

Tab 3:

Module 2: Electrical Analysis

Frank Wyant
Sandia National Laboratories

Dan Funk
EDAN Engineering

Tab 3.1:

Circuit Analysis Overview



EPRI/NRC-RES FIRE PRA METHODOLOGY

Module 2: Fire PRA Circuit Analysis Overview

D. Funk - Edan Engineering Corp.
F. Wyant - Sandia National Laboratories

Joint RES/EPRI Fire PRA Course
September and November 2008
Bethesda, MD

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CIRCUIT ANALYSIS Presentation Road Map

- Circuit Analysis “Big Picture” Overview
- Circuit Analysis Strategy & Implementation
- Introduction to Key Considerations & Factors
- Review and Discussion of Tasks
- Relationship to Appendix R & NFPA 805
- Discussion of Relevant FAQs
- Examples

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CIRCUIT ANALYSIS

Circuit Analysis Tasks

- Task 3 – Fire PRA Cable Selection
- Task 9 – Detailed Circuit Analysis
- Task 10 – Circuit Failure Mode Likelihood Analysis
- Support Task B – Fire PRA Database

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CIRCUIT ANALYSIS

Circuit Analysis Overview

- Substantial Technical and Process-Related Advances
 - Implication of these Advances: Circuit analysis is more complex and difficult than analyses performed under Appendix R
- Collective Awareness of Circuit Failure Implications Greatly Improved
- Knowledge Base Improvements
 - Fire Tests: EPRI, CAROLFIRE, Duke: Better but not perfect understanding of fire-Induced circuit failures
 - Practical experience from NFPA 805 transition projects
 - Important “Lessons Learned” from pilot plants
 - Significant insights from “in-progress” transition projects
 - Active FAQ Process
 - Interpretation of guidance
 - New guidance

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CIRCUIT ANALYSIS

Circuit Analysis Overview

- Circuit Analysis is Now an Integral and Formal Part of the Fire PRA Process
 - Rigorous and formal process for correlating cables-to-equipment-to-affected locations
 - Definitive data and criteria has replaced estimations and judgment
 - Essential that Fire PRA and NFPA-805 data be fully integrated

Note: The subtleties of aligning Fire PRA and traditional Appendix R/NFPA-805 data is more complex than originally anticipated. This primarily shows up in Component Selection (Task 2), but has major ramifications to the circuit analysis
 - Further Refinements to “State-of-the-Art” Techniques Realistic
 - Practical aspects of dealing with an integrated data set
 - Practical approach for dealing with MSOs

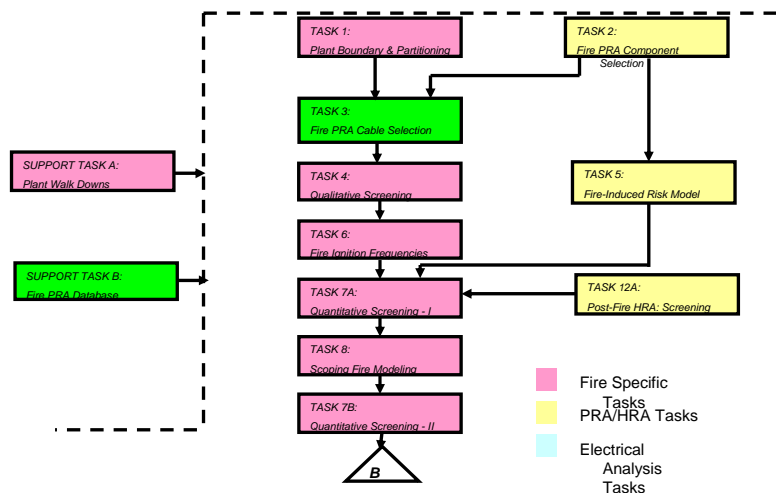
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CIRCUIT ANALYSIS

PRA Task Flow Chart

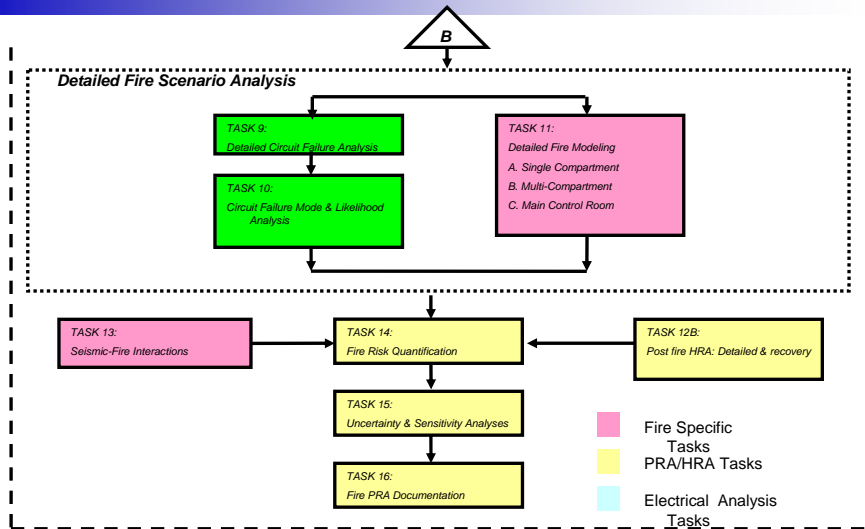


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CIRCUIT ANALYSIS PRA Task Flow Chart (continued)



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CIRCUIT ANALYSIS Overall Strategy & Implementation

- Each Electrical Analysis Task Represents a Refined Level of Detail, i.e., Graded Approach
- Level-of-Effort for the Electrical Work is a Key Driver for Project Scope, Schedule, and Resources
 - High Programmatic Risk if Not Carefully Controlled
 - Analysis and Routing of all Cables can be a Large Resource Sink with Minimal Overall Benefit
 - Concerns Validated by Numerous Projects
- Detailed Analysis Driven by Quantitative Screening Results
 - Intelligence-Based Circuit Analysis
 - Iterative Process
 - Important to screen out obvious “Not Required” cables during the initial cable selection process, with refinement driven by quantitative screening

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CIRCUIT ANALYSIS

Overall Strategy & Implementation, cont...

- Recommended Methods are Consistent with Industry Best Practices
- Use Risk Perspectives to Streamline and Focus Analysis
- Remains a Technically and Logistically Challenging Area
- Limitations to the State-of-the-Art:
 - Number of Multiple Hot Shorts/Spurious Actuations
 - Spurious Actuation Probabilities
 - Timing Considerations (being addressed by FAQ process)
- Existing Appendix R Circuit Analysis is NOT as Useful as Originally Envisioned

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CIRCUIT ANALYSIS

Overall Strategy – Related FAQ

- FAQ 08-0051 Hot Short Duration (Status: Open)
 - Issue:
 - The guidance does not provide a method for estimating the duration of a hot short once formed
 - This could be a significant factor for certain types of plant equipment that will return to a “fail safe” position if the hot short is removed
 - General approach to resolution:
 - Analyze the existing cable failure modes and effects test data to determine if an adequate basis exists to establish hot short duration distributions
 - Status:
 - Initial data analysis has been completed and results are under team review
 - NRC staff and industry review pending

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CIRCUIT ANALYSIS

Overall Strategy & Implementation, cont...

- Circuit Analysis (including cable tracing) Can Consume 40%-70% of Overall Budget
- Circuit Analysis Scope MUST be a Primary Consideration During Project Scoping
- Qualified and Experienced Electrical Analysts Must be Integral Member of PRA Team
- Coordination and Integration with Appendix R Must Occur Early and Must be Rigorous
- Coordination with Task 2 (Component Section) is Essential – MUST Understand the EXACT Functionality Credited for Each Component

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CIRCUIT ANALYSIS

Key Considerations

- Relationship with Appendix R/NFPA 805 Analysis
- Long-Term Strategy for Data Configuration Control – Especially if Shared Data with Appendix R/NFPA-805
- Availability, Quality, and Format of Cable Data
- Usability of Appendix R Circuit Analysis Data
 - Not as useful as originally envisioned
 - Automated tools are essential
 - Functional state analysis is critical – overly conservative cable selection will not work for Fire PRA
 - Many plants are finding that circuit analysis re-baseline is necessary to support upgraded Fire PRA and NFPA-805 projects
- User-Friendliness of Electrical Drawings
- Availability of Electrical Engineering Support
 - Circuit analysis is a developed expertise
 - Do not expect to be a proficient analyst based on a simple introductory course

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CIRCUIT ANALYSIS

Summary

- Do Not Underestimate Scope
- Ensure Proper Resources are Committed to Project
- Doable but **MUST** Work Smart
- Do Not “Broad Brush” Interface with Appendix R – Have a Detailed Plan Before Starting
- Constant Interaction with Systems Analysts is Critical
- Develop Project Procedures – But Don’t Get Carried Away
- Compilation and Management of Large Volume of Data
 - Automated Tools Imperative for Efficient Process
 - Be Mindful of Long-Term Configuration Management

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Tab 3.2:

Task 3 Cable Selection



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Module 2: Task 3 - Fire PRA Cable Selection

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F. Wyant - Sandia National Laboratories

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FIRE PRA CABLE SELECTION

Purpose & Scope

- Identify Circuits/Cables Associated with Fire PRA Components
- Determine Routing/Location of the Identified Cables
- Use Component-to-Cable-to-Location Relationships to Determine What Components Could be Affected for Postulated Fire Scenarios

Note: Scenario can be Fire Area, Room, Raceway, or Other Specific Location

- Identify Fire PRA Power Supplies

FIRE PRA CABLE SELECTION

Introduction

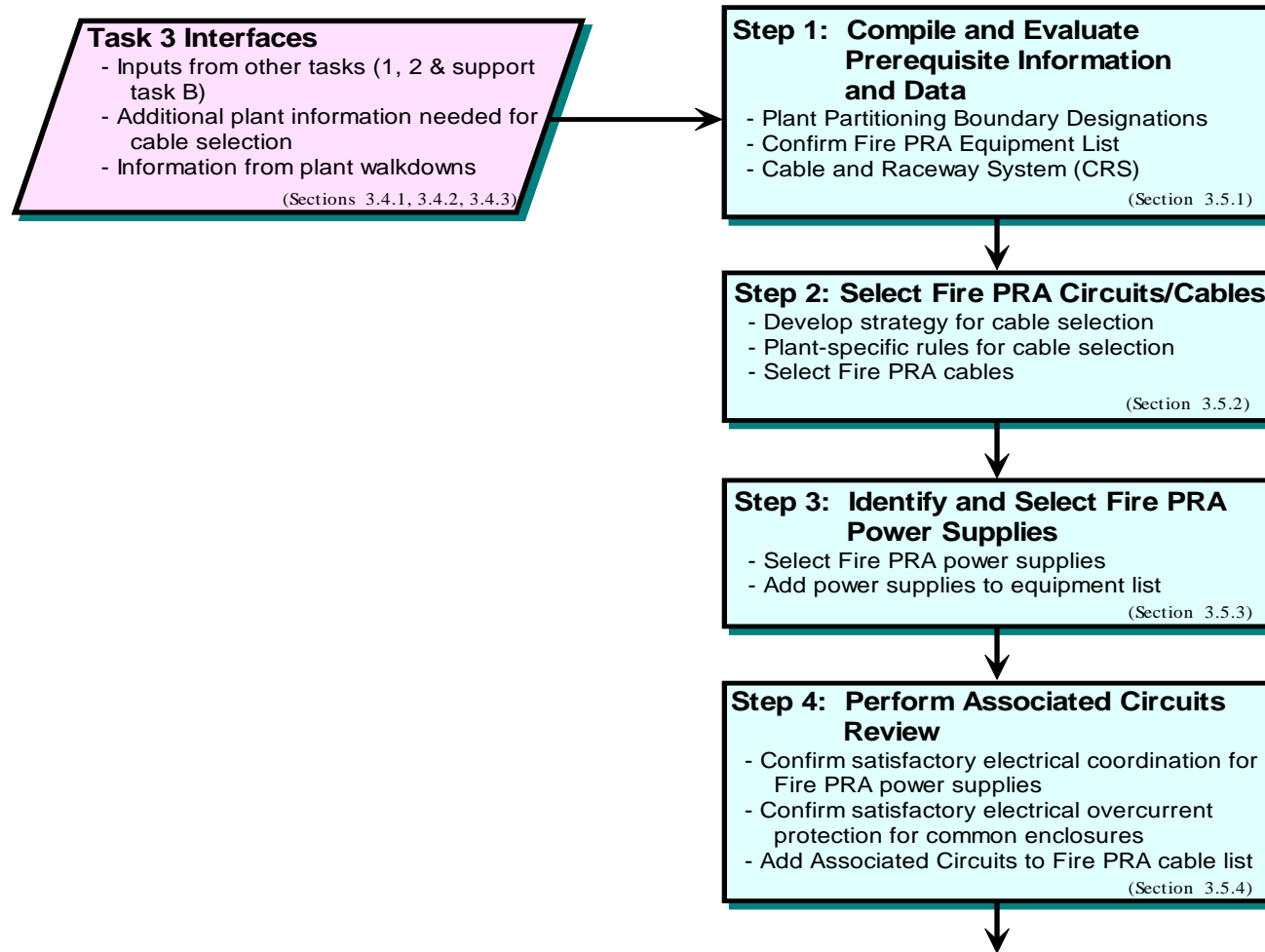
- Conducted for all Fire PRA Components

Note: Exceptions do exist

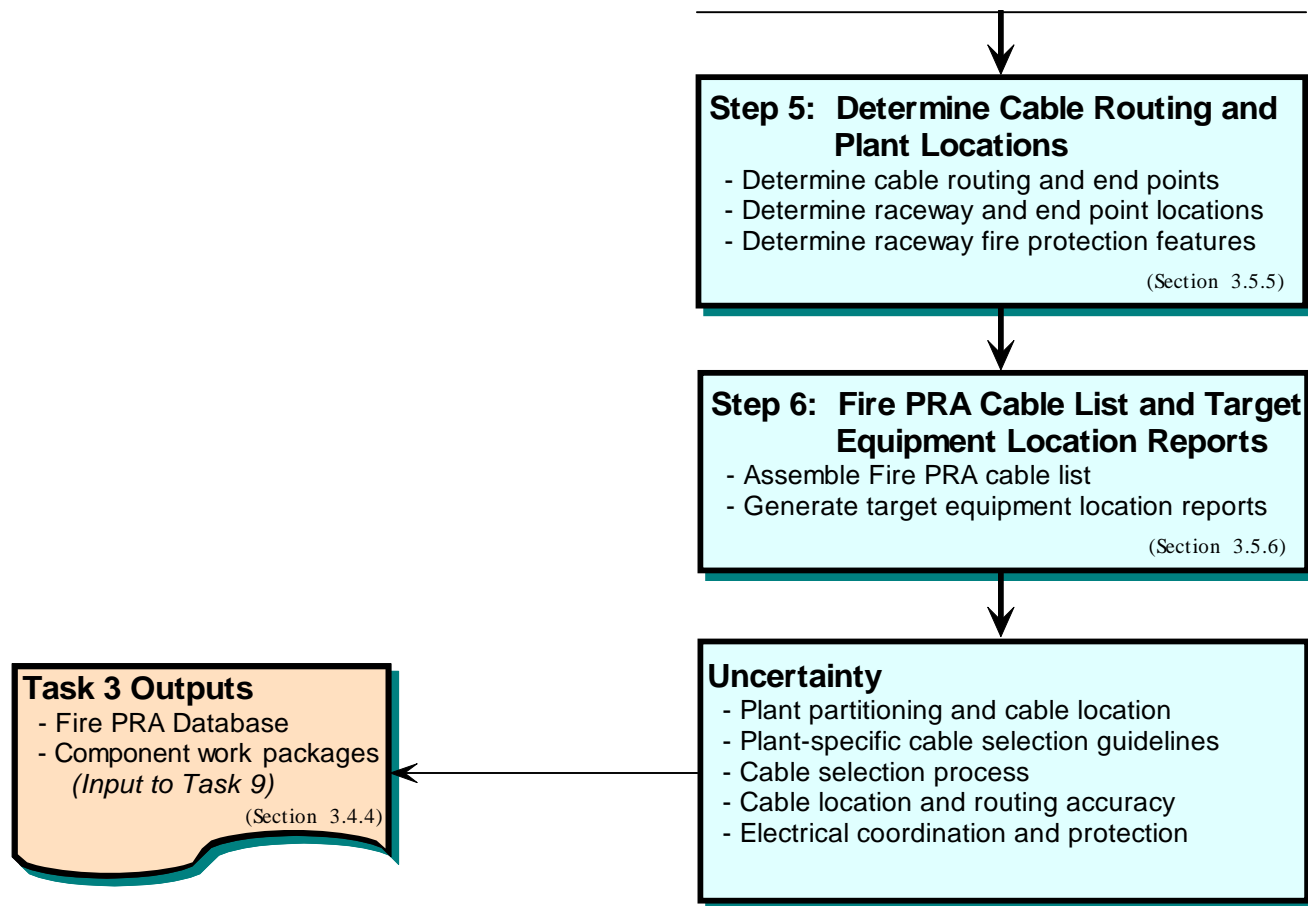
- Deterministic Process
- Cables Associated to Components Based on Specified Functionality
 - Basic circuit analysis (Task 9) incorporated into Task 3 work to prevent overwhelming the PRA model with inconsequential cable failures
 - Final product is a listing of defined Basic Events (component and credited function) that could be impacted by a fire for a given location (Fire Area, Fire Compartment, Fire Scenario)
- Procedure subdivided into six (6) distinct steps

FIRE PRA CABLE SELECTION

Flowchart



FIRE PRA CABLE SELECTION Flowchart



FIRE PRA CABLE SELECTION

Task Interfaces - Input

- Plant Boundary Partitions (Task 1)
- Fire PRA Component List (Task 2)
- Fire PRA Database (Support Task B)
- Appendix R Circuit Analysis
- Plant Cable & Raceway Database
- Plant Drawings

FIRE PRA CABLE SELECTION

Task Interfaces - Output

- Fire PRA Cable List
- Fire PRA Power Supply List
- Associated Circuits review
- Component Analysis Packages
- Target Equipment Loss Reports (Potential Equipment Functional Losses Broken Down by Location or Scenario)

FIRE PRA CABLE SELECTION

Step 1 – Prerequisite Information

- Confirm Plant Partitioning is Compatible
 - Do partitions align with cable location data?
 - What data is available and what is missing?
- Confirm PRA Equipment List is Final
 - Input into a formal and controlled database
 - For NFPA-805 transition projects a joint “consistency” review of NSP task and PRA component selection task is highly recommended
 - *Critical that electrical analysts understand what the Basic Events really mean*
- Evaluate Database Requirements
 - What currently exists?
 - What is needed to support work?
 - How is data to be managed and controlled?
 - This is a “Biggy”

FIRE PRA CABLE SELECTION

Step 2 – Select Fire PRA Cables

- Analysis Cases
 - Appendix R Component with Same Functional Requirements
 - Must consider which (if any) automatic features are included in the existing analysis
 - Aligning existing analyses to Fire PRA Basic Events is not straightforward
 - Appendix R Component with Different Functional Requirements
 - Non-Appendix R Component with Cable Location Data
 - Non-Appendix R Component without Cable Location Data
- Analysis Sub-Steps
 - Step 2.1 - Analysis Strategy
 - Step 2.2 - Plant Specific Rules
 - Step 2.3 - Select Cables

FIRE PRA CABLE SELECTION

Step 2.1 – Analysis Strategy

- Coordinate with Systems Analysts to Establish Functional Requirements and General Rules
 - Equipment functional states, basic events, initiators
 - Initial conditions and equipment lines (i.e., normal state)
 - Consistent conventions for equipment functions/state/position
 - Equipment-level dependencies and primary components
 - Multiple function components
 - Super components
- Evaluate Appendix R Component & Circuit Data
 - Ensure equipment list comparison conducted during Task 2
 - Review in detail the comparison list – ask questions!!!
 - Essential that comparison includes detailed review/comparison of “desired functional state(s)”

FIRE PRA CABLE SELECTION

Step 2.1 – Analysis Strategy (continued)

- Goal – Efficient and Accurate Process to Obtain Required Information
- Revisit Past Assumptions, Conventions, Approach
- Potential Trouble Areas
 - How is off-site power going to be handled?
 - Instrument circuits – understand exactly what is credited
 - ESAFA, Load-Shed, EDG Sequencer, other automatic functions
 - Medium-voltage switchgear control power
- Extent of Detailed Analysis to be Conducted Concurrently
- Determine How Analysis Will be Documented

FIRE PRA CABLE SELECTION

Step 2.2 – Plant Specific Cable Selection Rules

- Objective is Consistency
- Approach for Groups of Components
- Approach for Spurious Actuation Equipment
- Auxiliary Contacts – Critical Area for Completeness
- System-Wide Actuation Signals
- Bus or Breaker?
- Subcomponents & Primary Components
- Identification of Permanent Damage Scenarios
- Procedure - Develop Circuit Analysis Procedure/Guidelines

FIRE PRA CABLE SELECTION

Step 2.2 – Ready to Start?

- Develop Written Project Procedure/Guidelines
 - Consistency, Consistency, Consistency
 - Checking Process?
 - Data Entry
 - Problem Resolution
- Training for Analysts
 - Prior circuit analysis experience is a prerequisite for key team members
 - Familiarity with plant drawings and circuits is highly beneficial
 - A junior engineer with no prior circuit analysis experience will not be able to work independently

FIRE PRA CABLE SELECTION

Step 2.3 – Select Cables

- Case 1: Incorporate Existing Appendix R Analysis
 - Confirm adequacy of existing analyses IAW plan
 - Careful consideration of automatic functions
 - Exact alignment for credited functionality
- Cases 2 & 3: New Functional State/Component: w/ Cable Routing Data
 - Collect drawings and/or past analysis information
 - Identify/select cables IAW plant specific procedure/guidelines
 - Conduct detailed analysis to the extent decided upon
 - Formally document cable selection IAW established procedures/guidelines

FIRE PRA CABLE SELECTION

Step 2.3 – Select Cables (continued)

- Case 3: New Component: w/o Cable Routing Data Available
 - Same as Case 2 & 3, plus...
 - Determine cable routing and associate with plant locations, including cable end points
- Analysis Work Packages
 - Retrieve from Past Appendix R Analysis
 - Highly Recommended for New Components
 - Major time saver for future work

FIRE PRA CABLE SELECTION

Step 3 – Select Fire PRA Power Supplies

- Identify Power Supplies as Integral Part of Cable Selection
 - Make sure to differentiate between “Required” and “Not Required” power supplies
 - Switchgear and Instrument power supplies can be tricky
 - Useful to identify the applicable breaker/fuse
- Add Power Supplies to Fire PRA Component List
- Make sure Fire PRA model, equipment list, and electrical analysis are consistent
- Does Fire PRA model consider spurious circuit breaker operations?
 - Must understand how this is modeled to correctly select cables

FIRE PRA CABLE SELECTION

Step 4 – Associated Circuits Review

- Objective is to Confirm Existing Studies Adequate
- View the Process as a “Gap Analysis”
- Common Power Supply Circuits - Assess Plant Coordination Studies
- Common Enclosure Circuits - Assess Plant Electrical Protection
- Roll Up Results to Circuit Analysis or Model as Appropriate

Note: Ensure Switchgear Internal Fusing Supports Analysis Assumptions

FIRE PRA CABLE SELECTION

Step 5 – Determine Cable Routing and Locations

- Correlate Cables-to-Raceways-to-Locations
- Conceptually Straightforward
- Logistically Challenging
 - Labor intensive
 - Manual review of layout drawings
 - Plant walkdowns often required
- Determine Cable Protective Features
 - Fire wraps
 - Embedded conduit

FIRE PRA CABLE SELECTION

Step 6 – Target Equipment Loss Reports

- Data Entered into Fire PRA Database
- Sorts and Queries to Generate Target Equipment Loss Reports

Perspective....Cable selection process should be viewed as providing “Design Input” to the Fire PRA. It does not, however, provide any risk-based results. In its simplest form it provides a list of equipment that could be affected by a fire at a specified location or for a specific scenario.

Tab 3.3:

Task 9 Failure Modes Analysis



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Module 2: Task 9 - Detailed Circuit Failure Analysis

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DETAILED CIRCUIT FAILURE ANALYSIS

Purpose & Scope

The Detailed Circuit Failure Analysis Task is intended to:

- Identify the potential response of circuits and components to specific cable failure modes associated with fire-induced cable damage
- Screen out cables that do not impact the ability of a component to complete its credited function

DETAILED CIRCUIT FAILURE ANALYSIS

Introduction (1)

- Fundamentally a deterministic analysis
- Perform coincident with cable selection (Task 3) to the extent feasible and cost effective
- Difficult cases generally reserved for situations in which Quantitative Screening indicates a clear need and advantage for further analysis
- Detailed Failure Modes Analysis
 - Requires knowledge about desired functionality and component failure modes
 - Conductor-by-conductor evaluation (Hot Probe method recommended)
- Objective is to screen out all cables that **CANNOT** impact the ability of a component to fulfill the specific function of interest

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DETAILED CIRCUIT FAILURE ANALYSIS

Introduction (2)

- Failure Modes Considered
 - Single Shorts-to-Ground (Reference Ground)
 - Grounded System
 - Ungrounded System
 - Resistance Grounded System
 - Single Hot Shorts
 - Compatible Polarity Multiple Hot Shorts for Ungrounded AC and DC Circuits
 - Coincident Independent Hot Shorts On Separate Cables
 - Multiple Intra-cable Hot Shorts
 - Cables Associated Through Common Power Supply

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DETAILED CIRCUIT FAILURE ANALYSIS

Introduction (3)

- Failure Modes **NOT** Considered
 - 3-phase proper sequence hot shorts (except high consequence equipment with thermoplastic insulated conductor or ungrounded configuration)
 - Inter-cable hot shorts for armored cable and cable in dedicated conduit
 - Open circuit conductor failures
 - Multiple high-impedance faults

Note: if conducting a combined NFPA-805 and Fire PRA circuit analysis, NEI 00-01 suggests that open circuits be considered

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DETAILED CIRCUIT FAILURE ANALYSIS

Assumptions

The Following Assumptions Form the Basis for Task 9:

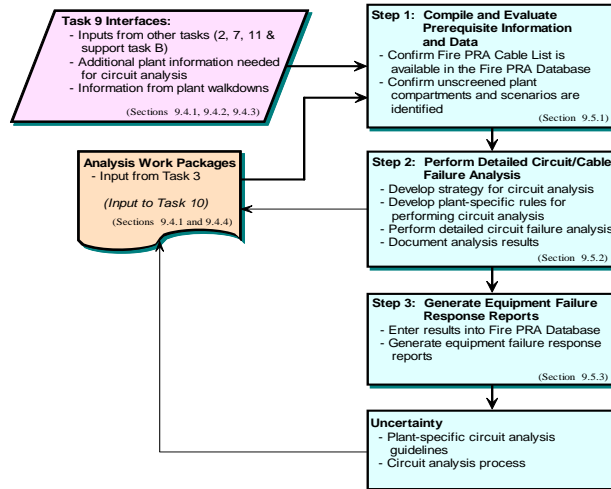
- An Appendix R analysis for the plant has been completed and is available for identifying equipment failure responses to specific cable failure modes
- Component **Work Packages** have been assembled as part of the Task 3 activities or previous Appendix R analyses
- Equipment is assumed to be in its normal position or operating condition at the onset of the fire – the equipment state might be variable
- Users of this procedure are knowledgeable on and have experience with circuit design and analysis methods

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DETAILED CIRCUIT FAILURE ANALYSIS Flowchart



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DETAILED CIRCUIT FAILURE ANALYSIS Task Interfaces - Inputs

- Fire PRA Components List (Task 2)
- Fire PRA Cable List (Task 3)
- Fire PRA Database (Support Task B)
- Results of Quantitative Screenings (Task 7)
- Results of Detailed Fire Modeling (Task 11)
- Appendix R Circuit Analysis
- Plant Drawings
- CRS Database

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DETAILED CIRCUIT FAILURE ANALYSIS

Task Interfaces - Outputs

- Equipment Failure Response Reports
- Component Analysis Packages (Updated)
- Revised Cable List
- Fire PRA Database & Model Updates

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DETAILED CIRCUIT FAILURE ANALYSIS

Step 1 - Compile Prerequisite Information

- Ensure that prerequisite information and data is available and usable before beginning the analyses (ideally the necessary drawings are already in the Work Packages).
- **Step 1.1:** Confirm Fire PRA Cable List is Available in the Fire PRA Database
 - Component \Rightarrow Cable \Rightarrow Raceway \Rightarrow Compartment
- **Step 1.2:** Confirm Unscreened Plant Compartments and Scenarios are Identified
 - Target Equipment Loss Reports
 - Equipment ID, Normal Status, Functional Requirements, etc.

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DETAILED CIRCUIT FAILURE ANALYSIS

Step 2 - Perform Circuit Failure Analysis

- Perform a *Deterministic-Based* detailed circuit analysis for the Fire PRA cables of interest that are located in the unscreened plant locations.
- Step 2.1: Develop Strategy/Plan for Circuit Analysis
- Step 2.2: Develop Plant-Specific Rules for Performing the Detailed Circuit Analysis
- Step 2.3: Perform Detailed Circuit Failure Analysis
- Document Analysis Results ⇒ Component Work Packages

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DETAILED CIRCUIT FAILURE ANALYSIS

Step 3 - Generate Equipment Failure Response Reports

- Enter Results into Fire PRA Database
- Generate Equipment Failure Response Reports
 - A Listing by location (room, zone, area) of equipment and associated cables affected by fire
 - Provides specific equipment responses (cable failure consequences) that affect the credited function being analyzed
 - Equipment losses should be correlated to each Basic Event

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DETAILED CIRCUIT FAILURE ANALYSIS

Caveats & Recommendations

- This Detailed Circuit Failure Analysis Methodology is a **Static Analysis** (No Timing Issues are Considered)
- Be Aware of Possible **Cable Logic Relationships**
- Work Packages (Highly Recommended!)
- “Hot Probe” (Conductor-to-Conductor) Analysis Must be Rolled-Up to Cable/Component Level
- Outputs Need to Be **Compatible with Fire PRA Database** Format and Field Structure
- Coordinate with the Fire PRA Modelers/Analysts Early-On to **Define the Fire PRA Component Failure Modes of Concern**

Tab 3.4:

Task 10 Failure Mode Likelihood Analysis

Tab 3.4a:

Task 10 Presentation Materials



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CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS

Purpose & Scope

The Circuit Failure Mode Likelihood Analysis Task is Intended to:

- Establish First-Order Probability Estimates for the Circuit Failure Modes of Interest

AND

- Correlate Those Failure Mode Probabilities to Specific Components

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CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS

Introduction (1)

- Probabilistic Based Analysis
- Two Methods Presented
 - Expert Panel Results (Look-Up Tables)
 - Computation-Based Analysis (Formulas)
- Requires Knowledge About Circuit Design, Cable Type and Construction, Installed Configuration, and Component Attributes
- Generally Reserved for Only Those Cases that Cannot be Resolved Through Other Means

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CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS

Introduction (2)

- Caveats:
 - Our Knowledge is Greatly Improved but Uncertainties are Still High
 - Very limited data for many issues
 - For This Reason, Implementing Guidance is **Conservative**
 - Practical Implementation is Challenging
 - Further Analysis of Existing Test Data and Follow-On Tests Would be Beneficial:
 - Reduce Uncertainties, including conservatisms as appropriate
 - Solidify Key Influence Factors
 - Incorporate Time as a Factor (FAQ 007-051)
 - Incorporate “End-Device” Functional Attributes and States (e.g., latching circuits vs. drop-out design)
 - Computation-based method (formula) is an extrapolation of existing data; validation remains to be done. Conservatism has not been established.
- Probabilities of sufficient quality to move ahead

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CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS

Introduction (3)

- Public and Peer Review Comments
 - Several Questions Involving Interpretation of the EPRI Test Data Lead to Extensive Discussions Regarding the Most Appropriate Way to Tally Spurious Actuation Probabilities (Many Subtleties for Implementation)
 - Team's Consensus is that Expert Panel Values are, in General, somewhat Conservative
 - Additional Independent Review of the Computational Method was Solicited as a Result of Peer and Public Comments
 - Review was Favorable, However the Team Acknowledges the Inevitable Limitations of the Methodology

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CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS

Assumptions

The Following Assumptions Form the Basis for Task 10:

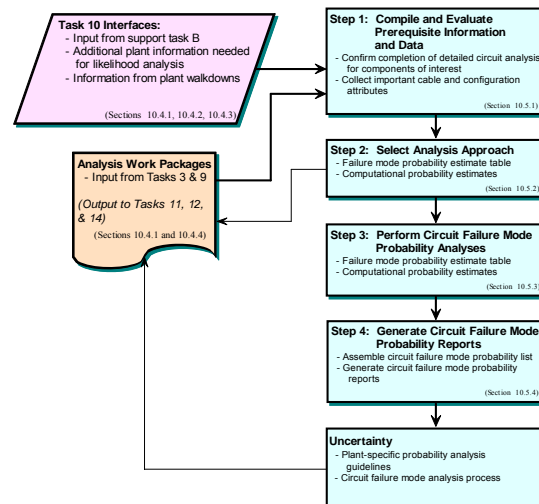
- Specific Cable/Circuit Configuration Attributes are Available or Can Be Determined
- The Equipment is in Its Normal Position or Operating Condition at the Onset of the Fire
- Users of This Procedure are Knowledgeable and Have Experience with Circuit Design and Analysis Methods and Probability Estimating Techniques
- This Analysis Method is Applied to Cables with **No More than 15 Conductors**

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CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS Flowchart



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CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS Task Interfaces - Inputs

- Fire PRA Cable List (Task 3)
- Fire PRA Database (Support Task B)
- Results of Detailed Circuit Failure Analysis (Task 9)
- Specific Scenarios Identifying Affected Cables (Tasks 11 & 14)
- Cable & Circuit Configuration Attributes
- Plant Drawings

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CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS

Task Interfaces - Outputs

- Quantification of Fire Risk (Task 14)
- Post-Fire HRA (Task 12)
- Detailed Fire Scenario Quantification (Task 11)
- Circuit Failure Mode Probability Reports
- Component Work Packages (Finalized)
- Fire PRA Database & Model

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CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS

Step 1 - Compile Prerequisite Information

Ensure that Prerequisite Information and Data is Available
and Usable before Beginning the Analyses.

- Confirm Completion of Detailed Circuit Analysis for
Components of Interest
- Collect Important Cable and Configuration Attributes
 - Insulation
 - Number of Conductors
 - Raceway Types
 - Power Source(s)
 - Number of Source & Target Conductors (for Option #2 Only)

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CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS

Step 2 - Select Analysis Approach

Decide Which Analysis Option is Best Suited for Conducting the Evaluation.

1. Failure Mode Probability Estimate Tables
 - Grounded Circuit Design
 - Non-Complex Control Circuit
 - Single Component Service
 - Cable Configuration Matches Table Categories
 - Principal Failure Mode of Concern is Spurious Actuation
2. Computational Probability Estimate Formulas
 - Ungrounded or Resistance-Grounded Circuit Design
 - Complex Circuit or Component
 - Failure Potentially Affects Multiple Components
 - Cable Configuration Not Easily Categorized in Tables

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CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS

Step 3 - Estimate Circuit Failure Mode Probabilities

Estimate Circuit Failure Mode Probabilities Employing the Selected Method

Option #1: Failure Mode Probability Estimate Tables

- Table 10-1, Thermoset Cables with CPTs
- Table 10-2, Thermoset Cables without CPTs
- Table 10-3, Thermoplastic Cables with CPTs
- Table 10-4, Thermoplastic Cables without CPTs
- Table 10-5, Armored or Shielded Cables

Option #2: Computational Probability Estimate Formulas

$$P_{CC} = (C_{Tot} - C_G) / [(C_{Tot} - C_G) + (2 \times C_G) + n]$$

$$CF = \{C_T \times [C_S + (0.5 / C_{Tot})]\} / C_{Tot}$$

$$P_{FM} = CF \times P_{CC}$$

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CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS

Step 3 – Related FAQ

- FAQ 08-0047 Cable Dependency (Status: Open)
 - Issue:
 - Guidance (Vol. 2, Page 10-7, Bullet 3) states that when more than one cable can cause the same spurious actuation you combine probabilities using “exclusive or”
 - This assumes faults/effects are independent
 - General approach to resolution:
 - Consensus reached that “exclusive or” is not appropriate if faults are dependent (e.g., a common power supply for both cables)
 - Clarify treatment to determine and address dependency
 - Status:
 - Team draft has been completed
 - Staff and final industry review pending

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CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS

Step 4 - Generate Failure Mode Probability Reports

- Enter Results into Fire PRA Database
- Generate Circuit Failure Mode Probability Reports
 - Listing the Probability Estimates for the Circuit Failure Modes of Concern for Each Component of Interest by Plant Area (Compartment, Fire Area, Fire Zone, etc.)

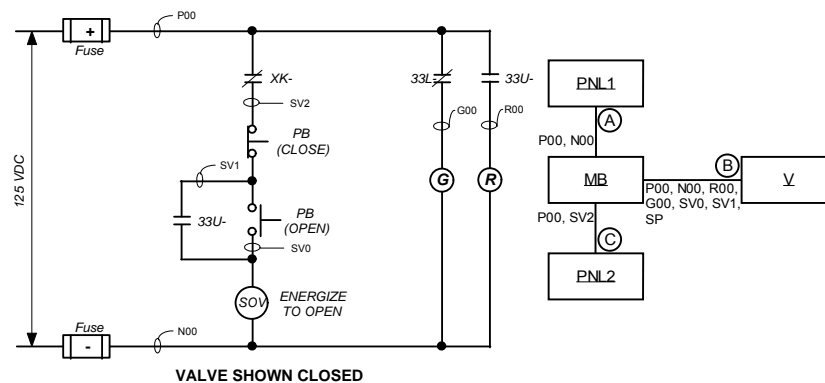
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CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS

Example - SOV Control Circuit



QUESTION: What is the probability that damage to Cable B will result in spurious opening of the SOV?

See next slide →

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CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS

Example – Step 1: Prerequisite Information

- Detailed circuit analysis completed & documented? **Yes**

Cable	+125 VDC Hot Probe	-125 VDC Hot Probe
A	LOC	LOC
B	LOC, EI, SO - Open	LOC
C	NC	LOC

- Collect important cable and configuration data:
 - Cable insulation? *Thermoset*
 - Number of conductors? *Seven*
 - Raceway type? *Tray*
 - Power source? *Ungrounded DC bus (no CPT)*
 - Number of source & target conductors? *3 sources, 1 target*

See next slide →

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CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS

Example – Step 2: Select Analysis Approach

- Option #1: Failure Mode Probability Tables
 - Grounded circuit design? **No**
 - Control circuit cable? **Yes**
 - Single component circuit? **Yes**
 - Known cable configuration? **Yes**
 - Spurious operation concern? **Yes**
- Option #2: Computational Probability Estimate
 - Ungrounded circuit? **Yes**
 - Complex circuit/component? **No**
 - Multiple component circuit? **No**
 - Cable configuration not categorized? **No**

For this example, we'll show both methods

See next slide →

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CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS

Example – Step 3: Perform Analysis (1)

- Option #1:
 - Which Table to Use? **Table 10-2, Thermoset Cable without CPT**

Raceway Type	Description of Hot Short	Best Estimate	High Confidence Range
Tray	M/C Intra-cable	0.60	0.20 – 1.0
	1/C Inter-cable	0.40	0.1 – 0.60
	M/C → 1/C Inter-cable	0.20	0.1 – 0.40
	M/C → M/C Inter-cable	0.02 – 0.1	
Conduit	M/C Intra-cable	0.15	0.05 – 0.25
	1/C Inter-cable	0.1	0.025 – 0.15
	M/C → 1/C Inter-cable	0.05	0.025 – 0.1
	M/C → M/C Inter-cable	0.01 – 0.02	

- SO_{Open} Probability Estimate, $P = \underline{0.62}$ ($0.60 + 0.06 - 0.60 \cdot 0.06$)

See next slide →

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CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS

Example – Step 3: Perform Analysis (2)

- **Option #2:**

- Calculate probability of a conductor-to-conductor short:

$$P_{CC} = (C_{Tot} - C_G) / [(C_{Tot} - C_G) + (2 * C_G)]$$

$$P_{CC} = (7 - 1) / [(7 - 1) + (2 * 1)]$$

$$P_{CC} = 6 / [6 + 2]$$

$$P_{CC} = 0.75$$

- Determine cable configuration factor:

$$CF_{SO} = \{C_T * [C_S + (0.5 / C_{Tot})]\} / C_{Tot}$$

$$CF_{SO} = \{1 * [3 + (0.5 / 7)]\} / 7$$

$$CF_{SO} = 3.071 / 7$$

$$CF_{SO} = 0.44$$

- Probability of spurious operation, $P_{SO(Open)} = 0.75 * 0.44 = \underline{0.33}$

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CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS

Example – Step 4: Failure Mode Probability Report

Failure Code	Estimated Probability (Calculated)	Estimated Probability (From Table 10-2)
SO (Open)	0.33	0.62

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Tab 3.4b:

Task 10 Classroom Exercises

Task 10: Circuit Failure Mode Likelihood Analysis Methodology

This document summarizes the process for determining the probability, or likelihood, of a particular circuit failure mode occurrence. It includes the five Failure Mode Probability Estimate Tables employed under the Option #1 analysis approach, and the Option #2 Computational Probability Estimate formulas. **Important!** Please refer to the complete discussion of this methodology provided in NUREG/CR-6850, EPRI 1011989, “EPRI/NRC-RES Fire PRA Methodology for Nuclear Power Facilities; Volume 2: Detailed Methodology,” Final Report, September 2005.

Selecting the Analysis Approach

1. Option #1: Failure Mode Probability Estimate Tables

Tables of probability estimates would appropriately be used for cables that meet the following criteria:

- The circuit is of a grounded design (including impedance grounded systems with ground fault trip capability),
- The cable is part of the control circuit for a typical component (e.g., non-complex MOVs, SOVs, pumps),
- The cable is associated with a single component,
- The cable configuration is known and can be readily associated with one of the defined configurations in Tables 1 through 5, and
- The principal hot short failure mode of concern is a spurious operation of the component.

2. Option #2: Computational Probability Estimates

Use of the probability estimate formulas are recommended for cases where:

- The circuit is ungrounded or is impedance grounded without ground fault trip capability,
- The cable is part of a relatively complex circuit or component,
- The cable is associated with or can influence the behavior of multiple components (e.g., safeguards actuation signal, bus shed scheme, etc.),
- The cable configuration is not easily categorized into one of the defined configurations contained in Tables 1 through 5.

Performing the Circuit Failure Mode Probability Analyses

Option #1: Failure Mode Probability Estimate Tables

1. Categorize the circuit of interest based on its configuration attributes.

2. From the appropriate table (Tables 1 to 5), select the probability estimates for the failure modes of concern.
3. If the cable failure mode can occur due to different cable interactions, the probability estimate is taken as the simple sum of both estimates. For example, if a particular thermoset cable failure mode can be induced either by an intra-cable shorting event ($P = 0.30$) or by an inter-cable shorting event ($P = 0.03$; mid-range of 0.01–0.05), the overall probability of that failure mode is estimated to be 0.33.

Table-1
Failure Mode Probability Estimates Given Cable Damage
Thermoset Cable with Control Power Transformer (CPT)

Raceway Type	Description of Hot Short	Best Estimate	High Confidence Range
Tray	M/C Intra-cable	0.30	0.10 – 0.50
	1/C Inter-cable	0.20	0.05 – 0.30
	M/C → 1/C Inter-cable	0.10	0.05 – 0.20
	M/C → M/C Inter-cable	0.01 – 0.05	
Conduit	M/C Intra-cable	0.075	0.025 – 0.125
	1/C Inter-cable	0.05	0.0125 – 0.075
	M/C → 1/C Inter-cable	0.025	0.0125 – 0.05
	M/C → M/C Inter-cable	0.005 – 0.01	

M/C: Multi-conductor cable

1/C: Single conductor cable

Intra-cable: An internally generated hot short. The source conductor is part of the cable of interest

Inter-cable: An externally generated hot short. The source conductor is from a separate cable

Table-2
Failure Mode Probability Estimates Given Cable Damage
Thermoset Cable without CPT

Raceway Type	Description of Hot Short	Best Estimate	High Confidence Range
Tray	M/C Intra-cable	0.60	0.20 – 1.0
	1/C Inter-cable	0.40	0.1 – 0.60
	M/C → 1/C Inter-cable	0.20	0.1 – 0.40
	M/C → M/C Inter-cable	0.02 – 0.1	
Conduit	M/C Intra-cable	0.15	0.05 – 0.25
	1/C Inter-cable	0.1	0.025 – 0.15
	M/C → 1/C Inter-cable	0.05	0.025 – 0.1
	M/C → M/C Inter-cable	0.01 – 0.02	

Table-3
Failure Mode Probability Estimates Given Cable Damage
Thermoplastic Cable with CPT

Raceway Type	Description of Hot Short	Best Estimate	High Confidence Range
Tray	M/C Intra-cable	0.30	0.10 – 0.50
	1/C Inter-cable	0.20	0.05 – 0.30
	M/C → 1/C Inter-cable	0.10	0.05 – 0.20
	M/C → M/C Inter-cable	0.01 – 0.05	
Conduit	M/C Intra-cable	0.075	0.025 – 0.125
	1/C Inter-cable	0.05	0.0125 – 0.075
	M/C → 1/C Inter-cable	0.025	0.0125 – 0.05
	M/C → M/C Inter-cable	0.005 – 0.01	

Table-4
Failure Mode Probability Estimates Given Cable Damage
Thermoplastic Cable without CPT

Raceway Type	Description of Hot Short	Best Estimate	High Confidence Range
Tray	M/C Intra-cable	0.60	0.20 – 1.0
	1/C Inter-cable	0.40	0.1 – 0.60
	M/C → 1/C Inter-cable	0.20	0.1 – 0.40
	M/C → M/C Inter-cable	0.02 – 0.1	
Conduit	M/C Intra-cable	0.15	0.05 – 0.25
	1/C Inter-cable	0.1	0.025 – 0.15
	M/C → 1/C Inter-cable	0.05	0.025 – 0.1
	M/C → M/C Inter-cable	0.01 – 0.02	

Table-5
Failure Mode Probability Estimates Given Cable Damage
Armored or Shielded Cable

Raceway Type	Description of Hot Short	Best Estimate	High Confidence Range
With CPT	M/C Intra-cable	0.075	0.02 – 0.15
Without CPT	M/C Intra-cable	0.15	0.04 – 0.30

- When more than one cable can cause the component failure mode of concern, and those cables are within the boundary of influence for the scenario under investigation, the

probability estimates associated with all affected cables should be considered when deriving a failure estimate for the component. In general, the probabilities should be combined as follows:

$$P_{\text{Component failure}} = (P_{\text{Failure Cable A}}) + (P_{\text{Failure Cable B}}) - (P_{\text{Failure Cable A}})(P_{\text{Failure Cable B}})$$

Option #2: Computational Probability Estimates

Application of this calculational method is more complex and is only recommended for cases where Option #1 cannot reasonably be applied. The intent is to give the analyst a means of refining the estimated circuit failure mode probabilities based on the most important characteristics of the cable/circuit under study.

This computational method involves applying circuit failure mode probability estimation formulas. The following discussions provide only the minimum definition of the failure mode likelihood estimation formulas and their terms. For a complete discussion of the technical basis, detailed explanations, and examples of usage, please refer to Appendices J and K in Volume 2 of EPRI 1011989, NUREG/CR-6850.

The probability of occurrence for a specific hot short failure mode (P_{FM}) is estimated by the formula:

$$P_{\text{FM}} = \text{CF} \times P_{\text{CC}}$$

Where:

P_{FM} = The probability that a specific hot short failure mode of interest will occur in a specific circuit given a fire of sufficient intensity to cause cable damage,

P_{CC} = The probability that a conductor-to-conductor short will occur prior to a short-to-ground or short to a grounded conductor, and

CF = A configuration factor applied to P_{CC} to account for the relative number of source conductors and target conductors. Target conductors are those conductors of a circuit that, if contacted by an electrical source of proper magnitude and voltage, will result in abnormal energization of the circuit, component or device of concern. Source conductors represent energized conductors that are a potential source of electrical energy.

1. Calculate P_{CC} as follows:

Cables in trays: $P_{\text{CC}} = (C_{\text{Tot}} - C_G) / [(C_{\text{Tot}} - C_G) + (2 \times C_G) + 1]$

Cables in conduit¹: $P_{\text{CC}} = (C_{\text{Tot}} - C_G) / [(C_{\text{Tot}} - C_G) + (2 \times C_G) + 3]$

Ungrounded systems: $P_{\text{CC}} = (C_{\text{Tot}} - C_G) / [(C_{\text{Tot}} - C_G) + (2 \times C_G)]$

¹ Armored and shielded cable should use the equation for conduit.

Where:

C_{Tot} = The total number of conductors in the cable of interest (including spares), and

C_G = The number of grounded (or common) conductors in the cable of interest. The analyst should determine the number of grounded/common conductors based on the circuit configuration (contact positions, etc.) that represent the normal operating state of the component. If this information is unavailable or indeterminate, the worst-case conditions should be assumed.

Note: For ungrounded AC and DC systems, C_G represents the number of return conductors to the power source associated with the circuit of interest (e.g., the negative polarity conductors for an ungrounded 125 VDC circuit)

2. Calculate CF as follows.

Non-armored cables: $CF = \{C_T \times [C_S + (0.5 / C_{Tot})]\} / C_{Tot}$

Armored cables: $CF = (C_T \times C_S) / C_{Tot}$

Where:

C_S = The total number of source conductors in the cable under evaluation,

C_T = The total number of target conductors in the cable², and

C_{Tot} = The total number of conductors in the cable, as before.

Note: CF should be ≤ 1.0 . If the calculated value of CF is greater than 1, then set $CF = 1$. In practical applications it is highly unlikely that the calculated value of CF will ever exceed 1. For this to occur, virtually all conductors in the cable would need to be either a source conductor or target conductor.

Note: The analyst should determine the number of target and source conductors based on the circuit configuration (contact positions, etc.) that represents the normal operating state of the component. If this information is unavailable or indeterminate, the worst-case conditions should be assumed.

3. Calculate P_{FM} as follows:

$$P_{FM} = CF \times P_{CC},$$

where CF and P_{CC} are determined using the formulas discussed above.

4. When more than one cable can cause the component failure mode of concern, and those cables are within the boundary of influence for the scenario under investigation, the

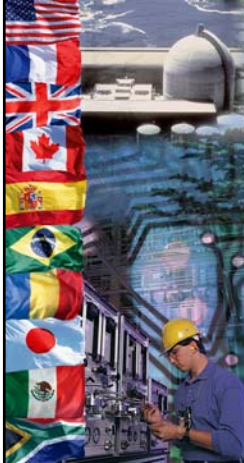
²Target conductors are only those cable conductors capable of forcing the component or circuit into the undesired state or condition of interest. For example, the target conductors associated with causing a spurious operation of the component will likely differ from target conductors associated with causing a loss of control condition.

probability estimates associated with all affected cables should be considered in deriving a failure estimate for the component. In general, the probabilities should be combined as follows:

$$P_{\text{Component failure}} = (P_{\text{Failure Cable A}}) + (P_{\text{Failure Cable B}}) - (P_{\text{Failure Cable A}})(P_{\text{Failure Cable B}})$$

Tab 3.5:

Task B FPRA Database



EPRI/NRC-RES FIRE PRA METHODOLOGY

Module 2: Support Task B - Fire PRA Database

D. Funk - Edan Engineering Corp.
F. Wyant - Sandia National Laboratories

Joint RES/EPRI Fire PRA Course
July and August 2007
Palo Alto, CA

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FIRE PRA DATABASE Purpose & Scope

- Identify Required Database Functionality
- Assess Capability of Existing Systems
- Implement Structured Process to Obtain the Required Database Capability
- New Software and Data Management Tools are Finding Their Way Into the Market

FIRE PRA DATABASE

Introduction

- Task is Distinctly Different from Other Tasks
- Essential Element of PRA
 - Proposed Methods Require Manipulation and Correlation of Large Amounts of Data
 - Must be Efficient and User Friendly for Effective Implementation
 - Manual Analysis Not Practical

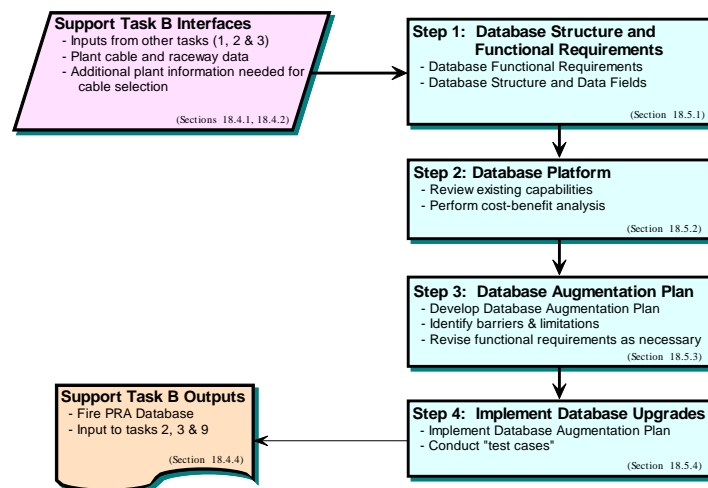
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FIRE PRA DATABASE

Flowchart



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FIRE PRA DATABASE

Step 1.1 - Database Functional Criteria

- Data Input Criteria
 - In what shape and format is existing data?
 - How and who will entered and control data?
 - Will data be shared by separate groups? If so, who can change data?
- Data Output Criteria
 - Define Required Output Reports
 - Define Sort and Query Options

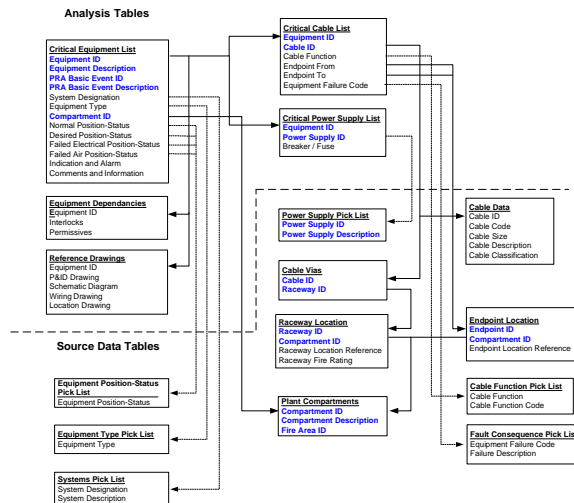
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FIRE PRA DATABASE

Step 1.2 - Database Structure (Example A)



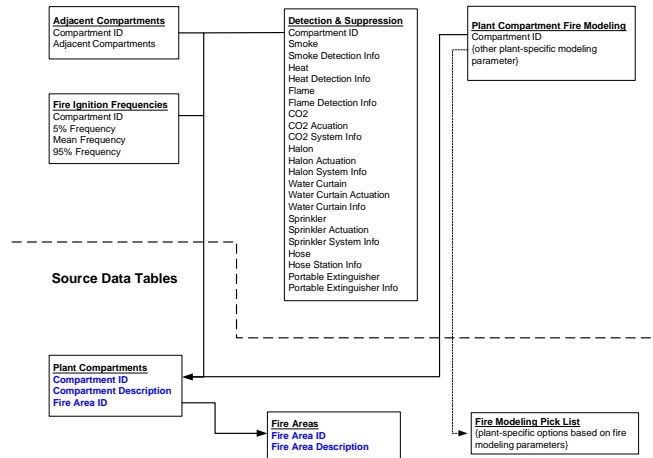
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FIRE PRA DATABASE Step 1.2 - Database Structure (Example A)

Analysis Tables



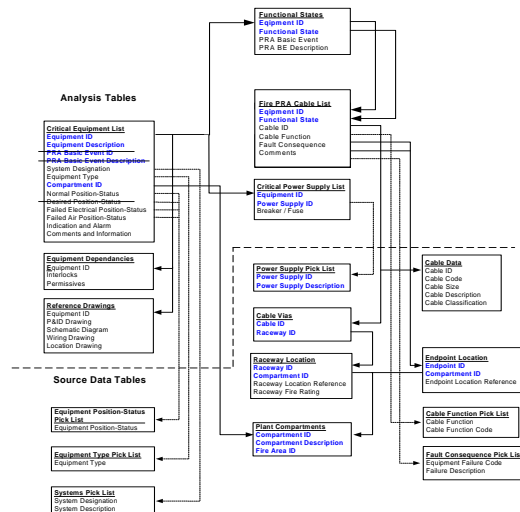
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FIRE PRA DATABASE Step 1.2 - Database Structure (Example B)

Analysis Tables



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FIRE PRA DATABASE

Step 2 - Database Platform

- Decide on Platform for Database
 - Existing System
 - New Stand Alone System
 - Upgrade Existing System
 - Combination of Existing and New
- Vendors are Responding to the Call for New and Improved Software Functionality
 - Highly Integrated Solutions are Emerging as the Standard for NFPA 805 Plants
 - Seamless Link to Fire PRA Software is in the Works But Not Yet Available as Production Software

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FIRE PRA DATABASE

Step 3 - Database Augmentation Plan

- Augmentation Plan is Based on the Results of Step 2
- Formalize Process for Upgrades/Changes
- Determine Necessary Resources
 - This Effort Can Innocently Affect Many Plant Organizations
 - The Cost, Resources, Schedule, Training, Procedural Changes and Overall Impact of Major Software Changes **ALWAYS** Seems to be Underestimated
- Involve IS/IT Department from the Beginning

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FIRE PRA DATABASE

Step 4 – Implement Database Upgrades

- Have a Clear Plan BEFORE Beginning any Significant Work
- Consider Long-Term Maintainability
- Plan for De-bugging and Test Runs
- Do Not Overlook Data Integrity and Configuration Control Features
- Determine All Affected Users and Involve Them Early
- The Days of “Rogue” PRA Databases are Gone!

Tab 3.6:

Electrical Analysis Examples



EPRI/NRC-RES FIRE PRA METHODOLOGY

Module 2: Electrical Examples

D. Funk - Edan Engineering Corp.
F. Wyant - Sandia National Laboratories

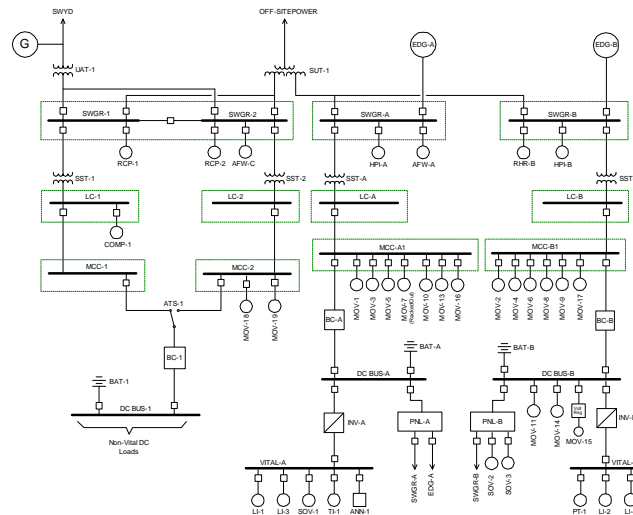
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OVERVIEW OF EXAMPLES

- Provide Hands-On Practical Experience
- Cover Many (But Not All) Typical Cases
- Exposure to Typical Problems and Decisions
- Appreciation for Challenges and Trade-Offs
- A Worn Out Expression, Yes...But for Circuit Analysis the “Devil is in the Details”

SNPP ONE-LINE DIAGRAM



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EXAMPLE PROBLEMS

Example No.	Component	Description of Analysis	NUREG/CR-6850	Comments
1	AOV-1 (SOV-1)	Std AC Solenoid Control Circuit	No	Multi-function component - analyzed for open and close
2	AOV-3 (SOV-3)	Std DC Solenoid Control Circuit	Yes - Figure I-2	Spurious only analysis
3	MOV-9	Typical MOV Control Circuit	Yes - Figure I-4	Functional analysis - change of position required
4	MOV-15	Double Pole DC Motor Control Circuit	Yes - Figure I-6	Functional analysis - change of position required
5	MOV-13	Ungrd AC, Inverted MOV Control Circuit	Yes - Figure I-8	Functional analysis - change of position required
6	MOV-10	Ungrd AC MOV Control Circuit	Yes - Figure I-10	Functional analysis - change of position required
7	MOV-8	MOV Control Circuit w/ Dual Controls	Yes - Figure I-12	Spurious only, classified as high consequence component
8	MOV-11	Typical DC MOV Control Circuit	No	Functional analysis - change of position required
9	MOV-16	Typical MOV Control Circuit	Yes - Figure I-4	Spurious Only
10	PI-1	Instrument Circuit	No	Indication only
11	ANN-1	Annunciator Circuit	No	No false indication
12	HPI-B	4.16 kV Motor	No	Functional analysis
13	COMP-1	480 V Motor	No	Functional analysis
14	SWGR-B	4.16 kV Bus	No	Multiple source options
15	LC-B	480V LC	No	Functional analysis
16	MCC-1B	480V MCC	No	Functional analysis

Joint Fire PRA Course, Sept. & Nov. 2008
Module 2: Electrical Examples

Slide 4

A Collaboration of U.S. NRC Office of Nuclear Regulatory Research (RES) & Electric Power Research Institute (EPRI)

HANDS ON WORK

CIRCUIT ANALYSIS WORKSHEET

Component ID _____ Component Type _____
 Component Description _____

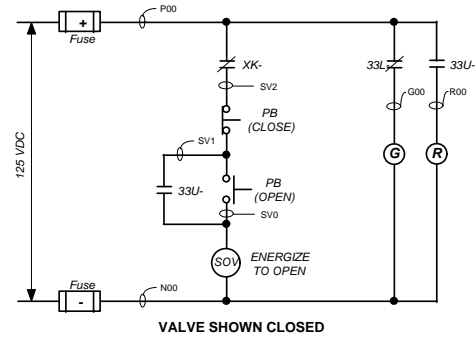
BE Code: _____
 Required Position: _____
 Functional State: _____
 Normal Position: _____
 Failed Electrical Position: _____
 Failed Air Position: _____
 High Consequence Component: Yes ☐ No ☐

Power Supplies: _____ Breaker: _____
 _____ Breaker: _____

Cable Analysis

Cable ID	Required?	Function	Fault Consequence	Comments

Comments



Joint Fire PRA Course, Sept. & Nov. 2008
Module 2: Electrical Examples

Slide 5

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 Research (RES) & Electric Power Research Institute (EPRI)

Tab 3.7:

Electrical Examples Summary and Loss Report

Circuit Analysis Example Summary

Example No.	Component	Description of Analysis	NUREG/CR-6850	Comments
1	AOV-1 (SOV-1)	Std AC Solenoid Control Circuit	No	Multi-function component - analyzed for open and close
2	AOV-3 (SOV-3)	Std DC Solenoid Control Circuit	Yes - Figure I-2	Spurious only analysis
3	MOV-9	Typical MOV Control Circuit	Yes - Figure I-4	Functional analysis - change of position required
4	MOV-15	Double Pole DC Motor Control Circuit	Yes - Figure I-6	Functional analysis - change of position required
5	MOV-13	Ungnd AC, Inverted MOV Control Circuit	Yes - Figure I-8	Functional analysis - change of position required
6	MOV-10	Ungnd AC MOV Control Circuit	Yes - Figure I-10	Functional analysis - change of position required
7	MOV-8	MOV Control Circuit w/ Dual Controls	Yes - Figure I-12	Spurious only, classified as high consequence component
8	MOV-11	Typical DC MOV Control Circuit	No	Functional analysis - change of position required
9	MOV-16	Typical MOV Control Circuit	Yes - Figure I-4	Spurious Only
10	PI-1	Instrument Circuit	No	Indication only
11	ANN-1	Annunciator Circuit	No	No false indication
12	HPI-B	4.16 kV Motor	No	Functional analysis
13	COMP-1	480 V Motor	No	Functional analysis
14	SWGR-B	4.16 kV Bus	No	Multiple source options
15	LC-B	480V LC	No	Functional analysis
16	MCC-1B	480V MCC	No	Functional analysis

CIRCUIT ANALYSIS WORKSHEET

Component ID: _____

Continuation Sheet (___ of ___)

Cable Analysis:

[illegible]

CIRCUIT ANALYSIS WORKSHEET

Component ID: _____ Component Type: _____

Component Description: _____

BE Code: _____

Required Position: _____
Functional State

Normal Position: _____

Failed Electrical Position: _____

Failed Air Position: _____

High Consequence Component Yes ☐ No ☐

Power Supplies: _____ Breaker: _____

_____ Breaker: _____

Cable Analysis:

Cable ID	Required?	Function	Fault Consequence	Comments

Comments:

Table 1: Target Equipment Loss Report

Equipment ID	Equipment Description	Equipment Type	Location	Desired Position/Status	Target Loss Locations
HPI-A	High pressure safety injection pump A	Pump	Aux Bldg. El. 0 Ft	On	1, 2, 3, 10
				On	1, 2, 3, 10
HPI-B	High pressure safety injection pump B	Pump	Aux Bldg. El. 0 Ft	On	1, 2, 3, 11
				On	1, 2, 3, 11
RHR-B	Residual heat removal pump B	Pump	Aux Bldg. El. -20 Ft	Off	1, 2, 3, 4A, 9, 11
AFW-A	Motor driven AFW pump A	Pump	Aux Bldg. EL. 0 Ft	On	1, 3, 4B, 9, 10
AFW-B	Steam driven AFW pump B	Pump	Aux Bldg. EL. 0 Ft	On	1, 3, 4B, 9, 11
AFW-C	Motor driven AFW pump C	Pump	Turbine Bldg. El. 0 Ft	On	1, 3, 12
RCP-1	Reactor coolant pump 1	Pump	Containment	Off	1, 2, 3, 7, 12
RCP-2	Reactor coolant pump 2	Pump	Containment	Off	1, 2, 3, 7, 12
COMP-1	Instrument air compressor	Compressor	Turbine Bldg. El. 0 Ft	Cycle	12
AOV-1 (SOV-1)	Power operated relief valve	AOV	Containment	Closed	1, 3, 7, 9
				Open	1, 3, 7, 9, 10
AOV-2 (SOV-2)	Letdown isolation valve	AOV	Aux Bldg. El. 0 Ft	Closed	1, 2, 3, 9
AOV-3 (SOV-3)	Charging pump injection valve	AOV	Aux Bldg. El. 0 Ft	Closed	1, 2, 3, 9
MOV-1	HPI discharge valve	MOV	Aux Bldg. El. 0 Ft	Open	1, 2, 3, 9, 10
MOV-2	VCT isolation valve	MOV	Aux Bldg. El. 0 Ft	Closed	1, 2, 3, 9, 11
MOV-3	Cont. sump recirc valve	MOV	Aux Bldg. El. -20 Ft	Open/ Closed ²	1, 2, 3, 4A, 9, 10
MOV-4	Cont. sump recirc valve	MOV	Aux Bldg. El. -20 Ft	Open/ Closed	1, 2, 3, 4A, 9, 11
MOV-5	RWST isolation valve	MOV	Aux Bldg. El. 0 Ft	Open	1, 2, 3, 12
MOV-6	RWST isolation valve	MOV	Aux Bldg. El. 0 Ft	Open	1, 2, 3, 12
MOV-7	RHR inboard suction valve	MOV	Containment	Closed	4A,7,9,12
MOV-8	RHR outboard suction valve	MOV	Aux Bldg. El. -20 Ft	Closed	4A,9,12
MOV-9	HPI discharge valve	MOV	Aux Bldg. El. 0 Ft	Open	1,2,3,,9
MOV-10	AFW pump A discharge valve	MOV	Aux Bldg. EL. 0 Ft	Open	1,3,4B,9,12
MOV-11	AFW pump B discharge valve	MOV	Aux Bldg. EL. 0 Ft	Open	1,3,4B,9,11,12
MOV-13	PORV block valve	MOV	Containment	Open/ Closed ¹	1, 3, 7, 9
MOV-14	AFW pump B turbine steam line isolation valve	MOV	Turbine Bldg. El. 0 Ft	Open	1, 3, 4B, 12

Equipment ID	Equipment Description	Equipment Type	Location	Desired Position/ Status	Target Loss Locations
MOV-15	AFW pump B steam inlet throttle valve	MOV	Turbine Bldg. El. 0 Ft	Throttled	1, 3, 4B, 12
MOV-16	AFW pump A test line isolation valve	MOV	Turbine Bldg. El. 0 Ft	Closed	2, 4B, 9
MOV-17	AFW pump B test line isolation valve	MOV	Turbine Bldg. El. 0 Ft	Closed	2, 4B, 9
MOV-18	AFW pump C discharge valve	MOV	Turbine Bldg. El. 0 Ft	Open	1, 3, 12
MOV-19	AFW pump C test line isolation valve	MOV	Turbine Bldg. El. 0 Ft	Closed	1, 3, 12
V-12	CST isolation valve	MOV	Turbine Bldg. El. 0 Ft	Open	12
LI-1	RWST level	Instrument	Yard	Available	1, 3, 12, 13
LI-2	RWST level	Instrument	Yard	Available	1, 3, 12, 13
LI-3	Cont. sump level	Instrument	Containment	Available	1, 3, 7, 12
LI-4	Cont. sump level	Instrument	Containment	Available	1, 3, 7, 12
TI-1	Letdown heat exchanger outlet temperature	Instrument	Aux Bldg El. 0 Ft	Available	1, 2, 3, 9
PT-1	RCS pressure	Instrument	Containment	Available	1, 3, 7
ANN-1	AFW motor high temperature	Annunciator	SWG Access Room	Non spurious	1, 2, 3, 9, 4B
SWGR-A	Train A 4160 V switchgear	Switchgear	Switchgear Room A	Energized from SUT-1	1, 3, 10, 12, 13
				Energized from EDG-A	1, 3, 8A, 10, 12
SWGR-B	Train B 4160 V switchgear	Switchgear	Switchgear Room B	Energized from SUT-1	1, 3, 9, 11, 12, 13
				Energized from EDG-A	1, 3, 8B, 9, 11, 12
SWGR-1	Non-safety 4160 V switchgear	Switchgear	Turbine Bldg. El. 0ft	Energized	1, 3, 12, 13
SWGR-2	Non-safety 4160 V switchgear	Switchgear	Turbine Bldg. El. 0ft	Energized	1, 3, 12, 13
SUT-1	Startup transformer	Transformer	Yard	Energized	1, 3, 12, 13
EDG-A	Train A emergency diesel generator	Diesel Generator	DG Bldg.	On	1, 3, 8A, 10, 12
EDG-B	Train B emergency diesel generator	Diesel Generator	DG Bldg.	On	1, 3, 8B, 10, 12
LC-1	Non-safety 480 V load center	Load Center	Turbine Bldg. El. 0 ft	Energized	1, 3, 12
LC-2	Non-safety 480 V load center	Load Center	Turbine Bldg. El. 0 ft	Energized	1, 3, 12
LC-A	Train A 480 V load center	Load Center	Switchgear Room A	Energized	1, 3, 10
LC-B	Train B 480 V load center	Load Center	Switchgear Room B	Energized	1, 3, 11
SST-1	Non-safety station service transformer	Transformer	Turbine Bldg. El. 0 F	Energized	12

Equipment ID	Equipment Description	Equipment Type	Location	Desired Position/ Status	Target Loss Locations
SST-2	Non-safety station service transformer	Transformer	Turbine Bldg. El. 0 F	Energized	12
SST-A	Train A station service transformer	Transformer	Switchgear Room A	Energized	10
SST-B	Train B station service transformer	Transformer	Switchgear Room B	Energized	11
MCC-1	Non-safety 480 V motor control center	Motor Control Center	Turbine Bldg El. 0 Ft	Energized	12
MCC-2	Non-safety 480 V motor control center	Motor Control Center	Turbine Bldg El. 0 Ft	Energized	12
MCC-A1	Train A 480 V motor control center	Motor Control Center	SWG Access Room	Energized	9, 10
MCC-B1	Train B 480 V motor control center	Motor Control Center	SWG Access Room	Energized	9, 11
ATS-1	Automatic transfer switch	ATS	SWG Access Room	Energized from MCC-1	12
BC-1	Non-safety swing battery charger	Battery Charger	Turbine Bldg El. 0 Ft	Energized	12
BC-A	Train A battery charger	Battery Charger	Switchgear Room A	Energized	9, 10
BC-B	Train B battery charger	Battery Charger	Switchgear Room B	Energized	9, 11
BAT-1	Non-safety battery	Battery	Turbine Bldg El. 0 Ft	Available	12, 15
BAT-A	Train A battery	Battery	Battery Room A	Available	5, 10
BAT-B	Train B battery	Battery	Battery Room B	Available	6, 11
DC BUS-1	Non-safety 250 VDC bus	DC Bus	Turbine Bldg El. 0 Ft	Energized	12
DC BUS-A	Train A 125 VDC bus	DC Bus	Switchgear Room A	Energized	10
DC BUS-B	Train B 125 VDC bus	DC Bus	Switchgear Room B	Energized	11
PNL-A	Train A 125 VDC panel	Panelboard	Switchgear Room A	Energized	10
PNL-B	Train B 125 VDC panel	Panelboard	Switchgear Room B	Energized	11
INV-A	Train A inverter	Inverter	Switchgear Room A	Energized	3, 9, 10
INV-B	Train B inverter	Inverter	Switchgear Room B	Energized	3, 9, 11
VITAL-A	Train A 120 VAC vital bus	120VAC Bus	SWG Access Room	Energized	9, 10
VITAL-B	Train B 120 VAC vital bus	120VAC Bus	SWG Access Room	Energized	9, 11

Tab 3.8:

Circuit Analysis Worksheets

CIRCUIT ANALYSIS WORKSHEET

Component ID: **LC-B** Component Type: **Load Center**

Component Description: **Train B 480 V Load Center**

BE Code: **EPS-480VLCBF (480V LOAD CENTER B FAULT)**

Required Position: **ENERGIZED**
Functional State

Normal Position: **ENERGIZED**

Failed Electrical Position: **Off**

Failed Air Position: **N/A**

High Consequence Component Yes ☐ No ☒

Power Supplies: _____ Breaker: _____
_____ Breaker: _____

Cable Analysis:

Cable ID	Required?	Function	Fault Consequence	Comments

Comments:

CIRCUIT ANALYSIS WORKSHEET

Component ID: **SWGR-B** Component Type: **Switchgear**
Component Description: **Train B 4160V Switchgear**

BE Code: **PNL-B EPS-4VBUSBF-2 (4KV BUS B FAULT)**
Required Position: **ENERGIZED FROM EDG-B**
Functional State
Normal Position: **ENERGIZED FROM SUT-1**
Failed Electrical Position: **Off**
Failed Air Position: **N/A**
High Consequence Component Yes ☐ No ☒

Power Supplies: _____ Breaker: _____
_____ Breaker: _____

Cable Analysis:

Cable ID	Required?	Function	Fault Consequence	Comments

Comments:

CIRCUIT ANALYSIS WORKSHEET

Component ID: **SWGR-B** Component Type: **Switchgear**
Component Description: **Train B 4160V Switchgear**

BE Code: **PNL-B EPS-4VBUSBF-1 (4KV BUS B FAULT)**
Required Position: **ENERGIZED FROM SUT-1**
Functional State
Normal Position: **ENERGIZED FROM SUT-1**
Failed Electrical Position: **Off**
Failed Air Position: **N/A**
High Consequence Component Yes ☐ No ☒

Power Supplies: _____ Breaker: _____
_____ Breaker: _____

Cable Analysis:

Cable ID	Required?	Function	Fault Consequence	Comments

Comments:

CIRCUIT ANALYSIS WORKSHEET

Component ID: **COMP-1** Component Type: **Compressor**
Component Description: **Instrument Air Compressor**

BE Code: **COMP-1_FTR (COMP-1 Fails to Run)**
Required Position: **CYCLE**
Functional State
Normal Position: **CYCLE**
Failed Electrical Position: **Off**
Failed Air Position: **N/A**
High Consequence Component Yes ☐ No ☒

Power Supplies: _____ Breaker: _____
_____ Breaker: _____

Cable Analysis:

Cable ID	Required?	Function	Fault Consequence	Comments

Comments:

CIRCUIT ANALYSIS WORKSHEET

Component ID: **HPI-B**

Component Type: **Pump**

Component Description: **High Pressure Injection Pump B**

BE Code: **HPIA_FTS (HPI-A Fails to Start)**
HPIA_FTR (HPI-A Fails to Run)

Required Position: **ON**
Functional State

Normal Position: **STANDBY / ON**

Failed Electrical Position: **Off**

Failed Air Position: **N/A**

High Consequence Component Yes ☐ No ☒

Power Supplies: _____ Breaker: _____

_____ Breaker: _____

Cable Analysis:

Cable ID	Required?	Function	Fault Consequence	Comments

Comments:

CIRCUIT ANALYSIS WORKSHEET

Component ID: **ANN-1**

Component Type: **Annunciator**

Component Description: **AFW Motor High Temperature**

BE Code: **ANN-1_FH (AFW Pump Motor Spurious High Ann)**

Required Position:
Functional State **NON-SPURIOUS**

Normal Position: **AVAILABLE**

Failed Electrical Position: **UNAVAILABLE**

Failed Air Position: **N/A**

High Consequence Component Yes ☐ No ☒

Power Supplies: _____ Breaker: _____

_____ Breaker: _____

Cable Analysis:

Cable ID	Required?	Function	Fault Consequence	Comments

Comments:

CIRCUIT ANALYSIS WORKSHEET

Component ID: **PI-1** Component Type: **Instrument**

Component Description: **RCS Pressure**

BE Code: **PI-1_FL (RCS Pressure Indication Fails High)**

Required Position: **AVAILABLE**
Functional State

Normal Position: **AVAILABLE**

Failed Electrical Position: **LOW**

Failed Air Position: **N/A**

High Consequence Component Yes ☐ No ☒

Power Supplies: _____ Breaker: _____
_____ Breaker: _____

Cable Analysis:

Cable ID	Required?	Function	Fault Consequence	Comments

Comments:

CIRCUIT ANALYSIS WORKSHEET

Component ID: **MOV-16**

Component Type: **MOV**

Component Description: **AFW Test Line Isolation Valve**

BE Code: **MOV-16_TO (MOV-16 TRANSFERS OPEN)**

Required Position: **CLOSED**
Functional State

Normal Position: **CLOSED**

Failed Electrical Position: **AS-IS**

Failed Air Position: **N/A**

High Consequence Component Yes ☐ No ☒

Power Supplies: _____ Breaker: _____

_____ Breaker: _____

Cable Analysis:

Cable ID	Required?	Function	Fault Consequence	Comments

Comments:

CIRCUIT ANALYSIS WORKSHEET

Component ID: **MOV-11** Component Type: **MOV**

Component Description: **AFW Discharge Isolation Valve**

BE Code: **MOV-11_FTO (MOV-11 FAILS TO OPEN)**

Required Position: **OPEN**
Functional State

Normal Position: **CLOSED**

Failed Electrical Position: **AS-IS**

Failed Air Position: **N/A**

High Consequence Component Yes ☐ No ☒

Power Supplies: _____ Breaker: _____
_____ Breaker: _____

Cable Analysis:

Cable ID	Required?	Function	Fault Consequence	Comments

Comments:

CIRCUIT ANALYSIS WORKSHEET

Component ID: **MOV-8**

Component Type: **MOV**

Component Description: **RHR Outboard Suction Valve**

BE Code: **MOV-8_TO (MOV-8 TRANSFERS OPEN)**

Required Position: **CLOSED**
Functional State

Normal Position: **CLOSED**

Failed Electrical Position: **AS-IS**

Failed Air Position: **N/A**

High Consequence Component Yes ☒ No ☐

Power Supplies: _____ Breaker: _____

_____ Breaker: _____

Cable Analysis:

Cable ID	Required?	Function	Fault Consequence	Comments

Comments:

CIRCUIT ANALYSIS WORKSHEET

Component ID: **MOV-10**

Component Type: **MOV**

Component Description: **AFW Discharge Isolation Valve**

BE Code: **MOV-10_FTO (MOV-10 FAILS TO OPEN)**

Required Position: **OPEN**
Functional State

Normal Position: **CLOSED**

Failed Electrical Position: **AS-IS**

Failed Air Position: **N/A**

High Consequence Component Yes ☐ No ☒

Power Supplies: _____ Breaker: _____

_____ Breaker: _____

Cable Analysis:

Cable ID	Required?	Function	Fault Consequence	Comments

Comments:

CIRCUIT ANALYSIS WORKSHEET

Component ID: **MOV-13** Component Type: **MOV**
Component Description: **PORV Block Valve**

BE Code: **MOV-13_FTC (MOV-13 FAILS TO CLOSE)**
Required Position: **OPEN / CLOSED**
Functional State
Normal Position: **OPEN**
Failed Electrical Position: **AS-IS**
Failed Air Position: **N/A**
High Consequence Component Yes ☐ No ☒

Power Supplies: _____ Breaker: _____
_____ Breaker: _____

Cable Analysis:

Cable ID	Required?	Function	Fault Consequence	Comments

Comments:

CIRCUIT ANALYSIS WORKSHEET

Component ID: **MOV-15**

Component Type: **MOV**

Component Description: **AFW Steam Inlet Throttle Valve**

BE Code: **MOV-15_FTO (MOV-15 FAILS TO OPEN)**

Required Position: **THROTTLED**
Functional State

Normal Position: **CLOSED**

Failed Electrical Position: **AS-IS**

Failed Air Position: **N/A**

High Consequence Component Yes ☐ No ☒

Power Supplies: _____ Breaker: _____

_____ Breaker: _____

Cable Analysis:

Cable ID	Required?	Function	Fault Consequence	Comments

Comments:

CIRCUIT ANALYSIS WORKSHEET

Component ID: **MOV-9** Component Type: **MOV**
Component Description: **High Pressure Injection Valve**

BE Code: **MOV-9_FTO (MOV-9 FAILS TO OPEN)**
Required Position: **OPEN**
Functional State
Normal Position: **CLOSED**
Failed Electrical Position: **AS-IS**
Failed Air Position: **N/A**
High Consequence Component Yes ☐ No ☒

Power Supplies: _____ Breaker: _____
_____ Breaker: _____

Cable Analysis:

Cable ID	Required?	Function	Fault Consequence	Comments

Comments:

Component ID:	AOV-3 (SOV-3)	Component Type:	AOV
Component Description:	Charging Pump Injection Valve		

BE Code:	AOV-3_FTC (AOV-3 FAILS TO CLOSE)
Required Position: Functional State	CLOSED
Normal Position:	OPEN
Failed Electrical Position:	CLOSED
Failed Air Position:	CLOSED
High Consequence Component	Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>

Power Supplies: _____	Breaker: _____
_____	Breaker: _____

Cable Analysis:

Cable ID	Required?	Function	Fault Consequence	Comments

Comments:

CIRCUIT ANALYSIS WORKSHEET

Component ID: **AOV-1 (SOV-1)** Component Type: **AOV**

Component Description: **Power Operated Relief Valve**

BE Code: **AOV-1_FTO (PORV AOV-1 FAILS TO OPEN)**

Required Position: **OPEN**
Functional State

Normal Position: **CLOSED**

Failed Electrical Position: **CLOSED**

Failed Air Position: **CLOSED**

High Consequence Component Yes ☐ No ☒

Power Supplies: _____ Breaker: _____
_____ Breaker: _____

Cable Analysis:

Cable ID	Required?	Function	Fault Consequence	Comments

Comments:

CIRCUIT ANALYSIS WORKSHEET

Component ID: **AOV-1 (SOV-1)** Component Type: **AOV**

Component Description: **Power Operated Relief Valve**

BE Code: **AOV-1_TO (PORV AOV-1 TRANSFERS OPEN)**

Required Position: **CLOSED**
Functional State

Normal Position: **CLOSED**

Failed Electrical Position: **CLOSED**

Failed Air Position: **CLOSED**

High Consequence Component Yes ☐ No ☒

Power Supplies: _____ Breaker: _____

_____ Breaker: _____

Cable Analysis:

Cable ID	Required?	Function	Fault Consequence	Comments

Comments:

CIRCUIT ANALYSIS WORKSHEET

Component ID: **MCC-1B** Component Type: **MCC**
Component Description: **Train B 480 V Motor Control Center**

BE Code: **EPS-480MCCB1F (480V MCC B1 FAULT)**
Required Position: **ENERGIZED**
Functional State
Normal Position: **ENERGIZED**
Failed Electrical Position: **Off**
Failed Air Position: **N/A**
High Consequence Component Yes ☐ No ☒

Power Supplies: _____ Breaker: _____
_____ Breaker: _____

Cable Analysis:

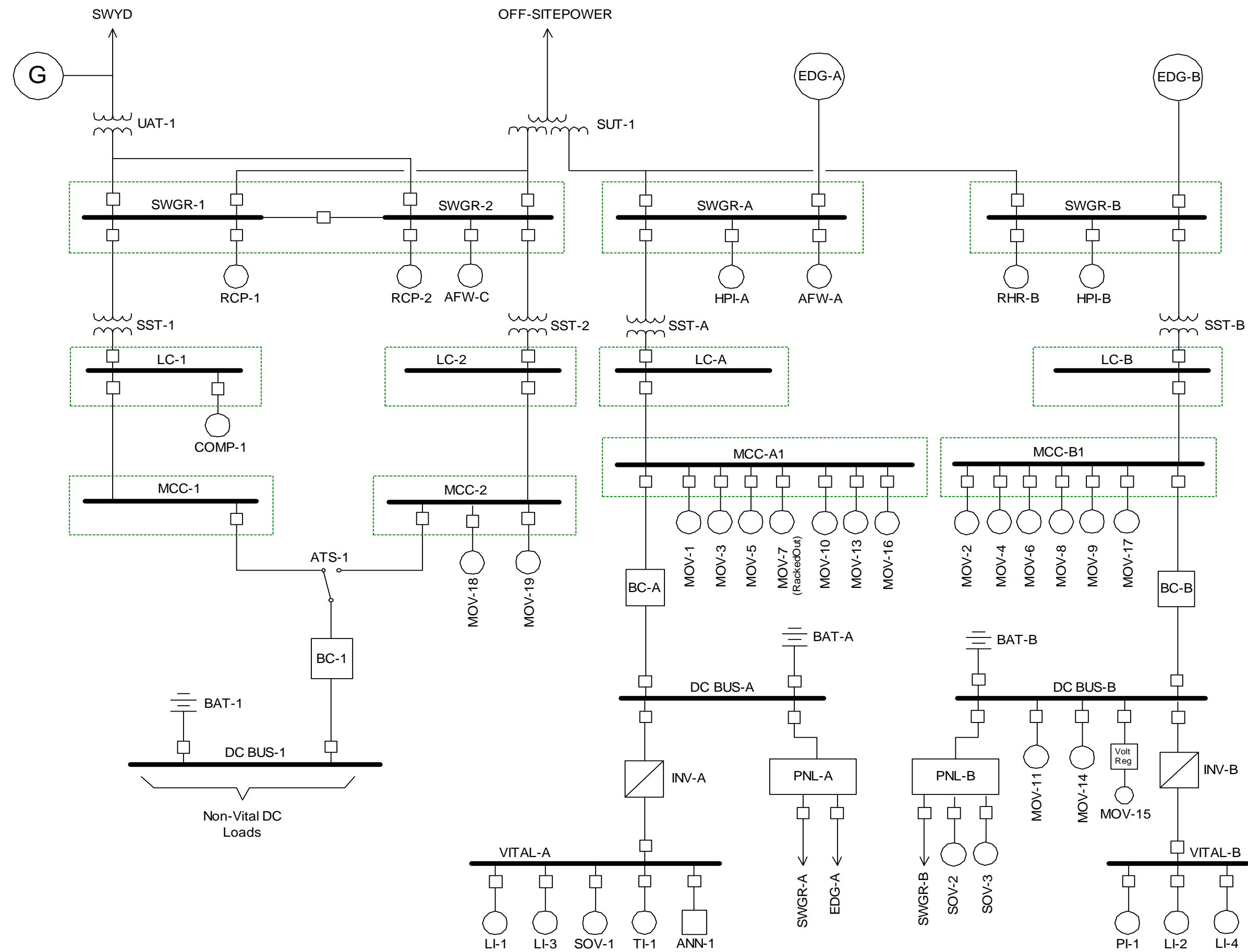
Cable ID	Required?	Function	Fault Consequence	Comments

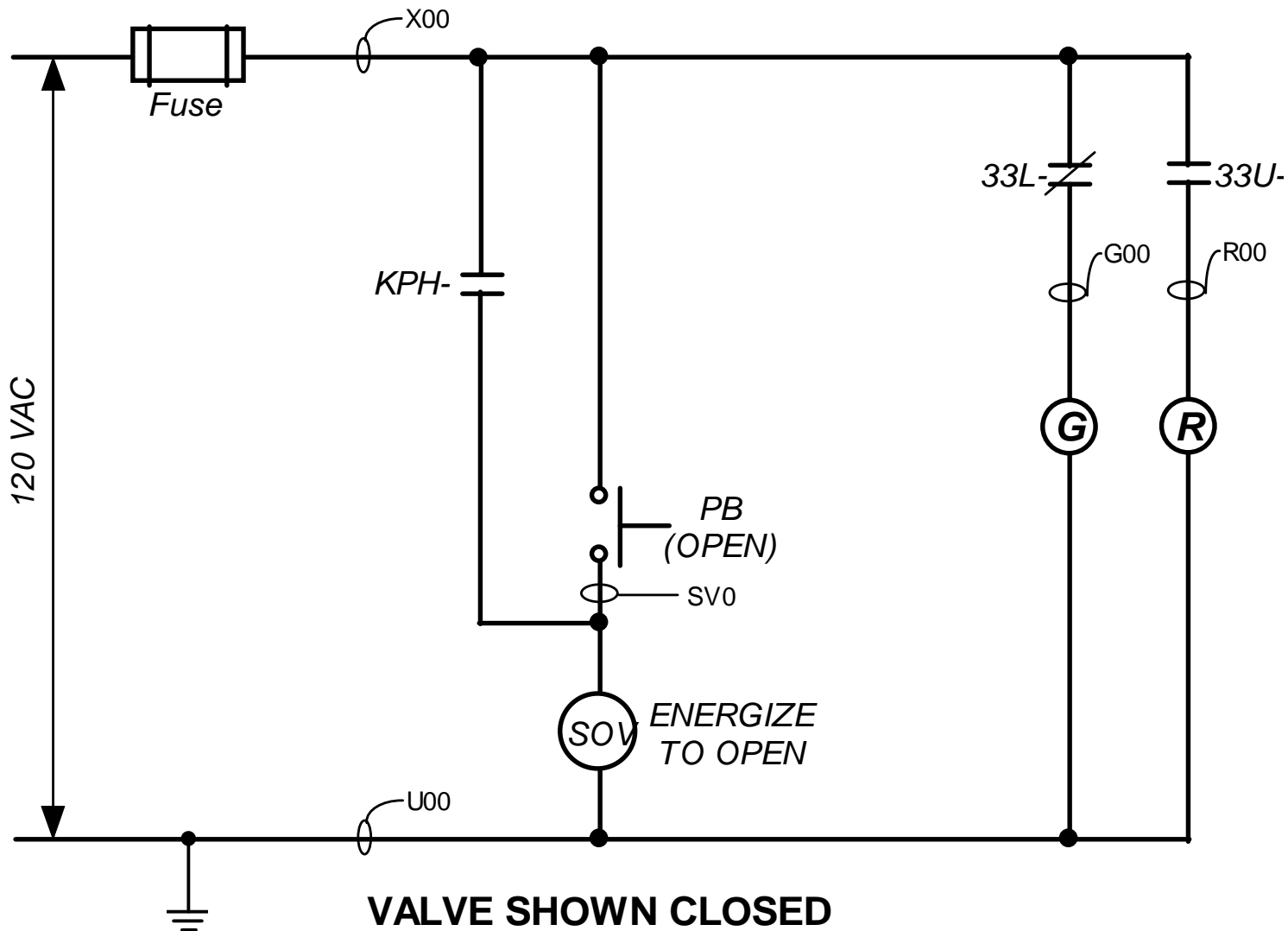
Comments:

Tab 3.9:

Drawing Package #1

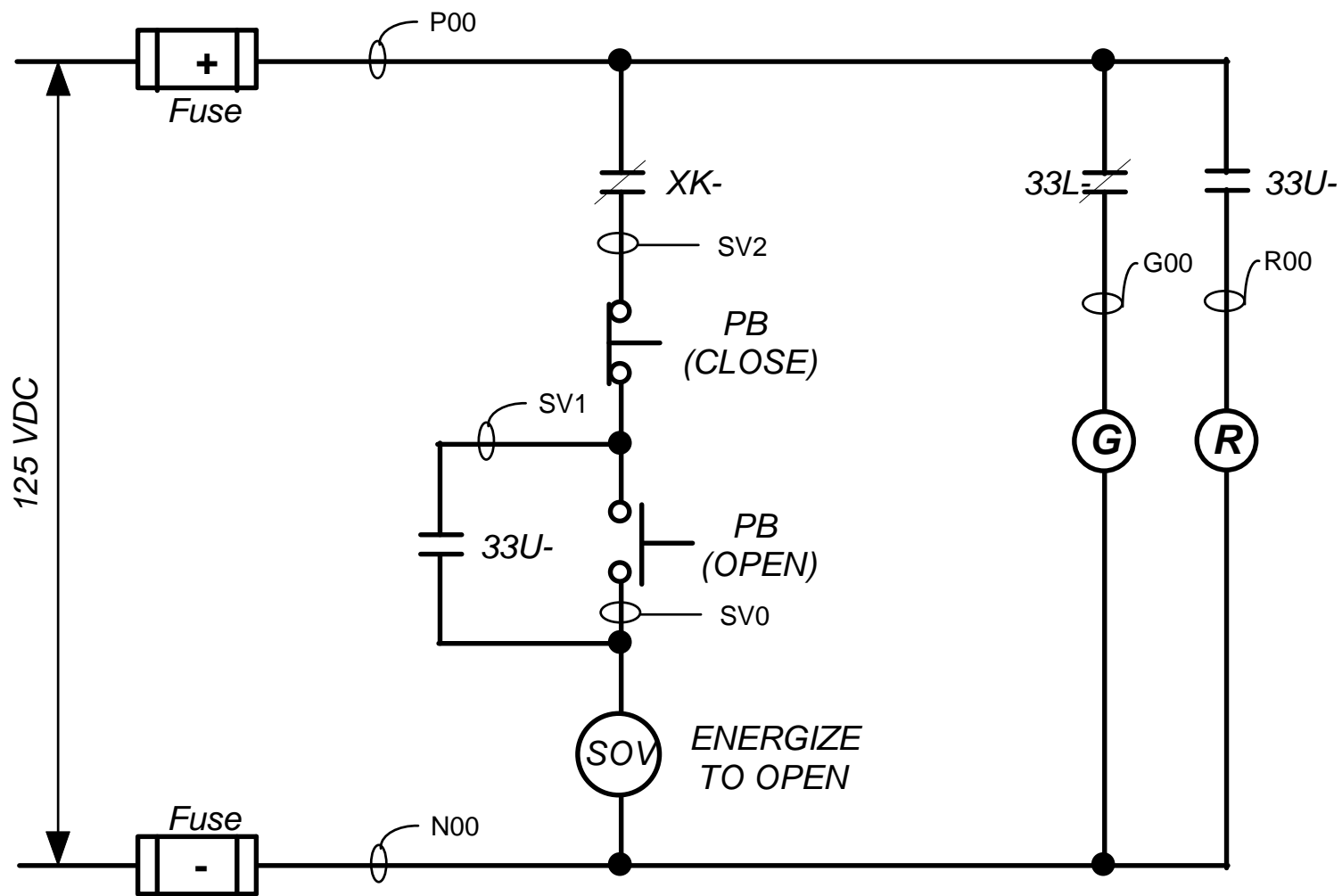
ELECTRICAL DISTRIBUTION SYSTEM - SIMPLIFIED ONE-LINE DIAGRAM





SCHEME VA3

SNPP SCHEMATIC DIAGRAM – PRESSURE OPERATED RELIEF SOLENOID VALVE SOV-1	Drawing No.:
	E-03
	Date:
	05/04/2007
	Revision No.:
	1



VALVE SHOWN CLOSED

VALVE	DESCRIPTION	SCHEME	SWITCH ID
SOV-2	LETDOWN ISOLATION	PB2	AOV-2
SOV-3	CHARGING PUMP INJECTION	PB3	AOV-3

SNPP

SCHEMATIC DIAGRAM --
PRIMARY MAKEUP SYSTEM
SOLENOID VALVES
SOV-2 & SOV-3

Drawing No.:

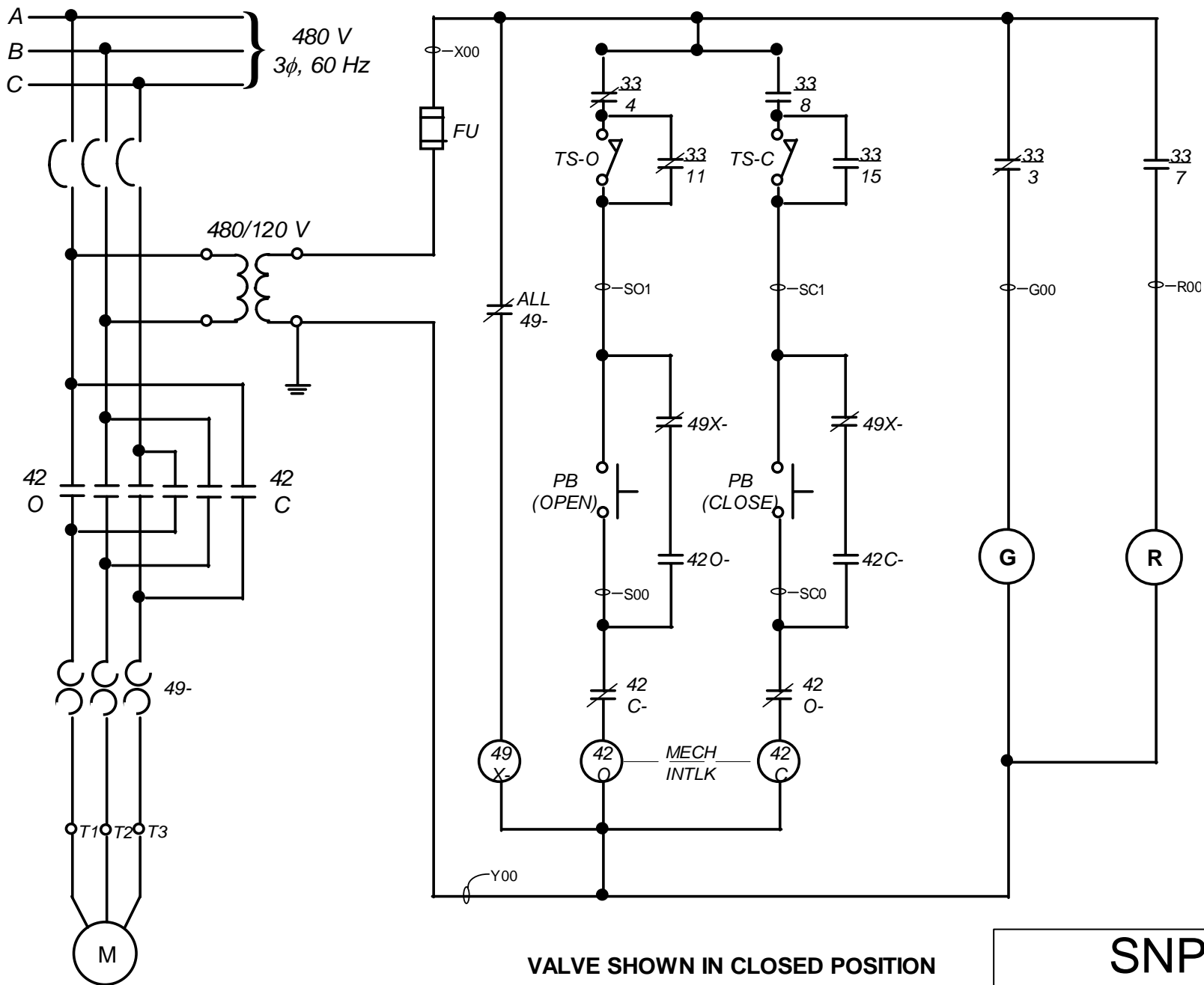
E-02

Date:

07/25/2008

Revision No.:

1



VALVE SHOWN IN CLOSED POSITION

VALVE	DESCRIPTION	SCHEME	SWITCH ID
MOV-1	HIGH PRESS INJECTION-A	MA12	MOV-1
MOV-9	HIGH PRESS INJECTION-B	MB15	MOV-9

SNPP

SCHEMATIC DIAGRAM – HIGH
PRESSURE INJECTION
MOTOR OPERATED VALVES
MOV-1 & MOV-9

Drawing No.:

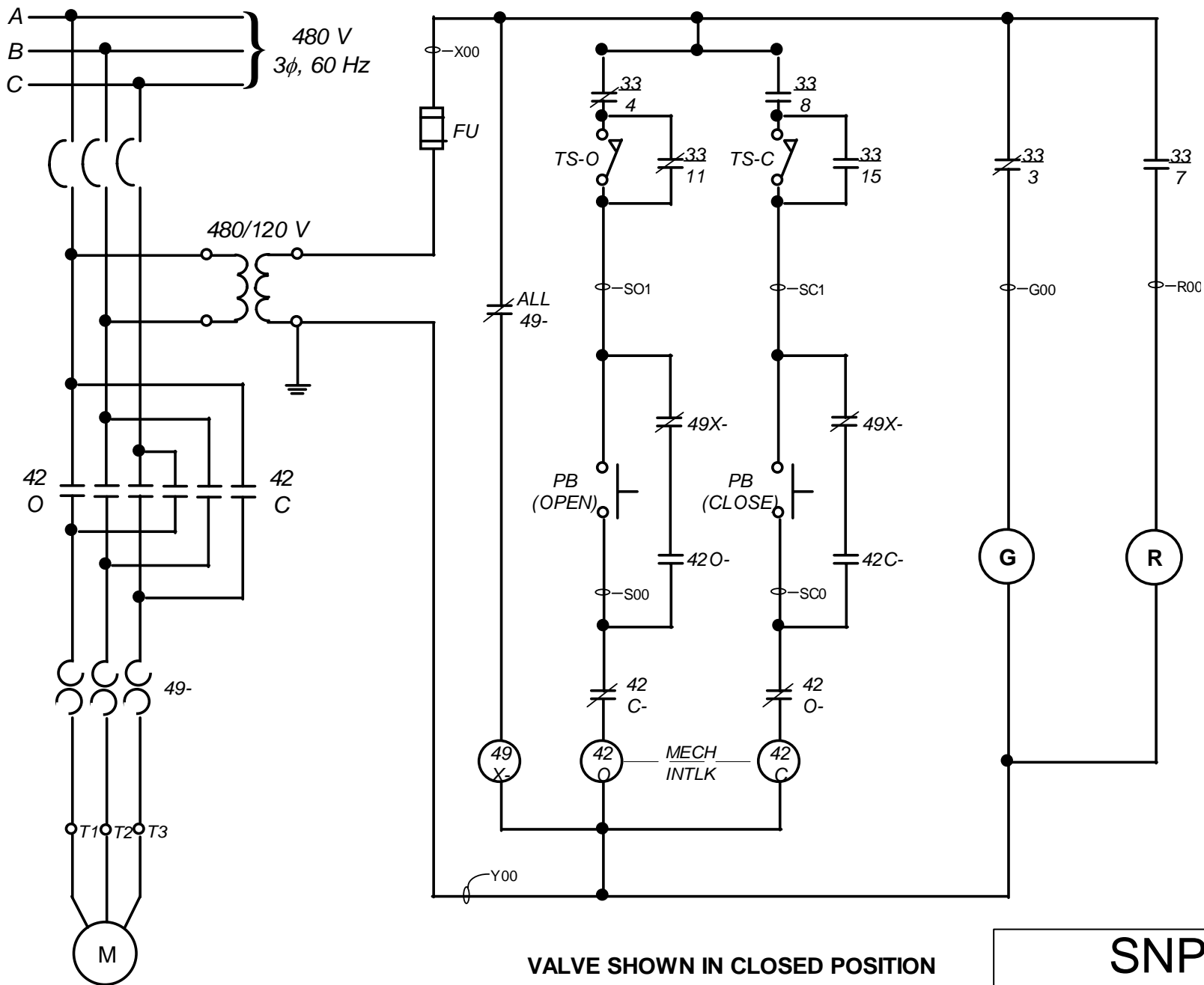
E-04

Date:

05/01/2007

Revision No.:

0



VALVE SHOWN IN CLOSED POSITION

VALVE	DESCRIPTION	SCHEME	SWITCH ID
MOV-16	AFW TEST LINE ISOLATION	MA18	MOV-16
MOV-17	AFW TEST LINE ISOLATION	MB16	MOV-17

SNPP

SCHEMATIC DIAGRAM – AFW
TEST LINE ISOLATION MOTOR
OPERATED VALVES
MOV-16 & MOV-17

Drawing No.:

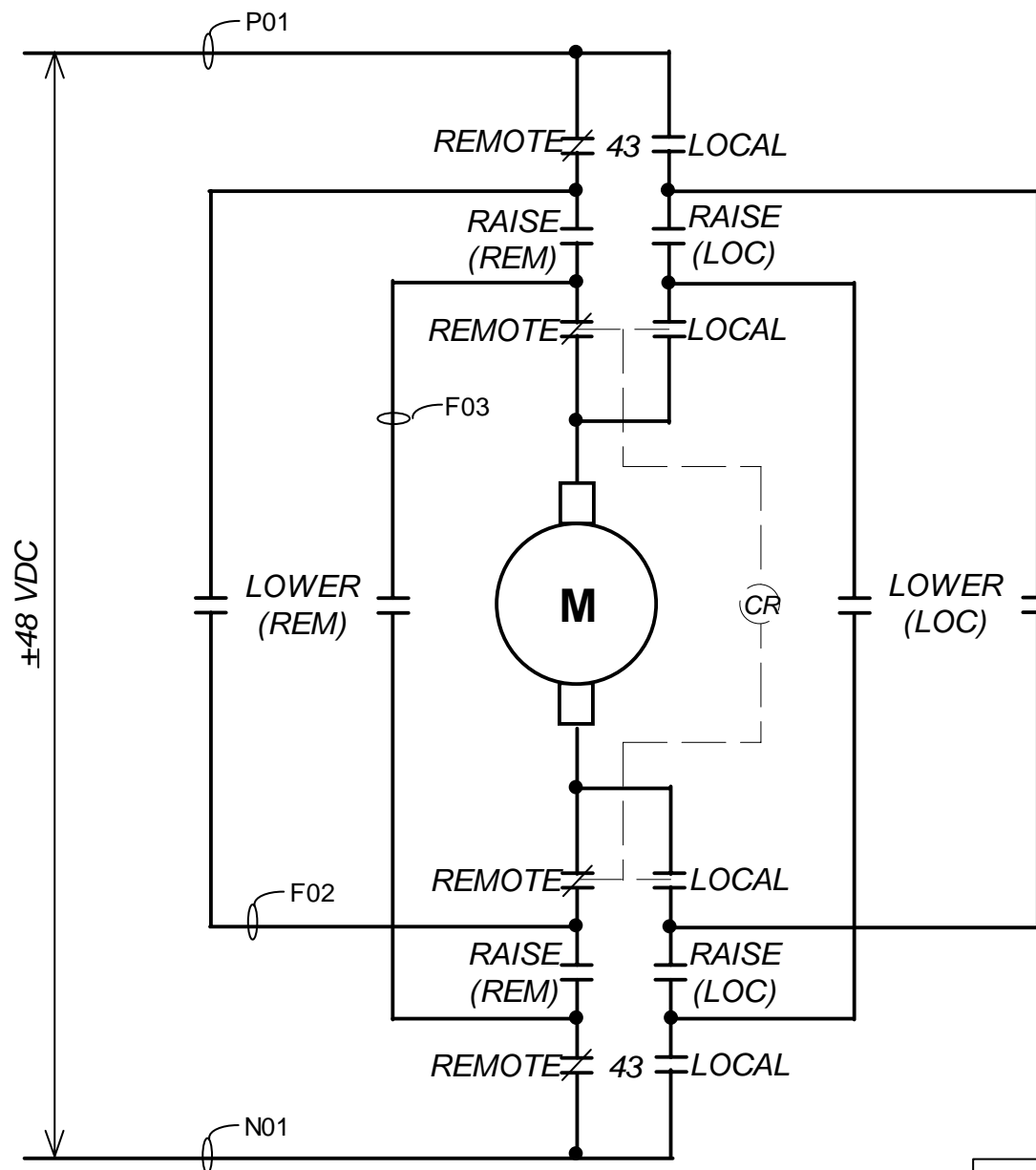
E-08

Date:

05/01/2007

Revision No.:

0



Motor Shown in Remote Operating Mode

MOV-15, SCHEME DB4

SNPP

SCHEMATIC DIAGRAM –
AFW- B STEAM THROTTLE
MOTOR OPERATED VALVE
MOV-15

Drawing No.:

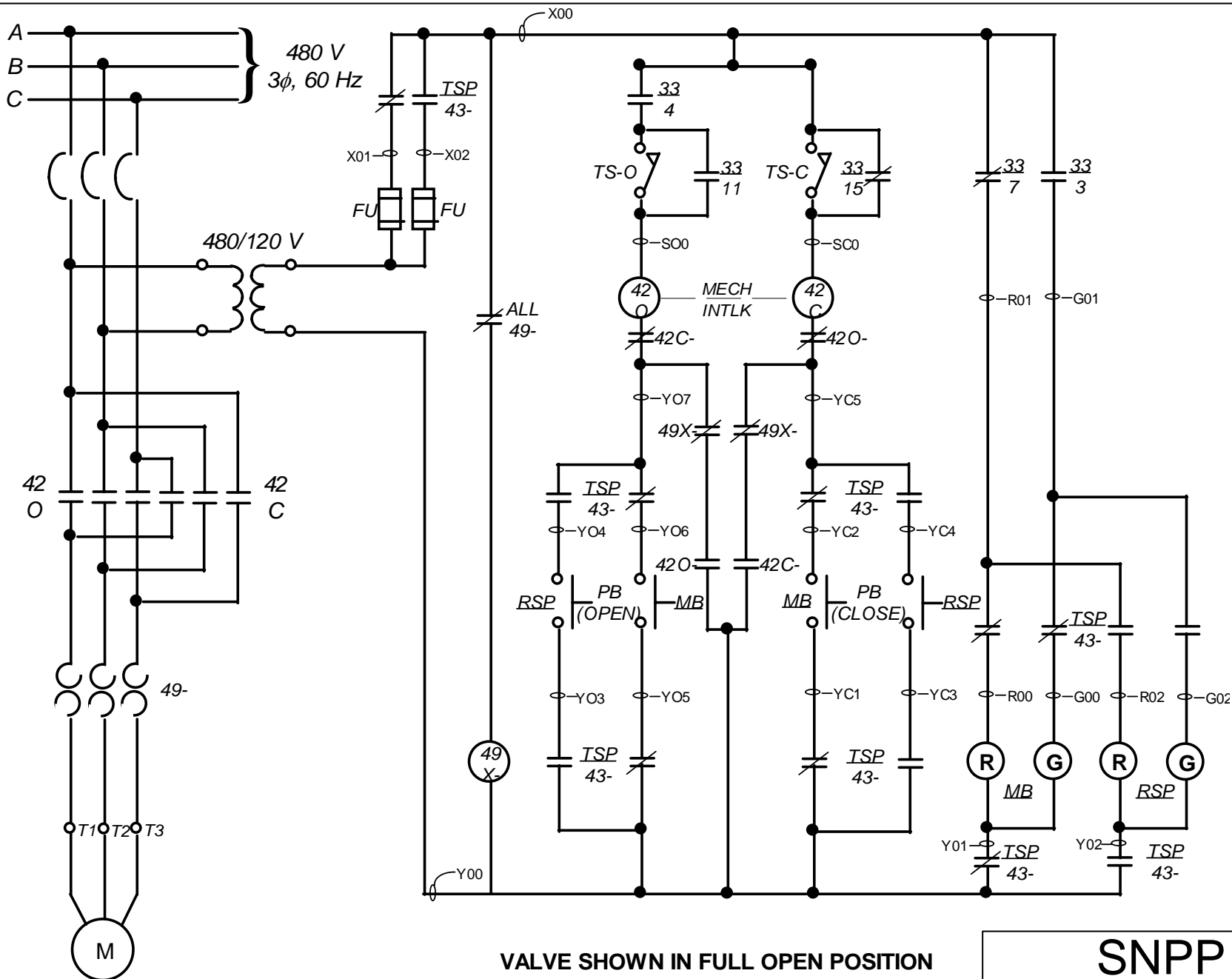
E-09

Date:

05/01/2007

Revision No.:

0



VALVE SHOWN IN FULL OPEN POSITION

MOV-13, SCHEME MA17

SNPP

SCHEMATIC DIAGRAM – PORV
BLOCK MOTOR OPERATED
VALVE
MOV-13

Drawing No.:

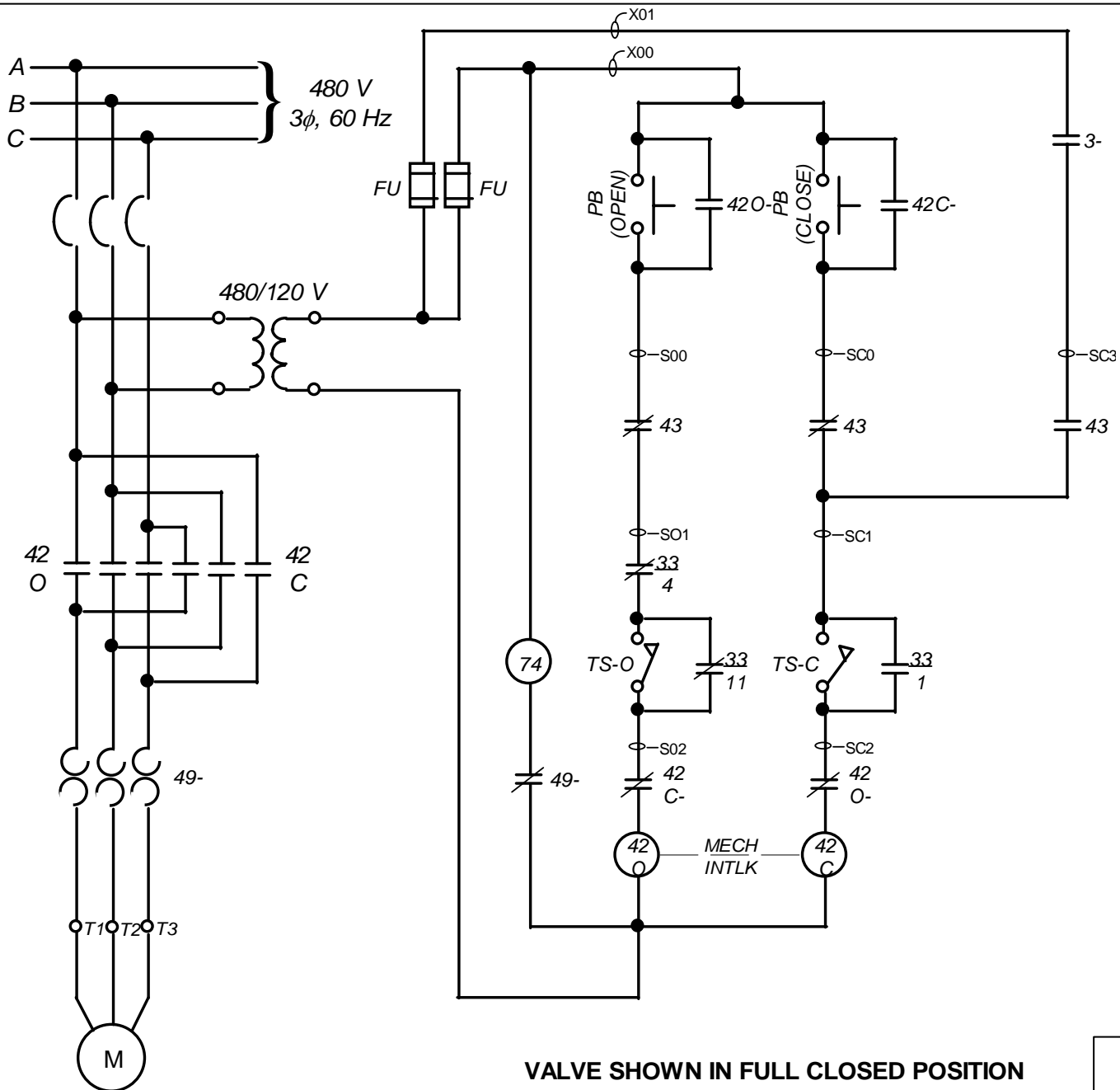
E-10

Date:

05/01/2007

Revision No.:

0



VALVE SHOWN IN FULL CLOSED POSITION

MOV-10, SCHEME MA16

SNPP

SCHEMATIC DIAGRAM –
AFW-A DISCHARGE MOTOR
OPERATED VALVE
MOV-10

Drawing No.:

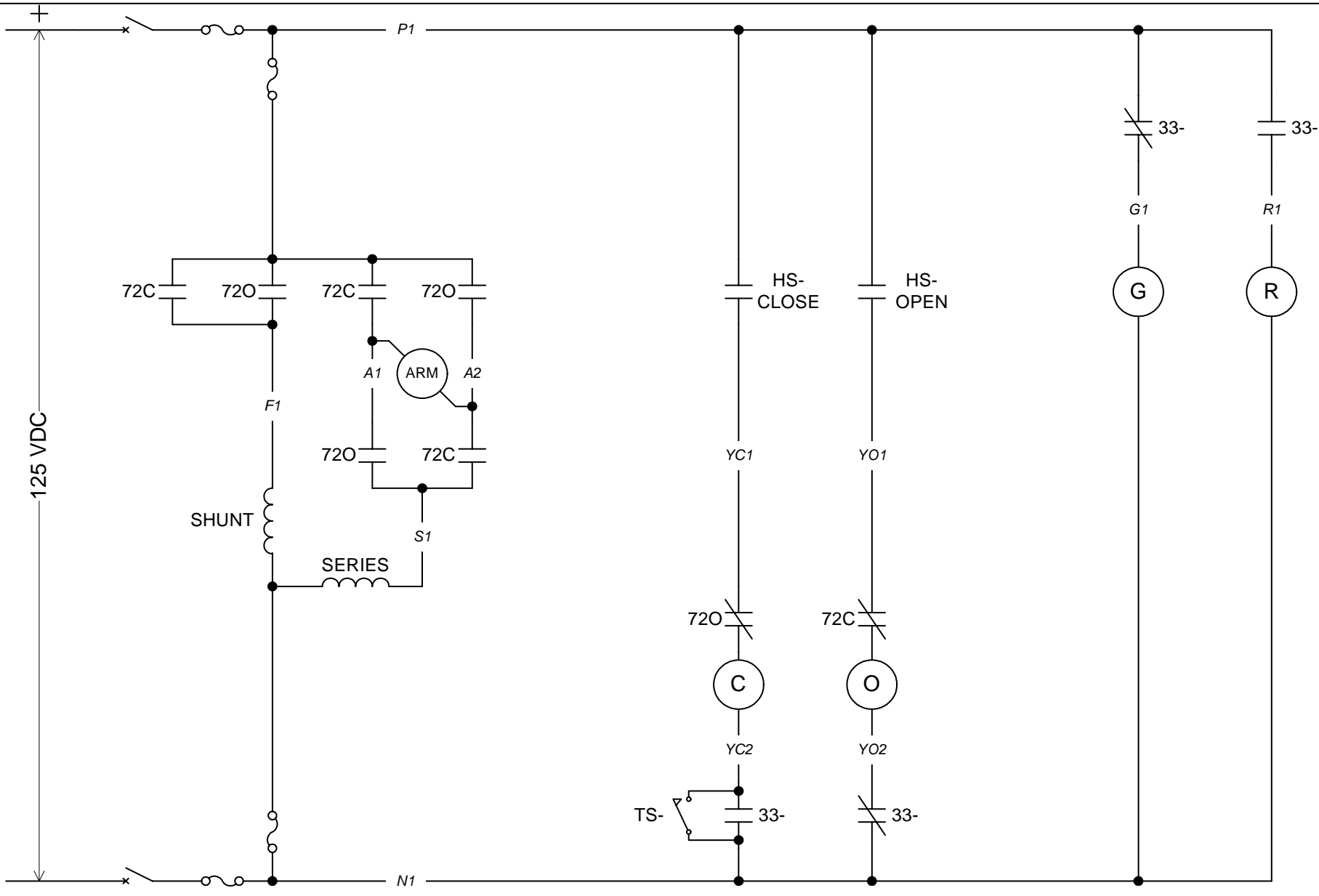
E-11

Date:

05/04/2007

Revision No.:

0



VALVE SHOWN IN CLOSED POSITION

MOV-11, SCHEME DB3

SNPP

SCHEMATIC DIAGRAM –
AFW-B DISCHARGE MOTOR
OPERATED VALVE
MOV-11

Drawing No.:

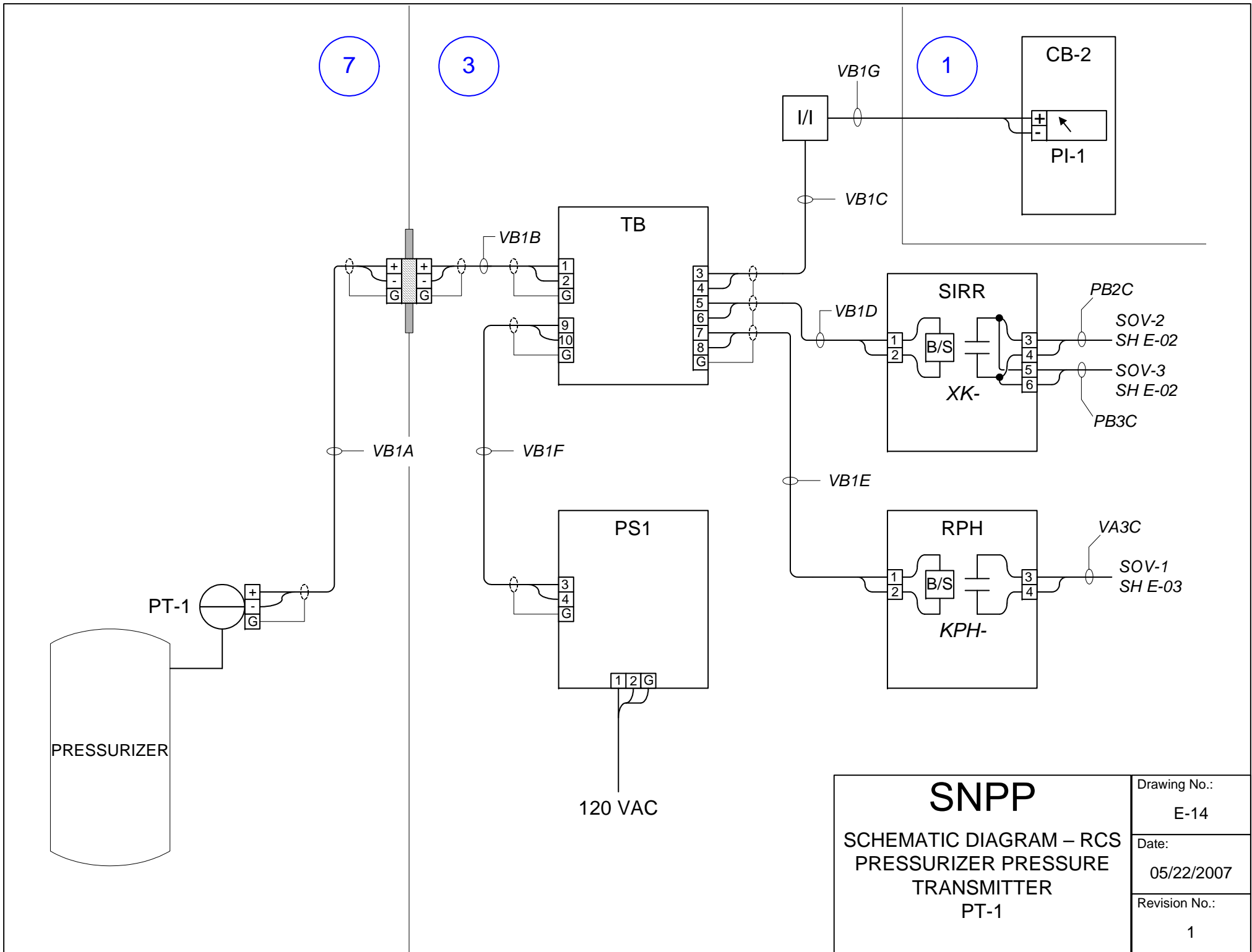
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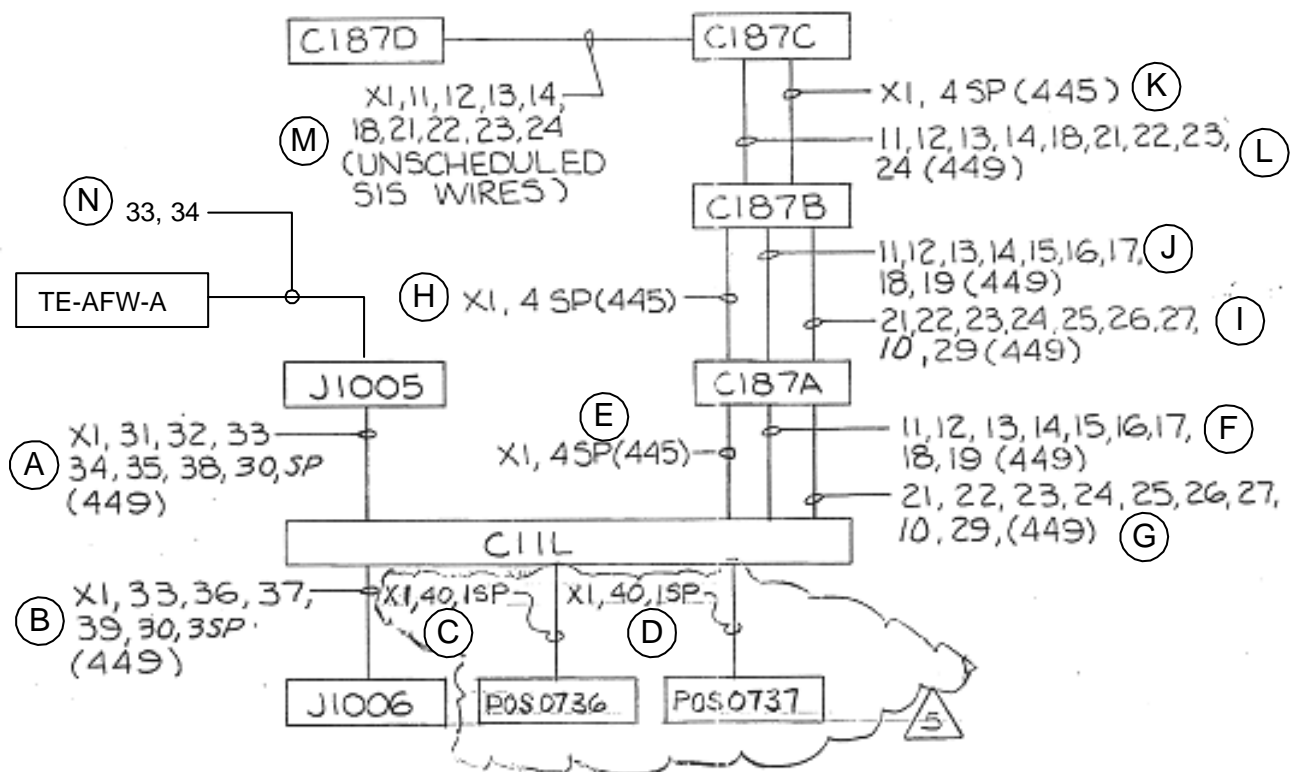
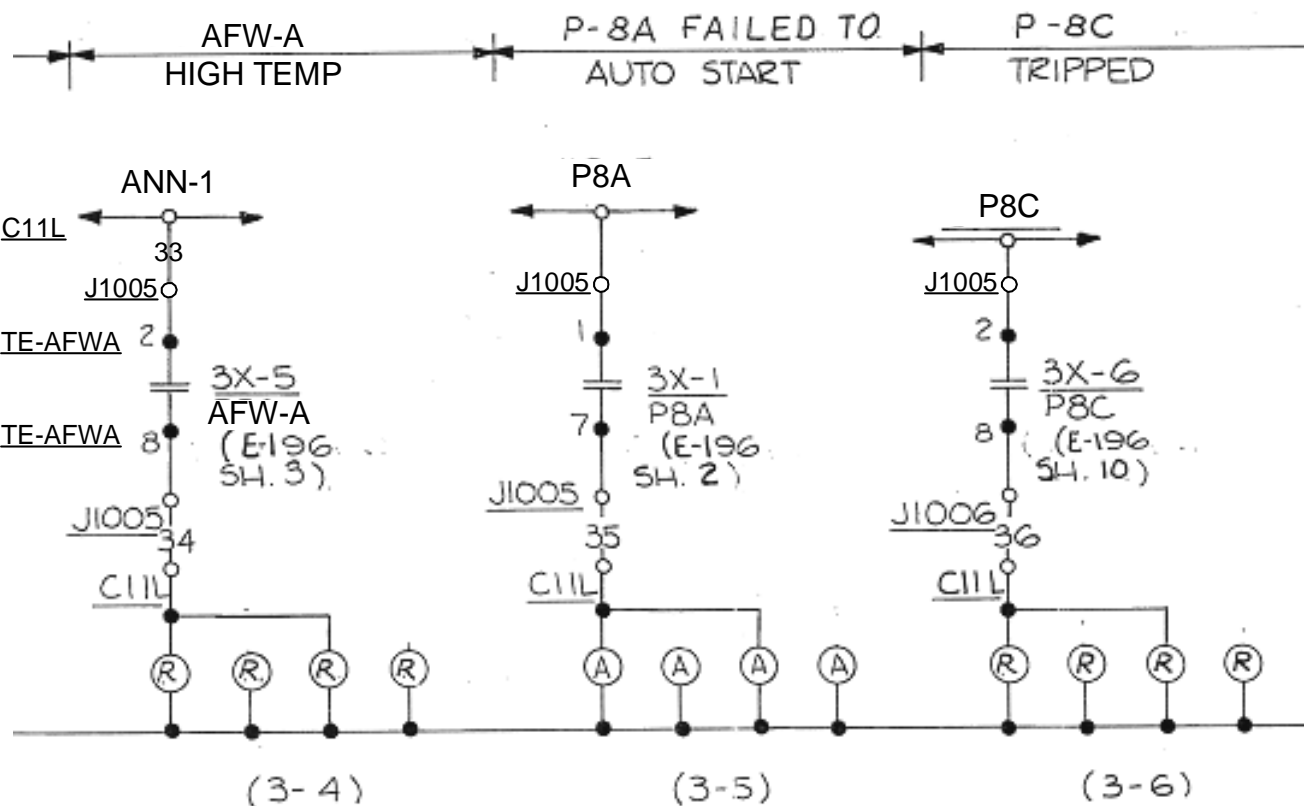
Date:

05/09/2007

Revision No.:

0





BLOCK DIAGRAM
SCHEME K16

SNPP

ANNUNCIATOR
SCHEME K16

Drawing No.:

ANN-1

Date:

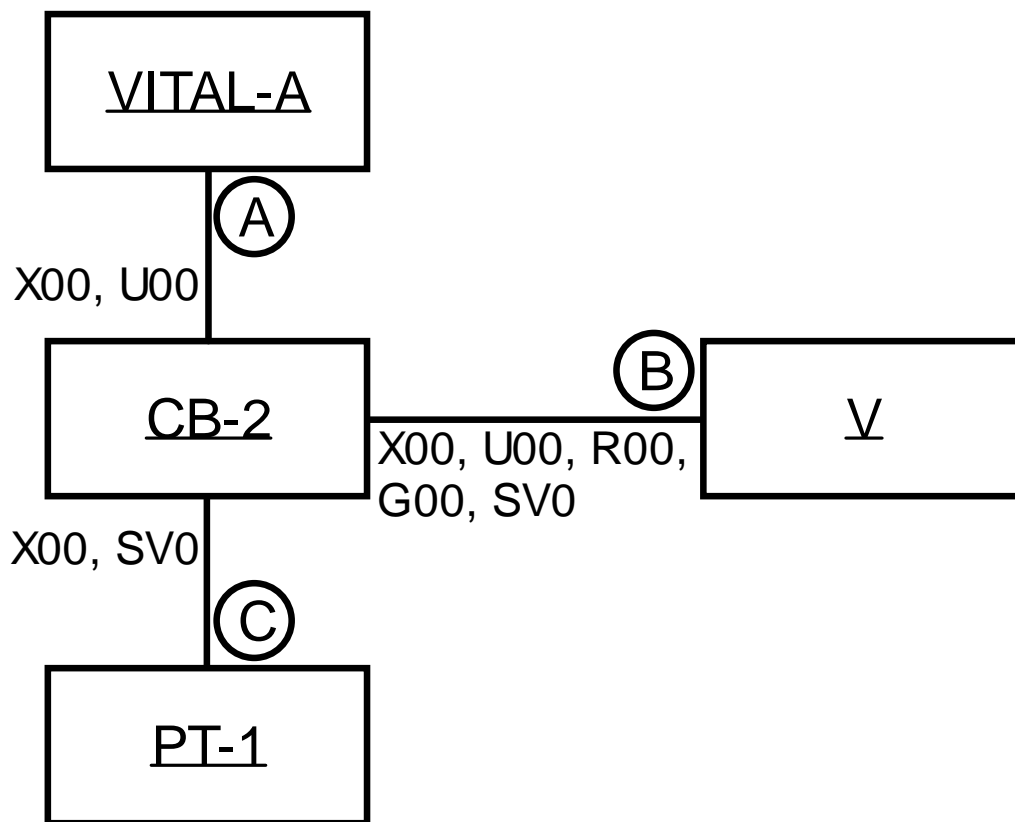
05/20/2007

Revision No.:

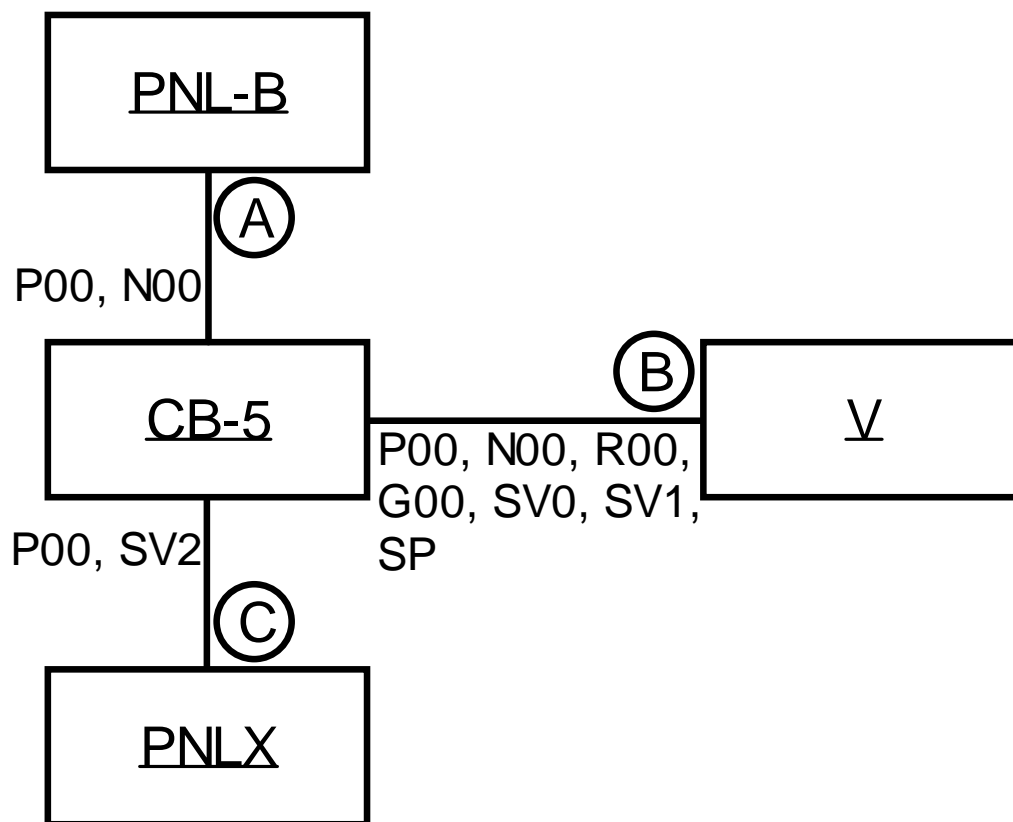
#8

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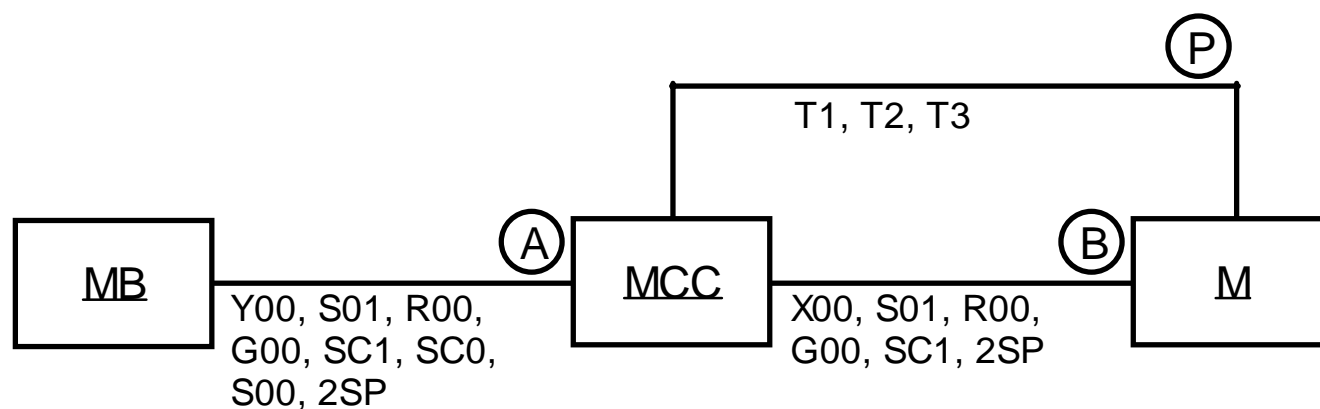
Drawing Package #2



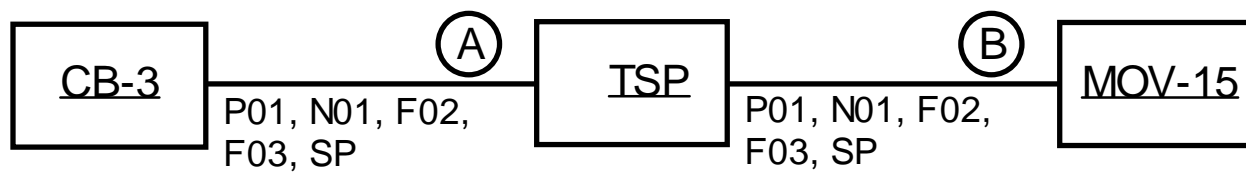
SOV-1, SCHEME VA3



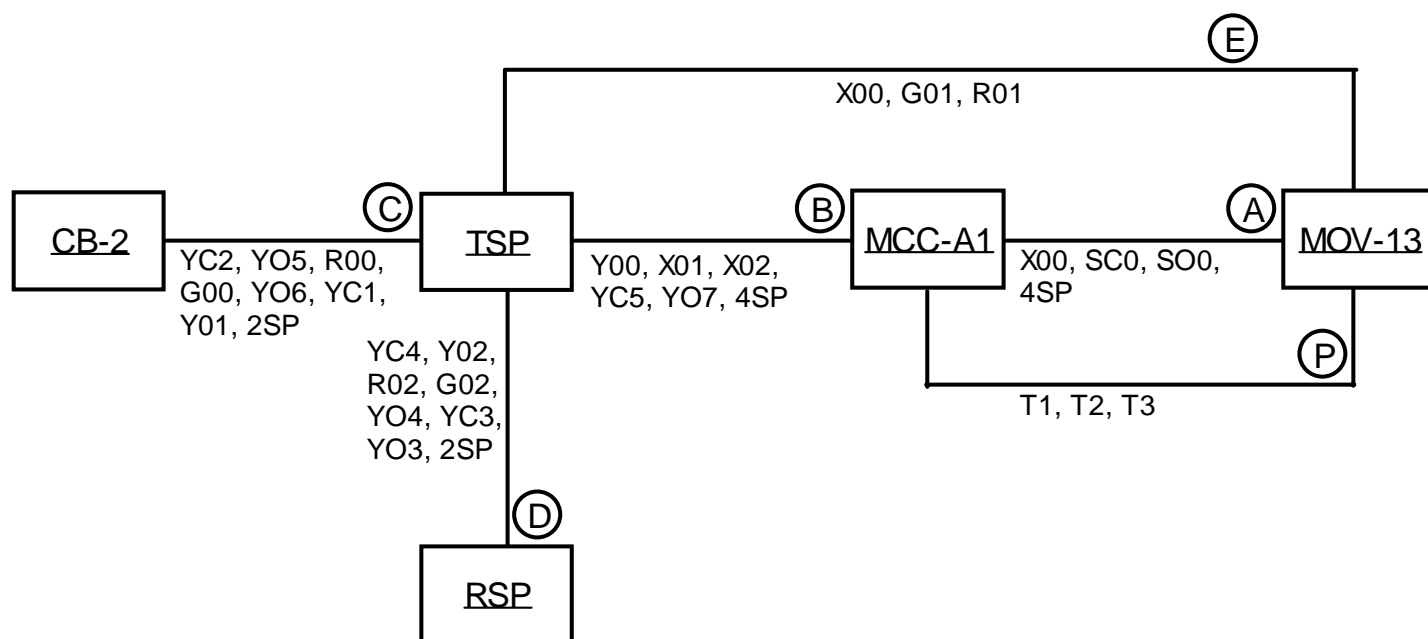
SOV-3, SCHEME PB3



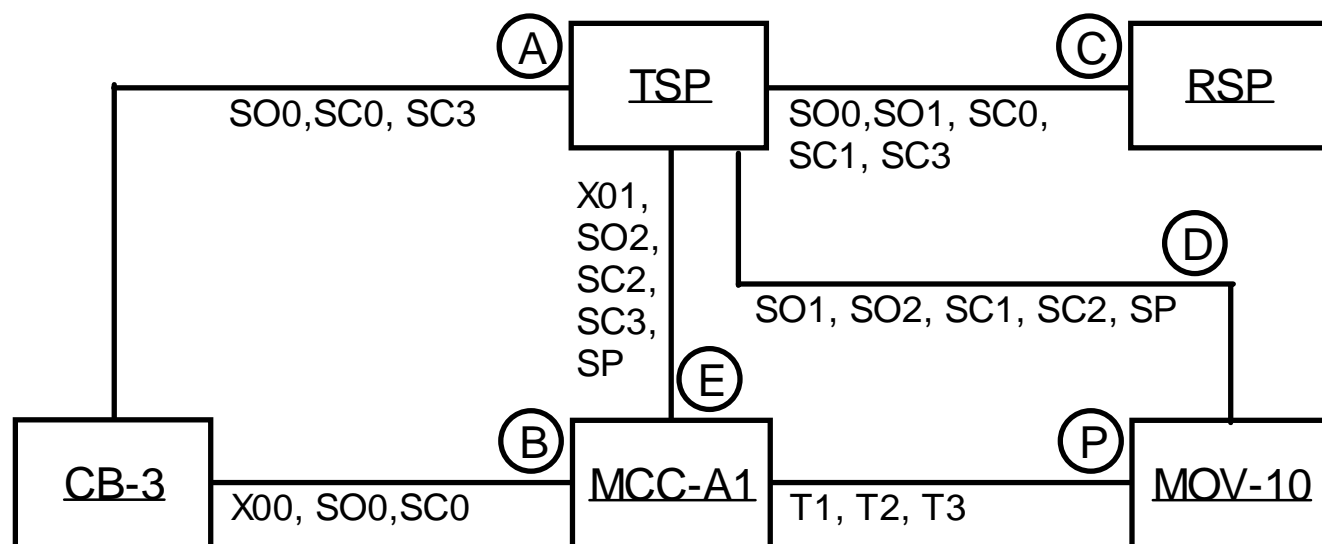
<u>M</u>	<u>MCC</u>	<u>CUBICLE</u>	<u>MB</u>	<u>SCHEME</u>
MOV-1	MCC-A1	2	CB-5	MA12
MOV-3	MCC-A1	3	CB-5	MA13
MOV-4	MCC-B1	2	CB-5	MB12
MOV-5	MCC-A1	4	CB-5	MA14
MOV-6	MCC-B1	3	CB-5	MB13
MOV-7	MCC-A1	5	CB-5	MA15
MOV-9	MCC-B1	5	CB-5	MB15
MOV-16	MCC-A1	8	CB-3	MA18
MOV-17	MCC-B1	6	CB-3	MB16



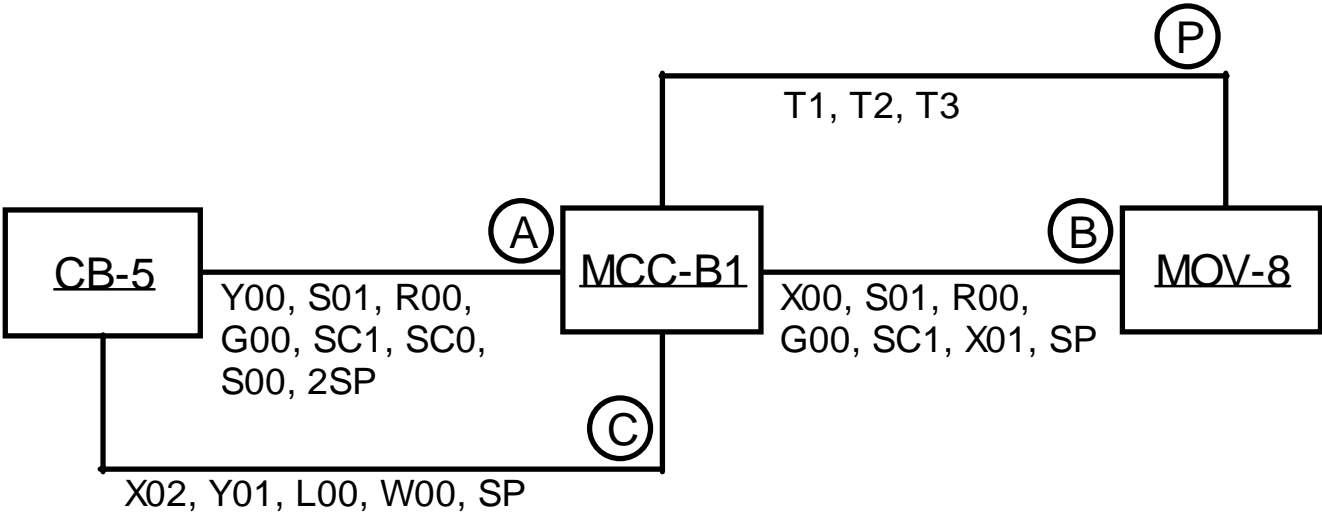
MOV-15, SCHEME DB4



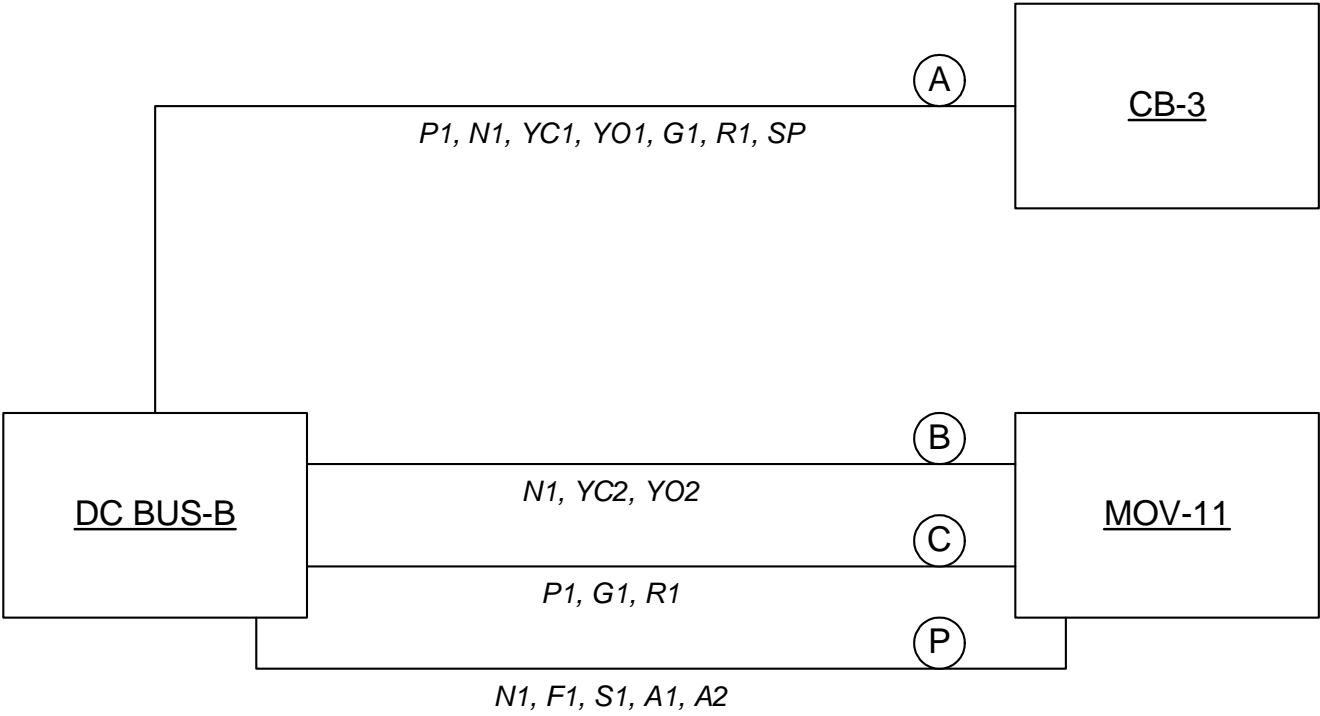
MOV-13, SCHEME MA17



MOV-10, SCHEME MA16



MOV-8, SCHEME MB14



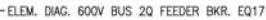
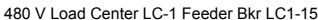
MOV-11, SCHEME DB3

Tab 3.11 Part 1:

Drawing Package #3 Part 1



Revision No.:
#6



REFERENCES:

D-207013, SH.1 SINGLE LINE PROTECTION & METERING 600V LOAD CTR. 2G

D-207676, SH.1 SINGLE LINE PROTECTION & METERING 600V LOAD CTR. 2Q

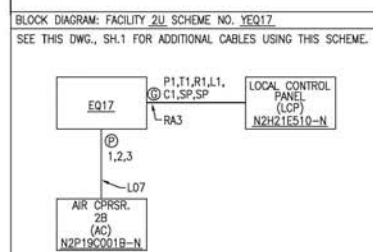
LOCAL HANDSWITCH (LH5)

BREAKER CONTROL

WEST. TYPE W2
NAMEPLATE —

CONTACT		POSITION		
1	2	1	2	
A11 - B11	X	0	0	BREAKER TRIP
A12 - B12	0	X	0	
A1 - B1	0	0	X	BREAKER CLOSE
A5 - B5	X	0	0	
A6 - B6	0	X	0	
A7 - B7	0	0	X	

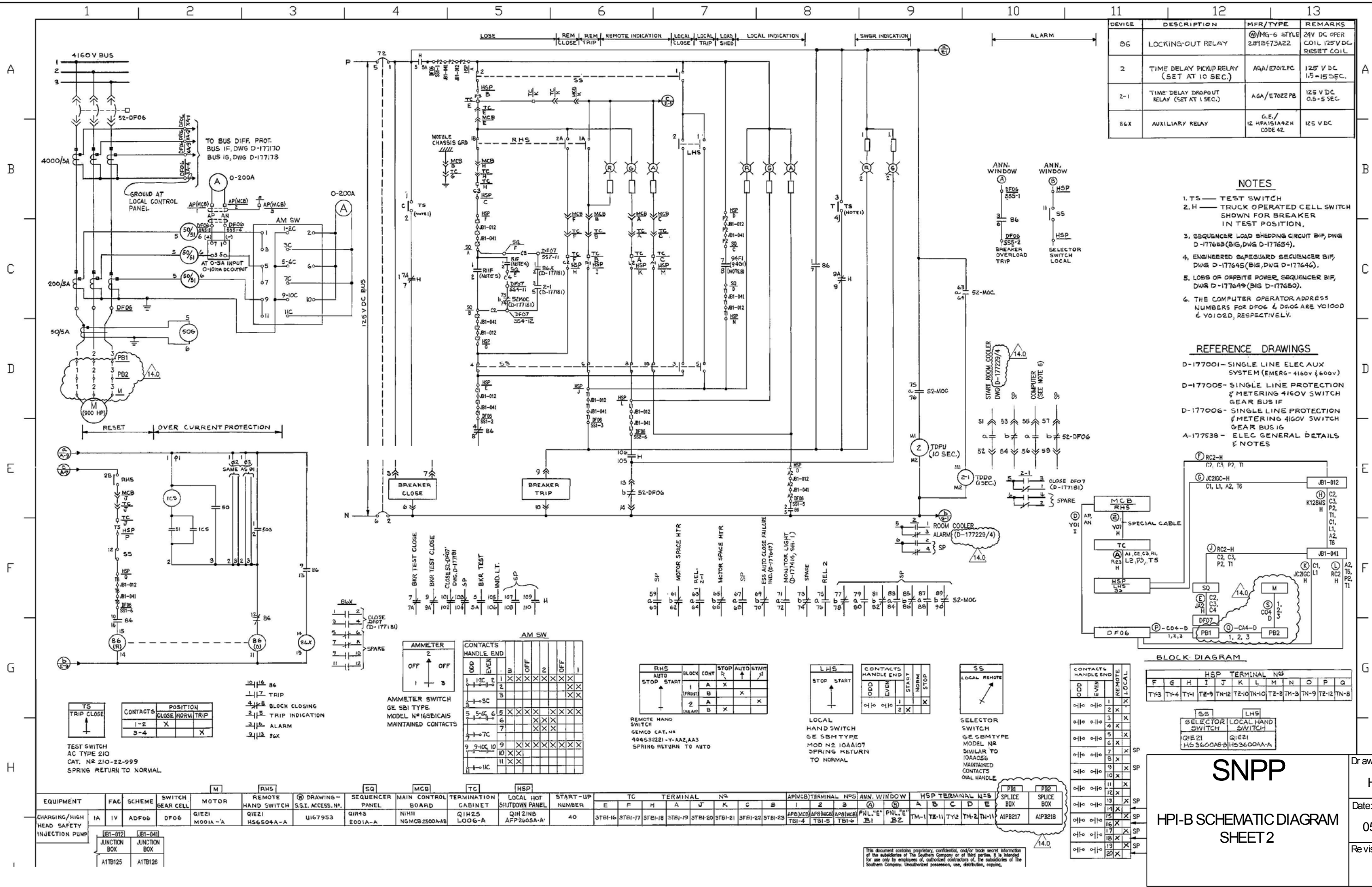
SPRING RETURN
TO NORMAL



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	JLO	CHK	NPA	DES	RPL
APPROVED	N.R. ANTINO				4/9/85
APPROVED	DEK CAB				4/9/85
APPROVED	JAMES R. CRANE				4/9/85

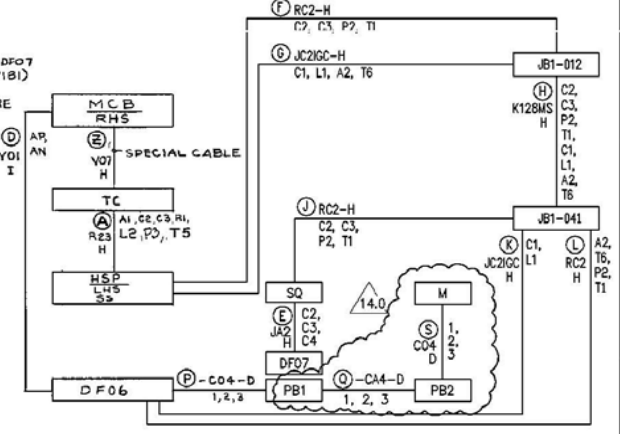
Drawing No.:	COMP-1-02
Date:	05/20/2007
Revision No.:	#6



DEVICE	DESCRIPTION	MFR/TYPER	REMARKS
0G	LOCKING-OUT RELAY	Q/MG-6 STYLE 281B73A22	24V DC OPER COIL 125VDC RESET COIL
2	TIME DELAY PICKUP RELAY (SET AT 10 SEC.)	AGA/ET02PC	125 V DC 1.5-15 SEC.
2-1	TIME DELAY DROPOUT RELAY (SET AT 1 SEC.)	AGA/ET022PB	125 V DC 0.5-5 SEC.
86X	AUXILIARY RELAY	G.E./ 12 HFA151A2H CODE 42	125 VDC

- NOTES**
1. TS — TEST SWITCH
 2. H — TRUCK OPERATED CELL SWITCH SHOWN FOR BREAKER IN TEST POSITION.
 3. SEQUENCER LOAD SHEDDING CIRCUIT BIF, DWG D-177653(B/S, DWG D-177654).
 4. ENGINEERED SAFEGUARD SEQUENCER BIF, DWG D-177645(B/S, DWG D-177646).
 5. LOSS OF OFFSITE POWER SEQUENCER BIF, DWG D-177649 (B/S D-177650).
 6. THE COMPUTER OPERATOR ADDRESS NUMBERS FOR DFO6 & D606 ARE Y0100D & Y0102D, RESPECTIVELY.

- REFERENCE DRAWINGS**
- D-177001-SINGLE LINE ELECAUX SYSTEM (EMERG-4160V & 600V)
 - D-177005-SINGLE LINE PROTECTION & METERING 4160V SWITCH GEAR BUS IF
 - D-177006-SINGLE LINE PROTECTION & METERING 4160V SWITCH GEAR BUS IG
 - A-177538-ELEC GENERAL DETAILS & NOTES



CONTACTS

CONTACTS	HANDLE END	REMOTE	LOCAL
ODD	1	X	
EVEN	2	X	
ODD	3	X	
EVEN	4	X	
ODD	5	X	
EVEN	6	X	
ODD	7	X	
EVEN	8	X	
ODD	9	X	
EVEN	10	X	
ODD	11	X	
EVEN	12	X	
ODD	13	X	
EVEN	14	X	
ODD	15	X	
EVEN	16	X	
ODD	17	X	
EVEN	18	X	
ODD	19	X	
EVEN	20	X	

SELECTOR SWITCH

SELECTOR	LOCAL HAND SWITCH
QIE21	QIE21
H53600A8-B	H53600A8-A

SNPP

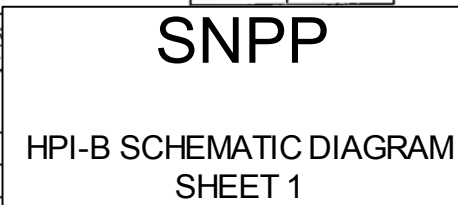
HPI-B SCHEMATIC DIAGRAM SHEET 2

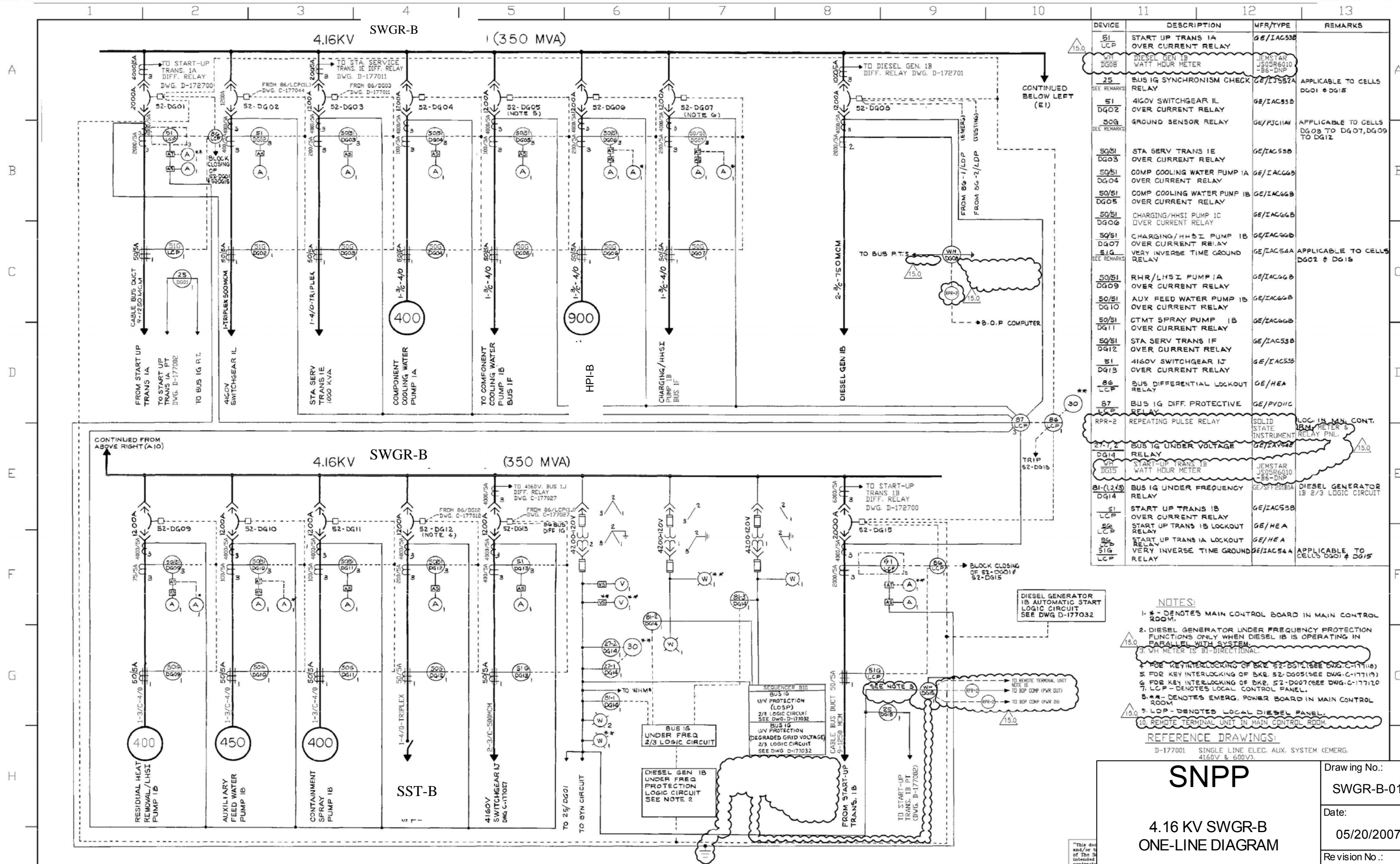
Drawing No.: HPI-B-02

Date: 05/20/2007

Revision No.: #6

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4.16 KV SWGR-B
ONE-LINE DIAGRAM

Draw ing No.:

SWGR-B-01

Date:

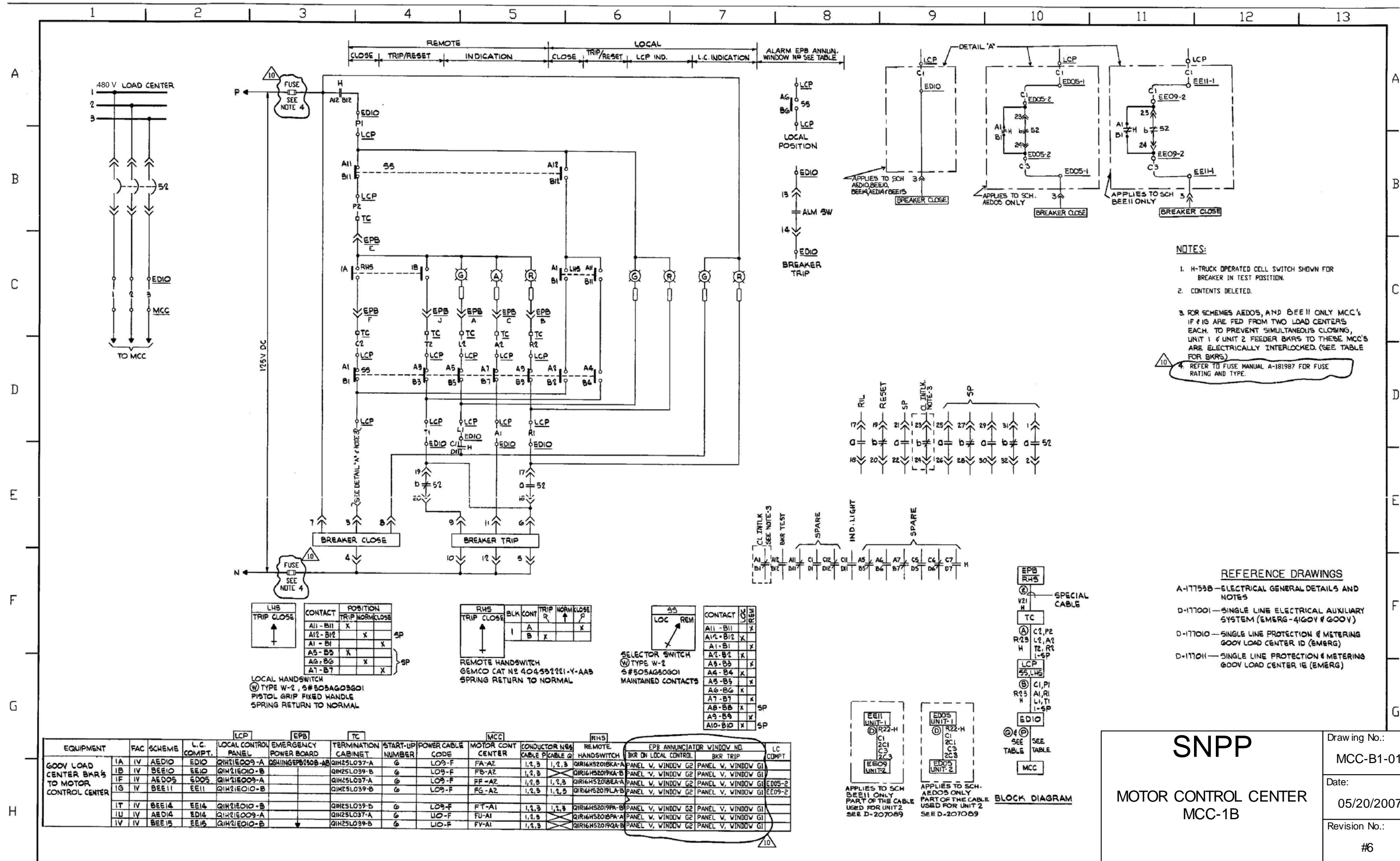
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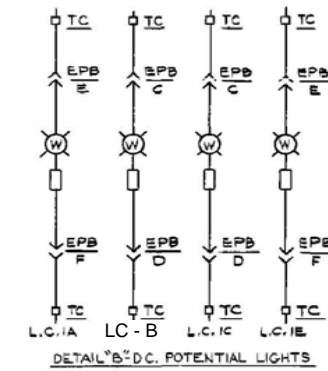
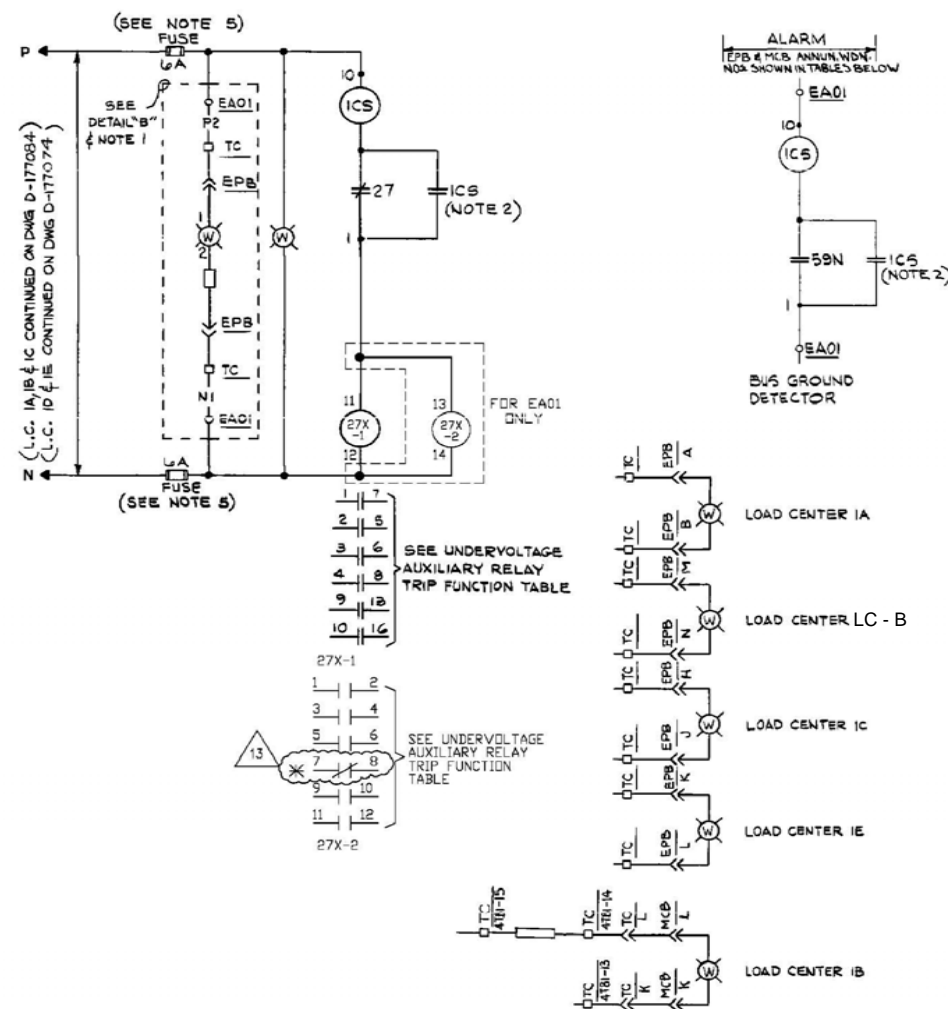
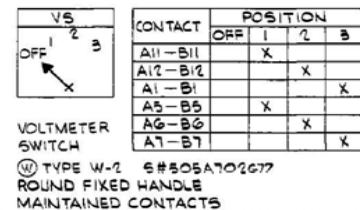
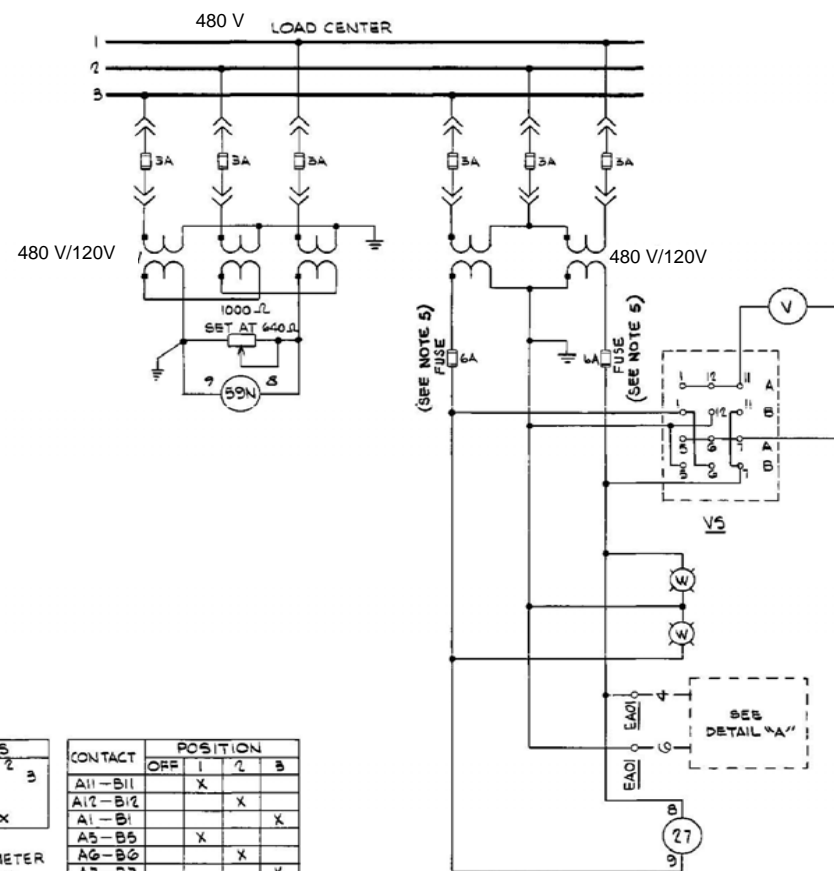
Re vision No.:

#6

Tab 3.11 Part &

Drawing Package #3 Part G





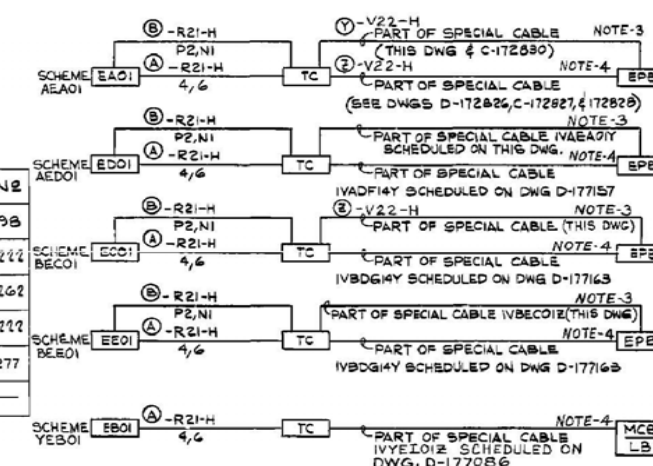
- NOTES:
- 1. DOES NOT APPLY TO EBO1.
 - 2. SEAL IN CONTACT TO BE DISCONNECTED
 - 3. CABLE FOR D.C. POTENTIAL LIGHTS.
 - 4. CABLE FOR A.C. POTENTIAL LIGHTS.
 - 5. SEE DRAWING A-181987 FOR FUSE RATING AND TYPE (LC COMPT'S EAO1, ECO1, EDO1, AND EEO1 ONLY).

UNDERVOLTAGE AUXILIARY RELAY TRIP FUNCTION TABLE											
27X-1 EAO1	LC BKR COMPT	TRIP FUNCTION	DWG NO	27X-1 ECO1	LC BKR COMPT	TRIP FUNCTION	DWG NO	27X-1 EDO1	LC BKR COMPT	TRIP FUNCTION	DWG NO
1 13	EA13	500-480/277V LIGHTING TRANS 1A	D-177090	4 8	EB05	CTMT COOLER 1B (NORMAL)	D-177221	2 5	ECO3	CRDM MG SET 1A	D-177198
2 5	EA06	CTMT PURGE ANU FAN STARTER PANEL	D-177242	3 6	EB06	CTMT COOLER 1C (NORMAL)	D-177221	1 7	ED15	CTMT COOLER 1A (EMERG)	D-177222
3 6	EA10	CTMT COOLER 1A (NORMAL)	D-177221	2 5	EB10	HYDRO TEST PUMP	D-177241	9 13	ED11	CRDM COOLER FAN 1B	D-177262
4 8	EA12	SPENT FUEL POOL PUMP 1B	D-177205	9 13	—	SPARE	—	4 8	ECO5	AUX BLDG MAIN EXHAUST FAN 1A	D-177157
1 7	EA03	CTMT PURGE EXH. FAN STARTER PANEL	D-177242	1 7	EB11	AUX BLDG MAIN EXHAUST FAN 1B	D-177257	3 6	ECO6	RADWASTE ANU SUPPLY FAN	D-177250
10 16	—	SPARE	—	10 16	—	SPARE	—	9 13	—	SPARE	—

27X-2 EAO1	LC BKR COMPT	TRIP FUNCTION	DWG NO.
1 2	EA11	PRESSURIZER HTR GROUP 1A	D-177109
3 4	EA15	STATION AIR COMPRESSOR 1C	D-172746 SH. 4
5 6	—	SPARE	—
7 8	EA15	STATION AIR COMPRESSOR 1C AUTO CLOSE	D-172746 SH. 4
9 10	—	SPARE	—
11 12	—	SPARE	—

EPB	TC	EPB	TC	EPB	TC
EMERGENCY POWER BUARD	TERMINATION CABINET	FAC	SWGR CELL	SCHEME	START-UP NUMBER
QSH1ING EPB2508-AB	Q1H25L037-A	1V	EA01	AEA01	5
QSH1ING EPB2508-AB	Q1H25L039-B	1V	ECO1	BEO01	5
QSH1ING EPB2508-AB	Q1H25L037-A	1V	EDO1	AED01	5
QSH1ING EPB2508-AB	Q1H25L039-B	1V	ECO1	BEO01	5

MCB	TC	MCB	TC	MCB	TC
MAIN CONTROL BUARD	TERMINATION CABINET	FAC	SWGR CELL	SCHEME	START-UP NUMBER
Q1H1ING MCB2508-AB	Q1H25L016-B	1V	EB01	YEB01	5
Q1H1ING MCB2508-AB	Q1H25L016-B	1V	EB01	YEB01	5



- REFERENCE DRAWINGS:
- A-177518 — ELECTRICAL GENERAL DETAILS AND NOTES
 - D-177000 — SINGLE LINE ELECTRICAL AUX SYSTEM (NORMAL - 4160V & 600V)
 - D-177001 — SINGLE LINE ELECTRICAL AUX SYSTEM (EMERG - 4160V & 600V)
 - D-177007 — SINGLE LINE PROTECTION AND METERING 600V LOAD CENTER 1A
 - C-177008 — SINGLE LINE PROTECTION AND METERING 600V LOAD CENTER 1B
 - C-177009 — SINGLE LINE PROTECTION AND METERING 600V LOAD CENTER 1C
 - D-177010 — SINGLE LINE PROTECTION AND METERING 600V LOAD CENTER 1D (EMERG)
 - D-177011 — SINGLE LINE PROTECTION AND METERING 600V LOAD CENTER 1E (EMERG)
 - A-181987 — FUSE REPLACEMENT MANUAL FOR SAFETY RELATED EQUIPMENT.

* CONSTRUCTION NOTE: FIELD TO CONVERT NO CONTACT 7-8 TO NC.

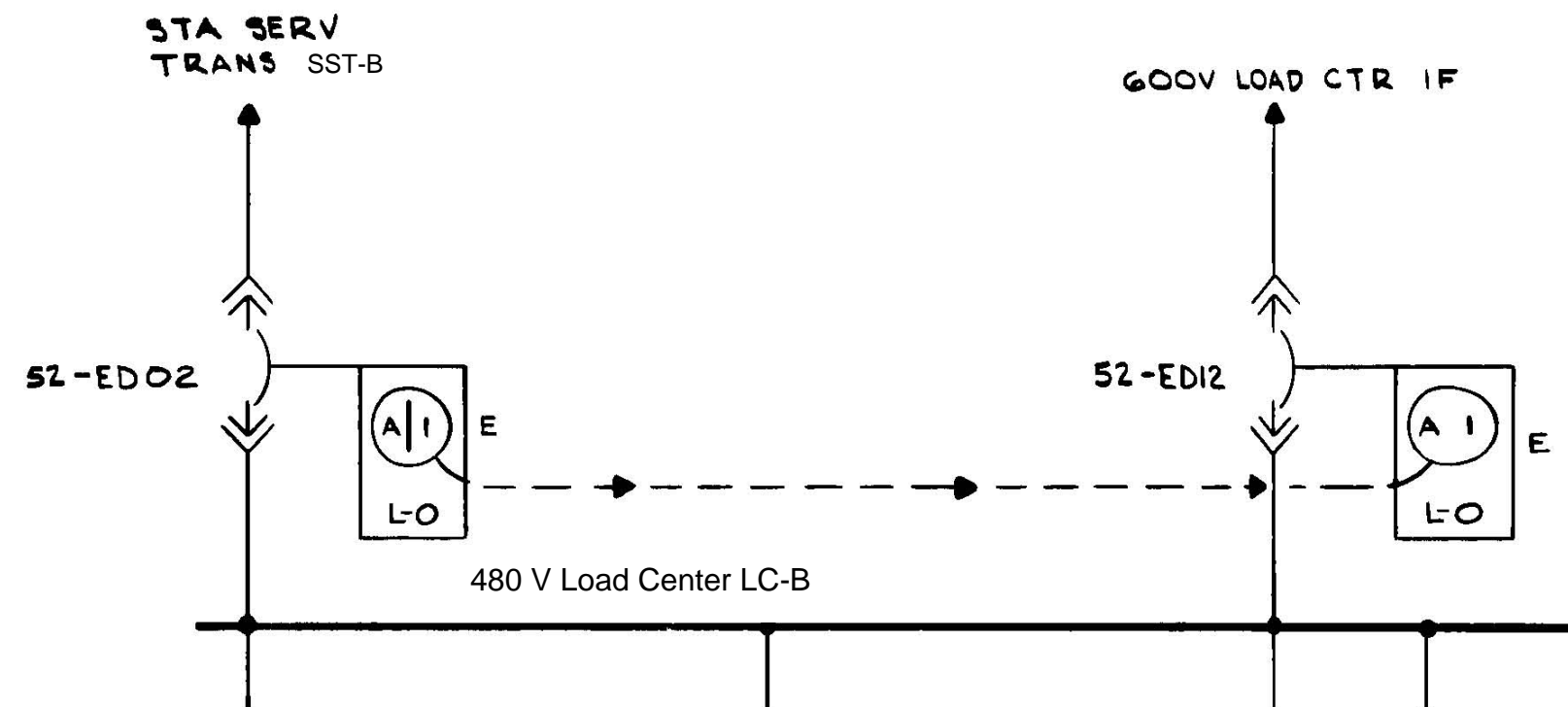
SNPP

LOAD CENTER
UNDERVOLTAGE SCHEME

Drawing No.:
LC-B-05

Date:
05/20/2007

Revision No.:
#6



OPERATION SEQUENCE

KEY IS HELD IN CIRCUIT BREAKER 52-ED02 INTERLOCK.
TO ESTABLISH SERVICE THROUGH CIRCUIT BREAKER
52-ED12

1. TRIP CIRCUIT BREAKER 52-ED02
2. TURN KEY AI IN L-O INTERLOCK ON CIRCUIT BREAKER
52-ED02 TO LOCK OPEN. KEY AI IS NOW FREE.
3. INSERT KEY AI IN L-O INTERLOCK ON CIRCUIT BREAKER
52-ED12 AND TURN TO UNLOCK. KEY AI IS NOW HELD.
4. CLOSE CIRCUIT BREAKER 52-ED12.

REVERSE SEQUENCE TO RESTORE SERVICE THROUGH
CIRCUIT BREAKER 52-ED02.

NOTE: AS AN EXCEPTION FOR MAINTENANCE WORK PER A PLANT
PROCEDURE, TWO KEYS MAY BE USED TO OVERRIDE THE
NORMAL CIRCUIT BREAKER INTERLOCK FEATURE.

4

NOTES

1. ALL INTERLOCKS ARE KIRK TYPE
2. CIRCUIT BREAKERS 52-ED09, 52-EE06 &
MOLDED CASE BREAKERS TO BATTERY
CHARGER IC ARE KEY INTERLOCKED SO
THAT ONLY ONE BREAKER AND CORRESPOND-
ING BATTERY CHARGER MOLDED CASE
BREAKER CAN BE CLOSED AT ANY TIME
(SEE DWG C-177133)

LEGEND

- INTERLOCK WITH KEY HELD.
- INTERLOCK WITH KEY REMOVED.
- L-O — (LOCKED OPEN) INDICATES THAT
THE KEY IS REMOVABLE WHEN THE
CIRCUIT BREAKER IS LOCKED IN THE
OPEN POSITION.
- E — INDICATES KEY REMOVABLE ONLY
WHEN BOLT EXTENDED.

INTERLOCK KEY TABLE

INTERLOCK	KEY NUMBER
AI	RE-14204

REFERENCE DWG.

- D-177001-SINGLE LINE ELEC AUX SYSTEM
(4160V & 600V)
- C-177010-SINGLE LINE PROTECTION &
METERING 600V LOAD CENTER ID
- A-177538-ELEC GEN DETAILS & NOTES

SNPP

LC-B
INCOMING BREAKER
INTERLOCKS

Drawing No.:

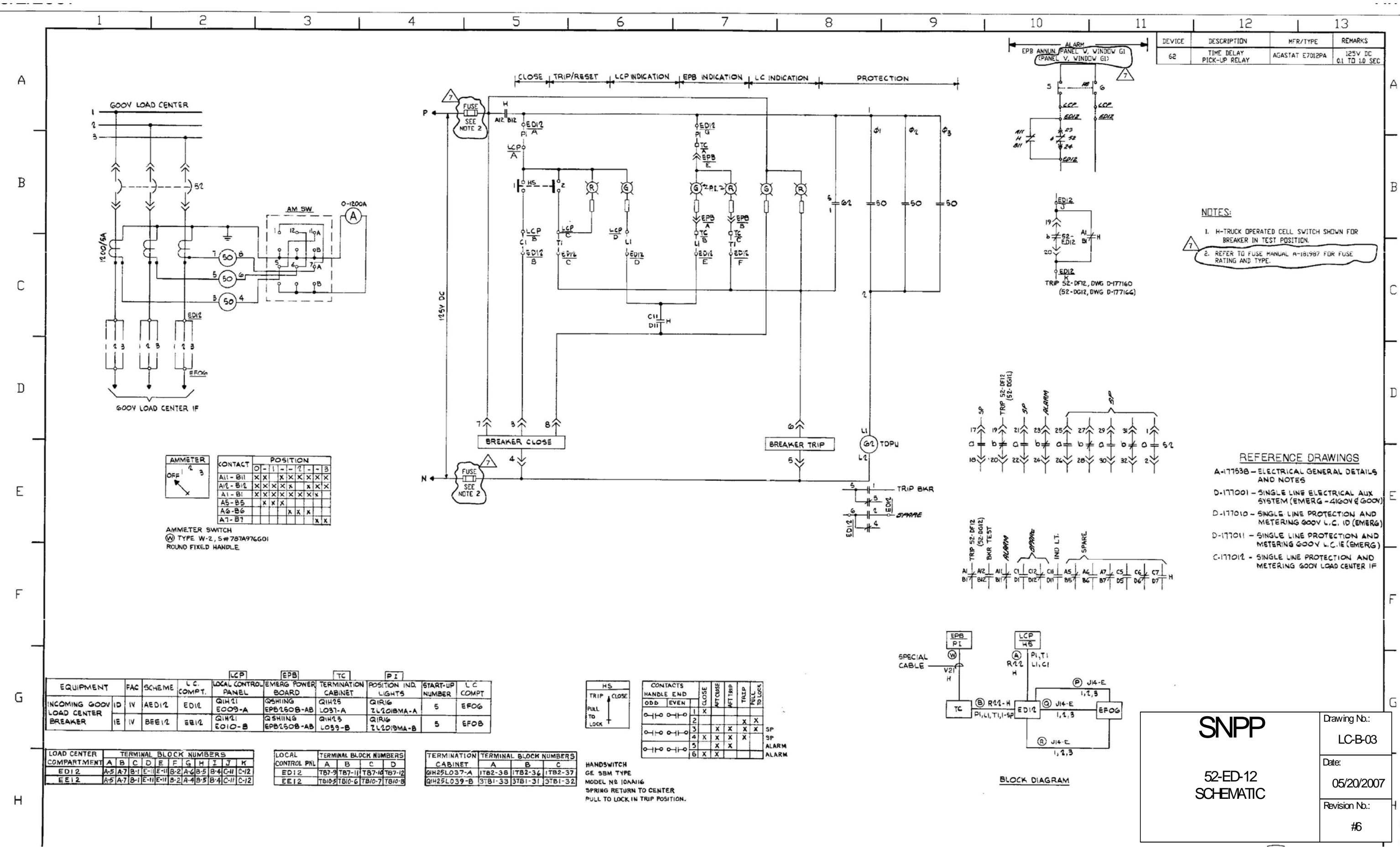
LC-B-04

Date:

05/20/2007

Revision No.:

#6



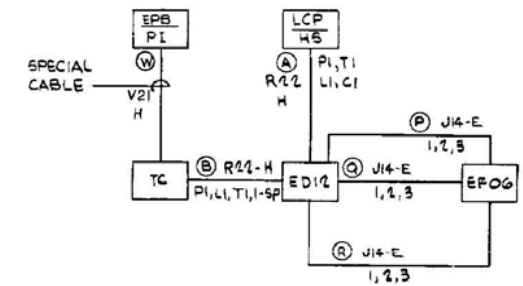
DEVICE	DESCRIPTION	MFR/TYPER	REMARKS
62	TIME DELAY PICK-UP RELAY	AGASTAT E7012PA	125V DC 0.1 TO 1.0 SEC

NOTES:

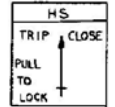
1. H-TRUCK OPERATED CELL SWITCH SHOWN FOR BREAKER IN TEST POSITION.
2. REFER TO FUSE MANUAL A-181987 FOR FUSE RATING AND TYPE.

REFERENCE DRAWINGS

- A-17538 - ELECTRICAL GENERAL DETAILS AND NOTES
- D-177001 - SINGLE LINE ELECTRICAL AUX SYSTEM (EMERG - 4160V & 600V)
- D-177010 - SINGLE LINE PROTECTION AND METERING GOOV L.C. ID (EMERG)
- D-177011 - SINGLE LINE PROTECTION AND METERING GOOV L.C. IE (EMERG)
- C-177012 - SINGLE LINE PROTECTION AND METERING GOOV LOAD CENTER IF



BLOCK DIAGRAM



HANDSWITCH
GE 58M TYPE
MODEL NO. 10A116
SPRING RETURN TO CENTER
PULL TO LOCK IN TRIP POSITION.

CONTACTS		HANDLE END		CLOSE		TRIP		TRIP		TRIP	
ODD	EVEN	1	2	3	4	5	6	7	8	9	10
0-1-0	0-1-0	1	2	3	4	5	6	7	8	9	10
0-1-0	0-1-0	1	2	3	4	5	6	7	8	9	10
0-1-0	0-1-0	1	2	3	4	5	6	7	8	9	10

EQUIPMENT		FAC	SCHEME	L.C. COMPT.	LCP	EPB	TC	PI	POSITION IND. LIGHTS	START-UP NUMBER	L.C. COMPT.
					LOCAL CONTROL PANEL	EMERG POWER BOARD	TERMINATION CABINET				
INCOMING GOOV LOAD CENTER BREAKER	ID	IV	AED12	ED12	Q1H21 EOO9-A	QSHING EPB12OB-AB	Q1H25 LO37-A	Q1R16 ZL201BMA-A	5	EFOG	
	IE	IV	BEE12	EE12	Q1H21 EO10-B	QSHING EPB12OB-AB	Q1H23 LO39-B	Q1R16 ZL201BMA-B	5	EFOB	

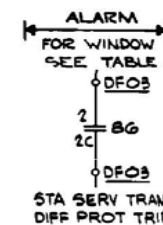
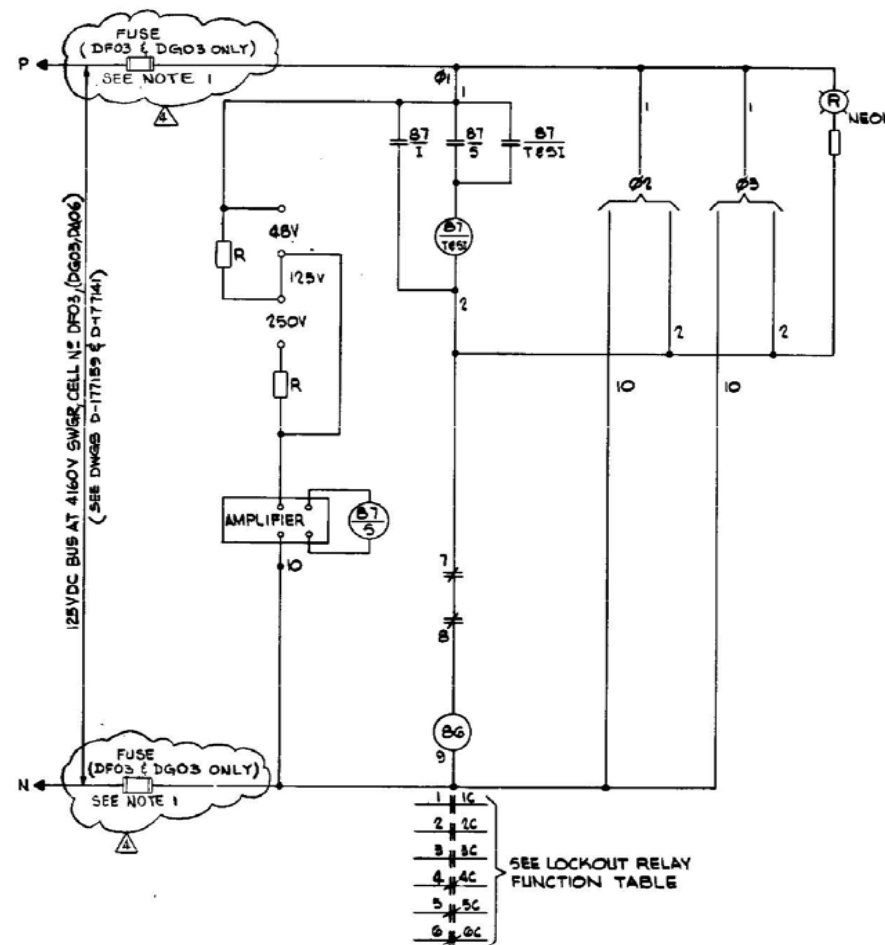
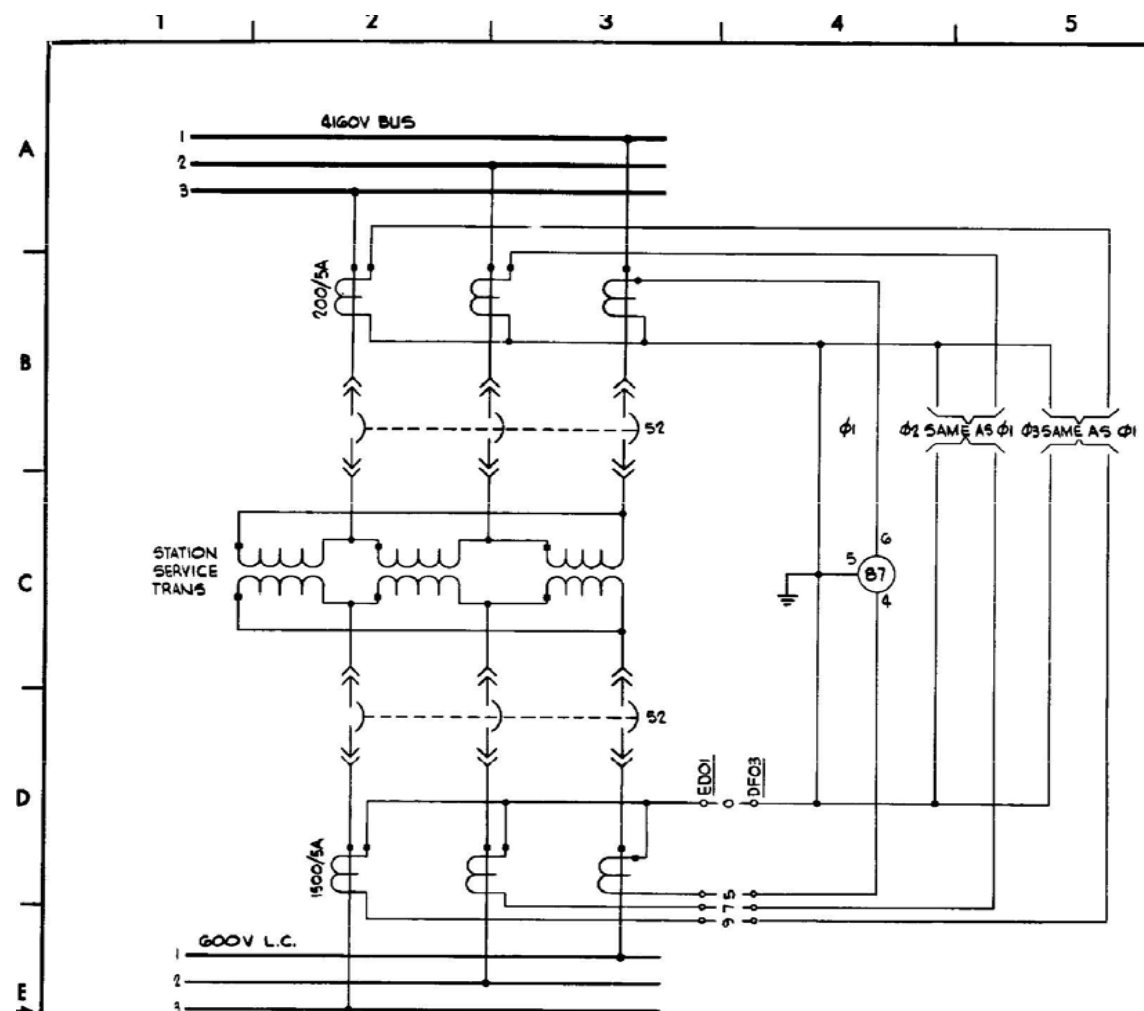
LOAD CENTER		TERMINAL BLOCK NUMBERS											
COMPARTMENT		A	B	C	D	E	F	G	H	I	J	K	
ED12	A-5	A-7	B-1	E-11	E-11	B-2	A-6	B-5	B-4	C-11	C-12		
EE12	A-5	A-7	B-1	E-11	E-11	B-2	A-4	B-5	B-4	C-11	C-12		

LOCAL CONTROL PNL		TERMINAL BLOCK NUMBERS			
		A	B	C	D
ED12		TB7-9	TB7-11	TB7-10	TB7-12
EE12		TB10-5	TB10-6	TB10-7	TB10-8

TERMINATION CABINET		TERMINAL BLOCK NUMBERS		
		A	B	C
Q1H25LO37-A		1TB2-38	1TB2-36	1TB2-37
Q1H25LO39-B		3TB1-33	3TB1-31	3TB1-32

SNPP
52-ED-12
SCHEMATIC

Drawing No.:
LC-B-03
Date:
05/20/2007
Revision No.:
#6

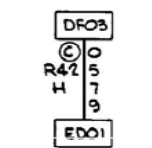


DEVICE	DESCRIPTION	MFR/TYPER	REMARKS
B6	LOCKOUT RELAY	GE/HEAGIA/213	125V DC

NOTES:
1. SEE DRAWING A-181987 FOR FUSE RATING & TYPE.

REFERENCE DRAWINGS

- A-177538—ELECTRICAL GENERAL DETAILS AND NOTES
- D-177001—SINGLE LINE ELECTRICAL AUX SYSTEM (EMERG-4160V & 600V)
- D-177002—SINGLE LINE PROTECTION AND METERING 4160V SWITCHGEAR, BUS 1A
- D-177005—SINGLE LINE PROTECTION AND METERING 4160V SWITCHGEAR BUS 1F (EMERG)
- D-177006—SINGLE LINE PROTECTION AND METERING 4160V SWITCHGEAR BUS 1G (EMERG)
- C-177010—SINGLE LINE PROTECTION AND METERING 600V LOAD CENTER 1D (EMERG)
- C-177011—SINGLE LINE PROTECTION AND METERING 600V LOAD CENTER 1E (EMERG)
- C-177674—SINGLE LINE PROTECTION AND METERING 600V LOAD CENTER 1I
- A-181987—FUSE REPLACEMENT MANUAL FOR SAFETY RELATED EQUIPMENT.



BLOCK DIAGRAM

LOCKOUT RELAY FUNCTION TABLE

B6 DFO3	FUNCTION	DWG N2	B6 DGO3	FUNCTION	DWG N2	B6 DAO6	FUNCTION	DWG N2
1 IC	TRIP BKR 52-DFO3	C-177159	1 IC	TRIP BKR 52-DGO3	C-177159	1 IC	TRIP BKR 52-DAO6	D-177141
2 2C	ALARM	THIS DWG	2 2C	ALARM	THIS DWG	2 2C	ALARM	THIS DWG
3 3C	SPARE	—	3 3C	SPARE	—	3 3C	SPARE	—
4 4C	SPARE	—	4 4C	SPARE	—	4 4C	BLOCK CLOSING BKR 52-DAO6	D-177141
5 5C	BLOCK CLOSING BKR 52-DFO3	C-177159	5 5C	BLOCK CLOSING BKR 52-DGO3	C-177159	5 5C	SPARE	—
6 6C	SPARE	—	6 6C	SPARE	—	6 6C	SPARE	—

EQUIPMENT	FAC	SCHEME	SWGR CELL	LOAD CENTER	START-UP	ANNUNCIATOR
DIFFERENTIAL RELAY FOR STATION SERV TRANSFORMER	ID	IV	ADFO3	DFO3	ED01	5
	IE	IV	BDO3	DGO3	ED01	5
	II	IV	XDAO6	DAO6	EIOI	5

SNPP

STATION SERVICE TRANSFORMER DIFFERENTIAL PROTECTION SCHEME

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