

  
**MITSUBISHI HEAVY INDUSTRIES, LTD.**  
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TOKYO, JAPAN

December 25, 2008

Document Control Desk  
U.S. Nuclear Regulatory Commission  
Washington, DC 20555-0001

Attention: Mr. Jeffrey A. Ciocco

Docket No. 52-021  
MHI Ref: UAP-HF-08292

**Subject: MHI's Response to US-APWR DCD RAI No. 120-793 Revision 0**

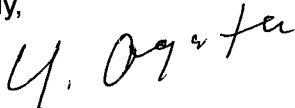
**Reference: 1)** "Request for Additional Information No. 120-793 Revision 0, SRP Section: 06.02.01.05, Application Section: 6.2.1.5" dated December 3, 2008.

With this letter, Mitsubishi Heavy Industries, Ltd. ("MHI") transmits to the U.S. Nuclear Regulatory Commission ("NRC") a document entitled "Response to Request for Additional Information No. 120-793 Revision 0."

Enclosed is the response to one RAI contained within Reference 1.

Please contact Dr. C. Keith Paulson, Senior Technical Manager, Mitsubishi Nuclear Energy Systems, Inc. if the NRC has questions concerning any aspect of the submittals. His contact information is below.

Sincerely,



Yoshiaki Ogata,  
General Manager- APWR Promoting Department  
Mitsubishi Heavy Industries, LTD.

Enclosure:

1. Response to Request for Additional Information No. 120-793 Revision 0

CC: J. A. Ciocco  
C. K. Paulson

Contact Information

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DOB  
NRO

Docket No. 52-021  
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Enclosure 1

UAP-HF-08292  
Docket Number 52-021

Response to Request for Additional Information  
No. 120-793 Revision 0

December 2008

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**RESPONSE TO REQUEST FOR ADDITIONAL INFORMATION**

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12/25/2008

**US-APWR Design Certification  
Mitsubishi Heavy Industries  
Docket No. 52-021**

**RAI NO.:** 120-793  
**SRP SECTION:** 06.02.01.05- MINIMUM CONTAINMENT PRESSURE ANALYSIS FOR EMERGENCY CORE COOLING SYSTEM PERFORMANCE CAPABILITY STUDIES  
**APPLICATION SECTION:** SRP 6.2.1.5  
**DATE OF RAI ISSUE:** 12/3/2008

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**QUESTION NO. : 06.02.01.05-6**

6.2.1.5: The exponent of the heat transfer coefficient, shown on page 6.2-38 of the DCD, is -0.62 instead of the value of -0.025 recommended in BTP 6-2, Figure 2. The exponent of -0.62 will reduce the heat transfer coefficient more rapidly than the exponent of -0.025, which is not conservative. However, Fig. 6.2.1-83 suggests the use of the value around -0.025. Please, clarify the discrepancy.

**ANSWER:**

The exponent of -0.62 in the equation on page 6.2-38 (the same equation is presented below) of the DCD is by a typo and -0.025 is correct. The value of -0.025 is used for the minimum containment pressure analysis actually as is confirmed from Figure 6.2.1-83.

$$H_{cond}(t) = 1.2 \times H_{Uchida} + \{H_{Tagami}(t_{end}) - 1.2 \times H_{Uchida}\} \exp\{-0.62(t - t_{eob})\}$$

This will be modified to the correct description in the next revision of the DCD.

**Impact on DCD**

Editorial: Correlation will be replaced.

The following equation will be presented in the subsection 6.2.1.5.8 on page 6.2-38 instead of the equation in the Answer.

$$H_{cond}(t) = 1.2 \times H_{Uchida} + \{H_{Tagami}(t_{end}) - 1.2 \times H_{Uchida}\} \exp\{-0.620.025(t - t_{eob})\}$$

**Impact on COLA**

There is no impact on the COLA

**Impact on PRA**

There is no impact on the PRA

This completes MHI's response to the NRC's question.