

1 **Division of Spent Fuel Storage and Transportation**
2 **Interim Staff Guidance-23**

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4
5 **Issue: Application of ASTM Standard Practice C1671-07 when performing**
6 **technical reviews of spent fuel storage and transportation packaging**
7 **licensing actions.**

8
9 **Introduction:**

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11 The standard review plans for storage of spent nuclear fuel and transportation of fissile
12 materials do not address, in detail, the technical considerations for crediting the neutron
13 absorber content of metal matrix composites used for preventing nuclear criticality. The Division
14 of Spent Fuel Storage and Transportation (SFST) considers the application of acceptance
15 criteria and methodology described in the recently developed American Standard for Testing
16 and Materials (ASTM) standard practice C1671-07, "Standard Practice for Qualification and
17 Acceptance of Boron Based Metallic Neutron Absorbers for Nuclear Criticality Control for Dry
18 Cask Storage Systems and Transportation Packaging,"¹ with some exceptions, additions, and
19 clarifications appropriate for staff use in their review activities. This Interim Staff Guidance (ISG)
20 provides guidance to the staff and is not a regulatory requirement. Alternative approaches are
21 acceptable if technically supportable.

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23 **Discussion:**

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25 Use of ASTM C1671-07

26 The staff considers the terminology and statements within ASTM Standard Practice C1671-07
27 as acceptable guidance with some additions, clarifications and exceptions delineated below, for
28 reviewing spent nuclear fuel storage cask and transportation packages, and therefore
29 appropriate for use by the Spent Fuel Storage and Transportation (SFST) staff.

30
31 Clarification regarding use of Section 5.2.1.3 of ASTM C1671-07

32 If the supplier has shown that process changes do not cause changes in the density, open
33 porosity, composition, surface finish, or cladding (if applicable) of the neutron absorber material,
34 the supplier should not be required to re-qualify the material with regard to thermal properties or
35 resistance to degradation by corrosion and elevated temperatures. This clarification *does not*
36 extend to long-term use (e.g., a year or more) of neutron absorbing materials in spent fuel
37 pools, where minor contaminants accrued during fabrication can significantly influence the
38 corrosion behavior of such materials.

39
40 Exception to Section 5.2.3 of ASTM C1671-07

41 The staff does not accept the following language in Section 5.2.3: "Requalification for a
42 qualified neutron absorber material produced by a new supplier may consist of review of key
43 processes and process controls to verify that they have been adequately replicated by the new
44 supplier."

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46 The staff considers a review of key processes and process controls alone insufficient to ensure
47 that qualified neutron absorbers produced by a new supplier will meet the same specifications
48 as those produced by the previous supplier.

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Clarification regarding use of Section 5.2.5.1 of ASTM C1671-07

Section 5.2.5.1 of C1671-07 requires that the neutron absorber material be exposed to “service conditions or equivalent accelerated conditions” as part of the qualifying tests. The staff should ensure that the service life adequately represents the term of the license or Certificate of Compliance, e.g., 5 or 20 years, or longer if subsequent renewals will be requested. The staff is cautioned that the effects of accelerated testing may not exactly match the actual effects encountered under operating conditions over the entire service life. Hence, for accelerated tests, the computed test period should represent a period longer than the anticipated service life. The staff should confirm that the service life for the neutron absorbing materials is specified in the Safety Analysis Report and Certificate of Compliance, or the Technical Specifications of the application.

Additional guidance regarding use of Section 5.2.5.3 of ASTM C1671-07

The following additional guidance applies to Section 5.2.5.3: Neutron absorbing materials should undergo testing to simulate submersion and subsequent cask drying conditions, as part of a qualifying test program.

Clad aluminum/boron carbide neutron absorbers with core porosities between one and three-percent have exhibited blistering after simulated cask or package drying events. This blistering was due to flash steaming of water that was trapped in pores. The staff is concerned that blistering could have an impact on retrievability and (during loading in the spent fuel pool) on the effective neutron multiplication factor, k_{eff} .

Clarification regarding use of Section 5.2.6.2 of ASTM C1671-07

If a coupon contiguous to every plate of neutron absorbing material is not examined during acceptance testing, the qualifying (or re-qualifying) neutron attenuation program should be done with a sufficient number of samples to ensure that the neutron absorbing properties of the materials meet the minimum required areal density of the neutron absorber.

Clarification regarding use of Section 5.2.6.2 and 5.3.4.1 of ASTM C1671-07

The following additional guidance applies to Section 5.2.6.2: The “credit” taken for the amount of boron-10 (^{10}B) present in the neutron absorbing material for the calculation of the effective neutron multiplication factor, k_{eff} , must be clearly stated in Chapter 8 of a Part 71 application, and the proposed Technical Specifications in a Part 72 application.

Based on recommendations in NUREG-1567³ and NUREG-1609⁴, NUREG-1617⁵ it has been the staff’s practice to limit the credit for neutron absorber materials to only 75-percent of the minimum amount of boron-10 (^{10}B) confirmed by acceptance tests. The staff has permitted up to 90-percent credit in certain cases where the absorber materials are shown by neutron attenuation testing of production lots to be effectively homogeneous, and the boron carbide particle size is sufficiently small to preclude neutron streaming.

If 90-percent credit is taken for the efficacy of the neutron absorber, then methods other than neutron attenuation should be used only as verification or partial substitution for attenuation tests. Benchmarking of other methods, against neutron attenuation testing, should be done periodically throughout acceptance testing, under appropriate attenuation conditions and with proper sample sizes. This should be done to confirm the adequacy of the proposed methods, as direct measurements of neutron attenuation are the most reliable method of measuring the

99 expected neutron absorbing behavior of the poison plates.
100 For neutron absorbing materials for which 75-percent credit is taken, direct neutron attenuation
101 measurements should be required only as part of a qualification program. Once qualified, other
102 methods which have been validated by attenuation measurements, such as wet chemistry
103 analyses, are sufficient to verify the minimum areal density of the neutron absorbing material
104 during acceptance testing.

105
106 Exception to Section 5.2.6.2(1) of ASTM C1671-07

107 The staff does not accept the following language in Section 5.2.6.2(1): “If materials with
108 discrete absorber particles or phases are used for calibration standards, then the size of the
109 particles containing the neutron absorber should be small enough so that neutron streaming and
110 self-shielding is insignificant.”

111
112 Only homogenous neutron absorbing materials such as zirconium diboride (ZrB_2) with uniform
113 absorption properties should be considered for neutron attenuation testing standards, as
114 homogenous materials preclude, or at least minimize, any neutron streaming effects which may
115 occur in heterogeneous materials. This exception to ASTM C1671-07 precludes the use of
116 materials such as boron carbide reinforced aluminum matrix composites as calibration
117 standards for neutron absorption.

118
119 Additional guidance regarding use of Section 5.2.6.2 of ASTM C1671-07

120 Section 5.2.6.2 states: “If uniformity testing for areal density will be by means other than
121 neutron attenuation, the user of the proposed method should confirm that the proposed method
122 is acceptable to the designer.”

123
124 The applicant should confirm that use of a uniformity testing method other than neutron
125 attenuation is acceptable to the NRC, not just the designer.

126
127 Additional guidance regarding use of Section 5.2.6.2(2) of ASTM C1671-07

128 The following additional guidance applies to Section 5.2.6.2(2): The size of the collimated
129 neutron beam should be specified for attenuation testing, and limited to 2.54-cm diameter, with
130 a tolerance of 10-percent.

131
132 A neutron beam 1-cm diameter is often used for attenuation measurements. There have been
133 requests for relief to increase the size of the neutron beam. The staff conducted an
134 independent criticality study using a typical spent nuclear fuel transportation package to
135 determine if neutron attenuation measurements using beam sizes in excess of 1-cm are unable
136 to detect localized regions in the neutron absorbing material deficient in neutron absorber. In
137 the study, it was assumed that the neutron absorber (^{10}B) arranged itself into a “checkerboard”
138 fashion of alternating boron-rich and boron-deficient regions where the boron concentration was
139 50-percent greater and 50-percent less than the average amount of boron in a homogenous
140 plate of boron and aluminum. The staff considers this hypothetical configuration bounding of
141 any possible “real-life” defects which might occur in actual manufacturing. In the simulations,
142 two models were considered. One model permitted a non-constant density, where boron was
143 removed from boron-deficient regions and directly added to adjacent regions. In the second
144 model, the quantity of aluminum and carbon were adjusted in each of the regions so that the
145 overall mass density of the plate remained uniform. The sizes of the boron-rich and boron
146 deficient regions were then gradually increased, and changes in k_{eff} were observed. This is
147 plotted in Figure 1.

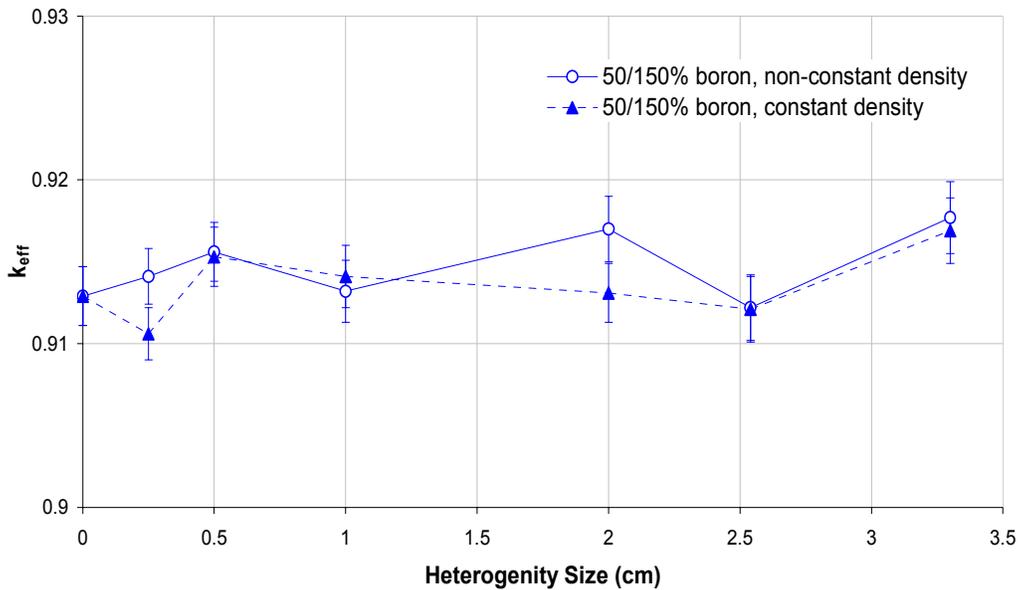


Figure 1: Plot of the Effective Neutron Multiplication Factor, k_{eff} , as a Function of Heterogeneity size

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153 The results of the study showed no significant difference in k_{eff} when the size of the
154 heterogeneities (the length of each boron deficit or rich region) increased from 1 cm to 2.54 cm.
155 It should be noted that this study was conducted on a single transportation package design.
156 The staff considers the heterogeneities introduced in the neutron absorbing materials sufficiently
157 exaggerated that this study suitably reflects the basis for a general determination.

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159 As such, the staff regards collimated neutron beams with nominal diameters between 1 and
160 2.54 cm, with tolerances of 10-percent, as sufficiently capable of detecting defects within the
161 neutron absorbing material, and should be considered acceptable for the purposes of
162 qualification and acceptance testing of neutron absorbing materials.

163

164 Additional guidance regarding use of Section 5.2.6.3 of ASTM C1671-07

165 The following additional guidance applies to Section 5.2.6.3: A visual inspection procedure
166 which describes the nominal inspection criteria should be specified in the applicant's
167 acceptance tests. Visual inspection should be conducted on all of the neutron absorbing
168 materials intended for service.

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170 Special consideration should be given to visual inspection of plate materials containing more
171 than 30 volume percent boron carbide. Plate materials with high loadings of boron carbide (>
172 30 volume percent) are subject to edge cracking during rolling operations, and the procedures
173 used for inspection of these edge effects need to be closely reviewed to determine the
174 adequacy of the specified procedures.

175

176 As part of the visual inspection of the neutron absorbing material, it is important to ensure that
177 there are no defects that might lead to problems in service; such as delaminations that could
178 appear on clad neutron absorbing materials. The concern is that any gross defect on the plate
179 or plate edge may lead to separations, especially from vibrations during transportation; this

180
181 could lead to a lack of absorber capability over the missing or misplaced region within a plate
182 material.

183
184 Additional guidance regarding use of Section 5.2.6.3 of ASTM C1671-07

185 The following additional guidance applies to Section 5.2.6.3: The maximum permissible
186 thickness deviation of the neutron absorbing material should be specified, and actions to be
187 taken if the thickness is outside the permissible limits.

188
189 During the production of neutron absorbing materials, minor deviations from the specified
190 physical dimensions are expected. These deviations, and in particular, variations of the neutron
191 absorbing material thickness should be discussed in the application, either in the Technical
192 Specifications or package drawings which are referenced in the Certificate of Compliance. The
193 applicant should specify the maximum permissible thickness deviation, and the actions taken if
194 the thickness is outside the permissible limits. This is done to ensure adequate performance of
195 the neutron absorbing materials. In the past, the staff have allowed acceptance testing where a
196 minimum plate thickness is specified, which permitted local depressions, so long as the
197 depressions were no more than 0.5-percent of the area on any given plate, and the thickness at
198 their location is not less than 90-percent of the minimum design thickness.

199
200 Clarification regarding use of Sections 5.2.7 and 5.3 of ASTM C1671-07

201 When implementing Sections 5.2.7 and 5.3, a description of the key process, operations
202 process controls, and the acceptance testing steps of neutron absorbing materials should be
203 included in Chapter 8 of a Part 71 application, and the proposed Technical Specifications in a
204 Part 72 application.

205
206 Additional guidance regarding use of Section 5.2.7.1 of ASTM C1671-07

207 In addition to the guidance provided in Section 5.2.7.1, a change of the matrix alloy, or a change
208 in the material's heat treatment which may cause an undesirable reaction to occur within the
209 matrix itself or between the matrix and a secondary phase should also be considered key
210 processes.

211
212 Heat treatments which cause the precipitation of water-soluble aluminum carbide (Al_4C_3) or
213 embrittling $Al_xB_yC_z$ phases could degrade the mechanical properties of the material.

214
215 Additional guidance regarding use of Section 5.4 of ASTM C1671-07

216 The following additional guidance applies to Section 5.4: Title 10 CFR Part 71 and Part 72
217 applications, neutron absorbing materials intended for criticality control should always have a
218 safety classification of "A", under the guidance of NUREG/CR-6407.⁷

219
220 **Regulatory Basis:**

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222 10 CFR 71.33(b)(4): The application must include a description of the proposed
223 package in sufficient detail to identify the package accurately and provide a sufficient
224 basis for evaluation of the package. The description must include extent of reflection, the
225 amount and identity of nonfissile materials used as neutron absorbers or moderators,
226 and the atomic ratio of moderator to fissile constituents;

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228
229 10 CFR 71.55(b): Except as provided in paragraph (c) or (g) of this section, a package
230 used for the shipment of fissile material must be so designed and constructed and its
231 contents so limited that it would be subcritical if water were to leak into the containment
232 system, or liquid contents were to leak out of the containment system so that, under the
233 following conditions, maximum reactivity of the fissile material would be attained: (1) The
234 most reactive credible configuration consistent with the chemical and physical form of
235 the material; (2) Moderation by water to the most reactive credible extent; and (3) Close
236 full reflection of the containment system by water on all sides, or such greater reflection
237 of the containment system as may additionally be provided by the surrounding material
238 of the packaging.

239
240 10 CFR 71.55(e): A package used for the shipment of fissile material must be so
241 designed and constructed and its contents so limited that under the tests specified in §
242 71.73 ("Hypothetical accident conditions"), the package would be subcritical. For this
243 determination, it must be assumed that: (1) The fissile material is in the most reactive
244 credible configuration consistent with the damaged condition of the package and the
245 chemical and physical form of the contents; (2) Water moderation occurs to the most
246 reactive credible extent consistent with the damaged condition of the package and the
247 chemical and physical form of the contents; and (3) There is full reflection by water on all
248 sides, as close as is consistent with the damaged condition of the package.

249 10 CFR 71.59(a)(2) A fissile material package must be controlled by either the shipper or
250 the carrier during transport to assure that an array of such packages remains subcritical.
251 To enable this control, the designer of a fissile material package shall derive a number
252 "N" based on all the following conditions being satisfied, assuming packages are stacked
253 together in any arrangement and with close full reflection on all sides of the stack by
254 water: two times "N" damaged packages, if each package were subjected to the tests
255 specified in § 71.73 ("Hypothetical accident conditions") would be subcritical with
256 optimum interspersed hydrogenous moderation

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258 10 CFR 71.64(a)(1)(iii): A package for the shipment of plutonium by air subject to §
259 71.88(a)(4), in addition to satisfying the requirements of §§ 71.41 through 71.63, as
260 applicable, must be designed, constructed, and prepared for shipment so that under the
261 tests specified in § 71.74 ("Accident conditions for air transport of plutonium") -- A single
262 package and an array of packages are demonstrated to be subcritical in accordance with
263 this part, except that the damaged condition of the package must be considered to be
264 that which results from the plutonium accident tests in § 71.74, rather than the
265 hypothetical accident tests in § 71.73.

266
267 10 CFR 72.124(b): Methods of criticality control. When practicable, the design of an
268 ISFSI or MRS must be based on favorable geometry, permanently fixed neutron
269 absorbing materials (poisons), or both. Where solid neutron absorbing materials are
270 used, the design must provide for positive means of verifying their continued efficacy.
271 For dry spent fuel storage systems, the continued efficacy may be confirmed by a
272 demonstration or analysis before use, showing that significant degradation of the
273 neutron absorbing materials cannot occur over the life of the facility.

274
275 10 CFR 72.154(a): The licensee, applicant for a license, certificate holder, and
276 applicant for a Certificate of Compliance shall establish measures to ensure that
277 purchased material, equipment, and services, whether purchased directly or

278 through contractors and subcontractors, conform to the procurement documents.
279 These measures must include provisions, as appropriate, for source evaluation
280 and selection, objective evidence of quality furnished by the contractor or
281 subcontractor, inspection at the contractor or subcontractor source, and
282 examination of products upon delivery.

283
284 10 CFR 72.236(c): (Certificate of Compliance holder only) The spent fuel
285 storage cask must be designed and fabricated so that the spent fuel is
286 maintained in a subcritical condition under credible conditions.

287
288 **Applicability:**

289 This guidance applies to reviews of dry cask storage and transport package designed for fissile
290 material conducted in accordance with NUREG-1536², "Standard Review Plan for Dry Cask
291 Storage Systems" (January 1997); NUREG-1567³, "Standard Review Plan for Spent Fuel Dry
292 Storage Facilities" (March 2000); NUREG-1609⁴, "Standard Review Plan for Transportation
293 Packages for Radioactive Material" (March 1999); NUREG-1617⁵, "Standard Review Plan for
294 Transportation Packages for Spent Nuclear Fuel" (March 2000); and Interim Staff Guidance 15
295 (ISG-15)⁶, "Materials Evaluation" (January 2001).
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298 **Technical Review Guidance:**

- 299
- 300 • Clarification on use of Section 5.2.1.3:
301 This clarification describes certain physical properties of the neutron absorbing material
302 which, when shown not to change, would not require requalification with regards to
303 corrosion or thermal degradation behavior.
304
 - 305 • Exception to Section 5.2.3:
306 New suppliers should re-qualify the neutron absorbing material.
307
 - 308 • Clarification on use of Section 5.2.5.1:
309 The staff should ensure that accelerated testing can justify the expected material
310 performance, potentially over a service life that is beyond the licensing time period.
311
 - 312 • Additional guidance on use of Section 5.2.5.3:
313 Testing should be added to simulate vacuum drying after submersion.
314
 - 315 • Clarification on use of Section 5.2.6.2:
316 Acceptance testing sampling is dependent on the statistical validity of qualification testing.
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 - 318 • Clarification on use of Section 5.2.6.2 and 5.3.4.1:
319 Methods other than neutron attenuation may be appropriate for acceptance testing of the
320 neutron absorbing material, depending on the amount of "credit" taken for the neutron
321 absorber.
322
 - 323 • Exception to Section 5.2.6.2(1):
324 Heterogeneous materials are not permitted to be used as neutron attenuation calibration
325 standards.

- 326
- 327 • Additional guidance on use of Section 5.2.6.2:
- 328 The applicant should confirm that its use of any alternative method for measuring the areal
- 329 density of ^{10}B is acceptable to the regulatory authority.
- 330
- 331 • Additional guidance on use of Section 5.2.6.2(2):
- 332 The neutron beam diameter used for attenuation measurements is limited to 1-inch with 10-
- 333 percent tolerance.
- 334
- 335 • Additional guidance on use of Section 5.2.6.3:
- 336 A visual inspection procedure for 100-percent of the plates of neutron absorbing material
- 337 should be specified in the application.
- 338
- 339 • Additional guidance on use of Section 5.2.6.3:
- 340 Maximum possible thickness variations in the neutron absorbing material should be
- 341 discussed in the application.
- 342
- 343 • Clarification of use of Sections 5.2.7 and 5.3:
- 344 Key processes and testing criteria should be placed in Chapter 8 of the Part 71 application
- 345 or in the Technical Specifications of a Part 72 application.
- 346
- 347 • Additional guidance on use of Section 5.2.7.1:
- 348 Changes to processing which may adversely affect the microstructure of the matrix may
- 349 require re-qualification of the neutron absorbing material.
- 350
- 351 • Additional guidance on use of Section 5.4:
- 352 For Part 71 and Part 72 applications, neutron absorbing materials should be given a safety
- 353 classification of "A", under the guidance of NUREG/CR-6407.⁷

354

355 **Recommendations:**

356

357 The staff recommends that the ASTM Standard Designation C1671-07, along with the qualifying

358 statements found in this document, be considered for use in the evaluation of licensing actions

359 which rely upon boron-based metallic neutron absorber materials for nuclear criticality control in

360 dry cask storage systems and transportation packaging.

361

362 **References:**

¹ ASTM C 1671-07, "Standard Practice for Qualification and Acceptance of Boron Based Metallic Neutron Absorber Materials for Nuclear Criticality Control for Dry Cask Storage Systems and Transportation Packaging," ASTM International, August 2007.

² NUREG-1536, "Standard Review Plan for Dry Cask Storage Systems," Spent Fuel Project Office, Office of Nuclear Material Safety and Safeguards, U.S. Nuclear Regulatory Commission, D.C. January 1997.

³ NUREG-1567, "Standard Review Plan for Spent Fuel Dry Storage Facilities," Spent Fuel Project Office, Office of Nuclear Material Safety and Safeguards, U.S. Nuclear Regulatory Commission, D.C. March 2000.

⁴ NUREG-1609, "Standard Review Plan for Transportation Packages for Radioactive Material" Spent Fuel Project Office, Office of Nuclear Material Safety and Safeguards, U.S. Nuclear Regulatory Commission, D.C. March 1999.

⁵ NUREG-1617, "Standard Review Plan for Transportation Packages for Spent Nuclear Fuel," Spent Fuel Project Office, Office of Nuclear Material Safety and Safeguards, U.S. Nuclear Regulatory Commission, D.C. March 2000.

⁶ Interim Staff Guidance 15 (ISG-15), "Materials Evaluation," Spent Fuel Project Office, Office of Nuclear Material Safety and Safeguards, U.S. Nuclear Regulatory Commission, D.C. January 2000.

⁷ NUREG/CR-6407, "Classification of Transportation Packaging and Dry Spent Fuel Storage System Components According to Importance to Safety," Idaho National Engineering Laboratory, ID. February 1996.

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E. William Brach, Director
Division of Spent Fuel Storage and Transportation