TAB 1

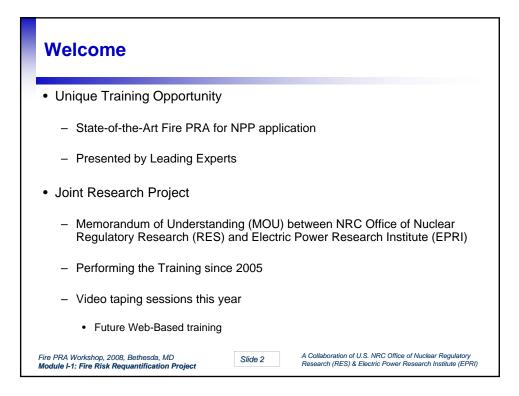
Opening Session: Welcome, Introductions and Overview

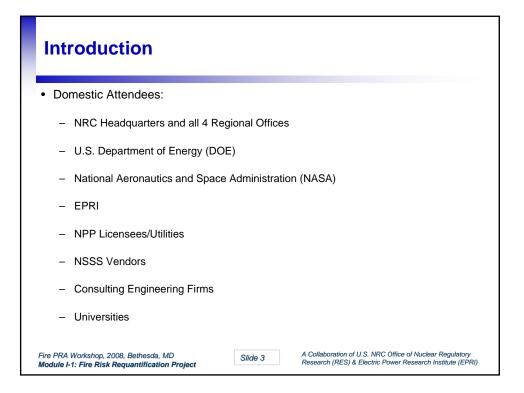
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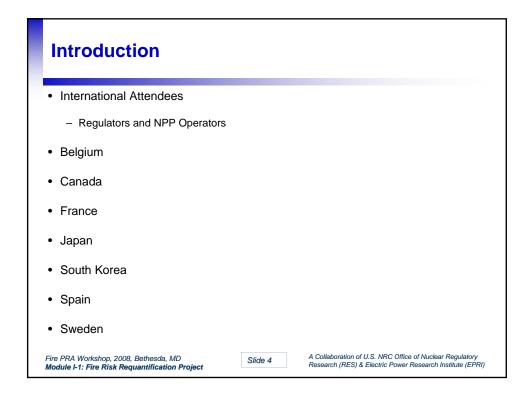
NRC Welcome

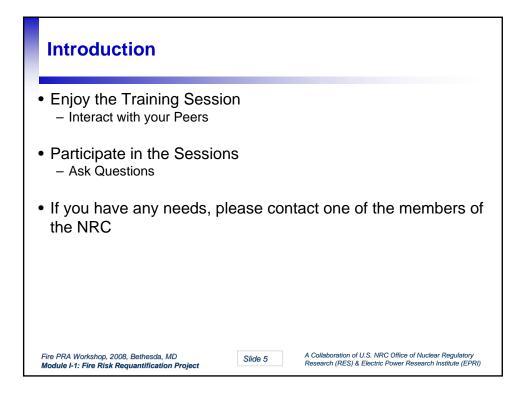
Mark Henry Salley U.S. NRC/RES Chief, Fire Protection Research Branch











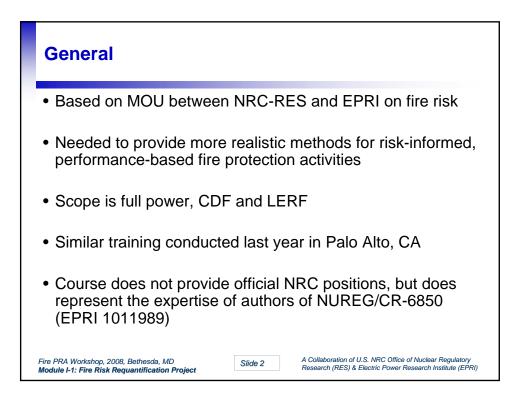
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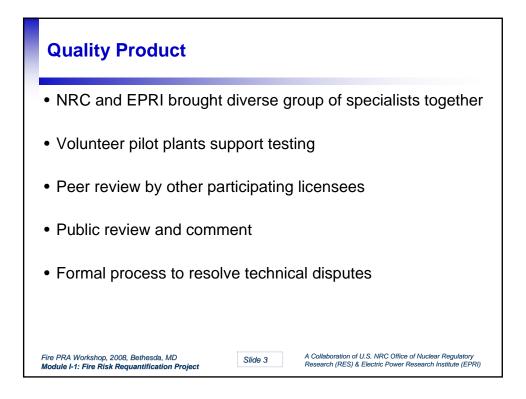
RES/EPRI Opening Remarks

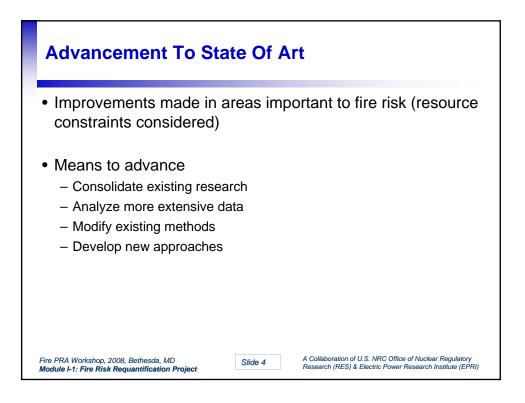
J. S. Hyslop NRC/RES/FPRB

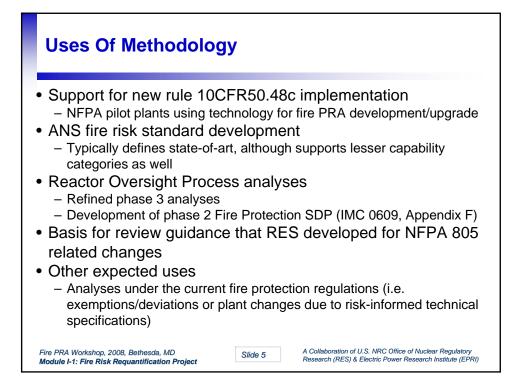
Ken Canavan EPRI

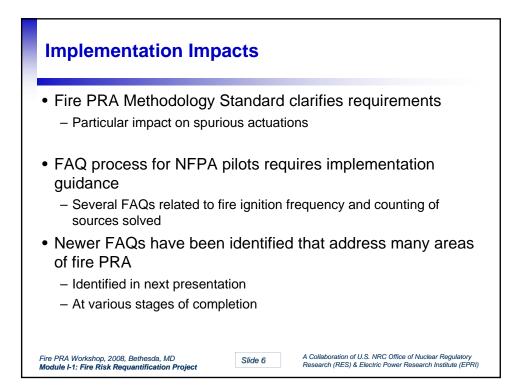


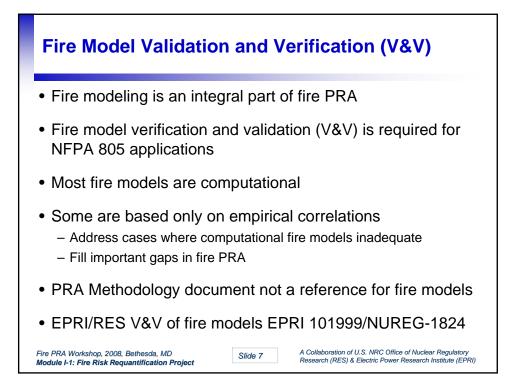




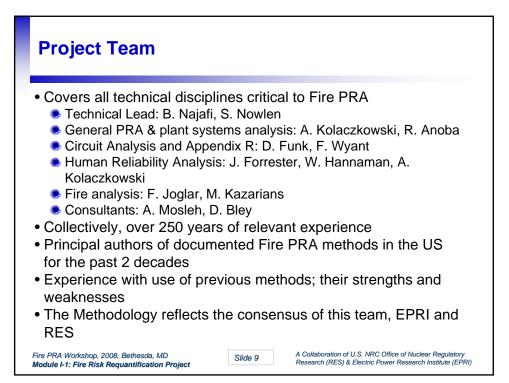








Related Activities	
• EPRI 1011989/NUREG/CR-6850	
 Publication 	Sept 2005
 First Workshop 	Jun 2005
 Second Workshop 	May 2006
 First detailed course 	Jul, Aug 2007
• EPRI 1011999/NUREG-1824	May 2007
 Current Fire PRA Course 	Sept, Nov 08
 Fire Modeling User's Guide 	mid 2009
 Fire HRA Methodology Development 	Fall 2009
FAQ Support	Ongoing
 Fire Modeling Training 	Ongoing
 Low Power/Shutdown Fire PRA Methods 	NRC
	U.S. NRC Office of Nuclear Regulatory Electric Power Research Institute (EPRI)



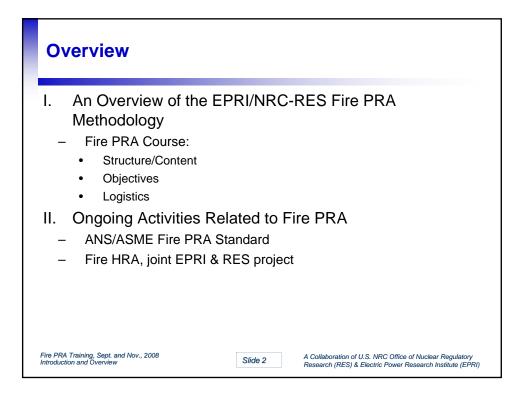
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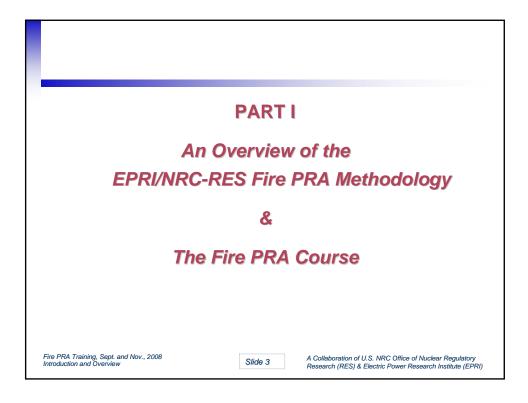
Methodology Overview, Course Structure and Course Objectives

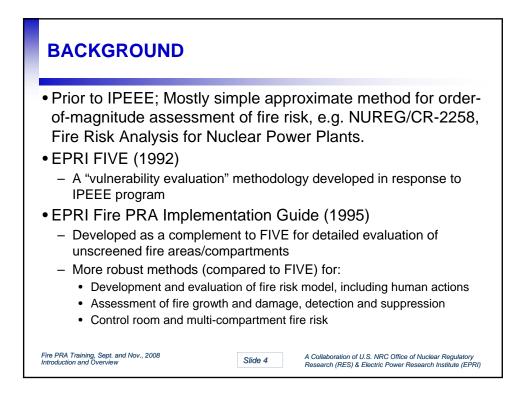
Steve Nowlen Sandia National Laboratories

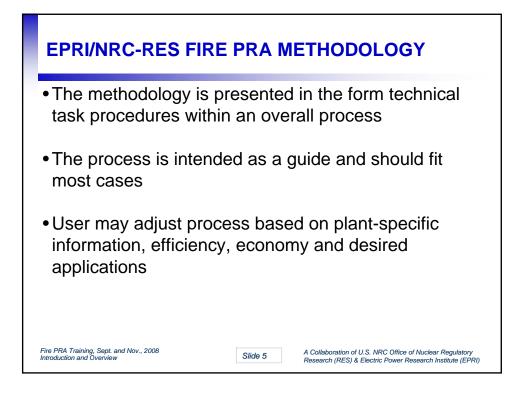
Bijan Najafi Science Applications International Corp.

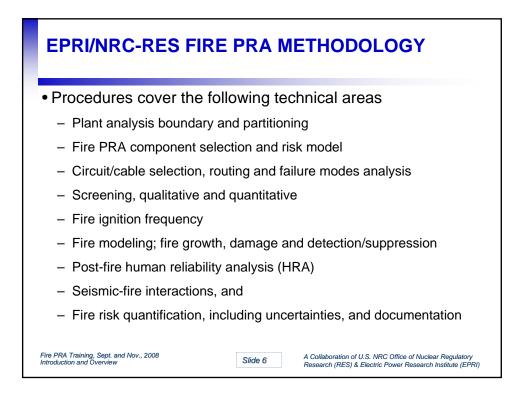






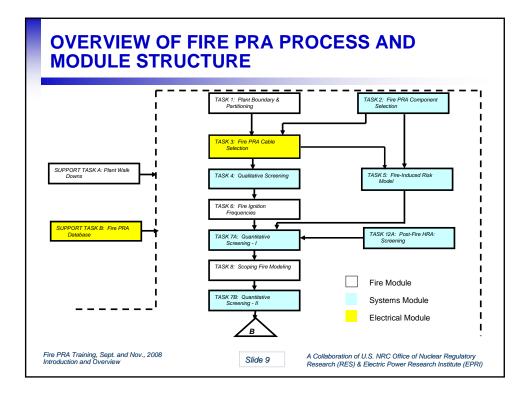


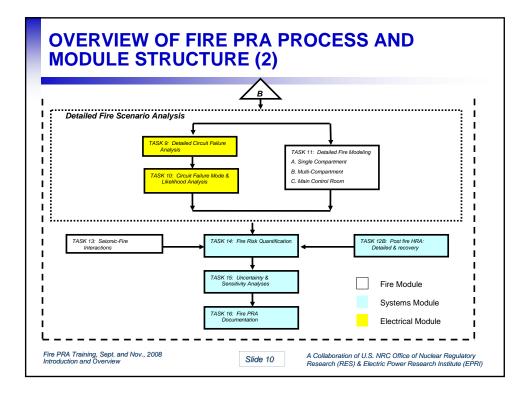


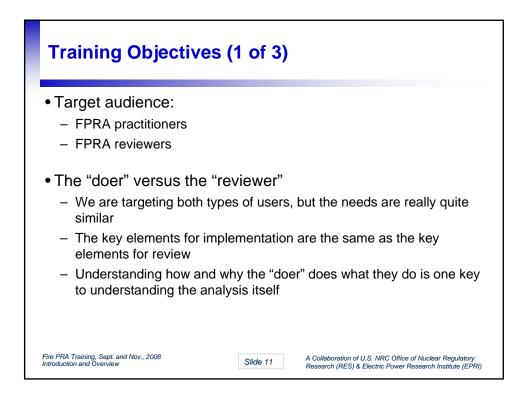


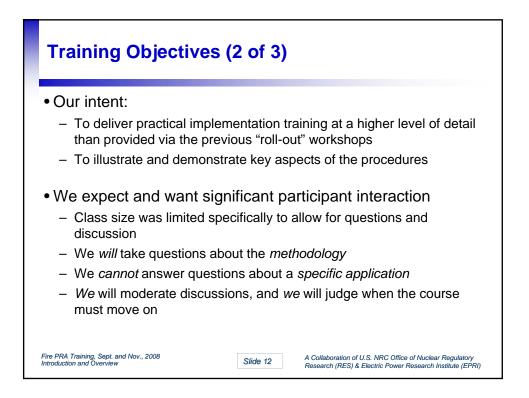
PROCEDURE CONTENT	
1. Purpose	
2. Scope	
Background information: General approach and assumptions	
Interfaces: Input/output to other tasks, plant and other information needed, walk-downs	
Procedure: Step-by-step instructions for conduct of the technical task	
6. References	
Appendices: Technical bases, data, examples, specia or instructions, tools or databases	l models
Fire PRA Training, Sept. and Nov., 2008 Slide 7 A Collaboration of U.S. NRC Office of Nu Introduction and Overview Research (RES) & Electric Power Research	

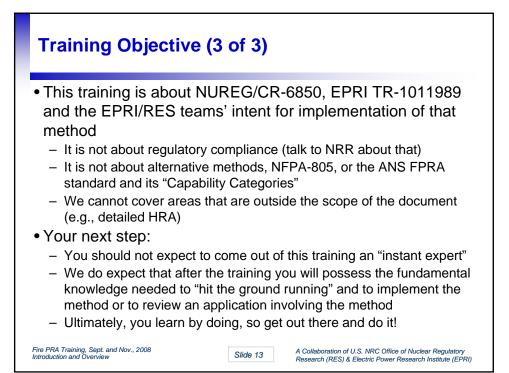
Course Structure	
Three parallel modules:	
– Module 1: Systems/PRA	
 Module 2: Electrical Analysis 	
 Module 3: Fire Analysis 	
 General structure for each module: 	
 PowerPoint presentations designed to convey key concepts and the general "how to" of each task 	
 Example problems designed to illustrate key elements of the procedures (more on this shortly) 	
Fire PRA Training, Sept. and Nov., 2008 Slide 8 A Collaboration of U.S. NRC Office of Nuclear Regulatory Research (RES) & Electric Power Research Institute (EPRI)	

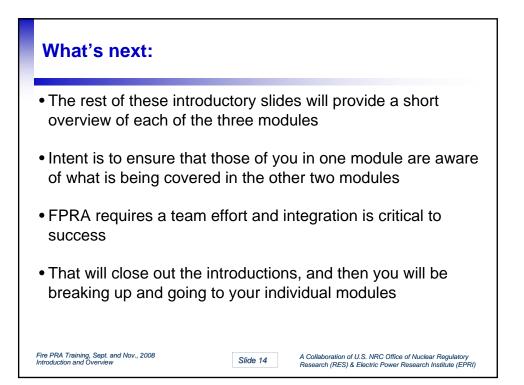


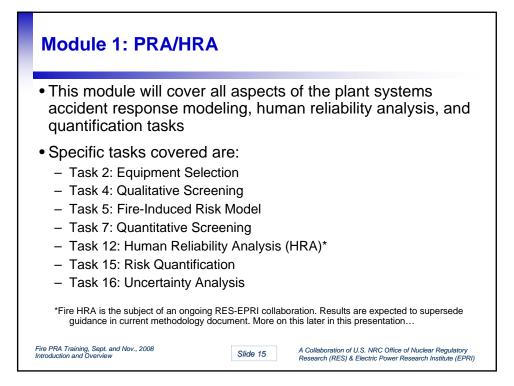


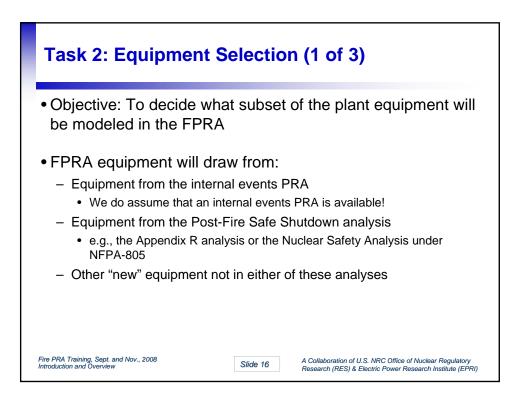


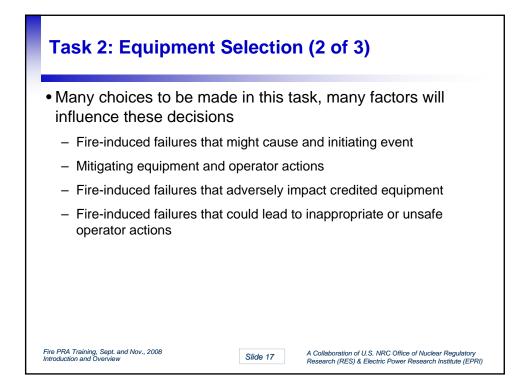


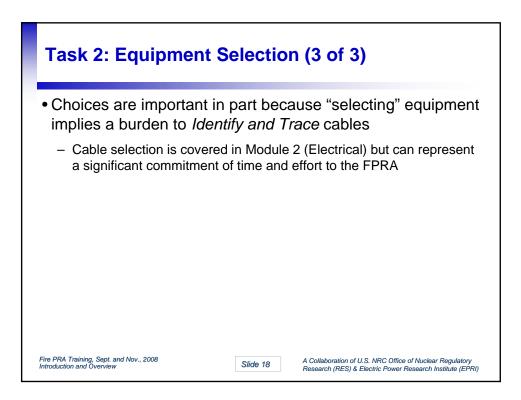


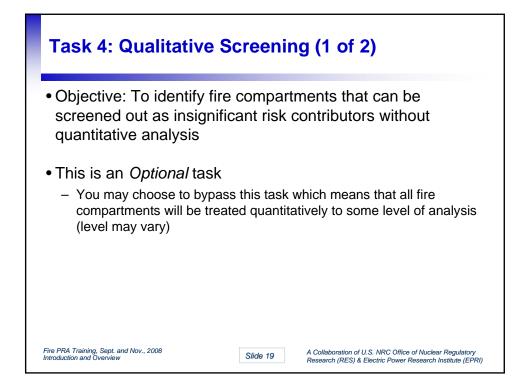


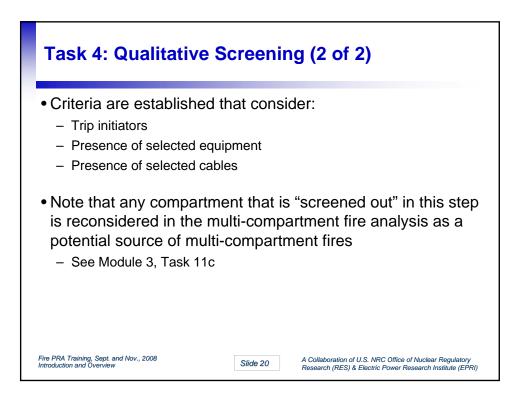


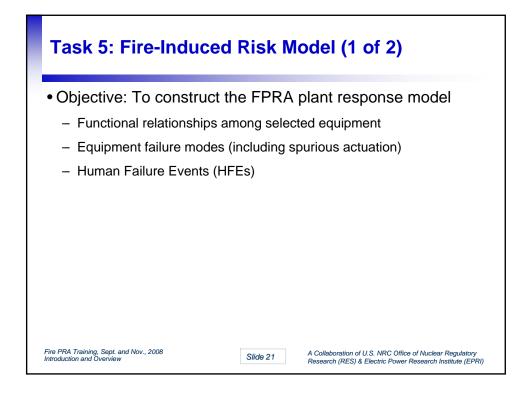


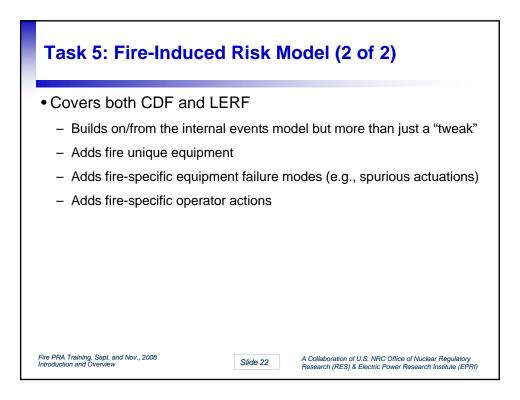


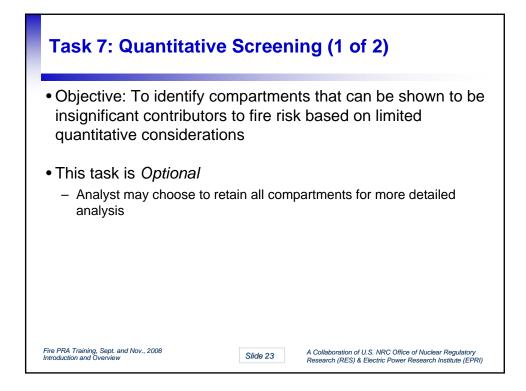


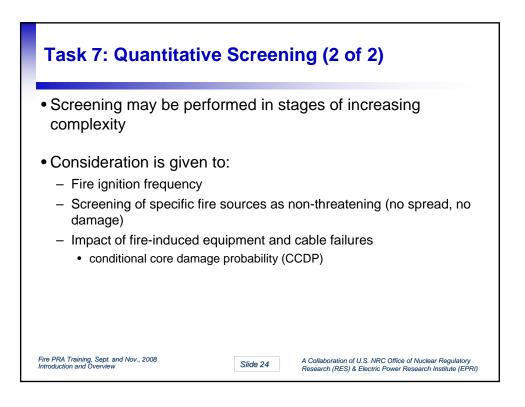


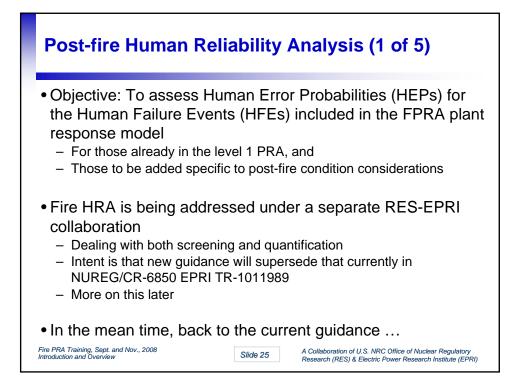


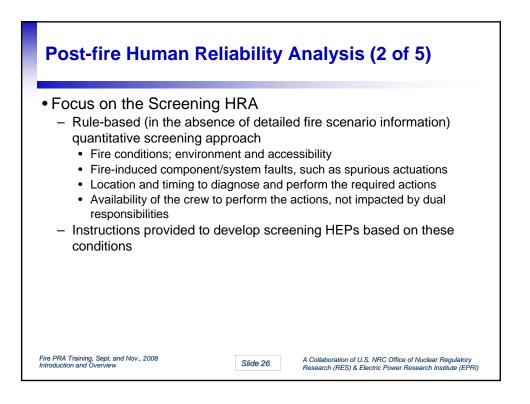


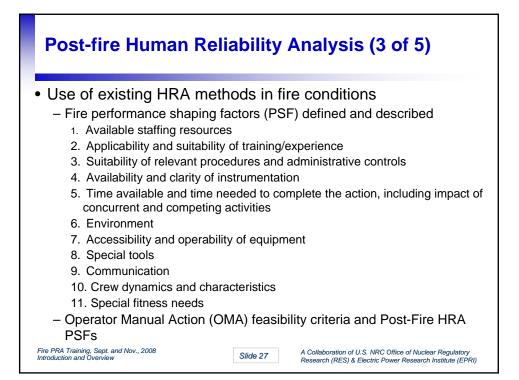


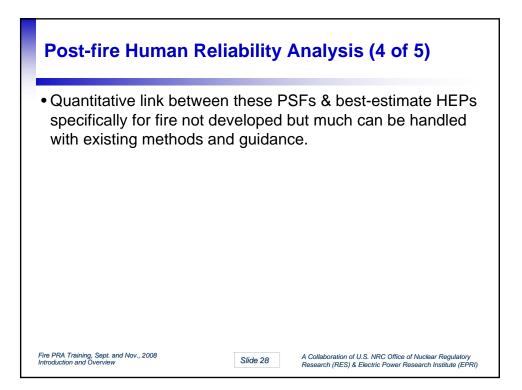


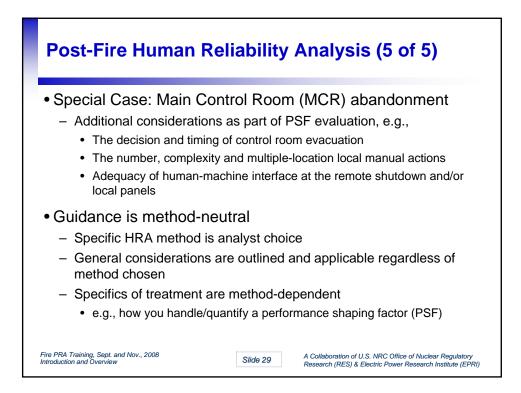


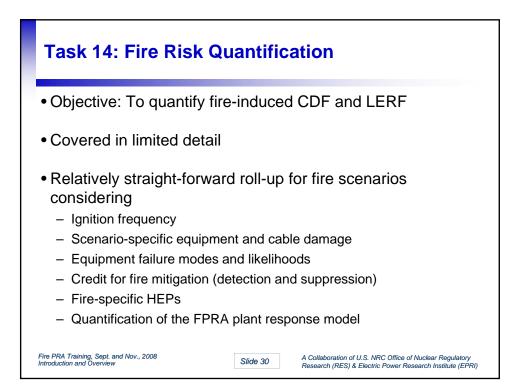


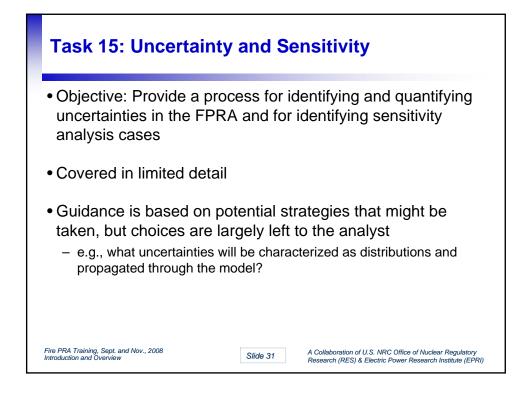


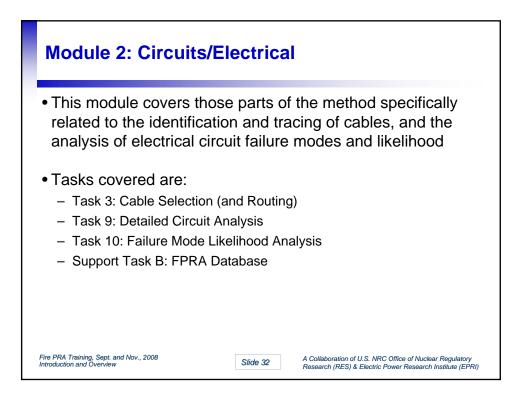


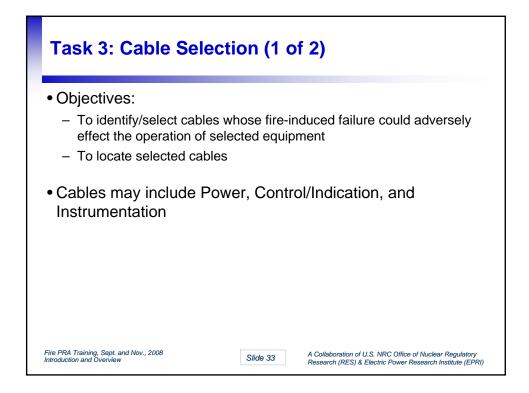


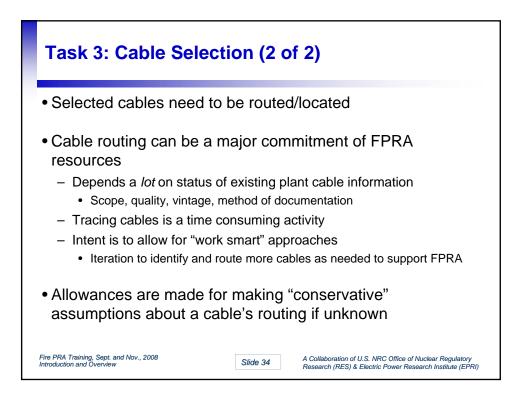


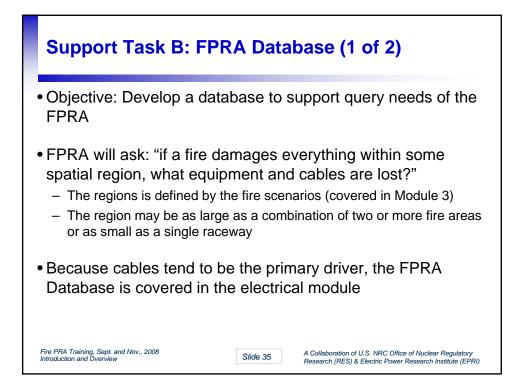


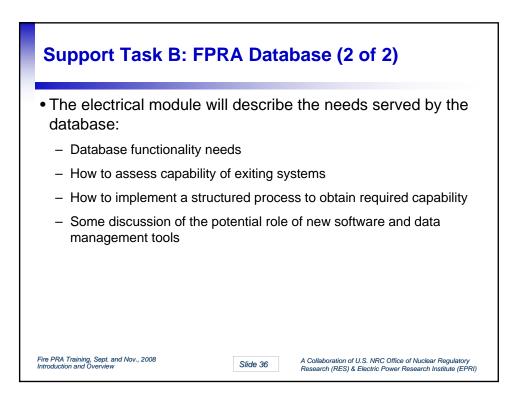


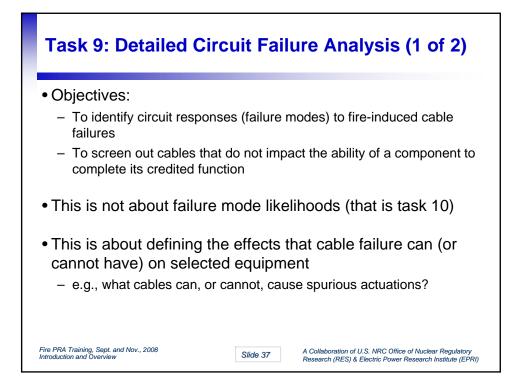


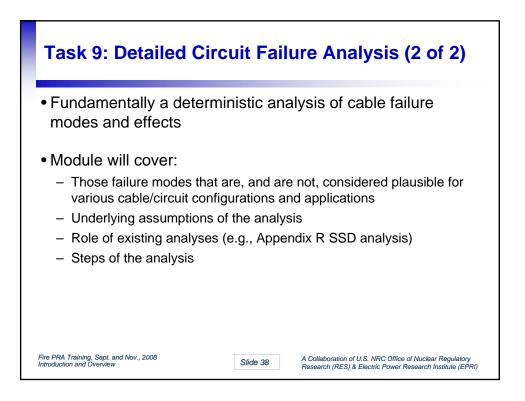


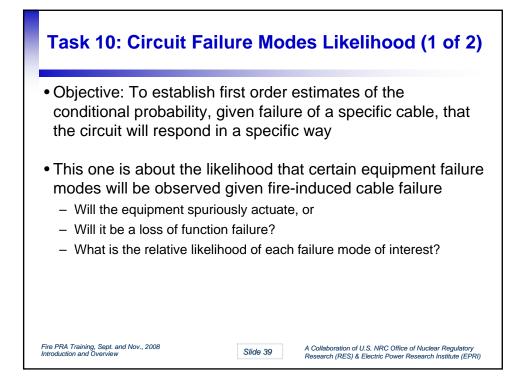


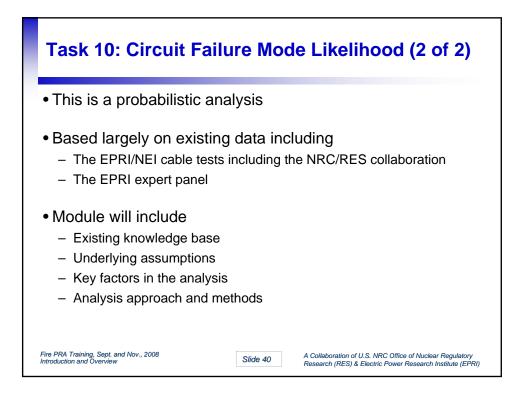


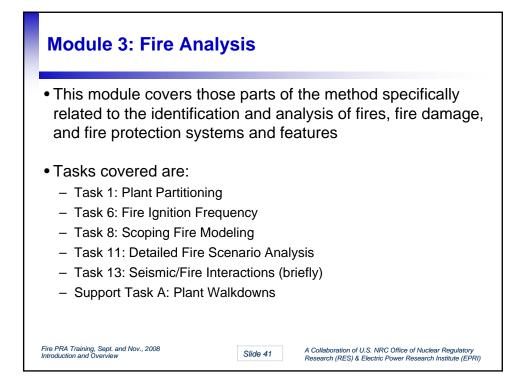


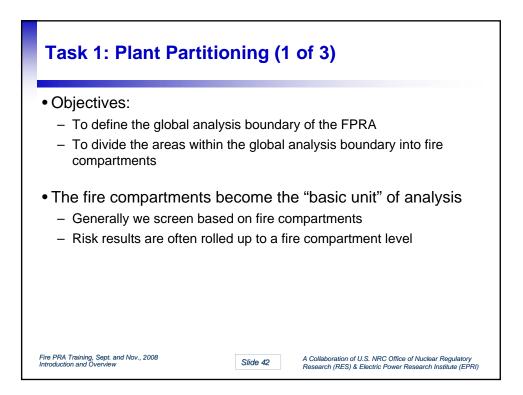


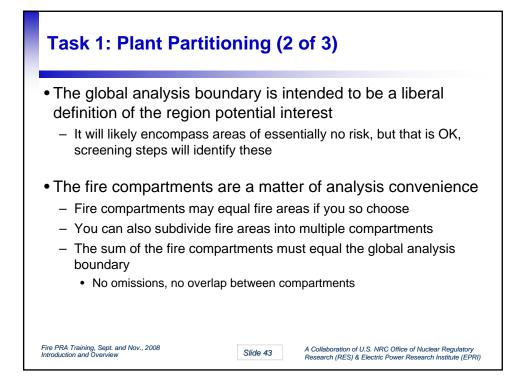


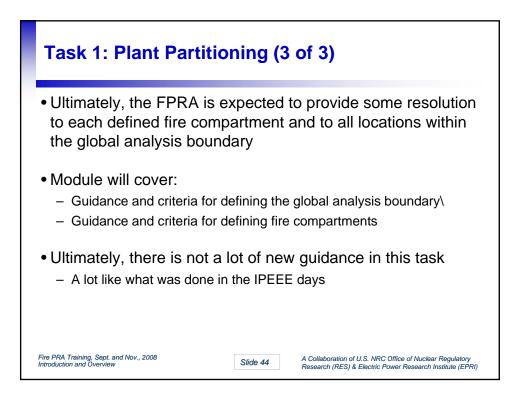


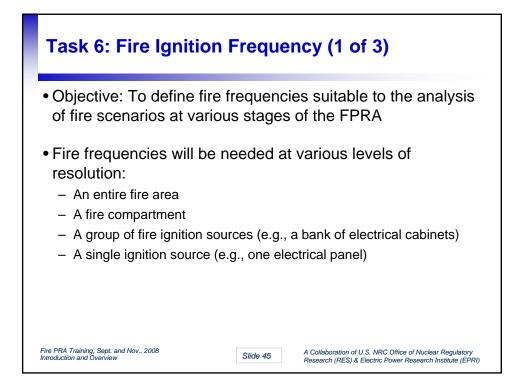


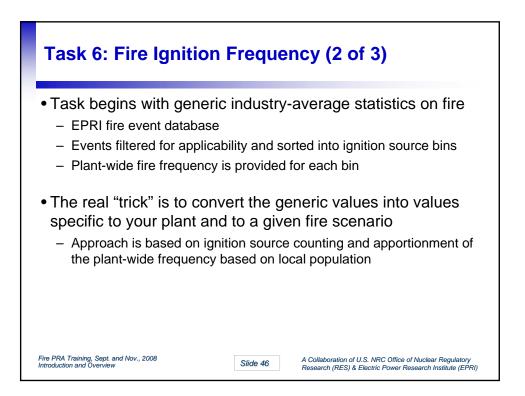


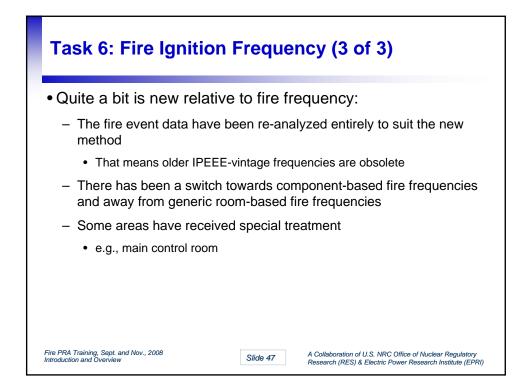


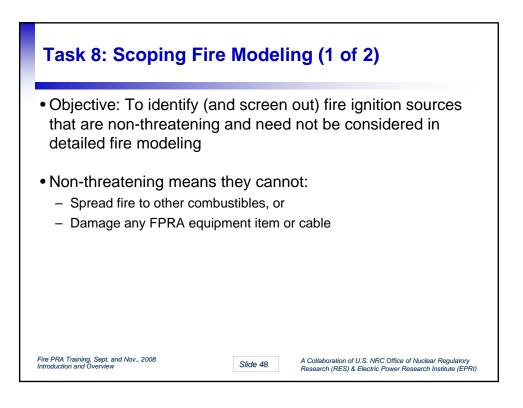


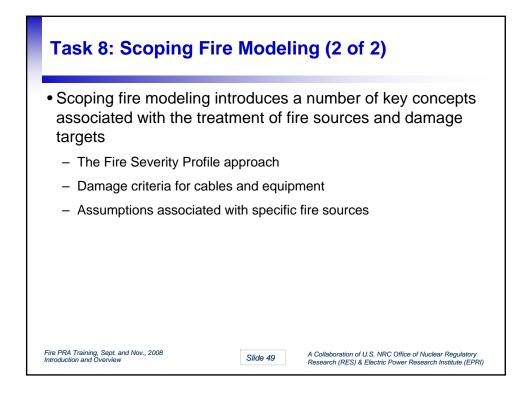


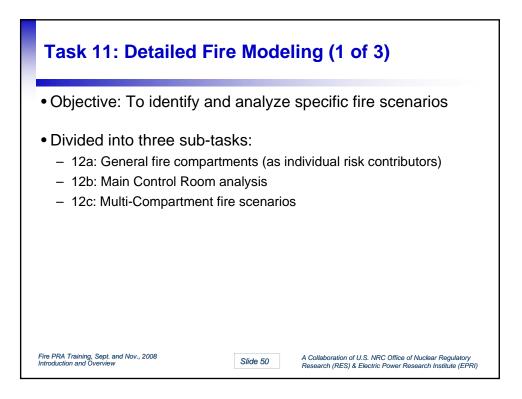


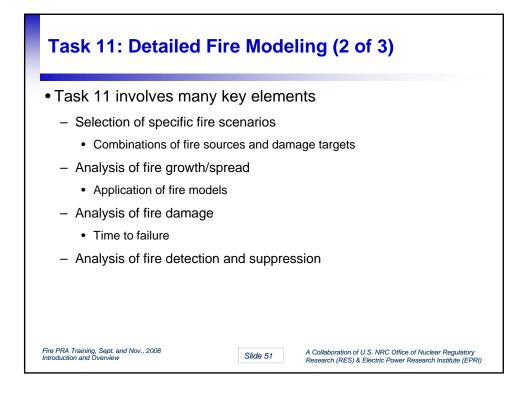


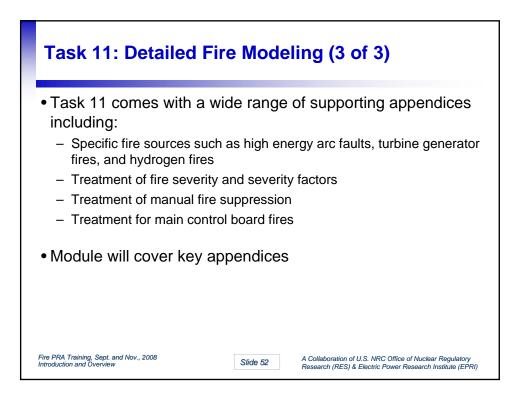


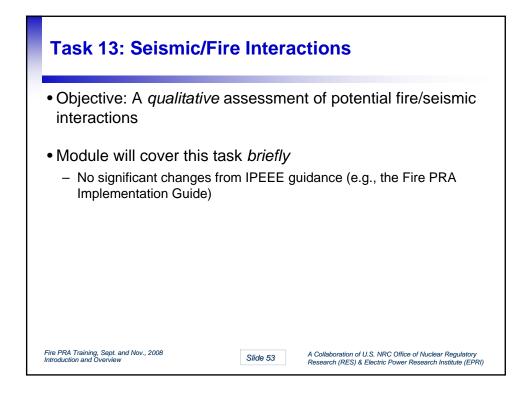


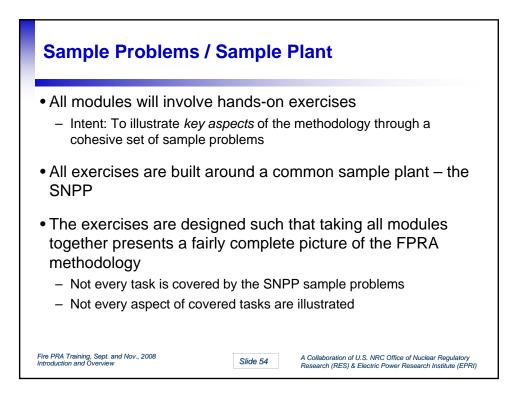


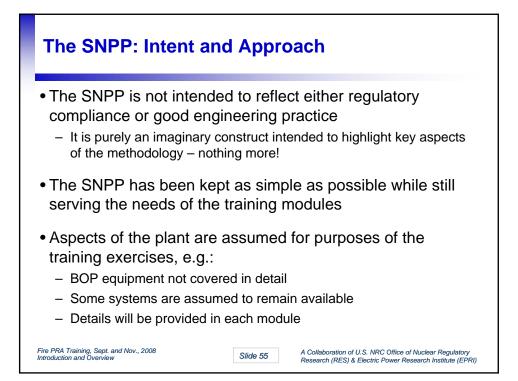


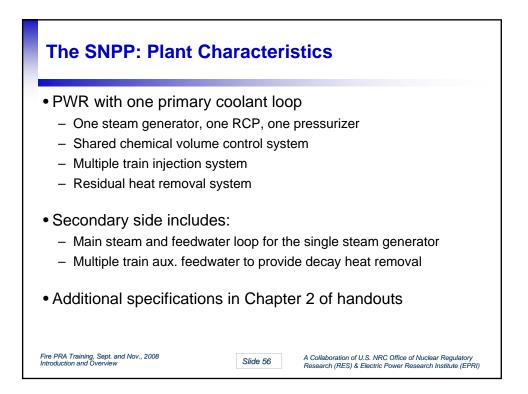


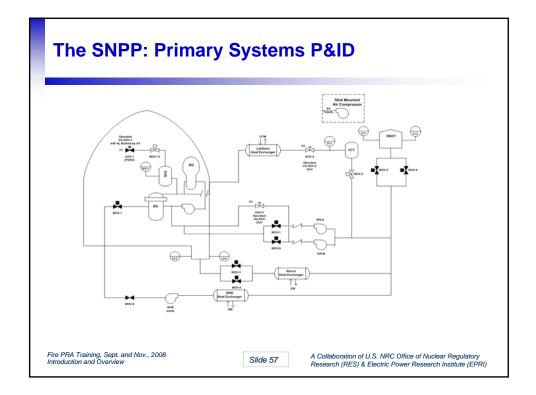


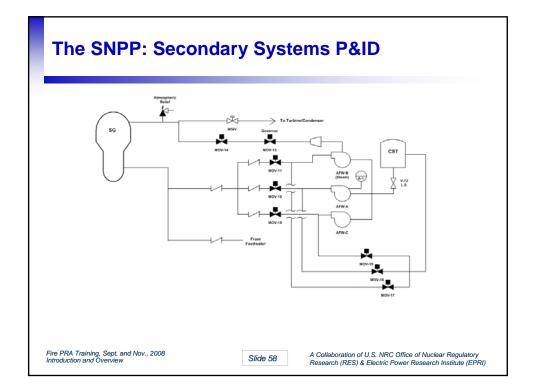


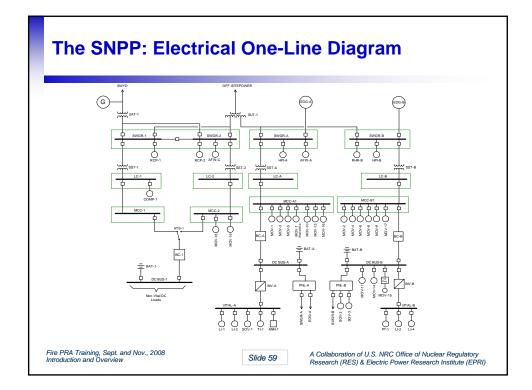


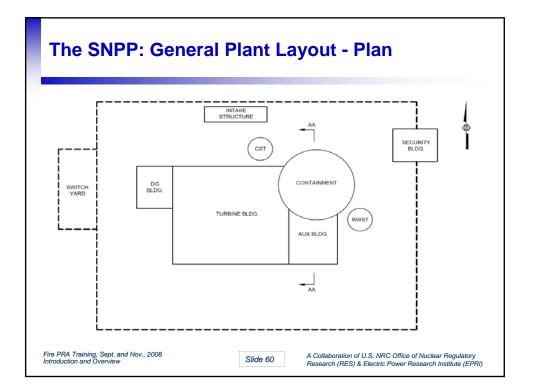


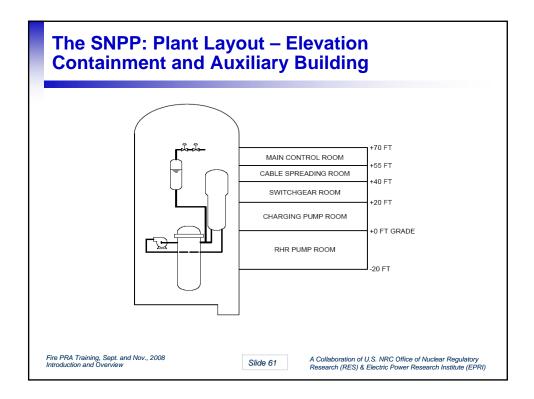


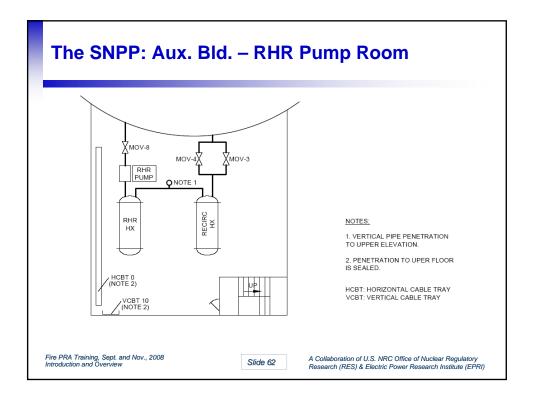


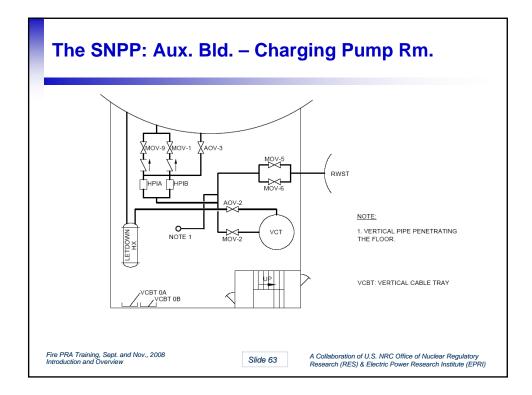


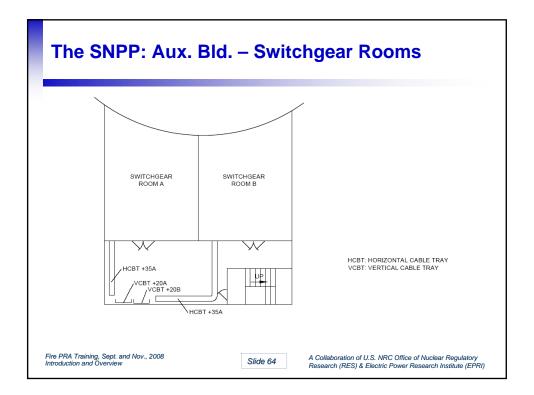


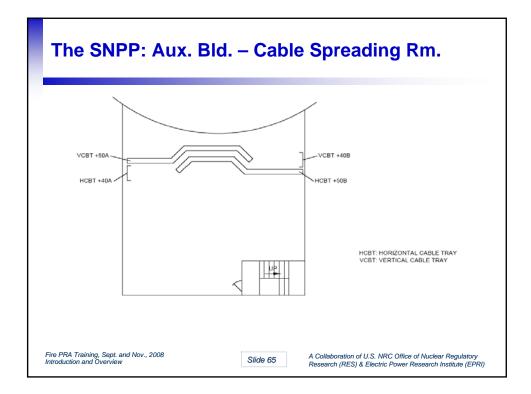


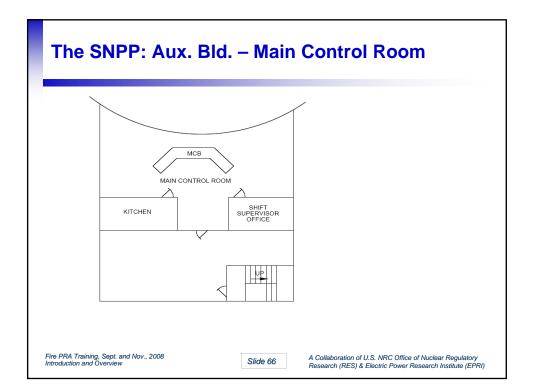


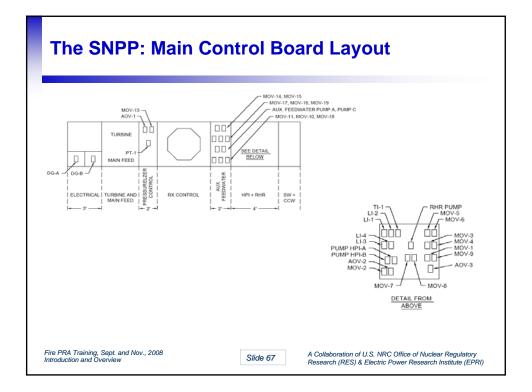


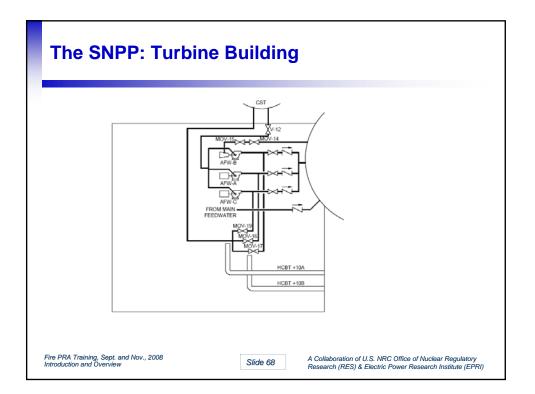


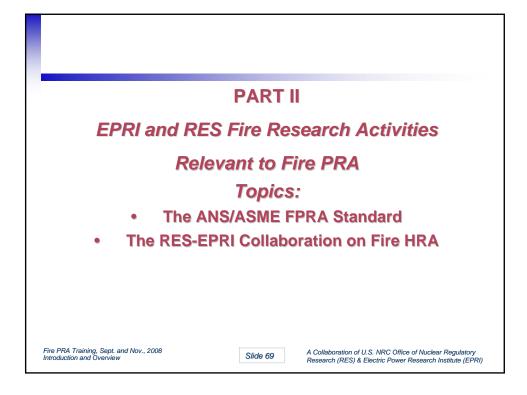


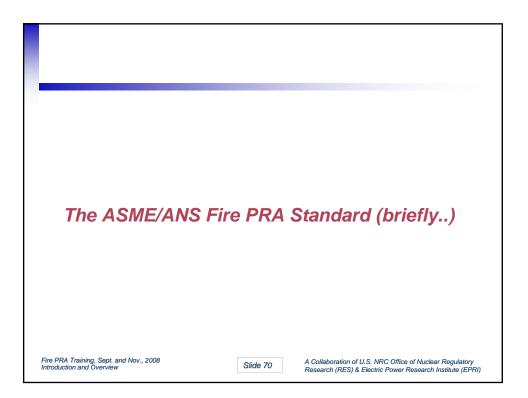


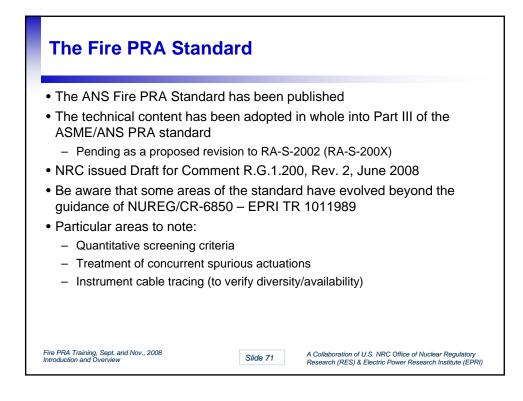




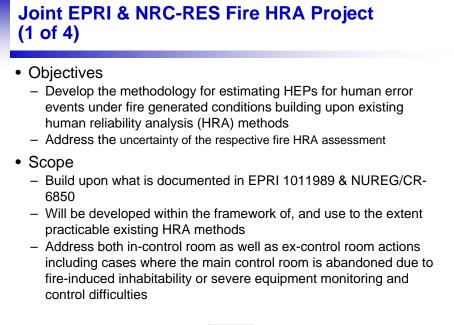












Fire PRA Training, Sept. and Nov., 2008 Introduction and Overview

Slide 73

A Collaboration of U.S. NRC Office of Nuclear Regulatory Research (RES) & Electric Power Research Institute (EPRI)

Joint EPRI & NRC-RES Fire HRA Project (2 of 4)

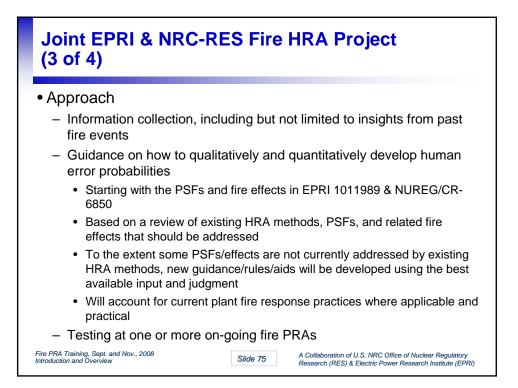
Post-fire human actions covered in the scope of this project are:

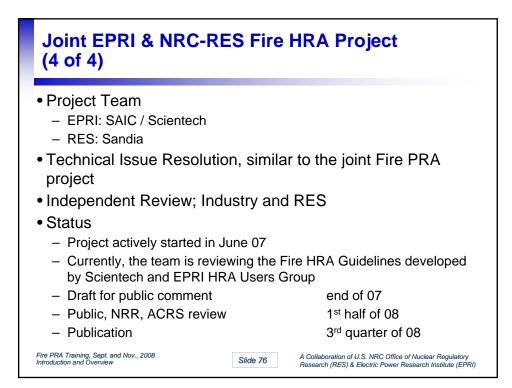
- · Mitigating challenges to plant safety systems, i.e., safe shutdown manual actions
 - Human failure events from the internal events PRA
 - Post-fire operator manual actions
 - Spurious actuation events
- Manual activation of fixed suppression systems
- Fire fighting actions are excluded from the scope of this project. Treated using operating experience [Ref. 1, EPRI 1011989 & NUREG/CR-6850]
- Pre-fire/initiator human events are excluded
- Focus on two cognitive/execution methods. Lessons learned can then be applied to other HRA methods on an as-needed basis
 - CBDT/THERP
 - ATHEANA
- Limited to at-power mode of operation

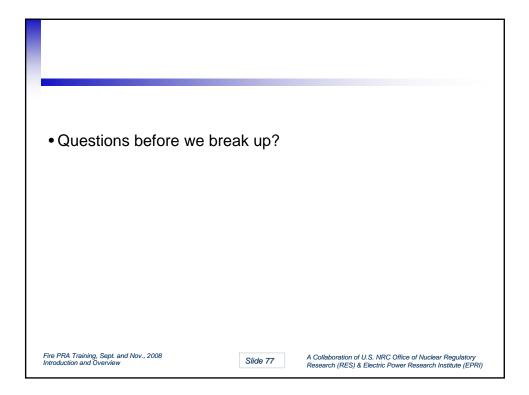
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Fire PRA Training, Sept. and Nov., 2008
Introduction and Overview
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Slide 74

A Collaboration of U.S. NRC Office of Nuclear Regulatory Research (RES) & Electric Power Research Institute (EPRI)







Tab 1.4:

Course Overview Document and the Sample Plant

EPRI/NRC-RES Fire PRA Course

September 28 – October 2, 2008 and November 17-20, 2008

Bethesda, MD

Electric Power Research Institute (EPRI)Fire Research Branch3412 Hillview AvenueOffice of Nuclear Regulatory Research (RES)Palo Alto, CA 94303U.S. Nuclear Regulatory Commission
Two White Flint North, 11545 Rockville Pike

Rockville, MD 20852-2738

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PROJECT MANAGERS

R.P. Kassawara

EPRI Project Manager

J.S. Hyslop

U.S. NRC-RES Project Manager

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5 MOD	ULE 3: FIRE ANALYSIS	1

LIST OF ACRONYMS

ACB	Air-cooled Circuit Breaker
ACRS	Advisory Committee on Reactor Safeguards
AEP	Abnormal Event Procedure
AFW	Auxiliary Feedwater
AGS	Assistance General Supervisor
AOP	Abnormal Operating Procedure
ATWS	Anticipated Transient Without Scram
BNL	Brookhaven National Laboratory
BWR	Boiling Water Reactor
CCDP	Conditional Core Damage Probability
CF	Cable (Configuration) Factors
CCPS	Center for Chemical Process Safety
CCW	Component Cooling Water
CDF	Core Damage Frequency
CFD	Computational Fluid Dynamics
CFR	Code of Federal Regulations
CLERP	Conditional Large Early Release Probability
СМ	Corrective Maintenance
CR	Control Room
CRS	Cable and Raceway (Database) System
CVCS	Chemical and Volume Control System
CWP	Circulating Water Pump
EDG	Emergency Diesel Generator
EF	Error Factor
EI	Erroneous Status Indicator
EOP	Emergency Operating Procedure
EPR	Ethylene-Propylene Rubber
EPRI	Electric Power Research Institute
FEDB	Fire Events Database
FEP	Fire Emergency Procedure
FHA	Fire Hazards Analysis
FIVE	Fire-Induced Vulnerability Evaluation (EPRI TR 100370)
FMRC	Factory Mutual Research Corporation
FPRAIG	Fire PRA Implementation Guide (EPRI TR 105928)
FRSS	Fire Risk Scoping Study (NUREG/CR-5088)
FSAR	Final Safety Analysis Report
HEAF	High Energy Arcing Fault
111.77 31	Ingh Energy / nemg i aan

HEP	Human Error Probability
HFE	Human Failure Event
HPI	High Pressure Injection
HPCI	High Pressure Coolant Injection
HRA	Human Reliability Analysis
HRR	Heat Release Rate
HTGR	High Temperature Gas-cooled Reactor
HVAC	Heating, Ventilation, and Air Conditioning
ICDP	Incremental Core Damage Probability
ILERP	Incremental Large Early Release Probability
INPO	Institute for Nuclear Power Operations
IPE	Individual Plant Examination
IPEEE	Individual Plant Examination of External Events
IS	Ignition Source
ISLOCA	-
	Interfacing Systems Loss of Coolant Accident
KS	Key Switch
LCO	Limiting Condition of Operation
LERF	Large Early Release Frequency
LFL	Lower Flammability Limit
LOC	Loss of Control
LOCA	Loss of Coolant Accident
LPG	Liquefied Petroleum Gas
LWGR	Light-Water-cooled Graphite Reactors (Russian design)
MCC	Motor Control Center
MCR	Main Control Room
MG	Motor-Generator
MFW	Main Feedwater
MOV	Motor Operated Valve
MQH	McCaffrey, Quintiere and Harkleroad's Method
MS	Main Steam
NC	No Consequence
NEI	Nuclear Energy Institute
NEIL	Nuclear Electric Insurance Limited
NFPA	National Fire Protection Association
NPP	Nuclear Power Plant
NPSH	Net Positive Suction Head
NQ cable	Non-Qualified (IEEE-383) cable
NRC	Nuclear Regulatory Commission
P&ID	Piping and Instrumentation Diagram
PE	Polyethylene
PM	Preventive Maintenance
PMMA	Polymethyl Methacrylate
PORV	Power Operated Relief Valve
PRA	Probabilistic Risk Assessment
PSF	Performance Shaping Factor
PTS	Pressurized Thermal Shock

PVC	Polyvinyl Chloride
PWR	Pressurized Water Reactor
Q cable	Qualified (IEEE-383) cable
RBMK	Reactor Bolshoy Moshchnosty Kanalny (high-power channel reactor)
RCIC	Reactor Core Isolation Cooling
RCP	Reactor Coolant Pump
RCS	Reactor Coolant System
RDAT	Computer program for Bayesian analysis
RES	The Office of Nuclear Regulatory Research (at NRC)
RHR	Residual Heat Removal
RI/PB	Risk-Informed / Performance-Based
RPS	Reactor Protection System
RWST	Refueling Water Storage Tank
SCBA	Self-Contained Breathing Apparatus
SDP	Significance Determination Process
SGTR	Steam Generator Tube Rupture
SI	Safety Injection
SMA	Seismic Margin Assessment
SO	Spurious Operation
SOV	Solenoid Operated Valve
SRV	Safety Relief Valve
SSD	Safe Shutdown
SSEL	Safe Shutdown Equipment List
SUT	Start-up Transformer
T/G	Turbine/Generator
TGB	Turbine-Generator Building
TSP	Transfer Switch Panel
UAT	Unit Auxiliary Transformer
VCT	Volume Control Tank
VTT	Valtion Teknillinen Tutkimuskeskus (Technical Research Centre of Finland)
VVER	The Soviet (and now, Russian Federation) designation for light water
	pressurized reactor
XLPE	Cross-Linked Polyethylene
ZOI	Zone of Influence

1 INTRODUCTION

1.1 Background

The U.S. Nuclear Regulatory Commission and Electric Power Research Institute under a Memorandum of Understanding (MOU) on Cooperative Nuclear Safety Research have been developing state of the art methods for conduct of fire PRA. In September 2005, this work produced the "EPRI/NRC RES Fire PRA Methodology for Nuclear Power Facilities," EPRI 1011989, and NUREG/CR 6850.

A Fire PRA Course has been put together to train interested parties in the application of this methodology. The Course/Seminar is provided in three parallel parts:

• Module 1: PRA/HRA - This module covers the technical tasks for development of the system and operator response to a fire. Specifically, this module covers EPRI 1011989, NUREG/CR-6850, Volume 2, Sections 2, 4, 5, 7, 12, 14, and 15.

- Module 2: Electrical Analysis This module covers the technical tasks for analysis of electrical failures as the result of a fire. Specifically, this module covers EPRI 1011989, NUREG/CR-6850, Volume 2, Sections 3, 9, and 10.
- Module 3: Fire Analysis This module covers technical tasks involved in development of fire scenarios from initiation to target (e.g., cable) impact. Specifically, this module covers EPRI 1011989, NUREG/CR-6850, Volume 2, sections 1, 6, 8, 11, and 13.

Integral to the Course is a set of hands-on problems based on a fictitious, simplified nuclear power plant. The same power plant is used in all three modules. This document provides the background information for the problem sets of each module. Clearly, the power plant defined in this package is an extremely simplified one that in many cases does not meet any regulatory requirements or good engineering practices. Design features presented are focused on bringing forward the various aspects of the Fire PRA methodology.

This package includes a general description of the power plant and the internal events PRA needed as input to the Fire PRA. The instruction package for specific technical tasks is provided in Sections 3, 4 and 5 which are organized by Modules (see above). A short description of the Fire PRA technical tasks is provided below. For further details, refer to the individual task descriptions in EPRI 1011989, NUREG/CR-6850, Volume 2.

• *Plant Boundary Definition and Partitioning (Task 1).* The first step in a Fire PRA is to define the physical boundary of the analysis, and to divide the area within that boundary into analysis compartments.

• *Fire PRA Component Selection (Task 2).* The selection of components that are to be credited for plant shutdown following a fire is a critical step in any Fire PRA. Components selected would generally include many, but not necessarily all components credited in the 10 CFR 50 Appendix R post-fire SSD analysis. Additional components will likely be selected, potentially including most but not all components credited in the plant's internal events PRA. Also, the proposed methodology would likely introduce components beyond either the 10 CFR 50 Appendix R list or the internal events PRA model. Such components are often of interest due to considerations of multiple spurious actuations that may threaten the credited functions and components; as well as due to concerns about fire effects on instrumentation used by the plant crew to respond to the event.

• *Fire PRA Cable Selection (Task 3).* This task provides instructions and technical considerations associated with identifying cables supporting those components selected in Task 2. In previous Fire PRA methods (such as EPRI FIVE and Fire PRA Implementation Guide) this task was relegated to the SSD analysis and its associated databases. This document offers a more structured set of rules for selection of cables.

This document offers a more structured set of rules for selection of cables.

• *Qualitative Screening (Task 4).* This task identifies fire analysis compartments that can be shown to have little or no risk significance without quantitative analysis. Fire compartments may be screened out if they contain no components or cables identified in Tasks 2 and 3, and if they cannot lead to a plant trip due to either plant procedures, an automatic trip signal, or technical specification requirements.

• *Plant Fire-Induced Risk Model (Task 5).* This task discusses steps for the development of a logic model that reflects plant response following a fire. Specific instructions have been provided for treatment of fire-specific procedures or preplans. These procedures may impact availability of functions and components, or include fire-specific operator actions (e.g., self-induced-station-blackout).

• *Fire Ignition Frequency (Task 6).* This task describes the approach to develop frequency estimates for fire compartments and scenarios. Significant changes from the EPRI FIVE method have been made in this task. The changes generally relate to use of challenging events, considerations associated with data quality, and increased use of a fully component-based ignition frequency model (as opposed to the location/component-based model used, for example, in FIVE).

• *Quantitative Screening (Task 7).* A Fire PRA allows the screening of fire compartments and scenarios based on their contribution to fire risk. This approach considers the cumulative risk associated with the screened compartments (i.e., the ones not retained for detailed analysis) to ensure that a true estimate of fire risk profile (as opposed to vulnerability) is obtained.

• *Scoping Fire Modeling (Task 8).* This step provides simple rules to define and screen fire ignition sources (and therefore fire scenarios) in an unscreened fire compartment.

• *Detailed Circuit Failure Analysis (Task 9).* This task provides an approach and technical considerations for identifying how the failure of specific cables will impact the components included in the Fire PRA SSD plant response model.

• *Circuit Failure Mode Likelihood Analysis (Task 10).* This task considers the relative likelihood of various circuit failure modes. This added level of resolution may be a desired

option for those fire scenarios that are significant contributors to the risk. The methodology provided in this document benefits from the knowledge gained from the tests performed in response to the circuit failure issue.

• **Detailed Fire Modeling (Task 11).** This task describes the method to examine the consequences of a fire. This includes consideration of scenarios involving single compartments, multiple fire compartments, and the main control room. Factors considered include initial fire characteristics, fire growth in a fire compartment or across fire compartments, detection and suppression, electrical raceway fire barrier systems, and damage from heat and smoke. Special consideration is given to turbine generator (T/G) fires, hydrogen fires, high-energy arcing faults, cable fires, and main control board (MCB) fires. There are considerable improvements in the method for this task over the EPRI FIVE and Fire PRA Implementation Guide in nearly all technical areas.

• *Post-Fire Human Reliability Analysis (Task 12).* This task considers operator actions for manipulation of plant components. The analysis task procedure provides structured instructions for identification and inclusion of these actions in the Fire PRA. The procedure also provides instructions for estimating screening human error probabilities (HEPs) before detailed fire modeling results (e.g., fire growth and damage behaviors) or detailed circuit analyses (e.g., can the circuit spuriously actuate as opposed to simply assuming it can) have necessarily been developed. Estimating HEP values with high confidence is critical to the effectiveness of screening in a Fire PRA. This report does not develop a detailed fire HRA methodology. There are a number of HRA methods that can be adopted for fire with appropriate additional instructions that superimpose fire effects on any of the existing HRA methods, such as THERP, CBDT, ATHEANA, etc. This would improve consistency across analyses i.e., fire and internal events PRA.

• *Seismic Fire Interactions (Task 13).* This task is a qualitative approach to help identify the risk from any potential interactions between an earthquake and fire.

• *Fire Risk Quantification (Task 14).* The task summarizes what is to be done for quantification of the fire risk results.

• Uncertainty and Sensitivity Analyses (Task 15). This task describes the approach to follow for identifying and treating uncertainties throughout the Fire PRA process. The treatment may vary from quantitative estimation and propagation of uncertainties where possible (e.g., in fire frequency and non-suppression probability) to identification of sources without quantitative estimation. The treatment may also include one-at-a-time variation of individual parameter values or modeling approaches to determine the effect on the overall fire risk (sensitivity analysis).

1.2 How to Use this Package

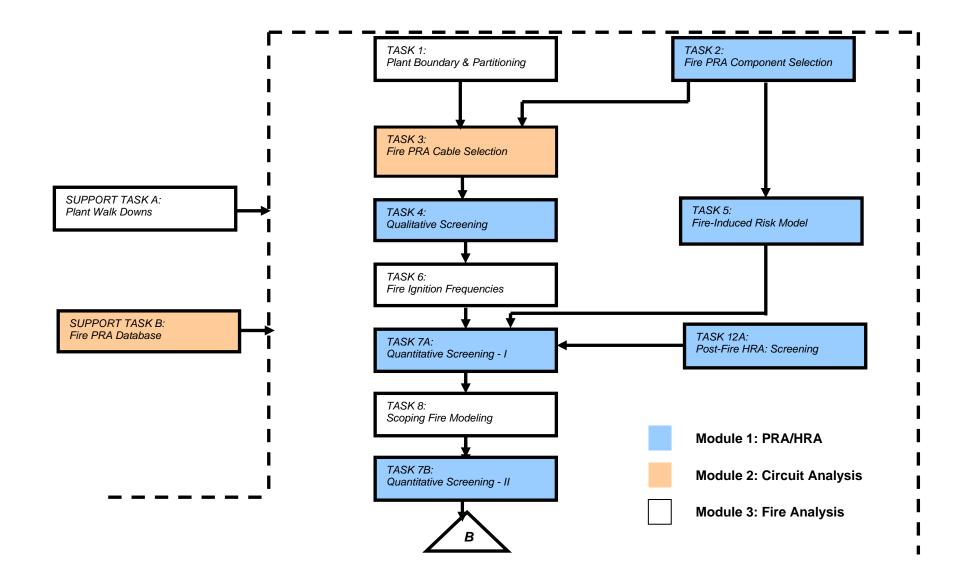
This package is intended to provide the background information necessary to perform some of the problem sets of the Course/Seminar. Please note:

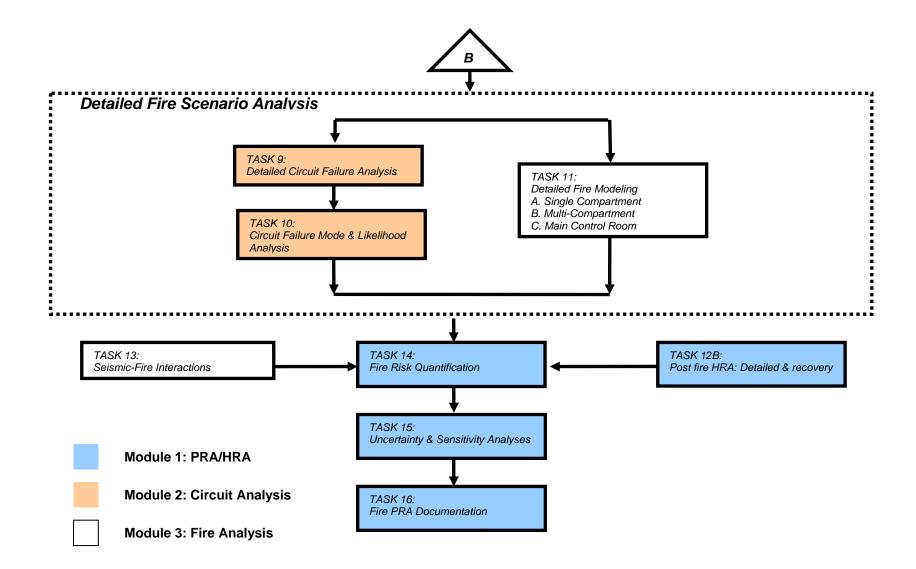
1. All Course/Seminar attendees are expected to review Section 2 of this document and become familiar with the power plant defined in that section.

- 2. The instructors of each module will provide questions or case study problem sets and will guide the attendees to sections relevant to each specific problem set. Attendees will be expected to review those relevant sections and use the information or examples provided in those sections to complete the assigned problem set.
- 3. Do not make any additional assumptions in terms of equipment, systems, or plant layout other than those presented in the problem package without consulting the instructor.

1.3 References

1. EPRI 1011989, NUREG/CR-6850, "EPRI/NRC-RES Fire PRA Methodology for Nuclear Power Facilities," September 2005.





2 GENERAL PLANT INFORMATION

2.1 Overall Plant Description

The following notes generally describe the plant, including its layout:

- 1. The plant is a Pressurized Water Reactor (PWR) consisting of one primary coolant loop, which consists of one steam generator, one reactor coolant pump and the pressurizer. A chemical volume control system and multiple train injection system, as well as a single train residual heat removal system interface with the primary system
- 2. The secondary side of the plant contains a main steam and feedwater loop associated with the single steam generator, and a multiple train auxiliary feedwater system to provide decay heat removal.
- 3. The operating conditions and parameters of this plant are similar to that of a typical PWR. For example, the primary side runs at about 2,200 psi pressure. The steam generator can reject the decay heat after a reactor trip. There is a possibility of feed and bleed, etc.
- 4. It is assumed that the reactor is initially at 100% power.
- 5. The plant is laid out in accordance with Figures 1 through 9. The plant consists of a Containment Building, Auxiliary Building, Turbine Building, Diesel Generator Building and the Yard. All other buildings and plant areas are shown but no details are provided.

2.2 Systems Description

This section provides a more detailed description of the various systems within the plant and addressed in the case studies. Each system is described separately.

2.2.1 Primary Coolant System

The following notes and Figure 10 define the Primary Coolant System:

- 1. The Primary Coolant Loop consists of the Reactor Vessel, one Reactor Coolant Pump, and one Steam Generator and the Pressurizer, along with associated piping.
- 2. The Pressurizer is equipped with a normally closed Power Operated Relief Valve (PORV), which is an air operated valve (AOV-1) with its pilot solenoid operated valve (SOV-1). There is also a normally open motor operated block valve (MOV-13) upstream of the PORV.

- 3. The Pressure Transmitter (PT-1) on the pressurizer provides the pressure reading for the Primary Coolant Loop and is used to signal a switch from Chemical and Volume Control System (CVCS) to High Pressure Injection (HPI) configuration.
- 4. A nitrogen bottle provides the necessary pressurized gas to operate the PORV in case of loss of plant air.

2.2.2 Chemical Volume Control and High Pressure Injection Systems

The following notes and Figure 10 define the shared Chemical and Volume Control System (CVCS) and High Pressure Injection (HPI) System:

- 1. The CVCS normally operates during power generation.
- 2. Valve type and position information include:

Valve	Туре	Status on Loss of Power (or Air as applicable)	Position During Normal Operation
AOV-2	Air Operated Valve	Fail Closed	Open
AOV-3	Air Operated Valve	Fail Closed	Open
MOV-1	Motor Operated Valve	Fail As Is	Closed
MOV-2	Motor Operated Valve	Fail As Is	Open
MOV-3	Motor Operated Valve	Fail As Is	Closed
MOV-4	Motor Operated Valve	Fail As Is	Closed
MOV-9	Motor Operated Valve	Fail As Is	Closed

- 3. One of the two HPI pumps runs when the CVCS is operating.
- 4. One of the two HPI pumps is sufficient to provide all injection needs after a reactor trip and all postulated accident conditions.
- 5. HPI and CVCS use the same set of pumps.
- 6. On a need for safety injection, the following lineup takes place automatically:
 - AOV-2 and AOV-3 close
 - MOV-5 and MOV-6 open
 - MOV-2 closes.
 - Both HPI pumps receive start signal, the stand-by pump starts and the operating pump continues operating.

- MOV-1 and MOV-9 open.
- 7. The HPI is used for re-circulating sump water after a LOCA using the pathway involving MOV-3 and MOV-4. For recirculation, the operator manually opens MOV-3 and MOV-4 and closes MOV-5 and MOV-6 upon proper indication of low RWST level and sufficient sump level.
- 8. RWST provides the necessary cooling water for the HPI pumps. It has enough capacity to depressurize the primary loop for RHR cooling.
- 9. There are level indications of the RWST and containment sump levels that are used by the operator to know when to switch from high pressure injection to recirculation cooling mode.
- 10. The Air Compressor provides the motive power for operating the Air Operated Valves but the detailed connections to the various valves are not shown (nor needed for exercises).

2.2.4 Residual Heat Removal System

The following notes and Figure 10 define the Residual Heat Removal (RHR) System:

- 1. The design pressure of the RHR system downstream of MOV-8 is low.
- 2. Valve type and position information include:

Valve	Туре	Status on Loss of Power	Position During Normal Operation
MOV-7	Motor Operated Valve	Fail As Is	Closed
MOV-8	Motor Operated Valve	Fail As Is	Closed

3. Operators have to align the system for low pressure cooling, after reactor vessel depressurization from the control room by opening MOV-7 and MOV-8, turn the RHR pump on and establish cooling in the RHR Heat Exchanger.

2.2.5 Auxiliary Feedwater System

The following notes and Figure 11 define the Auxiliary Feedwater (AFW) System:

- 1. One of three pumps of the AFW system can provide the necessary secondary side cooling for reactor heat removal after a reactor trip.
- 2. Pump AFW-B is steam turbine driven
- 3. Valve type and position information include:

General Plant Information

Valve	Туре	Status on Loss of Power	Position During Normal Operation
MOV-10	Motor Operated Valve	Fail As Is	Closed
MOV-11	Motor Operated Valve	Fail As Is	Closed
MOV-14	Motor Operated Valve	Fail As Is	Closed
MOV-15	Motor Operated Valve	Fail As Is	Closed
MOV-16	Motor Operated Valve	Fail As Is	Closed
MOV-17	Motor Operated Valve	Fail As Is	Closed
MOV-18	Motor Operated Valve	Fail As Is	Closed
MOV-19	Motor Operated Valve	Fail As Is	Closed

- 4. Upon a plant trip, Main Feedwater isolates and AFW automatically initiates by starting AFW-A and AFW-C pumps, opening the steam valves MOV-14 and MOV-15 to operate the AFW-B steam-driven pump, and opening valves MOV-10, MOV-11, and MOV-18.
- 5. The CST has sufficient capacity to provide core cooling until cold shutdown is achieved.
- 6. The test return paths through MOVs-16, 17, and 19 are low flow lines and do not represent significant diversions of AFW flow even if the valves are open.
- 7. There is a high motor temperature alarm on AFW pump A. Upon indication in the control room, the operator is to stop the pump immediately and have the condition subsequently checked by dispatching a local operator.
- 8. The atmospheric relief valve opens, as needed, automatically to remove decay heat if/should the main condenser path be unavailable.
- 9. The connections to the Main Turbine and Main Feedwater are shown in terms of one Main Steam Isolation Valve (MSIV) and a check valve. Portions of the plant beyond these interfacing components will not be addressed in the course.

2.2.6 Electrical System

Figure 12 is a one-line diagram of the electrical distribution system (EDS). Safety related buses are identified by the use of alphabetic letters (e.g., SWGR-A, MCC-B1, etc.) while the non-safety buses use numbers as part of their designations (e.g., SWGR-1 and MCC-2).

The safety-related portions of the EDS include 4160 volt switchgear buses SWGR-A and SWGR-B, which are normally powered from the startup transformer SUT-1. In the event that off-site power is lost, these switchgear receive power from emergency diesel generators EDG-A and EDG-B. The 480 volt safety-related load centers (LC-A and LC-B) receive power from the switchgear buses via station service transformers SST-A and SST-B. The motor control centers (MCC-A1 and MCC-B1) are powered directly from the load centers. The MCCs provide motive power to several safety-related motor operated valves (MOVs) and to DC buses DC BUS-A and DC BUS-B via Battery Chargers BC-A and BC-B. The two 125 VDC batteries, BAT-A and BAT-B, supply power to the DC buses in the event that all AC power is lost. DC control power for the 4160 safety-related switchgear is provided through distribution panels PNL-A and PNL-B. The 120 VAC vital loads are powered from buses VITAL-A and VITAL-B, which in turn receive their power from the DC buses through inverters INV-A and INV-B.

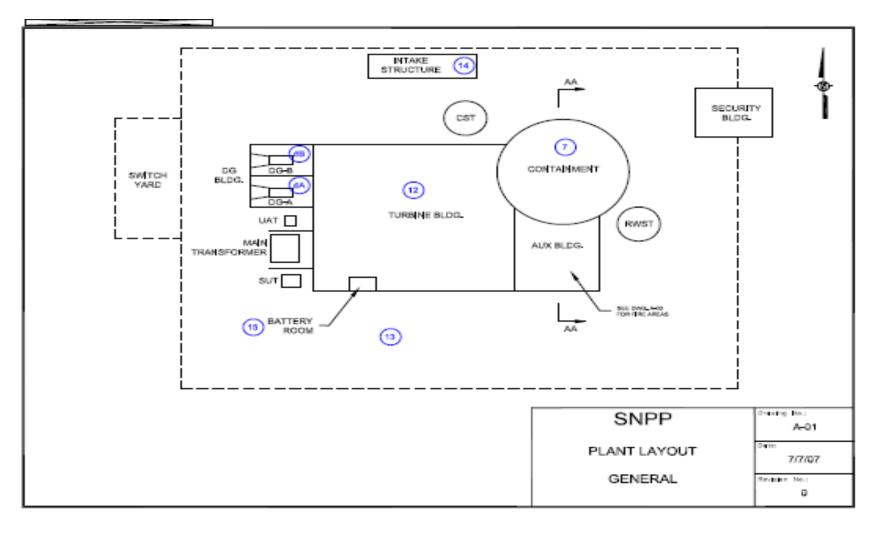
The non-safety portions of the EDS reflect a similar hierarchy of power flow. There are important differences however. For example, 4160 volt SWGR-1 and SWGR-2 are normally energized from the unit auxiliary transformer (UAT-1) with backup power available from SUT-1. A cross-tie breaker allows one non-safety switchgear bus to provide power to the other. Non-safety load centers LC-1 and LC-2 are powered at 480 volts from the 4160 volt switchgear via SST-1 and SST-2. These load centers provide power directly to the non-safety MCCs. The non-vital DC bus (DC BUS-1) can be powered from either MCC via an automatic transfer switch (ATS-1) and battery charger BC-1 or directly from the 250 volt DC battery, BAT-1.

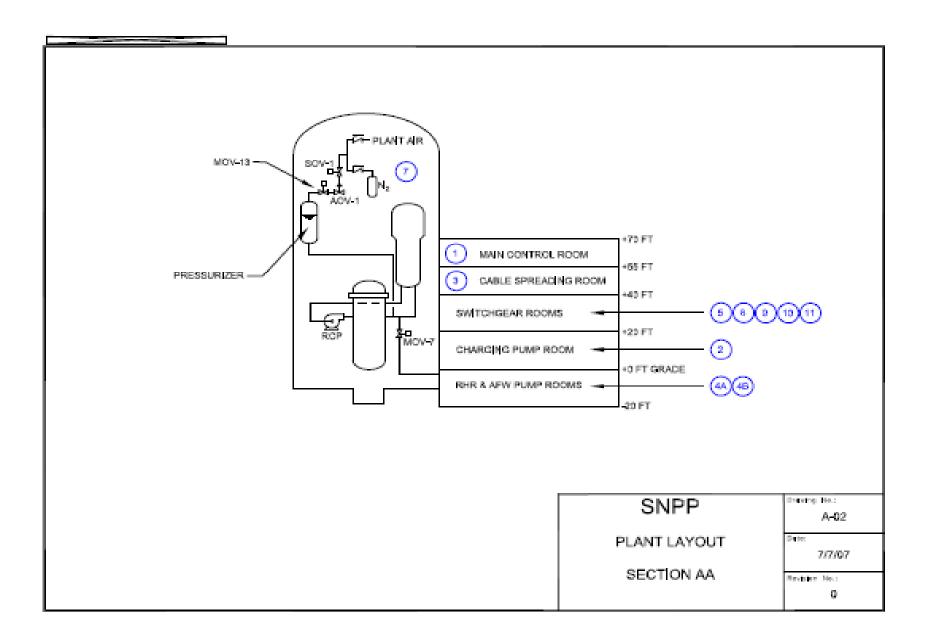
2.2.7 Other Systems

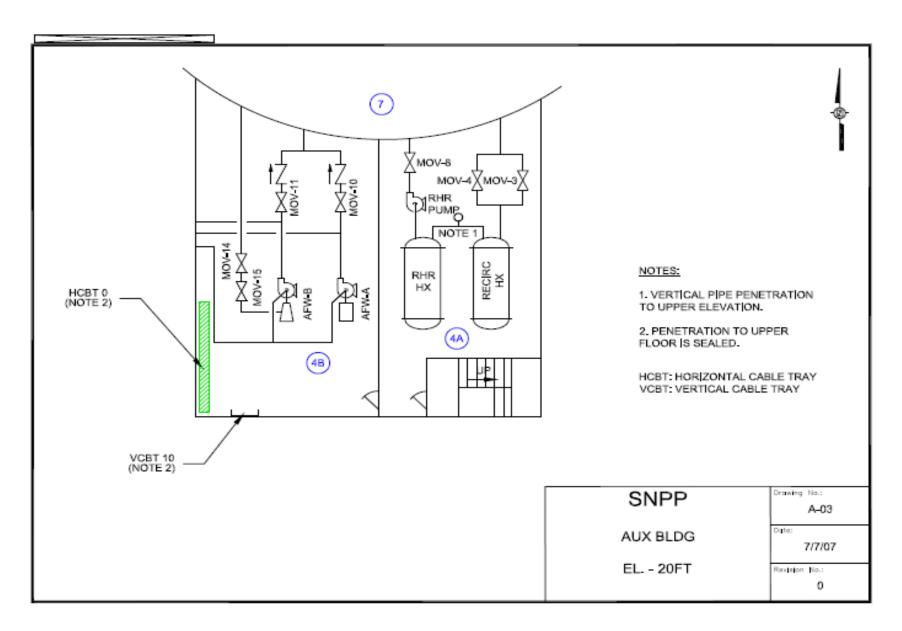
The following systems and equipment are mentioned in the plant description but not explicitly included in the fire PRA:

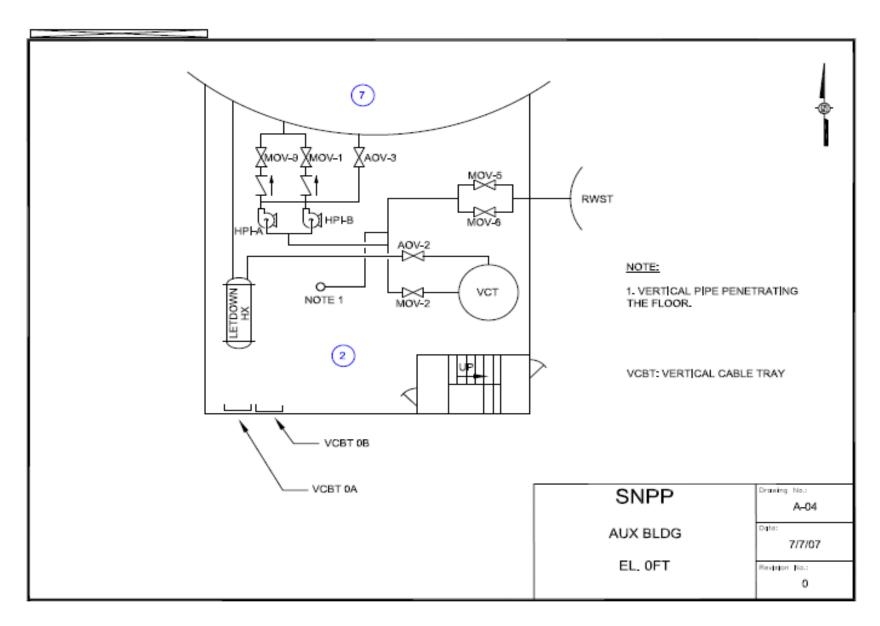
- Service Water (SW) –provides cooling to Re-circulating and Residual Heat Removal Heat Exchangers assumed to be available at all times
- Component Cooling Water (CCW) provides cooling to Letdown Heat Exchanger assumed to be available at all times.
- It is assumed that the control rods can successfully insert and shutdown the reactor under all conditions.
- It is assumed that the ECCS and other AFW related instrumentation and control circuits (other than those specifically noted in the diagrams) exist and are perfect such that in all cases, they would sense the presence of a Loss of Coolant Accident (LOCA) or otherwise a need to trip the plant and provide safety injection and auxiliary feedwater by sending the proper signals to the affected components (i.e., close valves and start pumps, insert control rods, etc.).

Figures 1 – 9 SNPP General Layout

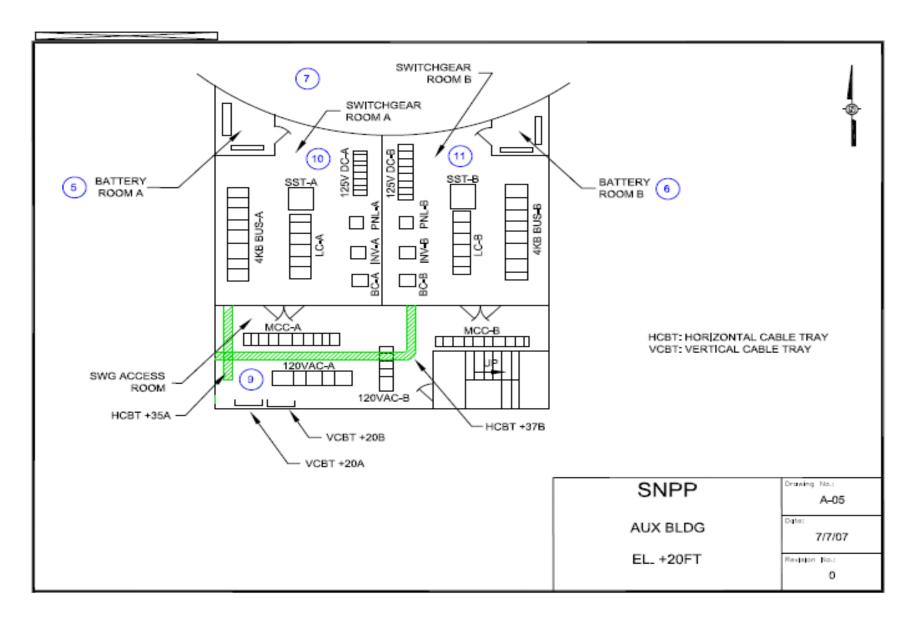




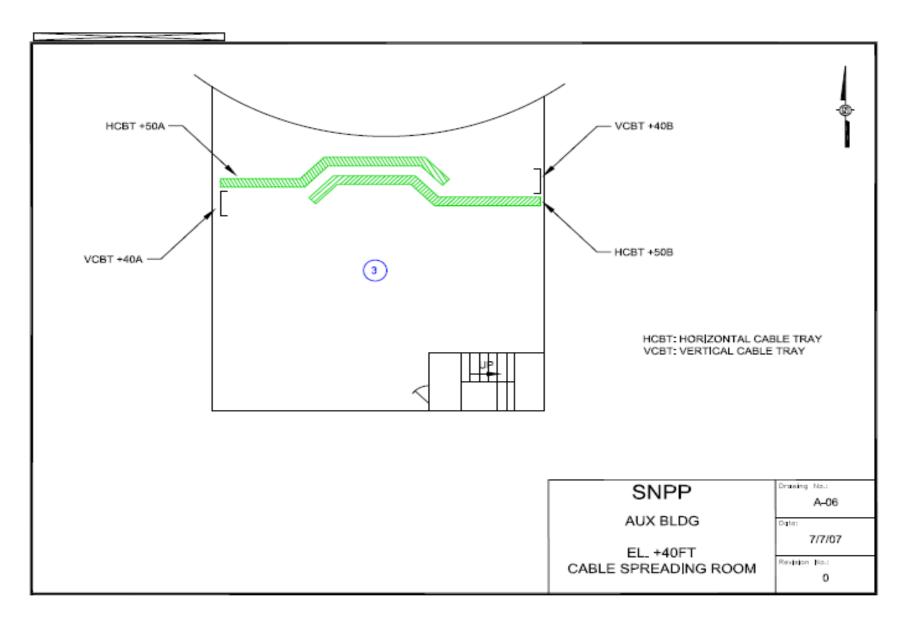




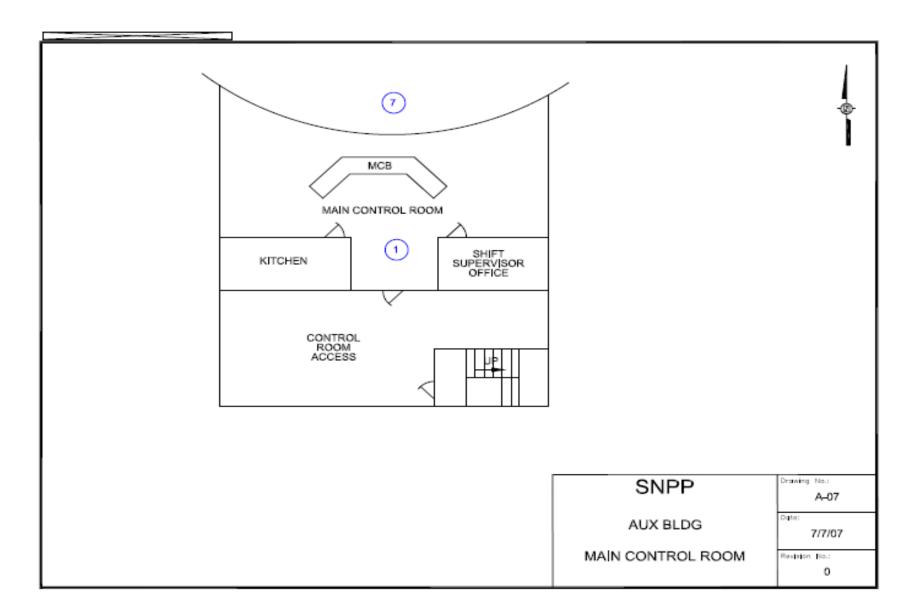
General Plant Information

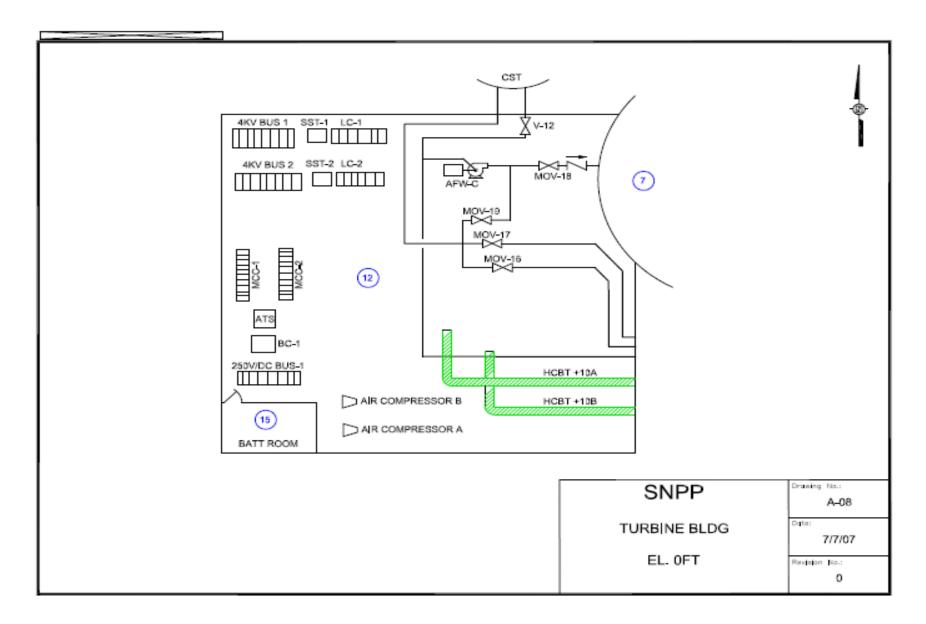


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General Plant Information





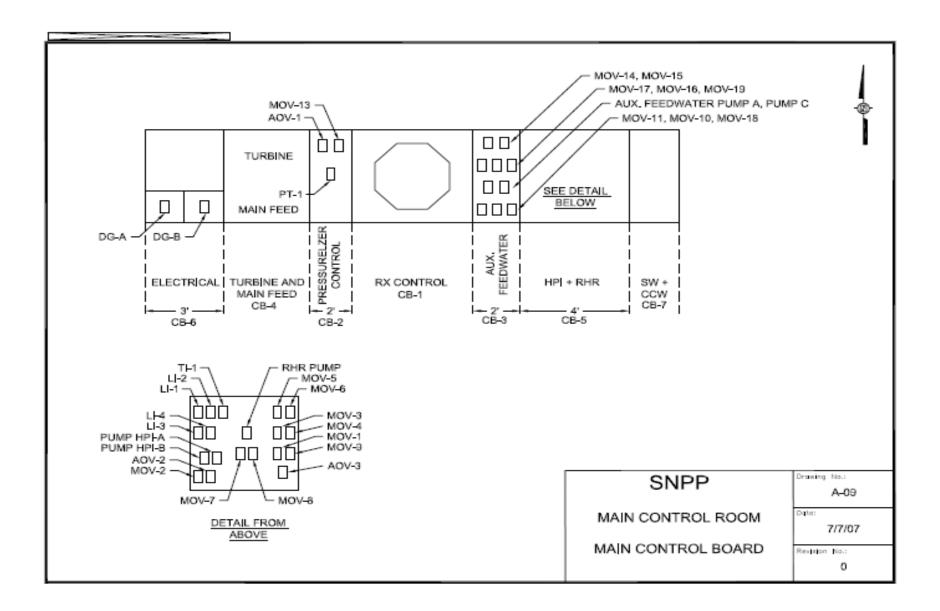
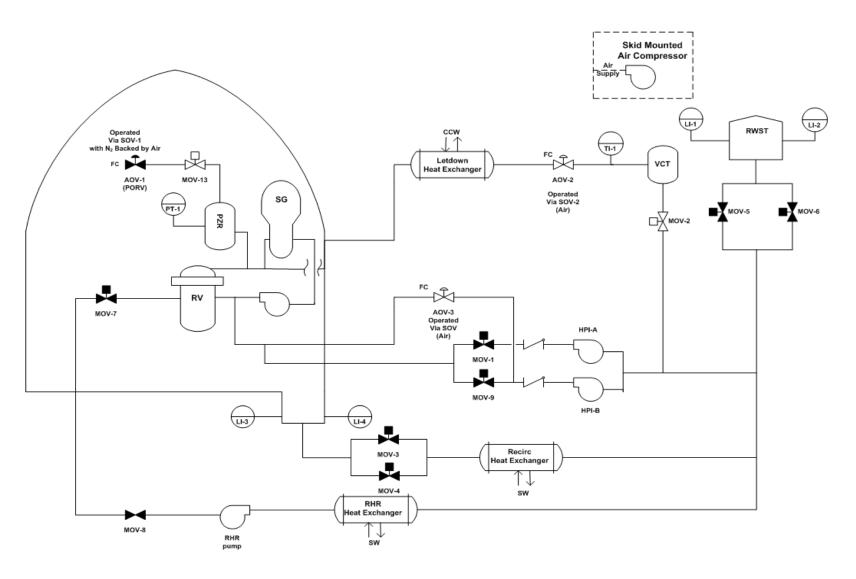


Figure 10 PRIMARY SYSTEM P & ID



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Figure 11 SECONDARY SYSTEM P & ID

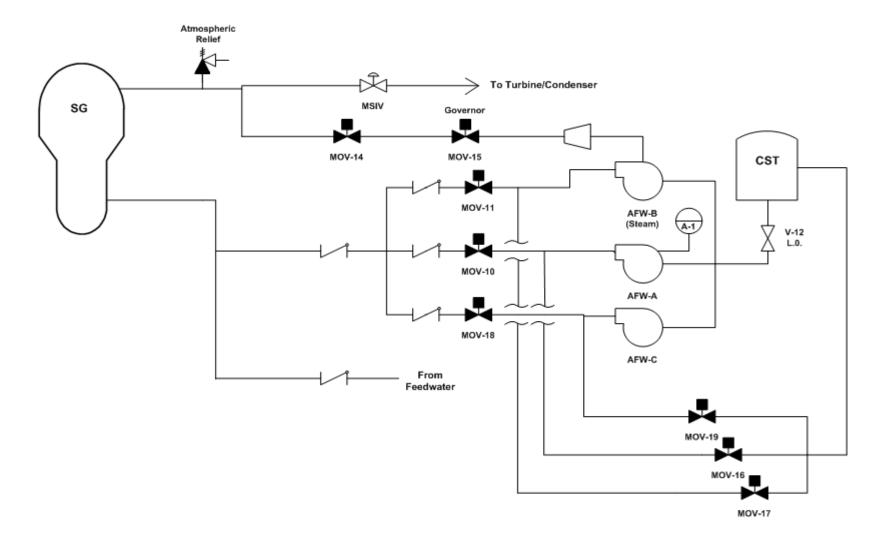
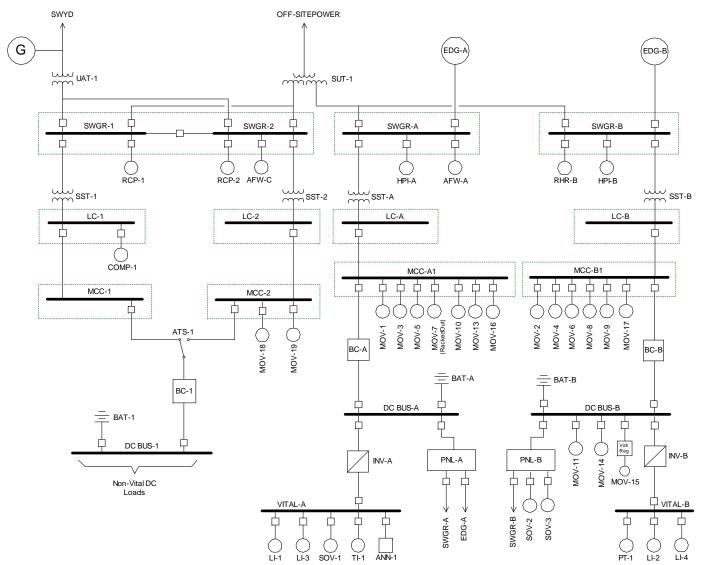


Figure 12 ELECTRICAL DISTRIBUTION SYSTEM - SIMPLIFIED ONE-LINE DIAGRAM



3 MODULE 1: PRA/HRA

The following is a short description of the Fire PRA technical tasks covered in this module. For further details, refer to the individual task descriptions in Volume 2 of EPRI 1011989, NUREG/CR-6850.

• *Fire PRA Component Selection (Task 2).* The selection of components that are to be credited for plant shutdown following a fire is a critical step in any Fire PRA. Components selected would generally include many components credited in the 10 CFR 50 Appendix R post-fire SSD analysis. Additional components will likely be selected, potentially including any and all components credited in the plant's internal events PRA. Also, the proposed methodology would likely introduce components beyond either the 10 CFR 50 Appendix R list or the internal events PRA model. Such components are often of interest due to considerations of multiple spurious actuations that may threaten the credited functions and components.

• *Qualitative Screening (Task 4).* This task identifies fire analysis compartments that can be shown to have little or no risk significance without quantitative analysis. Fire compartments may be screened out if they contain no components or cables identified in Tasks 2 and 3, and if they cannot lead to a plant trip due to either plant procedures, an automatic trip signal, or technical specification requirements.

• *Plant Fire-Induced Risk Model (Task 5).* This task discusses steps for the development of a logic model that reflects plant response following a fire. Specific instructions have been provided for treatment of fire-specific procedures or preplans. These procedures may impact availability of functions and components, or include fire-specific operator actions (e.g., self-induced-station-blackout).

• *Quantitative Screening (Task 7).* A Fire PRA allows the screening of fire compartments and scenarios based on their contribution to fire risk. This approach considers the cumulative risk associated with the screened compartments (i.e., the ones not retained for detailed analysis) to ensure that a true estimate of fire risk profile (as opposed to vulnerability) is obtained.

• **Post-Fire Human Reliability Analysis (Task 12).** This task considers operator actions for manipulation of plant components. The analysis task procedure provides structured instructions for identification and inclusion of these actions in the Fire PRA. The procedure also provides instructions for estimating screening human error probabilities (HEPs) before detailed fire modeling results (e.g., fire growth and damage behaviors) have been developed. Estimating HEP values with high confidence is critical to the effectiveness of screening in a Fire PRA. This report does not develop a detailed fire HRA methodology. There are a number of HRA methods that can be adopted for fire with appropriate additional instructions that superimpose fire effects on any of the existing HRA methods, such as SHARP, ATHEANA, etc. This would improve consistency across analyses i.e., fire and internal events PRA.

• *Fire Risk Quantification (Task 14).* The task summarizes what is to be done for quantification of the fire risk results.

• Uncertainty and Sensitivity Analyses (Task 15). This task describes the approach to follow for identifying and treating uncertainties throughout the Fire PRA process. The treatment may vary from quantitative estimation and propagation of uncertainties where possible (e.g., in fire frequency and non-suppression probability) to identification of sources without quantitative estimation. The treatment may also include one-at-a-time variation of individual parameter values or modeling approaches to determine the effect on the overall fire risk (sensitivity analysis).

4 MODULE 2: ELECTRICAL ANALYSIS

The following is a short description of the Fire PRA technical tasks covered in this module. For further details, refer to the individual task descriptions in Volume 2 of EPRI 1011989, NUREG/CR-6850.

• *Fire PRA Cable Selection (Task 3).* This task provides instructions and technical considerations associated with identifying cables supporting those components selected in Task 2. In previous Fire PRA methods (such as EPRI FIVE and Fire PRA Implementation Guide) this task was relegated to the SSD analysis and its associated databases. This document offers a more structured set of rules for selection of cables.

• *Detailed Circuit Failure Analysis (Task 9).* This task provides an approach and technical considerations for identifying how the failure of specific cables will impact the components included in the Fire PRA SSD plant response model.

• *Circuit Failure Mode Likelihood Analysis (Task 10).* This task considers the relative likelihood of various circuit failure modes. This added level of resolution may be a desired option for those fire scenarios that are significant contributors to the risk. The methodology provided in this document benefits from the knowledge gained from the tests performed in response to the circuit failure issue.

5 MODULE 3: FIRE ANALYSIS

The following is a short description of the Fire PRA technical tasks covered in this module. For further details, refer to the individual task descriptions in Volume 2 of EPRI 1011989, NUREG/CR-6850.

• *Plant Boundary Definition and Partitioning (Task 1).* The first step in a Fire PRA is to define the physical boundary of the analysis, and to divide the area within that boundary into analysis compartments.

• *Fire Ignition Frequency (Task 6).* This task describes the approach to develop frequency estimates for fire compartments and scenarios. Significant changes from the EPRI FIVE method have been made in this task. The changes generally relate to use of challenging events, considerations associated with data quality, and increased use of a fully component-based ignition frequency model (as opposed to the location/component-based model used, for example, in FIVE).

• *Scoping fire Modeling (Task 8).* Scoping fire modeling is the first task in the Fire PRA framework where fire modeling tolls are used to identify ignition sources that may impact the fire risk of the plant. Screening some of the ignition sources, along with the applications of severity factors to the unscreened ones, may reduce the compartment fire frequency previously calculated in Task 6.

• **Detailed Fire Modeling (Task 11).** This task describes the method to examine the consequences of a fire. This includes consideration of scenarios involving single compartments, multiple fire compartments, and the main control room. Factors considered include initial fire characteristics, fire growth in a fire compartment or across fire compartments, detection and suppression, electrical raceway fire barrier systems), and damage from heat and smoke. Special consideration is given to turbine generator (T/G) fires, hydrogen fires, high-energy arcing faults, cable fires, and main control board (MCB) fires. There are considerable improvements in the method for this task over the EPRI FIVE and Fire PRA Implementation Guide in nearly all technical areas.

• *Seismic Fire Interactions (Task 13).* This task is a qualitative approach to help identify the risk from any potential interactions between an earthquake and fire.