Summary of Stress Analysis Results for the US-APWR Reactor Coolant Loop Branch Piping

Non-Proprietary Version

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Revision History

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Abstract

This report provides a summary of the stress analyses results of Reactor Coolant Loop (RCL) Branch Piping in accordance with MHI's commitment letter (Reference 11) concerning the content of the Technical Report.

From the results summarized in this report and a review of the component design drawings, it is concluded that the US-APWR RCL Branch Piping satisfies all of the requirements of the Design Specification (Reference 1) for structural integrity, operability, and safety.

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List of Acronyms

The following list defines the acronyms used in this document.

SG	Steam Generator
RCL	Reactor Coolant Loop
RV	Reactor Vessel
RCP	Reactor Coolant Pump
PZR	Pressurizer
ACC	Accumulator
RHRS	Residual Heat Removal System
DVI	Direct Vessel Injection
CVCS	Chemical and Volume Control System
BAC	Bounding Analysis Curve
SRSS	Square Root Sum of the Squares
MCP	Main Coolant Pipe
FRS	Floor Response Spectrum
IC	Inner Concrete
CV	Containment Vessel
FW	Feedwater
MS	Main Steam
LBB	Leak-Before-Break
DBPB	Design Basis Pipe Break
ECCS	Emergency Core Cooling System
NPS	Nominal Pipe Size
N/A	Not Applicable

1.0 INTRODUCTION

This Stress Analysis Technical Report is a non-certified version of the ASME Design Report for the US-APWR RCL Branch Piping that has been prepared in support of the US-APWR DCD Review process. The content of this report follows the ASME guidelines for Design Reports (Section III Division 1 Appendix C) (Reference 5).

Design loads (pressure, deadweight and seismic inertia loads including loads associated with thermal expansion anchor motion and Seismic Anchor Motion (SAM)) used for pipe stress analysis were computed based on the conditions specified in the Design Specification (Reference 1). The thermal stress specified in Bulleting 88-08 was not considered since the valve system configurations and valve disk position adjustments were made to assure that a thermal oscillation would not be generated as described in DCD 3.12.5.9. As for the pressurizer surge line thermal stratification specified in Bulleting 88-11, structural analysis was carried out by setting the thermal stratification profile based on the thermal flow analysis results.

This Technical Report meets the requirements of the ASME Code Section III Division 1 NCA-3551.1 (Reference 5) by providing a summary of results and conclusions based upon detailed analyses that demonstrate the validity of the RCL Branch Piping component to meet the requirements of the Design Specification (Reference 1).

For the design of Class 1 piping (i.e. NB-3600 and NC-3600), the 1992 Edition of ASME Section III was used as required by 10CFR50.55a (b) (1) (iii).

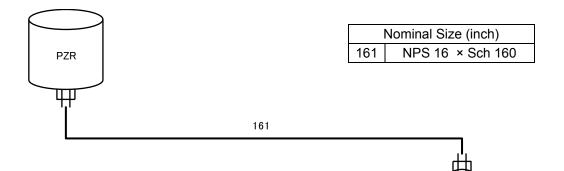
The scope of this Technical Report includes the piping systems and components (PSC) of the following RCL Branch Piping whose jurisdictional limits are identified in Figures 1.0-1 through 1.0-16. The selection of the RCL Branch Piping is consistent with MHI's intent to complete the Stress Analyses of "Risk Significant" PSCs prior to construction, and to allow NRC's audit during the DCD review phase.

- RC01 Pressurizer Surge Line
- RC02 Pressurizer Spray Line
- RC03 Pressurizer Safety Depressurization Valve Line
- RC04 Pressurizer Safety Valve Line
- RH01 and RH02 RHRS Suction Loop A and B Lines
- SI01and SI02 Accumulator Loop A and B Lines
- SI05 and SI06 DVI A and B Lines
- CS01 CVCS Charging Line
- CS02 CVCS Let Down Line
- CS04 through CS07 CVCS Seal Injection A, B, C and D Lines

For each of the above Branch Piping, the Scope of the Report provides the following:

- A Summary of the Specification
- The Loads and Load Combinations
- The structural model of the piping including supports, flanges, valves, equipment and penetrations.

- The results of the piping analysis in accordance with the piping Design Specification (Reference 1)
- A review of the calculated stresses including effects of stress intensification, demonstration of ASME III acceptability, and LBB applicability checks for LBB applied piping





	Nominal Size (inch)		
61 NPS 6 × Sch 160			
41 NPS 4 × Sch 160			
31 NPS 3 × Sch 160			
341 NPS 3/4 × Sch 160			

B-MCP H/L

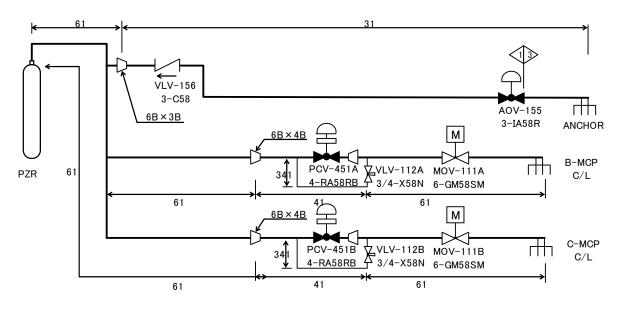


Figure 1.0-2 RC02 : Pressurizer spray line

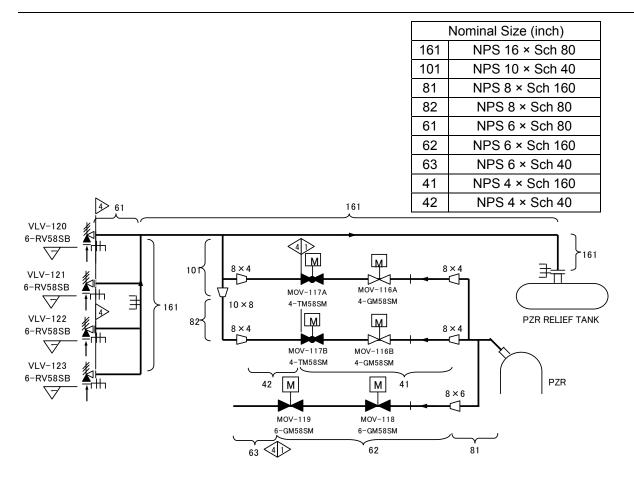


Figure 1.0-3 RC03: Pressurizer safety depressurization valve line

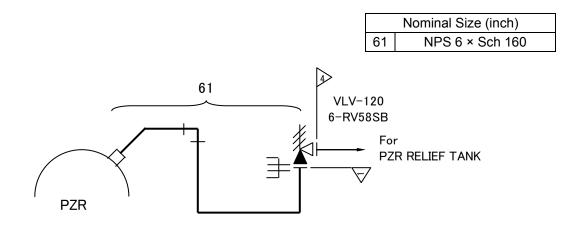


Figure 1.0-4 RC04: Pressurizer safety valve line

Nominal Size (inch)			
101	101 NPS 10 × Sch 160		
102 NPS 10 × Sch 80			
81 NPS 8 × Sch 160			
61 NPS 6 × Sch 80			
41 NPS 4 × Sch 160			
21	NPS 2 × Sch 160		

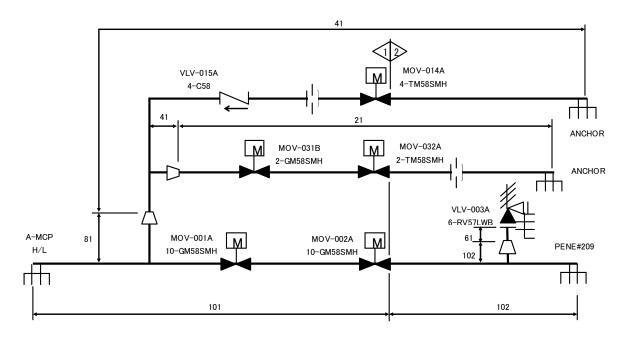


Figure 1.0-5 RH01: RHR suction loop A line

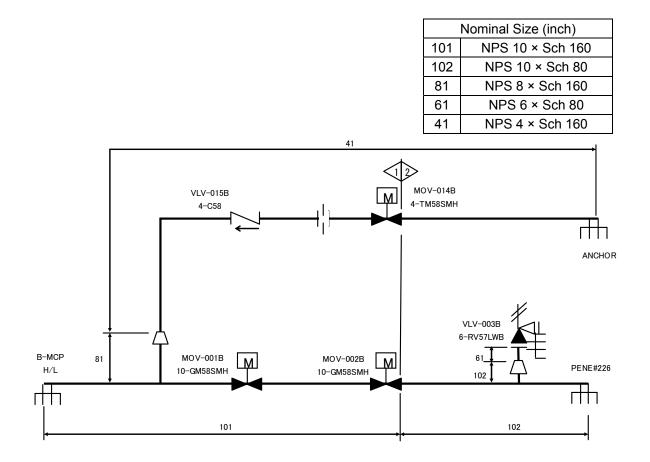


Figure 1.0-6 RH02: RHR suction loop B line

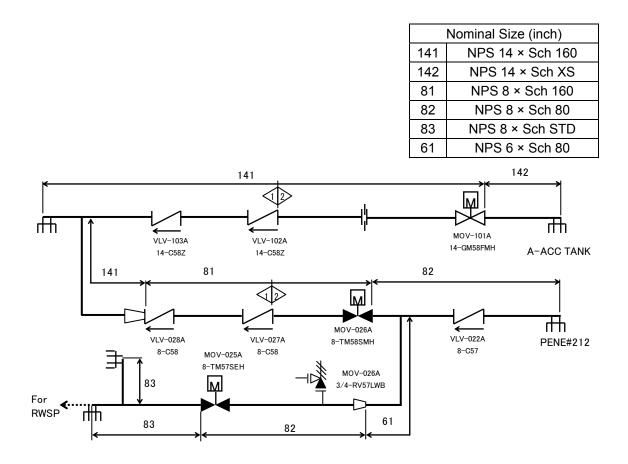


Figure 1.0-7 SI01: Accumulator loop A line

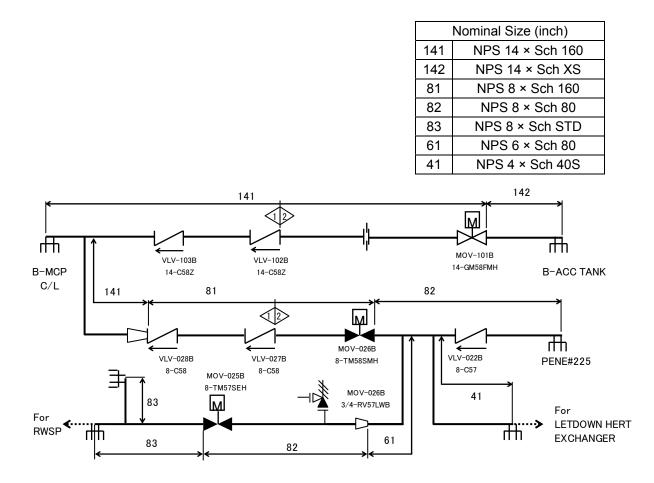
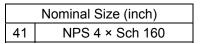
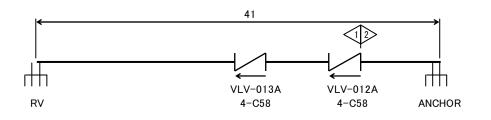


Figure 1.0-8 SI02: Accumulator loop B line







Nominal Size (inch)		
41	NPS 4 × Sch 160	

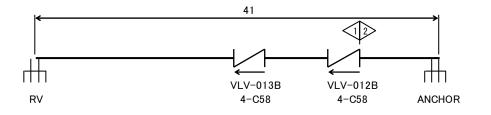
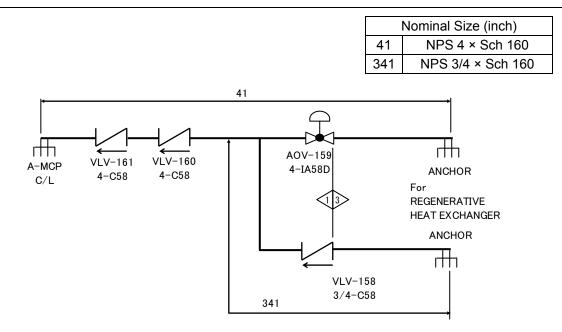


Figure 1.0-10 SI06: DVI B line





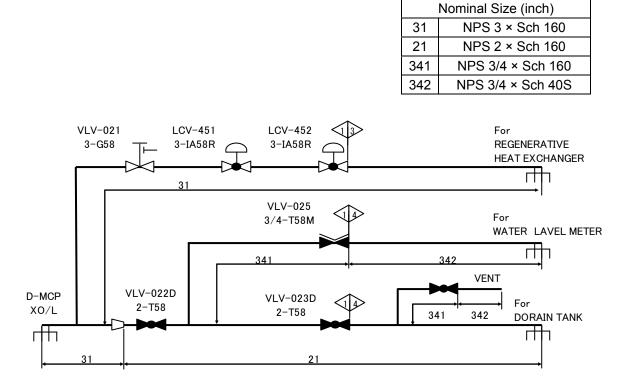


Figure 1.0-12 CS02: CVCS let down line

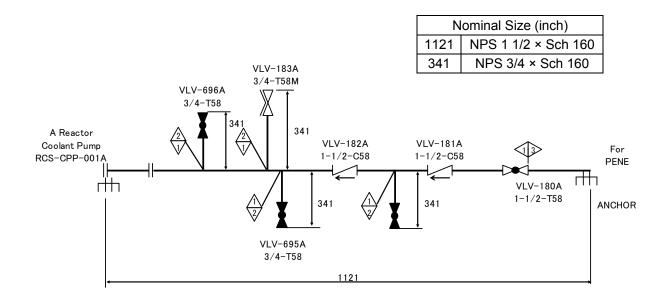


Figure 1.0-13 CS04: CVCS seal injection line (A-RCP)

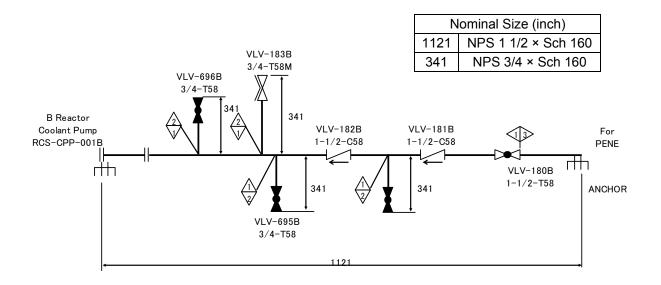


Figure 1.0-14 CS05: CVCS seal injection line (B-RCP)

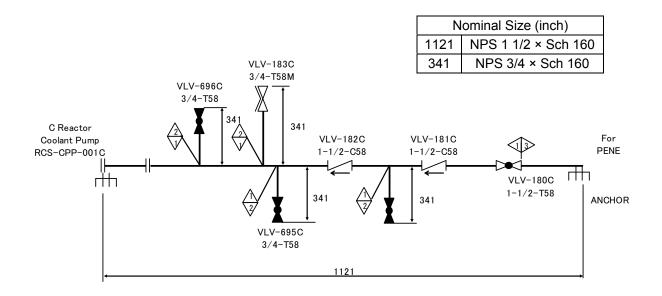


Figure 1.0-15 CS06: CVCS seal injection line (C-RCP)

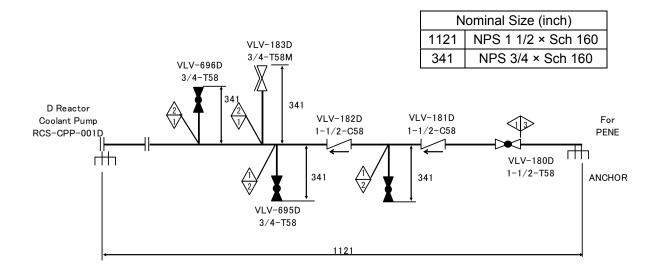


Figure 1.0-16 CS07: CVCS seal injection line (D-RCP)

2.0 SUMMARY OF RESULTS

The structural analysis results for each RCL Branch Piping are summarized in Section 11 and Appendix-1. The most limiting results in each evaluation are listed in Table 2-1 below.

Appendix	Evaluated Part	Max Stress / Allowable Ratio	Highest Fatigue Usage Factor	LBB Evaluation
App. 1-1	RC01 Pressurizer Surge Line	$\left(\right)$		-
App. 1-2	RC02 Pressurizer Spray Line			
App. 1-3	RC03 Pressurizer Safety Depressurization Valve Line			
App. 1-4	RC04 Pressurizer Safety Valve Line			
App. 1-5	RH01 RHR Suction Loop A Line			
App. 1-6	RH02 RHR Suction Loop B Line			
App. 1-7	SI01 Accumulator Loop A Line			
App. 1-8	SI02 Accumulator Loop B Line			
App. 1-9	SI05 DVI A Line			
App. 1-10	SI06 DVI B Line			
App. 1-11	CS01 CVCS Charging Line			
App. 1-12	CS02 CVCS Let Down Line			
App. 1-13	CS04 CVCS Seal Injection A Line			
App. 1-14	CS05 CVCS Seal Injection B Line			
App. 1-15	CS06 CVCS Seal Injection C Line			
App. 1-16	CS07 CVCS Seal Injection D Line			

Table 2-1	Summar	y of Most	Limiting	Results
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3.0 CONCLUSIONS

The US-APWR RCL Branch Piping was designed to the requirements of the ASME Boiler and Pressure Vessel Code, 1992 Edition including the 1992 Addenda for the Design, Service Loadings, Operating Conditions, and Test Conditions as specified in the Design Specification (Reference 1).

From the results summarized in this report, it is concluded that the US-APWR RCL Branch Piping satisfy all of the requirements of the Design Specification (Reference 1) for structural integrity, operability, and safety, and it is confirmed that pressurizer surge line satisfies the LBB criteria using Bounding Analysis Curves (BACs) as described in Appendix 1-1.

4.0 NOMENCLATURE

Table 4-1	Symbol	and	Definition
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Symbol	Unit	Definition
S _m	psi	Design Stress Intensity
Sy	psi	Yield Stress
Sc	psi	Allowable Stress at minimum (cold) temperature
S _h	psi	Allowable Stress at maximum (hot) temperature
S _A	psi	Allowable Stress Range for Expansion Stress
DL	-	Dead Load (The dead weight consists of the weight of the piping, insulation, and other loads permanently imposed upon the piping)
Р	-	Design Pressure
P_R	-	Range of Service Pressure
P_M	-	Maximum Service Pressure
TH _{MTL}	-	ASME Service Level A (Normal) and Service Level B (Upset) Miscellaneous Thermal Loads with Thermal Stratification and Thermal Cycling Effects
TH _{DISCON}	-	Thermal Discontinuity Loads
TH _{GRAD}	-	Thermal Radial Gradient Loads
L _{DM}	-	Design Mechanical Loads
L _{DFN}	-	ASME Service Level A (Normal) Dynamic Fluid Loads associated with hydraulic transients such as relief/safety valve open or water/steam hammer
L _{DFU}	-	ASME Service Level B (Upset) Dynamic Fluid Loads associated with hydraulic transients such as relief/safety valve open or water/steam hammer
L _{DFE}	-	ASME Service Level C (Emergency) Dynamic Fluid Loads associated with hydraulic transients such as relief/safety valve open or water/steam hammer
L _{DFF}	-	ASME Service Level D (Faulted) Dynamic Fluid Loads associated with hydraulic transients such as relief/safety valve open or water/steam hammer
1/3 SSE	-	Design Condition & Level B Service Loading Earthquake (i.e. OBE)
SSEI	-	Safe-Shutdown Earthquake Inertia Loads
SSEA	-	Safe-Shutdown Earthquake Anchor Loads
BS	-	Building Settlement
DBPB	-	Design Basis Pipe Breaks, include LOCA and non-LOCA
LOCA	-	Loss-of-Coolant Accident

5.0 ASSUMPTIONS AND OPEN ITEMS

5.1 Assumptions

The basic modeling assumptions from the detailed analyses are as follows:

- 1. Because the valve weight and rigidity have not been set by the valve specifications or the procurer, data was used for a similar valve of the earlier APWR plant.
- 2. Because the rigidity of supports has not been set by the procurer, the value was set on the basis of a trial design that was consistent with the earlier APWR plant.

5.2 Open Items

There are no open items in this Technical Report.

6.0 ACCEPTANCE CRITERIA

The stress limits acceptance criteria for RCL Branch piping greater than 1 inch are specified in NB-3650 and for RCL Branch piping equal to 1 inch or smaller than 1 inch are specified in NC-3650 of ASME Section III. Table 6-1 lists the stress limits for RCL Branch piping (greater than 1 inch) and Table 6-2 lists the stress limits for RCL Branch piping (1 inch or smaller than 1 inch).

Condition	Service Level	Category	Loading	Equation (NB-3650) ⁽⁴⁾	Stress Limit ⁽⁴⁾
Design	-	Primary Stress	P, DL, L _{DM} (including L _{DFN})	Eq. 9 NB-3652	1.5 S _m
		Primary + Secondary Stress Intensity Range (SIR)	(3) P _R , TH _{MTL} , TH _{DISCON} , L _{DFN} , L _{DFU} , SSEI, SSEA	Eq. 10 NB-3653.1	3 S _m
		Peak SIR	P _R , TH _{MTL} , TH _{DISCON} , TH _{GRAD} , L _{DFN} , L _{DFU} , SSEI, SSEA	Eq. 11 NB-3653.2	
Normal		Thermal Bending SIR	(2) TH _{MTL}	Eq. 12 NB-3653.6(a)	3 S _m
/Upset	A/B	Primary + Secondary Membrane + Bending SIR	(2) P _R , TH _{DISCON} , L _{DFN} , L _{DFU} , SSEI, SSEA	Eq. 13 NB-3653.6(b)	3 S _m
		Alternating Stress Intensity (Fatigue)	P _R , TH _{MTL} , TH _{DISCON} , TH _{GRAD} , L _{DFN} , L _{DFU} , SSEI, SSEA	NB-3653.3 NB-3653.4 NB-3653.5 NB-3653.6(c)	
		Thermal Stress Ratchet	TH _{GRAD} (linear)	NB3653.7	
Upset	В	Permissible Pressure	Pressure P _M		1.1 <i>Pa</i>
		Primary Stress	P_{M} , DL, L_{DFU}	NB-3654.2	$Min(1.8 S_m, 1.5 S_y)$
Emergency	С	Permissible Pressure	P_M	NB-3655.1	1.5 <i>Pa</i>
		Primary Stress	P _M , DL, L _{DFE}	NB-3655.2	Min(2.25 S _m , 1.8 S _y)
		Permissible Pressure	P _M	NB-3656(b)	2 Pa
Faulted	D	Primary Stress	P _M , DL, L _{DFF} ⁽¹⁾ , SSEI, DBPB ⁽¹⁾	NB-3656(a) NB-3656(b)	Appendix-F or Min(3 S _m ,2 S _v)
Faulted	D	Secondary Stress	SSEA	(5)	6 S _m ⁽⁵⁾

Notes:

1. Dynamic loads are to be combined considering timing and causal relationships. SSE and DBPB is combined using the SRSS method.

 The Thermal and Primary plus Secondary Membrane plus Bending Stress Intensity Ranges (Equations 12 and 13) need only be calculated for those load sets that do not meet the Primary plus Secondary Stress Intensity Range (Equation 10) allowable.

3. The earthquake inertial and anchor movement loads used in the Level B Stress Intensity Range and Alternating Stress calculations (Equations 10, 11, 13 and 14) is taken as 1/3 of the peak SSE inertial and anchor movement loads or as the peak SSE inertial and anchor movement loads. If the earthquake loads are taken as 1/3 of the peak SSE loads then the number of cycles to be considered for earthquake loading is to be 300 as derived in accordance with Appendix D of Institute of Electrical and Electronic Engineers Standard 344-2004 (Reference 6) If the earthquake loads are taken as the peak SSE loads then 20 cycles of earthquake loading is considered. Also, see Note 2.

4. ASME Boiler and Pressure Vessel Code, Section III (Reference 7).

MUAP-09011-NP (R0)

5.

	$\frac{C_2 D_o M_{AM}}{2I} \le 6$	$0.0S_m$ and $\frac{F_{AM}}{A_M} \le S_m$
where		
	Do	= Pipe Outer Diameter
	1	= Pipe Moment of Inertia
	A _M	= Area of cross-section of the pipe
	M _{AM}	= Range of resultant moment due to SSEA
	F _{AM}	= Amplitude of longitudinal force due to SSEA
	Sm	= Allowable design stress intensity value

The use of $6S_m$ limit assumes elastic behavior of the entire piping system. In the case of unbalanced systems, the design is modified to eliminate unbalance or the piping is qualified by using an allowable limit of $3S_m$.

Condition	Service Level	Loading	Equation (NC-3650)	Stress Limit ⁽³⁾
Design	-	P, DL	Eq. 8 NC-3652	1.5 S _h
		P _M , DL, L _{DFN} , L _{DFU} ,	Eq. 9 NC-3653.1	Min(1.8 S _h , 1.5 S _y)
Normal	A /D	TH _{MTL}	Eq. 10 NC-3653.2(a)	(1) S _A
/Upset	A/B	BS	Eq. 10a NC-3653.2(b)	3Sc
		P _M , DL, TH _{MTL}	Eq. 11 NC-3652.2(c)	$S_h + S_A $ ⁽¹⁾
Emergency	С	P _M , DL, L _{DFE} ,	Eq. 9 NC-3654	Min(2.25 S _h , 1.8 S _y)
Foulted	D	P _M , DL, L _{DFF} , SSEI, DBPB	Eq. 9 NC-3655	$Min(3 \ S_h, 2 \ S_y)$
Faulted	D	SSEA	(5)	(5) 6S _h

Table 6-2 RCL Branch Piping Stress Limits (1 inch or smaller than 1 inch piping)

Notes:

- 1. Stresses must meet the requirements of either Equation 10 or 11, not both.
- 2. If, during operation, the system normally carries a medium other than water (air, gas, steam), sustained loads should be checked for weight loads during hydrostatic testing as well as normal operation weight loads.
- 3. ASME Boiler and Pressure Vessel Code, Section III(Reference 7)
- 4. Dynamic loads are combined by the SRSS method.

5.

$$\frac{C_2 D_o M_{AM}}{2I} \le 6.0 S_h \text{ and } \frac{F_{AM}}{A_M} \le S_h$$

where

Do	= Pipe Outer Diameter
1	= Pipe Moment of Inertia
A _M	= Area of cross-section of the pipe
Мам	= Range of resultant moment due to SSEA
F _{AM}	= Amplitude of longitudinal force due to SSEA
Sh	= Allowable stress value

The use of $6S_h$ limit assumes elastic behavior of the entire piping system. In the case of unbalanced systems, the design is modified to eliminate unbalance or the piping is qualified by using an allowable limit of $3S_h$.

7.0 DESIGN INPUT

The piping was designed based on the design inputs described in the Design Specification (Reference 1) and the documents listed as follows:

- 1. N0-CF00004 Revision 0 "Piping Design Criteria" (Reference 2)
- 2. N0-GB00005 Revision 0 "Input Package of Stress Analysis of RCL Branch Piping and Main Steam Piping" (Reference 3)
- 3. N0-EE12001 Revision 0 " Class 1 Equipment Design Transients" (Reference 4)

8.0 LOAD AND LOAD COMBINATIONS

8.1 Loadings

8.1.1 Design Temperature and Design Pressure

The Class 1 Piping Design Temperature and Design Pressure are as shown in Table 8.1-1.

Table 8.1-1 Design Temperature and Design Pressure

Design Temperature (°F)	Design Pressure (psi)
650	2485

8.1.2 Sustained Loads

The weight of the piping system, its contents, any insulation and in-line equipment, and any other sustained loads identified in the Design Specification (Reference 1) were considered in the piping analysis. The mass contributed by the support was included in the analysis when it was greater than 10% of the total mass of the adjacent pipe span.

8.1.3 Thermal Expansion Loads

The effect of linear thermal expansion range during various operating modes was considered along with thermal movements of terminal equipment nozzles, anchors, or restraints (thermal anchor movements) corresponding to the operating modes. The stress free temperature was taken as 70°F.

8.1.4 Thermal Stratification Loads (for Pressurizer surge line)

The thermal stratification stress was generated by forming the thermal stratification in pipe fluid by switching from out-surge to in-surge or from in-surge to out-surge.

At the normal condition, the thermal stratification was not formed at the initial condition of the 8 gpm out-surge.

When the transient starts with an out-surge condition, the thermal stratification will not be formed. When the transient starts with an in-surge condition, the thermal stratification will be formed by shifting from the initial condition of the 8 gpm out-surge to in-surge.

When the transient is finished with an in-surge condition, the thermal stratification will be formed by shifting to the normal condition of the 8 gpm out-surge. When the transient is finished with an out-surge condition, the thermal stratification will not be formed because the out-surge condition is maintained.

The profile of the thermal stratification used in the analysis is shown in Figure 8.1-1.

Figure 8.1-1 Thermal Stratification Profile

8.1.5 Earthquake Loads

The effects of inertial loads and anchor movements due to SSE are considered as Service Level D loads in the design of piping. Fatigue effects due to earthquake loads are discussed in Section 9.5.

8.1.6 Fluid Transient Loads

The pressurizer safety valve and safety depressurization valve thrust loads are set in motion by the rapid actuation of valves. These loads are functions of valve opening, flow rate, flow area, and fluid properties.

8.1.7 Design Basis Pipe Break Loads

US-APWR has applied the leak-before-break (LBB) methodology. As a result the main coolant piping (MCP) break and surge line break dynamic evaluations were eliminated. The postulated pipe break events that were evaluated for the reactor coolant system branch piping are as follows.

- Hot Leg Branch Line break at the 10 inch Schedule 160 Residual Heat Removal (RHR)/ Safety Injection (SI) line nozzle
- Cold Leg Branch line break at the 14 inch Schedule 160 accumulator line nozzle
- Feedwater Line break at the SG FW nozzle
- Main Steam Line break at the SG MS nozzle

The following portions must be protected against mechanical loads of the LOCA and secondary side pipe rupture (MS line break and FW line break).

a. LOCA

- (a) Intact loop including branch piping and support components.
- (b) Intact main coolant pipe leg of the affected loop, SG support components and RCP support components in order to maintain the flow path.
- (c) Safety injection line connected to intact leg of affected loop in order to maintain safety injection.

(d) MS line and main FW line in order to prevent simultaneous rupture of secondary side.

b. All of the primary side must be protected against secondary side pipe rupture.

The information for the above types of piping is summarized in Table 8.1-2. For all of the displacements during accidents marked with "A" in Table 8.1-2, a factor of two margin was conservatively considered for dynamic effects. Forced displacements were assumed at the piping nozzle. Both translational and rotational directions were considered.

8.1.8 Design Transients

The design transient conditions for each system are presented in the tables listed below.

Pressurizer surge line	Table 8.1-3
Pressurizer spray line	Table 8.1-4
Pressurizer safety depressurization valve line	Table 8.1-5
Pressurizer safety valve line	Table 8.1-6
RHR suction loop A line	Table 8.1-7
RHR suction loop B line	Table 8.1-8
Accumulator line	Table 8.1-9
DVI line	Table 8.1-10
CVCS charging line	Table 8.1-11
CVCS let down line	Table 8.1-12
CVCS seal injection line	Table 8.1-13

Table 8.1-2 Application of Accidental Load (Displacement) for each piping system

Evaluated	Connected	Location of accident									
Line	Component	Break loop (loop occurred accident)			:)	Intact loop					
		Break at Hot-leg	Break at Cold-leg	RCP rocked rotor	MS break	FW break	Break at Hot-leg	Break at Cold-leg	RCP rocked rotor	MS break	FW break
RC01	Hot-leg, PZR	(10101					10101		
RC02	Cold-leg, PZR										
RC03	PZR										
RC04	PZR										
RH01	Hot-leg										
RH02	Hot-leg										
SI01	Cold-leg										
SI02	Cold-leg										
SI05	RV										
SI06	RV										
CS01	Cold-leg										
CS02	Cross-Over-leg										
CS04	RCP										
CS05	RCP										
CS06	RCP										
CS07	RCP										

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Table 8.1-3 Pressurizer surge line design transients (1/3)

.evel A			Pofe	ranca		
Mark	Transient	Occurrence -	Reference Document Fig. or Table		Remark	
I-a	Plant heat-up (100F/h)	120	Becamon	Fig. I-1		
	Plant cooldown (200F/h, 2235~400psig)	120		Fig. I-2		
I-b-2	Plant cooldown (200F/h, lower than 400psig)	120		Fig. I-2		
I-c-1	Ramp load increase between 15% and 100% of full power (5% of full power per minute)	600		Fig. I-3		
I-c-2	Ramp load increase between 50% and 100% of full power (5% of full power per minute)	19, 200		Fig. I-4		
I-d-1	Ramp load decrease between 15% and 100% of full power (5% of full power per minute)	600		Fig. I-5		
I-d-2	Ramp load decrease between 50% and 100% of full power (5% of full power per minute)	19, 200	Fig. I-6			
l-e	Step load increase of 10% of full power	600		Fig. I-7		
l-f	Step load decrease of 10% of full power	600	Def 4	Fig. I-8		
l-g	Large step load decrease with turbine bypass	60	Ref. 4	Fig. I-9		
l-h	Steady-state fluctuation and i) Steady-state fluctuation	1×10 ⁶		_	P _p ±50psi, T _{hot} , T _{cold} , T _{ave} ±3.1F	
	load regulation ii) Load regulation	8×10⁵		Table 4		
l-i	Main feedwater cycling	2, 100		Fig. I-10		
l-j	Refueling	60		Fig. I-11	Water is replaced in 10 minutes.	
l-k	Ramp load increase between 0% and 15% of full power	600		Fig. I-12		
-	Ramp load decrease between 0% and 15% of full power	600 3, 000		Fig. I-13		
l-m	I-m RCP startup			Fig. I-14		
l-n	I-n RCP shutdown			Fig. I-15		
l-o	Core lifetime extension	60		Fig. I-16		
l-p	Primary leakage test	120		Fig. I-17		
l-q	Turbine roll test	10		Fig, I-18		
l-r	Boron concentration equalization	39, 600		—		

Level	В					
Mark	Tra	Insient	Occurrence	Refe	erence	Remark
main			Cocarrence	Document	Fig. or Table	Koman
ll-a	Loss of load		60		Fig. II-1	
II-b	Loss of offsite power		60		Fig. II-2	
II-c	Partial loss of reactor coola	nt flow	30		Fig. II-3	
		i) With no inadvertent cooldown	60		Fig. II-4	
ll-d	Reactor trip from full	ii) With cooldown and no safety injection	30		Fig. II-5	Including the transient of Excessive feedwater flow
	power	iii) With cooldown and safety injection	10		Fig. II-6	
ll-e	Inadvertent	i) Umbrella case	30		Fig. II-7	
11-E	RCS depressurization			Fig. II-12		
ll-f	Control rod drop		30	Ref. 4	Fig. II-8	
ll-g	Inadvertent safeguards actu	uation	30		Fig. II-9	
ll-h	Emergency feedwater cyclin	ng	700		Fig. II-10	
II-i	Cold over-pressure		30		Fig. II-11	
II-j	Excessive feedwater flow		_		_	Be covered with the transient of Reactor trip from full power ii)
ll-k	Loss of offsite power with n	atural circulation cooldown	_		_	Be covered with the transient of Plant cooldown
11-1	Partial loss of emergency feedwater		30		_	Please use the figure of the transient of Loss of offsite power.
ll-m	Safe shutdown		_		_	Be covered with the transient of Plant cooldown

Table 8.1-3 Pressurizer surge line design transients (2/3)

Table 8.1-3 Pressurizer surge line design transients (3/3)

Level	C				
Mark	Transient	Occurrence	Refe	erence	Remark
IVIAIN		Occurrence	Document	Fig. or Table	Remark
III-a	Small loss of coolant accident	5		Fig. III-1	
III-b	Small steam line break	5		Fig. III-2	
III-c	Complete loss of flow	5	Ref. 4	Fig. III-3	
III-d	Small feedwater line break	5		Fig. III-4	
III-e	SG tube rupture	5		Fig. III-5	
Level	D				
IV-a	Large loss of coolant accident	1		Fig. IV-1	
IV-b	Large steam line break	1		Fig. IV-2	
IV-c	RCP locked rotor	1	Ref. 4	Fig. IV-3	
IV-d	Control rod ejection	1		Fig. IV-4	
IV-e	Large feedwater line break	1		Fig. IV-5	
Test					
V-a	Primary-side hydrostatic test	10	Ref. 4	_	

Table 8.1-4 Pressurizer spray line design transients (1/3)

Level	A				
Mark	Transient	Occurrence	Refe	erence	Remark
IVIAI K	Tansient	Coodinomoo	Document	Fig. or Table	Remark
I-a	Plant heat-up (100F/h)	120		Fig. I-1	
I-b-1	Plant cooldown (200F/h, 2235 \sim 400psig)	120		Fig. I-2	
I-b-2	Plant cooldown (200F/h, lower than 400psig)	120		Fig. I-2	
I-c-1	Ramp load increase between 15% and 100% of full power (5% of full power per minute)	600		Fig. I-3	
I-c-2	Ramp load increase between 50% and 100% of full power (5% of full power per minute)	19, 200		Fig. I-4	
l-d-1	Ramp load decrease between 15% and 100% of full power (5% of full power per minute)	600		Fig. I-5	
I-d-2	Ramp load decrease between 50% and 100% of full power (5% of full power per minute)	19, 200		Fig. I-6	
I-e	Step load increase of 10% of full power	600		Fig. I-7	
l-f	Step load decrease of 10% of full power	600	Ref. 4	Fig. I-8	
l-g	Large step load decrease with turbine bypass	60	Rel. 4	Fig. I-9	
l-h	Steady-state fluctuation i) Steady-state fluctuation	1×10 ⁶		_	P _p ±50psi, T _{hot} , T _{cold} , T _{ave} ±3.1F
	and load regulation ii) Load regulation	8×10 ⁵		Table 4	
I-i	Main feedwater cycling	2, 100		Fig. I-10	
I-j	Refueling	60		Fig. I-11	Water is replaced in 10 minutes.
l-k	Ramp load increase between 0% and 15% of full power	600		Fig. I-12	
I-I	Ramp load decrease between 0% and 15% of full power	600		Fig. I-13	
I-m	RCP startup	3, 000		Fig. I-14	
l-n	RCP shutdown	3, 000		Fig. I-15	
I-o	Core lifetime extension	60		Fig. I-16	
I-p	Primary leakage test	120		Fig. I-17	
l-q	Turbine roll test	10		Fig, I-18	
l-r	Boron concentration equalization	39, 600		—	

Level	В					
Mark	Tra	Insient	Occurrence	Refe	erence	Remark
Mark	nansient		Occurrence	Document	Fig. or Table	Kernark
ll-a	Loss of load		60		Fig. II-1	
II-b	Loss of offsite power		60		Fig. II-2	
ll-c	Partial loss of reactor coola	nt flow	30		Fig. II-3	
		i) With no inadvertent cooldown	60		Fig. II-4	
ll-d	Reactor trip from full	ii) With cooldown and no safety injection	30		Fig. II-5	Including the transient of Excessive feedwater flow
	power	iii) With cooldown and safety injection	10		Fig. II-6	
ll-e	Inadvertent	i) Umbrella case	30		Fig. II-7	
11-C	RCS depressurization	ii) Inadvertent auxiliary spray	15		Fig. II-12	
II-f	Control rod drop		30	Ref. 4	Fig. II-8	
ll-g	Inadvertent safeguards actu	uation	30		Fig. II-9	
ll-h	Emergency feedwater cyclir	ng	700		Fig. II-10	
II-i	Cold over-pressure		30		Fig. II-11	
II-j	Excessive feedwater flow		_		_	Be covered with the transient of Reactor trip from full power ii)
II-k	Loss of offsite power with natural circulation cooldown		_		_	Be covered with the transient of Plant cooldown
-	Partial loss of emergency feedwater		30		_	Please use the figure of the transient of Loss of offsite power.
ll-m	Safe shutdown		_		_	Be covered with the transient of Plant cooldown

Table 8.1-4 Pressurizer spray line design transients (2/3)

Table 8.1-4 Pressurizer spray line design transients (3/3)

Level	C				
Mark	Transient	Occurrence	Occurrence Refer		Remark
Mark	Tansient	Occurrence	Document	Fig. or Table	Remark
III-a	Small loss of coolant accident	5		Fig. III-1	
III-b	Small steam line break	5		Fig. III-2	
III-c	Complete loss of flow	5	Ref. 4	Fig. III-3	
III-d	Small feedwater line break	5		Fig. III-4	
III-e	SG tube rupture	5		Fig. III-5	
Level	D				
IV-a	Large loss of coolant accident	1		Fig. IV-1	
IV-b	Large steam line break	1		Fig. IV-2	
IV-c	RCP locked rotor	1	Ref. 4	Fig. IV-3	
IV-d	Control rod ejection	1		Fig. IV-4	
IV-e	Large feedwater line break	1	Ī	Fig. IV-5	
Test					
V-a	Primary-side hydrostatic test	10	Ref. 4	_	

Table 8.1-5 Pressurizer safety depressurization valve line design transients (1/4)

Level /	A				
Mark	Transient	Occurrence	Refe	erence	Remark
Wark	Tansicht	Occurrence	Document	Fig. or Table	
I-a	Plant heat-up (100F/h)	120		Fig. I-1	
I-b-1	Plant cooldown (200F/h, 2235 \sim 400psig)	120		Fig. I-2	
I-b-2	Plant cooldown (200F/h, lower than 400psig)	120		Fig. I-2	
I-c-1	Ramp load increase between 15% and 100% of full power (5% of full power per minute)	600		Fig. I-3	
I-c-2	Ramp load increase between 50% and 100% of full power (5% of full power per minute)	19, 200		Fig. I-4	
l-d-1	Ramp load decrease between 15% and 100% of full power (5% of full power per minute)	600		Fig. I-5	
I-d-2	Ramp load decrease between 50% and 100% of full power (5% of full power per minute)	19, 200	Def 4	Fig. I-6	
I-e	Step load increase of 10% of full power	600	Ref. 4	Fig. I-7	
l-f	Step load decrease of 10% of full power	600		Fig. I-8	
l-g	Large step load decrease with turbine bypass	60		Fig. I-9	
l-h	Steady-state fluctuation i) Steady-state fluctuation	1×10 ⁶		_	P _p ±50psi, T _{hot} , T _{cold} , T _{ave} ±3.1F
1-11	and load regulation ii) Load regulation	8×10⁵		Table 4	
I-i	Main feedwater cycling	2, 100		Fig. I-10	
l-m	RCP startup	3, 000		Fig. I-14	
l-n	RCP shutdown	3, 000		Fig. I-15	
I-p	Primary leakage test	120		Fig. I-17	
l-q	Turbine roll test	10		Fig, I-18	
l-r	Boron concentration equalization	39, 600		—	

Level	Level B								
Mark	Tra	nsient	Occurrence	Refe	erence	Remark			
Mark			Coourience	Document	Fig. or Table	T C Hulk			
ll-a	Loss of load		60		Fig. II-1				
II-b	Loss of offsite power		60		Fig. II-2				
II-c	Partial loss of reactor coola	nt flow	30		Fig. II-3				
		i) With no inadvertent	60		Fig. II-4				
		cooldown							
ll-d	Reactor trip from full	ii) With cooldown and no safety injection	30		Fig. II-5	Including the transient of Excessive feedwater flow			
	power	iii) With cooldown and safety injection	10		Fig. II-6				
ll-e	Inadvertent	i) Umbrella case	30		Fig. II-7				
11-C	RCS depressurization	ii) Inadvertent auxiliary spray	15		Fig. II-12				
II-f	Control rod drop		30	Ref. 4	Fig. II-8				
ll-g	Inadvertent safeguards actu	lation	30		Fig. II-9				
ll-h	Emergency feedwater cyclir	ng	700		Fig. II-10				
II-i	Cold over-pressure		30		Fig. II-11				
II-j	Excessive feedwater flow		_		—	Be covered with the transient of Reactor trip from full power ii)			
II-k	Loss of offsite power with natural circulation cooldown		_			Be covered with the transient of Plant cooldown			
-	Partial loss of emergency feedwater		30		_	Please use the figure of the transient of Loss of offsite power.			
II-m	Safe shutdown		_		_	Be covered with the transient of Plant cooldown			

Table 8.1-5 Pressurizer safety depressurization valve line design transients (2/4)

Table 8.1-5 Pressurizer safe	y depressurization valve lin	e design transients (3/4)

Level	2				
Mark	Transient	Occurrence Refe		erence	Remark
Mark	Tansient	Occurrence	Document	Fig. or Table	Kennark
III-a	Small loss of coolant accident	5		Fig. III-1	
III-b	Small steam line break	5		Fig. III-2	
III-c	Complete loss of flow	5	Ref. 4	Fig. III-3	
III-d	Small feedwater line break	5		Fig. III-4	
III-e	SG tube rupture	5		Fig. III-5	
Level					
IV-a	Large loss of coolant accident	1		Fig. IV-1	
IV-b	Large steam line break	1		Fig. IV-2	
IV-c	RCP locked rotor	1	Ref. 4	Fig. IV-3	
IV-d	Control rod ejection	1		Fig. IV-4	
IV-e	Large feedwater line break	1		Fig. IV-5	
Test					
V-a	Primary-side hydrostatic test	10	Ref. 4	_	

 Table 8.1-5 Pressurizer safety depressurization valve line design transients (4/4) (branch piping transients)

Level	Level A, B									
Mark	Transient	Occurrence -	Reference		Remark					
Mark	Tansient		Document	Fig. or Table	Remark					
_	Pressurizer safety depressurization valve actuation	60	Ref. 4	—						

Table 8.1-6 Pressurizer safety valve line design transients (1/4)

Level	A				
Mark	Transient	Occurrence	Refe	erence	Remark
Mark	Tansient	Occurrence	Document	Fig. or Table	Kennark
l-a	Plant heat-up (100F/h)	120		Fig. I-1	
I-b-1	Plant cooldown (200F/h, 2235 \sim 400psig)	120		Fig. I-2	
I-b-2	Plant cooldown (200F/h, lower than 400psig)	120		Fig. I-2	
I-c-1	Ramp load increase between 15% and 100% of full power (5% of full power per minute)	600		Fig. I-3	
I-c-2	Ramp load increase between 50% and 100% of full power (5% of full power per minute)	19, 200		Fig. I-4	
I-d-1	Ramp load decrease between 15% and 100% of full power (5% of full power per minute)	600		Fig. I-5	
I-d-2	Ramp load decrease between 50% and 100% of full power (5% of full power per minute)	19, 200		Fig. I-6	
l-e	Step load increase of 10% of full power	600	Ref. 4	Fig. I-7	
I-f	Step load decrease of 10% of full power	600		Fig. I-8	
l-g	Large step load decrease with turbine bypass	60		Fig. I-9	
l-h	Steady-state fluctuation i) Steady-state fluctuation	1×10 ⁶			P _p ±50psi, T _{hot} , T _{cold} , T _{ave} ±3.1F
	and load regulation ii) Load regulation	8×10 ⁵		Table 4	
I-i	Main feedwater cycling	2, 100		Fig. I-10	
I-m	RCP startup	3, 000		Fig. I-14	
l-n	RCP shutdown	3, 000		Fig. I-15	
I-p	Primary leakage test	120		Fig. I-17	
l-q	Turbine roll test	10		Fig, I-18	
l-r	Boron concentration equalization	39, 600		—	

Level I	В					
Mark	Tra	Insient	Occurrence	Refe	erence	Remark
Mark		Document		Document	Fig. or Table	Kennark
II-a	Loss of load		60		Fig. II-1	
II-b	Loss of offsite power		60		Fig. II-2	
II-c	Partial loss of reactor coola	nt flow	30		Fig. II-3	
ll-d	Reactor trip from full	-	60		Fig. II-4	
	power	cooldown ii) With cooldown and no safety injection	30		Fig. II-5	Including the transient of Excessive feedwater flow
		iii) With cooldown and safety injection	10		Fig. II-6	
ll-e	Inadvertent	i) Umbrella case	30		Fig. II-7	
	RCS depressurization	ii) Inadvertent auxiliary spray	15		Fig. II-12	
ll-f	Control rod drop		30	Ref. 4	Fig. II-8	
ll-g	Inadvertent safeguards actu	uation	30		Fig. II-9	
ll-h	Emergency feedwater cyclir	ng	700		Fig. II-10	
II-i	Cold over-pressure		30		Fig. II-11	
II-j	Excessive feedwater flow		_		_	Be covered with the transient of Reactor trip from full power ii)
ll-k	Loss of offsite power with natural circulation cooldown Partial loss of emergency feedwater				_	Be covered with the transient of Plant cooldown
-			30		-	Please use the figure of the transient of Loss of offsite power.
ll-m	Safe shutdown		_		-	Be covered with the transient of Plant cooldown

Table 8.1-6 Pressurizer safety valve line design transients (2/4)

Table 8.1-6	Pressurizer safety	valve line desig	n transients (3/4)
	· · · · · · · · · · · · · · · · · · ·		

Level	C				
Mark	Transient	Occurrence	Reference		Remark
IVIAIN	Tansient	Occurrence	Document	Fig. or Table	Remark
III-a	Small loss of coolant accident	5		Fig. III-1	
III-b	Small steam line break	5	Ref. 4	Fig. III-2	
III-c	Complete loss of flow	5		Fig. III-3	
III-d	Small feedwater line break	5		Fig. III-4	
III-e	SG tube rupture	5		Fig. III-5	
Level	D				
IV-a	Large loss of coolant accident	1		Fig. IV-1	
IV-b	Large steam line break	1		Fig. IV-2	
IV-c	RCP locked rotor	1	Ref. 4	Fig. IV-3	
IV-d	Control rod ejection	1		Fig. IV-4	
IV-e	Large feedwater line break	1		Fig. IV-5	
Test					
V-a	Primary-side hydrostatic test	10	Ref. 4	_	

Table 8.1-6 Pressurizer safety valve line design transients (4/4) (branch piping transients)

Level A, B						
Mark Transient		Occurrence	Reference		Remark	
IVIAIK	Tansient	Occurrence	Document	Fig. or Table	Kendik	
_	Pressurizer safety valve actuation	60	Ref. 4	_		

Level	Α				
Mark	Mark Transient		Reference		Remark
Marix	Hanolon	Occurrence	Document	Fig. or Table	
I-a	Plant heat-up (50F/h)	120		Fig. I-1	
I-b	Plant cooldown (100F/h)	120		Fig. I-2	Including the transient of Loss of offsite power with natural circulation cooldown (10 times) and Safe shutdown (1 time).
I-c-1	Ramp load increase between 15% and 100% of full power (5% of full power per minute)	600		Fig. I-3	
I-c-2	Ramp load increase between 50% and 100% of full power (5% of full power per minute)	19, 200		Fig. I-4	
I-d-1	Ramp load decrease between 15% and 100% of full power (5% of full power per minute)	600		Fig. I-5	
I-d-2	Ramp load decrease between 50% and 100% of full power (5% of full power per minute)	19, 200		Fig. I-6	
l-e	Step load increase of 10% of full power	600	Ref. 4	Fig. I-7	
l-f	Step load decrease of 10% of full power	600	IXEI: 4	Fig. I-8	
l-g	Large step load decrease with turbine bypass	60		Fig. I-9	
l-h	Steady-state fluctuation i) Steady-state fluctuation	1×10 ⁶		_	P _p ±50psi, T _{hot} , T _{cold} , T _{ave} ±3.1F
	and load regulation ii) Load regulation	8×10 ⁵		Table 4	
I-i	Main feedwater cycling	2, 100		Fig. I-10	
l-j	Refueling	60		Fig. I-11	Water is replaced in 10 minutes.
l-k	Ramp load increase between 0% and 15% of full power	600		Fig. I-12	
-	Ramp load decrease between 0% and 15% of full power	600		Fig. I-13	
l-m	RCP startup	3, 000		Fig. I-14	
l-n	RCP shutdown	3, 000		Fig. I-15	
I-o	Core lifetime extension	60		Fig. I-16	
I-p	Primary leakage test	120		Fig. I-17	
l-q	Turbine roll test	10		Fig, I-18	

Table 8.1-7 RHRS suction loop A line design transients (1/4)

Level	В					
Mark	Tra	nsient	Occurrence	Refe	erence	Remark
Mark	114			Document	Fig. or Table	Remain
ll-a	Loss of load	60		Fig. II-1		
II-b	Loss of offsite power		60		Fig. II-2	
II-c	Partial loss of reactor coolar	nt flow	30		Fig. II-3	
II-d	Reactor trip from full power	i) With no inadvertent cooldown	60		Fig. II-4	
		ii) With cooldown and no safety injection	30		Fig. II-5	Including the transient of Excessive feedwater flow
		iii) With cooldown and safety injection	10		Fig. II-6	
ll-e	Inadvertent RCS depressur	ization	30		Fig. II-7	
II-f	Control rod drop		30	Ref. 4	Fig. II-8	
ll-g	Inadvertent safeguards actu	lation	30	1.61.4	Fig. II-9	
ll-h	Emergency feedwater cyclir	ng	700		Fig. II-10	
II-i	Cold over-pressure		30		Fig. II-11	
II-j	Excessive feedwater flow		_		_	Be covered with the transient of Reactor trip from full power ii)
II-k	Loss of offsite power with na	atural circulation cooldown	_		_	Be covered with the transient of Plant cooldown
-	II-I Partial loss of emergency feedwater		30		_	Please use the figure of the transient of Loss of offsite power.
II-m	Safe shutdown		-		_	Be covered with the transient of Plant cooldown

Table 8.1-7 RHRS suction loop A line design transients (2/4)

Table 8.1-7 RHRS suction loop A line design transients (3/4)
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Level	C				
Mark	Transient	Occurrence	Reference		Remark
Mark	Transient	Occurrence	Document	Fig. or Table	Remark
III-a	Small loss of coolant accident	5		Fig. III-1	
III-b	Small steam line break	5	Ref. 4	Fig. III-2	
III-c	Complete loss of flow	5		Fig. III-3	
III-d	Small feedwater line break	5		Fig. III-4	
III-e	SG tube rupture	5	_	Fig. III-5	
Level	D				
IV-a	Large loss of coolant accident	1		Fig. IV-1	
IV-b	Large steam line break	1		Fig. IV-2	
IV-c	RCP locked rotor	1	Ref. 4	Fig. IV-3	
IV-d	Control rod ejection	1		Fig. IV-4	
IV-e	Large feedwater line break	1		Fig. IV-5	
Test					
V-a	Primary-side hydrostatic test	10	Ref. 4		

Table 8.1-7 RHRS suction loop A line design transients (4/4) (branch piping transients)

Level	Level A, B							
Mark	Mark Transient		Reference		Remark			
IVIAIK	Hansient	Occurrence	Document	Fig. or Table	Remark			
a)	Plant heat-up	120		Fig. I-26				
b)	Plant cooldown	120	Ref. 4	Fig. I-27				
c)	Safe shutdown	1		Fig. II-21				

Level	A				
Mark	Transient	Occurrence	Refe	erence	Remark
Wark	Turblent	Coourience	Document	Fig. or Table	
l-a	Plant heat-up (50F/h)	120		Fig. I-1	
I-b	Plant cooldown (100F/h)	120		Fig. I-2	Including the transient of Loss of offsite power with natural circulation cooldown (10 times) and Safe shutdown (1 time).
I-c-1	Ramp load increase between 15% and 100% of full power (5% of full power per minute)	600		Fig. I-3	
I-c-2	Ramp load increase between 50% and 100% of full power (5% of full power per minute)	19, 200		Fig. I-4	
I-d-1	Ramp load decrease between 15% and 100% of full power (5% of full power per minute)	600		Fig. I-5	
I-d-2	Ramp load decrease between 50% and 100% of full power (5% of full power per minute)	19, 200		Fig. I-6	
I-e	Step load increase of 10% of full power	600	Ref. 4	Fig. I-7	
I-f	Step load decrease of 10% of full power	600	1.1.4	Fig. I-8	
l-g	Large step load decrease with turbine bypass	60		Fig. I-9	
l-h	Steady-state fluctuation i) Steady-state fluctuation	1×10 ⁶			P _p ±50psi, T _{hot} , T _{cold} , T _{ave} ±3.1F
	and load regulation ii) Load regulation	8×10 ⁵		Table 4	
I-i	Main feedwater cycling	2, 100		Fig. I-10	
l-j	Refueling	60	-	Fig. I-11	Water is replaced in 10 minutes.
I-k	Ramp load increase between 0% and 15% of full power	600	-	Fig. I-12	
-	Ramp load decrease between 0% and 15% of full power	600	-	Fig. I-13	
I-m	RCP startup	3, 000	-	Fig. I-14	
l-n	RCP shutdown	3, 000	-	Fig. I-15	
l-o	Core lifetime extension	60	-	Fig. I-16	
I-p	Primary leakage test	120	-	Fig. I-17	
l-q	Turbine roll test	10		Fig, I-18	

Level	Level B							
Mark	Tra	nsient	Occurrence	Refe	erence	Remark		
Wark			Occurrence	Document	Fig. or Table	Kennark		
ll-a	Loss of load	60		Fig. II-1				
II-b	Loss of offsite power		60		Fig. II-2			
II-c	Partial loss of reactor coolar	nt flow	30		Fig. II-3			
ll-d	Reactor trip from full power	i) With no inadvertent cooldown	60		Fig. II-4			
		ii) With cooldown and no safety injection	30		Fig. II-5	Including the transient of Excessive feedwater flow		
		iii) With cooldown and safety injection	10		Fig. II-6			
ll-e	Inadvertent RCS depressuri	ization	30		Fig. II-7			
II-f	Control rod drop		30	Ref. 4	Fig. II-8			
ll-g	Inadvertent safeguards actu	lation	30	Rel. 4	Fig. II-9			
ll-h	Emergency feedwater cyclir	ng	700		Fig. II-10			
II-i	Cold over-pressure		30		Fig. II-11			
II-j	Excessive feedwater flow		_		_	Be covered with the transient of Reactor trip from full power ii)		
II-k	Loss of offsite power with natural circulation cooldown		_		_	Be covered with the transient of Plant cooldown		
-	II-I Partial loss of emergency feedwater		30		—	Please use the figure of the transient of Loss of offsite power.		
II-m	Safe shutdown		_		-	Be covered with the transient of Plant cooldown		

Table 8.1-8 RHRS suction loop B line design transients (2/4)

Table 8.1-8 RHRS suction loop B line design transients (3/4)

Level	C				
Mark	Transient	Occurrence	Reference		Remark
Mark	Hansient	Occurrence	Document	Fig. or Table	Kemark
III-a	Small loss of coolant accident	5		Fig. III-1	
III-b	Small steam line break	5	Ref. 4	Fig. III-2	
III-c	Complete loss of flow	5		Fig. III-3	
III-d	Small feedwater line break	5		Fig. III-4	
III-e	SG tube rupture	5		Fig. III-5	
Level	D				
IV-a	Large loss of coolant accident	1		Fig. IV-1	
IV-b	Large steam line break	1		Fig. IV-2	
IV-c	RCP locked rotor	1	Ref. 4	Fig. IV-3	
IV-d	Control rod ejection	1		Fig. IV-4	
IV-e	Large feedwater line break	1		Fig. IV-5	
Test					
V-a	Primary-side hydrostatic test	10	Ref. 4	_	

Table 8.1-8 RHRS suction loop B line design transients (4/4) (branch piping transients)

Level	Level A, B									
Mark	Transient	Occurrence	Reference		Remark					
Mark	Tansient		Document	Fig. or Table	Remark					
a)	Plant heat-up	120	Dof 4	Fig. I-26						
b)	Plant cooldown	120	Ref. 4	Fig. I-27						

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Level	A					
Mark	Transient	Occurrence	Reference		Remark	
Mark	Tansient	Occurrence	Document	Fig. or Table	I CHIAIN	
l-a	Plant heat-up (50F/h)	120		Fig. I-1		
I-b	Plant cooldown (100F/h)	120		Fig. I-2	Including the transient of Loss of offsite power with natural circulation cooldown (10 times) and Safe shutdown (1 time).	
I-c-1	Ramp load increase between 15% and 100% of full power (5% of full power per minute)	600		Fig. I-3		
I-c-2	Ramp load increase between 50% and 100% of full power (5% of full power per minute)	19, 200		Fig. I-4		
I-d-1	Ramp load decrease between 15% and 100% of full power (5% of full power per minute)	600		Fig. I-5		
I-d-2	Ramp load decrease between 50% and 100% of full power (5% of full power per minute)	19, 200		Fig. I-6		
l-e	Step load increase of 10% of full power	600	Ref. 4	Fig. I-7		
l-f	Step load decrease of 10% of full power	600	Rel. 4	Fig. I-8		
l-g	Large step load decrease with turbine bypass	60		Fig. I-9		
l-h	Steady-state fluctuation i) Steady-state fluctuation	1×10 ⁶			P _p ±50psi, T _{hot} , T _{cold} , T _{ave} ±3.1F	
	and load regulation ii) Load regulation	8×10 ⁵		Table 4		
I-i	Main feedwater cycling	2, 100		Fig. I-10		
l-j	Refueling	60		Fig. I-11	Water is replaced in 10 minutes.	
l-k	Ramp load increase between 0% and 15% of full power	600		Fig. I-12		
-	Ramp load decrease between 0% and 15% of full power	600		Fig. I-13		
I-m	RCP startup	3, 000		Fig. I-14		
l-n	RCP shutdown	3, 000		Fig. I-15		
I-o	Core lifetime extension	60		Fig. I-16		
I-p	Primary leakage test	120		Fig. I-17		
l-q	Turbine roll test	10		Fig, I-18		

Table 8.1-9 Accumulator line design transients (1/4)

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Level	В					
Mark	Tra	nsient	Occurrence	Refe	erence	Remark
Mark			Occurrence	Document	Fig. or Table	Kennark
ll-a	Loss of load		60		Fig. II-1	
ll-b	Loss of offsite power		60		Fig. II-2	
ll-c	Partial loss of reactor coola	nt flow	30		Fig. II-3	
		i) With no inadvertent cooldown	60		Fig. II-4	
ll-d	Reactor trip from full	ii) With cooldown and no safety injection	30		Fig. II-5	Including the transient of Excessive feedwater flow
	power	iii) With cooldown and safety injection	10		Fig. II-6	
II-e	Inadvertent RCS depressur	ization	30		Fig. II-7	
II-f	Control rod drop		30	Ref. 4	Fig. II-8	
ll-g	Inadvertent safeguards actu	lation	30		Fig. II-9	
ll-h	Emergency feedwater cyclir	ng	700		Fig. II-10	
II-i	Cold over-pressure		30		Fig. II-11	
II-j	Excessive feedwater flow		_		_	Be covered with the transient of Reactor trip from full power ii)
II-k	Loss of offsite power with natural circulation cooldown		_		_	Be covered with the transient of Plant cooldown
-	Partial loss of emergency feedwater		30		_	Please use the figure of the transient of Loss of offsite power.
II-m	Safe shutdown		_		_	Be covered with the transient of Plant cooldown

Table 8.1-9 Accumulator line design transients (2/4)

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Level	C								
Mark	Transient	Occurrence	Refe		Remark				
Mark	Transient	Occurrence	Document	Fig. or Table	Kennark				
III-a	Small loss of coolant accident	5		Fig. III-1					
III-b	Small steam line break	5		Fig. III-2					
III-c	Complete loss of flow	5	Ref. 4	Fig. III-3					
III-d	Small feedwater line break	5		Fig. III-4					
III-e	SG tube rupture	5		Fig. III-5					
Level	D								
IV-a	Large loss of coolant accident	1		Fig. IV-1					
IV-b	Large steam line break	1		Fig. IV-2					
IV-c	RCP locked rotor	1	Ref. 4	Fig. IV-3					
IV-d	Control rod ejection	1		Fig. IV-4					
IV-e	Large feedwater line break	1		Fig. IV-5					
Test	Test								
V-a	Primary-side hydrostatic test	10	Ref. 4	_					

Table 8.1-9 Accumulator line design transients (3/4)

Table 8.1-9 Accumulator line design transients (4/4) (branch piping transients)

Level	Level A, B								
Mark	Transient	Occurrence	Refe	erence	Remark				
Mark		Occurrence	Document	Fig. or Table	Keman				
a)	Inadvertent actuation of the accumulator tank	5		Fig. II-15					
b)	Plant cooldown	120		Fig. I-24					
c)	Refueling	60	Ref. 4	Fig. I-25					
d)	Inadvertent RCS depressurization	30		Fig. II-16					
e)	Plant heat-up	120		Fig. I-26					

Level	Α				
Mark	rk Transient		Occurrence Refer		Remark
Mark	Tansient	Occurrence	Document	Fig. or Table	Remark
l-a	Plant heat-up (50F/h)	120		Fig. I-1	
I-b	Plant cooldown (100F/h)	120		Fig. I-2	Including the transient of Loss of offsite power with natural circulation cooldown (10 times) and Safe shutdown (1 time).
I-c-1	Ramp load increase between 15% and 100% of full power (5% of full power per minute)	600		Fig. I-3	
I-c-2	Ramp load increase between 50% and 100% of full power (5% of full power per minute)	19, 200		Fig. I-4	
I-d-1	Ramp load decrease between 15% and 100% of full power (5% of full power per minute)	600		Fig. I-5	
I-d-2	Ramp load decrease between 50% and 100% of full power (5% of full power per minute)	19, 200		Fig. I-6	
l-e	Step load increase of 10% of full power	600	Ref. 4	Fig. I-7	
l-f	Step load decrease of 10% of full power	600		Fig. I-8	
l-g	Large step load decrease with turbine bypass	60		Fig. I-9	
l-h	Steady-state fluctuation i) Steady-state fluctuation	1×10 ⁶			P _p ±50psi, T _{hot} , T _{cold} , T _{ave} ±3.1F
	and load regulation ii) Load regulation	8×10 ⁵		Table 4	
l-i	Main feedwater cycling	2, 100		Fig. I-10	
l-j	Refueling	60		Fig. I-11	Water is replaced in 10 minutes.
l-k	Ramp load increase between 0% and 15% of full power	600		Fig. I-12	
-	Ramp load decrease between 0% and 15% of full power	600		Fig. I-13	
I-m	RCP startup	3, 000		Fig. I-14	
l-n	RCP shutdown	3, 000		Fig. I-15	
I-o	Core lifetime extension	60		Fig. I-16	
I-p	Primary leakage test	120		Fig. I-17	
I-q	Turbine roll test	10		Fig, I-18	

Table 8.1-10 DVI line design transients (1/4)

Level	В					
Mark	Tra	nsient	Occurrence	Decurrence Reference		Remark
mark			e courrentee	Document	Fig. or Table	Kennark
ll-a	Loss of load		60		Fig. II-1	
II-b	Loss of offsite power		60		Fig. II-2	
II-c	Partial loss of reactor coolar	nt flow	30		Fig. II-3	
		i) With no inadvertent	60		Fig. II-4	
		cooldown				
ll-d	Reactor trip from full	ii) With cooldown and no	30		Fig. II-5	Including the transient of Excessive
		safety injection	50		1 lg. ll-5	feedwater flow
		iii) With cooldown and safety	10		Fig. II-6	
	power	injection	10		1 19. 11 0	
ll-e	Inadvertent RCS depressurization		30		Fig. II-7	
II-f	Control rod drop		30	Ref. 4	Fig. II-8	
ll-g	Inadvertent safeguards actu	lation	30		Fig. II-9	
ll-h	Emergency feedwater cyclir	ng	700		Fig. II-10	
II-i	Cold over-pressure		30		Fig. II-11	
II-j	Excessive feedwater flow				_	Be covered with the transient of
11-j						Reactor trip from full power ii)
II-k	Loss of offsite power with na	atural circulation cooldown	_		_	Be covered with the transient of Plant
II-K						cooldown
-	II-I Partial loss of emergency feedwater		30		_	Please use the figure of the transient
			50	ļ		of Loss of offsite power.
ll-m	Safe shutdown		_		_	Be covered with the transient of Plant cooldown

Table 8.1-10 DVI line design transients (2/4)

Level	C								
Mark	Transient	Occurrence	Refe	erence	Remark				
Mark	Hansient	Occurrence	Document	Fig. or Table	Kennark				
III-a	Small loss of coolant accident	5		Fig. III-1					
III-b	Small steam line break	5		Fig. III-2					
III-c	Complete loss of flow	5	Ref. 4	Fig. III-3					
III-d	Small feedwater line break	5		Fig. III-4					
III-e	SG tube rupture	5		Fig. III-5					
Level	D								
IV-a	Large loss of coolant accident	1		Fig. IV-1					
IV-b	Large steam line break	1		Fig. IV-2					
IV-c	RCP locked rotor	1	Ref. 4	Fig. IV-3					
IV-d	Control rod ejection	1		Fig. IV-4					
IV-e	Large feedwater line break	1		Fig. IV-5					
Test	Test								
V-a	Primary-side hydrostatic test	10	Ref. 4	—					

Table 8.1-10 DVI line design transients (3/4)

Table 8.1-10 DVI line design transients (4/4) (branch piping transients)

Level A, B								
Mark	Transient	Occurrence	Reference		Remark			
Widitt	Hanolon	Coourience	Document	Fig. or Table	Kemaik			
a)	Reactor trip from full power with cooldown and safety	10		Fig. II-17				
	injection							
b)	Inadvertent RCS depressurization	30	Ref. 4	Fig. II-18				
C)	Inadvertent safeguards actuation	30		Fig. II-19				
d)	Safe shutdown	1		Fig. II-20				

Table 8.1-11	CVCS charging line design tr	ansients (1/4)
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Level	A					
Mark	Transient	Occurrence	Refe	erence	Remark	
Mark	Tansient	Occurrence	Document	Fig. or Table	Remark	
l-a	Plant heat-up (50F/h)	120		Fig. I-1		
I-b	Plant cooldown (100F/h)	120		Fig. I-2	Including the transient of Loss of offsite power with natural circulation cooldown (10 times) and Safe shutdown (1 time).	
I-c-1	Ramp load increase between 15% and 100% of full power (5% of full power per minute)	600		Fig. I-3		
I-c-2	Ramp load increase between 50% and 100% of full power (5% of full power per minute)	19, 200		Fig. I-4		
I-d-1	Ramp load decrease between 15% and 100% of full power (5% of full power per minute)	600		Fig. I-5		
I-d-2	Ramp load decrease between 50% and 100% of full power (5% of full power per minute)	19, 200		Fig. I-6		
l-e	Step load increase of 10% of full power	600	Ref. 4	Fig. I-7		
l-f	Step load decrease of 10% of full power	600		Fig. I-8		
l-g	Large step load decrease with turbine bypass	60		Fig. I-9		
l-h	Steady-state fluctuation i) Steady-state fluctuation	1×10 ⁶			P _p ±50psi, T _{hot} , T _{cold} , T _{ave} ±3.1F	
1-11	and load regulation ii) Load regulation	8×10 ⁵		Table 4		
I-i	Main feedwater cycling	2, 100		Fig. I-10		
I-j	Refueling	60		Fig. I-11	Water is replaced in 10 minutes.	
l-k	Ramp load increase between 0% and 15% of full power	600		Fig. I-12		
 -	Ramp load decrease between 0% and 15% of full power	600		Fig. I-13		
I-m	RCP startup	3, 000		Fig. I-14		
l-n	RCP shutdown	3, 000		Fig. I-15		
I-o	Core lifetime extension	60		Fig. I-16		
I-p	Primary leakage test	120		Fig. I-17		
l-q	Turbine roll test	10		Fig, I-18		

Level	В					
Mark	Transient		Occurrence	Reference		Remark
Mark			Occurrence	Document	Fig. or Table	Remark
ll-a	Loss of load		60		Fig. II-1	
II-b	Loss of offsite power		60		Fig. II-2	
ll-c	Partial loss of reactor coola	nt flow	30		Fig. II-3	
		i) With no inadvertent cooldown	60		Fig. II-4	
ll-d	Reactor trip from full	ii) With cooldown and no safety injection	30		Fig. II-5	Including the transient of Excessive feedwater flow
	power	iii) With cooldown and safety injection	10		Fig. II-6	
ll-e	Inadvertent RCS depressurization		30		Fig. II-7	
II-f	Control rod drop		30	Ref. 4	Fig. II-8	
ll-g	Inadvertent safeguards actu	lation	30		Fig. II-9	
ll-h	Emergency feedwater cyclir	ng	700		Fig. II-10	
II-i	Cold over-pressure		30		Fig. II-11	
II-j	Excessive feedwater flow		_		_	Be covered with the transient of Reactor trip from full power ii)
II-k	Loss of offsite power with na	atural circulation cooldown	_		_	Be covered with the transient of Plant cooldown
11-1	Partial loss of emergency feedwater		30		_	Please use the figure of the transient of Loss of offsite power.
ll-m	Safe shutdown		_		_	Be covered with the transient of Plant cooldown

Table 8.1-11 CVCS charging line design transients (2/4)

Table 8.1-11 CVCS charging line design transients (3/4)

Level	C				
Mark	Transient	Occurrence	Refe	erence	Remark
Mark	Transient	Occurrence	Document	Fig. or Table	Remark
III-a	Small loss of coolant accident	5		Fig. III-1	
III-b	Small steam line break	5	Ref. 4	Fig. III-2	
III-c	Complete loss of flow	5		Fig. III-3	
III-d	Small feedwater line break	5		Fig. III-4	
III-e	SG tube rupture	5		Fig. III-5	
Level	D				
IV-a	Large loss of coolant accident	1		Fig. IV-1	
IV-b	Large steam line break	1		Fig. IV-2	
IV-c	RCP locked rotor	1	Ref. 4	Fig. IV-3	
IV-d	Control rod ejection	1	-	Fig. IV-4	
IV-e	Large feedwater line break	1		Fig. IV-5	
Test					
V-a	Primary-side hydrostatic test	10	Ref. 4	_	

Table 8.1-11 CVCS charging line design transients (4/4) (branch piping transients)

Level	А, В					
Mark	Transient		Occurrence	Reference		Remark
Mark	114	noient	Occurrence	Document	Fig. or Table	Remark
1.A	Letdown shut off and re-initi	ated	70		Fig. II-13	
1.B	Charging line shut off and	a) Maintenance	30		Fig. I-19	
1.0	charging line shut on and	b) SI	70		Fig. II-14	
	re-initiated			Ref. 4		
2.A	Charging flow 50% step decrease and return		20, 400	Rel. 4	Fig. I-20	
2.B	Charging flow 50% step increase and return		23, 600		Fig. I-21	
2.C	Letdown flow 50% step decrease and return		2, 900		Fig. I-22	
2.D	Letdown flow 100% step inc	rease and return	19, 800		Fig. I-23	

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Level	Α				
Mark	Transient	Occurrence	Reference		Remark
IVIAIN			Document	Fig. or Table	Reliark
I-a	Plant heat-up (50F/h)	120		Fig. I-1	
I-b	Plant cooldown (100F/h)	120		Fig. I-2	Including the transient of Loss of offsite power with natural circulation cooldown (10 times) and Safe shutdown (1 time).
I-c-1	Ramp load increase between 15% and 100% of full power (5% of full power per minute)	600		Fig. I-3	
I-c-2	Ramp load increase between 50% and 100% of full power (5% of full power per minute)	19, 200		Fig. I-4	
I-d-1	Ramp load decrease between 15% and 100% of full power (5% of full power per minute)	600		Fig. I-5	
I-d-2	Ramp load decrease between 50% and 100% of full power (5% of full power per minute)	19, 200		Fig. I-6	
I-e	Step load increase of 10% of full power	600	Ref. 4	Fig. I-7	
l-f	Step load decrease of 10% of full power	600		Fig. I-8	
l-g	Large step load decrease with turbine bypass	60		Fig. I-9	
I-h	Steady-state fluctuation i) Steady-state fluctuation	1×10 ⁶			P _p ±50psi, T _{hot} , T _{cold} , T _{ave} ±3.1F
	and load regulation ii) Load regulation	8×10 ⁵		Table 4	
l-i	Main feedwater cycling	2, 100		Fig. I-10	
l-j	Refueling	60		Fig. I-11	Water is replaced in 10 minutes.
l-k	Ramp load increase between 0% and 15% of full power	600		Fig. I-12	
-	Ramp load decrease between 0% and 15% of full power	600		Fig. I-13	
I-m	RCP startup	3, 000		Fig. I-14	
l-n	RCP shutdown	3, 000		Fig. I-15	
l-o	Core lifetime extension	60		Fig. I-16	
I-p	Primary leakage test	120		Fig. I-17	
l-q	Turbine roll test	10		Fig, I-18	

Table 8.1-12 CVCS let down line design transients (1/4)

MUAP-09011-NP (R0)

Level	В					
Mark	Tra	nsient	Occurrence	Refe	erence	Remark
Wark	114	holent	Occurrence	Document	Fig. or Table	Kennark
ll-a	Loss of load		60		Fig. II-1	
ll-b	Loss of offsite power		60		Fig. II-2	
ll-c	Partial loss of reactor coolar	nt flow	30		Fig. II-3	
		i) With no inadvertent cooldown	60		Fig. II-4	
ll-d	Reactor trip from full	ii) With cooldown and no safety injection	30		Fig. II-5	Including the transient of Excessive feedwater flow
	power	iii) With cooldown and safety injection	10		Fig. II-6	
II-e	Inadvertent RCS depressuri	zation	30		Fig. II-7	
II-f	Control rod drop		30	Ref. 4	Fig. II-8	
ll-g	Inadvertent safeguards actuation		30		Fig. II-9	
ll-h	Emergency feedwater cycling		700		Fig. II-10	
II-i	Cold over-pressure		30		Fig. II-11	
II-j	Excessive feedwater flow		_		_	Be covered with the transient of Reactor trip from full power ii)
II-k	Loss of offsite power with natural circulation cooldown		_		_	Be covered with the transient of Plant cooldown
11-1	Partial loss of emergency feedwater		30		_	Please use the figure of the transient of Loss of offsite power.
ll-m	Safe shutdown		_		-	Be covered with the transient of Plant cooldown

Table 8.1-12 CVCS let down line design transients (2/4)

Level	C				
Mark	Transient	Occurrence	Refe	erence	Remark
Mark	Hansient	Occurrence	Document		Kemark
III-a	Small loss of coolant accident	5		Fig. III-1	
III-b	Small steam line break	5		Fig. III-2	
III-c	Complete loss of flow	5	Ref. 4	Fig. III-3	
III-d	Small feedwater line break	5		Fig. III-4	
III-e	SG tube rupture	5		Fig. III-5	
Level I	D				
IV-a	Large loss of coolant accident	1		Fig. IV-1	
IV-b	Large steam line break	1		Fig. IV-2	
IV-c	RCP locked rotor	1	Ref. 4	Fig. IV-3	
IV-d	Control rod ejection	1		Fig. IV-4	
IV-e	Large feedwater line break	1		Fig. IV-5	
Test					
V-a	Primary-side hydrostatic test	10	Ref. 4	_	

Table 8.1-12 CVCS let down line design transients (3/4)

Table 8.1-12 CVCS let down line design transients (4/4) (branch piping transients)

Level	А, В				
Mark	Transient	Occurrence	Refe	erence	Remark
Mark	Hansient	Occurrence	Document	Fig. or Table	Kennark
a)	Plant heat-up	120		Fig. I-26	
b)	Plant cooldown	120		Fig. I-27	
C)	Letdown line shut off and re-initiated (maintenance)	30	Ref. 4	Fig. I-28	c) and d) have the same transient
d)	Letdown line shut off and re-initiated (SI)	70]	Fig. I-28	diagram.
e)	RCS drain	120		Fig. I-29	

Level	Α				
Mark	Transient	Occurrence	Reference		Remark
IVIAIN	Transient		Document	Fig. or Table	Remark
l-a	Plant heat-up (50F/h)	120		Fig. I-1	
l-b	Plant cooldown (100F/h)	120		Fig. I-2	Including the transient of Loss of offsite power with natural circulation cooldown (10 times) and Safe shutdown (1 time).
I-c-1	Ramp load increase between 15% and 100% of full power (5% of full power per minute)	600		Fig. I-3	
I-c-2	Ramp load increase between 50% and 100% of full power (5% of full power per minute)	19, 200		Fig. I-4	
I-d-1	Ramp load decrease between 15% and 100% of full power (5% of full power per minute)	600		Fig. I-5	
I-d-2	Ramp load decrease between 50% and 100% of full power (5% of full power per minute)	19, 200		Fig. I-6	
l-e	Step load increase of 10% of full power	600	Ref. 4	Fig. I-7	
l-f	Step load decrease of 10% of full power	600		Fig. I-8	
l-g	Large step load decrease with turbine bypass	60		Fig. I-9	
I-h	Steady-state fluctuation i) Steady-state fluctuation	1×10 ⁶			P _p ±50psi, T _{hot} , T _{cold} , T _{ave} ±3.1F
	and load regulation ii) Load regulation	8×10 ⁵		Table 4	
l-i	Main feedwater cycling	2, 100		Fig. I-10	
l-j	Refueling	60		Fig. I-11	Water is replaced in 10 minutes.
l-k	Ramp load increase between 0% and 15% of full power	600		Fig. I-12	
-	Ramp load decrease between 0% and 15% of full power	600		Fig. I-13	
I-m	RCP startup	3, 000		Fig. I-14	
l-n	RCP shutdown	3, 000		Fig. I-15	
l-o	Core lifetime extension	60		Fig. I-16	
I-p	Primary leakage test	120		Fig. I-17	
l-q	Turbine roll test	10		Fig, I-18	

Table 8.1-13 CVCS seal injection line design transients (1/3)

Level	В					
Mark	Tra	nsient	Occurrence	Refe	erence	Remark
Wark		holent	Occurrence	Document	Fig. or Table	Kennark
ll-a	Loss of load		60		Fig. II-1	
II-b	Loss of offsite power		60		Fig. II-2	
ll-c	Partial loss of reactor coolar	nt flow	30		Fig. II-3	
		i) With no inadvertent cooldown	60		Fig. II-4	
ll-d	Reactor trip from full	ii) With cooldown and no safety injection	30		Fig. II-5	Including the transient of Excessive feedwater flow
	power	iii) With cooldown and safety injection	10		Fig. II-6	
ll-e	Inadvertent RCS depressuri	zation	30		Fig. II-7	
II-f	Control rod drop		30	Ref. 4	Fig. II-8	
ll-g	Inadvertent safeguards actuation		30		Fig. II-9	
ll-h	Emergency feedwater cycling		700		Fig. II-10	
II-i	Cold over-pressure		30		Fig. II-11	
II-j	Excessive feedwater flow		_		_	Be covered with the transient of Reactor trip from full power ii)
II-k	Loss of offsite power with natural circulation cooldown		_		_	Be covered with the transient of Plant cooldown
-	Partial loss of emergency feedwater		30		-	Please use the figure of the transient of Loss of offsite power.
II-m	Safe shutdown		_		_	Be covered with the transient of Plant cooldown

Table 8.1-13 CVCS seal injection line design transients (2/3)

Table 8.1-13 CVCS seal injection line design transients (3/3)	Table 8.1-13	CVCS seal injecti	ion line design	transients (3/3)
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Level	C				
Mark	Transient	Occurrence	Refe	erence	Remark
Mark	Transient	Document		Fig. or Table	Reindik
III-a	Small loss of coolant accident	5		Fig. III-1	
III-b	Small steam line break	5		Fig. III-2	
III-c	Complete loss of flow	5	Ref. 4	Fig. III-3	
III-d	Small feedwater line break	5		Fig. III-4	
III-e	SG tube rupture	5		Fig. III-5	
Level	D				
IV-a	Large loss of coolant accident	1		Fig. IV-1	
IV-b	Large steam line break	1		Fig. IV-2	
IV-c	RCP locked rotor	1	Ref. 4	Fig. IV-3	
IV-d	Control rod ejection	1		Fig. IV-4	
IV-e	Large feedwater line break	1		Fig. IV-5	
Test					
V-a	Primary-side hydrostatic test	10	Ref. 4	_	

8.2 Load Combinations

The loading conditions consist of various combinations of pressure, thermal and external loads.

The loads combinations considered in the analysis are listed in the Table below.

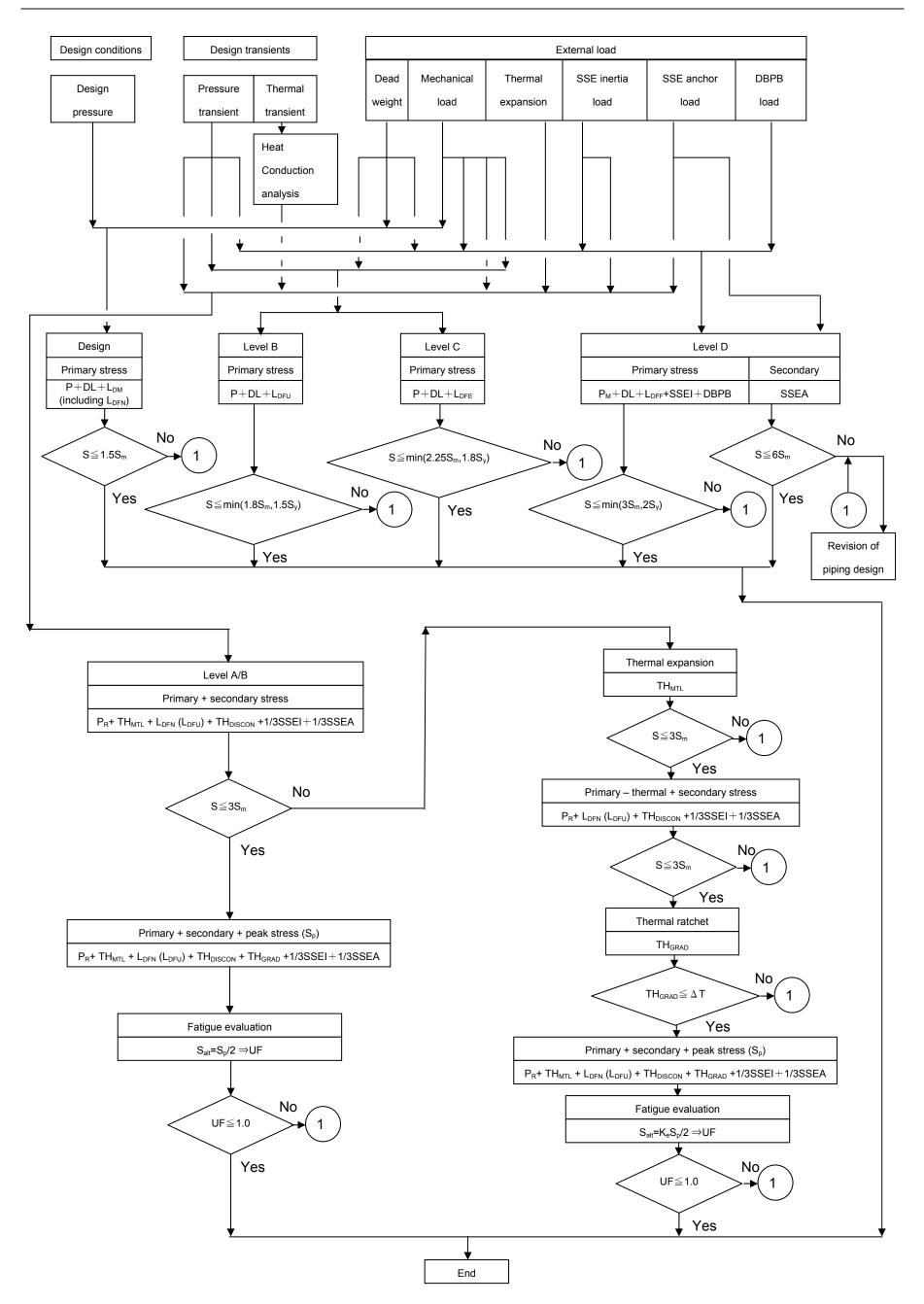
Loading Conditions	Design	Level A/B	Level C	Level D
Design Pressure	✓			
Maximum Operating Pressure		✓	✓	✓
Dead Load	✓		✓	✓
Mechanical load (pressurizer safety valve and safety depressurization valve thrust load)	~	✓	~	~
Level A thermal, pressure transient load		~		
Level B thermal, pressure transient load		~		
Level C pressure transient load			\checkmark	
Level D pressure transient load				~
1/3 SSE Loads		~		
SSE Loads				\checkmark
Design Basis Pipe Break				\checkmark

Table 8.2-1	Loadings to be considered for various Load Condition
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9.0 METHODOLOGY

9.1 Logic diagram of Evaluation

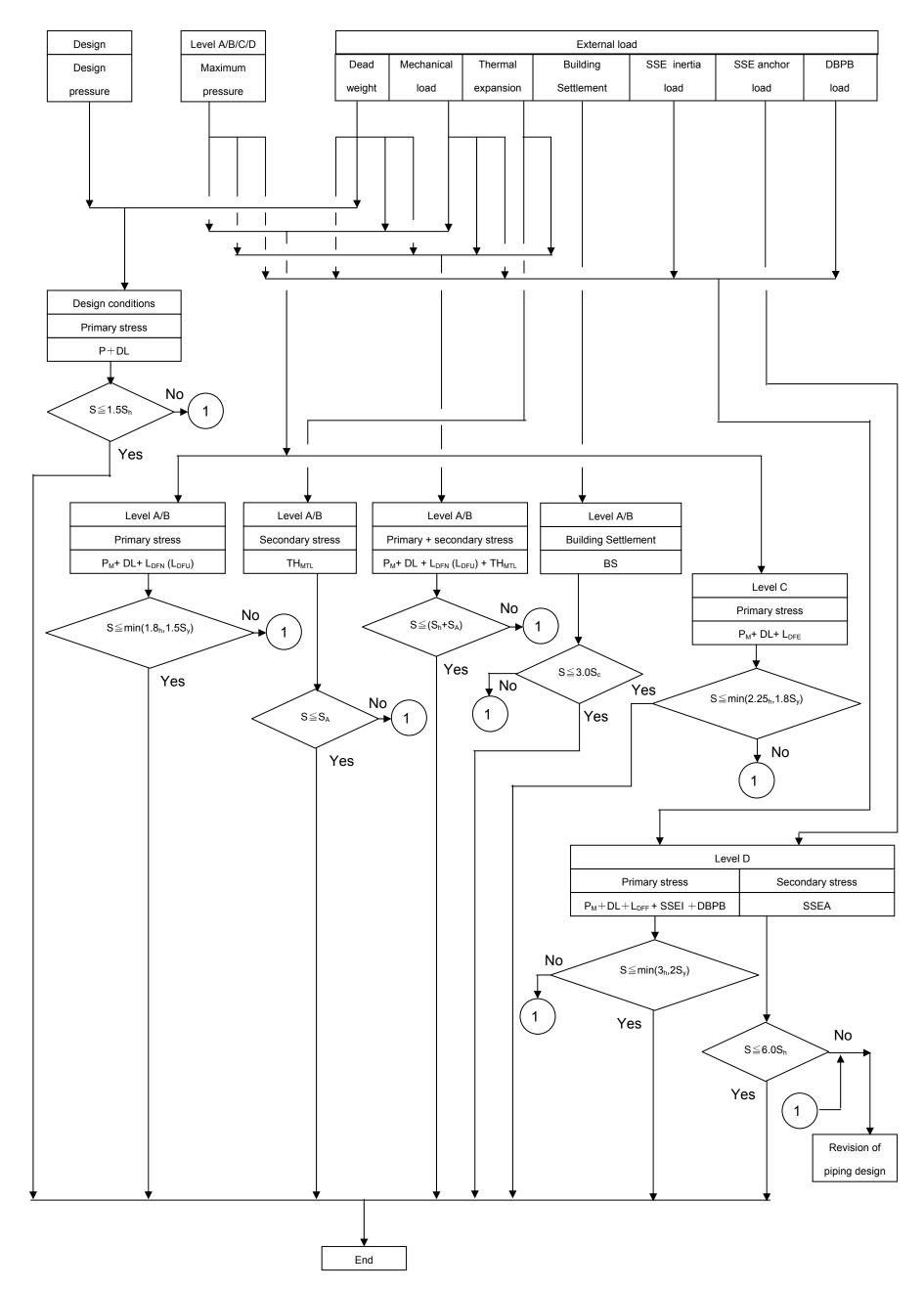
For the Reactor Coolant Branch Piping, piping that exceeds 1 inch was evaluated according to NB-3650 (Reference 7) and 1 inch or smaller than 1 inch piping was evaluated according to NC-3650 (Reference 7). The evaluation logic diagrams are shown in Figure 9.1-1 and Figure 9.1-2.



Note 1: In addition to the logic diagram shown above, permissible pressure was evaluated for Levels B, C, and D.

Figure 9.1-1 Evaluation Logic Diagram (greater than 1 inch piping)

Mitsubishi Heavy Industries, LTD.



Note 1: Either secondary stress evaluation or primary plus secondary stress evaluation may be used.

Figure 9.1-2 Evaluation Logic Diagram (1 inch or smaller than 1 inch piping)

Mitsubishi Heavy Industries, LTD.

9.2 Structural Analysis

A structural analysis was performed with the following conditions according to the Piping Design Criteria (Reference 2).

9.2.1 Analysis model

For dynamic analysis, the piping system is idealized as a three dimensional space frame. The analysis model consists of a sequence of nodes connected by straight pipe elements and curved pipe elements with stiffness properties representing the piping, and other in-line components.

Piping restraints and supports are idealized as zero length springs with appropriate stiffness values for the restrained degrees of freedom.

In the dynamic mathematical model, the distributed mass of the system, including pipe, contents, and insulation weight, is represented as lumped masses located at each node, which is designated as a mass point.

The following formula is used to determine the spacing between two successive mass points. The PIPESTRESS program uses this formula for mass point spacing.

$$L = \sqrt{\left[\frac{K}{F_R}\right]}\sqrt{\frac{EI}{W}}$$

where

- K = 0.743
- L = Mass point spacing (ft)
- F_R = Cut-off frequency (Hz)
- *E* = Modulus of elasticity of pipe material (psi)
- I = Moment of inertia of pipe cross-section (in⁴)
- W = Mass per unit length of piping + insulation + contents (lbm/ft)

Concentrated weights of in-line components, such as valves, flanges, and instrumentation, are also modeled as lumped masses.

Torsional effects of eccentric masses are included in the analysis.

Seismic analysis of RCL branch lines including DVI lines, decoupled from the analysis model of the RCL or RV, were performed using applicable envelope response spectra for the RCL or RV considering the connection point as an anchor. The movements (displacements and rotations) of the RCL and RV from the thermal, SAM or pipe break analysis were applied as anchor movement with their respective load cases in the decoupled branch line analysis.

9.2.2 Seismic Analysis Method

9.2.2.1 Damping Values

The damping value used for the SSE was 4%, which is consistent with Table 3 of the RG 1.61, Rev.1.

9.2.2.2 Combination of Modal Responses

For piping systems with no closely spaced modes, the SRSS method was applied to obtain the representative maximum response of each element, for each direction of excitation. A 10% grouping method was used for combining the responses of closely spaced modes.

9.2.2.3 High-Frequency Mode

The PIPESTRESS computer program was used for analyzing the piping systems. This program uses the LOF method to calculate the effect of the high frequency rigid modes. The results obtained were treated as an additional modal result from a non-closely spaced last mode, and were combined with other modal responses by the methods described in Subsection 9.2.2.2.

9.2.2.4 Directional Combination

The collinear responses due to each of the three spatial input components of motion were combined using the SRSS method

9.2.2.5 Seismic Anchor Motion

The effects of differential displacements of equipment or structures to which the piping system attaches during a SSE were considered.

The analysis of these seismic anchor motions (SAMs) was performed as a static analysis with all dynamic supports active. The results of this analysis were combined with the piping system seismic inertia analysis results by absolute summation.

Where supports were located within a single structure, the seismic motions were considered to be in-phase and the relative displacement between the support locations was considered in the analysis. Where supports were located within different structures, the seismic motions at these locations were assumed to move 180 degrees out-of-phase while performing the analysis.

9.2.2.6 Independent Support Motion Method

The supports were divided into support groups. Each support group was made up of supports that had similar time-history input. The responses caused by each support group were combined by the ABS method. The modal and directional responses were then combined as discussed above. Floor response spectrum curves used for ISM were generated using damping values identified in Section 9.2.2.1.

9.2.3 Time-History Method

The fluid transient analysis was performed to provide the hydraulic transient input for the pressurizer safety valve and safety depressurization valve piping using RELAP5-3D (Reference 7). The time history hydraulic forces were calculated using the pressure transient, flow rate, and other fluid property obtained by the fluid transient analysis. The structural time history analysis was performed using PIPESTRESS (Reference 8) by modal superposition method.

9.3 Thermal Stress Analysis

A heat conduction analysis was performed to obtain the piping temperature distribution during a thermal transient. For heat conduction analysis, the ABAQUS (Reference 10) general finite element method program was used.

In the heat conduction analysis, the temperature distribution was obtained for structural discontinuities (valves or reducers, for example) and in the piping plate thickness direction during the transient. From those results, the temperatures, Ta and Tb, of the structural discontinuity, and the temperature differences of the inner and outer pipe surfaces, Δ T1 and Δ T2, were computed using our independently developed P4TEDIA program (see section 10).

Of the Level A and Level B transients, the transient that applied to each system was used. The change in the fluid temperature and heat transfer coefficient at the inner surface of the pipingwere used. The heat transfer coefficient used was the value obtained from the equation, described below (Gnielinski's equation), for turbulent flow within a cylindrical pipe. The outer surface of the piping was considered as a heat-retaining insulator.

$$Nu = \frac{(f/2)(Re - 1000)Pr}{1 + 12.7(f/2)^{1/2}(Pr^{2/3} - 1)}$$

$$0.5 \le Pr \le 2000$$

$$2300 \le Re \le 5 \times 10^{6}$$

$$1/f^{0.5} = 1.5635\ell n(Re/7) \qquad (4 \times 10^{3} \le Re \le 1 \times 10^{7})$$

$$\alpha = Nu \cdot \lambda / d$$

$$Re = u \cdot d / v$$

$$Nu : \text{Nusselt number}$$

$$Re : \text{Reynolds number}$$

- Pr : Prandtl number
- α : Heat transfer coefficient
- λ : Thermal conductivity of fluid
- v : Kinematic viscosity of fluid
- *u* : Flow velocity
- d : Inner diameter of pipe

9.4 Stress Evaluation

Stress limits for design and service loadings are as follows.

9.4.1 Piping that exceeds 1 inch (evaluated according to NB-3650)

(1) Design limit

(a) Primary stress evaluation (eq.9)

$$B_1 \frac{PD_0}{2t} + B_2 \frac{D_0}{2I} M_i \le 1.5S_m$$

B₁, B₂: Stress indices
P: Design pressure
D₀: Outside diameter
t: Wall thickness
I: Moment of inertia
M_i: Dead weight, mechanical load (pressurizer safety depressurization valve and safety valve water hammer load) moment

(2) Level A/B service limits

(a) primary plus secondary stress evaluation (eq.10)

$$S_{n} = C_{1} \frac{P_{0} D_{0}}{2t} + C_{2} \frac{D_{0}}{2I} M_{i} + C_{3} E \alpha |T_{a} - T_{b}| \le 3S_{m}$$

C₁, C₂: Stress indices

P₀: Pressure range

- M_i: Moment ranges for following loads. Thermal expansion, mechanical load (pressurizer safety depressurization valve and safety valve water hammer load), seismic inertia load (1/3SSE), seismic anchor load (1/3SSE)
- E: modulus of elasticity (room temperature)

α: Coefficient of thermal expansion (room temperature)

Ta-Tb: Structural discontinuity temperature difference range

(b) Primary plus secondary plus peak stress evaluation (Eq.11)

$$S_{p} = K_{1}C_{1}\frac{P_{0}D_{0}}{2t} + K_{2}C_{2}\frac{D_{0}}{2I}M_{i} + \frac{1}{2(1-\nu)}K_{3}E\alpha|\Delta T_{1}| + K_{3}C_{3}E\alpha|T_{a} - T_{b}| + \frac{1}{1-\nu}E\alpha|\Delta T_{2}|$$

 K_1, K_2, K_3 : Stress indices

 ΔT_1 :Absolute value of the range of the temperature difference between the temperature of the outside T_0 and the temperature of the inside surface T_1 of the piping product assuming moment generating equivalent linear temperature distribution

- ΔT_2 : Absolute value of the range for that portion of the nonlinear thermal gradient through the wall thickness not included in ΔT_1 .
- v: Poisson's ratio (=0.3)

Sp is computed to obtain the stress intensity Salt for the fatigue analysis described later. Sp does not have any allowable stress.

(c) Fatigue evaluation

For
$$S_n \le 3S_m$$

 $S_{alt} = \frac{S_p}{2}$,

 $UF \leq 1.0$

(d) Simplified elastic-plastic discontinuity analysis For $S_n > 3S_m$

$$S_e = C_2 \frac{D_0}{2I} M_i^* \le 3S_m$$
 (eq.12)

M^{*}_i: Thermal expansion (including anchor movements) moment range

$$C_1 \frac{P_0 D_0}{2t} + C_2 \frac{D_0}{2I} M_i + C'_3 E \alpha |T_a - T_b| \le 3S_m \text{ (eq.13)}$$

- M_i: Moment ranges for following loads. Dead weight, mechanical load (pressurizer safety depressurization valve and safety valve water hammer load), seismic inertial load (1/3SSE), seismic anchor load (1/3SSE)
- C_3 ': Stress index

$$S_{alt} = K_e \frac{S_p}{2} \text{ (eq. 14)}$$

$$UF \leq 1.0$$

where

$$K_e = 1.0 \cdots S_n \leq 3S_m$$

$$K_e = 1.0 + \frac{1-n}{n(m-1)} \left(\frac{S_n}{3S_m} - 1 \right) \cdots 3S_m < S_n < 3mS_m$$

$$K_e = \frac{1}{n} \cdots S_n \geq 3mS_m$$

n=0.3, m=1.7 \dots for austenitic stainless steel

4)

$$\Delta T_1 range \leq_e \frac{y'S_y}{0.7E\alpha}C_4$$

$$\boxed{\begin{array}{c|c|c|c|c|c|c|c|c|} x & 0.3 & 0.5 & 0.7 & 0.8 \\ \hline y' & 3.33 & 2.00 & 1.20 & 0.80 \\ \hline \end{array}}$$

$$x = \frac{PD_0}{2t} \frac{1}{S_v}$$

P: maximum pressure for the set of conditions under consideration C4: 1.3 (austenitic stainless steel)

Sy: Yield point at the average fluid temperature of the load set

(3) Level B service limits

(a) Permissible pressure

$$P_{M} \leq 1.1 P_{a}$$
$$P_{a} = \frac{2S_{m}t}{D_{0} - 2yt}$$

 P_m : maximum pressure for Level B y:0.4

(b) Primary stress evaluation (eq.9)

$$B_1 \frac{PD_0}{2t} + B_2 \frac{D_0}{2I} M_i \le \min(1.8S_m, 1.5S_y)$$

P: Maximum pressure for Level B

M_i: Moment ranges for following loads. Dead weight, mechanical load (pressurizer safety depressurization valve and safety valve water hammer load)

(4) Level C service limits

(a) Permissible pressure

 $P_M \leq 1.5 P_a$

$$P_a = \frac{2S_m t}{D_0 - 2yt}$$

P_m: maximum pressure for Level C y:0.4

(b) Primary stress evaluation (eq.9)

$$B_1 \frac{PD_0}{2t} + B_2 \frac{D_0}{2I} M_i \le \min(2.25S_m, 1.8S_y)$$

P: Level C maximum pressure

- M_i: Moment ranges for following loads. Dead weight, mechanical load (pressurizer safety depressurization valve and safety valve water hammer load)
- (5) Level D service limits

(a) Permissible pressure

$$P_{M} \leq 2.0P_{a}$$

$$P_{a} = \frac{2S_{m}t}{D_{0} - 2yt}$$

 P_m : maximum pressure for Level D y:0.4

(b) Primary stress evaluation (eq.9)

$$B_1 \frac{PD_0}{2t} + B_2 \frac{D_0}{2I} M_i \le \min(3S_m, 2S_y)$$

- P: maximum pressure for Level D
- M_i: Moment ranges for following loads. Dead weight, mechanical load (pressurizer safety depressurization valve and safety valve water hammer load), SSE seismic inertia load, DBPB load

Note that the SSE seismic inertia load and DBPB load were combined using the SRSS method.

(c) Secondary stress evaluation

$$\frac{C_2 D_0 M_{AM}}{2I} \le 6.0 S_m$$

$$\frac{F_{AM}}{A_M} \le S_m$$

 M_{AM} : Range of resultant moment due to SSEA F_{AM} : Amplitude of longitudinal force due to SSEA A_M : Piping cross-sectional area

9.4.2 1 inch or smaller than 1 inch piping (evaluated according to NC-3650)

(1) Design limit
(a) Primary stress evaluation (eq.8)

$$S_{SL} = B_1 \frac{PD_0}{2t_n} + B_2 \frac{M_A}{Z} \le 1.5S_h$$
B₁, B₂: Stress indices
P: Design pressure
D₀: Outside diameter

t_n: Wall thickness
 Z: Section modulus
 M_A: Dead weight (no sustained mechanical load other than dead weight)

(2) Level A/B service limits

(a) Primary stress evaluation(eq.9)

$$S_{OL} = B_1 \frac{P_{\max} D_0}{2t_n} + B_2 (\frac{M_A + M_B}{Z}) \le \min(1.8S_h, 1.5S_y)$$

P_{max}: Peak pressure

M_B: mechanical load (this load was not applied in NPS 1 and less piping)

(b) secondary stress evaluation (eq.10)

$$S_{E} = \frac{iM_{c}}{Z} \le S_{A}$$

$$S_{A} = f(1.25S_{c} + 0.25S_{h})$$

i: Stress intensification factor
M_c: Thermal expansion

(c) primary plus secondary stress evaluation (eq.11)

$$S_{TE} = \frac{PD_0}{4t_n} + 0.75i(\frac{M_A}{Z}) + i(\frac{M_c}{Z}) \le (S_h + S_A)$$

Evaluation may use either (b) or (c).

(d) Building Settlement evaluation (eq.10a) $\frac{iM_{D}}{Z} \leq 3.0S_{c}$ M_D: Building Settlement load (3) Level C service limit

(a) primary stress evaluation (eq.9)

$$S_{OL} = B_1 \frac{P_{\max} D_0}{2t_n} + B_2 (\frac{M_A + M_B}{Z}) \le \min(2.25S_h, 1.8S_y)$$

P_{max}: Peak pressure

M_B: Mechanical load (this load was not applied in NPS 1 and less piping),

(4) Level D service limits

(a) Primary stress evaluation (eq.9)

$$S_{OL} = B_1 \frac{P_{\max} D_0}{2t_n} + B_2 (\frac{M_A + M_B}{Z}) \le \min(3S_h, 2S_y)$$

P_{max}: Peak pressure

M_B: Mechanical load (this load was not applied in NPS 1 and less piping), SSE seismic inertia load, DBPB load

Here, SSE seismic inertia load and DBPB load were combined by the SRSS method.

(b) Secondary stress evaluation

$$\frac{C_2 D_0 M_{AM}}{2I} \le 6.0 S_h$$

$$\frac{F_{AM}}{A_M} \le S_h$$

 M_{AM} : Range of resultant moment due to SSEA F_{AM} : Amplitude of longitudinal force due to SSEA A_M : Piping cross-sectional area

9.5 Fatigue Evaluation

The fatigue analysis was based on the rules of NB-3653 of ASME Section III. These rules require calculation of the total stress, including the peak stress, to determine the allowable number of stress cycles for the specified Service Loadings.

The design transients for ASME Level A and B service conditions (Table 8.1-3 to Table 8.1-13) were used in the evaluation of cyclic fatigue. The effect of 300 cycles of a 1/3 SSE seismic event was included in the evaluation of cyclic fatigue, treated as a Level B service condition. The number of cycles was based on equivalent fatigue usage for 20 cycles of a single SSE event.

10.0 COMPUTER PROGRAMS USED

The Table below provides a brief description of each of the computer programs used.

No.	Program Name	Version	Description	
1	PIPESTRESS	3.6.0	PIPESTRESS is a computer program for the analysis of piping systems. This program is used for the analysis of ASME Code, Section III, Class 1, 2, 3 and ASME B31.1 piping systems under various load conditions.	
2	ABAQUS	6.7.1	ABAQUS is a general-purpose finite element compute program that performs a wide range of linear and nonlinea engineering simulations. This program is used fo temperature distribution analysis and thermal stress analysis according to piping geometries and desigr transients such as fluid temperature and coefficient of hea transfer.	
3	RELAP5-3D	2.4.2	RELAP5-3D is a computer program for the fluid transient analysis. This program is used for the analysis of a behavior, such as water hammer, by modeling flow volume and flow path.	
4	P4TEDIA	1.2	P4TEDIA is an in-house program to obtain temperature difference between in-side and out-side of pipe Δ T1, Δ T2 and temperature difference at structural discontinuous point Ta-Tb. This program uses the thermal distribution analysis results generated by ABAQUS.	
5	PICEP	06/30/87	PICEP is a program developed by the Electric Power Research Institute. This program is used for predicting leakage rate from assumed through-wall cracks in the leak-before-break evaluation of piping.	

Table 10-1	Computer	Program	Description
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All these computer programs were verified and validated in compliance with the MHI quality assurance program. The computer programs were validated using one of the methods described below. Verification tests demonstrate the capability of the computer program to produce valid results for the test problems encompassing the range of permitted usage defined by the program documentation.

- Hand calculations
- Known solution for similar or standard problem
- Acceptable experimental test results
- Published analytical results
- Results from other similar verified programs

11.0 ANALYSIS RESULTS

The calculated stress-to-allowable ratio (calculated stress divided by allowable value), the cumulative fatigue usage factor, and the thermal stress ratchet results for the most limiting locations are summarized in the Table 11-1 and 11-2. The ASME Code allowable limits were satisfied in all cases.

The detailed analysis models and results for each piping system are described in the Appendix 1.

LBB evaluation was applied for Pressurizer Surge Line and it was confirmed that this line satisfies the LBB criteria using BAC as described in Appendix 1-1.

Condition	Service Level	Category	Loading	Equation (NB-3650)	Stress Limit	Stress-to- Allowable Ratio
Design	-	Primary Stress	P, DL, L _{DM} (including L _{DFN})	Eq. 9 NB-3652	1.5 S _m	
	A/B	Primary + Secondary Stress Intensity Range (SIR)	P _R , TH _{MTL} , TH _{DISCON} , L _{DFN} , L _{DFU} , SSEI, SSEA	Eq. 10 NB-3653.1	3 S _m	
		Peak SIR	P _R , TH _{MTL} , TH _{DISCON} , TH _{GRAD} , L _{DFN} , L _{DFU} , SSEI, SSEA	Eq. 11 NB-3653.2		
Normal		Thermal Bending SIR	TH _{MTL}	Eq. 12 NB-3653.6(a)	3 S _m	
/Upset		Primary + Secondary Membrane + Bending SIR	P _R , TH _{DISCON} , L _{DFN} , L _{DFU} , SSEI, SSEA	Eq. 13 NB-3653.6(b)	3 S _m	
		Alternating Stress Intensity (Fatigue)	P _R , TH _{MTL} , TH _{DISCON} , TH _{GRAD} , L _{DFN} , L _{DFU} , SSEI, SSEA	NB-3653.3 NB-3653.4 NB-3653.5 NB-3653.6(c)		
		Thermal Stress Ratchet	<i>TH_{GRAD}</i> (linear)	NB3653.7		
Upset	В	Permissible Pressure	P _M	NB-3654.1	1.1 <i>Pa</i>	
		Primary Stress	P _M , DL, L _{DFU}	NB-3654.2	Min(1.8 S_m , 1.5 S_y)	
Emergency	С	Permissible Pressure	P_M	NB-3655.1	1.5 <i>Pa</i>	
		Primary Stress	P_{M} , DL, L_{DFE}	NB-3655.2	$Min(2.25 S_m, 1.8 S_v)$	
	D	Permissible Pressure	P _M	NB-3656(b)	2 Pa	
Faulted		Primary Stress	P _M , DL, L _{DFF} SSEI, DBPB	NB-3656(a) NB-3656(b)	Appendix-F or Min(3 <i>S_m</i> ,2 <i>S_v</i>)	
Faulted	D	Secondary Stress	SSEA		6 S _m	

Table 11-1 RCL Branch Piping Result Summary (greater than 1 inch piping)

Condition	Service Level	Loading	Equation (NC-3650)	Stress Limit	Stress-to- Allowable Ratio
Design	-	P, DL	Eq. 8 NC-3652	1.5 S _h	
	A/B	P _M , DL, L _{DFN} , L _{DFU}	Eq. 9 NC-3653.1	Min(1.8 S _h , 1.5 S _y)	
Normal		TH _{MTL}	Eq. 10 NC-3653.2(a)	S _A	
/Upset		BS	Eq. 10a NC-3653.2(b)	3Sc	
		P_{M}, DL, TH_{MTL}	Eq. 11 NC-3652.2(c)	$S_h + S_A$	
Emergency	С	P _M , DL, L _{DFE}	Eq. 9 NC-3654	Min(2.25 S _h ,1.8 S _y)	
Faulted	D	P _M , DL, L _{DFF} , SSEI, DBPB	Eq. 9 NC-3655	$Min(3 S_h, 2 S_y)$	
		SSEA		6S _h	

Table 11-2 RCL Branch Piping Result Summary (1 inch or smaller than 1 inch piping)

12.0 REFERENCES

- 1. N0-GB00002 Revision 0 "Class 1 Piping ASME Design Specification (excluding RCS Main Coolant Piping)"
- 2. N0-CF00004 Revision 0 "Piping Design Criteria"
- 3. N0-GB00005 Revision 0 "Input Package of Stress Analysis of RCL Branch Piping and Main Steam Piping"
- 4. N0-EE12001 Revision 0 " Class 1 Equipment Design Transients"
- 5. ASME Boiler and Pressure Vessel Code, Section III, Division 1, 2001 Edition through 2003 Addenda
- 6. IEEE Recommended Practice for Seismic Qualification of Class 1E Equipment for Nuclear Power Generating Stations, IEEE Std 344-2004, Appendix D, Institute of Electrical and Electronic Engineers Power Engineering Society, New York, New York, June 2005.
- 7. ASME Boiler and Pressure Vessel Code, Section III, Division 1, 1992 Edition
- 8. INEL, "RELAP5-3D Code manual", 2001
- 9. DST Computer Services. S.A., "PIPESTRESS User's Manual", Version 3.6.0, 2007
- 10. SIMURIA, "ABAQUS Analysis User's Manual", Version 6.7, 2007
- 11. "Additional Information for Design Completion Plan of US-APWR Piping and Components" UAP-HF-08123, July, 2008.

Appendix 1-1

RC01 Pressurizer Surge Line

Piping Analysis Results

1.	INPUT					
	1.1 Used for creating the pipe structural model					
	1.1.1 Block division and piping specifications	Table A1-1-1-1				
	1.1.2 Piping isometrics	Figure A1-1-1-1				
	1.1.3 Concentrated mass	Table A1-1-1-2				
	1.1.4 Support point rigidity	Table A1-1-1-3				
	1.1.5 Valve rigidity	Table A1-1-1-4				
	1.2 Used for creating load conditions					
	1.2.1 Level A/B design transient	see main text				
	1.2.2 Level A/B thermal displacement input data	Table A1-1-1-5				
	1.2.3 Level A, B temperature and pressure input data	Table A1-1-1-6				
	1.2.4 Level C, D maximum temperature and pressure input data	Table A1-1-1-7				
	1.2.5 Floor response curve	Figure A1-1-1-2				
	1.2.6 Seismic anchor displacement input data	Table A1-1-1-8				
	1.2.7 DBPB displacement input data	Table A1-1-1-9				
2.	OUTPUT					
	2.1 PIPESTRESS analysis model diagram	Figure A1-1-2-1				
	2.2 Natural frequency analysis results	Table A1-1-2-1				
	2.3 Frequency mode diagram (primary to tertiary)	Figure A1-1-2-2				
	2.4 Thermal analysis results (Δ T1, Δ T2, Ta-Tb)	Table A1-1-2-2				
	2.5 Piping stress and fatigue evaluation results	Table A1-1-2-3				
	2.6 LBB evaluation results	Figure A1-1-2-3				

 Table A1-1-1-1
 Block division and piping specifications

 Table A1-1-1-2
 Concentrated mass

 Table A1-1-1-3
 Support point rigidity

 Table A1-1-1-4
 Valve rigidity

Table A1-1-1-5Level A/B thermal displacement input data (1/2)
(Point: 9010)

Table A1-1-1-5Level A/B thermal displacement input data (2/2)
(Point: 9010)

Table A1-1-1-6Level A, B temperature and pressure input data (1/3)
(Section I)

Table A1-1-1-6Level A, B temperature and pressure input data (2/3)
(Section I)

Table A1-1-1-6Level A, B temperature and pressure input data (3/3)
(Section I)

 Table A1-1-1-7
 Level C, D maximum temperature and pressure input data

Figure A1-1-1-2 Floor response curve (1/12) Pressurizer Surge Line (RC01) FRS for Piping X(EW) direction (damping 3.0%)

Figure A1-1-1-2 Floor response curve (2/12) Pressurizer Surge Line (RC01) FRS for Piping Y (NS) direction (damping 3.0%)

Figure A1-1-1-2 Floor response curve (3/12) Pressurizer Surge Line (RC01) FRS for Piping Z (Vert.) direction (damping 3.0%)

Figure A1-1-1-2 Floor response curve (4/12) Pressurizer Surge Line (RC01) FRS for MCP Nozzle X (EW) direction (damping 3.0%)

Figure A1-1-1-2 Floor response curve (5/12) Pressurizer Surge Line (RC01) FRS for MCP Nozzle Y (NS) direction (damping 3.0%)

Figure A1-1-1-2 Floor response curve (6/12) Pressurizer Surge Line (RC01) FRS for MCP Nozzle Z (Vert.) direction (damping 3.0%)

Figure A1-1-1-2 Floor response curve (7/12) Pressurizer Surge Line (RC01) FRS for Pressurizer Base Plate X (EW) direction (damping 3.0%)

Figure A1-1-1-2 Floor response curve (8/12) Pressurizer Surge Line (RC01) FRS for Pressurizer Base Plate Y (NS) direction (damping 3.0%)

Figure A1-1-1-2 Floor response curve (9/12) Pressurizer Surge Line (RC01) FRS for Pressurizer Base Plate Z (Vert.) direction (damping 3.0%)

Figure A1-1-1-2 Floor response curve (10/12) Pressurizer Surge Line (RC01) FRS for Pressurizer Support X (EW) direction (damping 3.0%)

Figure A1-1-1-2 Floor response curve (11/12) Pressurizer Surge Line (RC01) FRS for Pressurizer Support Y (NS) direction (damping 3.0%)

Figure A1-1-1-2 Floor response curve (12/12) Pressurizer Surge Line (RC01) FRS for Pressurizer Support Z (Vert.) direction (damping 3.0%)
 Table A1-1-1-8
 Seismic anchor displacement input data

 Table A1-1-1-9
 DBPB displacement input data

Figure A1-1-2-1 PIPESTRESS analysis model diagram

 Table A1-1-2-1
 Natural frequency analysis results (1/2)

 Table A1-1-2-1
 Natural frequency analysis results (2/2)

Figure A1-1-2-2 Frequency mode diagram (primary)

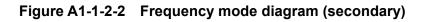


Figure A1-1-2-2 Frequency mode diagram (tertiary)

Table A1-1-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (1/3)
(Section I)



Table A1-1-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (2/3)
(Section I)

Table A1-1-2-2Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (3/3)
(Section I)

Table A1-1-2-3Piping stress and fatigue evaluation results
(Piping that exceeds 1 inch NB–3650 evaluation)

Table A1-1-2-3Piping stress and fatigue evaluation results(Piping of 1 inch or less NC-3650 evaluation)

Figure A1-1-2-3 LBB evaluation results

Appendix 1-2

RC02 Pressurizer Spray Line

Piping Analysis Results

1. INPUT

	 1.1 Used for creating the pipe structural model 1.1.1 Block division and piping specifications 1.1.2 Piping isometrics 1.1.3 Concentrated mass 1.1.4 Support point rigidity 1.1.5 Valve rigidity 1.2 Used for creating load conditions 	Table A1-2-1-1 Figure A1-2-1-1 Table A1-2-1-2 Table A1-2-1-3 Table A1-2-1-4
	 1.2.1 Level A/B design transient 1.2.2 Level A/B thermal displacement input data 1.2.3 Level A, B temperature and pressure input data 1.2.4 Level C, D maximum temperature and pressure input data 1.2.5 Floor response curve 1.2.6 Seismic relative displacement input data 1.2.7 DBPB displacement input data 	see main text Table A1-2-1-5 Table A1-2-1-6 Table A1-2-1-7 Figure A1-2-1-2 Table A1-2-1-8 Table A1-2-1-9
2.	OUTPUT 2.1 PIPESTRESS analysis Model diagram 2.2 Natural frequency analysis results 2.3 Frequency mode diagram (primary to tertiary) 2.4 Thermal analysis results (Δ T1, Δ T2, Ta-Tb) 2.5 Piping stress and fatigue evaluation results	Figure A1-2-2-1 Table A1-2-2-1 Figure A1-2-2-2 Table A1-2-2-2 Table A1-2-2-3

2.5 Piping stress and fatigue evaluation results

 Table A1-2-1-1
 Block division and piping specifications (1/2)

 Table A1-2-1-1
 Block division and piping specifications (2/2)

Table A1-2-1-2 Concentrated mass

 Table A1-2-1–3
 Support point rigidity

Table A1-2-1-4Valve rigidity

Table A1-2-1-5Level A/B thermal displacement input data (1/4)
(Point: 9010)

Table A1-2-1-5Level A/B thermal displacement input data (2/4)(Point: 9010)

Table A1-2-1-5Level A/B thermal displacement input data (3/4)
(Point: 9020)

Table A1-2-1-5Level A/B thermal displacement input data (4/4)(Point: 9020)

Table A1-2-1-6Level A, B temperature and pressure input data(1/15)(Section I, IX, X)

Table A1-2-1-6Level A, B temperature and pressure input data(2/15)(Section I , IX , X)

Table A1-2-1-6Level A, B temperature and pressure input data(3/15)(Section I , IX , X)

 Table A1-2-1-6
 Level A, B temperature and pressure input data(4/15) (Section II , III)

 Table A1-2-1-6
 Level A, B temperature and pressure input data(5/15) (Section II , III)

 Table A1-2-1-6
 Level A, B temperature and pressure input data(6/15) (Section II , III)
 Table A1-2-1-6Level A, B temperature and pressure input data(7/15)(Section IV , V , VI , VII , VII)

Table A1-2-1-6Level A, B temperature and pressure input data(8/15)(Section IV , V , VI , VII , VII)

Table A1-2-1-6Level A, B temperature and pressure input data(9/15)(Section IV , V , VI , VII , VII)

 Table A1-2-1-6
 Level A, B temperature and pressure input data(10/15) (Section XI)

 Table A1-2-1-6
 Level A, B temperature and pressure input data(11/15) (Section XI)
 Table A1-2-1-6Level A, B temperature and pressure input data(12/15)(Section XI)

 Table A1-2-1-6
 Level A, B temperature and pressure input data(13/15) (Section XII)

 Table A1-2-1-6
 Level A, B temperature and pressure input data(14/15) (Section XII)

 Table A1-2-1-6
 Level A, B temperature and pressure input data(15/15) (Section XII)

 Table A1-2-1-7
 Level C, D maximum temperature and pressure input data

Figure A1-2-1-2 Floor response curve (1/12) Pressurizer Spray Line (RC02) FRS for piping X (EW) direction (damping 3.0%)

Figure A1-2-1-2 Floor response curve (2/12) Pressurizer Spray Line (RC02) FRS for piping Y (NS) direction (damping 3.0%)

Figure A1-2-1-2 Floor response curve (3/12) Pressurizer Spray Line (RC02) FRS for piping Z (Vert.) direction (damping 3.0%)

Figure A1-2-1-2 Floor response curve (4/12) Pressurizer Spray Line (RC02) FRS for MCP nozzle X (EW) direction (damping 3.0%)

Figure A1-2-1-2 Floor response curve (5/12) Pressurizer Spray Line (RC02) FRS for MCP nozzle Y (NS) direction (damping 3.0%)

Figure A1-2-1-2 Floor response curve (6/12) Pressurizer Spray Line (RC02) FRS for MCP nozzle Z (Vert.) direction (damping 3.0%)

Figure A1-2-1-2 Floor response curve (7/12) Pressurizer Spray Line (RC02) FRS for Pressurizer base plate X (EW) direction (damping 3.0%)

Figure A1-2-1-2 Floor response curve (8/12) Pressurizer Spray Line (RC02) FRS for Pressurizer base plate Y (NS) direction (damping 3.0%)

Figure A1-2-1-2 Floor response curve (9/12) Pressurizer Spray Line (RC02) FRS for Pressurizer base plate Z (Vert.) direction (damping 3.0%)

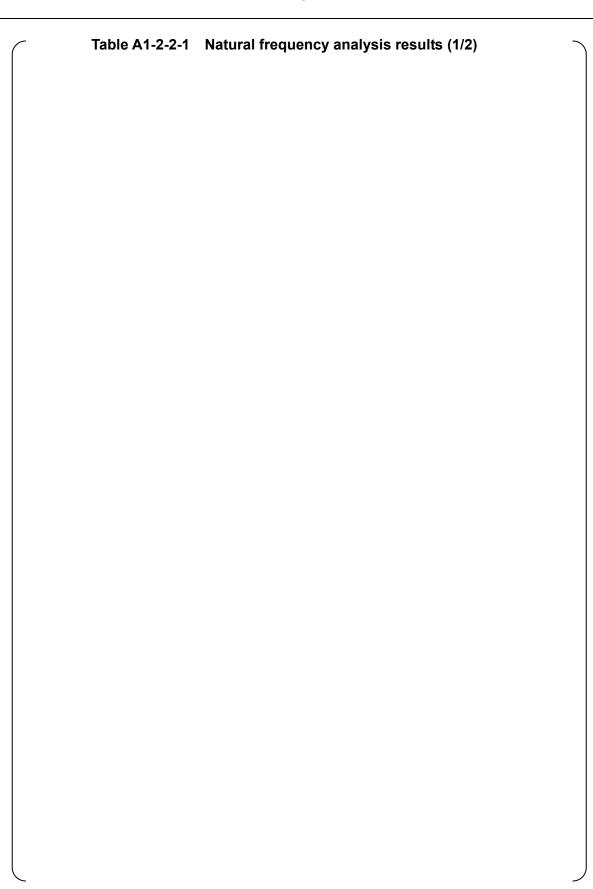
Figure A1-2-1-2 Floor response curve (10/12) Pressurizer Spray Line (RC02) FRS for Pressurizer support X (EW) direction (damping 3.0%)

Figure A1-2-1-2 Floor response curve (11/12) Pressurizer Spray Line (RC02) FRS for Pressurizer support Y (NS) direction (damping 3.0%)

Figure A1-2-1-2 Floor response curve (12/12) Pressurizer Spray Line (RC02) FRS for Pressurizer support Z (Vert.) direction (damping 3.0%)
 Table A1-2-1-8
 Seismic relative displacement input data

 Table A1-2-1-9
 DBPB displacement input data









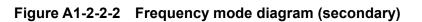




Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (1/33)
(Section I)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (2/33)
(Section I)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (3/33)
(Section I)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (4/33)
(Section II)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (5/33)
(Section II)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (6/33)
(Section II)

Table A1-2-2-2Thermal analysis results (Δ T1, Δ T2, Ta-Tb)(7/33)(Section III)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (8/33)(Section III)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (9/33)
(Section III)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb)(10/33)
(Section IV)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb)(11/33)
(Section IV)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (12/33)
(Section IV)

Table A1-2-2-2 Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (13/33) (Section V)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb)(14/33)
(Section V)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (15/33)
(Section V)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (16/33)
(Section VI)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (17/33)
(Section VI)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (18/33)
(Section VI)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (19/33)
(Section VII)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (20/33)
(Section VII)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (21/33)
(Section VII)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (22/33)
(Section VIII)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (23/33)
(Section VIII)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (24/33)
(Section VIII)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (25/33)
(Section IX)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (26/33)
(Section IX)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (27/33)
(Section IX)

Table A1-2-2-2Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (28/33)
(Section X)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (29/33)
(Section X)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (30/33)
(Section X)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (31/33)
(Section XI)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (32/33)
(Section XI)

Table A1-2-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (33/33)
(Section XI)

Table A1-2-2-3Piping stress and fatigue evaluation results
(Piping that exceeds 1 inch NB–3650 evaluation)

Table A1-2-2-3Piping stress and fatigue evaluation results(Piping of 1 inch or less NC-3650 evaluation)

Appendix 1-3

RC03 Pressurizer Safety Depressurization Valve Line

Piping Analysis Results

1.	INPUT	
	1.1 Used for creating the pipe structural model	
	1.1.1 Block division and piping specifications	Table A1-3-1-1
	1.1.2 Piping isometrics	Figure A1-3-1-1
	1.1.3 Concentrated mass	Table A1-3-1-2
	1.1.4 Support point rigidity	Table A1-3-1-3
	1.1.5 Valve rigidity	Table A1-3-1-4
	1.2 Used for creating load conditions	
	1.2.1 Level A/B design transient	see main text
	1.2.2 Level A/B thermal displacement input data	Table A1-3-1-5
	1.2.3 Level A, B temperature and pressure input data	Table A1-3-1-6
	1.2.4 Level C, D maximum temperature and pressure input data	Table A1-3-1-7
	1.2.5 Floor response curve	Figure A1-3-1-2
	1.2.6 Seismic anchor displacement input data	Table A1-3-1-8
	1.2.7 DBPB displacement input data	Table A1-3-1-9
	1.2.8 Initial condition and valve open characteristics (Water hammer)	Table A1-3-1-10
2.	OUTPUT	
2.	2.1 PIPESTRESS analysis model diagram	Figure A1-3-2-1
	2.2 Water hammer analysis model diagram	Figure A1-3-2-2
	2.3 Natural frequency analysis results	Table A1-3-2-1
	2.4 Frequency mode diagram (primary to tertiary)	Figure A1-3-2-3
	2.5 Thermal analysis results ($\Delta T1$, $\Delta T2$, Ta-Tb)	Table A1-3-2-2

- 2.5 Thermal analysis results (Δ T1, Δ T2, Ta-Tb)
- 2.6 Piping stress and fatigue evaluation results

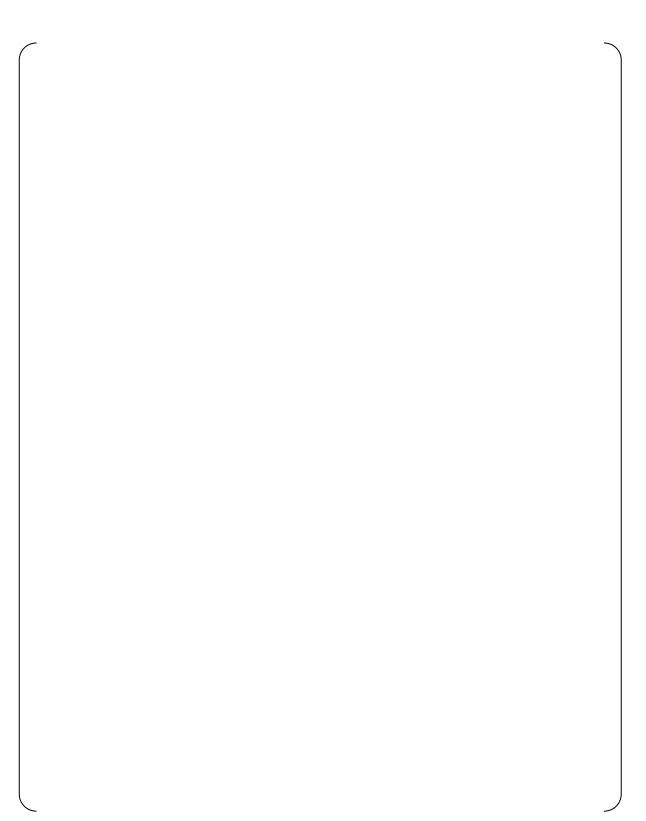
Mitsubishi Heavy Industries, LTD.

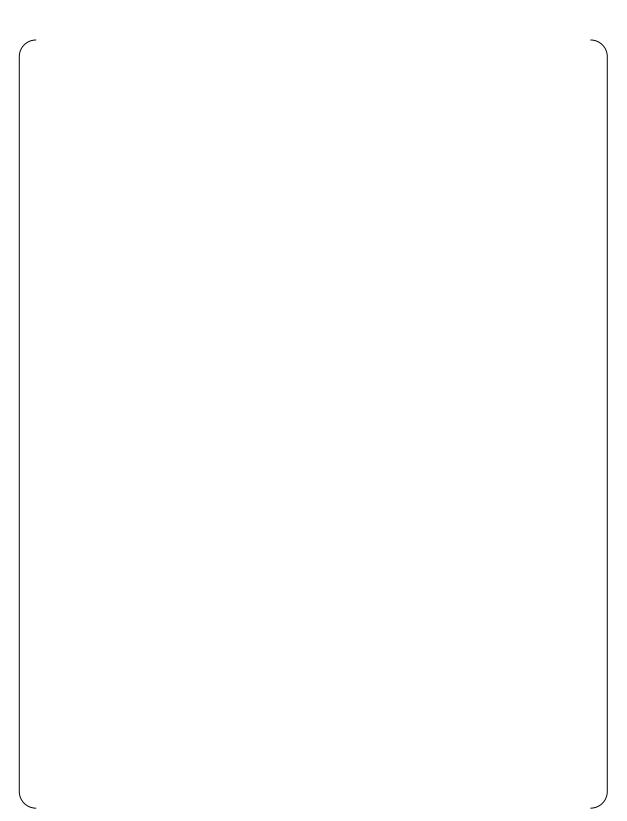
Table A1-3-2-3

 Table A1-3-1-1
 Block division and piping specifications (1/3)

 Table A1-3-1-1
 Block division and piping specifications (2/3)

 Table A1-3-1-1
 Block division and piping specifications (3/3)







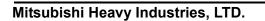


 Table A1-3-1-3
 Support point rigidity

 Table A1-3-1-4
 Valve rigidity

Table A1-3-1-5 Level A/B thermal displacement input data (Point: -)

Table A1-3-1-6Level A, B temperature and pressure input data (1/21)
(Section I)

Table A1-3-1-6Level A, B temperature and pressure input data (2/21)
(Section I)

 Table A1-3-1-6
 Level A, B temperature and pressure input data (3/21) (Section I)
 Table A1-3-1-6Level A, B temperature and pressure input data (4/21)
(Section II)

 Table A1-3-1-6
 Level A, B temperature and pressure input data (5/21) (Section II)

 Table A1-3-1-6
 Level A, B temperature and pressure input data (6/21) (Section II)

 Table A1-3-1-6
 Level A, B temperature and pressure input data (7/21) (Section III)

 Table A1-3-1-6
 Level A, B temperature and pressure input data (8/21) (Section III)

 Table A1-3-1-6
 Level A, B temperature and pressure input data (9/21) (Section III)
 Table A1-3-1-6Level A, B temperature and pressure input data (10/21)
(Section IV)

Table A1-3-1-6Level A, B temperature and pressure input data (11/21)
(Section IV)

Table A1-3-1-6Level A, B temperature and pressure input data (12/21)
(Section IV)

Table A1-3-1-6Level A, B temperature and pressure input data (13/21)
(Section V)

Table A1-3-1-6Level A, B temperature and pressure input data (14/21)
(Section V)

Table A1-3-1-6Level A, B temperature and pressure input data (15/21)
(Section V)

Table A1-3-1-6Level A, B temperature and pressure input data (16/21)
(Section VI)

 Table A1-3-1-6
 Level A, B temperature and pressure input data (17/21) (Section VI)
 Table A1-3-1-6Level A, B temperature and pressure input data (18/21)
(Section VI)

 Table A1-3-1-6
 Level A, B temperature and pressure input data (19/21) (Section VII)

 Table A1-3-1-6
 Level A, B temperature and pressure input data (20/21) (Section VII)

 Table A1-3-1-6
 Level A, B temperature and pressure input data (21/21) (Section VII)

 Table A1-3-1-7
 Level C, D maximum temperature and pressure input data

Figure A1-3-1-2 Floor response curve (1/9) Pressurizer Safety Depressurization Valve Line (RC03) FRS for Pressurizer base plate X (EW) direction (damping 3.0%)

Figure A1-3-1-2 Floor response curve (2/6) Pressurizer Safety Depressurization Valve Line (RC03) FRS for Pressurizer base plate Y (NS) direction (damping 3.0%)

Figure A1-3-1-2 Floor response curve (3/9) Pressurizer Safety Depressurization Valve Line (RC03) FRS for Pressurizer base plate Z (Vert.) direction (damping 3.0%)

Figure A1-3-1-2Floor response curve (4/9)Pressurizer Safety Depressurization Valve Line (RC03) FRS for Pressurizer support
X (EW) direction (damping 3.0%)

Figure A1-3-1-2 Floor response curve (5/9) Pressurizer Safety Depressurization Valve Line (RC03) FRS for Pressurizer support Y (NS) direction (damping 3.0%)

Figure A1-3-1-2 Floor response curve (6/9) Pressurizer Safety Depressurization Valve Line (RC03) FRS for Pressurizer support Z (Vert.) direction (damping 3.0%)

Figure A1-3-1-2 Floor response curve (7/9) Pressurizer Safety Depressurization Valve Line (RC03) FRS for Piping X (EW) direction (damping 3.0%)

Figure A1-3-1-2 Floor response curve (8/9) Pressurizer Safety Depressurization Valve Line (RC03) FRS for Piping Y (NS) direction (damping 3.0%)

Figure A1-3-1-2 Floor response curve (9/9) Pressurizer Safety Depressurization Valve Line (RC03) FRS for Piping Z (Vert.) direction (damping 3.0%)
 Table A1-3-1-8
 Seismic anchor displacement input data

 Table A1-3-1-9
 DBPB displacement input data

 Table A1-3-1-10
 Initial condition and valve open characteristics (Water hammer)

Figure A1-3-2-1 PIPESTRESS analysis model diagram

Figure A1-3-2-2 Water hammer analysis model diagram (1/2) Analysis model for Pressurizer safety depressurization valve water hammer calculation

Figure A1-3-2-2Water hammer analysis model diagram (2/2)Analysis model for Pressurizer safety valve water hammer calculation

 Table A1-3-2-1
 Natural frequency analysis results

Figure A1-3-2-3 Frequency mode diagram (primary)

Figure A1-3-2-3 Frequency mode diagram (secondary)

Figure A1-3-2-3 Frequency mode diagram (tertiary)

Table A1-3-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (1/15)
(Section I)

Table A1-3-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (2/15)
(Section I)

Table A1-3-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (3/15)
(Section I)

Table A1-3-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (4/15)(Section II)

Table A1-3-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (5/15)
(Section II)

Table A1-3-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (6/15)(Section II)

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Table A1-3-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (7/15)(Section III)

Table A1-3-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (8/15)(Section III)

Table A1-3-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (9/15)(Section III)

Table A1-3-2-2Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (10/15)
(Section IV)

Table A1-3-2-2Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (11/15)
(Section IV)

Table A1-3-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (12/15)
(Section IV)

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Table A1-3-2-2Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (13/15)
(Section V)

Table A1-3-2-2 Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (14/15) (Section V)

Table A1-3-2-2Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (15/15)
(Section V)

Table A1-3-2-3Piping stress and fatigue evaluation results
(Piping that exceeds 1 inch NB–3650 evaluation)

Table A1-3-2-3Piping stress and fatigue evaluation results(Piping of 1 inch or less NC-3650 evaluation)

Appendix 1-4

RC04 Pressurizer Safety Valve Line

Piping Analysis Results

Table A1-4-2-2

Table A1-4-2-3

1.	INPUT	
	1.1 Used for creating the pipe structural model	
	1.1.1 Block division and piping specifications	Table A1-4-1-1
	1.1.2 Piping isometrics	Figure A1-4-1-1
	1.1.3 Concentrated mass	Table A1-4-1-2
	1.1.4 Support point rigidity	Table A1-4-1-3
	1.1.5 Valve rigidity	Table A1-4-1-4
	1.2 Used for creating load conditions	
	1.2.1 Level A/B design transient	see main text
	1.2.2 Level A/B thermal displacement input data	Table A1-4-1-5
	1.2.3 Level A, B temperature and pressure input data	Table A1-4-1-6
	1.2.4 Level C, D maximum temperature and pressure input data	Table A1-4-1-7
	1.2.5 Floor response curve	Figure A1-4-1-2
	1.2.6 Seismic anchor displacement input data	Table A1-4-1-8
	1.2.7 DBPB displacement input data	Table A1-4-1-9
	1.2.8 Initial condition and valve open characteristics (Water hammer)	Table A1-4-1-10
2.	OUTPUT	
	2.1 PIPESTRESS analysis model diagram	Figure A1-4-2-1
	2.2 Water hammer analysis model diagram	Figure A1-4-2-2
	2.3 Natural frequency analysis results	Table A1-4-2-1
	2.4 Frequency mode diagram (primary to tertiary)	Figure A1-4-2-3

- 2.4 Frequency mode diagram (primary to tertiary) 2.5 Thermal analysis results (Δ T1, Δ T2, Ta-Tb)
- 2.6 Piping stress and fatigue evaluation results

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 Table A1-4-1-1
 Block division and piping specifications

Table A1-4-1-2 Concentrated mass

 Table A1-4-1-3
 Support point rigidity

 Table A1-4-1-4
 Valve rigidity

Table A1-4-1-5 Level A/B thermal displacement input data (1/1) (Point: -)

Table A1-4-1-6 Level A, Btemperature and pressure input data (1/6)(Section I)

Table A1-4-1-6Level A, B temperature and pressure input data (2/6)(Section I)

Table A1-4-1-6Level A, B temperature and pressure input data (3/6)(Section I)

Table A1-4-1-6Level A, B temperature and pressure input data (4/6)(Section II)

Table A1-4-1-6Level A, B temperature and pressure input data (5/6)(Section II)

Table A1-4-1-6Level A, B temperature and pressure input data (6/6)(Section II)

 Table A1-4-1-7
 Level C, D maximum temperature and pressure input data

Figure A1-4-1-2 Floor response curve (1/4) Pressurizer Safety Valve Line (RC04-07) FRS for PZR Base Plate X-Y direction envelope (damping 3.0%)

Figure A1-4-1-2 Floor response curve (2/4) Pressurizer Safety Valve Line (RC04-07) FRS for PZR Base Plate Z (Vert.) direction (damping 3.0%)

Figure A1-4-1-2 Floor response curve (3/4) Pressurizer Safety Valve Line (RC04-07) FRS for PZR Support X-Y direction envelope (damping 3.0%)

Figure A1-4-1-2 Floor response curve (4/4) Pressurizer Safety Valve Line (RC04-07) FRS for PZR Support Z (Vert.) direction (damping 3.0%)
 Table A1-4-1-8
 Seismic anchor displacement input data

 Table A1-4-1-9
 DBPB displacement input data

 Table A1-4-1-10
 Initial condition and valve open characteristics (Water hammer)

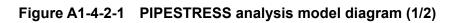


Figure A1-4-2-1 PIPESTRESS analysis model diagram (2/2)

Figure A1-4-2-2 Water hammer analysis model diagram Analysis model for Pressurizer safety valve water hammer calculation

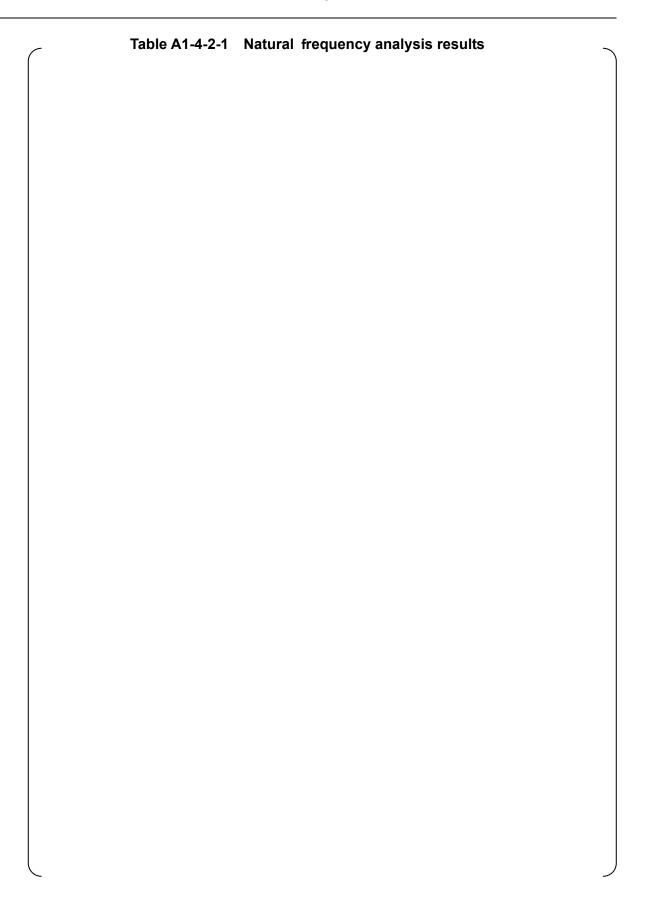


Figure A1-4-2-3 Frequency mode diagram (primary)

Figure A1-4-2-3 Frequency mode diagram (secondary)



Table A1-4-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (1/6)(Section I)

Table A1-4-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (2/6)(Section I)

Table A1-4-2-2Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (3/6)(Section I)

Table A1-4-2-2Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (4/6)(Section II)

Table A1-4-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (5/6)(Section II)

Table A1-4-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (6/6)(Section II)

Table A1-4-2-3Piping stress and fatigue evaluation results(Piping that exceeds 1 inch NB–3650 evaluation)

Table A1-4-2-3Piping stress and fatigue evaluation results(Piping of 1 inch or less NC-3650 evaluation)

Appendix 1-5

RH01 RHRS Suction Loop A Line

Piping Analysis Results

Table A1-5-1-1

Figure A1-5-1-1

Table A1-5-1-2

Table A1-5-1-3

Table A1-5-1-4

see main text

Table A1-5-1-5

Table A1-5-1-6

Table A1-5-1-7

Figure A1-5-1-2

Table A1-5-1-8

Table A1-5-1-9

Figure A1-5-2-1

Table A1-5-2-1

Figure A1-5-2-2

Table A1-5-2-2

Table A1-5-2-3

- 1.1 Used for creating the pipe structural model
 - 1.1.1 Block division and piping specifications
 - 1.1.2 Piping isometrics
 - 1.1.3 Concentrated mass
 - 1.1.4 Support point rigidity
 - 1.1.5 Valve rigidity
- 1.2 Used for creating load conditions
 - 1.2.1 Level A/B design transient
 - 1.2.2 Level A/B thermal displacement input data
 - 1.2.3 Level A, B temperature and pressure input data
 - 1.2.4 Level C, D maximum temperature and pressure input data
 - 1.2.5 Floor response curve
 - 1.2.6 Seismic anchor displacement input data
 - 1.2.7 DBPB displacement input data
- 2. OUTPUT

2.1 PIPESTRESS analysis model dia	agram
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- 2.2 Natural frequency analysis results
- 2.3 Frequency mode diagram (primary to tertiary)
- 2.4 Thermal analysis results (Δ T1, Δ T2, Ta-Tb)
- 2.5 Piping stress and fatigue evaluation results

 Table A1-5-1-1
 Block division and piping specifications (1/3)

 Table A1-5-1-1
 Block division and piping specifications (2/3)

 Table A1-5-1-1
 Block division and piping specifications (3/3)

Table A1-5-1-2 Concentrated mass

 Table A1-5-1-3
 Support point rigidity

 Table A1-5-1-4
 Valve rigidity

Table A1-5-1-5Level A/B thermal displacement input data (1/3)
(Point: 9010)

Table A1-5-1-5Level A/B thermal displacement input data (2/3)
(Point: 9010)

Table A1-5-1-5Level A/B thermal displacement input data (3/3)
(Point: 9010)

Table A1-5-1-6Level A, B temperature and pressure input data (1/33)
(Section I)

Table A1-5-1-6Level A, B temperature and pressure input data (2/33)
(Section I)

Table A1-5-1-6Level A, B temperature and pressure input data (3/33)(Section I)

 Table A1-5-1-6
 Level A, B temperature and pressure input data (4/33) (Section II)

 Table A1-5-1-6
 Level A, B temperature and pressure input data (5/33) (Section II)
 Table A1-5-1-6Level A, B temperature and pressure input data (6/33)
(Section II)

 Table A1-5-1-6
 Level A, B temperature and pressure input data (7/33) (Section III)

 Table A1-5-1-6
 Level A, B temperature and pressure input data (8/33) (Section III)

 Table A1-5-1-6
 Level A, B temperature and pressure input data (9/33) (Section III)
 Table A1-5-1-6Level A, B temperature and pressure input data (10/33)
(Section IV)

 Table A1-5-1-6
 Level A, B temperature and pressure input data (11/33) (Section IV)
 Table A1-5-1-6Level A, B temperature and pressure input data (12/33)
(Section IV)

Table A1-5-1-6Level A, B temperature and pressure input data (13/33)
(Section V)

Table A1-5-1-6Level A, B temperature and pressure input data (14/33)
(Section V)

Table A1-5-1-6Level A, B temperature and pressure input data (15/33)
(Section V)

 Table A1-5-1-6
 Level A, B temperature and pressure input data (16/33) (Section VI)

 Table A1-5-1-6
 Level A, B temperature and pressure input data (17/33) (Section VI)

 Table A1-5-1-6
 Level A, B temperature and pressure input data (18/33) (Section VI)

 Table A1-5-1-6
 Level A, B temperature and pressure input data (19/33) (Section VII)

 Table A1-5-1-6
 Level A, B temperature and pressure input data (20/33) (Section VII)

 Table A1-5-1-6
 Level A, B temperature and pressure input data (21/33) (Section VII)

 Table A1-5-1-6
 Level A, B temperature and pressure input data (22/33) (Section VIII)

 Table A1-5-1-6
 Level A, B temperature and pressure input data (23/33) (Section VIII)

 Table A1-5-1-6
 Level A, B temperature and pressure input data (24/33) (Section VIII)

 Table A1-5-1-6
 Level A, B temperature and pressure input data (25/33) (Section IX)

 Table A1-5-1-6
 Level A, B temperature and pressure input data (26/33) (Section IX)

 Table A1-5-1-6
 Level A, B temperature and pressure input data (27/33) (Section IX)
 Table A1-5-1-6Level A, B temperature and pressure input data (28/33)
(Section X)

Table A1-5-1-6Level A, B temperature and pressure input data (29/33)
(Section X)

 Table A1-5-1-6
 Level A, B temperature and pressure input data (30/33) (Section X)
 Table A1-5-1-6Level A, B temperature and pressure input data (31/33)
(Section XI)

Table A1-5-1-6Level A, B temperature and pressure input data (32/33)
(Section XI)

Table A1-5-1-6Level A, B temperature and pressure input data (33/33)
(Section XI)

 Table A1-5-1-7
 Level C, D maximum temperature and pressure input data

Figure A1-5-1-2 Floor response curve (1/6) RHRS Suction (RH01-02) FRS for MCP Nozzle X (EW) direction (damping 4.0%)

Figure A1-5-1-2 Floor response curve (2/6) RHRS Suction (RH01-02) FRS for MCP Nozzle Y (NS) direction (damping 4.0%)

Figure A1-5-1-2 Floor response curve (3/6) RHRS Suction (RH01-02) FRS for MCP Nozzle Z (Vert.) direction (damping 4.0%)

Figure A1-5-1-2 Floor response curve (4/6)

RHRS Suction (RH01-02) FRS for Piping X (EW) direction (damping 4.0%)

Figure A1-5-1-2 Floor response curve (5/6) RHRS Suction (RH01-02) FRS for Piping

Y (NS) direction (damping 4.0%)

Figure A1-5-1-2 Floor response curve (6/6) RHRS Suction (RH01-02) FRS for Piping

Z (Vert.) direction (damping 4.0%)

 Table A1-5-1-8
 Seismic anchor displacement input data

 Table A1-5-1-9
 DBPB displacement input data



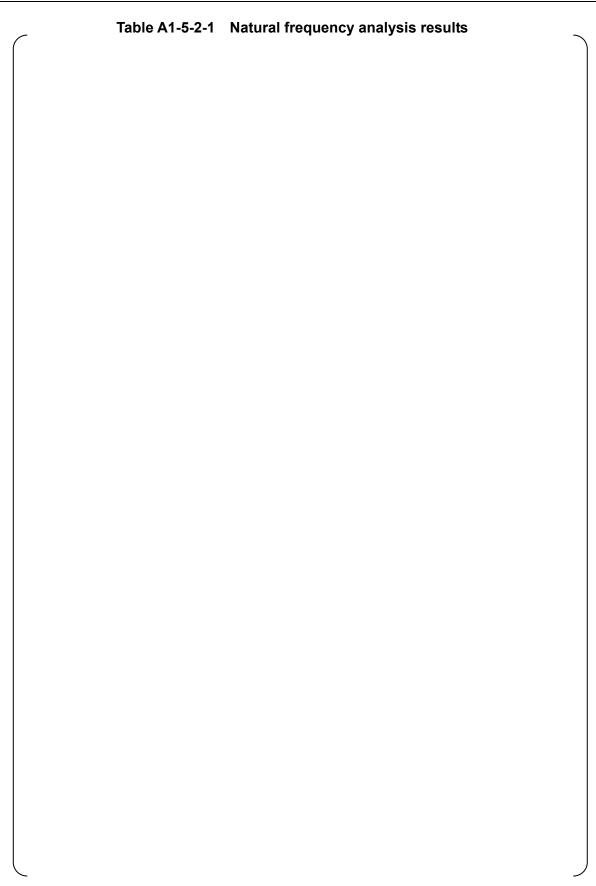




Figure A1-5-2-2 Frequency mode diagram (primary)

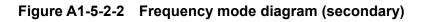


Figure A1-5-2-2 Frequency mode diagram (tertiary)

Table A1-5-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (1/21)
(Section I)

Table A1-5-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (2/21)
(Section I)

Table A1-5-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (3/21)
(Section I)

Table A1-5-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (4/21)
(Section II)

Table A1-5-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (5/21)(Section II)

Table A1-5-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (6/21)(Section II)

Table A1-5-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (7/21)(Section III)

Table A1-5-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (8/21)(Section III)

Table A1-5-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (9/21)(Section III)

Table A1-5-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (10/21)
(Section IV)

Table A1-5-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (11/21)
(Section IV)

Table A1-5-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (12/21)
(Section IV)

Table A1-5-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (13/21)
(Section V)

Table A1-5-2-2 Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (14/21) (Section V)

Table A1-5-2-2Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (15/21)
(Section V)

Table A1-5-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (16/21)
(Section VI)

Table A1-5-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (17/21)
(Section VI)

Table A1-5-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (18/21)
(Section VI)

Table A1-5-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (19/21)(Section VII)

Table A1-5-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (20/21)(Section VII)

Table A1-5-2-2Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (21/21)(Section VII)

Table A1-5-2-3Piping stress and fatigue evaluation results
(Piping that exceeds 1 inch NB-3650 evaluation)

Table A1-5-2-3Piping stress and fatigue evaluation results
(Piping of 1 inch or less NC-3650 evaluation)

Appendix 1-6

RH02 RHRS suction Loop B Line

Piping Analysis Results

1.	INPUT

- 1.1 Used for creating the pipe structural model
 - 1.1.1 Block division and piping specifications
 - 1.1.2 Piping isometrics
 - 1.1.3 Concentrated mass
 - 1.1.4 Support point rigidity
 - 1.1.5 Valve rigidity
- 1.2 Used for creating load conditions
 - 1.2.1 Level A/B design transient
 - 1.2.2 Level A/B thermal displacement input data
 - 1.2.3 Level A, B temperature and pressure input data
 - 1.2.4 Level C, D maximum temperature and pressure input data
 - 1.2.5 Floor response curve
 - 1.2.6 Seismic anchor displacement input data
 - 1.2.7 DBPB displacement input data
- 2. OUTPUT
 - 2.1 PIPESTRESS analysis model diagram
 - 2.2 Natural frequency analysis results
 - 2.3 Frequency mode diagram (primary to tertiary)
 - 2.4 Thermal analysis results (Δ T1, Δ T2, Ta-Tb)
 - 2.5 Piping stress and fatigue evaluation results

- Table A1-6-1-1 Figure A1-6-1-1 Table A1-6-1-2 Table A1-6-1-3 Table A1-6-1-4
- see main text Table A1-6-1-5 Table A1-6-1-6 Table A1-6-1-7 Figure A1-6-1-2 Table A1-6-1-8 Table A1-6-1-9
- Figure A1-6-2-1 Table A1-6-2-1 Figure A1-6-2-2 Table A1-6-2-2 Table A1-6-2-3

 Table A1-6-1-1
 Block division and piping specifications (1/2)

 Table A1-6-1-1
 Block division and piping specifications (2/2)

Table A1-6-1-2 Concentrated mass

Table A1-6-1-3 Support point rigidity

 Table A1-6-1-4
 Valve rigidity

Table A1-6-1-5Level A/B thermal displacement input data (1/3)
(Point: 9010)

Table A1-6-1-5Level A/B thermal displacement input data (2/3)
(Point: 9010)

Table A1-6-1-5Level A/B thermal displacement input data (3/3)
(Point: 9010)

Table A1-6-1-6Level A, B temperature and pressure input data (1/21)(Section I)

Table A1-6-1-6Level A, B temperature and pressure input data (2/21)(Section I)

 Table A1-6-1-6
 Level A, B temperature and pressure input data (3/21) (Section I)

 Table A1-6-1-6
 Level A, B temperature and pressure input data (4/21) (Section II)

 Table A1-6-1-6
 Level A, B temperature and pressure input data (5/21) (Section II)

 Table A1-6-1-6
 Level A, B temperature and pressure input data (6/21) (Section II)

 Table A1-6-1-6
 Level A, B temperature and pressure input data (7/21) (Section III)

 Table A1-6-1-6
 Level A, B temperature and pressure input data (8/21) (Section III)

 Table A1-6-1-6
 Level A, B temperature and pressure input data (9/21) (Section III)
 Table A1-6-1-6Level A, B temperature and pressure input data (10/21)
(Section IV)

Table A1-6-1-6Level A, B temperature and pressure input data (11/21)
(Section IV)

Table A1-6-1-6Level A, B temperature and pressure input data (12/21)
(Section IV)

Table A1-6-1-6Level A, B temperature and pressure input data (13/21)
(Section V)

Table A1-6-1-6Level A, B temperature and pressure input data (14/21)
(Section V)

Table A1-6-1-6Level A, B temperature and pressure input data (15/21)
(Section V)

 Table A1-6-1-6
 Level A, B temperature and pressure input data (16/21) (Section VI)

 Table A1-6-1-6
 Level A, B temperature and pressure input data (17/21) (Section VI)

 Table A1-6-1-6
 Level A, B temperature and pressure input data (18/21) (Section VI)

 Table A1-6-1-6
 Level A, B temperature and pressure input data (19/21) (Section VII)

 Table A1-6-1-6
 Level A, B temperature and pressure input data (20/21) (Section VII)

 Table A1-6-1-6
 Level A, B temperature and pressure input data (21/21) (Section VII)

 Table A1-6-1-7
 Level C, D maximum temperature and pressure input data

Figure A1-6-1-2 Floor response curve (1/6) RHRS Suction (RH01-02) FRS for MCP Nozzle X (EW) direction (damping 4.0%)

Figure A1-6-1-2 Floor response curve (2/6) RHRS Suction (RH01-02) FRS for MCP Nozzle Y (NS) direction (damping 4.0%)

Figure A1-6-1-2 Floor response curve (3/6) RHRS Suction (RH01-02) FRS for MCP Nozzle Z (Vert.) direction (damping 4.0%)

Figure A1-6-1-2 Floor response curve (4/6) RHRS Suction (RH01-02) FRS for Piping

X (EW) direction (damping 4.0%)

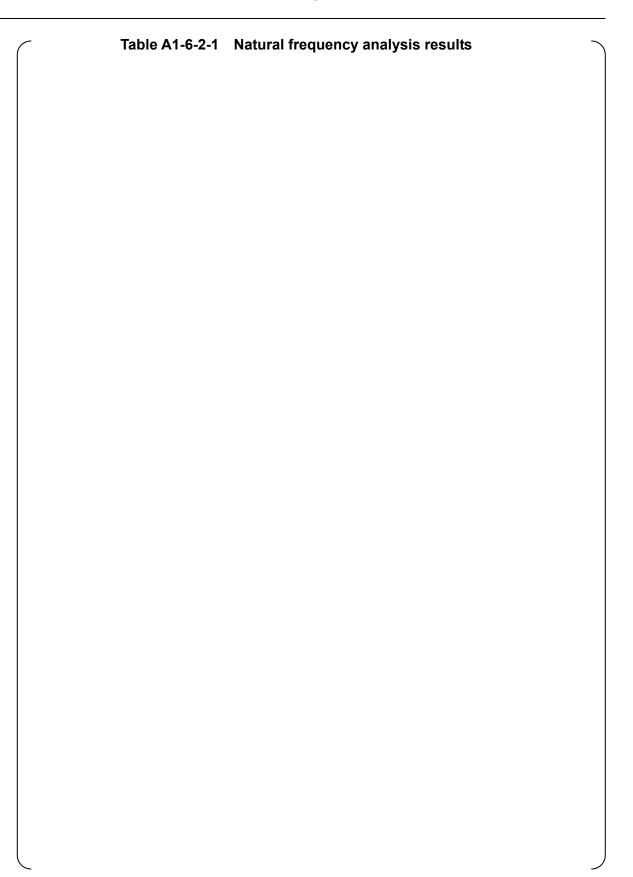
Figure A1-6-1-2 Floor response curve (5/6) RHRS Suction (RH01-02) FRS for Piping

Y (NS) direction (damping 4.0%)

Figure A1-6-1-2 Floor response curve (6/6) RHRS Suction (RH01-02) FRS for Piping Z (Vert.) direction (damping 4.0%)
 Table A1-6-1-8
 Seismic anchor displacement input data

 Table A1-6-1-9
 DBPB displacement input data





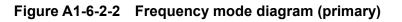


Figure A1-6-2-2 Frequency mode diagram (secondary)

Figure A1-6-2-2 Frequency mode diagram (tertiary)

Table A1-6-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (1/15)
(Section I)

Table A1-6-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (2/15)
(Section I)

Table A1-6-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (3/15)
(Section I)

Table A1-6-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (4/15)(Section II)

Table A1-6-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (5/15)(Section II)

Table A1-6-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (6/15)(Section II)

Table A1-6-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (7/15)(Section III)

Table A1-6-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (8/15)(Section III)

Table A1-6-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (9/15)(Section III)

Table A1-6-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (10/15)(Section IV)

Table A1-6-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (11/15)(Section IV)

Table A1-6-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (12/15)(Section IV)

Table A1-6-2-2Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (13/15)
(Section V)

Table A1-6-2-2Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (14/15)
(Section V)

Table A1-6-2-2Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (15/15)
(Section V)

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Table A1-6-2-3Piping stress and fatigue evaluation results
(Piping that exceeds 1 inch NB-3650 evaluation)

Table A1-6-2-3Piping stress and fatigue evaluation results
(Piping of 1 inch or less NC-3650 evaluation)

Appendix 1-7

SI01 Accumulator Loop A Line

Piping Analysis Results

- 1.1 Used for creating the pipe structural model
 - 1.1.1 Block division and piping specifications
 - 1.1.2 Piping isometrics
 - 1.1.3 Concentrated mass
 - 1.1.4 Support point rigidity
 - 1.1.5 Valve rigidity
- 1.2 Used for creating load conditions
 - 1.2.1 Level A/B design transient
 - 1.2.2 Level A/B thermal displacement input data
 - 1.2.3 Level A, B temperature and pressure input data
 - 1.2.4 Level C, D maximum temperature and pressure input data
 - 1.2.5 Floor response curve
 - 1.2.6 Seismic anchor displacement input data
 - 1.2.7 DBPB displacement input data
- 2. OUTPUT
 - 2.1 PIPESTRESS analysis model diagram
 - 2.2 Natural frequency analysis results
 - 2.3 Frequency mode diagram (primary to tertiary)
 - 2.4 Thermal analysis results (Δ T1, Δ T2, Ta-Tb)
 - 2.5 Piping stress and fatigue evaluation results

- Table A1-7-1-1 Figure A1-7-1-1 Table A1-7-1-2 Table A1-7-1-3 Table A1-7-1-4
- see main text Table A1-7-1-5 Table A1-7-1-6 Table A1-7-1-7 Figure A1-7-1-2 Table A1-7-1-8 Table A1-7-1-9
- Figure A1-7-2-1 Table A1-7-2-1 Figure A1-7-2-2 Table A1-7-2-2 Table A1-7-2-3

 Table A1-7-1-1
 Block division and piping specifications (1/3)

 Table A1-7-1-1
 Block division and piping specifications (2/3)

 Table A1-7-1-1
 Block division and piping specifications (3/3)

Table A1-7-1-2 Concentrated mass

 Table A1-7-1-3
 Support point rigidity

 Table A1-7-1-4
 Valve rigidity

Summary of Stress Analysis Results for the US-APWR Reactor Coolant Loop Branch Piping

MUAP-09011-NP (R0)

Table A1-7-1-5Level A/B thermal displacement input data (1/3)
(Point: 9010)

Table A1-7-1-5Level A/B thermal displacement input data (2/3)
(Point: 9010)

Table A1-7-1-5Level A/B thermal displacement input data (3/3)
(Point: 9010)

 Table A1-7-1-6
 Level A, B temperature and pressure input data (1/33) (Section I)
 Table A1-7-1-6Level A, B temperature and pressure input data (2/33)
(Section I)

 Table A1-7-1-6
 Level A, B temperature and pressure input data (3/33) (Section I)
 Table A1-7-1-6Level A, B temperature and pressure input data (4/33)
(Section II)

Table A1-7-1-6Level A, B temperature and pressure input data (5/33)
(Section II)

Table A1-7-1-6Level A, B temperature and pressure input data (6/33)
(Section II)

 Table A1-7-1-6
 Level A, B temperature and pressure input data (7/33) (Section III)
 Table A1-7-1-6Level A, B temperature and pressure input data (8/33)
(Section III)

 Table A1-7-1-6
 Level A, B temperature and pressure input data (9/33) (Section III)

 Table A1-7-1-6
 Level A, B temperature and pressure input data (10/33) (Section IV)

 Table A1-7-1-6
 Level A, B temperature and pressure input data (11/33) (Section IV)

 Table A1-7-1-6
 Level A, B temperature and pressure input data (12/33) (Section IV)
 Table A1-7-1-6Level A, B temperature and pressure input data (13/33)
(Section V)

Table A1-7-1-6Level A, B temperature and pressure input data (14/33)
(Section V)

Table A1-7-1-6Level A, B temperature and pressure input data (15/33)
(Section V)

 Table A1-7-1-6
 Level A, B temperature and pressure input data (16/33) (Section VI)

 Table A1-7-1-6
 Level A, B temperature and pressure input data (17/33) (Section VI)

 Table A1-7-1-6
 Level A, B temperature and pressure input data (18/33) (Section VI)

 Table A1-7-1-6
 Level A, B temperature and pressure input data (19/33) (Section VII)

 Table A1-7-1-6
 Level A, B temperature and pressure input data (20/33) (Section VII)

 Table A1-7-1-6
 Level A, B temperature and pressure input data (21/33) (Section VII)

 Table A1-7-1-6
 Level A, B temperature and pressure input data (22/33) (Section VIII)

 Table A1-7-1-6
 Level A, B temperature and pressure input data (23/33) (Section VIII)

 Table A1-7-1-6
 Level A, B temperature and pressure input data (24/33) (Section VIII)
 Table A1-7-1-6Level A, B temperature and pressure input data (25/33)
(Section IX)

Table A1-7-1-6Level A, B temperature and pressure input data (26/33)
(Section IX)

Table A1-7-1-6Level A, B temperature and pressure input data (27/33)
(Section IX)

Table A1-7-1-6Level A, B temperature and pressure input data (28/33)
(Section X)

Table A1-7-1-6Level A, B temperature and pressure input data (29/33)
(Section X)

Table A1-7-1-6Level A, B temperature and pressure input data (30/33)
(Section X)

Table A1-7-1-6Level A, B temperature and pressure input data (31/33)
(Section XI)

 Table A1-7-1-6
 Level A, B temperature and pressure input data (32/33) (Section XI)
 Table A1-7-1-6Level A, B temperature and pressure input data (33/33)
(Section XI)

 Table A1-7-1-7
 Level C, D maximum temperature and pressure input data

Figure A1-7-1 -2 Floor response curve (1/6) Accumulator (SI01-02) FRS for MCP Nozzle X (EW) direction (damping 4.0%)

Figure A1-7-1-2 Floor response curve (2/6) Accumulator (SI01-02) FRS for MCP Nozzle Y (NS) direction (damping 4.0%)

Figure A1-7-1 -2 Floor response curve (3/6) Accumulator (SI01-02) FRS for MCP Nozzle Z (Vert.) direction (damping 4.0%)

Figure A1-7-1 -2 Floor response curve (4/6) Accumulator (SI01-02) FRS for Piping X (EW) direction (damping 4.0%)

Figure A1-7-1-2 Floor response curve (5/6)

Accumulator (SI01-02) FRS for Piping Y (NS) direction (damping 4.0%)

Figure A1-7-1-2 Floor response curve (6/6) Accumulator (SI01-02) FRS for Piping Z (Vert.) direction (damping 4.0%)
 Table A1-7-1-8
 Seismic anchor displacement input data

 Table A1-7-1-9 DBPB displacement input data

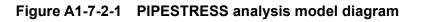


 Table A1-7-2-1
 Natural frequency analysis results

A1-7-63

Figure A1-7-2-2 Frequency mode diagram (primary)

Figure A1-7-2-2 Frequency mode diagram (secondary)

Figure A1-7-2-2 Frequency mode diagram (tertiary)

Table A1-7-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (1/18)
(Section I)

Table A1-7-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (2/18)
(Section I)

Table A1-7-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (3/18)
(Section I)

Table A1-7-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (4/18)(Section II)

Table A1-7-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (5/18)(Section II)

Table A1-7-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (6/18)(Section II)

Table A1-7-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (7/18)(Section III)

Table A1-7-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (8/18)(Section III)

Table A1-7-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (9/18)(Section III)

Table A1-7-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (10/18)
(Section IV)

Table A1-7-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (11/18)
(Section IV)

Table A1-7-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (12/18)
(Section IV)

Table A1-7-2-2 Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (13/18) (Section V)

Table A1-7-2-2 Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (14/18) (Section V)

Table A1-7-2-2 Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (15/18) (Section V)

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Table A1-7-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (16/18)
(Section VI)

Table A1-7-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (17/18)
(Section VI)

Table A1-7-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (18/18)
(Section VI)

Table A1-7-2-3Piping stress and fatigue evaluation results
(Piping that exceeds 1 inch NB–3650 evaluation)

Table A1-7-2-3Piping stress and fatigue evaluation results(Piping of 1 inch or less NC-3650 evaluation)

Appendix 1-8

SI02 Accumulator Loop B Line

Piping Analysis Results

1.	INPUT

- 1.1 Used for creating the pipe structural model
 - 1.1.1 Block division and piping specifications
 - 1.1.2 Piping isometrics
 - 1.1.3 Concentrated mass
 - 1.1.4 Support point rigidity
 - 1.1.5 Valve rigidity
- 1.2 Used for creating load conditions
 - 1.2.1 Level A/B design transient
 - 1.2.2 Level A/B thermal displacement input data
 - 1.2.3 Level A, B temperature and pressure input data
 - 1.2.4 Level C, D maximum temperature and pressure input data
 - 1.2.5 Floor response curve
 - 1.2.6 Seismic anchor displacement input data
 - 1.2.7 DBPB displacement input data
- 2. OUTPUT
 - 2.1 PIPESTRESS analysis model diagram
 - 2.2 Natural frequency analysis results
 - 2.3 Frequency mode diagram (primary to tertiary)
 - 2.4 Thermal analysis results (Δ T1, Δ T2, Ta-Tb)
 - 2.5 Piping stress and fatigue evaluation results

Table A1-8-1-2 Table A1-8-1-3 Table A1-8-1-4 see main text Table A1-8-1-5 Table A1-8-1-6

Table A1-8-1-7

Figure A1-8-1-2

Table A1-8-1-8

Table A1-8-1-9

Table A1-8-1-1

Figure A1-8-1-1

Figure A1-8-2-1 Table A1-8-2-1 Figure A1-8-2-2 Table A1-8-2-2 Table A1-8-2-3
 Table A1-8-1-1
 Block division and piping specifications (1/3)

 Table A1-8-1-1 Block
 division and piping specifications (2/3)

 Table A1-8-1-1
 Block division and piping specifications (3/3)

Table A1-8-1-2 Concentrated mass

 Table A1-8-1-3
 Support point rigidity

Table A1-8-1-4 Valve rigidity

Table A1-8-1-5Level A/B thermal displacement input data (1/3)
(Point: 9010)

Table A1-8-1-5Level A/B thermal displacement input data (2/3)
(Point: 9010)

Table A1-8-1-5Level A/B thermal displacement input data (3/3)
(Point: 9010)

 Table A1-8-1-6
 Level A, B temperature and pressure input data (1/33) (Section I)

 Table A1-8-1-6
 Level A, B temperature and pressure input data (2/33) (Section I)

 Table A1-8-1-6
 Level A, B temperature and pressure input data (3/33) (Section I)

 Table A1-8-1-6
 Level A, B temperature and pressure input data (4/33) (Section II)

 Table A1-8-1-6
 Level A, B temperature and pressure input data (5/33) (Section II)

 Table A1-8-1-6
 Level A, B temperature and pressure input data (6/33) (Section II)

 Table A1-8-1-6
 Level A, B temperature and pressure input data (7/33) (Section III)

 Table A1-8-1-6
 Level A, B temperature and pressure input data (8/33) (Section III)

 Table A1-8-1-6
 Level A, B temperature and pressure input data (9/33) (Section III)

 Table A1-8-1-6
 Level A, B temperature and pressure input data (10/33) (Section VI)

 Table A1-8-1-6
 Level A, B temperature and pressure input data (11/33) (Section VI)

 Table A1-8-1-6
 Level A, B temperature and pressure input data (12/33) (Section VI)
 Table A1-8-1-6Level A, B temperature and pressure input data (13/33)
(Section V)

Table A1-8-1-6Level A, B temperature and pressure input data (14/33)
(Section V)

Table A1-8-1-6Level A, B temperature and pressure input data (15/33)
(Section V)

 Table A1-8-1-6
 Level A, B temperature and pressure input data (16/33) (Section VI)

 Table A1-8-1-6
 Level A, B temperature and pressure input data (17/33) (Section VI)

 Table A1-8-1-6
 Level A, B temperature and pressure input data (18/33) (Section VI)

 Table A1-8-1-6
 Level A, B temperature and pressure input data (19/33) (Section VII)

 Table A1-8-1-6
 Level A, B temperature and pressure input data (20/33) (Section VII)

 Table A1-8-1-6
 Level A, B temperature and pressure input data (21/33) (Section VII)

 Table A1-8-1-6
 Level A, B temperature and pressure input data (22/33) (Section VIII)

 Table A1-8-1-6
 Level A, B temperature and pressure input data (23/33) (Section VIII)

 Table A1-8-1-6
 Level A, B temperature and pressure input data (24/33) (Section VIII)
 Table A1-8-1-6Level A, B temperature and pressure input data (25/33)
(Section IX)

Table A1-8-1-6Level A, B temperature and pressure input data (26/33)
(Section IX)

Table A1-8-1-6Level A, B temperature and pressure input data (27/33)
(Section IX)

Table A1-8-1-6Level A, B temperature and pressure input data (28/33)
(Section X)

Table A1-8-1-6Level A, B temperature and pressure input data (29/33)
(Section X)

Table A1-8-1-6Level A, B temperature and pressure input data (30/33)
(Section X)

 Table A1-8-1-6
 Level A, B temperature and pressure input data (31/33) (Section XI)

 Table A1-8-1-6
 Level A, B temperature and pressure input data (32/33) (Section XI)
 Table A1-8-1-6Level A, B temperature and pressure input data (33/33)
(Section XI)

 Table A1-8-1-7
 Level C, D maximum temperature and pressure input data

Figure A1-8-1-2 Floor response curve (1/6) Accumulator (SI01-02) FRS for MCP Nozzle

X (EW) direction (damping 4.0%)

Figure A1-8-1-2 Floor response curve (2/6) Accumulator (SI01-02) FRS for MCP Nozzle

Y (NS) direction (damping 4.0%)

Figure A1-8-1-2 Floor response curve (3/6) Accumulator (SI01-02) FRS for MCP Nozzle

Z (Vert.) direction (damping 4.0%)

Figure A1-8-1-2 Floor response curve (4/6) Accumulator (SI01-02) FRS for Piping

X (EW) direction (damping 4.0%)

Figure A1-8-1-2 Floor response curve (5/6) Accumulator (SI01-02) FRS for Piping Y (NS) direction (damping 4.0%)

Figure A1-8-1-2 Floor response curve (6/6) Accumulator (SI01-02) FRS for Piping Z (Vert.) direction (damping 4.0%)
 Table A1-8-1-8
 Seismic anchor displacement input data

 Table A1-8-1-9
 DBPB displacement input data

Figure A1-8-2-1 PIPESTRESS analysis model diagram



Figure A1-8-2-2 Frequency mode diagram (primary)

Figure A1-8-2-2 Frequency mode diagram (secondary)

Figure A1-8-2-2 Frequency mode diagram (tertiary)

Table A1-8-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (1/18)
(Section I)

Table A1-8-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (2/18)
(Section I)

Table A1-8-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (3/18)
(Section I)

Table A1-8-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (4/18)(Section II)

Table A1-8-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (5/18)(Section II)

Table A1-8-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (6/18)(Section II)

Table A1-8-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (7/18)(Section III)

Table A1-8-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (8/18)(Section III)

Table A1-8-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (9/18)(Section III)

Table A1-8-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (10/18)
(Section IV)

Table A1-8-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (11/18)
(Section IV)

Table A1-8-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (12/18)
(Section IV)

Table A1-8-2-2Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (13/18)
(Section V)

Table A1-8-2-2Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (14/18)
(Section V)

Table A1-8-2-2Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (15/18)
(Section V)

Table A1-8-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (16/18)
(Section VI)

Table A1-8-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (17/18)
(Section VI)

Table A1-8-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (18/18)
(Section VI)

Table A1-8-2-3Piping stress and Fatigue evaluation results
(Piping that exceeds 1inch NB-3650 evaluation)

Table A1-8-2–3Piping stress and Fatigue evaluation results
(Piping of 1 inch or less NC–3650 evaluation)

Appendix 1-9

SI05 DVI A Line

Piping Analysis Results

Table A1-9-1-1

Figure A1-9-1-1

Table A1-9-1-2

Table A1-9-1-3

Table A1-9-1-4

see main text

Table A1-9-1-5

Table A1-9-1-6

Table A1-9-1-7

Figure A1-9-1-2

Table A1-9-1-8

Table A1-9-1-9

1. INPUT

- 1.1 Used for creating the pipe structural model
 - 1.1.1 Block division and piping specifications
 - 1.1.2 Piping isometrics
 - 1.1.3 Concentrated mass
 - 1.1.4 Support point rigidity
 - 1.1.5 Valve rigidity
- 1.2 Used for creating load conditions
 - 1.2.1 Level A/B design transient
 - 1.2.2 Level A/B thermal displacement input data
 - 1.2.3 Level A, B temperature and pressure input data
 - 1.2.4 Level C, D maximum temperature and pressure input data
 - 1.2.5 Floor response curve
 - 1.2.6 Seismic anchor displacement input data
 - 1.2.7 DBPB displacement input data

2. OUTPUT

Figure A1-9-2-1
Table A1-9-2-1
Figure A1-9-2-2
Table A1-9-2-2
Table A1-9-2-3

 Table A1-9-1-1
 Block division and piping specifications

Table A1-9-1-2 Concentrated mass

 Table A1-9-1-3
 Support point rigidity

 Table A1-9-1-4
 Valve rigidity

Table A1-9-1-5Level A/B thermal displacement input data (1/3)
(Point: 9100)

Table A1-9-1-5Level A/B thermal displacement input data (2/3)
(Point: 9100)

Table A1-9-1-5Level A/B thermal displacement input data (3/3)
(Point: 9100)

Table A1-9-1-6Level A, B temperature and pressure input data (1/9)
(Section I)

Table A1-9-1-6Level A, B temperature and pressure input data (2/9)
(Section I)

Table A1-9-1-6Level A, B temperature and pressure input data (3/9)
(Section I)

Table A1-9-1-6Level A, B temperature and pressure input data (4/9)(Section II)

Table A1-9-1-6Level A, B temperature and pressure input data (5/9)(Section II)

Table A1-9-1-6Level A, B temperature and pressure input data (6/9)(Section II)

Table A1-9-1-6Level A, B temperature and pressure input data (7/9)(Section III)

 Table A1-9-1-6
 Level A, B temperature and pressure input data (8/9) (Section III)
 Table A1-9-1-6Level A, B temperature and pressure input data (9/9)(Section III)

 Table A1-9-1-7
 Level C, D maximum temperature and pressure input data

Figure A1-9-1-2 Floor response curve (1/6) DVI (SI05-06) FRS for RV Nozzle X (EW) direction (damping 4.0%)

Figure A1-9-1-2 Floor response curve (2/6) DVI (SI05-06) FRS for RV Nozzle Y (NS) direction (damping 4.0%)

Figure A1-9-1-2 Floor response curve (3/6) DVI (SI05-06) FRS for RV Nozzle Z (Vert.) direction (damping 4.0%)

Figure A1-9-1-2 Floor response curve (4/6) DVI (SI05-06) FRS for Piping X (EW) direction (damping 4.0%)

Figure A1-9-1-2 Floor response curve (5/6) DVI (SI05-06) FRS for Piping Y (NS) direction (damping 4.0%)

Figure A1-9-1-2 Floor response curve (6/6) DVI (SI05-06) FRS for Piping Z (Vert.) direction (damping 4.0%)
 Table A1-9-1-8
 Seismic anchor displacement input data

 Table A1-9-1-9
 DBPB displacement input data

Figure A1-9-2-1 PIPESTRESS analysis model diagram

 Table A1-9-2-1
 Natural frequency analysis results

Figure A1-9-2-2 Frequency mode diagram (primary)

Figure A1-9-2-2 Frequency mode diagram (secondary)

Figure A1-9-2-2 Frequency mode diagram (tertiary)

Table A1-9-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (1/6)(Section I)

Table A1-9-2-2Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (2/6)
(Section I)

Table A1-9-2-2Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (3/6)
(Section I)

Table A1-9-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (4/6)(Section II)

Table A1-9-2-2Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (5/6)(Section II)

Table A1-9-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (6/6)(Section II)

Table A1-9-2-3Piping stress and fatigue evaluation results(Piping that exceeds 1 inch NB–3650 evaluation)

Table A1-9-2-3 Piping stress and fatigue evaluation results(Piping of 1 inch or less NC-3650 evaluation)

Appendix 1-10

SI06 DVI B Line

Piping Analysis Results

- 1. INPUT
 - 1.1 Used for creating the pipe structural model
 - 1.1.1 Block division and piping specifications
 - 1.1.2 Piping isometrics
 - 1.1.3 Concentrated mass
 - 1.1.4 Support point rigidity
 - 1.1.5 Valve rigidity
 - 1.2 Used for creating load conditions
 - 1.2.1 Level A/B design transient
 - 1.2.2 Level A/B thermal displacement input data
 - 1.2.3 Level A, B temperature and pressure input data
 - 1.2.4 Level C, D maximum temperature and pressure input data
 - 1.2.5 Floor response curve
 - 1.2.6 Seismic anchor displacement input data
 - 1.2.7 DBPB displacement input data
- 2. OUTPUT
 - 2.1 PIPESTRESS analysis model diagram
 - 2.2 Natural frequency analysis results
 - 2.3 Frequency mode diagram (primary to tertiary)
 - 2.4 Thermal analysis results (Δ T1, Δ T2, Ta-Tb)
 - 2.5 Piping stress and fatigue evaluation results

- Table A1-10-1-1 Figure A1-10-1-1 Table A1-10-1-2 Table A1-10-1-3 Table A1-10-1-4
- see main text Table A1-10-1-5 Table A1-10-1-6 Table A1-10-1-7 Figure A1-10-1-2 Table A1-10-1-8 Table A1-10-1-9
- Figure A1-10-2-1 Table A1-10-2-1 Figure A1-10-2-2 Table A1-10-2-2 Table A1-10-2-3

 Table A1-10-1-1
 Block division and piping specifications

Table A1-10-1-2 Concentrated mass

 Table A1-10-1-3
 Support point rigidity

 Table A1-10-1-4
 Valve rigidity

Table A1-10-1-5Level A/B thermal displacement input data (1/3)
(Point: 9100)

Table A1-10-1-5Level A/B thermal displacement input data (2/3)
(Point: 9100)

Table A1-10-1-5Level A/B thermal displacement input data (3/3)(Point: 9100)

Table A1-10-1-6Level A, B temperature and pressure input data (1/9)(Section I)

Table A1-10-1-6Level A, B temperature and pressure input data (2/9)(Section I)

Table A1-10-1-6Level A, B temperature and pressure input data (3/9)(Section I)

 Table A1-10-1-6
 Level A, B temperature and pressure input data (4/9) (Section II)

 Table A1-10-1-6
 Level A, B temperature and pressure input data (5/9) (Section II)

 Table A1-10-1-6
 Level A, B temperature and pressure input data (6/9) (Section II)

 Table A1-10-1-6
 Level A, B temperature and pressure input data (7/9) (Section III)

 Table A1-10-1-6
 Level A, B temperature and pressure input data (8/9) (Section III)

 Table A1-10-1-6
 Level A, B temperature and pressure input data (9/9) (Section III)

 Table A1-10-1-7
 Level C, D maximum temperature and pressure input data

Figure A1-10-1-2 Floor response curve (1/6) DVI (SI05-06) FRS for RV Nozzle X (EW) direction (damping 4.0%)

Figure A1-10-1-2 Floor response curve (2/6) DVI (SI05-06) FRS for RV Nozzle Y (NS) direction (damping 4.0%)

Figure A1-10-1-2 Floor response curve (3/6) DVI (SI05-06) FRS for RV Nozzle Z (Vert.) direction (damping 4.0%)

X (EW) direction (damping 4.0%)

Figure A1-10-1-2 Floor response curve (5/6) DVI (SI05-06) FRS for Piping

Y (NS) direction (damping 4.0%)

Z (Vert.) direction (damping 4.0%)

 Table A1-10-1-8
 Seismic anchor displacement input data

 Table A1-10-1-9
 DBPB displacement input data

Figure A1-10-2-1 PIPESTRESS analysis model diagram

 Table A1-10-2-1
 Natural frequency analysis results

Figure A1-10-2-2 Frequency mode diagram (primary)

Figure A1-10-2-2 Frequency mode diagram (secondary)

Figure A1-10-2-2 Frequency mode diagram (tertiary)

Table A1-10-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (1/6)(Section I)

Mitsubishi Heavy Industries, LTD.	

Table A1-10-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (2/6)
(Section I)

Table A1-10-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (3/6)(Section I)

Table A1-10-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (4/6)
(Section II)

Mitsubishi Heavy Industries, LTD.	

Table A1-10-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (5/6)(Section II)

Table A1-10-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (6/6)(Section II)

Table A1-10-2-3Piping stress and fatigue evaluation results
(Piping that exceeds 1 inch NB–3650 evaluation)

Table A1-10-2-3Piping stress and fatigue evaluation results
(Piping of 1 inch or less NC-3650 evaluation)

Appendix 1-11

CS01 CVCS Charging Line

Piping Analysis Results

- 1.1 Used for creating the pipe structural model
 - 1.1.1 Block division and piping specifications
 - 1.1.2 Piping isometrics
 - 1.1.3 Concentrated mass
 - 1.1.4 Support point rigidity
 - 1.1.5 Valve rigidity
- 1.2 Used for creating load conditions
 - 1.2.1 Level A/B design transient
 - 1.2.2 Level A/B thermal displacement input data
 - 1.2.3 Level A, B temperature and pressure input data
 - 1.2.4 Level C, D maximum temperature and pressure input data
 - 1.2.5 Floor response curve
 - 1.2.6 Seismic anchor displacement input data
 - 1.2.7 DBPB displacement input data
- 2. OUTPUT
 - 2.1 PIPESTRESS analysis model diagram
 - 2.2 Natural frequency analysis results
 - 2.3 Frequency mode diagram (primary to tertiary)
 - 2.4 Thermal analysis results (Δ T1, Δ T2, Ta-Tb)
 - 2.5 Piping stress and fatigue evaluation results

- Table A1-11-1-1 Figure A1-11-1-1 Table A1-11-1-2 Table A1-11-1-3 Table A1-11-1-4
- see main text Table A1-11-1-5 Table A1-11-1-6 Table A1-11-1-7 Figure A1-11-1-2 Table A1-11-1-8 Table A1-11-1-9
- Figure A1-11-2-1 Table A1-11-2-1 Figure A1-11-2-2 Table A1-11-2-2 Table A1-11-2-3

 Table A1-11-1-1
 Block division and piping specifications

Table A1-11-1-2 Concentrated mass

 Table A1-11-1-3
 Support point rigidity

Table A1-11-1-4 Valve rigidity

Table A1-11-1-5Level A/B thermal displacement input data (1/3)
(Point: 9010)

Table A1-11-1-5Level A/B thermal displacement input data (2/3)
(Point: 9010)

Table A1-11-1-5Level A/B thermal displacement input data (3/3)
(Point: 9010)

Table A1-11-1-6Level A, B temperature and pressure input data (1/12)
(Section I)

Table A1-11-1-6Level A, B temperature and pressure input data (2/12)
(Section I)

Table A1-11-1-6Level A, B temperature and pressure input data (3/12)
(Section I)

 Table A1-11-1-6
 Level A, B temperature and pressure input data (4/12) (Section II)

 Table A1-11-1-6
 Level A, B temperature and pressure input data (5/12) (Section II)

 Table A1-11-1-6
 Level A, B temperature and pressure input data (6/12) (Section II)

 Table A1-11-1-6
 Level A, B temperature and pressure input data (7/12) (Section III)

 Table A1-11-1-6
 Level A, B temperature and pressure input data (8/12) (Section III)

 Table A1-11-1-6
 Level A, B temperature and pressure input data (9/12) (Section III)

 Table A1-11-1-6
 Level A, B temperature and pressure input data (10/12) (Section IV)
 Table A1-11-1-6Level A, B temperature and pressure input data (11/12)
(Section IV)

 Table A1-11-1-6
 Level A, B temperature and pressure input data (12/12) (Section IV)

 Table A1-11-1-7
 Level C, D maximum temperature and pressure input data

Figure A1-11-1-2 Floor response curve (1/6) CVCS Charging (CS01) FRS for MCP Nozzle X (EW) direction (damping 4.0%)

Figure A1-11-1-2 Floor response curve (2/6) CVCS Charging (CS01) FRS for MCP Nozzle Y (NS) direction (damping 4.0%)

Figure A1-11-1-2 Floor response curve (3/6) CVCS Charging (CS01) FRS for MCP Nozzle Z (Vert.) direction (damping 4.0%)

Figure A1-11-1-2 Floor response curve (4/6) CVCS Charging (CS01) FRS for Piping X (EW) direction (damping 4.0%)

Figure A1-11-1-2 Floor response curve (5/6) CVCS Charging (CS01) FRS for Piping Y (NS) direction (damping 4.0%)

Figure A1-11-1-2 Floor response curve (6/6) CVCS Charging (CS01) FRS for Piping Z (Vert.) direction (damping 4.0%)
 Table A1-11-1-8
 Seismic anchor displacement input data

 Table A1-11-1-9
 DBPB displacement input data

Figure A1-11-2-1 PIPESTRESS analysis model diagram

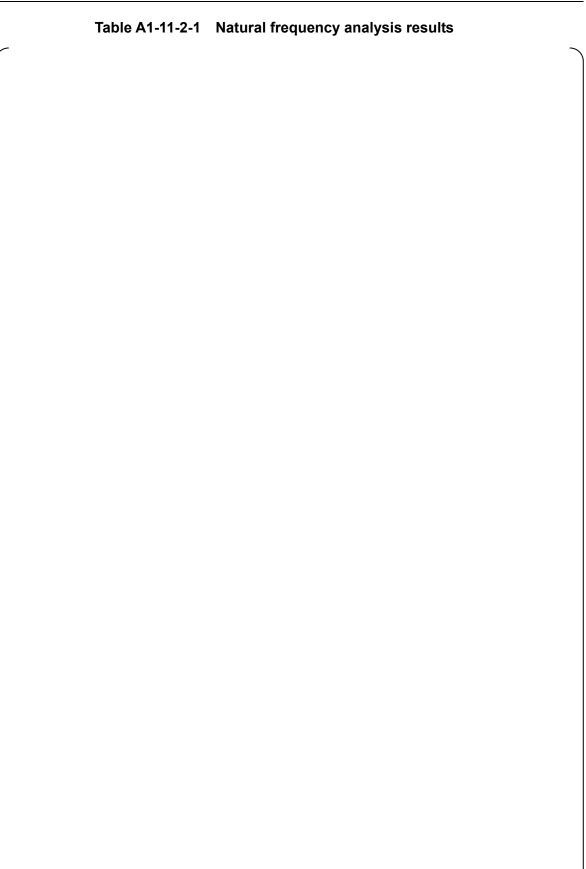
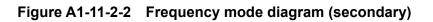




Figure A1-11-2-2 Frequency mode diagram (primary)



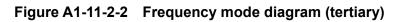


Table A1-11-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (1/9)
(Section I)

Table A1-11-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (2/9)
(Section I)

Table A1-11-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (3/9)
(Section I)

Table A1-11-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (4/9)
(Section II)

Table A1-11-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (5/9)
(Section II)

Table A1-11-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (6/9)
(Section II)

Table A1-11-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (7/9)
(Section III)

Table A1-11-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (8/9)
(Section III)

Table A1-11-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (9/9)
(Section III)

Table A1-11-2-3Piping stress and fatigue evaluation results
(Piping that exceeds 1 inch NB–3650 evaluation)

Table A1-11-2-3Piping stress and fatigue evaluation results
(Piping of 1 inch or less NC-3650 evaluation)

Appendix 1-12

CS02 CVCS Letdown Line

Piping Analysis Results

- 1. INPUT
 - 1.1 Used for creating the pipe structural model
 - 1.1.1 Block division and piping specifications
 - 1.1.2 Piping isometrics
 - 1.1.3 Concentrated mass
 - 1.1.4 Support point rigidity
 - 1.1.5 Valve rigidity
 - 1.2 Used for creating load conditions
 - 1.2.1 Level A/B design transient
 - 1.2.2 Level A/B thermal displacement input data
 - 1.2.3 Level A, B temperature and pressure input data
 - 1.2.4 Level C, D maximum temperature and pressure input data
 - 1.2.5 Floor response curve
 - 1.2.6 Seismic anchor displacement input data
 - 1.2.7 DBPB displacement input data
- 2. OUTPUT
 - 2.1 PIPESTRESS analysis model diagram
 - 2.2 Natural frequency analysis results
 - 2.3 Frequency mode diagram (primary to tertiary)
 - 2.4 Thermal analysis results (Δ T1, Δ T2, Ta-Tb)
 - 2.5 Piping stress and fatigue evaluation results

- Table A1-12-1-1 Figure A1-12-1-1 Table A1-12-1-2 Table A1-12-1-3 Table A1-12-1-4
- see main text Table A1-12-1-5 Table A1-12-1-6 Table A1-12-1-7 Figure A1-12-1-2 Table A1-12-1-8 Table A1-12-1-9
- Figure A1-12-2-1 Table A1-12-2-1 Figure A1-12-2-2 Table A1-12-2-2 Table A1-12-2-3

 Table A1-12-1-1
 Block division and piping specifications

Table A1-12-1-2 Concentrated mass

 Table A1-12-1-3
 Support point rigidity

 Table A1-12-1-4
 Valve rigidity

Table A1-12-1-5Level A/B thermal displacement input data (1/3)
(Point: 9010)

Table A1-12-1-5Level A/B thermal displacement input data (2/3)
(Point: 9010)

Table A1-12-1-5Level A/B thermal displacement input data (3/3)(Point: 9010)

Table A1-12-1-6Level A, B temperature and pressure input data (1/27)
(Section I)

 Table A1-12-1-6
 Level A, B temperature and pressure input data (2/27) (Section I)

 Table A1-12-1-6
 Level A, B temperature and pressure input data (3/27) (Section I)

 Table A1-12-1-6
 Level A, B temperature and pressure input data (4/27) (Section II)

 Table A1-12-1-6
 Level A, B temperature and pressure input data (5/27) (Section II)

 Table A1-12-1-6
 Level A, B temperature and pressure input data (6/27) (Section II)

 Table A1-12-1-6
 Level A, B temperature and pressure input data (7/27) (Section III)

 Table A1-12-1-6
 Level A, B temperature and pressure input data (8/27) (Section III)

 Table A1-12-1-6
 Level A, B temperature and pressure input data (9/27) (Section III)

 Table A1-12-1-6
 Level A, B temperature and pressure input data (10/27) (Section IV)

 Table A1-12-1-6
 Level A, B temperature and pressure input data (11/27) (Section IV)
 Table A1-12-1-6Level A, B temperature and pressure input data (12/27)
(Section IV)

Table A1-12-1-6Level A, B temperature and pressure input data (13/27)
(Section V)

Table A1-12-1-6Level A, B temperature and pressure input data (14/27)
(Section V)

Table A1-12-1-6Level A, B temperature and pressure input data (15/27)(Section V)

Table A1-12-1-6Level A, B temperature and pressure input data (16/27)
(Section VI)

Table A1-12-1-6Level A, B temperature and pressure input data (17/27)
(Section VI)

 Table A1-12-1-6
 Level A, B temperature and pressure input data (18/27) (Section VI)

 Table A1-12-1-6
 Level A, B temperature and pressure input data (19/27) (Section VII)

 Table A1-12-1-6
 Level A, B temperature and pressure input data (20/27) (Section VII)

 Table A1-12-1-6
 Level A, B temperature and pressure input data (21/27) (Section VII)

 Table A1-12-1-6
 Level A, B temperature and pressure input data (22/27) (Section VIII)

 Table A1-12-1-6
 Level A, B temperature and pressure input data (23/27) (Section VIII)

 Table A1-12-1-6
 Level A, B temperature and pressure input data (24/27) (Section VIII)

 Table A1-12-1-6
 Level A, B temperature and pressure input data (25/27) (Section IX)

 Table A1-12-1-6
 Level A, B temperature and pressure input data (26/27) (Section IX)

 Table A1-12-1-6
 Level A, B temperature and pressure input data (27/27) (Section IX)

 Table A1-12-1-7
 Level C, D maximum temperature and pressure input data

Figure A1-12-1-2 Floor response curve (1/6) CVCS Letdown (CS02) FRS for MCP Nozzle X (EW) direction (damping 4.0%)

Figure A1-12-1-2 Floor response curve (2/6) CVCS Letdown (CS02) FRS for MCP Nozzle Y (NS) direction (damping 4.0%)

Figure A1-12-1-2 Floor response curve (3/6) CVCS Letdown (CS02) FRS for MCP Nozzle Z (Vert.) direction (damping 4.0%)

Figure A1-12-1-2 Floor response curve (4/6) CVCS Letdown (CS02) FRS for Piping X (EW) direction (damping 4.0%)

Figure A1-12-1-2 Floor response curve (5/6) CVCS Letdown (CS02) FRS for Piping Y (NS) direction (damping 4.0%)

Figure A1-12-1-2 Floor response curve (6/6) CVCS Letdown (CS02) FRS for Piping Z (Vert.) direction (damping 4.0%)
 Table A1-12-1-8
 Seismic anchor displacement input data

 Table A1-12-1-9
 DBPB displacement input data

Figure A1-12-2-1 PIPESTRESS analysis model diagram



Table A1-12-2-1 Natural frequency analysis results

Figure A1-12-2-2 Frequency mode diagram (primary)

Figure A1-12-2-2 Frequency mode diagram (secondary)

Figure A1-12-2-2 Frequency mode diagram (tertiary)

Table A1-12-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (1/18)
(Section I)

Table A1-12-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (2/18)
(Section I)

Table A1-12-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (3/18)
(Section I)

Table A1-12-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (4/18)(Section II)

Table A1-12-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (5/18)(Section II)

Table A1-12-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (6/18)(Section II)

Table A1-12-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (7/18)(Section III)

Table A1-12-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (8/18)(Section III)

Table A1-12-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (9/18)(Section III)

Table A1-12-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (1018)
(Section IV)

Table A1-12-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (11/18)(Section IV)

Table A1-12-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (12/18)(Section IV)

Table A1-12-2-2Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (13/18)
(Section V)

Table A1-12-2-2Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (14/18)
(Section V)

Table A1-12-2-2Thermal analysis results (Δ T1, Δ T2, Ta-Tb) (15/18)(Section V)

Table A1-12-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (16/18)
(Section VI)

Table A1-12-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (17/18)(Section VI)

Table A1-12-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (18/18)(Section VI)

Table A1-12-2-3Piping stress and fatigue evaluation results
(Piping that exceeds 1 inch NB–3650 evaluation)

Table A1-12-2-3Piping stress and fatigue evaluation results
(Piping of 1 inch or less NC-3650 evaluation)

Appendix 1-13

CS04 CVCS Seal Injection A Line

Piping Analysis Results

|--|

- 1.1 Used for creating the pipe structural model
 - 1.1.1 Block division and piping specifications
 - 1.1.2 Piping isometrics
 - 1.1.3 Concentrated mass
 - 1.1.4 Support point rigidity
 - 1.1.5 Valve rigidity
- 1.2 Used for creating load conditions
 - 1.2.1 Level A/B design transient
 - 1.2.2 Level A/B thermal displacement input data
 - 1.2.3 Level A, B temperature and pressure input data
 - 1.2.4 Level C, D maximum temperature and pressure input data
 - 1.2.5 Floor response curve
 - 1.2.6 Seismic anchor displacement input data
 - 1.2.7 DBPB displacement input data
- 2. OUTPUT

2.1 PIPESTRESS analysis model diagram	
2.2 Natural frequency analysis results	

- 2.3 Frequency mode diagram (primary to tertiary)
- 2.4 Thermal analysis results ($\Delta T1$, $\Delta T2$, Ta-Tb)
- 2.5 Piping stress and fatigue evaluation results

- Table A1-13-1-1 Figure A1-13-1-1 Table A1-13-1-2 Table A1-13-1-3 Table A1-13-1-4
- see main text Table A1-13-1-5 Table A1-13-1-6 Table A1-13-1-7 Figure A1-13-1-2 Table A1-13-1-8 Table A1-13-1-9
- Figure A1-13-2-1 Table A1-13-2-1 Figure A1-13-2-2 Table A1-13-2-2 Table A1-13-2-3

 Table A1-13-1-1
 Block division and piping specifications

Table A1-13-1-2 Concentrated mass

Table A1-13-1-3 Support point rigidity

Table A1-13-1-4 Valve rigidity

Table A1-13-1-5Level A/B thermal displacement input data (1/3)
(Point: 9100)

Table A1-13-1-5Level A/B thermal displacement input data (2/3)
(Point: 9100)

Table A1-13-1-5Level A/B thermal displacement input data (3/3)
(Point: 9100)

Table A1-13-1-6Level A, B temperature and pressure input data (1/18)(Section I)

Table A1-13-1-6Level A, B temperature and pressure input data (2/18)(Section I)

Table A1-13-1-6Level A, B temperature and pressure input data (3/18)(Section I)

Table A1-13-1-6Level A, B temperature and pressure input data (4/18)(Section II)

Table A1-13-1-6Level A, B temperature and pressure input data (5/18)(Section II)

Table A1-13-1-6Level A, B temperature and pressure input data (6/18)(Section II)

 Table A1-13-1-6
 Level A, B temperature and pressure input data (7/18) (Section III)

 Table A1-13-1-6
 Level A, B temperature and pressure input data (8/18) (Section III)
 Table A1-13-1-6Level A, B temperature and pressure input data (9/18)(Section III)

 Table A1-13-1-6
 Level A, B temperature and pressure input data (10/18) (Section IV)

 Table A1-13-1-6
 Level A, B temperature and pressure input data (11/18) (Section IV)
 Table A1-13-1-6Level A, B temperature and pressure input data (12/18)
(Section IV)

Table A1-13-1-6Level A, B temperature and pressure input data (13/18)
(Section V)

Table A1-13-1-6Level A, B temperature and pressure input data (14/18)
(Section V)

Table A1-13-1-6Level A, B temperature and pressure input data (15/18)
(Section V)

 Table A1-13-1-6
 Level A, B temperature and pressure input data (16/18) (Section VI)
 Table A1-13-1-6Level A, B temperature and pressure input data (17/18)
(Section VI)

Table A1-13-1-6Level A, B temperature and pressure input data (18/18)(Section VI)

 Table A1-13-1-7
 Level C, D maximum temperature and pressure input data

Figure A1-13-1-2 Floor response curve (1/6) CVCS Seal Injection (CS04-07) FRS for RCP Nozzle X (EW) direction (damping 4.0%)

Figure A1-13-1-2 Floor response curve (2/6) CVCS Seal Injection (CS04-07) FRS for RCP Nozzle Y (NS) direction (damping 4.0%)

Figure A1-13-1-2 Floor response curve (3/6) CVCS Seal Injection (CS04-07) FRS for RCP Nozzle Z (Vert.) direction (damping 4.0%)

Figure A1-13-1-2 Floor response curve (4/6) CVCS Seal Injection (CS04-07) FRS for Piping X (EW) direction (damping 4.0%)

Figure A1-13-1-2 Floor response curve (5/6) CVCS Seal Injection (CS04-07) FRS for Piping Y (NS) direction (damping 4.0%)

Figure A1-13-1-2 Floor response curve (6/6) CVCS Seal Injection (CS04-07) FRS for Piping Z (Vert.) direction (damping 4.0%)
 Table A1-13-1-8
 Seismic anchor displacement input data

 Table A1-13-1-9
 DBPB displacement input data

Figure A1-13-2-1 PIPESTRESS analysis model diagram

 Table A1-13-2-1
 Natural frequency analysis results

Figure A1-13-2-2 Frequency mode diagram (primary)

Figure A1-13-2-2 Frequency mode diagram (secondary)

Figure A1-13-2-2 Frequency mode diagram (tertiary)

TableA1-13- 2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (1/9)
(Section I)

Table A1-13-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (2/9)
(Section I)

Table A1-13-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (3/9)
(Section I)

Table A1-13-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (4/9)
(Section II)

Table A1-13-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (5/9)
(Section II)

Table A1-13-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (6/9)
(Section II)

Table A1-13-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (7/9)
(Section III)

Table A1-13-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (8/9)
(Section III)

Table A1-13-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (9/9)
(Section III)

Table A1-13-2-3Piping stress and fatigue evaluation results
(Piping that exceeds 1 inch NB–3650 evaluation)

Table A1-13-2-3Piping stress and fatigue evaluation results
(Piping of 1 inch or less NC–3650 evaluation)

Appendix 1-14

CS05 CVCS Seal Injection B Line

Piping Analysis Results

- 1.1 Used for creating the pipe structural model
 - 1.1.1 Block division and piping specifications
 - 1.1.2 Piping isometrics
 - 1.1.3 Concentrated mass
 - 1.1.4 Support point rigidity
 - 1.1.5 Valve rigidity
- 1.2 Used for creating load conditions
 - 1.2.1 Level A/B design transient
 - 1.2.2 Level A/B thermal displacement input data
 - 1.2.3 Level A, B temperature and pressure input data
 - 1.2.4 Level C, D maximum temperature and pressure input data
 - 1.2.5 Floor response curve
 - 1.2.6 Seismic anchor displacement input data
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- 2. OUTPUT
 - 2.1 PIPESTRESS analysis model diagram
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 - 2.3 Frequency mode diagram (primary to tertiary)
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 Block division and piping specifications

Table A1-14-1-2 Concentrated mass

Table A1-14-1-3 Support point rigidity

Table A1-14-1-4 Valve rigidity

Table A1-14-1-5Level A/B thermal displacement input data (1/3)
(Point: 9100)

Table A1-14-1-5Level A/B thermal displacement input data (2/3)
(Point: 9100)

Table A1-14-1-5Level A/B thermal displacement input data (3/3)
(Point: 9100)

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 Table A1-14-1-6
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 Table A1-14-1-6Level A, B temperature and pressure input data (13/18)(Section V)

Table A1-14-1-6Level A, B temperature and pressure input data (14/18)(Section V)

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Figure A1-14-1-2 Floor response curve (3/6) CVCS Seal Injection (CS04-07) FRS for RCP Nozzle Z (Vert.) direction (damping 4.0%)

Figure A1-14-1-2 Floor response curve (4/6) CVCS Seal Injection (CS04-07) FRS for Piping X (EW) direction (damping 4.0%)

Figure A1-14-1-2 Floor response curve (5/6) CVCS Seal Injection (CS04-07) FRS for Piping Y (NS) direction (damping 4.0%)

Figure A1-14-1-2 Floor response curve (6/6) CVCS Seal Injection (CS04-07) FRS for Piping

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 Seismic anchor displacement input data

 Table A1-14-1-9
 DBPB displacement input data

Figure A1-14-2-1 PIPESTRESS analysis model diagram

 Table A1-14-2-1
 Natural frequency analysis results



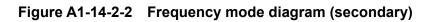




Table A1-14-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (1/9)
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Table A1-14-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (9/9)
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Table A1-14-2-3Piping stress and fatigue evaluation results
(Piping that exceeds 1 inch NB-3650 evaluation)

Table A1-14-2-3 Piping stress and fatigue evaluation results(Piping of 1 inch or less NC-3650 evaluation)

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CS06 CVCS Seal Injection C Line

Piping Analysis Results

- 1. INPUT
 - 1.1 Used for creating the pipe structural model
 - 1.1.1 Block division and piping specifications
 - 1.1.2 Piping isometrics
 - 1.1.3 Concentrated mass
 - 1.1.4 Support point rigidity
 - 1.1.5 Valve rigidity
 - 1.2 Used for creating load conditions
 - 1.2.1 Level A/B design transient
 - 1.2.2 Level A/B thermal displacement input data
 - 1.2.3 Level A, B temperature and pressure input data
 - 1.2.4 Level C, D maximum temperature and pressure input data
 - 1.2.5 Floor response curve
 - 1.2.6 Seismic anchor displacement input data
 - 1.2.7 DBPB displacement input data
- 2. OUTPUT
 - 2.1 PIPESTRESS analysis model diagram
 - 2.2 Natural frequency analysis results
 - 2.3 Frequency mode diagram (primary to tertiary)
 - 2.4 Thermal analysis results (Δ T1, Δ T2, Ta-Tb)
 - 2.5 Piping stress and fatigue evaluation results

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 Table A1-15-1-1
 Block division and piping specifications

Table A1-15-1-2 Concentrated mass

Table A1-15-1-3 Support point rigidity

 Table A1-15-1-4
 Valve rigidity

Table A1-15-1-5Level A/B thermal displacement input data (1/3)
(Point: 9100)

Table A1-15-1-5Level A/B thermal displacement input data (2/3)
(Point: 9100)

Table A1-15-1-5Level A/B thermal displacement input data (3/3)
(Point: 9100)

Table A1-15-1-6Level A, B temperature and pressure input data (1/18)(Section I)

Table A1-15-1-6Level A, B temperature and pressure input data (2/18)(Section I)

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 Table A1-15-1-6
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Table A1-15-1-6Level A, B temperature and pressure input data (11/18)(Section IV)

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Table A1-15-1-6Level A, B temperature and pressure input data (13/18)(Section V)

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Table A1-15-1-6Level A, B temperature and pressure input data (17/18)(Section VI)

Table A1-15-1-6Level A, B temperature and pressure input data (18/18)(Section VI)

 Table A1-15-1-7
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Figure A1-15-1-2 Floor response curve (2/6) CVCS Seal Injection (CS04-07) FRS for RCP Nozzle Y (NS) direction (damping 4.0%)

Figure A1-15-1-2 Floor response curve (3/6) CVCS Seal Injection (CS04-07) FRS for RCP Nozzle Z (Vert.) direction (damping 4.0%)

Figure A1-15-1-2 Floor response curve (4/6) CVCS Seal Injection (CS04-07) FRS for Piping X (EW) direction (damping 4.0%)

Figure A1-15-1-2 Floor response curve (5/6)

CVCS Seal Injection (CS04-07) FRS for Piping Y (NS) direction (damping 4.0%)

Figure A1-15-1-2 Floor response curve (6/6)

CVCS Seal Injection (CS04-07) FRS for Piping Z (Vert.) direction (damping 4.0%)
 Table A1-15-1-8
 Seismic anchor displacement input data

 Table A1-15-1-9
 DBPB displacement input data

Figure A1-15-2-1 PIPESTRESS analysis model diagram

 Table A1-15-2-1
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Figure A1-15-2-2 Frequency mode diagram (primary)

Figure A1-15-2-2 Frequency mode diagram (secondary)

Figure A1-15-2-2 Frequency mode diagram (tertiary)

Table A1-15-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (1/9)
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Table A1-15-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (2/9)
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Table A1-15-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (3/9)
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Table A1-15-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (4/9)
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Table A1-15-2-3Piping stress and fatigue evaluation results
(Piping that exceeds 1 inch NB–3650 evaluation)

Table A1-15-2-3Piping stress and fatigue evaluation results
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CS07 CVCS Seal Injection D Line

Piping Analysis Results

- 1. INPUT
 - 1.1 Used for creating the pipe structural model
 - 1.1.1 Block division and piping specifications
 - 1.1.2 Piping isometrics
 - 1.1.3 Concentrated mass
 - 1.1.4 Support point rigidity
 - 1.1.5 Valve rigidity
 - 1.2 Used for creating load conditions
 - 1.2.1 Level A/B design transient
 - 1.2.2 Level A/B thermal displacement input data
 - 1.2.3 Level A, B temperature and pressure input data
 - 1.2.4 Level C, D maximum temperature and pressure input data
 - 1.2.5 Floor response curve
 - 1.2.6 Seismic anchor displacement input data
 - 1.2.7 DBPB displacement input data
- 2. OUTPUT
 - 2.1 PIPESTRESS analysis model diagram
 - 2.2 Natural frequency analysis results
 - 2.3 Frequency mode diagram (primary to tertiary)
 - 2.4 Thermal analysis results (Δ T1, Δ T2, Ta-Tb)
 - 2.5 Piping stress and fatigue evaluation results

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 Table A1-16-1-1
 Block division and piping specifications

Table A1-16-1-2 Concentrated mass

Table A1-16-1-3 Support point rigidity

 Table A1-16-1-4
 Valve rigidity

Table A1-16-1-5Level A/B thermal displacement input data (1/3)
(Point: 9100)

Table A1-16-1-5Level A/B thermal displacement input data (2/3)
(Point: 9100)

Table A1-16-1-5Level A/B thermal displacement input data (3/3)(Point: 9100)

Table A1-16-1-6Level A, B temperature and pressure input data (1/18)(Section I)

Table A1-16-1-6Level A, B temperature and pressure input data (2/18)(Section I)

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 Table A1-16-1-6
 Level A, B temperature and pressure input data (5/18) (Section II)

 Table A1-16-1-6
 Level A, B temperature and pressure input data (6/18) (Section II)

 Table A1-16-1-6
 Level A, B temperature and pressure input data (7/18) (Section III)

 Table A1-16-1-6
 Level A, B temperature and pressure input data (8/18) (Section III)

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 Table A1-16-1-6
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 Table A1-16-1-7
 Level C, D maximum temperature and pressure input data

Figure A1-16-1-2 Floor response curve (1/6) CVCS Seal Injection (CS04-07) FRS for RCP Nozzle X (EW) direction (damping 4.0%)

Figure A1-16-1-2 Floor response curve (2/6) CVCS Seal Injection (CS04-07) FRS for RCP Nozzle Y (NS) direction (damping 4.0%)

Figure A1-16-1-2 Floor response curve (3/6) CVCS Seal Injection (CS04-07) FRS for RCP Nozzle Z (Vert.) direction (damping 4.0%)

Figure A1-16-1-2 Floor response curve (4/6) CVCS Seal Injection (CS04-07) FRS for Piping X (EW) direction (damping 4.0%)

Figure A1-16-1-2 Floor response curve (5/6) CVCS Seal Injection (CS04-07) FRS for Piping Y (NS) direction (damping 4.0%)

Figure A1-16-1-2 Floor response curve (6/6) CVCS Seal Injection (CS04-07) FRS for Piping Z (Vert.) direction (damping 4.0%)
 Table A1-16-1-8
 Seismic anchor displacement input data

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 DBPB displacement input data

Figure A1-16-2-1 PIPESTRESS analysis model diagram

 Table A1-16-2-1
 Natural frequency analysis results

Figure A1-16-2-2 Frequency mode diagram (primary)

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Table A1-16-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (1/9)
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Table A1-16-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (2/9)
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Table A1-16-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (3/9)
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Table A1-16-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (4/9)
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Table A1-16-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (5/9)
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Table A1-16-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (6/9)
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Table A1-16-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (7/9)
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Table A1-16-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (8/9)
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Table A1-16-2-2Thermal analysis results (ΔT1, ΔT2, Ta-Tb) (9/9)
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Table A1-16-2-3Piping stress and fatigue evaluation results
(Piping that exceeds 1 inch NB–3650 evaluation)

Table A1-16-2-3Piping stress and fatigue evaluation results
(Piping of 1 inch or less NC-3650 evaluation)

Appendix 2

LEAK BEFORE BREAK EVALUATION

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A2 LEAK BEFORE BREAK EVALUATION

A2.1 Introduction

The leak-before-break (LBB) evaluation of the US-APWR follows the methodology in accordance with General Design Criteria (GDC) 4 of 10CFR50, Appendix A (Ref. 1), NUREG-0800, Standard Review Plan (SRP) 3.6.3, Rev. 1, (Ref. 2), and NUREG-1061, Volume 3 (Ref. 3). The evaluation includes an assessment of all potential failure mechanisms, and development of bounding analysis curves (BACs) that define the allowable maximum stress as a function of the normal operating stress for each piping systems or subsystem with different materials.

The LBB analysis is described in detail in Section 3.6.3 of the US-APWR Design Control Document (DCD), with details in Appendix 3B. That appendix provides the development of the BACs for the piping.

A LBB analysis was done for the pressurizer surge line. Table A2-1 shows the conditions used for development of the BAC.

A2.2 Modified Bounding Analysis Curve Approach

Work has currently been completed to update the BAC analysis for Appendix 3B of the DCD, Rev.1. The following methods will be used for the LBB evaluation:

- (1) Calculation of a leakage rate and determination of leakage flaw sizes as a function of normal operating conditions
- (2) Calculation of critical flaw sizes as a function of applied stress
- (3) Development of the BACs from the above

A2.2.1 Leak Rate Determination

The DCD described the thermal-hydraulics model used to develop the DCD curves. The fundamental equations for calculation of flow through a circumferential crack in a pipe are described. For the revised leakage rate calculations, the following revisions have been made:

- (1) The EPRI-developed PICEP computer program (Ref. 4) was used to calculate leakage. PICEP incorporates the thermal-hydraulic model described in the DCD but has improved methods for calculation of the crack opening area based on the EPRIdeveloped methods for elastic plastic fracture mechanics (Ref. 5).
- (2) For conservatism, the crack opening area was calculated without taking credit for the plastic opening. This is consistent with the approach in the DCD. In addition, the plastic zone correction factor was conservatively based on a flow stress (not yield stress) of 51 ksi (consistent with the maximum flow stress in SRP 3.6.3), minimizing the effects of plastic zone correction on the crack opening area increase due to plasticity effects.

- (3) The coefficient of discharge (C_D) was taken as 0.61. Consistent with testing conducted at the time of the PICEP development and verification that it would adequately calculate leakage, the crack roughness for assumed fatigue cracks was taken as 0.000197 inches and no turns were included. These assumptions are consistent with those made at the time that SRP 3.6.3 and NUREG-1061 Volume were published that required a factor of 10 between the calculated leakage and the plant leakage detection system to cover various uncertainties (Ref. 6).
- (4) Based on a review of revisions to Regulatory Guide 1.45 (Ref. 7), it was determined that the sensitivity of the US-APWR leakage detection system can be reduced to 0.5 gpm, allowing the leakage flaw sizes to be based on a leak of 5 gpm.

A2.2.2. Fracture Mechanics Analysis

Because austenitic stainless steel has high fracture toughness, limit load methodology can be applied to evaluate the fracture behavior of the piping. The methods for limit load evaluation as described in SRP 3.6.3 and in the DCD are used. The flow stress used in the analysis is based on ASME Code minimum values at temperature, conservatively applying these same values for SMAW weldments, since this is less than the specified value of 51 ksi in SRP 3.6.3. Since stresses for the various loadings will be combined by absolute sum methods, the factor of safety for maximum load is 1.0, such that the critical flaw size was determined to be twice the leakage flaw size.

A2.2.3 Generation of BAC

The BAC methodology uses a LBB assessment diagram to show that LBB requirements are met for all weld locations in each piping system. In the BAC diagram $\sigma_{nor} = |P_m| + |P_b|$, the sum of the membrane stress and the bending stress under normal operation, is plotted along the abscissa, and $\sigma_{max} = |P_{m_max}| + |P_{b_max}|$, the absolute sum of the membrane stress and the bending stress under the maximum load, is plotted along the ordinate. The procedure used in developing the BAC diagram was as follows:

- (1) Determine the leakage crack length for a crack with a leak rate 10 times as large as the detectable leak rate by applying the abscissa's normal stress σ_{nor} .
- (2) Based on a critical crack size of twice the leakage crack length, determine the maximum stress σ_{max} that is required to produce this critical crack size.
- (3) Perform the above steps at a sufficient number of points of normal operating stress to develop of smooth curve of the maximum stress σ_{max} as a function of the abscissa's normal stress σ_{nor} .
- (4) For the modified BACs, the normal operating stress was varied from that due to pressure up to a limit of 50 ksi. This upper bound is arbitrary and is a stress greater than will be limited by the ASME Code stress limits for the piping that also must be satisfied.

Per the requirements in SRP 3.6.3, the maximum stress is a combination of the effects of pressure + dead weight + maximum seismic stress if the weld is TIG. If the weld is SMAW or

SAW, the maximum stress is a combination of the effects of pressure + dead weight + thermal expansion + maximum seismic stress.

For the BAC curves, the membrane stresses were calculated based on the axial force divided by the metal area. For the piping evaluated in this report, the axial loads due to loads other than pressure are not significant. The axial pressure force was based on the internal pipe pressure times the internal area of the weld. For convenience, the bending stresses included in the BAC curves were based on the piping moment divided by the weld section modulus, effectively using the stress at the outside of the piping. All of the BACs were developed using the nominal thickness and diameter of the welds.

If the actual stresses in the piping system, calculated using the same methods as above, fall in the regions below the BAC, then LBB requirements are satisfied.

A2.3 Calculation of LBB Evaluation Points

The assessment of LBB acceptability was performed based on the calculated stresses at each weld in the piping system being evaluated. For each weld, stresses for normal operation and the maximum stress conditions were calculated from the piping stress analysis.

The stress for normal operation along the abscissa of the BAC was calculated for each weld in the piping system as follows.

 For all types of welds, calculate the algebraic sum of the axial force, the bending and torque moment due to deadweight, the internal pressure, and the thermal expansion. Thermal expansion is always included since it will contribute to the crack opening area.

$$F = F_{DW} + F_{Th} + F_P$$

$$M = \sqrt{((M_X)^2 + (M_Y)^2 + (M_Z)^2)}$$

$$M_X = (M_X)_{DW} + (M_X)_{Th}$$

$$M_Y = (M_Y)_{DW} + (M_Y)_{Th}$$

$$M_Z = (M_Z)_{DW} + (M_Z)_{Th}$$

Where *F* = Axial force

M = Bending moment

Subscripts indicate the loads shown below

DW	= Deadweight
Th	= Thermal expansion
Ρ	= Internal pressure

x, y and z = Component of x,y and z direction.

- 2) Calculate the cross sectional area *A* and the section modulus *Z* assuming the minimum wall thickness.
- 3) Calculate the stress σ_{nor} at the evaluation point under normal operation.

$$\sigma_{nor} = P_m + P_b = F/A + M/Z$$

The maximum stress for each weld in the piping system was evaluated as follows:

1) For SMAW and SAW welds, calculate the absolute sum of the axial force, the bending and torque moment due to deadweight, the internal pressure, the thermal expansion, and earthquake using the following equations:

$$\begin{aligned} |F| &= |F_{DW}| + |F_{Th}| + |F_{P}| + |F_{SSE}| + |F_{SAM}| \\ |M| &= \sqrt{((M_{X})^{2} + (M_{Y})^{2} + (M_{Z})^{2})} \\ M_{X} &= |(M_{X})_{DW}| + |(M_{X})_{Th}| + |(M_{X})_{SSE}| + |(M_{X})_{SAM}| \\ M_{Y} &= |(M_{Y})_{DW}| + |(M_{Y})_{Th}| + |(M_{Y})_{SSE}| + |(M_{Y})_{SAM}| \\ M_{Z} &= |(M_{Z})_{DW}| + |(M_{Z})_{Th}| + |(M_{Z})_{SSE}| + |(M_{Z})_{SAM}| \end{aligned}$$

Where subscripts indicate the following loads.

- SSE = Inertia load due to SSE
- SAM = Seismic anchor motion load due to SSE.
- If the weld is a TIG weld, the loads due to thermal expansion and seismic anchor movements may be excluded per SRP 3.6.3.
- 3) Calculate stress under the maximum load σ_{max} at the weld joint.

$$\left|\sigma_{\max}\right| = \left|P_{m_{\max}}\right| + \left|P_{b_{\max}}\right| = \left(\left|F\right|/A + \left|M\right|/Z\right)$$

The BAC assessment points were then plotted on the BAC to determine LBB acceptance. In some cases, the welds may not be acceptable if the assessment is based on the assumption of a SMAW weld joint. In this case, the weld joint can be qualified as a TIG weld, and this can be implemented in the piping system fabrication/construction on a location-unique basis.

A2.4 BAC Setting for LBB Evaluation

Table A2-1 lists the Pressurizer surge piping property selected for setting the BAC. The detailed BACs are shown in Figure A2-3. Table A2-2 is the tabulated BAC points.

A2.5 References

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2. Leak-Before-Break Evaluation Procedures,' "Design of Structures, Components, Equipment, and Systems," <u>Standard Review Plan for the Review of Safety Analysis Reports for Nuclear</u> <u>Power Plants</u>. NUREG-0800, Standard Review Plan 3.6.3, Rev. 1, U.S. Nuclear Regulatory Commission, Washington, DC, March 2007.

3. "Evaluation of Potential for Pipe Breaks," <u>Report of U.S. NRC Piping Review Committee</u>. NUREG-1061, Vol. 3, U.S. Nuclear Regulatory Commission< Washington, DC, 1984.

4. <u>PICEP: Pipe Crack Evaluation Program</u>. NP-3596-SR, Rev. 1, Electric Power Research Institute, 1987.

5. Kumar, V, and German, M. D., "Elastic-Plastic Fracture Analysis of Through-Wall and Surface Flaws in Cylinders," EPRI NP-5596, January 1988.

6. D. Abdollahian and B. Chexal, "Calculation of Leak Rates Through Cracks in Pipes and Tubes," EPRI NP-3395, Electric Power Research Institute, Palo Alto, CA, December 1983.

7. Regulatory Guide 1.45, "Guidance On Monitoring And Responding To Reactor Coolant System Leakage." U. S. Nuclear Regulatory Commission, May 2008.

Subsystem	OD, inches	t, inches	Material	Temp, ⁰F ⁽¹⁾	Pressure, psig ⁽¹⁾	Axial. Stress, ksi	BAC Figure And Table No.
Surge Line ⁽¹⁾	16	1.594	SA-312 TP316	653	2,248 ⁽¹⁾	4.017	A2-1

Table A2-1 the Pressurizer surge piping property

Note:

1. Used conservative lower 2243 psig for leakage which is the pressurizer end pressure

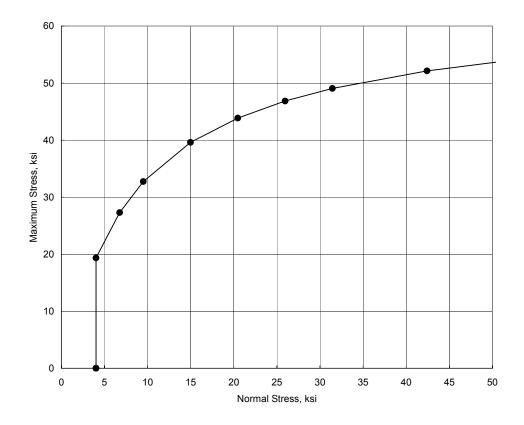


Figure A2-1. BAC for Surge Line

r	
Normal	Maximum
Stress,	Stress,
ksi	ksi
4.008	0
4.008	19.355
6.751	27.288
9.494	32.738
14.98	39.619
20.466	43.873
25.952	46.847
31.438	49.059
42.411	52.148
53.383	54.242