	an internet at a .	Totals:	14555.1	22126.1	65.8%		
				alculation	s (CW & CC	W Tresled a	is Single Side	d Examinati	on)
NNER 1	5%T (EU	VITATIO	NS)		다. 기관: 1 12	i e li i	· · ·		한 전 교육 방법에 가장 가장 가지 않는 전 성실은 실상 것이 있는 것이 있는 것이다.
					a ta Maria a sa sa sa sa sa sa	and a second			
	Exam.		Area	Longih	Volume	Volume	·		
1995 - 11	Angle	Beam	A		J-Examined		Percent	ar air i sail in ai	
Entry #	(deg.)	Direction	(solin)	(in.)	(cu, in.)	(cu, in,)	Examined	Limited	Limitations
1	70U/45L	Un	1093	21.69	297.1	930,8	25.5%	Yes	Lugs & Flow Stabilizer
384	701/451	Dówn CW & CCM	(10,99) 7,79	24.69	237.1 125.0	930.8 930.8	25.5% 13,4%	Yes	Lugs & Flow Stabilizer Lugs & Flow Stabilizer
3044	NULLYOL	1344 Brighter		16.05 Totals:	599.2	2792.5	21.5%	19 69	Ende of Linda Digramites
	50/ T /1 1	MITATIO	NCA			(&)) 3 & 10	· · · · · · · · · · · · · · · · · · ·	in the second	2017 - 10 10 - 10 - 10 - 10 - 10 - 10 - 10 -
WUTER C	19 101 (EI	WILLIA LING							소작공항한 원이 너 빛감을 얻어 있다. 기억님 이 것은 제가 바람이 다.
1			1000 1000 1000	1	an far an	W. Finthermore		et de la c	
	Exam.	10 2 2 2 2 2	Area	Length	Volume	Volume	Dare		
Entry	Angle	Beam	a start a start a start		Examined	· · · · · · · · · · · · · · · · · · ·	Percent Examined	Limited	Limitations
	(deg.) 45L/45S	Direction	<u>(\$0.14.)</u> 64,93	21:69	(ou, In,) 1408:5	<u>(cu, kt)</u> 5531.6	25.5%	Yes	Lugs & Flow Stabilize
2	450455	Down	64.94	21/69	1408.5	5531.5	25.5%	Yes	Lugs & Flow Stabilize
		CW & CCV			1036.8			233.214	Lugs & Flow Stabilize
384	45 445*	1.00 . 1.1	64.60	16:05	1036.8	5531.5	18.7%	Yes	AND THE PLANMAN STRATCHER

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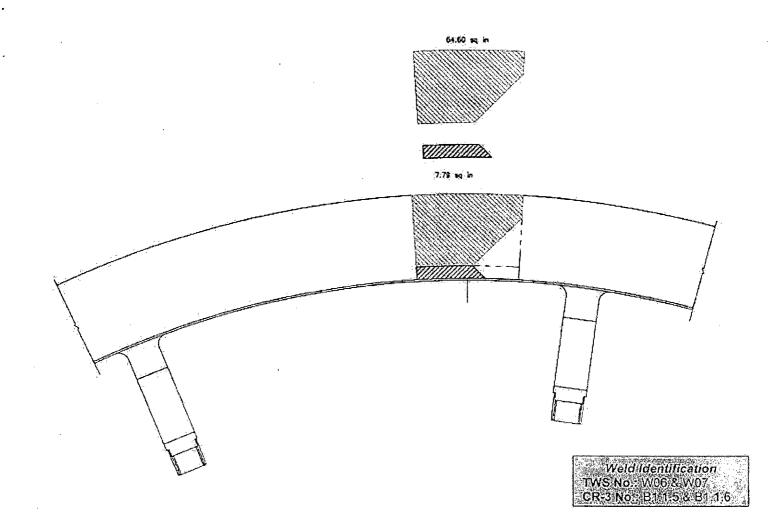
15% & 85%T Coverage Plot (Axial Scan - Parallel to weld)

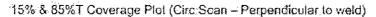
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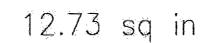


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75.65 sq in



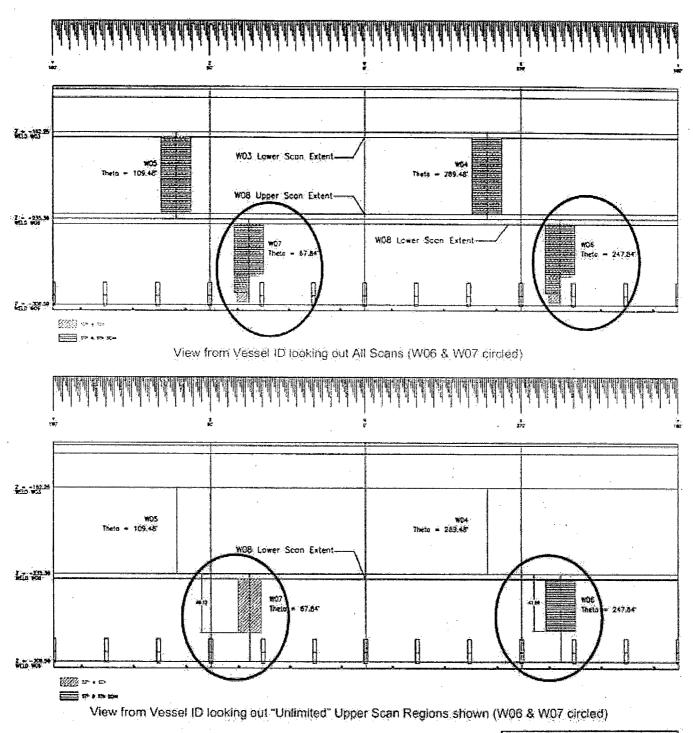
15% & 85%T Total Cross Sectional Area

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Weld Identification TWS No.: W06 & W07 CR-3 No.: B1 1.5 & B1 1.6

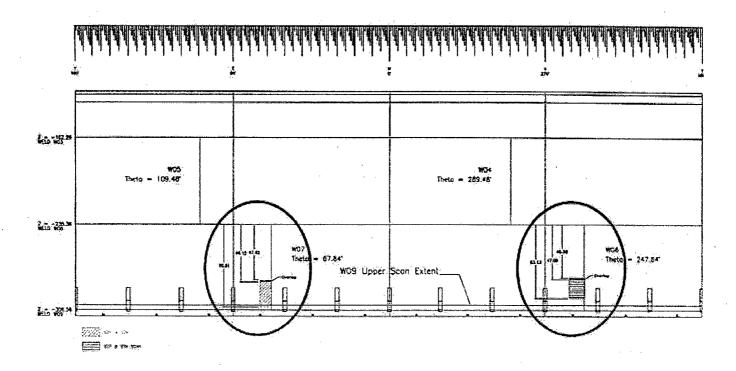


Weld Identification TWS No.: W06 & W07 CR-3 No.: B1 1 5 & B1 1 6

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View from Vessel ID looking out "Limited" Lower Scan Region (W06 & W07 circled)

Weld Identification TWS No.: W06& W07 CR-3 No.: B1.1.5 & B1.1.6

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NUMBER OF STREET

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Coverage Layout & Calculations

Neld Description:Outlet Nozzle to Shell @ X axis & Z axisASME Code Item No.:B3.90ASME Code Figure No.:IWB-2500-7CR-3 Weld ID (TWS Weld Designator):B1.4.7A (W15) and B1.4.8A (W23)AREVA Drawing No.:8019749

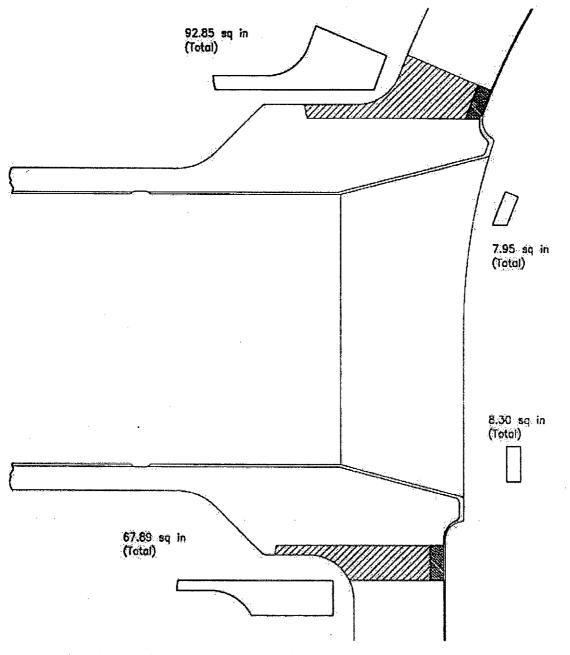
AGGREGATE COVERAGE: 69.8%

			Zone	Coverag	e Obtain	ed	<u> </u>	
Innerd	5%T:	39.6%	Q	uter 85%T:	100.0%			
			Exami	nation Volu	ime Definit	lon		ennet filte en en stille Britensinis sign sinner in som
	Area M	easurement		Volume Ca	lculation			·
Area Me	asurement	not calculated for n	ozzles.	Inner 15%T Outer 85%	2		1300.0 c 12859:2 c	
Limita	tions	Limits sca	n by:	A Martin Contractor Contractor Contractor	<u></u>	Compe	nsation(s)	
Ye	is.	Weld/scan surfac	e geometry	;	с с ,7:		a shah a t	*
	·				•			
		Examination Co	verage Ca	lculations (Treated as	Dual Sided E	xamination)	
NNER 1	5%T							
MAR a charair i i	Exam.		Lonath	Volume	Volume			
	Angle	Beam	Examined	Examined	Required	Percent		
Entry #	(degr)	Direction	(degs)	(où in)	(cu. in)	Examined	Limited	Limitations
<u></u>	70L/45L	Bore: Radial Out	360	1300.0	1300.0	100.0%	Yes	4.(1) M(\$2(10)70
2	70L/45L	RVID: Radial In	360	401,6	1300.0	30.9%	Yes	
3	70E/45L	CW.	360	180.0	1300.0	13.8%	Yes	· .*
3	70L/45L	ccw	360	180.0	1300.0	13 8%	Yes	
			Totals:	2061.6	5200.0	39.6%	n dan series	
DUTER 8	C0/T							
ZUTERC	10/01			· · · ·				2
	a to an a start of			ر الع محمد مع كرك مع ال	1 here in 1999			· · ·
ч., 	Exam.		Length	Volume	Volume			
	Angle	Beam	Examined	Examined	Required	Percent	A start of the	
Enloy #	(deg.)	Direction	(in)	(cu. la.)	(cu, In)	Examined	Limited	Limitalions
	15L/45S	Bore: Radial Out	360	12659.2	12859.2	100.0%	No	
an a	n agus shika Nga kasar			の必要があって。 人の表示。2月 ~		문 가슴에게 가져있는. 실험		
	n se la serie	an Ann	a and				an an tha an	100 C 100 C 100 C
andra an taona da ta Na taona da t			Totals:	12859.2	12859.2	100.0%		

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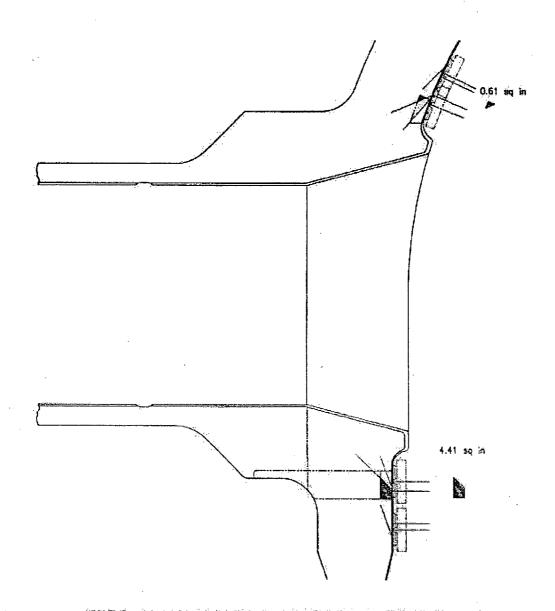
15% & 85%T Coverage Plot (Radial Scan – Perpendicular to weld from Nozzle Bore)

Weld/Identification CR3 No. (TWS No.): B1.47A (W15), B1.4.8A (W23)

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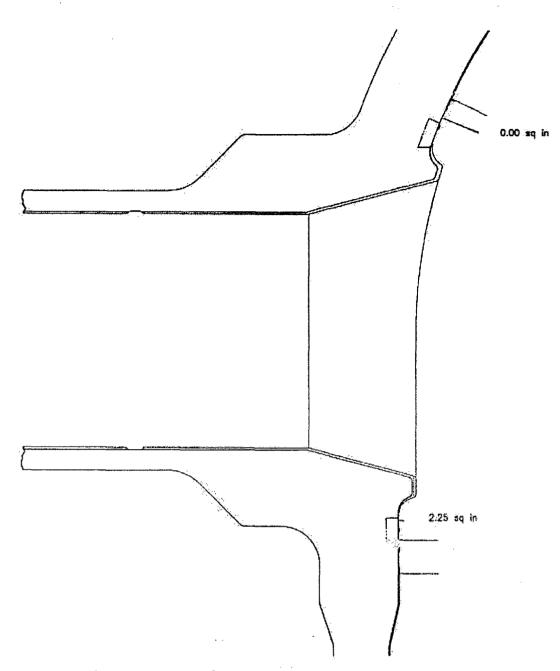
15%T Coverage Plot (Radial Scan – Perpendicular to weld from Shell ID) Beam Direction toward Bore ID

> Weld Identification (CR3 No. (TWS No.): B1.4.7A (W15): B1.4.8A (W23)

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15% T Coverage Plot (Circumferential Scan - Parallel to weld from Shell ID)

Weld Identification CR3 No. (TWS No.): B14.7A (W15), B1.4.8A (W23)

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