ATTACHMENT 6

Calculation L-003063, "Alternative Source Term Onsite and Offsite X/Q Values," Revision 1



ATTACHMENT 1
Design Analysis Major Revision Cover Sheet

Design Analysis (Major Revision)		**Last Page No.:**	33/Att. R, Page R1
Analysis No.:	L-003063	**Revision:**	1
Title:	Alternative Source Term Onsite and Offsite X/Q Values		
EC/ECR No.:	352505	**Revision:**	0
Station(s):	LaSalle County Station	**Component(s):**	
Unit No.:	1 & 2	N/A	
Discipline:	MECH		
Descrip. Code/Keyword:	R01&R02/ AST, DBA, Dose, X/Q, Dispersion		
Safety/QA Class:	SR		
System Code:	VC, VE, VG, VS		
Structure:	Z		

CONTROLLED DOCUMENT REFERENCES

Document No.:	From/To	Document No.:	From/To
Drawing M-4	From		
Drawing M-14	From	L-003067	To
Drawing M-13	From	L-003068	To
Drawing M-25	From	Drawing M-812	From
Drawing M-15	From	Drawing M-8	From
UFSAR Chapters 2.3.4, 11.3.3 and 15.0.5	From	Drawing M-824	From

Is this Design Analysis Safeguards Information? Yes ☐ No ☒ If yes, see SY-AA-101-106

Does this Design Analysis contain Unverified Assumptions? Yes ☐ No ☒ If yes, ATI/ARs:

This Design Analysis SUPERCEDES: L-003063 Rev 0 **In its entirety**

Description of Revision (list affected pages for partials): revision bars are used to show the changes

Preparer: Traci Thomas (Print Name) — (Sign Name) — 10/6/08 (Date)

Method of Review: Detailed Review ☒ Alternate Calculations (attached) ☐ Testing ☐

Reviewer: Jack Robinson (Print Name) — (Sign Name) — 10/06/08 (Date)

William Paff (Print Name) — (Sign Name) — 10/6/08 (Date)

Review Notes: Independent review ☒ Peer review ☐

All inputs, assumptions, approaches, numerical analyses, and results were independently reviewed and checked.

(For External Analyses Only)

External Approver: J. Tsang (Print Name) — (Sign Name) — 10/07/08 (Date)

Exelon Reviewer: T. J. Maciaz (Print Name) — (Sign Name) — 10/07/08 (Date)

Independent 3rd Party Review Reqd? Yes ☒ No ☐ *

Exelon Approver: W. Hilton (Print Name) — (Sign Name) — 10-08-08 (Date)

WPM 10/8/08

* Original Revision & ITPR performed by WGI (J. Lahti). Additional technical and editorial reviews for Revision 1 performed by WGI (W. Paff) and Exelon (J. DeLaRosa and W. McDonald).

ATTACHMENT 2
Owners Acceptance Review Checklist for External Design Analysis
Page 1 of 1

DESIGN ANALYSIS NO. L-003063 **REV:** 1

		Yes	No	N/A
1.	Do assumptions have sufficient rationale?	☑	☐	☐
2.	Are assumptions compatible with the way the plant is operated and with the licensing basis? (using AST)	☑	☐	☐
3.	Do the design inputs have sufficient rationale?	☑	☐	☐
4.	Are design inputs correct and reasonable?	☑	☐	☐
5.	Are design inputs compatible with the way the plant is operated and with the licensing basis? (using AST)	☑	☐	☐
6.	Are Engineering Judgments clearly documented and justified?	☑	☐	☐
7.	Are Engineering Judgments compatible with the way the plant is operated and with the licensing basis? (using AST)	☑	☐	☐
8.	Do the results and conclusions satisfy the purpose and objective of the Design Analysis?	☑	☐	☐
9.	Are the results and conclusions compatible with the way the plant is operated and with the licensing basis? (using AST)	☑	☐	☐
10.	Does the Design Analysis include the applicable design basis documentation?	☑	☐	☐
11.	Have any limitations on the use of the results been identified and transmitted to the appropriate organizations? (Passport # 773640)	☑	☐	☐
12.	Are there any unverified assumptions?	☐	☑	☐
13.	Do all unverified assumptions have a tracking and closure mechanism in place?	☐	☐	☑
14.	Have all affected design analyses been documented on the Affected Documents List (ADL) for the associated Configuration Change?	☐	☑	☐
15.	Do the sources of inputs **and** analysis methodology used meet current technical requirements and regulatory commitments? (If the input sources or analysis methodology are based on an out-of-date methodology or code, additional reconciliation may be required if the site has since committed to a more recent code)	☑	☐	☐
16.	Have vendor supporting technical documents and references (including GE DRFs) been reviewed when necessary?	☑	☐	☐

EXELON REVIEWER: T. J. Mszisz / [signature] **DATE:** 10/07/08
Print / Sign

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R1

R1

R1

1.0 PURPOSE

This calculation, L-003063, Rev. 1, presents the atmospheric relative concentration (X/Q) values for Alternative Source Term (AST) accident evaluations for the LaSalle County Station. The purpose of this calculation is to determine the Control Room/Auxiliary Electric Equipment Room, henceforth CR/AEER (both the Control Room and Auxiliary Electric Equipment Room have the same intakes, therefore, the X/Q's for both the Control Room and AEER are identical), Technical Support Center (TSC), Exclusion Area Boundary (EAB), and the Low Population Zone (LPZ) outer boundary relative concentration values (X/Q, sec/m^3) resulting from certain postulated accidental radiological releases. The values resulting from this calculation will serve as input to the calculation of the radiological doses for use of the Alternative Source Terms (AST) per Regulatory Guide (RG) 1.183 (Reference 1). R1

The X/Q values resulting at the CR/AEER Intakes and TSC are calculated using the NRC-sponsored computer codes ARCON96 (Reference 2) and PAVAN (Reference 3) consistent with the procedures in RG 1.194 (Reference 4). These analyses are presented in Section 2.0 (ARCON96) and in Section 3.0 (PAVAN). R1

The X/Q values resulting at the EAB and LPZ are calculated using the NRC-sponsored computer code PAVAN, consistent with the procedures in RG 1.145 (Reference 5). This analysis is presented in Section 3.0.

2.0 ARCON96 ANALYSIS OF CR/AEER AND TSC X/Q

2.1 Identification of Computer Programs/Method of Analysis

ARCON96 is a commercial software package designated by WGI as NU-830, an "active" program applicable to nuclear safety related analyses as well as non-safety related studies and evaluations. Its use is principally control room habitability assessments. The NU-830 code has been verified for 0-2 hour, 2-8 hour, 8-24 hour, 1-4 day and 4-30 day centerline and sector X/Q averages and the 95% maximum X/Q. This verification is in accordance with Revision 4 of the (then) Washington Group International (WGI) Nuclear Engineering Standard for Computer Software Control, NEP-09. Revision 0 of NU-830 was verified for ground-level and zero exit velocity uncapped vents, and Revision 1 was verified for zero exit velocity stack releases. R1

ARCON96 Program Description [excerpted from NUREG/CR-6331 Rev. 1 (Reference 2)]

ARCON96 is a straight line Gaussian dispersion model used in control room habitability assessments for estimating dispersion in the vicinity of buildings to calculate relative concentrations at control room air intakes that would be exceeded no more than five percent of the time. The basic diffusion model implemented in the ARCON96 code is a straight-line Gaussian model that assumes the release rate is constant for the entire period of release. This assumption is made to permit evaluation of potential effects of accidental releases without having to specify a complete release sequence. Ambient atmospheric conditions measured in accordance with RG 1.23 (Reference 6) are input to ARCON96 by way of a sequential hour-by-hour meteorological database of jointly measured wind speed, wind direction, and Pasquill stability class, as derived from the vertical temperature difference recorded at a representative location and elevation (i.e., tower level).

ARCON96 permits evaluation of ground-level, vent, and elevated releases. Building wake effects are considered in the evaluation of relative concentrations from ground-level and vent releases as a function of R1

the ratio between the effluent vertical velocity and the release-height wind speed, using the same procedure used in the NRC XOQDOQ code (Reference 7). An elevated release, defined as a stack more than 2.5 times the height of structures in the immediate vicinity, is treated in the usual manner with no correction for stack downwash, and taking in account differences in terrain elevation between the stack and the control room intake. Even though the LaSalle Stack is not 2.5 times the height of its highest adjacent building, the Reactor Building, it is considered an elevated release as documented in the LaSalle SER (Reference 8) and Attachment A "Evolution of the LaSalle Stack Design". With an assumed zero (0) vertical exit velocity, vents are treated as ground-level releases. Otherwise, a vent release is treated as a mixed ground-level and elevated release.

ARCON96 requires an input of a horizontal source-receptor distance, which is defined in RG 1.194 Section 3.4 as "the shortest horizontal distance between the release point and the intake." However, for releases in building complexes, a 'taut string length' can be utilized as justifiable. Per phone conversation with Mr. Steve Lavie of NRC on May 17, 2004 (Ref. 20), when the 'taut string length' is utilized, the intake and release height should be set equal to each other so as not to also take undue advantage of the slant distance that ARCON96 calculates. R1

Diffusion coefficients used in ARCON96 have three components. The first component is the diffusion coefficient used in other NRC models, for example XOQDOQ, and PAVAN. The other two components are corrections to account for enhanced dispersion under low wind speed conditions and in building wakes. Derivations of the low wind speed and building wake corrections are described by Ramsdell and Fosmire (Reference 9). Parameter values for the correction factors are based on analysis of diffusion data collected in various building wake diffusion experiments. The experiments were conducted under a wide range of meteorological conditions. However, a large number of experiments were conducted during low wind speeds, when wake effects are minimal. The wake correction model included in ARCON96 treats diffusion under these conditions much better than previous models. Thus, the diffusion coefficients in ARCON96 account for both low-wind speed meander and wake effects.

ARCON96 calculates relative concentrations using hourly meteorological data. It then combines the hourly averages to estimate concentrations for periods ranging in duration from 2 hours to 30 days. Wind direction is considered as the averages are formed. As a result, the averages account for persistence in both diffusion conditions and wind direction. Cumulative frequency distributions are prepared from the average relative concentrations. Relative concentrations that are exceeded no more than five percent of the time (95^{th} percentile relative concentrations) are determined from the cumulative frequency distributions for each averaging period. Finally, the relative concentrations for five standard averaging periods used in control room habitability assessments are calculated from the 95^{th} percentile relative concentrations.

2.2 Assumptions

None

2.3 Inputs

2.3.1 Meteorological Data

The LaSalle meteorological tower data for the six-year period, 1998-2003, as supplied by Murray & Trettel, Inc. (Attachment B, Reference 10), were applied in the ARCON96 modeling analyses. This six-year period was the most recent data available when this revised X/Q calculation for AST was initiated. Wind measurements were taken at tower elevations 33 ft, 200 ft and 375 ft, and the vertical temperature difference (i.e., delta T) was measured between 200 ft and 33 ft and between 375 ft and 33 ft on the tower.

Wind speeds reported as "calm" were assigned a value of 0.3 mph (i.e. 0.13 m/s). ARCON96, however, re-assigns a default value of 0.5 m/s to each wind speed lower than 0.5 m/s.

Executing ARCON96 requires the meteorological input file to contain two (2) wind levels (lower and upper) and one (1) delta T stability class. Since the LaSalle X/Q analysis necessitates the modeling of both ground-level and elevated sources, two ARCON96 meteorological databases were obtained from Murray & Trettel as shown in Table 2-1.

TABLE 2-1 R1

Meteorological Database	Lower Level Wind	Upper Level Wind	Delta T Stability Class Levels
Lower	33 ft	200 ft	200-33 ft
Upper	33 ft	375 ft	375-33 ft

The most representative database was then selected to be utilized in ARCON96 for each of the release points as shown below:

TABLE 2-2

Release	Meteorological Database*
Unit 1 and 2 MSIV	Lower
Stack as an elevated release	Upper
Stack as a ground-level release	Upper
Reactor Building Hatch Access to Auxiliary Building Roof	Lower
Reactor Building Truck Bay Door	Lower
Integrated Leak Rate Test Penetration	Lower
Reactor Building Wall (Diffuse Area)	Lower

R1

* Identified in Table 2-1.

Attachment C includes the five-year wind rose diagrams based on the 33 ft, 200 ft and 375 ft meteorological tower wind data. Attachment D contains the joint wind direction, wind speed, and stability class distribution tables based on the 33 ft wind and 200-33 ft delta T, and the 375 ft wind and 375-33 ft delta T. (These data are provided both in the format of number of observations and percent occurrence frequency).

The 200 ft wind speed data were sorted in Microsoft Excel and analyzed to find the 95% highest wind speed values for use in the evaluation of the effect of high wind speeds on the ability of the secondary containment to maintain a negative pressure. This value is shown below:

Tower Level	95% Wind Speed (mph)*
200 ft	28.2

*Calculation contained in Attachment E

2.3.2 CR/AEER Intake Modeling Scenarios

The release locations identified for investigation for LaSalle are the Stack (inclusive of the Standby Gas Treatment Stack (SGTS)), the Unit 1 and Unit 2 Main Steam Isolation Valves (MSIV) pathway through the turbine seals, the Reactor Building (RB) Hatch Access to the Auxiliary Building Roof (i.e. the Auxiliary Building Roof access door at elevation 893'-6" (Grade El. = 710'-0"), extending north of column 8.9), the R1

Reactor Building Truck Bay Door, the Reactor Building Wall, and the penetration location for the Integrated Leak Rate Test (ILRT). The Stack, Unit 1 and Unit 2 MSIV, the RB Hatch Access to the Auxiliary Building Roof, the RB Truck Bay Door, and the ILRT release scenarios are modeled as point sources, and the Reactor Building Wall is modeled as a diffuse area source. R1

The North and South CR/AEER Intakes are located 40.7 m (133.5 ft) above grade as seen in Attachment K (High Point Roof El = 843'-6", Grade El. = 710'-0", Reference 15), and are identified with respect to the Stack and Auxiliary Building Roof Access in Attachment G and with respect to the MSIV, the RB Truck Bay Door, and the ILRT in Attachment H. R1

Point Sources

ARCON96 is executed for separate releases from the Stack, Unit 1 MSIV, Unit 2 MSIV, the RB Hatch Access to the Auxiliary Building Roof, the RB Truck Bay Door, and the ILRT to each of the two CR/AEER Intakes (i.e. North and South). A release from the Unit 1 MSIV to the South Control Room Intake would yield X/Q values identical to those for the Unit 2 MSIV to North Control Room Intake since all input parameters are the equal; therefore; one (1) ARCON96 run applicable to both scenarios was executed. R1

The Stack was modeled in ARCON96 as both an elevated release and a ground-level release. Modeling the Stack as an elevated release is consistent with the original LaSalle Station licensing as documented in the LaSalle SER and in Attachment A "Evolution of the LaSalle Stack Design", even though its height of 112.8 m (Reference 11) above grade is less than 2.5 times the height of its highest adjacent building, the Reactor Building. For elevated releases, aerodynamic building plume downwash effects are not present. The stack was modeled as a ground-level release to obtain X/Q values to be utilized for the Fuel Handling Accident (FHA) only. Aerodynamic building plume downwash effects are present for ground-level releases, therefore, in accordance with RG 1.194, the building area perpendicular to the wind direction is utilized. Calculation of these building areas is provided in Attachment F. The location of the Stack can be seen in Attachment G, Page G1 (Reference 12).

The Unit 1 MSIV and Unit 2 MSIV, both with a release height of 20.4 m (66.9 ft) above grade (Reference 13), are conservatively assumed located at the closest point to both the North CR/AEER and South CR/AEER intakes along the high and low pressure turbines as shown in Attachment H, Page H1 (Reference 14), and is executed by ARCON96 as a ground-level release.

The RB Hatch Access to the Auxiliary Building Roof release, with a release height of 55.9 m (183.3 ft) (Reference 13), is also conservatively located at the closest point of the roof access to the North CR/AEER and South CR/AEER Intakes as shown in Attachment G, Page G2. R1

The RB Truck Bay Door is located at ground-level between columns 14 and 15 (columns are shown in Attachment H, Page H1) and extends east from the Reactor Building with a height of 7.77 m (25.5 ft) as shown in Attachment H Page H2, (Reference 13). The RB Truck Bay Door release is also conservatively located at the closest point of the door to each of the intakes.

The penetrations for the ILRT are located 4 feet above grade, near column 10, as shown in Attachment H, pages H3 through H5 (References 21 through 23). Consistent with the application of the "taut string method" described in RG 1.194, Section 3.4, the CR/AEER Intake height is set equal to the ILRT release height. Calculations associated with the distance and direction from the CR/AEER Intakes to the ILRT point source are contained in Attachment J. R1

In accordance with RG 1.194, the building area perpendicular to the wind direction is utilized for each of the MSIV, RB Hatch Access to the Auxiliary Building Roof, RB Truck Bay Door, and ILRT scenarios. Calculations of these building areas are provided in Attachment I. | R1

All point source scenarios are conservatively assumed to have vertical velocity, exhaust flow and stack/vent radius values equal to zero (0).

Diffuse Area Source (i.e. Reactor Building Wall)

Calculations associated with the distance and direction from the CR/AEER Intakes to the Reactor Building Wall diffuse area source are contained in Attachment J. | R1

Per RG 1.194, Section 3.2.4.5, the diffuse area source representation in ARCON96 requires the building cross-sectional area to be calculated from the maximum building dimensions projected onto a vertical plane perpendicular to the line of sight from the building center to the intake.

RG 1.194, Figure 2 specifies that, for a diffuse area source, "only that part of the structure above grade or an enclosing building should be included in the building height. " For the Reactor Building Wall scenarios, the portion of the Reactor Building above the Auxiliary Building roof height was utilized for determining the release height, building area and vertical diffusion coefficient (σ_z). | R1

RG 1.194 also requires the diffuse area source release height to be assumed at the vertical center of the projected area, and initial lateral (σ_y) and vertical (σ_z) diffusion coefficients to be specified.

The diffuse source release area representing a portion of the Reactor Building wall, as calculated in compliance with RG 1.194, is shown in Attachment J.

The ARCON96 input parameter values were set in accordance with RG 1.194, Table A-2 (e.g. surface roughness length = 0.2 m; wind direction window = 90 degrees, 45 degree on either side of line of sight from source to receptor; minimum wind speed = 0.5 m/s; and sector averaging constant = 4.3).

A summary of ARCON96 input parameters and certain output meteorological data statistics is shown below in Table 2-3.

TABLE 2-3 (Sheet 1 of 6)
Stack to CR/AEER Intake ARCON96 Modeling Scenario Summary*

R1

PARAMETER	ELEVATED RELEASE		GROUND-LEVEL RELEASE	
	CR/AEER North Intake to Stack	South CR/AEER Intake to Stack	North CR/AEER Intake to Stack	South CR/AEER Intake to Stack
Number of meteorological data files	6	6	6	6
Height of lower wind instrument (m)	10.1 (33 ft)	10.1 (33 ft)	10.1 (33 ft)	10.1 (33 ft)
Height of upper wind instrument (m)	114.3 (375 ft)	114.3 (375 ft)	114.3 (375 ft)	114.3 (375 ft)
Release height (m)	112.8 (370 ft)	112.8 (370 ft)	112.8 (370 ft)	112.8 (370 ft)
Building area (m^2)	N/A**	N/A**	3907.7	3907.7
Effluent vertical velocity (m/s)	0	0	0	0
Vent or stack flow (m^3/s)	0	0	0	0
Vent or stack radius (m)	0	0	0	0
Direction .. intake to source (deg)	160	020	160	020
Wind direction sector width (deg)	90	90	90	90
Wind direction window (deg)	115-205	335-065	115-205	335-065
Distance to intake (m)	54.1 (177.5 ft)	54.1 (177.5 ft)	54.1 (177.5 ft)	54.1 (177.5 ft)
Intake height (m)	40.7 (133.5 ft)	40.7 (133.5 ft)	40.7 (133.5 ft)	40.7 (133.5 ft)
Terrain elevation difference (m)	0	0	0	0
Minimum wind speed (m/s)	0.5 (1.12 mph)	0.5 (1.12 mph)	0.5 (1.12 mph)	0.5 (1.12 mph)
Surface roughness length (m)	0.20	0.20	0.20	0.20
Sector averaging constant	4.3	4.3	4.3	4.3
Initial value of sigma y	0	0	0	0
Initial value of sigma z	0	0	0	0
Total number of hours of data processed	52584	52584	52584	52584
Hours of missing data	115	115	115	115
Hours direction in window	12083	11089	12077	11086
Hours elevated plume w/ dir. in window	58	41	0	0
Hours of calm winds	5	5	23	23
Hours direction not in window or calm	40381	41375	40369	41360
Location of ARCON96 runs showing input and output values	Attachment N, pages N2-N6	Attachment N, pages N7-N11	Attachment N, pages N17-N21	Attachment N, pages N12-N16

* Shaded cells indicate data obtained from ARCON96 output.
**Building area is not utilized by ARCON96 for elevated releases.

R1

TABLE 2-3 (Sheet 2 of 6)
MSIV to CR/AEER Intake ARCON96 Modeling Scenario Summary*

PARAMETER	GROUND-LEVEL RELEASE			
	North CR/AEER Intake		South CR/AEER Intake	
	Unit 1 MSIV	Unit 2 MSIV	Unit 1 MSIV	Unit 2 MSIV
Number of meteorological data files	6	6	6	6
Height of lower wind instrument (m)	10.1 (33 ft)	10.1 (33 ft)	10.1 (33 ft)	10.1 (33 ft)
Height of upper wind instrument (m)	61 (200 ft)	61 (200 ft)	61 (200 ft)	61 (200 ft)
Release height (m)	20.4 (67 ft)	20.4 (67 ft)	20.4 (67 ft)	20.4 (67 ft)
Building area (m^2)	3518.0	5369.3	5369.3	3518.0
Effluent vertical velocity (m/s)	0	0	0	0
Vent or stack flow (m^3/s)	0	0	0	0
Vent or stack radius (m)	0	0	0	0
Direction .. intake to source (deg)	195	270	270	345
Wind direction sector width (deg)	90	90	90	90
Wind direction window (deg)	150-240	225-315	225-315	300-030
Distance to intake (m)	80.6 (264.4 ft)	19.3 (63.3 ft)	19.3 (63.3 ft)	80.6 (264.4 ft)
Intake height (m)	40.7 (133.5 ft)	40.7 (133.5 ft)	40.7 (133.5 ft)	40.7 (133.5 ft)
Terrain elevation difference (m)	0	0	0	0
Minimum wind speed (m/s)	0.5 (1.12 mph)	0.5 (1.12 mph)	0.5 (1.12 mph)	0.5 (1.12 mph)
Surface roughness length (m)	0.2	0.2	0.2	0.2
Sector averaging constant	4.3	4.3	4.3	4.3
Initial value of sigma y	0	0	0	0
Initial value of sigma z	0	0	0	0
Total number of hours of data processed	52584	52584	52584	52584
Hours of missing data	55	55	55	55
Hours direction in window	16103	17305	17305	11878
Hours elevated plume w/ dir. in window	0	0	0	0
Hours of calm winds	17	17	17	17
Hours direction not in window or calm	36409	35207	35207	40634
Location of ARCON96 runs showing input and output values	Attachment N, pages N42-N46	Attachment N, pages N37-N41	Attachment N, pages N37-N41	Attachment N, pages N32-N36

* Shaded cells indicate data obtained from ARCON96 output.

TABLE 2-3 (Sheet 3 of 6)
RB Hatch Access to Auxiliary Building Roof to CR/AEER Intake
ARCON96 Modeling Scenario Summary*

R1

PARAMETER	GROUND-LEVEL RELEASE	
	North CR/AEER Intake	South CR/AEER Intake
	RB Hatch Access to Aux. Bldg Roof	RB Hatch Access to Aux. Bldg Roof
Number of meteorological data files	6	6
Height of lower wind instrument (m)	10.1 (33 ft)	10.1 (33 ft)
Height of upper wind instrument (m)	61 (200 ft)	61 (200 ft)
Release height (m)	55.9 (183.3 ft)	55.9 (183.3 ft)
Building area (m^2)	3436	5542
Effluent vertical velocity (m/s)	0	0
Vent or stack flow (m^3/s)	0	0
Vent or stack radius (m)	0	0
Direction .. intake to source (deg)	166	85
Wind direction sector width (deg)	90	90
Wind direction window (deg)	121 – 211	040 – 130
Distance to intake (m)	89.3 (293 ft)	22.1 (72.4 ft)
Intake height (m)	40.7 (133.5 ft)	40.7 (133.5 ft)
Terrain elevation difference (m)	0	0
Minimum wind speed (m/s)	0.5 (1.12 mph)	0.5 (1.12 mph)
Surface roughness length (m)	0.2	0.2
Sector averaging constant	4.3	4.3
Initial value of sigma y	0	0
Initial value of sigma z	0	0
Total number of hours of data processed	52584	52584
Hours of missing data	55	55
Hours direction in window	13407	10315
Hours elevated plume w/ dir. in window	0	0
Hours of calm winds	26	26
Hours direction not in window or calm	39096	42188
Location of ARCON96 runs showing input and output values	Attachment N, pages N57-N61	Attachment N, pages N62-N66

R1

R1

* Shaded cells indicate data obtained from ARCON96 output.

TABLE 2-3 (Sheet 4 of 6)
RB Truck Bay Door to CR/AEER Intake
ARCON96 Modeling Scenario Summary* R1

PARAMETER	GROUND-LEVEL RELEASE	
	North CR/AEER Intake	South CR/AEER Intake R1
	Truck Bay Door	Truck Bay Door
Number of meteorological data files	6	6
Height of lower wind instrument (m)	10.1 (33 ft)	10.1 (33 ft)
Height of upper wind instrument (m)	61 (200 ft)	61 (200 ft)
Release height (m)	7.77 (25.5 ft)	7.77 (25.5 ft)
Building area (m^2)	5776	5805
Effluent vertical velocity (m/s)	0	0
Vent or stack flow (m^3/s)	0	0
Vent or stack radius (m)	0	0
Direction .. intake to source (deg)	118	67 R1
Wind direction sector width (deg)	90	90
Wind direction window (deg)	073 – 163	022 – 112
Distance to intake (m)	104.2 (341.7 ft)	100 (328.2 ft)
Intake height (m)	40.7 (133.5 ft)	40.7 (133.5 ft)
Terrain elevation difference (m)	0	0
Minimum wind speed (m/s)	0.5 (1.12 mph)	0.5 (1.12 mph)
Surface roughness length (m)	0.2	0.2
Sector averaging constant	4.3	4.3
Initial value of sigma y	0	0
Initial value of sigma z	0	0
Total number of hours of data processed	52584	52584
Hours of missing data	55	55
Hours direction in window	10377	10483
Hours elevated plume w/ dir. in window	0	0
Hours of calm winds	17	17
Hours direction not in window or calm	42135	42029
Location of ARCON96 runs showing input and output values	Attachment N, pages N67-N71	Attachment N, pages N72-N76 R1

* Shaded cells indicate data obtained from ARCON96 output. R1

TABLE 2-3 (Sheet 5 of 6)
ILRT to CR/AEER Intake ARCON96 Modeling Scenario Summary[1]

PARAMETER	GROUND-LEVEL RELEASE		
	North CR/AEER Intake	South CR/AEER Intake	
	ILRT	ILRT	ILRT with redirected direction and building area [2]
Number of meteorological data files	6	6	6
Height of lower wind instrument (m)	10.1 (33 ft)	10.1 (33 ft)	10.1 (33 ft)
Height of upper wind instrument (m)	61.0 (200 ft)	61.0 (200 ft)	61.0 (200 ft)
Release height (m)	1.2 (4 ft)	2 (4 ft)	1.2 (4 ft)
Building area (m^2)	4885.5	5692.4	5478.7
Effluent vertical velocity (m/s)	0	0	0
Vent or stack flow (m^3/s)	0	0	0
Vent or stack radius (m)	0	0	0
Direction...intake to source (deg)	145	79	87
Wind direction sector width (deg)	90	90	90
Wind direction window (deg)	100 - 190	034 – 124	042 – 132
Distance to intake (m) [3]	163.9 (537.7 ft)	83.6 (274.4 ft)	83.6 (274.4 ft)
Intake height (m) [4]	1.2 (4 ft)	1.2 (4 ft)	1.2 (4 ft)
Terrain elevation difference (m)	0	0	0
Minimum wind speed (m/s)	0.5 (1.12 mph)	0.5 (1.12 mph)	0.5 (1.12 mph)
Surface roughness length (m)	0.2	0.2	0.2
Sector averaging constant	4.3	4.3	4.3
Initial value of sigma y	0	0	0
Initial value of sigma z	0	0	0
Total number of hours of data processed	52584	52584	52584
Hours of missing data	55	55	55
Hours direction in window	10926	10486	10367
Hours elevated plume w/ dir. in window	0	0	0
Hours of calm winds	17	17	17
Hours direction not in window or calm	41586	42026	42145
Location of ARCON96 runs showing input and output values	Attachment N, pages N77- N81	Attachment N, pages N82- N86	Attachment N, pages N87-N91

[1] Shaded cells indicate data obtained from ARCON96 output.
[2] Consistent with RG 1.194 Table A-2 guidance, redirected intake-source direction and redirected projected building area are utilized to account for the redirected flow from the taut string building edge nearest to the CR/AEER Intake.
[3] Taut string length method was utilized per RG 1.194, Section 3.4.
[4] Intake height of 40.7 has been set equal to the ILRT release height of 1.2 m

TABLE 2-3 (Sheet 6 of 6)
Reactor Building Wall (Diffuse Area) to CR/AEER Intake
ARCON96 Modeling Scenario Summary*

PARAMETER	GROUND-LEVEL RELEASE	
	North CR/AEER Intake to Reactor Building Wall	South CR/AEER Intake to Reactor Building Wall
Number of meteorological data files	6	6
Height of lower wind instrument (m)	10.1 (33 ft)	10.1 (33 ft)
Height of upper wind instrument (m)	61 (200 ft)	61 (200 ft)
Release height (m)	48.4	48.4
Building area (m^2)	1423	1423
Effluent vertical velocity (m/s)	0	0
Vent or stack flow (m^3/s)	0	0
Vent or stack radius (m)	0	0
Direction .. intake to source (deg)	139	049
Wind direction sector width (deg)	90	90
Wind direction window (deg)	094-184	004-094
Distance to intake (m)	14.4	14.4
Intake height (m)	40.7 (133.5 ft)	40.7 (133.5 ft)
Terrain elevation difference (m)	0	0
Minimum wind speed (m/s)	0.5 (1.12 mph)	0.5 (1.12 mph)
Surface roughness length (m)	0.2	0.2
Sector averaging constant	4.3	4.3
Initial value of sigma y	15.40	15.40
Initial value of sigma z	2.60	2.60
Total number of hours of data processed	52584	52584
Hours of missing data	55	55
Hours direction in window	10547	10796
Hours elevated plume w/ dir. in window	0	0
Hours of calm winds	28	28
Hours direction not in window or calm	41954	41705
Location of ARCON96 runs showing input and output values	Attachment N, pages N47-N51	Attachment N, pages N52-N56

* Shaded cells indicate data obtained from ARCON96 output.

R1

2.3.3 Technical Support Center Intake Scenarios

There are two (2) release points identified for the TSC Intake X/Q analysis: the Stack and the Unit 2 MSIV. The Stack has a release height of 112.8 m above grade and is modeled as an elevated release as stated in Section 2.3.1. The stack location is shown in Attachment H. The Unit 2 MSIV has a release height of 20.4 m (Reference 13) and is less than 2.5 times the height of its adjacent buildings; therefore, per RG 1.194, it is modeled as a "ground" level release. The Unit 2 MSIV was chosen since it is conservatively located at the closest point to the intake along the high and low pressure turbines as shown Attachment H.

The TSC Intake is conservatively treated as having a height of 4.4 m above grade elevation as seen in Attachment L. Its location is identified with respect to the Stack and MSIV in Attachment H.

ARCON96 is executed for each of the two releases (i.e. Stack and MSIV) with respect to the TSC intake.

Per RG 1.194 Table A-2, for the elevated release, the building area projected perpendicular to the wind direction should be utilized in ARCON96. For the MSIV scenario, the Reactor Building cross-sectional area was utilized. Calculations of these building areas are shown in Attachment M.

The releases for the TSC Intake modeling scenarios are each treated as a point source, and are conservatively assumed to have a zero (0) vertical velocity, exhaust flow and stack radius. The ARCON96 input parameter values were set in accordance with RG 1.194, Table A-2 (e.g. surface roughness length = 0.2 m; wind direction window = 90 degrees, 45 degree on either side of line of sight from source to receptor; minimum wind speed = 0.5 m/s; and sector averaging constant = 4.3).

A summary of ARCON96 input parameters and certain output meteorological statistics is shown below in Table 2-4.

TABLE 2-4
TSC ARCON96 Modeling Scenario Summary*

PARAMETER	ELEVATED RELEASE	GROUND-LEVEL RELEASE
	Stack to TSC Intake	Unit 2 MSIV to TSC Intake
Number of meteorological data files	6	6
Height of lower wind instrument (m)	10.1	10.1
Height of upper wind instrument (m)	114.3	61
Release height (m)	112.8	20.4
Building area (m^2)	N/A**	5355.6
Effluent vertical velocity (m/s)	0	0
Vent or stack flow (m^3/s)	0	0
Vent or stack radius (m)	0	0
Direction .. intake to source (deg)	143	135
Wind direction sector width (deg)	90	90
Wind direction window (deg)	098-188	090-180
Distance to intake (m)	164.7	85.9
Intake height (m)	4.4	4.4
Terrain elevation difference (m)	0	0
Minimum wind speed (m/s)	0.5	0.5
Surface roughness length (m)	0.20	0.20
Sector averaging constant	4.3	4.3
Initial value of sigma y	0	0
Initial value of sigma z	0	0
Total number of hours of data processed	52584	52584
Hours of missing data	115	55
Hours direction in window	10231	10485
Hours elevated plume w/ dir. in window	143	0
Hours of calm winds	5	17
Hours direction not in window or calm	42233	42027
Location of ARCON96 runs showing input and output values	Attachment N, pages N22-N26	Attachment N, pages N27-N31

R1

* Shaded cells indicate data obtained from ARCON96 output.
** Building area is not utilized by ARCON96 for elevated releases.

2.4 Numeric Results

2.4.1 CR/AEER Intake X/Q Summary

The X/Q values resulting from the ARCON96 modeling analysis of each source to CR/AEER Intake scenario are presented in Table 2-5 below. The modeling details and computer output for these scenarios are contained in Attachment N. R1

TABLE 2-5
ARCON96 X/Q Results: CR/AEER Intakes

SCENARIO			X/Q (sec/m^3)				
Source	**Receptor**	**Type of Release**	**0-2 hrs**	**2-8 hrs**	**8-24 hrs**	**1-4 days**	**4-30 days**
Stack	North CR/AEER Intake	Elevated[1]	1.00E-24[2]	1.00E-24	1.00E-24	1.00E-24	1.00E-24
	South CR/AEER Intake		1.00E-24	1.00E-24	1.00E-24	1.00E-24	2.07E-24
Stack	North CR/AEER Intake	Ground-Level	6.64E-04	4.40E-04	1.67E-04	1.12E-04	9.53E-05
	South CR/AEER Intake		6.84E-04	5.07E-04	2.14E-04	1.34E-04	9.64E-05
Unit 1 MSIV	North CR/AEER Intake	Ground-Level	1.01E-03	7.51E-04	3.10E-04	2.27E-04	1.75E-04
	South CR/AEER Intake		8.09E-03	6.09E-03	2.47E-03	1.74E-03	1.45E-03
Unit 2 MSIV	North CR/AEER Intake	Ground-Level	8.09E-03	6.09E-03	2.47E-03	1.74E-03	1.45E-03
	South CR/AEER Intake		8.74E-04	6.84E-04	2.73E-04	1.72E-04	1.29E-04
RB Hatch Access to Auxiliary Building Roof	North CR/AEER Intake	Ground-Level	7.11E-04	5.12E-04	2.07E-04	1.43E-04	1.11E-04
	South CR/AEER Intake		7.15E-03	5.16E-03	2.07E-03	1.39E-03	9.79E-04
RB Truck Bay Door	North CR/AEER Intake	Ground-Level	5.67E-04	4.53E-04	1.77E-04	1.03E-04	8.41E-05
	South CR/AEER Intake		5.71E-04	4.43E-04	1.90E-04	1.23E-04	8.83E-05
ILRT	North CR/AEER Intake	Ground-Level	2.78E-04	2.12E-04	8.41E-05	4.96E-05	3.99E-05
	South CR/AEER Intake		8.96E-04	6.90E-04	2.87E-04	1.84E-04	1.33E-04
	South CR/AEER Intake (redirected flow[3]		9.08E-04	6.97E-04	2.90E-04	1.82E-04	1.33E-04
RB Wall (Diffuse Area)	North CR/AEER Intake	Ground-Level	1.44E-03	1.07E-03	4.45E-04	2.76E-04	2.30E-04
	South CR/AEER Intake		1.67E-03	1.24E-03	5.50E-04	3.60E-04	2.60E-04

(1) These X/Q values are used in conjunction with PAVAN 0-2 hr, 1-4 day and 4-30 day values to calculate final X/Q stack values (as contained in Table 4-1) in accordance with RG 1.194 methodology.
(2) The values of 1.00E-24 in this table are a result of inherent computational limitation. Actual values would be smaller.
(3) Redirected intake-source direction and redirected projected building area are utilized.

2.4.2 Technical Support Center Intake X/Q Summary

The X/Q values resulting from the ARCON96 modeling analysis of the Stack/TSC Intake and MSIV/TSC Intake scenarios are presented in Table 2-6 below. The modeling details and computer output for these scenarios are contained in Attachment N.

TABLE 2-6
ARCON96 X/Q Results:
Technical Support Center Intake

SCENARIO				X/Q (sec/m^3)*				
Source	**Receptor**	**Type of Release**	**Building Area**	**0-2 hrs**	**2-8 hrs**	**8-24 hrs**	**1-4 days**	**4-30 days**
Stack**	TSC Intake	Elevated	N/A	1.00E-12	1.00E-12	1.00E-13	1.00E-13	1.00E-13
MSIV	TSC Intake	Ground-Level	Reactor Building	9.07E-04	6.43E-04	2.59E-04	1.54E-04	1.27E-04

* The values of 1.00E-12 and 1.00E-13 are a result of inherent computational limitations. Actual values would be smaller.

** These X/Q values are used in conjunction with PAVAN 0-2 hr, 1-4 day and 4-30 day values to calculate final X/Q stack values (as contained in Table 4-1) in accordance with RG 1.194 methodology.

3.0 PAVAN ANALYSIS OF CR/AEER, TSC, EAB AND LPZ X/Q

3.1 Identification of Computer Programs/ Method of Analysis

PAVAN is a commercial software package designated by WGI as MC-131, an "active" program applicable to nuclear safety related analyses as well as non-safety related studies and evaluations. The PAVAN code Revision 1 verification was performed for the 0-2 hour, 0-8 hour, 8-24, 1-4 day, and 4-30 day 0.5-percentile, and annual average direction-specific X/Q values, and the overall site 95-percentile maximum X/Q for each of the 0-2 hour, 0-8 hour, 8-24 hour, 1-4 day, and 4-30 day time-averaging periods. This verification was performed with (then) WGI (formerly Raytheon Engineers & Constructors, Inc.) corporate standards, and is consistent with Computer Software Control, NEP-09. Revision 1 of MC-131 was verified for ground-level (i.e., non-elevated) releases, as well as elevated releases, with zero (0) vertical exit velocity assumed. R1

While its use is principally for EAB and LPZ X/Q evaluations, PAVAN is also referenced for use in accordance with NRC RG 1.194 methodology for control room habitability assessments of elevated releases. In supplement to the use of ARCON96 for this purpose, NRC recommends that PAVAN also be executed, and its results incorporated into the determination of the 0-2 hour, and the 1-4 and 4-30 day X/Q time intervals. The 0-8 hour and 8-24 hour X/Q PAVAN results are not included in the RG 1.194 methodology. The maximum PAVAN X/Q at ground-level (excluding the "fumigation" condition) replaces the corresponding ARCON96 0-2 hour value if the PAVAN value is greater. For deriving the two longer interval X/Q values, the maximum PAVAN 1-4 day X/Q is added to the product of 23 times the maximum 1-4 day ARCON96 value, and then the total is divided by 24, resulting in the final X/Q value for the 1-4 day interval value; and similarly, the maximum PAVAN 4-30 day X/Q is added together with the product of 23 times the maximum 4-30 day ARCON96 value and then divided by 24 to obtain the X/Q value for the 4-30 day interval value.

The computer code PAVAN is a straight line Gaussian dispersion model utilized to estimate relative ground-level air concentrations (X/Q) for potential accidental releases of radioactive material from nuclear facilities, as detailed in Reference 3. Such assessment is required by 10 CFR 100 and 10 CFR 50, and the program implements the NRC guidance provided in RG 1.145. The technical basis for the program is presented by Snell and Jubach (Reference 16). Utilizing joint frequency of occurrence distributions of wind direction, wind speed and Pasquill atmospheric stability class, PAVAN calculates X/Q values as a function of direction for various time-averaging periods at the EAB and the outer boundary of the LPZ. Calculations are made from assumed ground-level (i.e., non-elevated) releases (such as vents and building penetrations), which are less than 2.5 times the height of adjacent solid structures, and from elevated releases (i.e., stacks). In conformance with RG 1.145, X/Q is calculated according to both a direction-dependent approach and an overall site X/Q approach.

The PAVAN model contains certain model options for executing the program. Table 3-1 below summarizes the options invoked for the CR/AEER, TSC, EAB and LPZ X/Q calculations.

TABLE 3-1
PAVAN Modeling Options

Option No.	Description	Option Invoked?
1	Calculate σ_y and σ_x based on desert diffusion.	No
2	X/Q values include evaluation for no building wake.	No
3	ENVLOP calculations printed which describe upper envelope curve.	No
4	Print points used in upper envelope curve and calculation.	Yes
5	Null	---
6	Joint frequency distribution in % frequency format.	No
7	Print X/Q calculation details	Yes
8	Distribute calm winds observations into first wind speed category.	Yes
9	Use site-specific terrain adjustment factors for the annual average calculations.	Yes*
10	Assume a default terrain adjustment factor for the average annual calculations. Option 10 is applied, which together with application of Option 9 means that site specific terrain factors will be used.	Yes

* A uniform value of 1.0 is used.

3.2 Assumptions

None

3.3 Inputs

3.3.1 Meteorological Data

The LaSalle meteorological data from the six-year period, 1998-2003, as supplied by Murray & Trettel, Inc., were used in the PAVAN analysis. The format of PAVAN meteorological input consists of a joint wind direction (based on sixteen 22.5 degree sectors), wind speed (14 intervals), and stability class (7 classes) occurrence frequency distribution.

Each such meteorological joint frequency distribution for input to PAVAN was prepared by using the WGI pre-qualified program ARCONtoPAVANMETrev1 (Program Number NU-840) to transform the data to a joint wind-stability occurrence frequency distribution. The fourteen wind speed categories were derived based on Section 4 of the NRC Regulatory Issue Summary 2006-04 (Reference 17) with the first category identified as "calm" as shown below in Table 3-2. The minimum (non-calm) wind speed was assumed to be 0.7 mph, based on the higher of the wind speed and direction instrument starting thresholds. Calm wind speed occurrences were assigned a value of 0.3 mph.

TABLE 3-2
DEFINED WIND SPEED CATEGORY RANGES FOR PAVAN MODELING

Category No.	Wind Speed Category Speed Intervals* (mph)
1 (Calm)	0 to<0.7
2	>=0.7 to <1.12
3	>=1.12 to <1.68
4	>=1.68 to <2.24
5	>=2.24 to <2.80
6	>=2.80 to <3.36
7	>=3.36 to <4.47
8	>=4.47 to <6.71
9	>=6.71 to <8.95
10	>=8.95 to <11.18
11	>=11.18 to <13.42
12	>=13.42 to <17.90
13	>=17.90 to <22.40
14	>=22.40

*The wind speed category speed intervals were derived based on Section 4 of the NRC Regulatory Issue Summary 2006-04.

The wind measurement level and delta T measurement layer utilized for each release elevation are identified in Table 3-3. The joint wind-stability frequency distribution matrix input to each PAVAN modeling scenario was compiled from the data measured at the indicated levels. These joint frequency distributions are shown in Attachment D.

TABLE 3-3
PAVAN Modeling Scenario Meteorology

Scenario	PAVAN Release Mode	Wind Level	Delta T Stability Class Layer
Stack to EAB and LPZ	Elevated	375 ft	375-33 ft
Turbine Building to EAB and LPZ	Ground	33 ft	375-33 ft
Stack to CR/AEER Intake	Elevated	375 ft	375-33 ft
Stack to TSC	Elevated	375 ft	375-33 ft

3.3.2 CR/AEER Intake Scenarios

For the Stack to CR/AEER Intake scenario, PAVAN was executed in ground-level release mode with a stack-to-intake horizontal distance of 54 m. The release height of the Stack is 112.8 m, however, for this PAVAN assessment RG 1.194, Section 3.2.2 requires the release height to be measured from the height of

the intake (40.7 m above grade elevation); therefore, the actual stack release height of 112.8 m above grade was reduced by 40.7 m, to 72.1 m for modeling purposes.

An additional set of PAVAN runs was also executed for the Stack to CR/AEER Intake scenario in accordance with RG 1.194 guidance to determine the distance at which the actual maximum X/Q would occur in each given downwind sector. The additional distances modeled are as follows: 50, 54 (actual), 100, 200, 300, 400, 600, 800, 1000, 1500, 1600, 1700, 1800, 1900, 2000, 2100, 2200, 2300, 2400, 2500, 3000, 3500, 4000, 4500, and 5000 meters.

In order to conservatively account for isolated areas of terrain higher than the plant grade, terrain elevations of 17 m (55.8 ft) above plant grade were used for the SSW through NW sectors for all distances 1600 m and greater. Elsewhere, plant grade receptor elevation was assumed.

3.3.3 Technical Support Center Intake Scenarios

The Stack to TSC Intake scenario was executed in elevated release mode with a stack-to-intake horizontal distance of 165 m. The release height of the Stack is 112.8 m, however, RG 1.194, Section 3.2.2 requires the release height to be measured from the height of the TSC Intake (conservatively 4.4 m above grade elevation); therefore, the actual stack release height of 112.8 m above grade was reduced by 4.4 m, to 108.8 m for modeling.

In like manner to that for the CR/AEER Intake, an additional set of PAVAN runs was executed for the stack to TSC Intake scenario in accordance with RG 1.194 guidance to determine the distance at which the actual maximum X/Q would occur in each given downwind sector. The additional distances modeled are as follows: 100, 150, 165 (actual), 200, 300, 400, 600, 800, 1000, 1500, 1600, 1700, 1800, 1900, 2000, 2100, 2200, 2300, 2400, 2500, 2600, 2700, 2800, 2900, 3000, 3100, 3200, 3300, 3400, 3500, 4000, and 4500 meters.

Conservatively, terrain elevations of 17 m above plant grade were used for the SSW through NW sectors for all distances 1600 m and greater. Elsewhere, plant grade receptor elevation was assumed.

3.3.4 EAB and LPZ Scenarios

The PAVAN model was also executed to determine the X/Q for a stack and turbine building release to the EAB and LPZ.

The Stack was modeled as an elevated release with a height of 112.8 m and the turbine building release as a ground-level release with a height of 10.0 m (as required by PAVAN for ground-level releases). An EAB distance of 509 m (Reference 18), the shortest distance between the stack and EAB, was used for the elevated release scenarios. For all ground-level release scenarios the worst-case EAB distance of 423 m (Reference 11), the shortest distance between the turbine building and EAB was conservatively utilized. An LPZ distance of 6400 m (Reference 11) was used for both the elevated and ground-level release scenarios.

The EAB distance is dependent on the wind direction sector; therefore, in order to determine the distance at which the maximum EAB X/Q value would occur, additional distances of 440, 460, 480, 500 m, and 1200 through 3300 m in increments of 100 m were executed in PAVAN for both the elevated and ground-level releases.

For the elevated release, terrain elevations of 17 m above plant grade were used for the SSW through NW sectors for distances of 1600 m and greater. Otherwise, plant grade receptor elevation was assumed. No terrain elevations were used for the ground-level release.

3.4 Numeric Results

3.4.1 CR/AEER Intake X/Q Summary

Table 3-4 presents the Stack (elevated release) to CR/AEER Intake X/Q results of PAVAN. Each listed value is the higher of the sector-specific and site limit values computed by PAVAN. X/Q values are given for the actual intake distance and for distances closer to and further from the intake location. In accordance with RG 1.194 methodology, for each distance and time period, maximum predicted X/Q values regardless of stack-to-intake direction are listed. Overall maximum values of X/Q appear in a shaded box for easy reference. The modeling details and computer output for these scenarios are contained in Attachment O. R1

TABLE 3-4
PAVAN Stack X/Q Results: CR/AEER Intake

Source	Receptor	Horizontal Distance from the Stack (m)	X/Q (sec/m^3) *				
			0-2 hours	0-8 hours	8-24 hours	1-4 days	4-30 days
Stack	CR/AEER Intake **	50	6.33E-06	1.75E-09	2.91E-11	4.01E-15	1.15E-20
		54 (Actual Distance)	6.33E-06	4.80E-09	1.32E-10	5.43E-14	7.48E-19
		100	6.33E-06	3.76E-07	9.17E-08	4.29E-09	5.28E-11
		200	6.33E-06	1.46E-06	7.01E-07	1.43E-07	1.45E-08
		300	6.33E-06	1.85E-06	1.00E-06	2.63E-07	3.87E-08
		400	6.33E-06	1.94E-06	1.07E-06	2.98E-07	4.72E-08
		600	6.32E-06	2.24E-06	1.34E-06	4.34E-07	8.65E-08
		800	6.31E-06	2.52E-06	1.59E-06	5.87E-07	1.40E-07
		1000	6.30E-06	2.75E-06	1.82E-06	7.43E-07	2.05E-07
		1500	9.84E-06	4.31E-06	2.86E-06	1.17E-06	3.23E-07
		1600	1.19E-05	5.69E-06	3.92E-06	1.75E-06	5.51E-07
		1700	1.16E-05	5.51E-06	3.80E-06	1.70E-06	5.36E-07
		1800	1.08E-05	5.17E-06	3.58E-06	1.62E-06	5.15E-07
		1900	1.05E-05	5.03E-06	3.48E-06	1.57E-06	5.00E-07
		2000	9.84E-06	4.74E-06	3.30E-06	1.49E-06	4.80E-07
		2100	9.65E-06	4.64E-06	3.22E-06	1.46E-06	4.66E-07
		2200	9.41E-06	4.52E-06	3.14E-06	1.42E-06	4.52E-07
		2300	9.61E-06	4.58E-06	3.16E-06	1.41E-06	4.45E-07
		2400	9.75E-06	4.61E-06	3.17E-06	1.40E-06	4.36E-07
		2500	9.04E-06	4.30E-06	2.97E-06	1.32E-06	4.16E-07
		3000	8.18E-06	3.85E-06	2.64E-06	1.16E-06	3.60E-07
		3500	6.73E-06	3.19E-06	2.19E-06	9.74E-07	3.04E-07
		4000	6.29E-06	2.94E-06	2.01E-06	8.80E-07	2.69E-07
		4500	5.91E-06	2.73E-06	1.86E-06	8.02E-07	2.41E-07
		5000	5.47E-06	2.51E-06	1.70E-06	7.28E-07	2.16E-07

* Shading identifies maximum for each given time period.

** X/Q values equally applicable to the North and South CR/AEER Intakes, since the distance from both Intakes to the Stack are equal; thus, utilizing applicable RG 1.145 methodology as specified by RG 1.194 for elevated release, the resulting controlling X/Q values are directionally independent. R1

3.4.2 Technical Support Center Intake X/Q Summary

Table 3-5 presents the Stack (as an elevated release) to TSC Intake scenario X/Q results of PAVAN. Each listed value is the higher of the sector-specific and site limit values computed by PAVAN. X/Q values are given for the actual intake distance and for distances closer to and further from the intake location. In accordance with RG 1.194 methodology, for each distance and time period, maximum predicted X/Q values regardless of stack-to-intake direction are listed. Overall maximum values of X/Q appear in a shaded box for easy reference. The modeling details and computer output for these scenarios are contained in Attachment O. R1

TABLE 3-5
PAVAN Stack X/Q Results:
Technical Support Center Intake

Source	Receptor	Horizontal Distance from the Stack(m)	X/Q (sec/m^3)*				
			0-2 hrs	0-8 hrs	8-24 hrs	1-4 days	4-30 days
Stack	TSC Intake	100	2.14E-06	1.06E-08	7.45E-10	2.35E-12	6.00E-16
		150	2.14E-06	1.03E-07	2.25E-08	8.35E-10	7.36E-12
		165 (Actual Distance)	2.14E-06	1.55E-07	4.18E-08	2.42E-09	4.05E-11
		200	2.14E-06	2.97E-07	1.10E-07	1.29E-08	5.94E-10
		300	2.14E-06	5.77E-07	2.99E-07	7.20E-08	9.31E-09
		400	2.14E-06	6.48E-07	3.56E-07	9.72E-08	1.51E-08
		600	2.13E-06	6.60E-07	3.67E-07	1.03E-07	1.67E-08
		800	2.13E-06	7.25E-07	4.23E-07	1.31E-07	2.44E-08
		1000	2.13E-06	7.71E-07	4.63E-07	1.54E-07	3.14E-08
		1500	2.12E-06	8.74E-07	5.60E-07	2.14E-07	5.35E-08
		1600	3.14E-06	1.42E-06	9.57E-07	4.05E-07	1.18E-07
		1700	3.14E-06	1.44E-06	9.73E-07	4.17E-07	1.24E-07
		1800	3.13E-06	1.45E-06	9.83E-07	4.26E-07	1.28E-07
		1900	3.13E-06	1.46E-06	9.93E-07	4.33E-07	1.32E-07
		2000	3.13E-06	1.46E-06	1.00E-06	4.39E-07	1.35E-07
		2100	3.13E-06	1.47E-06	1.01E-06	4.44E-07	1.37E-07
		2200	3.11E-06	1.47E-06	1.01E-06	4.46E-07	1.38E-07
		2300	3.12E-06	1.48E-06	1.01E-06	4.49E-07	1.40E-07
		2400	3.20E-06	1.51E-06	1.03E-06	4.57E-07	1.41E-07
		2500	3.20E-06	1.51E-06	1.04E-06	4.58E-07	1.42E-07
		2600	3.15E-06	1.49E-06	1.02E-06	4.54E-07	1.41E-07
		2700	3.13E-06	1.48E-06	1.02E-06	4.52E-07	1.41E-07
		2800	3.11E-06	1.47E-06	1.01E-06	4.50E-07	1.40E-07
		2900	3.09E-06	1.46E-06	1.01E-06	4.47E-07	1.39E-07
		3000	3.06E-06	1.45E-06	9.97E-07	4.43E-07	1.38E-07
		3100	3.05E-06	1.44E-06	9.92E-07	4.40E-07	1.37E-07
		3200	3.04E-06	1.44E-06	9.88E-07	4.38E-07	1.36E-07
		3300	2.97E-06	1.41E-06	9.68E-07	4.30E-07	1.34E-07
		3400	2.93E-06	1.39E-06	9.56E-07	4.25E-07	1.33E-07
		3500	2.91E-06	1.38E-06	9.48E-07	4.21E-07	1.31E-07
		4000	2.65E-06	1.26E-06	8.68E-07	3.87E-07	1.21E-07
		4500	2.51E-06	1.19E-06	8.17E-07	3.63E-07	1.13E-07

* Shading identifies maximum for each given time period.

3.4.3 EAB and LPZ X/Q Summary

The LaSalle X/Q results of PAVAN are presented in Table 3-6 for the specific EAB and LPZ distances (423m and 509 m, and 6400 m, respectively). Tables 3-7 and 3-8 contain elevated and ground-level stack X/Q values, respectively, for the additional distances that were modeled. These additional modeled distances demonstrate that the maximum EAB X/Q value for the elevated release is predicted to occur at or beyond 509 m, and for ground-level releases, at or beyond 423 m.

TABLE 3-6
PAVAN X/Q Results:
EAB and LPZ

Scenario			X/Q (sec/m^3) [1]					
Source	**Receptor**	**X/Q Parameter [2]**	**0-0.5 hour (max fumigation)**	**0-2 hrs**	**0-8 hrs**	**8-24 hrs**	**1-4 days**	**4-30 days**
Stack (Elevated Release)	EAB (509 m)	Direction-Specific Max	8.80E-05 (All Sectors)	1.90E-06 (SW)	5.87E-07 (SW)	3.26E-07 (SW)	9.09E-08 (SW)	1.45E-08 (SW)
		Site Limit	N/A [3]	1.89E-06	5.84E-07	3.24E-07	9.06E-08	1.45E-08
	LPZ (6400 m)	Direction-Specific Max	1.05E-05 (SSW - NW)	1.76E-06 (SW)	8.32E-07 (SW)	5.72E-07 (SW)	2.54E-07 (SW)	7.91E-08 (SW)
		Site Limit	N/A	1.81E-06	8.52E-07	5.84E-07	2.58E-07	7.98E-08
Turbine Building (Ground-Level Release)	EAB (423 m) [4]	Direction-Specific Max	N/A	5.40E-04 (NNW)	2.47E-04 (NNW and NE)	1.73E-04 (NE)	8.02E-05 (NE)	2.65E-05 (NE)
		Site Limit	N/A	4.67E-04	2.32E-04	1.64E-04	7.68E-05	2.59E-05
	LPZ (6400 m)	Direction-Specific Max	N/A	2.26E-05 (NNW)	9.17E-06 (NE)	5.97E-06 (NE)	2.36E-06 (NE)	6.21E-07 (NE)
		Site Limit	N/A	1.97E-05	8.48E-06	5.57E-06	2.23E-06	6.03E-07

(1) Shading indicates the higher of the Direction-Specific Max and Site Limit.
(2) Direction-Specific Max and Site Limit are defined in RG 1.145, Sections C.2 and C.3, respectively.
(3) N/A – Not Applicable
(4) 423 m, the shortest distance from the Turbine Building to the EAB, was conservatively used for ground-level release scenarios.

TABLE 3-7
PAVAN Stack X/Q Results:
Elevated Release Maximum EAB X/Q Determination

Source	Receptor	Horizontal Distance from the Stack (m)	X/Q (sec/m^3) *					
			0-0.5 hrs	0-2 hrs	0-8 hrs	8-24 hrs	1-4 days	4-30 days
Stack	EAB	509 (minimum EAB distance)	8.80E-05 All Sectors	1.90E-06 SW	5.87E-07 SW	3.26E-07 SW	9.09E-08 SW	1.45E-08 SW
		520	8.63E-05 All Sectors	1.90E-06 SW	5.86E-07 SW	3.26E-07 SW	9.10E-08 SW	1.46E-08 SW
		540	8.34E-05 All Sectors	1.90E-06 SW	5.87E-07 SW	3.26E-07 SW	9.12E-08 SW	1.46E-08 SW
		560	8.08E-05 All Sectors	1.89E-06 Site Limit** and SW	5.85E-07 Site Limit and SW	3.26E-07 SW	9.13E-08 SW	1.47E-08 SW
		580	7.82E-05 All Sectors	1.89E-06 Site Limit and SW	5.86E-07 SW	3.26E-07 Site Limit and SW	9.15E-08 Site Limit and SW	1.48E-08 Site Limit and SW
		600	7.59E-05 All Sectors	1.89E-06 Site Limit and SW	5.86E-07 Site Limit and SW	3.27E-07 Site Limit and SW	9.18E-08 Site Limit and SW	1.49E-08 Site Limit and SW
		700	6.60E-05 All Sectors	1.89E-06 Site Limit	6.11E-07 Site Limit	3.47E-07 Site Limit	1.02E-07 Site Limit	1.76E-08 Site Limit
		800	5.85E-05 All Sectors	1.88E-06 Site Limit	6.36E-07 Site Limit	3.69E-07 Site Limit	1.14E-07 Site Limit	2.09E-08 Site Limit
		900	5.26E-05 All Sectors	1.88E-06 Site Limit	6.56E-07 Site Limit	3.87E-07 Site Limit	1.23E-07 Site Limit	2.38E-08 Site Limit
		1000	4.78E-05 All Sectors	1.88E-06 Site Limit	6.74E-07 Site Limit	4.03E-07 Site Limit	1.32E-07 Site Limit	2.67E-08 Site Limit
		1100	4.39E-05 All Sectors	1.90E-06 Site Limit	6.96E-07 Site Limit	4.22E-07 Site Limit	1.42E-07 Site Limit	2.98E-08 Site Limit
		1200	4.06E-05 All Sectors	1.89E-06 Site Limit	7.12E-07 Site Limit	4.37E-07 Site Limit	1.51E-07 Site Limit	3.31E-08 Site Limit
		1300	3.77E-05 All Sectors	1.89E-06 Site Limit	7.29E-07 Site Limit	4.52E-07 Site Limit	1.61E-07 Site Limit	3.65E-08 Site Limit
		1400	3.53E-05 All Sectors	1.89E-06 Site Limit	7.45E-07 Site Limit	4.68E-07 Site Limit	1.71E-07 Site Limit	4.00E-08 Site Limit
		1500	3.32E-05 All Sectors	1.89E-06 Site Limit	7.60E-07 Site Limit	4.82E-07 Site Limit	1.80E-07 Site Limit	4.36E-08 Site Limit
		1600	3.68E-05 SSW - NW	2.82E-06 Site Limit	1.25E-06 Site Limit	8.36E-07 Site Limit	3.47E-07 Site Limit	9.81E-08 Site Limit
		1700	3.49E-05 SSW - NW	2.82E-06 Site Limit	1.27E-06 Site Limit	8.52E-07 Site Limit	3.59E-07 Site Limit	1.04E-07 Site Limit
		1800	3.31E-05 SSW - NW	2.81E-06 Site Limit	1.28E-06 Site Limit	8.63E-07 Site Limit	3.68E-07 Site Limit	1.08E-07 Site Limit and SW
		1900	3.15E-05 SSW - NW	2.81E-06 Site Limit	1.29E-06 Site Limit	8.74E-07 Site Limit	3.76E-07 Site Limit	1.12E-07 Site Limit and SW
		2000	3.01E-05 SSW - NW	2.81E-06 Site Limit	1.30E-06 Site Limit	8.83E-07 Site Limit	3.83E-07 Site Limit	1.15E-07 Site Limit and SW
		2100	2.88E-05 SSW - NW	2.81E-06 Site Limit	1.31E-06 Site Limit	8.90E-07 Site Limit	3.88E-07 Site Limit	1.18E-07 Site Limit
		2200	2.76E-05 SSW - NW	2.81E-06 Site Limit	1.31E-06 Site Limit	8.96E-07 Site Limit	3.92E-07 Site Limit	1.20E-07 Site Limit

		2300	2.65E-05 SSW - NW	2.80E-06 Site Limit	1.31E-06 Site Limit	8.98E-07 Site Limit	3.95E-07 Site Limit	1.21E-07 Site Limit and SW
		2400	2.55E-05 SSW - NW	2.79E-06 Site Limit	1.31E-06 Site Limit	9.00E-07 Site Limit	3.97E-07 Site Limit	1.22E-07 Site Limit and SW
		2500	2.46E-05 SSW - NW	2.81E-06 Site Limit	1.32E-06 Site Limit	9.05E-07 Site Limit	3.99E-07 Site Limit	1.23E-07 Site Limit and SW
		2600	2.38E-05 SSW - NW	2.78E-06 SW	1.31E-06 Site Limit and SW	8.99E-07 Site Limit and SW	3.98E-07 Site Limit and SW	1.23E-07 Site Limit and SW
		2700	2.30E-05 SSW - NW	2.78E-06 SW	1.31E-06 Site Limit and SW	9.01E-07 SW	3.99E-07 SW	1.24E-07 Site Limit and SW
		2800	2.22E-05 SSW - NW	2.78E-06 SW	1.31E-06 SW	9.00E-07 SW	3.99E-07 SW	1.24E-07 SW
		2900	2.15E-05 SSW - NW	2.77E-06 SW	1.31E-06 SW	8.97E-07 SW	3.97E-07 Site Limit and SW	1.23E-07 Site Limit and SW
		3000	2.09E-05 SSW - NW	2.75E-06 SW	1.30E-06 Site Limit and SW	8.93E-07 SW	3.95E-07 Site Limit and SW	1.23E-07 Site Limit and SW
		3100	2.03E-05 SSW - NW	2.75E-06 Site Limit	1.30E-06 Site Limit	8.91E-07 Site Limit	3.94E-07 Site Limit	1.22E-07 Site Limit and SW
		3200	1.97E-05 SSW - NW	2.75E-06 Site Limit	1.30E-06 Site Limit	8.90E-07 Site Limit	3.93E-07 Site Limit	1.22E-07 Site Limit
		3300	1.92E-05 SSW - NW	2.72E-06 Site Limit	1.28E-06 Site Limit	8.82E-07 Site Limit	3.90E-07 Site Limit	1.21E-07 Site Limit

* Shading identifies maxima.
** Site Limit is defined in RG 1.145, Section C.3.

 |R1

TABLE 3-8
PAVAN Turbine Building X/Q Results:
Ground-Level Release Maximum EAB X/Q Determination

Source	Receptor	Horizontal Distance from the Stack (m)	X/Q (sec/m^3) *				
			0-2 hrs	0-8 hrs	8-24 hrs	1-4 days	4-30 days
Turbine Building	EAB	423 (minimum EAB distance)	5.40E-04 NNW	2.47E-04 NNW and NE	1.73E-04 NE	8.02E-05 NE	2.65E-05 NE
		440	5.05E-04 NNW	2.31E-04 NNW and NE	1.62E-04 NE	7.50E-05 NE	2.48E-05 NE
		460	4.69E-04 NNW	2.14E-04 NNW and NE	1.50E-04 NE	6.96E-05 NE	2.30E-05 NE
		480	4.36E-04 NNW	2.00E-04 NE	1.40E-04 NE	6.48E-05 NE	2.14E-05 NE
		500	4.07E-04 NNW	1.86E-04 NNW and NE	1.31E-04 NE	6.04E-05 NE	2.00E-05 NE
		1200	1.23E-04 NNW	5.58E-05 NE	3.83E-05 NE	1.69E-05 NE	5.25E-06 NE
		1300	1.15E-04 NNW	5.17E-05 NE	3.54E-05 NE	1.55E-05 NE	4.74E-06 NE
		1400	1.08E-04 NNW	4.83E-05 NE	3.29E-05 NE	1.43E-05 NE	4.33E-06 NE
		1500	1.02E-04 NNW	4.52E-05 NE	3.07E-05 NE	1.33E-05 NE	3.97E-06 NE
		1600	9.60E-05 NNW	4.25E-05 NE	2.88E-05 NE	1.23E-05 NE	3.66E-06 NE
		1700	9.09E-05 NNW	4.00E-05 NE	2.70E-05 NE	1.15E-05 NE	3.39E-06 NE
		1800	8.63E-05 NNW	3.78E-05 NE	2.55E-05 NE	1.08E-05 NE	3.15E-06 NE
		1900	8.21E-05 NNW	3.58E-05 NE	2.40E-05 NE	1.01E-05 NE	2.94E-06 NE
		2000	7.82E-05 NNW	3.40E-05 NE	2.28E-05 NE	9.56E-06 NE	2.75E-06 NE
		2100	7.46E-05 NNW	3.23E-05 NE	2.16E-05 NE	9.04E-06 NE	2.59E-06 NE
		2200	7.13E-05 NNW	3.07E-05 NE	2.05E-05 NE	8.56E-06 NE	2.44E-06 NE
		2300	6.83E-05 NNW	2.93E-05 NE	1.96E-05 NE	8.12E-06 NE	2.30E-06 NE
		2400	6.55E-05 NNW	2.80E-05 NE	1.87E-05 NE	7.73E-06 NE	2.18E-06 NE
		2500	6.28E-05 NNW	2.68E-05 NE	1.78E-05 NE	7.37E-06 NE	2.07E-06 NE
		2600	6.04E-05 NNW	2.57E-05 NE	1.71E-05 NE	7.04E-06 NE	1.97E-06 NE
		2700	5.84E-05 NNW	2.48E-05 NE	1.65E-05 NE	6.76E-06 NE	1.88E-06 NE
		2800	5.63E-05 NNW	2.39E-05 NE	1.58E-05 NE	6.48E-06 NE	1.80E-06 NE
		2900	5.42E-05 NNW	2.30E-05 NE	1.52E-05 NE	6.21E-06 NE	1.72E-06 NE
		3000	5.24E-05 NNW	2.21E-05 NE	1.46E-05 NE	5.97E-06 NE	1.65E-06 NE
		3100	5.04E-05 NNW	2.13E-05 NE	1.41E-05 NE	5.73E-06 NE	1.58E-06 NE
		3200	4.87E-05 NNW	2.05E-05 NE	1.35E-05 NE	5.51E-06 NE	1.51E-06 NE
		3300	4.70E-05 NNW	1.98E-05 NE	1.31E-05 NE	5.30E-06 NE	1.46E-06 NE

*Shading identifies maxima. |R1

4.0 RESULTS AND CONCLUSIONS

The ARCON96 and PAVAN X/Q modeling calculations are summarized in Attachment P for the various release-receptor combinations. The maxima are summarized in Table 4-1 for use in the Alternative Source Term (AST) radiological accident assessments. Note that the elevated release X/Q values determined for the CR/AEER and TSC Intakes combine values of the ARCON96 and PAVAN determinations per the RG 1.194, Section 3.2.2 methodology.

TABLE 4-1
LaSalle Maximum X/Q Results Summary

SCENARIO			X/Q (sec/m^3)					
Receptor	**Source**	**Release Type**	**0-0.5 hour (max fumigation)**	**0-2 hrs**	**2-8 hrs (1)**	**8-24 hrs**	**1-4 days**	**4-30 days**
North CR/AEER Intake	Stack	Elevated[3]	N/A	1.19E-05	1.00E-24	1.00E-24	7.29E-08	2.30E-08
		Ground[4]	N/A	6.64E-04	4.40E-04	1.67E-04	1.12E-04	9.53E-05
	Unit 2 MSIV	Ground	N/A	8.09E-03	6.09E-03	2.47E-03	1.74E-03	1.45E-03
	RB Hatch Access to Auxiliary Building Roof	Ground	N/A	7.11E-04	5.12E-04	2.07E-04	1.43E-04	1.11E-04
	RB Truck Bay Door	Ground	N/A	5.67E-04	4.53E-04	1.77E-04	1.03E-04	8.41E-05
	ILRT	Ground	N/A	2.78E-04	2.12E-04	8.41E-05	4.96E-05	3.99E-05
	RB Wall (Diffuse Area)	Ground	N/A	1.44E-03	1.07E-03	4.45E-04	2.76E-04	2.30E-04
South CR/AEER Intake	Stack	Elevated (3)	N/A	1.19E-05	1.00E-24	1.00E-24	7.29E-08	2.30E-08
		Ground (4)	N/A	6.84E-04	5.07E-04	2.14E-04	1.34E-04	9.64E-05 R1
	Unit 1 MSIV	Ground	N/A	8.09E-03	6.09E-03	2.47E-03	1.74E-03	1.45E-03
	RB Hatch Access to Auxiliary Building Roof	Ground	N/A	7.15E-03	5.16E-03	2.07E-03	1.39E-03	9.79E-04
	RB Truck Bay Door	Ground	N/A	5.71E-04	4.43E-04	1.90E-04	1.23E-04	8.83E-05
	ILRT	Ground	N/A	9.08E-04	6.97E-04	2.90E-04	1.82E-04	1.33E-04
	RB Wall (Diffuse Area)	Ground	N/A	1.67E-03	1.24E-03	5.50E-04	3.60E-04	2.60E-04
TSC	Stack	Elevated (3)	N/A	3.20E-06	1.00E-12	1.00E-13	1.91E-08	5.92E-09
	MSIV	Ground	N/A	9.07E-04	6.43E-04	2.59E-04	1.54E-04	1.27E-04
EAB (2) (509 m)	Stack	Elevated	8.80E-05 (509 m)	2.82E-06 (1600 m)	1.32E-06 (2500 m)	9.05E-07 (2500 m)	3.99E-07 (2500 m)	1.24E.07 (2500 m)
EAB (423 m)	Turbine Building	Ground	N/A	5.40E-04 (NNW)	2.47E-04 (NNW and NE)	1.73E-04 (NE)	8.02E-05 (NE)	2.65E-05 (NE)
LPZ (6400 m)	Stack	Elevated	1.05E-05 (SSW-NW)	1.81E-06 (Site Limit (5))	8.52E-07 (Site Limit)	5.84E-07 (Site Limit)	5.58E-07 (Site Limit)	7.98E-08 (Site Limit)
	Turbine Building	Ground	N/A	2.26E-05 (NNW)	9.17E-06 (NE)	5.97E-06 (NE)	2.36E-06 (NE)	6.21E-07 (NE)

1) Results for the EAB and LPZ represent a 0-8 hour time period as calculated by PAVAN
2) The nearest distance at which the maximum elevated EAB X/Q value was found is shown below the X/Q value.
3) These X/Q values are calculated based on ARCON96 and PAVAN X/Q values in accordance with RG 1.194, Section 3.2.2 methodology.
4) Ground-level Stack X/Q values for FHA only.
5) Site Limit is defined in RG 1.145, Section C.3.

All input and output files associated with the ARCON96 and PAVAN modeling results are provided in Attachments N and O, respectively. PAVAN output has been shortened to include only the input and X/Q summary. The corresponding WGI Computer Disclosure Sheets are contained in Attachments Q and R.

5.0 REFERENCES

1) *Regulatory Guide 1.183, "Alternative Radiological Source Terms For Evaluating Design Basis Accidents At Nuclear Power Reactors"*; U.S. Nuclear Regulatory Commission; July 2000.

2) *Atmospheric Relative Concentrations in Building Wakes*; NUREG/CR-6331, PNNL-10521, Rev. 1; prepared by J. V. Ramsdell, Jr., C. A. Simmons, Pacific Northwest National Laboratory; prepared for U.S. Nuclear Regulatory Commission; May 1997 (Errata, July 1997).

3) *Atmospheric Dispersion Code System for Evaluating Accidental Radioactivity Releases from Nuclear Power Stations;* PAVAN, Version 2; Oak Ridge National Laboratory; U.S. Nuclear Regulatory Commission; December 1997.

4) *Regulatory Guide 1.194; Atmospheric Relative Concentrations for Control Room Radiological Habitability Assessments at Nuclear Power Plants*; U.S. Nuclear Regulatory Commission; June 2003.

5) *Regulatory Guide 1.145; Atmospheric Dispersion Models for Potential Accident Consequence Assessments at Nuclear Power Plants (Revison 1)*; U.S. Nuclear Regulatory Commission; November 1982.

6) *Regulatory Guide 1.23, Revision 1; Meteorological Monitoring Programs for Nuclear Power Plants*; U. S. Nuclear Regulatory Commission; USNRC Office of Nuclear Regulatory Research; Washington, D.C.; March 2007.

7) *XOQDOQ: Computer Program for the Meteorological Evaluation of Routine Releases at Nuclear Power Stations*; NUREG/CR-2919; J. F. Sagendorf, J. T. Goll, and W. F. Sandusky, U.S. Nuclear Regulatory Commission; Washington, D.C; 1982.

8) NRC SER (NUREG-0519), Table 2.2, March 1981. R1

9) *Atmospheric Dispersion Estimates in the Vicinity of Buildings*; J. V. Ramsdell and C. J. Fosmire, Pacific Northwest Laboratory; 1995.

10) LaSalle 1998-2003 Meteorological Tower Data; provided by Murray & Trettel, Inc. via e-mail from Dan Davidson on 8/3/2004.

11) Transmittal of Design Information (TODI) SEAG 07-000092, *LaSalle County Station-Unit 1 &2, Transmittal of Design Information of Parameters and Source of Reference for AST Analyses,* December 12, 2007.

12) Drawing M-4, *General Arrangement Roof Plan,* Units 1 & 2, Rev. C, 11/03/1980.

13) Drawing M-15, *General Arrangement Section "C-C",* Rev F, 8/3/2001.

14) Drawing M-25, *Shielding Access, Control and Radiation Zones Mezzanine Floor Plan,* Units 1 & 2, Rev. D, 11/17/1981.

15) Drawing M-13, *General Arrangement Section "A-A",* Rev. H, 8/2/2001.

16) *Technical Basis for Regulatory Guide 1.145, Atmospheric Dispersion Models for Potential Accident Consequence Assessments at Nuclear Power Plants;* NUREG/CR-2260; W. G. Snell and R. W. Jubach, U.S. Nuclear Regulatory Commission, Washington, D.C; 1981.

17) NRC Regulatory Issue Summary 2006-04, *Experience with Implementation of Alternative Source Terms*, March 7, 2006.

18) LSCS UFSAR, Section 15.0.5, Rev. 17, April 2008.

19) Drawing M-14, *General Arrangement Section "B-B",* Rev. J, 8/2/2001.

20) Washington Group International phone conversation with Mr. Steve Lavie of NRC; May 17, 2004.

21) Drawing M-824, Sheet 21, Rev. D, "Reactor Building Service Air Piping", Aug 23, 1982.

22) Drawing M-9, Rev. Q, "General Arrangement Ground Floor Plan".

23) Drawing M-812, Sheet 1, Rev. T, "Service Water Piping".

Evolution of the LaSalle Stack Design

Jerry Lahti
Draft 29 January 1998

The following is a plausible explanation of the LaSalle stack design

11/3/70. PSAR and Application filed. Station design included a free standing 300 ft. tall chimney (separate from the plant structures) which would handle SJAE and SGTS effluents. All other plant ventilation air would be discharged through a short stack on the reactor building. This configuration is shown in the NRC's Final Environmental Statement of February 1973.

1971 to 1973. Rulemaking on what would become Appendix I to 10CFR50. The emphasis on doses due to normal releases of radioactivity and effluent monitoring requirements led to the design change of replacing the original two release points by a single release point.

10/11/73. This design change was discussed at a meeting with the NRC. The design was presented as being a "tall" stack, two (2) times the reactor building height. Its physical location is atop the auxiliary building adjacent to the reactor building. This new stack would be a class I structure and would provide significant reduction is calculated doses due to it being an elevated release. The AEC received this proposal well and agreed it was an improvement over the PSAR design. A PSAR Amendment detailing the design change was requested.

4/9/74. Amendment 14 to the PSAR included "Special Report No. 1" which addressed details of the stack design. Figure 1 of this report shows the stack, 18.5 feet in diameter and 370'-0 above grade. [It is not clear from the notes in my possession, but some revisions to this design were made and resubmitted as Amendment 16, 11/8/74.]

4/3/75. The NRC letter of 4/3/75 to Commonwealth Edison states "Special Report No. 1, Common Exhaust Stack has been reviewed by our staff and we find the proposed modifications described in this report to be acceptable."

1/7/75. While the 370'-0 tall, 18.5' diameter stack was being reviewed (and being found acceptable) the engineering design was continuing to be scrutinized. It was realized that if the SGTS was operating at its design flow (4000 cfm) and discharging into an 18.5' diameter stack, the discharge velocity would be extremely low if the non-safety-related station ventilation systems were not running. This scenario offers the possibility of stack downwash under accident conditions, negating the benefit of the elevated release. A design change was recommended (S&L letter, 1/7/75) to include a separate 24-inch diameter pipe within the large stack; this 24-inch pipe would handle only the SGTS effluent. The pipe would extend one foot above the top of the main stack. The exit

~6+ m/sec.

velocity for SGTS discharge would be 1270 fpm [UFSAR 6.5.1.1.1] and should be sufficient to ensure the release being elevated under accident conditions.

8/31/76. To the best of my knowledge, the 24-inch SGTS pipe never made an entry into the PSAR, but was included in the initial FSAR tendered 8/31/76. The design details in section 11.3.3 and Figure 11.3-2 are unchanged from their original submittal. These include a depiction of both the main stack and the SGTS stack. [NOTE----The wording in the figure and text are a bit confusing and should be clarified. The main stack is 237.5 feet above the aux. bldg AND 186 feet above the reactor building. The text says "186 above the building structure" without saying which building.] Similar information in included in the UFSAR, Appendix I, which addressed the stations response to Appendix to 10CFR50 questions.

12/76. The NRC asked several questions regarding the station's gaseous effluent release points [321.2, 321.4, 372.22] and responses were provided in he acceptance review edition of the FSAR (12/76). The responses referred the reviewers to FSAR Appendix I which contained details of the vents. No questions specifically addressed the SGTS vent pipe.

3/81. The NRC's Safety Evaluation Report NUREG-0519 (3/81), in Table 2.2 provides X/Q values consistent with accepting the LaSalle release point as being an elevated one for accident assessments.

LaSalle 1998-2003 Meteorological Tower Data

Note: Filenames containing an "M" contain winds levels of 33 ft and 200 ft and Delta T Stability Class Levels of 200-33 ft. Filenames containing a "T" contain wind levels of 33 ft and 375 ft and Delta T Stability Class Levels of 375-33 ft.

LSCS98M.MET B2
LSCS98T.MET B128
LSCS99M.MET B254
LSCS99T.MET B380
LSCS00M.MET B506
LSCS00T.MET B632
LSCS01M.MET B758
LSCS01T.MET B884
LSCS02M.MET B1010
LSCS02T.MET B1136
LSCS03M.MET B1262
LSCS03T.MET B1388

LSC98M.MET

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 LSCS   1 4  189 192  5  193 313
 LSCS   1 5  195 207  5  199 342
 LSCS   1 6  204 204  5  205 331
 LSCS   1 7  210 222  5  211 340
 LSCS   1 8  218 204  5  217 312
 LSCS   1 9  220 210  5  220 312
 LSCS   110  219 247  5  219 361
 LSCS   111  218 240  4  218 347
 LSCS   112  220 235  5  220 338
 LSCS   113  221 220  5  220 328
 LSCS   114  222 205  5  221 314
 LSCS   115  230 177  5  228 270
 LSCS   116  219 110  6  219 214
 LSCS   117  211 136  6  211 263
 LSCS   118  218 161  6  216 283
 LSCS   119  218 132  5  215 248
 LSCS   120  213 111  6  213 232
 LSCS   121  218 124  6  217 250
 LSCS   122  218 144  6  219 268
 LSCS   123  217 132  6  217 250
 LSCS   2 0  218 152  5  217 264
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 LSCS   2 2  213 167  5  212 280
 LSCS   2 3  208 159  5  210 264
 LSCS   2 4  206 169  5  208 278
 LSCS   2 5  203 157  5  205 273
 LSCS   2 6  202 148  5  204 269
 LSCS   2 7  201 152  5  203 283
 LSCS   2 8  200 153  6  202 286
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 LSCS   220  198 225  5  200 348
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 LSCS   223  207 208  5  208 310
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 LSCS   3 2  204 191  5  205 281
 LSCS   3 3  205 168  5  206 256
 LSCS   3 4  204 188  5  206 280
 LSCS   3 5  207 183  5  207 276
 LSCS   3 6  206 192  5  206 285
 LSCS   3 7  204 211  5  205 309
 LSCS   3 8  204 214  5  204 319
 LSCS   3 9  204 197  4  205 293
 LSCS   310  206 201  4  206 289
 LSCS   311  210 215  4  211 287
 LSCS   312  212 202  4  213 276
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 LSCS   314  215 181  4  215 260
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LSCS   512 85 45 5 143 58
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LSCS   518 294 36 5 323 52
LSCS   519 208 21 6 304 38
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LSCS   522 265 74 5 267 122
LSCS   523 261 83 5 262 125
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LSCS   6 6 302 36 5 270 29
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