

PMBelCOL PEmails

From: Creek, Carolyn P [cpcreek@tva.gov]
Sent: Thursday, July 24, 2008 2:31 PM
To: Mallecia Hood
Cc: Neil Haggerty
Subject: Letter to NRC Date 7/23/08
Attachments: BLN Response to NRC Trip Report for signature 20080723.pdf

Mallecia

Here is a copy of the letter we mailed to you on Wednesday.

<<BLN Response to NRC Trip Report for signature 20080723.pdf>>

Carolyn Creek

Management Assistant
Nuclear Generation Development
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Hearing Identifier: Bellefonte_COL_Public_EX
Email Number: 977

Mail Envelope Properties (28921B76CDD05940A918AEEC9EBCA7C007B4C0CF)

Subject: Letter to NRC Date 7/23/08
Sent Date: 7/24/2008 2:30:41 PM
Received Date: 7/24/2008 2:32:15 PM
From: Creek, Carolyn P

Created By: cpcreek@tva.gov

Recipients:
"Neil Haggerty" <neilhaggerty@comcast.net>
Tracking Status: None
"Mallecia Hood" <Mallecia.Hood@nrc.gov>
Tracking Status: None

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| Files | Size | Date & Time |
|--|-------------|------------------------|
| MESSAGE | 308 | 7/24/2008 2:32:15 PM |
| BLN Response to NRC Trip Report for signature 20080723.pdf | | 1329884 |

Options
Priority: Standard
Return Notification: No
Reply Requested: No
Sensitivity: Normal
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Tennessee Valley Authority, 1101 Market Street, LP 5A, Chattanooga, Tennessee 37402-2801

July 23, 2008

10 CFR 52.79

U.S. Nuclear Regulatory Commission
ATTN: Document Control Desk
Washington, D.C. 20555

In the Matter of)
Tennessee Valley Authority)

Docket No. 52-014 and 52-015

BELLEFONTE COMBINED LICENSE APPLICATION – ITEMS IDENTIFIED IN NRC
HYDROLOGY RELATED SITE VISIT TRIP REPORT

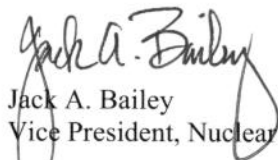
Reference: Memorandum from Joseph Sebrosky (NRC) to Stephanie Coffin (NRC), Trip
Report – May 13-16, 2008, Hydrology-Related Site Visit in Support of the
Bellefonte Combined License Application, dated June 12, 2008

This letter provides information to address the four items identified in the cover memorandum of
the referenced Nuclear Regulatory Commission (NRC) trip report. Each item is addressed in the
enclosure.

If you should have any questions, please contact Thomas Spink at 1101 Market Street, LP5A,
Chattanooga, Tennessee 37402-2801, by telephone at (423) 751-7062, or via email at
tespink@tva.gov.

I declare under penalty of perjury that the foregoing is true and correct.

Executed on this 23rd day of July, 2008.


Jack A. Bailey
Vice President, Nuclear Generation Development

Enclosure
cc: See Page 2

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Page 2
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cc: (with Enclosure)

J. P. Berger, EDF
J. M. Sebrosky, NRC/HQ
E. Cummins, Westinghouse
S. P. Frantz, Morgan Lewis
M.W. Gettler, FP&L
R. Grumbir, NuStart
P. S. Hastings, NuStart
P. Hinnenkamp, Entergy
M.C. Kray, NuStart
D. Lindgren, Westinghouse
G. D. Miller, PG&N
M.C. Nolan, Duke Energy
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G. A. Zinke, NuStart

cc: (w/o Enclosure)

B. C. Anderson, NRC/HQ
M.M. Comar, NRC/HQ
B. Hughes/NRC/HQ
R. G. Joshi, NRC/HQ
R. H. Kitchen, PGN
M.C. Kray, NuStart
A. M. Monroe, SCE&G
C. R. Pierce, SNC
R. Reister, DOE/PM
L. Reyes, NRC/RII
T. Simms, NRC/HQ

Enclosure
TVA letter dated July 23, 2008
Trip Report Actions

Actions Identified by NRC Trip Report Related to May 13-16, 2008, Hydrology-Related Site Visit.

(8 pages, including this list)

Item 1 indicates that the NRC Staff requested the Tennessee Valley Authority (TVA) to document in a letter that it was revising its schedule for a planned revision to the April 17, 2008, white paper regarding the hydrology analysis description and to provide a justification for why the delay should not impact the overall schedule. This information was provided to NRC in a letter from TVA dated June 30, 2008.

Item 2 indicates that the NRC Staff requested the TVA to identify the schedule for completion of various items related to 1) the confirmation of the input data packages for the SOCH model, 2) the availability of the SOCH model simulations, and 3) completion of the verification and validation of the SOCH computer code. This information was provided to NRC in a second letter from TVA dated June 30, 2008.

Item 3 indicates that the TVA would provide a revised porosity analysis. This information is provided on the remaining pages of this enclosure.

Item 4 indicates that the NRC Staff would be requesting additional information. TVA will respond to the requests for additional information (RAI) following receipt of each formal request.

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**NRC Hydrology Site Visit Trip Report Action 3
Related to Discussion Items 12 and 25**

This information addresses item 3 identified in the NRC hydrology site visit trip report. During the site visit, TVA had indicated that the porosity value used for determining the groundwater velocity at the BLN site had been determined to be incorrect and that the evaluation and FSAR description would be revised. Related items are identified in the trip report as discussion items numbered 12 and 25.

The identified actions to revise the evaluation are:

1. Determine correct porosity value to be used in calculations.
2. Determine the proper value of hydraulic conductivity to be used in calculations.
3. Tie porosity information from Section 2.5 to Section 2.4.
4. Determine proper groundwater velocity.
5. Identify necessary FSAR updates associated with above items.
6. Provide pump test report data to the NRC.

These required actions are addressed in the following BLN RESPONSE as follows:

1. The revised porosity value is determined and the value and supporting information are contained in Section 2.0 and Attachment A.
2. The revised hydraulic conductivity value is determined and is contained in Section 1.0, second paragraph, Subsection 3.1.
3. With the FSAR corrections associated with actions 1 and 2 above, the porosity values used in Section 2.4 are changed to specific values for the depths of interest for the groundwater velocity calculations. Section 2.5 was investigated and determined to discuss total boring program void ratios encountered; these Section 2.5 void ratios described are not used in Section 2.4.
4. Groundwater velocity calculations are revised with the process, assumptions, and supporting documentation described in Sections 1.0 through 4.0.
5. FSAR changes related to the revised porosity value are addressed in "ASSOCIATED BLN COL APPLICATION REVISIONS", items #1 and #4.
FSAR changes related to the revised hydraulic conductivity value are addressed in "ASSOCIATED BLN COL APPLICATION REVISIONS", item #4.
FSAR changes related to the revised groundwater velocity calculations are addressed in "ASSOCIATED BLN COL APPLICATION REVISIONS", items #2 through #5.
6. Pump test report data is provided in Attachment B.

BLN RESPONSE:

1.0 Introduction

On May 13, 2008, it was determined that the porosity value identified in Subsection 2.4.12.2.4.2 of the BLN FSAR required revision. The FSAR states that the porosity of the upper 20 feet of the Stones River Group limestone was historically reported as 0.04 and the porosity determined during the 2006 pre-COL application investigation was 0.05.

Additionally, Subsection 2.4.12.3 stated that, for conservatism, the highest hydraulic conductivity measured on-site to-date was used in the calculations. The hydraulic conductivity from the September, 2006 aquifer pump testing (observation well OW-12 value) was used (3.95×10^{-3} cm/s); however, it has been determined that the packer test from boring B-1046 reported a hydraulic conductivity of 4.2×10^{-3} cm/s. Therefore, this value is also being revised.

The groundwater velocities for the BLN site have been recalculated using a formation porosity of 0.018 and the B-1046 packer test hydraulic conductivity of 4.2×10^{-3} cm/s with the calculated monthly groundwater velocities (in ft/day) from Unit #3 towards Town Creek (Figure 1a) as follows:

| 7/11/06 | 8/31/06 | 9/21/06 | 10/26/06 | 11/13/06 | 12/11/06 | 1/4/07 | 2/1/07 | 3/5/07 | 4/17/07 | 5/8/07 |
|---------|---------|---------|----------|----------|----------|--------|--------|--------|---------|--------|
| 1.20 | 2.24 | 2.49 | 2.84 | 2.90 | 2.17 | 3.05 | 3.32 | 3.32 | 3.05 | 2.49 |

Although the conservative groundwater pathway was assessed from Unit #4 to the Intake Channel (see Figure 1b), this pathway is considered unlikely due to the flow dynamics near the southeast edge of the Unit #4 construction zone and monthly variations in observed groundwater flow gradient direction.

2.0 Porosity Evaluation

The ratio of voids encountered to the length of the core borings (void ratio), roughly equivalent to the formation, or “karst,” porosity, was 0.005 for the core borings performed during the 2006 geotechnical investigation (see Attachment A). As the majority of groundwater is considered to move in the upper 20 feet of rock (i.e., the epikarst) the void ratios were determined for the intervals 5 ft, 10 ft, 20 ft, and 30 ft below the top of rock. These ratios are presented as follows:

| | |
|---------------------|-------|
| Top 5 feet of rock | 0.014 |
| Top 10 feet of rock | 0.021 |
| Top 20 feet of rock | 0.018 |
| Top 30 feet of rock | 0.013 |

As predicted, the upper 5 to 20 feet of rock has the highest porosity and therefore, should constitute the majority of groundwater flow. Because the field boring program was only able to identify voids greater than or equal to approximately 0.1 ft thick, this void ratio would be an underestimation of the actual porosity within the formation. However, this method would not be able to determine that amount of the total void space that was isolated from, or poorly connected

to, the main groundwater hydrologic flow pathways, thus potentially causing an overestimation of the effective formation porosity.

The highest porosity value is reported in the upper 10 ft of rock (0.021), however, to allow for conservatism and account for potential unconnected and undetected void spaces, the effective porosity is estimated as the void ratio of the upper 20 ft of rock, or 0.018.

3.0 Groundwater Velocity Calculations

Based on information from present and previous field investigations, the karst system in the area of the BLN facility is poorly developed in that groundwater flow within the aquifer is dominated by poorly integrated pores, joints, and tubes, most with soil or clay fill. Karst aquifers exhibiting these types of groundwater conditions are termed "diffuse-type" karst aquifer systems. Due to the similarities of flow and response to aquifer input and drainage, movement of water through a diffuse karst aquifer is similar to conditions found within a granular (sand, silt, gravel) aquifer system. Movement of water in a granular aquifer can be characterized by use of Darcy's Law; therefore, application of Darcy's Law calculations is appropriate for a diffuse karst aquifer system as found at the BLN.

3.1 Pathway #1: Unit #3 to Town Creek

Based on the above findings, the groundwater velocities for the BLN site have been recalculated using a formation porosity of 0.018 and a hydraulic conductivity of 4.2×10^{-3} cm/s. Monthly groundwater velocities from Unit #3 towards Town Creek are presented in Table 1.

The sensitivity of the groundwater velocity calculations to potential differences in the actual formation porosity was investigated by calculating groundwater velocities for the range of reported porosities for the upper 5 ft, 10 ft, 20 ft, and 30 ft rock intervals, as discussed above. As shown in Table 2, and graphically depicted in Figure 2, groundwater velocities increase with decreasing porosity. Because groundwater flows are expected to be greatest in the regions with highest porosity, and porosities rapidly decrease below the top 20 ft of rock, the 30 ft porosity value was considered overly conservative. As the majority of water flow will be concentrated in the 5 to 20 foot rock depth region, the 20 ft porosity value was chosen as the conservative value as it produced higher groundwater flow velocities than the 10 ft porosity value and should capture the zone of greatest groundwater flow, compensating for undetected and unconnected voids.

The sensitivity of the groundwater velocity calculations to potential differences in the actual formation hydraulic conductivity was investigated by assessing groundwater velocities for a range of hydraulic conductivities, also compared to changing range of porosities. The highest hydraulic conductivity value (4.2×10^{-3} cm/s) was reported from packer testing of boring B-1046. As shown in Table 3, and graphically depicted in Figure 3, the average monthly groundwater velocities increase linearly by 0.08 ft/day for each 0.1×10^{-3} cm/s increase in hydraulic conductivity. Historic and recent maximum hydraulic conductivities at the site have all been reported in the same magnitude or lower than 4.2×10^{-3} cm/s; therefore, the packer test value reported from boring B-1046 is considered a conservative value and used in the groundwater velocity calculations.

3.2 Pathway #2: Unit #4 to the Intake Channel

Although the conservative groundwater pathway was assessed from Unit #4 to the Intake Channel (Table 4), this scenario is considered unlikely due to the flow dynamics near the southeast edge of the Unit #4 construction zone and monthly variations in observed groundwater flow gradient direction. Groundwater velocities were determined between MW-1205c and MW-1211c (Table

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5) to assess the time that would be required for a release in the vicinity of BLN Unit #4 to reach the point where the potential groundwater surface would intersect the backfilled portion of the Essential Raw Cooling Water (ERCW) trench, determined to be approximately 680 feet from MW-1205c. Using the monthly groundwater elevations in MW-1205c and MW-1211c between July 11, 2006 and May 8, 2007, this assessment showed that the overall trend of groundwater movement from MW-1205c would be away from the intake structure (shown as negative distance values in Table 5) and groundwater from the area of BLN Unit #4 would not migrate towards the intake structure far enough to enter the ERCW trench. Therefore, this groundwater would not likely migrate to the Intake Channel.

4.0 Conclusions

Groundwater flow path and aquifer parameters of porosity and hydraulic conductivity are very difficult to determine within a poorly developed karstic system as is present at the BLN. To compensate for the inherent difficulties of determining aquifer characteristics within this type of groundwater system, a worst case method of postulating a single, straight line/shortest distance groundwater transport has been used to simplify the complex groundwater system and provide conservative values of groundwater flow velocity and transport times.

Based on this analysis, TVA has determined that using the calculated formation porosity of 0.018, from the void ratio of the upper 20 ft of rock, and the B-1046 packer test hydraulic conductivity of 4.2×10^{-3} cm/s, provides a conservative estimate of the worst case groundwater velocities and groundwater transport for any accidental release from the BLN.

Groundwater velocities were recalculated based on the corrected values of porosity and hydraulic conductivity previously described and are presented in the revised FSAR Table 2.4.12-206. This analysis resulted in faster groundwater travel times than was previously reported. Revisions to the BLN COL application are described below.

ASSOCIATED BLN COL APPLICATION REVISIONS:

1. COLA Part 2, FSAR, Chapter 2, Subsection 2.4.12.2.4.2, 1st paragraph, will be revised from:

Water occurs in the Stones River Group Limestone in openings along fractures and bedding planes in bedrock (some of which are solutionally enlarged), and in pore spaces in the overburden. Porosity of the Stones River Group Formation limestone above and below a 20-ft. depth is 0.04 and 0.01, respectively. Total porosity is estimated at 0.05 based on total number of voids encountered during the 2006 pre-COL application site investigation; however, this is probably an underestimation of total porosity as many small cavities and fractures were not captured in the estimate.

To read:

Water occurs in the Stones River Group Limestone in openings along fractures and bedding planes in bedrock (some of which are solutionally enlarged), and in pore spaces in the overburden. Total porosity of the Stones River Group Formation limestone in the area of the BLN was determined to be approximately 0.005, based on total number of voids encountered during the 2006 pre-COL application site investigation (Subsection 2.5.4.1.3.1); however, this is probably an underestimation of total porosity as many small cavities and fractures were not captured in the estimate.

As the majority of groundwater is considered to move in the upper 20 feet of rock (i.e., epikarst) the void ratios were determined for the intervals 5 ft, 10 ft, 20 ft, and 30 ft below the

top of rock. The upper 5 to 20 feet of rock has the highest porosity and therefore, should constitute the majority of groundwater flow. As the field boring program was only able to identify voids greater than or equal to approximately 0.1 ft thick, the void ratio identified in Section 2.5 would be an underestimation of the actual formation porosity within the formation. Further, this method would not be able to determine that amount of the total void space that was isolated from, or poorly connected to, the main groundwater hydrologic flow pathways, thus potentially causing an overestimation of the effective formation porosity.

The highest porosity value is reported in the upper 10 ft of rock (0.021), however, to allow for conservatism and account for potential unconnected and undetected void spaces, the effective porosity is estimated as the void ratio of the upper 20 ft of rock, or 0.018.

2. COLA Part 2, FSAR, Chapter 2, Subsection 2.4.12.2.4.2, 2nd to last paragraph, will be revised from:

Monthly groundwater gradients were calculated to be 1.8×10^{-3} - 5.0×10^{-3} from Unit 3 to the Town Creek embayment, and 5.0×10^{-3} - 6.7×10^{-3} between Unit 4 and the intake structure channel. Monthly groundwater flow velocities were calculated to be 0.5 – 1.4 ft/day from Unit 3 to the Town Creek embayment, and 1.4 – 1.9 ft/day between Unit 4 and the intake structure channel. A summary of the monthly groundwater hydraulic gradients and flow velocities is presented in Table 2.4.12-206. Groundwater flow from Unit 4 towards the intake structure channel only occurs for short periods of time during wet months and normally flows towards Town Creek during the majority of the year.

To read:

Monthly groundwater gradients were calculated to be 1.8×10^{-3} - 5.0×10^{-3} from Unit 3 to the Town Creek embayment, and 5.0×10^{-3} - 6.7×10^{-3} between Unit 4 and the intake structure channel. Monthly groundwater flow velocities were calculated to be 1.20 – 3.32 ft/day from Unit 3 to the Town Creek embayment, and 3.31 – 4.44 ft/day between Unit 4 and the intake structure channel. A summary of the monthly groundwater hydraulic gradients and flow velocities is presented in Table 2.4.12-206. Groundwater flow from Unit 4 towards the intake structure channel only occurs for short periods of time during wet months and normally flows towards Town Creek during the majority of the year.

3. COLA Part 2, FSAR, Chapter 2, Subsection 2.4.12.2.4.2, last paragraph, will be revised from:

Horizontal groundwater flow velocities were determined using a conservative straight-line-flow bounding method from the groundwater well nearest the liquid radioactive waste tank in the unit closest to the discharge point using the highest measured hydraulic conductivity on-site. A straight line flow path is considered the most conservative because the actual groundwater pathways are expected to be tortuous, resulting in longer transport times, and hydraulic conductivities of the fractures/joints lower than the highest measured on-site. Because of the lower hydraulic conductivities in the soil and deeper bedrock, the majority of groundwater flow is conservatively assumed to be within the epikarst zone. Groundwater conditions are further discussed in Subsection 2.5.4.6. Groundwater characteristics associated with the karst development at the BLN is discussed in detail in Subsection 2.5.4.1.

To read:

Horizontal groundwater flow velocities were determined using a conservative straight-line-flow bounding method from the groundwater well nearest the liquid radioactive waste tank in the unit closest to the discharge point using the highest measured hydraulic conductivity on-site. A straight line flow path is considered the most conservative because the actual groundwater pathways are expected to be tortuous, resulting in longer transport times, and hydraulic

conductivities of the fractures/joints lower than the highest measured on-site. Because of the lower hydraulic conductivities in the soil and deeper bedrock, the majority of groundwater flow is conservatively assumed to be within the epikarst zone.

Based on information from present and previous field investigations, the karst system in the area of the BLN facility is poorly developed in that groundwater flow within the aquifer is dominated by poorly integrated pores, joints, and tubes, most with soil or clay fill. Karst aquifers exhibiting these types of groundwater conditions are termed "diffuse-type" karst aquifer systems. Due to the similarities of flow and response to aquifer input and drainage, movement of water through a diffuse karst aquifer is similar to conditions found within a granular (sand, silt, gravel) aquifer system. Movement of water in a granular aquifer can be characterized by use of Darcy's Law; therefore, application of Darcy's Law calculations is appropriate for a diffuse karst aquifer system as found at the BLN (Reference 249).

Groundwater conditions are further discussed in Subsection 2.5.4.6. Groundwater characteristics associated with the karst development at the BLN is discussed in detail in Subsection 2.5.4.1.

4. COLA Part 2, FSAR, Chapter 2, Table 2.4.12-206 (2 Sheets), will be replaced with the revised Table 2.4.12-206 (2 Sheets) provided in the ASSOCIATED BLN COL APPLICATION REVISIONS ATTACHMENTS (following Attachment B).
5. COLA Part 2, FSAR Chapter 2, Subsection 2.4.16, will be revised to add the following new reference:
 249. U.S. Environmental Protection Agency, *Ground-Water Monitoring in Karst Terranes, Recommended Protocols & Implicit Assumptions*, EPA / 600 / x-89 / 050, March 1989.

ATTACHMENTS/ENCLOSURES:

FIGURES (7 pages including the cover sheet)

- Figure 1a: Conceptual Groundwater Pathway #1
- Figure 1b: Conceptual Groundwater Pathway #2
- Figure 2: Change in Groundwater Velocity with Change in Porosity
- Figure 3: Average Groundwater Velocity
- Figure 4: Table 5 Velocity Function
- Figure 5: Groundwater Distance Traveled

TABLES (6 pages including the cover sheet)

- Table 1: Monthly Groundwater Gradient and Flow Velocity: BLN Unit #3 to Town Creek
- Table 2: Change in Velocity due to Change in Porosity with Depth
- Table 3: Average Monthly Change in Groundwater Velocity due to Change in Porosity and Hydraulic Conductivity

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Table 4: Monthly Groundwater Gradient and Flow Velocity: BLN Unit #4 to Intake Channel

Table 5: Groundwater Travel Distance from MW-1205c to MW-1211c

ATTACHMENT A (3 pages including the cover sheet)

William Lettis Associates, Inc., Determination of Stones River Group Void Ratios for the BLN Site

ATTACHMENT B (38 pages including the cover sheet)

BLN Pump Test Report Data

ASSOCIATED BLN COL APPLICATION REVISIONS ATTACHMENTS (3 pages including the cover sheet)

Revised Table 2.4.12-206, 2 Sheets

FIGURES

TOWN CREEK EMBAYMENT

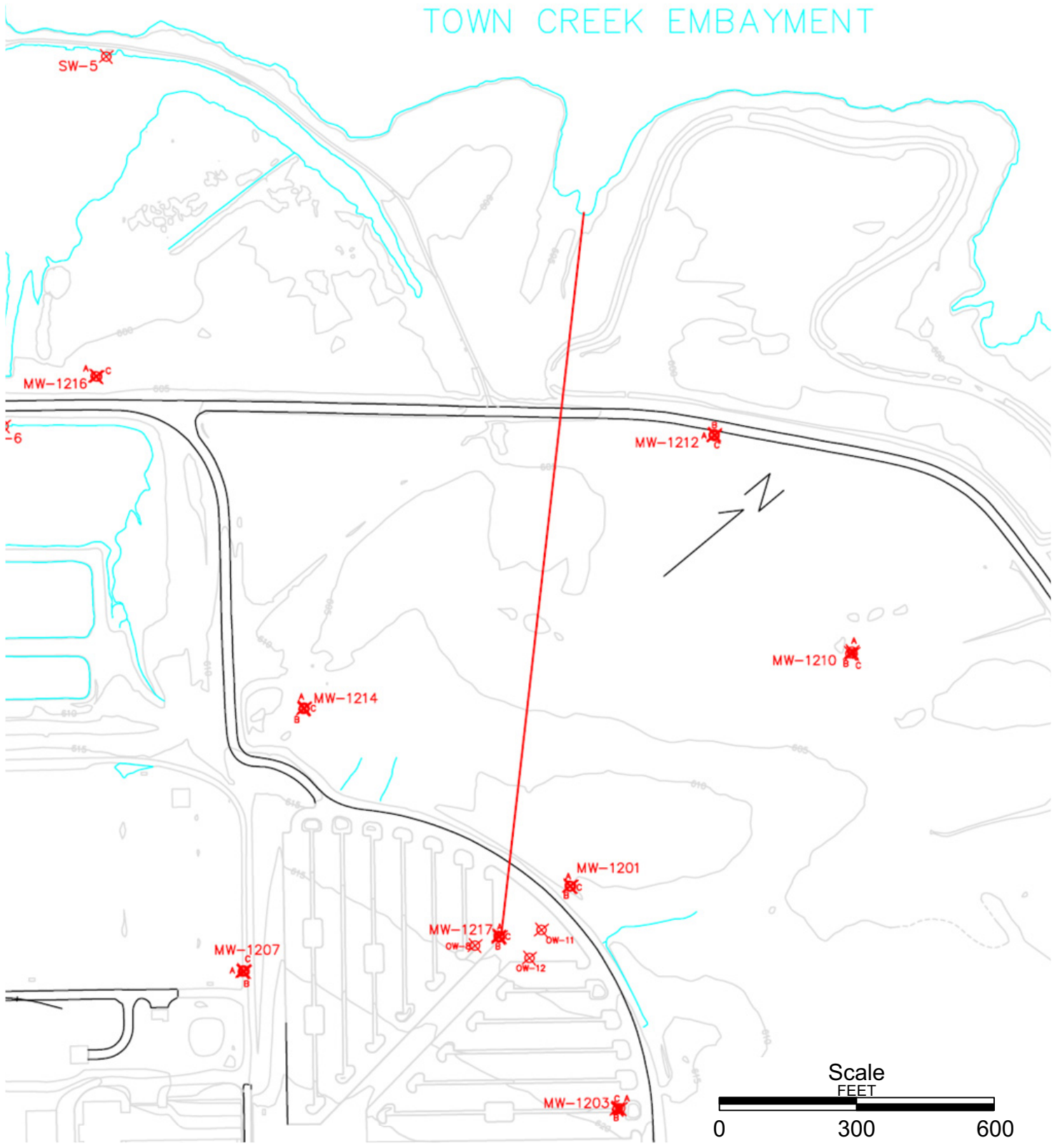


Figure 1a: Conceptual Groundwater Pathway #1

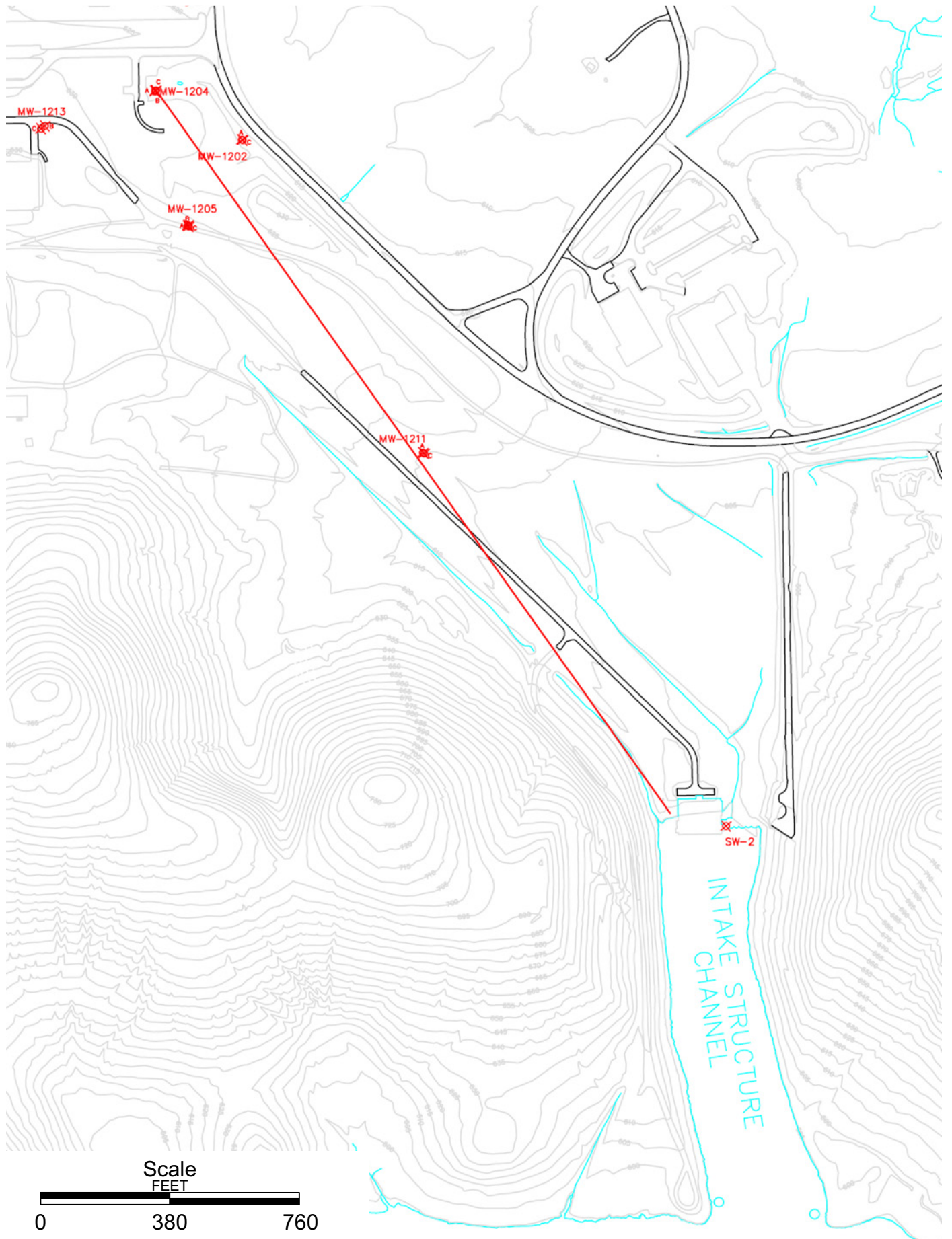


Figure 1b: Conceptual Groundwater Pathway #2

Figure 2
Change in Groundwater Velocity with Change in Porosity

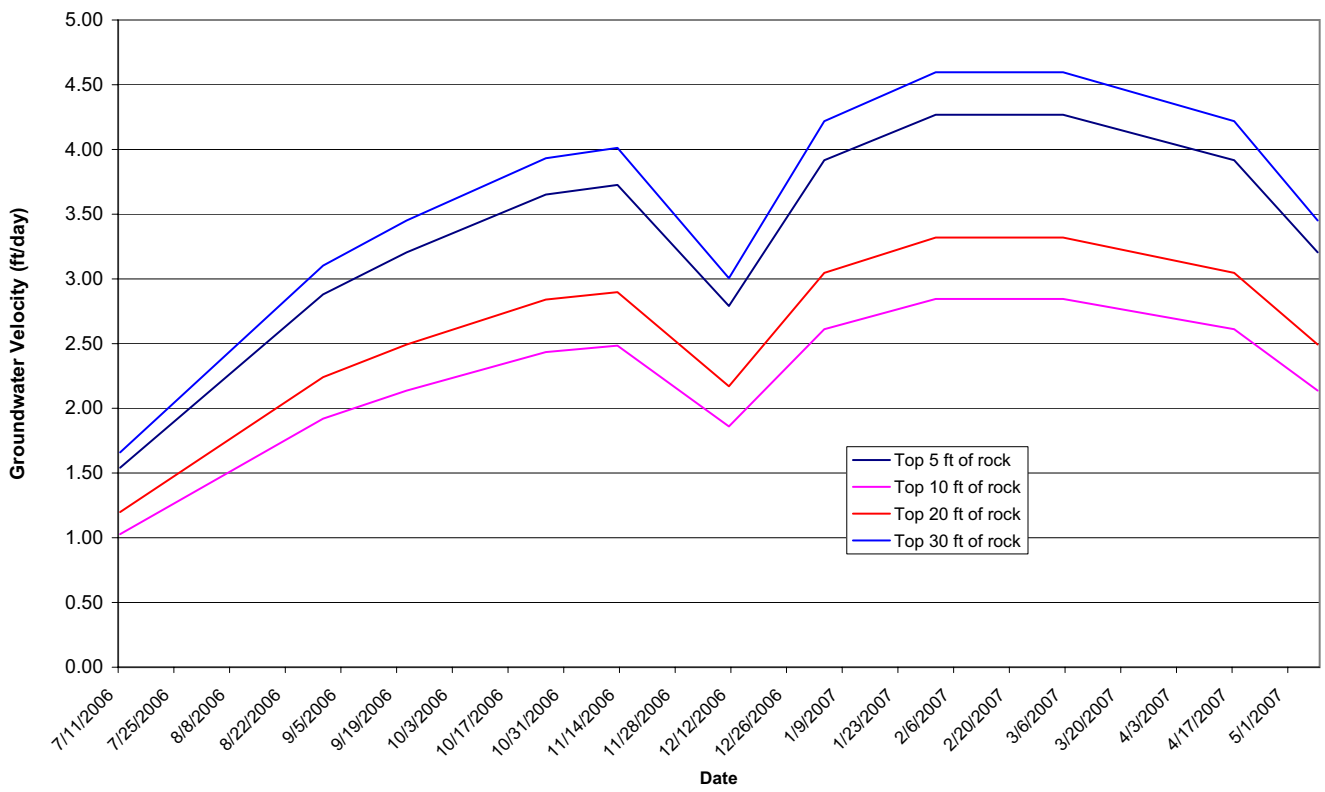


Figure 3
Average Groundwater Velocity

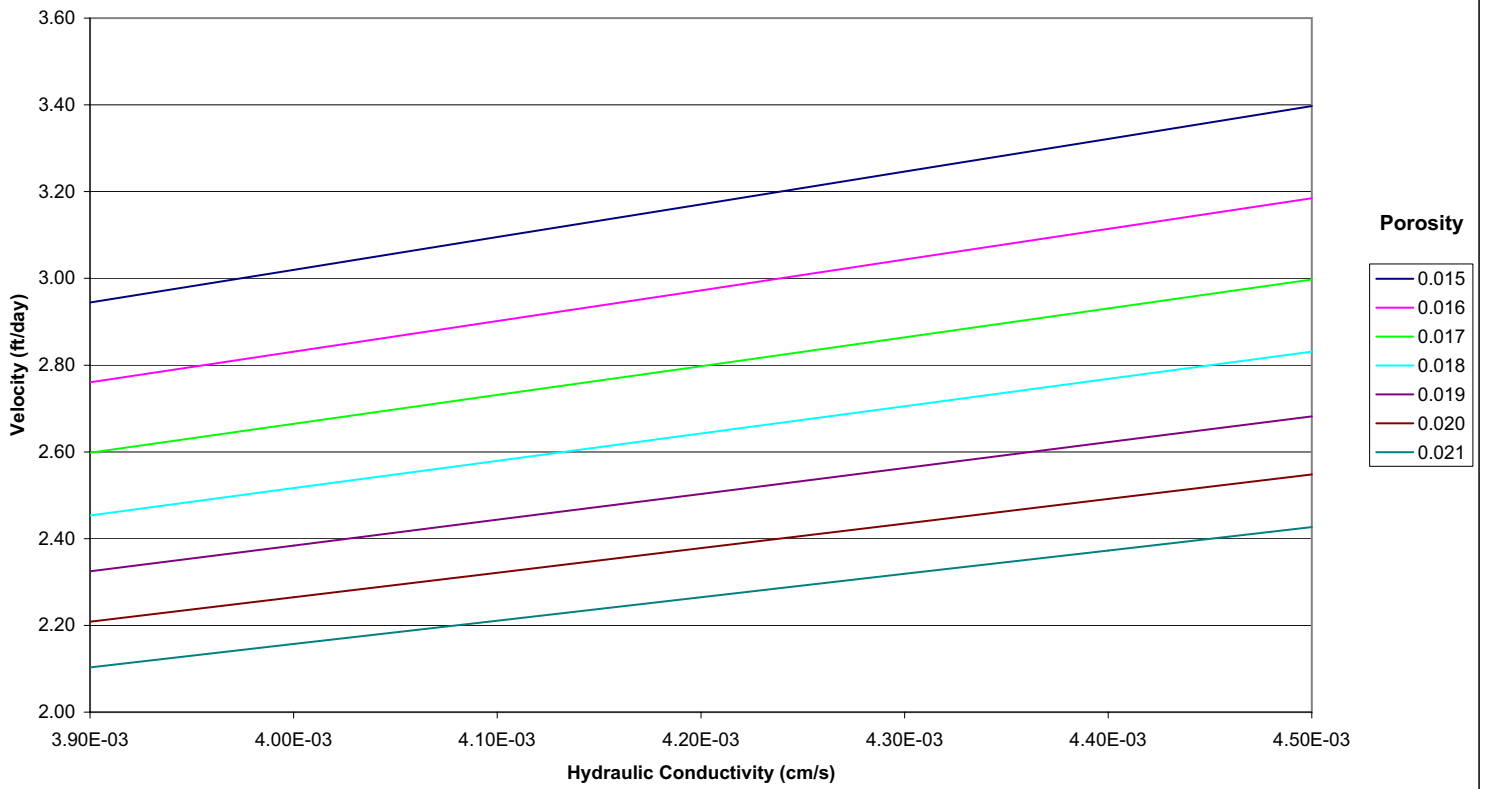


Figure 4
Table 5 Velocity Function

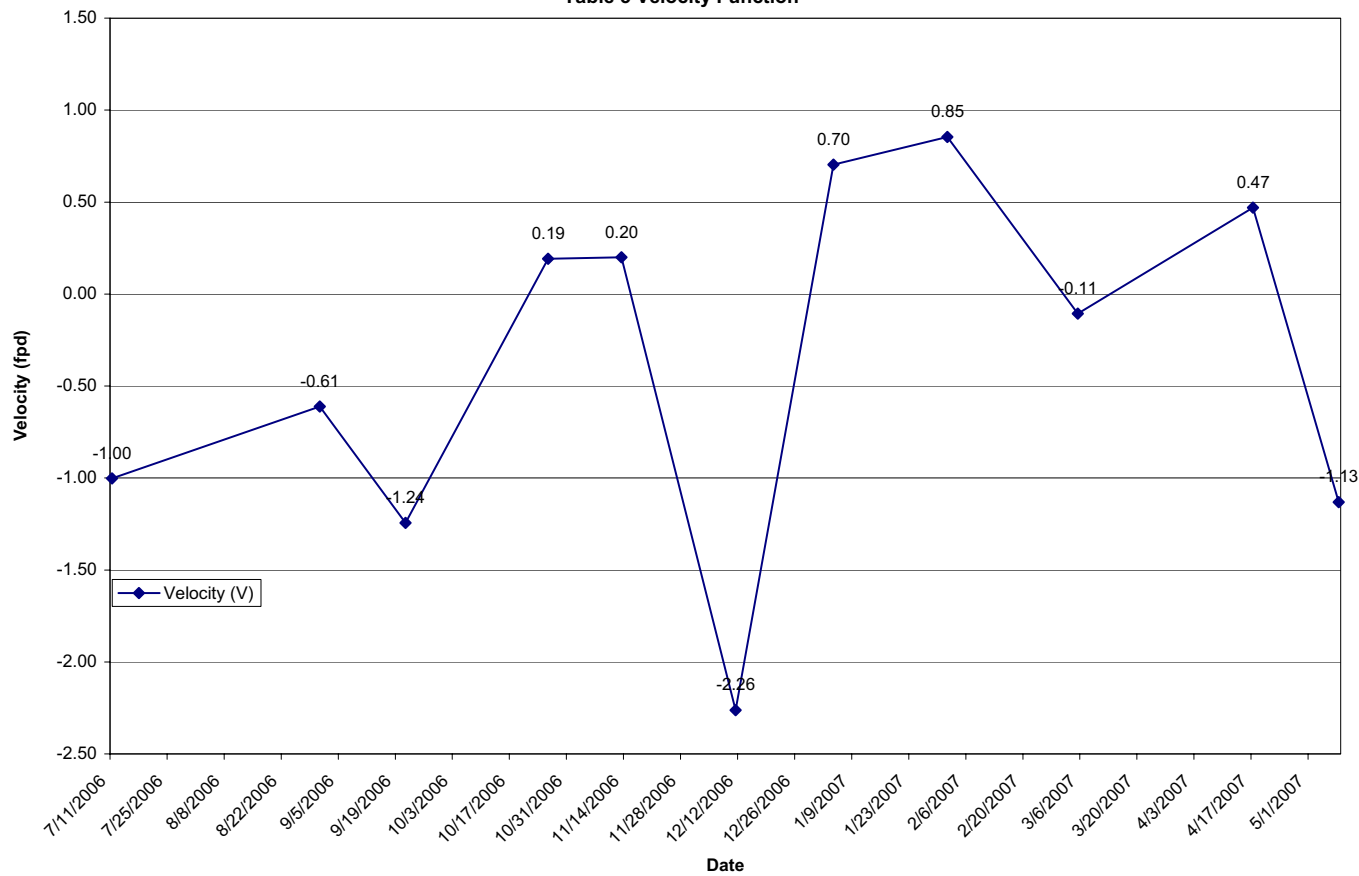
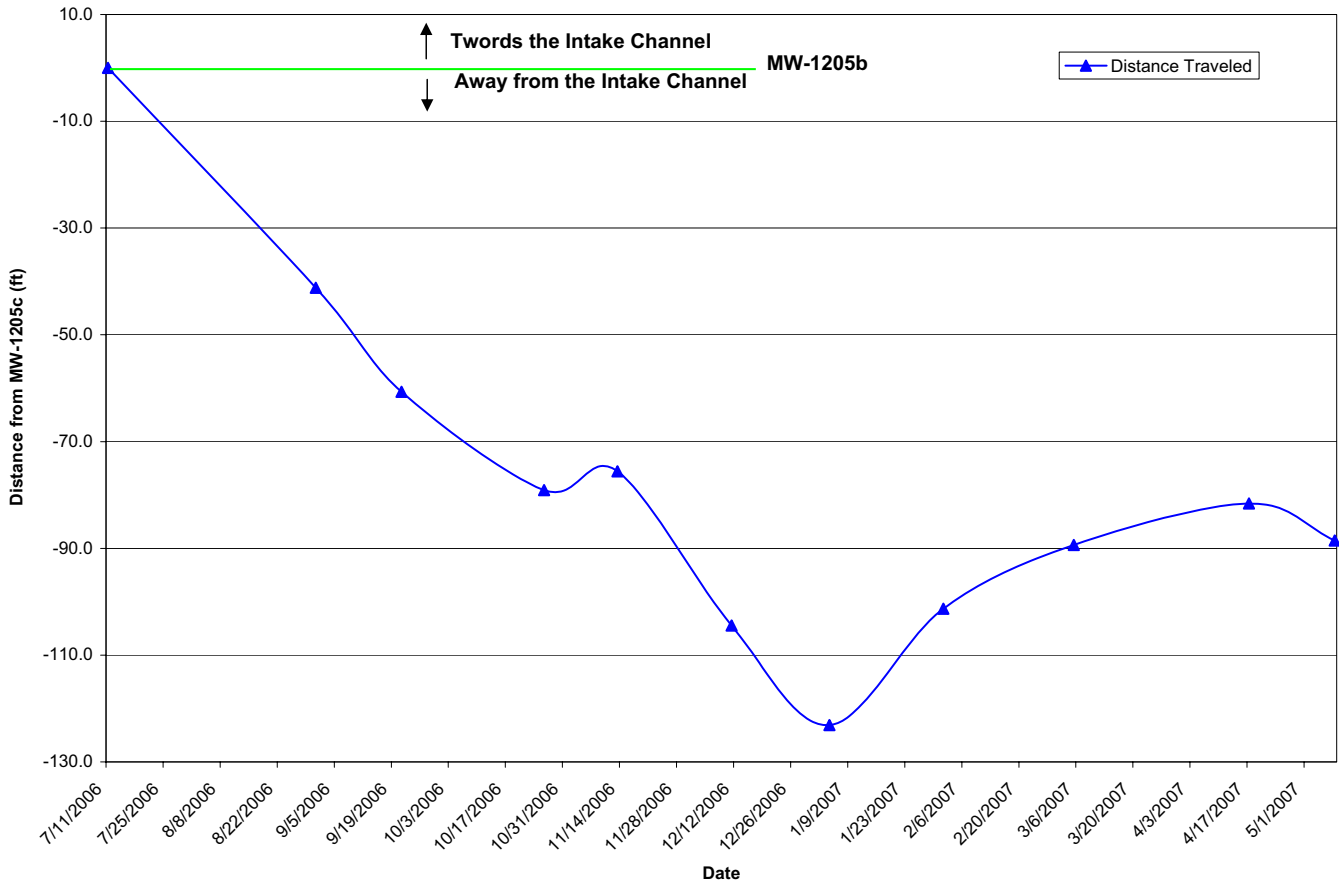


Figure 5
Groundwater Distance Traveled



TABLES

Table 1
Monthly Groundwater Hydraulic Gradient and Flow Velocity
BLN Unit #3 to Town Creek

| Date | | 07/11/06 | 08/31/06 | 09/21/06 | 10/26/06 | 11/13/06 | 12/11/06 | 01/04/07 | 02/01/07 | 03/05/07 | 04/17/07 | 05/08/07 |
|------------------------------|--------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| Elevation High (Eh) | ft | 598.08 | 600.07 | 599.97 | 601.38 | 601.69 | 599.23 | 602.31 | 602.14 | 602.09 | 601.94 | 600.84 |
| Elevation Low (El) | ft | 595.18 | 594.65 | 593.94 | 594.51 | 594.68 | 593.98 | 594.94 | 594.11 | 594.06 | 594.57 | 594.81 |
| Hydraulic Gradient (Eh-El)/L | ft/ft | 1.81E-03 | 3.39E-03 | 3.77E-03 | 4.29E-03 | 4.38E-03 | 3.28E-03 | 4.61E-03 | 5.02E-03 | 5.02E-03 | 4.61E-03 | 3.77E-03 |
| Velocity (V) | ft/day | 1.20 | 2.24 | 2.49 | 2.84 | 2.90 | 2.17 | 3.05 | 3.32 | 3.32 | 3.05 | 2.49 |
| Travel Time (T) | days | 1335 | 714 | 642 | 563 | 552 | 737 | 525 | 482 | 482 | 525 | 642 |
| | hrs | | | | | | | | | | | |
| | mins | | | | | | | | | | | |
| | hrs | 3.65 | 1.96 | 1.76 | 1.54 | 1.51 | 2.02 | 1.44 | 1.32 | 1.32 | 1.44 | 1.76 |
| Pathway Distance (L) | ft | 1,600 | | | | | | | | | | |
| Hydraulic Conductivity (Kh) | cm/sec | 4.20E-03 | | | | | | | | | | |
| | ft/sec | 1.38E-04 | | | | | | | | | | |
| | ft/day | 11.9055 | | | | | | | | | | |
| porosity (η) | | 0.018 | | | | | | | | | | |

Assumptions: Hydraulic gradient is between MW-1217b (Eh) and SW-4 Town Creek Embayment surface (El)

Equation for Velocity: $V = (Kh (Eh-El)/L)/\eta$ Darcy equation for Average Linear Velocity

Equations for Travel Time: $T = L/V$

Conversions: 1day = 86,400 seconds; 1 foot = 30.48 centimeters; 1 year = 365.25 days

| | | |
|------------------------|--------|--------|
| Average GW Velocity | ft/day | 2.64 |
| Average GW Travel Time | days | 654.51 |
| | hrs | 1.79 |

Table 2
Change in Velocity due to Change in Porosity with Depth
BLN Unit #3 to Town Creek

| Date | | 07/11/06 | 08/31/06 | 09/21/06 | 10/26/06 | 11/13/06 | 12/11/06 | 01/04/07 | 02/01/07 | 03/05/07 | 04/17/07 | 05/08/07 |
|-------------------------------------|--------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| Elevation High (Eh) | ft | 598.08 | 600.07 | 599.97 | 601.38 | 601.69 | 599.23 | 602.31 | 602.14 | 602.09 | 601.94 | 600.84 |
| Elevation Low (El) | ft | 595.18 | 594.65 | 593.94 | 594.51 | 594.68 | 593.98 | 594.94 | 594.11 | 594.06 | 594.57 | 594.81 |
| Hydraulic Gradient (Eh-El)/L | ft/ft | 1.81E-03 | 3.39E-03 | 3.77E-03 | 4.29E-03 | 4.38E-03 | 3.28E-03 | 4.61E-03 | 5.02E-03 | 5.02E-03 | 4.61E-03 | 3.77E-03 |
| Velocity (V) | | | | | | | | | | | | |
| $\eta = 0.014$ | ft/day | 1.54 | 2.88 | 3.20 | 3.65 | 3.73 | 2.79 | 3.92 | 4.27 | 4.27 | 3.92 | 3.20 |
| $\eta = 0.021$ | ft/day | 1.03 | 1.92 | 2.14 | 2.43 | 2.48 | 1.86 | 2.61 | 2.85 | 2.85 | 2.61 | 2.14 |
| $\eta = 0.018$ | ft/day | 1.20 | 2.24 | 2.49 | 2.84 | 2.90 | 2.17 | 3.05 | 3.32 | 3.32 | 3.05 | 2.49 |
| $\eta = 0.013$ | ft/day | 1.66 | 3.10 | 3.45 | 3.93 | 4.01 | 3.00 | 4.22 | 4.60 | 4.60 | 4.22 | 3.45 |
| Travel Time (T) | | | | | | | | | | | | |
| $\eta = 0.014$ | yrs | 2.84 | 1.52 | 1.37 | 1.20 | 1.18 | 1.57 | 1.12 | 1.03 | 1.03 | 1.12 | 1.37 |
| $\eta = 0.021$ | yrs | 4.26 | 2.28 | 2.05 | 1.80 | 1.76 | 2.35 | 1.68 | 1.54 | 1.54 | 1.68 | 2.05 |
| $\eta = 0.018$ | yrs | 3.65 | 1.96 | 1.76 | 1.54 | 1.51 | 2.02 | 1.44 | 1.32 | 1.32 | 1.44 | 1.76 |
| $\eta = 0.013$ | yrs | 2.64 | 1.41 | 1.27 | 1.11 | 1.09 | 1.46 | 1.04 | 0.95 | 0.95 | 1.04 | 1.27 |
| Pathway Distance (L) | ft | 1,600 | | | | | | | | | | |
| Hydraulic Conductivity (Kh) | cm/sec | 4.20E-03 | | | | | | | | | | |
| | ft/sec | 1.38E-04 | | | | | | | | | | |
| | ft/day | 11.9055 | | | | | | | | | | |
| porosity (η) | | | | | | | | | | | | |
| Top 5 ft of rock | | 0.014 | | | | | | | | | | |
| Top 10 ft of rock | | 0.021 | | | | | | | | | | |
| Top 20 ft of rock | | 0.018 | | | | | | | | | | |
| Top 30 ft of rock | | 0.013 | | | | | | | | | | |

Assumptions: Hydraulic gradient is between MW-1217b (Eh) and SW-4 Town Creek Embayment surface (El)

Equation for Velocity: $V = (Kh (Eh-El)/L)/n$ Darcy equation for Average Linear Velocity

Equations for Travel Time: $T = L/V$

Conversions: 1day = 86,400 seconds; 1 foot = 30.48 centimeters; 1 year = 365.25 days

Table 3
Average Monthly Change in Groundwater Velocity
due to Change in Porosity and Hydraulic Conductivity
BLN Unit #3 to Town Creek

| Date | | 07/11/06 | 08/31/06 | 09/21/06 | 10/26/06 | 11/13/06 | 12/11/06 | 01/04/07 | 02/01/07 | 03/05/07 | 04/17/07 | 05/08/07 |
|------------------------------|--------------|--|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|----------|----------|----------|----------|
| Elevation High (Eh) | ft | 598.08 | 600.07 | 599.97 | 601.38 | 601.69 | 599.23 | 602.31 | 602.14 | 602.09 | 601.94 | 600.84 |
| Elevation Low (El) | ft | 595.18 | 594.65 | 593.94 | 594.51 | 594.68 | 593.98 | 594.94 | 594.11 | 594.06 | 594.57 | 594.81 |
| Hydraulic Gradient (Eh-El)/L | ft/ft | 1.81E-03 | 3.39E-03 | 3.77E-03 | 4.29E-03 | 4.38E-03 | 3.28E-03 | 4.61E-03 | 5.02E-03 | 5.02E-03 | 4.61E-03 | 3.77E-03 |
| | | Hydraulic Conductivity (cm/sec) | | | | | | | | | | |
| Velocity (V) (ft/day) | | 3.90E-03 | 4.00E-03 | 4.10E-03 | 4.20E-03 | 4.30E-03 | 4.40E-03 | 4.50E-03 | | | | |
| | porosity (n) | 0.015 | 2.94 | 3.02 | 3.10 | 3.17 | 3.25 | 3.32 | 3.40 | | | |
| | | 0.016 | 2.76 | 2.83 | 2.90 | 2.97 | 3.04 | 3.11 | 3.18 | | | |
| | | 0.017 | 2.60 | 2.66 | 2.73 | 2.80 | 2.86 | 2.93 | 3.00 | | | |
| | | 0.018 | 2.45 | 2.52 | 2.58 | 2.64 | 2.71 | 2.77 | 2.83 | | | |
| | | 0.019 | 2.32 | 2.38 | 2.44 | 2.50 | 2.56 | 2.62 | 2.68 | | | |
| | | 0.020 | 2.21 | 2.26 | 2.32 | 2.38 | 2.43 | 2.49 | 2.55 | | | |
| | | 0.021 | 2.10 | 2.16 | 2.21 | 2.26 | 2.32 | 2.37 | 2.43 | | | |
| Pathway Distance (L) | ft | 1,600 | | | | | | | | | | |
| Hydraulic Conductivity (Kh) | cm/sec | 3.90E-03 | 4.00E-03 | 4.10E-03 | 4.20E-03 | 4.30E-03 | 4.40E-03 | 4.50E-03 | | | | |
| | ft/sec | 1.28E-04 | 1.31E-04 | 1.35E-04 | 1.38E-04 | 1.41E-04 | 1.44E-04 | 1.48E-04 | | | | |
| | ft/day | 11.0551 | 11.3386 | 11.6220 | 11.9055 | 12.1890 | 12.4724 | 12.7559 | | | | |

Assumptions: Hydraulic gradient is between MW-1217b (Eh) and SW-4 Town Creek Embayment surface (El)

Equation for Velocity: $V = (Kh (Eh-El)/L)/n$ Darcy equation for Average Linear Velocity

Equations for Travel Time: $T = L/V$

Conversions: 1day = 86,400 seconds; 1 foot = 30.48 centimeters; 1 year = 365.25 days

Table 4
Monthly Groundwater Hydraulic Gradient and Flow Velocity
BLN Unit #4 to Intake Channel

| Date | | 07/11/06 | 08/31/06 | 09/21/06 | 10/26/06 | 11/13/06 | 12/11/06 | 01/04/07 | 02/01/07 | 03/05/07 | 04/17/07 | 05/08/07 |
|------------------------------|--------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| Elevation High (Eh) | ft | 608.10 | 608.57 | 608.05 | 610.58 | 610.48 | 607.99 | 612.15 | 609.99 | 610.25 | 610.40 | 608.28 |
| Elevation Low (El) | ft | 595.07 | 593.69 | 593.97 | 594.37 | 594.58 | 594.17 | 594.70 | 594.09 | 593.95 | 594.55 | 594.66 |
| Hydraulic Gradient (Eh-El)/L | ft | 5.01E-03 | 5.72E-03 | 5.42E-03 | 6.23E-03 | 6.12E-03 | 5.32E-03 | 6.71E-03 | 6.12E-03 | 6.27E-03 | 6.10E-03 | 5.24E-03 |
| Velocity (V) | ft/day | 3.31 | 3.79 | 3.58 | 4.12 | 4.04 | 3.52 | 4.44 | 4.04 | 4.15 | 4.03 | 3.46 |
| Travel Time (T) | days | 784 | 687 | 726 | 631 | 643 | 740 | 586 | 643 | 627 | 645 | 750 |
| | yrs | 2.15 | 1.88 | 1.99 | 1.73 | 1.76 | 2.02 | 1.60 | 1.76 | 1.72 | 1.77 | 2.05 |
| | | | | | | | | | | | | |
| Pathway Distance (L) | ft | 2,600 | | | | | | | | | | |
| Hydraulic Conductivity (Kh) | cm/sec | 4.20E-03 | | | | | | | | | | |
| | ft/sec | 1.38E-04 | | | | | | | | | | |
| | ft/day | 11.906 | | | | | | | | | | |
| porosity (η) | | 0.018 | | | | | | | | | | |

Assumptions: Hydraulic gradient is between MW-1204c (Eh) and SW-2 Intake Structure surface (El)
Equation for Velocity: $V = (Kh (Eh-El)/L)/n$ Darcy equation for Average Linear Velocity
Equations for Travel Time: $T = L/V$
Conversions: 1day = 86,400 seconds; 1 foot = 30.48 centimeters; 1 year = 365.25 days

| | | |
|------------------------|--------|--------|
| Average GW Velocity | ft/day | 3.86 |
| Average GW Travel Time | days | 678.25 |
| | yrs | 1.86 |

Table 5
Groundwater Travel Distance from MW-1205c to MW-1211c

| Date | | 07/11/06 | 08/31/06 | 09/21/06 | 10/26/06 | 11/13/06 | 12/11/06 | 01/04/07 | 02/01/07 | 03/05/07 | 04/17/07 | 05/08/07 |
|------------------------------|--------|-----------|-----------|-----------|----------|----------|-----------|----------|----------|-----------|----------|-----------|
| Elevation High (Eh) | ft | 607.14 | 607.95 | 606.91 | 611.15 | 610.98 | 607.18 | 612.90 | 611.61 | 610.59 | 610.59 | 607.41 |
| Elevation Low (El) | ft | 608.55 | 608.81 | 608.66 | 610.88 | 610.70 | 610.36 | 611.91 | 610.41 | 610.74 | 609.93 | 609.00 |
| Hydraulic Gradient (Eh-El)/L | ft | -1.52E-03 | -9.25E-04 | -1.88E-03 | 2.90E-04 | 3.01E-04 | -3.42E-03 | 1.06E-03 | 1.29E-03 | -1.61E-04 | 7.10E-04 | -1.71E-03 |
| Days | | | 51 | 21 | 35 | 18 | 28 | 24 | 28 | 32 | 43 | 21 |
| Velocity (V) | ft/day | -1.00 | -0.61 | -1.24 | 0.19 | 0.20 | -2.26 | 0.70 | 0.85 | -0.11 | 0.47 | -1.13 |
| Distance Traveled | ft | 0.0 | -41.2 | -19.5 | -18.4 | 3.5 | -28.9 | -18.7 | 21.8 | 11.9 | 7.8 | -6.9 |
| Total Distance Traveled | ft | 0.0 | -41.2 | -60.7 | -79.1 | -75.6 | -104.4 | -123.1 | -101.3 | -89.4 | -81.6 | -88.5 |
| Pathway Distance (L) | ft | 930 | | | | | | | | | | |
| Hydraulic Conductivity (Kh) | cm/sec | 4.20E-03 | | | | | | | | | | |
| | ft/sec | 1.38E-04 | | | | | | | | | | |
| | ft/day | 11.906 | | | | | | | | | | |
| porosity (η) | | 0.018 | | | | | | | | | | |

Assumptions: Hydraulic gradient is between MW-1205c (Eh) and MW-1211c (El)

Negative values denote groundwater flow from MW-1211c towards MW-1205c.

Pathway distance is from MW-1205c to MW-1211c (930 feet).

Equation for Velocity: $V = (Kh (Eh-El)/L)/n$ Darcy equation for Average Linear Velocity

Equations for Travel Time: $T = L/V$

Conversions: 1 day = 86,400 seconds; 1 foot = 30.48 centimeters; 1 year = 365.25 days

Assumption for Total Distance Traveled is that groundwater velocity changes linearly from one interval to the next interval.

ATTACHMENT A

| Borehole | Interval (bgs) | | Average Depth Below TOR (ft) | Thickness (ft) | Cavity Description and Drilling Notes |
|----------|----------------|--------|------------------------------|----------------|---|
| | Top | Bottom | | | |
| B-1001 | 13.4 | 14 | 1.1 | 0.8 | Clay-filled cavity. Clay (10 YR 5/6), wet, stiff, medium plasticity, sand to gravel sized limestone clasts. |
| | 15.4 | 16.1 | 6 | 0.85 | Clay-filled cavity |
| | 17.8 | 19.1 | 6 | 1.5 | Clay-filled cavity |
| | 19.8 | 20.5 | 8.4 | 0.8 | Clay-filled cavity |
| | 20.6 | 21 | 9.3 | 0.5 | Clay-filled cavity. Rod drop 20.5-21.6. 21' water circulation lost, did not recover. |
| B-1002 | 27.8 | 28 | 11.4 | 0.2 | Cavity. Poor to moderate fluid returns 51-120.5' bgs. |
| | 33.4 | 33.5 | 16.9 | 0.1 | Cavity. Poor to moderate fluid returns 51-120.5' bgs. |
| B-1008 | 18.3 | 20.5 | 6.4 | 2.2 | Clay filled cavity. Lost water circulation 18.3-21.3' and 36.4-121.3' bgs. 90% water loss. |
| | 23.9 | 24 | 10.9 | 0.1 | Clay-filled cavity |
| B-1027 | 17.4 | 17.7 | 5.2 | 0.3 | Cavity. Water circulation lost at 17'. Poor fluid return until 50' bgs. |
| B-1033 | 14.1 | 14.2 | 1.6 | 0.1 | Clay-filled cavity. |
| | 14.6 | 14.7 | 2.1 | 0.1 | Clay-filled cavity. |
| | 19 | 19.2 | 6.6 | 0.2 | Clay-filled cavity. |
| | 19.3 | 19.5 | 6.8 | 0.2 | Clay-filled cavity. |
| | 19.7 | 19.9 | 7.2 | 0.2 | Clay-filled cavity. |
| | 30.1 | 30.2 | 17.6 | 0.1 | Clay-filled cavity. |
| B-1036 | 18 | 18.1 | 2 | 0.1 | Clay-filled cavity. Water circulation lost. 20.8-22' and 40.1' bgs to the bottom of the boring. |
| | 18.2 | 18.3 | 2.2 | 0.1 | Clay-filled cavity. |
| B-1038 | 17.9 | 18 | 5.2 | 0.1 | Clay filled cavity. |
| B-1044 | 15.2 | 15.4 | 7.3 | 0.2 | Cavity. Rod drop during drilling of ~1' at 15.2' bgs. |
| | 63 | 63.1 | 55 | 0.1 | Cavity. |
| B-1046 | 27.8 | 27.9 | 4.3 | 0.1 | Calcareous clay infilled cavity. Lost water circulation at 25.4' bgs. |
| B-1050 | 16.2 | 16.9 | 1.7 | 0.7 | Clay filled cavity. No water circulation throughout boring. |
| | 17.5 | 17.7 | 2.8 | 0.2 | Clay filled cavity. No water circulation throughout boring. |
| | 18.8 | 19 | 4.1 | 0.2 | Clay filled cavity. No water circulation throughout boring. |
| B-1052 | 44.2 | 44.5 | 18.1 | 0.3 | Cavity. No water circulation throughout boring. |
| | 44.7 | 45.5 | 18.9 | 0.8 | Cavity. No water circulation throughout boring. |
| | 59.2 | 60.8 | 33.8 | 1.6 | Clay filled cavity; (7.5YR 4/8), highly plastic. |
| B-1065 | 20.1 | 20.6 | 2.8 | 0.5 | Clay-filled cavity. |
| | 24.4 | 24.5 | 6.9 | 0.1 | Clay-filled cavity. |
| | 27.7 | 27.9 | 10.3 | 0.2 | Clay-filled cavity. |
| B-1066 | 20.2 | 20.4 | 10.8 | 0.2 | Clay-filled cavity. No water circulation throughout boring. |
| B-1069 | 31.3 | 31.4 | 22 | 0.1 | Clay-filled cavity. Water circulation lost for first 26' bgs. |
| | 33.4 | 33.5 | 24.1 | 0.1 | Clay-filled cavity. |
| | 34.5 | 34.6 | 25.2 | 0.1 | Clay-filled cavity. |
| | 37.5 | 37.6 | 28.2 | 0.1 | Clay-filled cavity. |
| | 38.2 | 38.3 | 28.9 | 0.1 | Clay-filled cavity. |
| B-1070 | 8.2 | 8.8 | 5.2 | 0.6 | Clay-filled cavity. |
| B-1071 | 16.4 | 17.4 | 3.3 | 1 | Soil-filled cavity. Rod drop at ~ 16' bgs. Water circulation lost at ~28' bgs. |
| B-1072 | 14.6 | 15.4 | 8.4 | 1.2 | Soil-filled cavity. |
| | 15.7 | 15.9 | 9 | 0.2 | Soil-filled cavity. |
| | 20.4 | 28.4 | 17.6 | 8 | Soil-filled cavity. |
| | 28.8 | 29.8 | 22.5 | 1 | Soil-filled cavity. Water circulation lost at 45.5' bgs. |
| B-1074 | 16.3 | 17.6 | 11.2 | 1.3 | Clay-filled cavity. |
| | 20.1 | 21.8 | 15.2 | 1.6 | Cavity. |
| | 25 | 25.2 | 19.4 | 0.2 | Cavity. Water circulation low at 26' bgs. |
| B-1076 | 12.6 | 16.6 | 6.3 | 4 | Soil-filled cavity. Water circulation lost 13-50' bgs. |
| B-1077A | 14.5 | 14.6 | 1 | 0.1 | Clay-filled cavity. |
| B-1080 | 34.2 | 34.3 | 24.2 | 0.1 | Clay-filled cavity. No water circulation throughout boring. |
| B-1082 | 10.8 | 12.9 | 4.3 | 2.1 | Soil-filled cavity; medium stiff. |
| | 13 | 16 | 7 | 3 | Soil-filled, medium stiff |
| B-1093 | 11.5 | 11.6 | 1.7 | 0.1 | Clay-filled cavity. Slight loss of water circulation. |
| | 11.7 | 11.8 | 1.9 | 0.1 | Clay-filled cavity. Slight loss of water circulation. |
| | 12.6 | 12.7 | 2.8 | 0.1 | Clay-filled cavity. Slight loss of water circulation. |
| | 12.8 | 12.9 | 3 | 0.1 | Clay-filled cavity. Slight loss of water circulation. |
| B-1094 | 12.2 | 12.3 | 1.2 | 0.1 | Clay-filled cavity. Poor to no water circulation through 16' bgs. |
| B-1095 | 14.4 | 14.8 | 1.3 | 0.4 | Soil-filled cavity; medium stiff. |

Total rock core up to 20' into Rock
= 1974.8 Feet

Total Thickness of Cavities in top 20' of Rock (ft)
= 36.25 Feet

Total rock core up to 10' into Rock
= 1103.9 Feet

Total Thickness of Cavities in top 10' of Rock (ft) = 23.15

Total rock core up to 5' into Rock
= 508.5 Feet

Total Thickness of Cavities in top 5' of Rock (ft) = 7

Total rock core up to 30' into Rock
= 2813.4 Feet

Total Thickness of Cavities in top 30' of Rock (ft) = 37.85

| | | |
|--|---|---|
| Calculation for Percent Cavities in top 20 feet of rock | | |
| $\frac{\text{Sum Cavity length in top 20' of Rock}}{\text{Sum Core length (20 unless less rock drilled)}}$ | = | Porosity |
| $\frac{36.25}{1974.8}$ | = | 0.0184 $\frac{\text{Cavities ft}}{\text{Rock Core ft}}$ |

| | | |
|--|---|--|
| Calculation for Percent Cavities in top 10 feet of rock | | |
| $\frac{\text{Sum Cavity length in top 10' of Rock}}{\text{Sum Core length (10 unless less rock drilled)}}$ | = | Porosity |
| $\frac{23.15}{1103.9}$ | = | 0.021 $\frac{\text{Cavities ft}}{\text{Rock Core ft}}$ |

| | | |
|--|---|---|
| Calculation for Percent Cavities in top 5 feet of rock | | |
| $\frac{\text{Sum Cavity length in top 5' of Rock}}{\text{Sum Core length (5 unless less rock drilled)}}$ | = | Porosity |
| $\frac{7}{508.5}$ | = | 0.0138 $\frac{\text{Cavities ft}}{\text{Rock Core ft}}$ |

| | | |
|--|---|---|
| Calculation for Percent Cavities in top 30 feet of rock | | |
| $\frac{\text{Sum Cavity length in top 30' of Rock}}{\text{Sum Core length (30 unless less rock drilled)}}$ | = | Porosity |
| $\frac{37.85}{2814.3}$ | = | 0.0134 $\frac{\text{Cavities ft}}{\text{Rock Core ft}}$ |

ATTACHMENT B

GROUNDWATER AQUIFER TEST REPORT
BELLEFONTE NUCLEAR SITE
SCOTTSBORO, JACKSON COUNTY, ALABAMA

ENERCON Services Project #NUSTART006
Terra-Solve Project #06575

Prepared For:



12100 Ford Road, Suite 200
Dallas, TX 75234
(972) 484-3854
(972) 484-8835 Fax

Prepared By: 
Perry Evans, Consulting Hydrogeologist, Terra-Solve, Inc.

Approved By: 
Randall Lantz, P.G. (AL #1164) Sr. Geologist



PUMPING TEST FIELD DATA

September 18 - 21, 2006

BELLEFONTE NUCLEAR SITE

SCOTTSBORO, JACKSON COUNTY, AL

TERRA-SOLVE PROJECT NO. 06575

TEST TYPE: Variable Discharge
 REFERENCE POINT: TOC
 STATIC DEPTH TO WATER: 19.29 feet
 DEPTH TO PUMP INTAKE: 29.50 feet
 WELL TOTAL DEPTH: 33.30 feet
 WELL DIAMETER: 4 -inch
 ASSOCIATED WITH PUMPING WELL: MW-1217B
 DISTANCE FROM PUMPING WELL: 0.0 feet

OBSERVATION WELL: MW-1217B

| Date | Time (min) | Depth to Water (feet) | Drawdown (feet) | Pumping Rate (gpm) |
|-----------------|------------|-----------------------|-----------------|--------------------|
| 9/18/06 1:00 PM | 0 | 19.29 | | |
| 9/18/06 1:01 PM | 1 | 23.04 | 3.75 | 1.23 |
| 9/18/06 1:02 PM | 2 | 22.18 | 2.89 | 1.23 |
| 9/18/06 1:03 PM | 3 | 22.38 | 3.09 | 1.23 |
| 9/18/06 1:04 PM | 4 | 24.65 | 5.36 | 4.81 |
| 9/18/06 1:05 PM | 5 | 24.56 | 5.27 | 7.37 |
| 9/18/06 1:06 PM | 6 | 24.91 | 5.62 | 4.71 |
| 9/18/06 1:07 PM | 7 | 25.06 | 5.77 | 4.40 |
| 9/18/06 1:08 PM | 8 | 25.11 | 5.82 | 4.09 |
| 9/18/06 1:09 PM | 9 | 25.08 | 5.79 | 4.09 |
| 9/18/06 1:10 PM | 10 | 25.08 | 5.79 | 4.09 |
| 9/18/06 1:11 PM | 11 | 25.11 | 5.82 | 3.99 |
| 9/18/06 1:12 PM | 12 | 25.09 | 5.80 | 3.89 |
| 9/18/06 1:13 PM | 13 | 25.08 | 5.79 | 4.40 |
| 9/18/06 1:14 PM | 14 | 25.09 | 5.80 | 4.09 |
| 9/18/06 1:15 PM | 15 | 25.09 | 5.80 | 4.20 |
| 9/18/06 1:20 PM | 20 | 25.42 | 6.13 | 3.79 |
| 9/18/06 1:25 PM | 25 | 25.48 | 6.19 | 3.81 |
| 9/18/06 1:30 PM | 30 | 25.50 | 6.21 | 3.34 |
| 9/18/06 1:35 PM | 35 | 25.52 | 6.23 | 3.40 |
| 9/18/06 1:40 PM | 40 | 25.58 | 6.29 | 3.48 |
| 9/18/06 1:45 PM | 45 | 26.62 | 7.33 | 2.84 |
| 9/18/06 1:50 PM | 50 | 24.52 | 5.23 | 2.83 |
| 9/18/06 1:55 PM | 55 | 25.72 | 6.43 | 3.91 |
| 9/18/06 2:00 PM | 60 | 25.58 | 6.29 | 2.85 |
| 9/18/06 2:30 PM | 90 | 23.85 | 4.56 | 2.91 |
| 9/18/06 3:00 PM | 120 | 24.15 | 4.86 | 2.92 |
| 9/18/06 3:30 PM | 150 | 24.33 | 5.04 | 2.92 |
| 9/18/06 4:00 PM | 180 | 24.50 | 5.21 | 2.92 |
| 9/18/06 4:30 PM | 210 | 24.75 | 5.46 | 2.92 |
| 9/18/06 5:00 PM | 240 | 27.68 | 8.39 | 2.92 |
| 9/18/06 5:30 PM | 270 | 27.68 | 8.39 | 2.91 |
| 9/18/06 6:00 PM | 300 | 27.68 | 8.39 | 2.80 |
| 9/18/06 7:00 PM | 360 | 24.14 | 4.85 | 2.46 |
| 9/18/06 8:00 PM | 420 | 25.04 | 5.75 | 2.70 |
| 9/18/06 9:00 PM | 480 | 25.60 | 6.31 | 2.68 |

September 18 - 21, 2006
 BELLEFONTE NUCLEAR SITE
 SCOTTSBORO, JACKSON COUNTY, AL
 TERRA-SOLVE PROJECT NO. 06575

TEST TYPE: Variable Discharge
 REFERENCE POINT: TOC
 STATIC DEPTH TO WATER: 19.29 feet
 DEPTH TO PUMP INTAKE: 29.50 feet
 WELL TOTAL DEPTH: 33.30 feet
 WELL DIAMETER: 4 -inch
 ASSOCIATED WITH PUMPING WELL: MW-1217B
 DISTANCE FROM PUMPING WELL: 0.0 feet

OBSERVATION WELL: MW-1217B

| | | | | |
|------------------|------|-------|-------|------|
| 9/18/06 10:00 PM | 540 | 27.68 | 8.39 | 2.67 |
| 9/18/06 11:00 PM | 600 | 27.68 | 8.39 | 2.41 |
| 9/19/06 12:00 AM | 660 | 27.68 | 8.39 | 2.30 |
| 9/19/06 1:00 AM | 720 | 27.68 | 8.39 | 2.25 |
| 9/19/06 2:00 AM | 780 | 27.68 | 8.39 | 2.45 |
| 9/19/06 3:00 AM | 840 | 27.68 | 8.39 | 1.98 |
| 9/19/06 4:00 AM | 900 | 27.68 | 8.39 | 2.13 |
| 9/19/06 5:00 AM | 960 | 27.68 | 8.39 | 1.80 |
| 9/19/06 6:00 AM | 1020 | 27.68 | 8.39 | 1.97 |
| 9/19/06 7:00 AM | 1080 | 27.68 | 8.39 | 2.06 |
| 9/19/06 8:00 AM | 1140 | 27.68 | 8.39 | 2.05 |
| 9/19/06 9:00 AM | 1200 | 27.68 | 8.39 | 1.93 |
| 9/19/06 10:00 AM | 1260 | 27.68 | 8.39 | 2.01 |
| 9/19/06 11:00 AM | 1320 | 27.68 | 8.39 | 2.12 |
| 9/19/06 12:00 PM | 1380 | 27.68 | 8.39 | 2.20 |
| 9/19/06 1:00 PM | 1440 | 27.68 | 8.39 | 2.04 |
| 9/19/06 2:00 PM | 1500 | 27.68 | 8.39 | 1.98 |
| 9/19/06 2:01 PM | 1501 | 25.11 | 5.82 | 0 |
| 9/19/06 2:02 PM | 1502 | 22.06 | 2.77 | 0 |
| 9/19/06 2:03 PM | 1503 | 20.18 | 0.89 | 0 |
| 9/19/06 2:04 PM | 1504 | 19.43 | 0.14 | 0 |
| 9/19/06 2:05 PM | 1505 | 18.98 | -0.31 | 0 |
| 9/19/06 2:06 PM | 1506 | 18.80 | -0.49 | 0 |
| 9/19/06 2:07 PM | 1507 | 18.68 | -0.61 | 0 |
| 9/19/06 2:08 PM | 1508 | 18.63 | -0.66 | 0 |
| 9/19/06 2:09 PM | 1509 | 18.58 | -0.71 | 0 |
| 9/19/06 2:10 PM | 1510 | 18.56 | -0.73 | 0 |
| 9/19/06 2:11 PM | 1511 | 18.53 | -0.76 | 0 |
| 9/19/06 2:12 PM | 1512 | 18.52 | -0.77 | 0 |
| 9/19/06 2:13 PM | 1513 | 18.51 | -0.78 | 0 |
| 9/19/06 2:14 PM | 1514 | 18.50 | -0.79 | 0 |
| 9/19/06 2:15 PM | 1515 | 18.49 | -0.80 | 0 |
| 9/19/06 2:20 PM | 1520 | 18.43 | -0.86 | 0 |
| 9/19/06 2:25 PM | 1525 | 18.41 | -0.88 | 0 |
| 9/19/06 2:30 PM | 1530 | 18.38 | -0.91 | 0 |
| 9/19/06 2:35 PM | 1535 | 18.35 | -0.94 | 0 |
| 9/19/06 2:40 PM | 1540 | 18.33 | -0.96 | 0 |
| 9/19/06 2:45 PM | 1545 | 18.31 | -0.98 | 0 |
| 9/19/06 2:50 PM | 1550 | 18.29 | -1.00 | 0 |

September 18 - 21, 2006
 BELLEFONTE NUCLEAR SITE
 SCOTTSBORO, JACKSON COUNTY, AL
 TERRA-SOLVE PROJECT NO. 06575

TEST TYPE: Variable Discharge
 REFERENCE POINT: TOC
 STATIC DEPTH TO WATER: 19.29 feet
 DEPTH TO PUMP INTAKE: 29.50 feet
 WELL TOTAL DEPTH: 33.30 feet
 WELL DIAMETER: 4 -inch
 ASSOCIATED WITH PUMPING WELL: MW-1217B
 DISTANCE FROM PUMPING WELL: 0.0 feet

OBSERVATION WELL: MW-1217B

| | | | | |
|-----------------|------|-------|-------|---|
| 9/19/06 2:55 PM | 1555 | 18.28 | -1.01 | 0 |
| 9/19/06 3:00 PM | 1560 | 18.26 | -1.03 | 0 |
| 9/19/06 3:30 PM | 1590 | 18.17 | -1.12 | 0 |
| 9/19/06 4:00 PM | 1620 | 18.09 | -1.20 | 0 |
| 9/19/06 4:30 PM | 1650 | 18.03 | -1.26 | 0 |
| 9/19/06 5:00 PM | 1680 | 17.99 | -1.30 | 0 |
| 9/20/06 8:12 AM | 2592 | 17.38 | -1.91 | 0 |
| 9/20/06 2:51 PM | 2991 | 17.21 | -2.08 | 0 |
| 9/21/06 8:21 AM | 4041 | 17.13 | -2.16 | 0 |

Pump off after 1500 minutes.

PUMPING TEST FIELD DATA

September 18 - 21, 2006
BELLEFONTE NUCLEAR SITE
SCOTTSBORO, JACKSON COUNTY, AL
TERRA-SOLVE PROJECT NO. 06575

TEST TYPE: Variable Discharge
REFERENCE POINT: TOC
STATIC DEPTH TO WATER: 46.61 feet
WELL TOTAL DEPTH: 52.80 feet
WELL DIAMETER: 4 -inch
ASSOCIATED WITH PUMPING WELL: MW-1217B
DISTANCE FROM PUMPING WELL: 3.45 feet

OBSERVATION WELL: MW-1217C

| Date | Time (min) | Depth to Water (feet) | Drawdown (feet) |
|-----------------|------------|-----------------------|-----------------|
| 9/18/06 1:00 PM | 0 | 46.61 | |
| 9/18/06 1:02 PM | 2 | 46.61 | 0.00 |
| 9/18/06 1:04 PM | 4 | 46.62 | 0.01 |
| 9/18/06 1:06 PM | 6 | 46.62 | 0.01 |
| 9/18/06 1:08 PM | 8 | 46.62 | 0.01 |
| 9/18/06 1:10 PM | 10 | 46.62 | 0.01 |
| 9/18/06 1:12 PM | 12 | 46.62 | 0.01 |
| 9/18/06 1:14 PM | 14 | 46.62 | 0.01 |
| 9/18/06 1:16 PM | 16 | 46.62 | 0.01 |
| 9/18/06 1:18 PM | 18 | 46.62 | 0.01 |
| 9/18/06 1:20 PM | 20 | 46.62 | 0.01 |
| 9/18/06 1:22 PM | 22 | 46.62 | 0.01 |
| 9/18/06 1:24 PM | 24 | 46.62 | 0.01 |
| 9/18/06 1:26 PM | 26 | 46.62 | 0.01 |
| 9/18/06 1:28 PM | 28 | 46.62 | 0.01 |
| 9/18/06 1:30 PM | 30 | 46.62 | 0.01 |
| 9/18/06 1:32 PM | 32 | 46.62 | 0.01 |
| 9/18/06 1:34 PM | 34 | 46.62 | 0.01 |
| 9/18/06 1:36 PM | 36 | 46.62 | 0.01 |
| 9/18/06 1:38 PM | 38 | 46.62 | 0.01 |
| 9/18/06 1:40 PM | 40 | 46.62 | 0.01 |
| 9/18/06 1:42 PM | 42 | 46.62 | 0.01 |
| 9/18/06 1:44 PM | 44 | 46.62 | 0.01 |
| 9/18/06 1:46 PM | 46 | 46.62 | 0.01 |
| 9/18/06 1:48 PM | 48 | 46.62 | 0.01 |
| 9/18/06 1:50 PM | 50 | 46.62 | 0.01 |
| 9/18/06 1:52 PM | 52 | 46.62 | 0.01 |
| 9/18/06 1:54 PM | 54 | 46.62 | 0.01 |
| 9/18/06 1:56 PM | 56 | 46.62 | 0.01 |
| 9/18/06 1:58 PM | 58 | 46.62 | 0.01 |
| 9/18/06 2:00 PM | 60 | 46.62 | 0.01 |
| 9/18/06 2:05 PM | 65 | 46.62 | 0.01 |
| 9/18/06 2:30 PM | 90 | 46.63 | 0.02 |
| 9/18/06 3:00 PM | 120 | 46.63 | 0.02 |
| 9/18/06 3:30 PM | 150 | 46.63 | 0.02 |
| 9/18/06 4:00 PM | 180 | 46.63 | 0.02 |
| 9/18/06 4:30 PM | 210 | 46.63 | 0.02 |
| 9/18/06 5:00 PM | 240 | 46.63 | 0.02 |
| 9/18/06 5:30 PM | 270 | 46.63 | 0.02 |
| 9/18/06 6:00 PM | 300 | 46.63 | 0.02 |

September 18 - 21, 2006
 BELLEFONTE NUCLEAR SITE
 SCOTTSBORO, JACKSON COUNTY, AL
 TERRA-SOLVE PROJECT NO. 06575

TEST TYPE: Variable Discharge
 REFERENCE POINT: TOC
 STATIC DEPTH TO WATER: 46.61 feet
 WELL TOTAL DEPTH: 52.80 feet
 WELL DIAMETER: 4 -inch
 ASSOCIATED WITH PUMPING WELL: MW-1217B
 DISTANCE FROM PUMPING WELL: 3.45 feet

OBSERVATION WELL: MW-1217C

| | | | |
|------------------|------|-------|-------|
| 9/18/06 6:30 PM | 330 | 46.63 | 0.02 |
| 9/18/06 7:00 PM | 360 | 46.63 | 0.02 |
| 9/18/06 8:00 PM | 420 | 46.63 | 0.02 |
| 9/18/06 9:00 PM | 480 | 46.63 | 0.02 |
| 9/18/06 10:00 PM | 540 | 46.63 | 0.02 |
| 9/18/06 11:00 PM | 600 | 46.62 | 0.01 |
| 9/19/06 12:00 AM | 660 | 46.63 | 0.02 |
| 9/19/06 1:00 AM | 720 | 46.62 | 0.01 |
| 9/19/06 2:00 AM | 780 | 46.62 | 0.01 |
| 9/19/06 3:00 AM | 840 | 46.62 | 0.01 |
| 9/19/06 4:00 AM | 900 | 46.61 | 0.00 |
| 9/19/06 5:00 AM | 960 | 46.59 | -0.02 |
| 9/19/06 6:00 AM | 1020 | 46.62 | 0.01 |
| 9/19/06 7:00 AM | 1080 | 46.62 | 0.01 |
| 9/19/06 8:00 AM | 1140 | 46.62 | 0.01 |
| 9/19/06 9:00 AM | 1200 | 46.62 | 0.01 |
| 9/19/06 10:00 AM | 1260 | 46.62 | 0.01 |
| 9/19/06 11:00 AM | 1320 | 46.62 | 0.01 |
| 9/19/06 12:00 PM | 1380 | 46.62 | 0.01 |
| 9/19/06 1:00 PM | 1440 | 46.62 | 0.01 |
| 9/19/06 2:00 PM | 1500 | 46.62 | 0.01 |
| 9/19/06 2:02 PM | 1502 | 46.62 | 0.01 |
| 9/19/06 2:04 PM | 1504 | 46.62 | 0.01 |
| 9/19/06 2:06 PM | 1506 | 46.62 | 0.01 |
| 9/19/06 2:08 PM | 1508 | 46.62 | 0.01 |
| 9/19/06 2:10 PM | 1510 | 46.62 | 0.01 |
| 9/19/06 2:12 PM | 1512 | 46.62 | 0.01 |
| 9/19/06 2:14 PM | 1514 | 46.62 | 0.01 |
| 9/19/06 2:16 PM | 1516 | 46.62 | 0.01 |
| 9/19/06 2:18 PM | 1518 | 46.62 | 0.01 |
| 9/19/06 2:20 PM | 1520 | 46.62 | 0.01 |
| 9/19/06 2:22 PM | 1522 | 46.62 | 0.01 |
| 9/19/06 2:24 PM | 1524 | 46.61 | 0.00 |
| 9/19/06 2:26 PM | 1526 | 46.61 | 0.00 |
| 9/19/06 2:28 PM | 1528 | 46.61 | 0.00 |
| 9/19/06 2:30 PM | 1530 | 46.61 | 0.00 |
| 9/19/06 2:32 PM | 1532 | 46.61 | 0.00 |
| 9/19/06 2:34 PM | 1534 | 46.61 | 0.00 |
| 9/19/06 2:36 PM | 1536 | 46.61 | 0.00 |
| 9/19/06 2:38 PM | 1538 | 46.61 | 0.00 |
| 9/19/06 2:40 PM | 1540 | 46.61 | 0.00 |
| 9/19/06 2:42 PM | 1542 | 46.61 | 0.00 |
| 9/19/06 2:44 PM | 1544 | 46.61 | 0.00 |

September 18 - 21, 2006
 BELLEFONTE NUCLEAR SITE
 SCOTTSBORO, JACKSON COUNTY, AL
 TERRA-SOLVE PROJECT NO. 06575

TEST TYPE: Variable Discharge
 REFERENCE POINT: TOC
 STATIC DEPTH TO WATER: 46.61 feet
 WELL TOTAL DEPTH: 52.80 feet
 WELL DIAMETER: 4 -inch
 ASSOCIATED WITH PUMPING WELL: MW-1217B
 DISTANCE FROM PUMPING WELL: 3.45 feet

OBSERVATION WELL: MW-1217C

| | | | |
|-----------------|------|-------|------|
| 9/19/06 2:46 PM | 1546 | 46.61 | 0.00 |
| 9/19/06 2:48 PM | 1548 | 46.61 | 0.00 |
| 9/19/06 2:50 PM | 1550 | 46.61 | 0.00 |
| 9/19/06 2:52 PM | 1552 | 46.61 | 0.00 |
| 9/19/06 2:54 PM | 1554 | 46.61 | 0.00 |
| 9/19/06 2:56 PM | 1556 | 46.61 | 0.00 |
| 9/19/06 2:58 PM | 1558 | 46.61 | 0.00 |
| 9/19/06 3:00 PM | 1560 | 46.61 | 0.00 |
| 9/19/06 3:05 PM | 1565 | 46.61 | 0.00 |
| 9/19/06 3:10 PM | 1570 | 46.61 | 0.00 |
| 9/19/06 3:15 PM | 1575 | 46.61 | 0.00 |
| 9/19/06 3:20 PM | 1580 | 46.61 | 0.00 |
| 9/19/06 3:25 PM | 1585 | 46.61 | 0.00 |
| 9/19/06 3:30 PM | 1590 | 46.61 | 0.00 |
| 9/19/06 3:35 PM | 1595 | 46.61 | 0.00 |
| 9/19/06 3:40 PM | 1600 | 46.61 | 0.00 |
| 9/19/06 3:45 PM | 1605 | 46.61 | 0.00 |
| 9/19/06 3:50 PM | 1610 | 46.61 | 0.00 |
| 9/19/06 3:55 PM | 1615 | 46.61 | 0.00 |
| 9/19/06 4:00 PM | 1620 | 46.61 | 0.00 |
| 9/19/06 4:10 PM | 1630 | 46.61 | 0.00 |
| 9/19/06 4:20 PM | 1640 | 46.61 | 0.00 |
| 9/19/06 4:30 PM | 1650 | 46.61 | 0.00 |
| 9/19/06 4:40 PM | 1660 | 46.61 | 0.00 |
| 9/19/06 4:50 PM | 1670 | 46.61 | 0.00 |
| 9/19/06 5:00 PM | 1680 | 46.61 | 0.00 |
| 9/20/06 8:11 AM | 2591 | 46.61 | 0.00 |
| 9/20/06 2:50 PM | 2990 | 46.61 | 0.00 |
| 9/21/06 8:19 AM | 4039 | 46.61 | 0.00 |

Pump off after 1500 minutes.

PUMPING TEST FIELD DATA

September 18 - 21, 2006

BELLEFONTE NUCLEAR SITE

SCOTTSBORO, JACKSON COUNTY, AL

TERRA-SOLVE PROJECT NO. 06575

TEST TYPE: Variable Discharge
REFERENCE POINT: TOC
STATIC DEPTH TO WATER: 77.37 feet
WELL TOTAL DEPTH: 77.81 feet
WELL DIAMETER: 2 -inch
ASSOCIATED WITH PUMPING WELL: MW-1217B
DISTANCE FROM PUMPING WELL: 186.10 feet

OBSERVATION WELL: MW-1201B

| Date | Time (min) | Depth to Water (feet) | Drawdown (feet) |
|-----------------|------------|-----------------------|-----------------|
| 9/18/06 1:00 PM | 0 | 77.37 | |
| 9/19/06 8:00 AM | 1140 | 77.31 | -0.06 |
| 9/19/06 1:00 PM | 1440 | 77.31 | -0.06 |
| 9/19/06 2:00 PM | 1500 | 77.31 | -0.06 |
| 9/19/06 3:30 PM | 1590 | 77.31 | -0.06 |
| 9/21/06 8:13 AM | 4033 | 77.33 | -0.04 |

Pump off after 1500 minutes.

PUMPING TEST FIELD DATA

September 18 - 21, 2006
BELLEFONTE NUCLEAR SITE
SCOTTSBORO, JACKSON COUNTY, AL
TERRA-SOLVE PROJECT NO. 06575

TEST TYPE: Variable Discharge
REFERENCE POINT: TOC
STATIC DEPTH TO WATER: 46.55 feet
WELL TOTAL DEPTH: 52.85 feet
WELL DIAMETER: 2 -inch
ASSOCIATED WITH PUMPING WELL: MW-1217B
DISTANCE FROM PUMPING WELL: 46.00 feet

OBSERVATION WELL: OW-7

| Date | Time (min) | Depth to Water (feet) | Drawdown (feet) |
|-----------------|------------|-----------------------|-----------------|
| 9/18/06 1:00 PM | 0 | 46.55 | |
| 9/18/06 1:02 PM | 2 | 46.55 | 0.00 |
| 9/18/06 1:04 PM | 4 | 46.55 | 0.00 |
| 9/18/06 1:06 PM | 6 | 46.55 | 0.00 |
| 9/18/06 1:08 PM | 8 | 46.55 | 0.00 |
| 9/18/06 1:10 PM | 10 | 46.55 | 0.00 |
| 9/18/06 1:12 PM | 12 | 46.55 | 0.00 |
| 9/18/06 1:14 PM | 14 | 46.55 | 0.00 |
| 9/18/06 1:16 PM | 16 | 46.55 | 0.00 |
| 9/18/06 1:18 PM | 18 | 46.55 | 0.00 |
| 9/18/06 1:20 PM | 20 | 46.55 | 0.00 |
| 9/18/06 1:22 PM | 22 | 46.55 | 0.00 |
| 9/18/06 1:24 PM | 24 | 46.55 | 0.00 |
| 9/18/06 1:26 PM | 26 | 46.55 | 0.00 |
| 9/18/06 1:28 PM | 28 | 46.55 | 0.00 |
| 9/18/06 1:30 PM | 30 | 46.55 | 0.00 |
| 9/18/06 1:32 PM | 32 | 46.55 | 0.00 |
| 9/18/06 1:34 PM | 34 | 46.55 | 0.00 |
| 9/18/06 1:36 PM | 36 | 46.55 | 0.00 |
| 9/18/06 1:38 PM | 38 | 46.55 | 0.00 |
| 9/18/06 1:40 PM | 40 | 46.55 | 0.00 |
| 9/18/06 1:42 PM | 42 | 46.55 | 0.00 |
| 9/18/06 1:44 PM | 44 | 46.55 | 0.00 |
| 9/18/06 1:46 PM | 46 | 46.55 | 0.00 |
| 9/18/06 1:48 PM | 48 | 46.55 | 0.00 |
| 9/18/06 1:50 PM | 50 | 46.55 | 0.00 |
| 9/18/06 1:52 PM | 52 | 46.55 | 0.00 |
| 9/18/06 1:54 PM | 54 | 46.55 | 0.00 |
| 9/18/06 1:56 PM | 56 | 46.55 | 0.00 |
| 9/18/06 1:58 PM | 58 | 46.55 | 0.00 |
| 9/18/06 2:00 PM | 60 | 46.55 | 0.00 |
| 9/18/06 2:05 PM | 65 | 46.55 | 0.00 |
| 9/18/06 2:10 PM | 70 | 46.55 | 0.00 |
| 9/18/06 2:15 PM | 75 | 46.55 | 0.00 |
| 9/18/06 2:20 PM | 80 | 46.55 | 0.00 |
| 9/18/06 2:25 PM | 85 | 46.55 | 0.00 |
| 9/18/06 2:30 PM | 90 | 46.55 | 0.00 |
| 9/18/06 3:00 PM | 120 | 46.55 | 0.00 |
| 9/18/06 3:30 PM | 150 | 46.55 | 0.00 |
| 9/18/06 4:00 PM | 180 | 46.55 | 0.00 |

September 18 - 21, 2006
 BELLEFONTE NUCLEAR SITE
 SCOTTSBORO, JACKSON COUNTY, AL
 TERRA-SOLVE PROJECT NO. 06575

TEST TYPE: Variable Discharge
 REFERENCE POINT: TOC
 STATIC DEPTH TO WATER: 46.55 feet
 WELL TOTAL DEPTH: 52.85 feet
 WELL DIAMETER: 2 -inch
 ASSOCIATED WITH PUMPING WELL: MW-1217B
 DISTANCE FROM PUMPING WELL: 46.00 feet

OBSERVATION WELL: OW-7

| | | | |
|------------------|------|-------|------|
| 9/18/06 4:30 PM | 210 | 46.55 | 0.00 |
| 9/18/06 5:00 PM | 240 | 46.55 | 0.00 |
| 9/18/06 5:30 PM | 270 | 46.55 | 0.00 |
| 9/18/06 6:00 PM | 300 | 46.55 | 0.00 |
| 9/18/06 6:30 PM | 330 | 46.55 | 0.00 |
| 9/18/06 7:00 PM | 360 | 46.55 | 0.00 |
| 9/18/06 8:00 PM | 420 | 46.55 | 0.00 |
| 9/18/06 9:00 PM | 480 | 46.55 | 0.00 |
| 9/18/06 10:00 PM | 540 | 46.55 | 0.00 |
| 9/18/06 11:00 PM | 600 | 46.55 | 0.00 |
| 9/19/06 12:00 AM | 660 | 46.55 | 0.00 |
| 9/19/06 1:00 AM | 720 | 46.55 | 0.00 |
| 9/19/06 2:00 AM | 780 | 46.55 | 0.00 |
| 9/19/06 3:00 AM | 840 | 46.55 | 0.00 |
| 9/19/06 4:00 AM | 900 | 46.55 | 0.00 |
| 9/19/06 5:00 AM | 960 | 46.55 | 0.00 |
| 9/19/06 6:00 AM | 1020 | 46.55 | 0.00 |
| 9/19/06 7:00 AM | 1080 | 46.55 | 0.00 |
| 9/19/06 8:00 AM | 1140 | 46.55 | 0.00 |
| 9/19/06 9:00 AM | 1200 | 46.55 | 0.00 |
| 9/19/06 10:00 AM | 1260 | 46.55 | 0.00 |
| 9/19/06 11:00 AM | 1320 | 46.55 | 0.00 |
| 9/19/06 12:00 PM | 1380 | 46.55 | 0.00 |
| 9/19/06 1:00 PM | 1440 | 46.55 | 0.00 |
| 9/19/06 2:00 PM | 1500 | 46.55 | 0.00 |
| 9/19/06 2:02 PM | 1502 | 46.55 | 0.00 |
| 9/19/06 2:04 PM | 1504 | 46.55 | 0.00 |
| 9/19/06 2:06 PM | 1506 | 46.55 | 0.00 |
| 9/19/06 2:08 PM | 1508 | 46.55 | 0.00 |
| 9/19/06 2:10 PM | 1510 | 46.55 | 0.00 |
| 9/19/06 2:12 PM | 1512 | 46.55 | 0.00 |
| 9/19/06 2:14 PM | 1514 | 46.55 | 0.00 |
| 9/19/06 2:16 PM | 1516 | 46.56 | 0.01 |
| 9/19/06 2:18 PM | 1518 | 46.56 | 0.01 |
| 9/19/06 2:20 PM | 1520 | 46.56 | 0.01 |
| 9/19/06 2:22 PM | 1522 | 46.56 | 0.01 |
| 9/19/06 2:24 PM | 1524 | 46.56 | 0.01 |
| 9/19/06 2:26 PM | 1526 | 46.56 | 0.01 |
| 9/19/06 2:28 PM | 1528 | 46.57 | 0.02 |
| 9/19/06 2:30 PM | 1530 | 46.57 | 0.02 |
| 9/19/06 2:32 PM | 1532 | 46.57 | 0.02 |
| 9/19/06 2:34 PM | 1534 | 46.57 | 0.02 |
| 9/19/06 2:36 PM | 1536 | 46.57 | 0.02 |

September 18 - 21, 2006
 BELLEFONTE NUCLEAR SITE
 SCOTTSBORO, JACKSON COUNTY, AL
 TERRA-SOLVE PROJECT NO. 06575

TEST TYPE: Variable Discharge
 REFERENCE POINT: TOC
 STATIC DEPTH TO WATER: 46.55 feet
 WELL TOTAL DEPTH: 52.85 feet
 WELL DIAMETER: 2 -inch
 ASSOCIATED WITH PUMPING WELL: MW-1217B
 DISTANCE FROM PUMPING WELL: 46.00 feet

OBSERVATION WELL: OW-7

| | | | |
|-----------------|------|-------|-------|
| 9/19/06 2:38 PM | 1538 | 46.57 | 0.02 |
| 9/19/06 2:40 PM | 1540 | 46.57 | 0.02 |
| 9/19/06 2:42 PM | 1542 | 46.57 | 0.02 |
| 9/19/06 2:44 PM | 1544 | 46.57 | 0.02 |
| 9/19/06 2:46 PM | 1546 | 46.57 | 0.02 |
| 9/19/06 2:48 PM | 1548 | 46.57 | 0.02 |
| 9/19/06 2:50 PM | 1550 | 46.57 | 0.02 |
| 9/19/06 2:52 PM | 1552 | 46.57 | 0.02 |
| 9/19/06 2:54 PM | 1554 | 46.57 | 0.02 |
| 9/19/06 2:56 PM | 1556 | 46.57 | 0.02 |
| 9/19/06 2:58 PM | 1558 | 46.57 | 0.02 |
| 9/19/06 3:00 PM | 1560 | 46.57 | 0.02 |
| 9/19/06 3:05 PM | 1565 | 46.57 | 0.02 |
| 9/19/06 3:10 PM | 1570 | 46.57 | 0.02 |
| 9/19/06 3:15 PM | 1575 | 46.57 | 0.02 |
| 9/19/06 3:20 PM | 1580 | 46.57 | 0.02 |
| 9/19/06 3:25 PM | 1585 | 46.57 | 0.02 |
| 9/19/06 3:30 PM | 1590 | 46.57 | 0.02 |
| 9/19/06 3:35 PM | 1595 | 46.57 | 0.02 |
| 9/19/06 3:40 PM | 1600 | 46.57 | 0.02 |
| 9/19/06 3:45 PM | 1605 | 46.57 | 0.02 |
| 9/19/06 3:50 PM | 1610 | 46.57 | 0.02 |
| 9/19/06 3:55 PM | 1615 | 46.57 | 0.02 |
| 9/19/06 4:00 PM | 1620 | 46.57 | 0.02 |
| 9/19/06 4:10 PM | 1630 | 46.57 | 0.02 |
| 9/19/06 4:20 PM | 1640 | 46.57 | 0.02 |
| 9/19/06 4:30 PM | 1650 | 46.57 | 0.02 |
| 9/19/06 4:40 PM | 1660 | 46.57 | 0.02 |
| 9/19/06 4:50 PM | 1670 | 46.57 | 0.02 |
| 9/19/06 5:00 PM | 1680 | 46.57 | 0.02 |
| 9/20/06 8:10 AM | 2590 | 46.57 | 0.02 |
| 9/20/06 2:43 PM | 2983 | 46.54 | -0.01 |
| 9/21/06 8:12 AM | 4032 | 46.54 | -0.01 |

Pump off after 1500 minutes.

PUMPING TEST FIELD DATA

September 18 - 21, 2006
BELLEFONTE NUCLEAR SITE
SCOTTSBORO, JACKSON COUNTY, AL
TERRA-SOLVE PROJECT NO. 06575

TEST TYPE: Variable Discharge
REFERENCE POINT: TOC
STATIC DEPTH TO WATER: 19.77 feet
WELL TOTAL DEPTH: 54.20 feet
WELL DIAMETER: 2 -inch
ASSOCIATED WITH PUMPING WELL: MW-1217B
DISTANCE FROM PUMPING WELL: 58.20 feet

OBSERVATION WELL: OW-8

| Date | Time (min) | Depth to Water (feet) | Drawdown (feet) |
|-----------------|------------|-----------------------|-----------------|
| 9/18/06 1:00 PM | 0 | 19.77 | |
| 9/18/06 1:02 PM | 2 | 19.77 | 0.00 |
| 9/18/06 1:04 PM | 4 | 19.77 | 0.00 |
| 9/18/06 1:06 PM | 6 | 19.77 | 0.00 |
| 9/18/06 1:08 PM | 8 | 19.77 | 0.00 |
| 9/18/06 1:10 PM | 10 | 19.78 | 0.01 |
| 9/18/06 1:12 PM | 12 | 19.79 | 0.02 |
| 9/18/06 1:14 PM | 14 | 19.80 | 0.03 |
| 9/18/06 1:16 PM | 16 | 19.81 | 0.04 |
| 9/18/06 1:18 PM | 18 | 19.82 | 0.05 |
| 9/18/06 1:20 PM | 20 | 19.82 | 0.05 |
| 9/18/06 1:22 PM | 22 | 19.83 | 0.06 |
| 9/18/06 1:24 PM | 24 | 19.83 | 0.06 |
| 9/18/06 1:26 PM | 26 | 19.84 | 0.07 |
| 9/18/06 1:28 PM | 28 | 19.84 | 0.07 |
| 9/18/06 1:30 PM | 30 | 19.87 | 0.10 |
| 9/18/06 1:32 PM | 32 | 19.87 | 0.10 |
| 9/18/06 1:34 PM | 34 | 19.89 | 0.12 |
| 9/18/06 1:36 PM | 36 | 19.89 | 0.12 |
| 9/18/06 1:38 PM | 38 | 19.90 | 0.13 |
| 9/18/06 1:40 PM | 40 | 19.90 | 0.13 |
| 9/18/06 1:42 PM | 42 | 19.91 | 0.14 |
| 9/18/06 1:44 PM | 44 | 19.92 | 0.15 |
| 9/18/06 1:46 PM | 46 | 19.93 | 0.16 |
| 9/18/06 1:48 PM | 48 | 19.94 | 0.17 |
| 9/18/06 1:50 PM | 50 | 19.95 | 0.18 |
| 9/18/06 1:52 PM | 52 | 19.95 | 0.18 |
| 9/18/06 1:54 PM | 54 | 19.96 | 0.19 |
| 9/18/06 1:56 PM | 56 | 19.97 | 0.20 |
| 9/18/06 1:58 PM | 58 | 19.98 | 0.21 |
| 9/18/06 2:00 PM | 60 | 19.99 | 0.22 |
| 9/18/06 2:05 PM | 65 | 20.03 | 0.26 |
| 9/18/06 2:10 PM | 70 | 20.05 | 0.28 |
| 9/18/06 2:15 PM | 75 | 20.05 | 0.28 |
| 9/18/06 2:20 PM | 80 | 20.07 | 0.30 |
| 9/18/06 2:25 PM | 85 | 20.08 | 0.31 |
| 9/18/06 2:30 PM | 90 | 20.10 | 0.33 |
| 9/18/06 3:00 PM | 120 | 20.20 | 0.43 |
| 9/18/06 3:30 PM | 150 | 20.28 | 0.51 |
| 9/18/06 4:00 PM | 180 | 20.33 | 0.56 |

September 18 - 21, 2006
 BELLEFONTE NUCLEAR SITE
 SCOTTSBORO, JACKSON COUNTY, AL
 TERRA-SOLVE PROJECT NO. 06575

TEST TYPE: Variable Discharge
 REFERENCE POINT: TOC
 STATIC DEPTH TO WATER: 19.77 feet
 WELL TOTAL DEPTH: 54.20 feet
 WELL DIAMETER: 2 -inch
 ASSOCIATED WITH PUMPING WELL: MW-1217B
 DISTANCE FROM PUMPING WELL: 58.20 feet

OBSERVATION WELL: OW-8

| | | | |
|------------------|------|-------|-------|
| 9/18/06 4:30 PM | 210 | 20.37 | 0.60 |
| 9/18/06 5:00 PM | 240 | 20.41 | 0.64 |
| 9/18/06 5:30 PM | 270 | 20.43 | 0.66 |
| 9/18/06 6:00 PM | 300 | 20.45 | 0.68 |
| 9/18/06 6:30 PM | 330 | 20.45 | 0.68 |
| 9/18/06 7:00 PM | 360 | 20.43 | 0.66 |
| 9/18/06 8:00 PM | 420 | 20.41 | 0.64 |
| 9/18/06 9:00 PM | 480 | 20.39 | 0.62 |
| 9/18/06 10:00 PM | 540 | 20.36 | 0.59 |
| 9/18/06 11:00 PM | 600 | 20.32 | 0.55 |
| 9/19/06 12:00 AM | 660 | 20.25 | 0.48 |
| 9/19/06 1:00 AM | 720 | 20.20 | 0.43 |
| 9/19/06 2:00 AM | 780 | 20.13 | 0.36 |
| 9/19/06 3:00 AM | 840 | 20.03 | 0.26 |
| 9/19/06 4:00 AM | 900 | 19.98 | 0.21 |
| 9/19/06 5:00 AM | 960 | 19.90 | 0.13 |
| 9/19/06 6:00 AM | 1020 | 19.78 | 0.01 |
| 9/19/06 7:00 AM | 1080 | 19.68 | -0.09 |
| 9/19/06 8:00 AM | 1140 | 19.60 | -0.17 |
| 9/19/06 9:00 AM | 1200 | 19.50 | -0.27 |
| 9/19/06 10:00 AM | 1260 | 19.45 | -0.32 |
| 9/19/06 11:00 AM | 1320 | 19.37 | -0.40 |
| 9/19/06 12:00 PM | 1380 | 19.32 | -0.45 |
| 9/19/06 1:00 PM | 1440 | 19.25 | -0.52 |
| 9/19/06 2:00 PM | 1500 | 19.19 | -0.58 |
| 9/19/06 2:02 PM | 1502 | 19.19 | -0.58 |
| 9/19/06 2:04 PM | 1504 | 19.19 | -0.58 |
| 9/19/06 2:06 PM | 1506 | 19.19 | -0.58 |
| 9/19/06 2:08 PM | 1508 | 19.19 | -0.58 |
| 9/19/06 2:10 PM | 1510 | 19.19 | -0.58 |
| 9/19/06 2:12 PM | 1512 | 19.19 | -0.58 |
| 9/19/06 2:14 PM | 1514 | 19.19 | -0.58 |
| 9/19/06 2:16 PM | 1516 | 19.16 | -0.61 |
| 9/19/06 2:18 PM | 1518 | 19.16 | -0.61 |
| 9/19/06 2:20 PM | 1520 | 19.15 | -0.62 |
| 9/19/06 2:22 PM | 1522 | 19.14 | -0.63 |
| 9/19/06 2:24 PM | 1524 | 19.13 | -0.64 |
| 9/19/06 2:26 PM | 1526 | 19.13 | -0.64 |
| 9/19/06 2:28 PM | 1528 | 19.12 | -0.65 |
| 9/19/06 2:30 PM | 1530 | 19.12 | -0.65 |
| 9/19/06 2:32 PM | 1532 | 19.11 | -0.66 |
| 9/19/06 2:34 PM | 1534 | 19.10 | -0.67 |
| 9/19/06 2:36 PM | 1536 | 19.09 | -0.68 |

September 18 - 21, 2006
 BELLEFONTE NUCLEAR SITE
 SCOTTSBORO, JACKSON COUNTY, AL
 TERRA-SOLVE PROJECT NO. 06575

TEST TYPE: Variable Discharge
 REFERENCE POINT: TOC
 STATIC DEPTH TO WATER: 19.77 feet
 WELL TOTAL DEPTH: 54.20 feet
 WELL DIAMETER: 2 -inch
 ASSOCIATED WITH PUMPING WELL: MW-1217B
 DISTANCE FROM PUMPING WELL: 58.20 feet

OBSERVATION WELL: OW-8

| | | | |
|-----------------|------|-------|-------|
| 9/19/06 2:38 PM | 1538 | 19.08 | -0.69 |
| 9/19/06 2:40 PM | 1540 | 19.08 | -0.69 |
| 9/19/06 2:42 PM | 1542 | 19.07 | -0.70 |
| 9/19/06 2:44 PM | 1544 | 19.06 | -0.71 |
| 9/19/06 2:46 PM | 1546 | 19.06 | -0.71 |
| 9/19/06 2:48 PM | 1548 | 19.05 | -0.72 |
| 9/19/06 2:50 PM | 1550 | 19.05 | -0.72 |
| 9/19/06 2:52 PM | 1552 | 19.04 | -0.73 |
| 9/19/06 2:54 PM | 1554 | 19.03 | -0.74 |
| 9/19/06 2:56 PM | 1556 | 19.02 | -0.75 |
| 9/19/06 2:58 PM | 1558 | 19.01 | -0.76 |
| 9/19/06 3:00 PM | 1560 | 19.00 | -0.77 |
| 9/19/06 3:05 PM | 1565 | 19.00 | -0.77 |
| 9/19/06 3:10 PM | 1570 | 18.98 | -0.79 |
| 9/19/06 3:15 PM | 1575 | 18.95 | -0.82 |
| 9/19/06 3:20 PM | 1580 | 18.94 | -0.83 |
| 9/19/06 3:25 PM | 1585 | 18.93 | -0.84 |
| 9/19/06 3:30 PM | 1590 | 18.91 | -0.86 |
| 9/19/06 3:35 PM | 1595 | 18.89 | -0.88 |
| 9/19/06 3:40 PM | 1600 | 18.87 | -0.90 |
| 9/19/06 3:45 PM | 1605 | 18.86 | -0.91 |
| 9/19/06 3:50 PM | 1610 | 18.86 | -0.91 |
| 9/19/06 3:55 PM | 1615 | 18.83 | -0.94 |
| 9/19/06 4:00 PM | 1620 | 18.81 | -0.96 |
| 9/19/06 4:10 PM | 1630 | 18.78 | -0.99 |
| 9/19/06 4:20 PM | 1640 | 18.74 | -1.03 |
| 9/19/06 4:30 PM | 1650 | 18.73 | -1.04 |
| 9/19/06 4:40 PM | 1660 | 18.70 | -1.07 |
| 9/19/06 4:50 PM | 1670 | 18.67 | -1.10 |
| 9/19/06 5:00 PM | 1680 | 18.64 | -1.13 |
| 9/20/06 8:10 AM | 2590 | 17.86 | -1.91 |
| 9/20/06 2:54 PM | 2994 | 17.68 | -2.09 |
| 9/21/06 8:23 AM | 4043 | 17.59 | -2.18 |

Pump off after 1500 minutes.

PUMPING TEST FIELD DATA

September 18 - 21, 2006

BELLEFONTE NUCLEAR SITE

SCOTTSBORO, JACKSON COUNTY, AL

TERRA-SOLVE PROJECT NO. 06575

TEST TYPE: Variable Discharge
 REFERENCE POINT: TOC
 STATIC DEPTH TO WATER: 32.57 feet
 WELL TOTAL DEPTH: 52.70 feet
 WELL DIAMETER: 2 -inch
 ASSOCIATED WITH PUMPING WELL: MW-1217B
 DISTANCE FROM PUMPING WELL: 69.30 feet

| | |
|--------------------------|-------------|
| OBSERVATION WELL: | OW-9 |
|--------------------------|-------------|

| Date | Time (min) | Depth to Water (feet) | Drawdown (feet) |
|------------------|------------|-----------------------|-----------------|
| 9/18/06 1:00 PM | 0 | 32.57 | |
| 9/18/06 1:18 PM | 18 | 32.56 | -0.01 |
| 9/18/06 1:25 PM | 25 | 32.56 | -0.01 |
| 9/18/06 1:36 PM | 36 | 32.56 | -0.01 |
| 9/18/06 1:40 PM | 40 | 32.56 | -0.01 |
| 9/18/06 1:46 PM | 46 | 32.56 | -0.01 |
| 9/18/06 2:00 PM | 60 | 32.56 | -0.01 |
| 9/18/06 2:10 PM | 70 | 32.56 | -0.01 |
| 9/18/06 2:15 PM | 75 | 32.56 | -0.01 |
| 9/18/06 2:25 PM | 85 | 32.56 | -0.01 |
| 9/18/06 2:30 PM | 90 | 32.56 | -0.01 |
| 9/18/06 3:00 PM | 120 | 32.56 | -0.01 |
| 9/18/06 3:30 PM | 150 | 32.54 | -0.03 |
| 9/18/06 4:00 PM | 180 | 32.54 | -0.03 |
| 9/18/06 4:30 PM | 210 | 32.54 | -0.03 |
| 9/18/06 5:00 PM | 240 | 32.54 | -0.03 |
| 9/18/06 5:30 PM | 270 | 32.52 | -0.05 |
| 9/18/06 6:00 PM | 300 | 32.52 | -0.05 |
| 9/18/06 6:30 PM | 330 | 32.51 | -0.06 |
| 9/18/06 7:00 PM | 360 | 32.50 | -0.07 |
| 9/18/06 8:00 PM | 420 | 32.50 | -0.07 |
| 9/18/06 9:00 PM | 480 | 32.49 | -0.08 |
| 9/18/06 10:00 PM | 540 | 32.48 | -0.09 |
| 9/18/06 11:00 PM | 600 | 32.47 | -0.10 |
| 9/19/06 12:00 AM | 660 | 32.45 | -0.12 |
| 9/19/06 1:00 AM | 720 | 32.45 | -0.12 |
| 9/19/06 2:00 AM | 780 | 32.45 | -0.12 |
| 9/19/06 3:00 AM | 840 | 32.43 | -0.14 |
| 9/19/06 4:00 AM | 900 | 32.40 | -0.17 |
| 9/19/06 5:00 AM | 960 | 32.40 | -0.17 |
| 9/19/06 6:00 AM | 1020 | 32.40 | -0.17 |
| 9/19/06 7:00 AM | 1080 | 32.41 | -0.16 |
| 9/19/06 8:00 AM | 1140 | 32.40 | -0.17 |
| 9/19/06 9:00 AM | 1200 | 32.41 | -0.16 |
| 9/19/06 10:00 AM | 1260 | 32.41 | -0.16 |
| 9/19/06 11:00 AM | 1320 | 32.40 | -0.17 |
| 9/19/06 12:00 PM | 1380 | 32.40 | -0.17 |
| 9/19/06 1:00 PM | 1440 | 32.36 | -0.21 |
| 9/19/06 2:00 PM | 1500 | 32.35 | -0.22 |
| 9/19/06 2:02 PM | 1502 | 32.34 | -0.23 |

September 18 - 21, 2006
 BELLEFONTE NUCLEAR SITE
 SCOTTSBORO, JACKSON COUNTY, AL
 TERRA-SOLVE PROJECT NO. 06575

TEST TYPE: Variable Discharge
 REFERENCE POINT: TOC
 STATIC DEPTH TO WATER: 32.57 feet
 WELL TOTAL DEPTH: 52.70 feet
 WELL DIAMETER: 2 -inch
 ASSOCIATED WITH PUMPING WELL: MW-1217B
 DISTANCE FROM PUMPING WELL: 69.30 feet

| | |
|--------------------------|-------------|
| OBSERVATION WELL: | OW-9 |
|--------------------------|-------------|

| | | | |
|-----------------|------|-------|-------|
| 9/19/06 2:04 PM | 1504 | 32.34 | -0.23 |
| 9/19/06 2:06 PM | 1506 | 32.34 | -0.23 |
| 9/19/06 2:08 PM | 1508 | 32.34 | -0.23 |
| 9/19/06 2:10 PM | 1510 | 32.34 | -0.23 |
| 9/19/06 2:12 PM | 1512 | 32.34 | -0.23 |
| 9/19/06 2:14 PM | 1514 | 32.34 | -0.23 |
| 9/19/06 2:16 PM | 1516 | 32.34 | -0.23 |
| 9/19/06 2:18 PM | 1518 | 32.34 | -0.23 |
| 9/19/06 2:20 PM | 1520 | 32.34 | -0.23 |
| 9/19/06 2:22 PM | 1522 | 32.34 | -0.23 |
| 9/19/06 2:24 PM | 1524 | 32.34 | -0.23 |
| 9/19/06 2:26 PM | 1526 | 32.34 | -0.23 |
| 9/19/06 2:28 PM | 1528 | 32.34 | -0.23 |
| 9/19/06 2:30 PM | 1530 | 32.34 | -0.23 |
| 9/19/06 2:32 PM | 1532 | 32.34 | -0.23 |
| 9/19/06 2:34 PM | 1534 | 32.34 | -0.23 |
| 9/19/06 2:36 PM | 1536 | 32.34 | -0.23 |
| 9/19/06 2:38 PM | 1538 | 32.34 | -0.23 |
| 9/19/06 2:40 PM | 1540 | 32.34 | -0.23 |
| 9/19/06 2:42 PM | 1542 | 32.34 | -0.23 |
| 9/19/06 2:44 PM | 1544 | 32.34 | -0.23 |
| 9/19/06 2:46 PM | 1546 | 32.34 | -0.23 |
| 9/19/06 2:48 PM | 1548 | 32.34 | -0.23 |
| 9/19/06 2:50 PM | 1550 | 32.34 | -0.23 |
| 9/19/06 2:52 PM | 1552 | 32.34 | -0.23 |
| 9/19/06 2:54 PM | 1554 | 32.33 | -0.24 |
| 9/19/06 2:56 PM | 1556 | 32.33 | -0.24 |
| 9/19/06 2:58 PM | 1558 | 32.33 | -0.24 |
| 9/19/06 3:00 PM | 1560 | 32.33 | -0.24 |
| 9/19/06 3:05 PM | 1565 | 32.33 | -0.24 |
| 9/19/06 3:10 PM | 1570 | 32.33 | -0.24 |
| 9/19/06 3:15 PM | 1575 | 32.33 | -0.24 |
| 9/19/06 3:20 PM | 1580 | 32.33 | -0.24 |
| 9/19/06 3:25 PM | 1585 | 32.33 | -0.24 |
| 9/19/06 3:30 PM | 1590 | 32.33 | -0.24 |
| 9/19/06 3:35 PM | 1595 | 32.32 | -0.25 |
| 9/19/06 3:40 PM | 1600 | 32.32 | -0.25 |
| 9/19/06 3:45 PM | 1605 | 32.32 | -0.25 |
| 9/19/06 3:50 PM | 1610 | 32.32 | -0.25 |
| 9/19/06 3:55 PM | 1615 | 32.32 | -0.25 |
| 9/19/06 4:00 PM | 1620 | 32.32 | -0.25 |
| 9/19/06 4:10 PM | 1630 | 32.32 | -0.25 |
| 9/19/06 4:20 PM | 1640 | 32.31 | -0.26 |

September 18 - 21, 2006
BELLEFONTE NUCLEAR SITE
SCOTTSBORO, JACKSON COUNTY, AL
TERRA-SOLVE PROJECT NO. 06575

TEST TYPE: Variable Discharge
REFERENCE POINT: TOC
STATIC DEPTH TO WATER: 32.57 feet
WELL TOTAL DEPTH: 52.70 feet
WELL DIAMETER: 2 -inch
ASSOCIATED WITH PUMPING WELL: MW-1217B
DISTANCE FROM PUMPING WELL: 69.30 feet

| | |
|--------------------------|-------------|
| OBSERVATION WELL: | OW-9 |
|--------------------------|-------------|

| | | | |
|-----------------|------|-------|-------|
| 9/19/06 4:30 PM | 1650 | 32.31 | -0.26 |
| 9/19/06 4:40 PM | 1660 | 32.31 | -0.26 |
| 9/19/06 4:50 PM | 1670 | 32.31 | -0.26 |
| 9/19/06 5:00 PM | 1680 | 32.31 | -0.26 |
| 9/20/06 8:10 AM | 2590 | 32.20 | -0.37 |
| 9/20/06 2:48 PM | 2988 | 32.09 | -0.48 |
| 9/21/06 8:17 AM | 4037 | 31.95 | -0.62 |

Pump off after 1500 minutes.

PUMPING TEST FIELD DATA

September 18 - 21, 2006
BELLEFONTE NUCLEAR SITE
SCOTTSBORO, JACKSON COUNTY, AL
TERRA-SOLVE PROJECT NO. 06575

TEST TYPE: Variable Discharge
REFERENCE POINT: TOC
STATIC DEPTH TO WATER: 19.65 feet
WELL TOTAL DEPTH: 33.45 feet
WELL DIAMETER: 2 -inch
ASSOCIATED WITH PUMPING WELL: MW-1217B
DISTANCE FROM PUMPING WELL: 77.00 feet

OBSERVATION WELL: OW-10

| Date | Time (min) | Depth to Water (feet) | Drawdown (feet) |
|------------------|------------|-----------------------|-----------------|
| 9/18/06 1:00 PM | 0 | 19.65 | |
| 9/18/06 1:15 PM | 15 | 19.66 | 0.01 |
| 9/18/06 1:26 PM | 26 | 19.66 | 0.01 |
| 9/18/06 1:34 PM | 34 | 19.66 | 0.01 |
| 9/18/06 1:40 PM | 40 | 19.66 | 0.01 |
| 9/18/06 1:46 PM | 46 | 19.66 | 0.01 |
| 9/18/06 2:00 PM | 60 | 19.66 | 0.01 |
| 9/18/06 2:10 PM | 70 | 19.66 | 0.01 |
| 9/18/06 2:15 PM | 75 | 19.66 | 0.01 |
| 9/18/06 2:20 PM | 80 | 19.66 | 0.01 |
| 9/18/06 2:25 PM | 85 | 19.61 | -0.04 |
| 9/18/06 2:30 PM | 90 | 19.62 | -0.03 |
| 9/18/06 3:00 PM | 120 | 19.62 | -0.03 |
| 9/18/06 3:30 PM | 150 | 19.62 | -0.03 |
| 9/18/06 4:00 PM | 180 | 19.62 | -0.03 |
| 9/18/06 4:30 PM | 210 | 19.62 | -0.03 |
| 9/18/06 5:00 PM | 240 | 19.62 | -0.03 |
| 9/18/06 5:30 PM | 270 | 19.62 | -0.03 |
| 9/18/06 6:00 PM | 300 | 19.62 | -0.03 |
| 9/18/06 6:30 PM | 330 | 19.62 | -0.03 |
| 9/18/06 7:00 PM | 360 | 19.62 | -0.03 |
| 9/18/06 8:00 PM | 420 | 19.62 | -0.03 |
| 9/18/06 9:00 PM | 480 | 19.62 | -0.03 |
| 9/18/06 10:00 PM | 540 | 19.61 | -0.04 |
| 9/18/06 11:00 PM | 600 | 19.61 | -0.04 |
| 9/19/06 12:00 AM | 660 | 19.59 | -0.06 |
| 9/19/06 1:00 AM | 720 | 19.60 | -0.05 |
| 9/19/06 2:00 AM | 780 | 19.59 | -0.06 |
| 9/19/06 3:00 AM | 840 | 19.59 | -0.06 |
| 9/19/06 4:00 AM | 900 | 19.58 | -0.07 |
| 9/19/06 5:00 AM | 960 | 19.59 | -0.06 |
| 9/19/06 6:00 AM | 1020 | 19.59 | -0.06 |
| 9/19/06 7:00 AM | 1080 | 19.59 | -0.06 |
| 9/19/06 8:00 AM | 1140 | 19.60 | -0.05 |
| 9/19/06 9:00 AM | 1200 | 19.61 | -0.04 |
| 9/19/06 10:00 AM | 1260 | 19.61 | -0.04 |
| 9/19/06 11:00 AM | 1320 | 19.61 | -0.04 |
| 9/19/06 12:00 PM | 1380 | 19.61 | -0.04 |
| 9/19/06 1:00 PM | 1440 | 19.58 | -0.07 |
| 9/19/06 2:00 PM | 1500 | 19.56 | -0.09 |

September 18 - 21, 2006
 BELLEFONTE NUCLEAR SITE
 SCOTTSBORO, JACKSON COUNTY, AL
 TERRA-SOLVE PROJECT NO. 06575

TEST TYPE: Variable Discharge
 REFERENCE POINT: TOC
 STATIC DEPTH TO WATER: 19.65 feet
 WELL TOTAL DEPTH: 33.45 feet
 WELL DIAMETER: 2 -inch
 ASSOCIATED WITH PUMPING WELL: MW-1217B
 DISTANCE FROM PUMPING WELL: 77.00 feet

OBSERVATION WELL: OW-10

| | | | |
|-----------------|------|-------|-------|
| 9/19/06 2:02 PM | 1502 | 19.55 | -0.10 |
| 9/19/06 2:04 PM | 1504 | 19.55 | -0.10 |
| 9/19/06 2:06 PM | 1506 | 19.55 | -0.10 |
| 9/19/06 2:08 PM | 1508 | 19.56 | -0.09 |
| 9/19/06 2:10 PM | 1510 | 19.56 | -0.09 |
| 9/19/06 2:12 PM | 1512 | 19.56 | -0.09 |
| 9/19/06 2:14 PM | 1514 | 19.56 | -0.09 |
| 9/19/06 2:16 PM | 1516 | 19.56 | -0.09 |
| 9/19/06 2:18 PM | 1518 | 19.56 | -0.09 |
| 9/19/06 2:20 PM | 1520 | 19.56 | -0.09 |
| 9/19/06 2:22 PM | 1522 | 19.56 | -0.09 |
| 9/19/06 2:24 PM | 1524 | 19.57 | -0.08 |
| 9/19/06 2:26 PM | 1526 | 19.56 | -0.09 |
| 9/19/06 2:28 PM | 1528 | 19.56 | -0.09 |
| 9/19/06 2:30 PM | 1530 | 19.56 | -0.09 |
| 9/19/06 2:32 PM | 1532 | 19.57 | -0.08 |
| 9/19/06 2:34 PM | 1534 | 19.57 | -0.08 |
| 9/19/06 2:36 PM | 1536 | 19.57 | -0.08 |
| 9/19/06 2:38 PM | 1538 | 19.57 | -0.08 |
| 9/19/06 2:40 PM | 1540 | 19.57 | -0.08 |
| 9/19/06 2:42 PM | 1542 | 19.57 | -0.08 |
| 9/19/06 2:44 PM | 1544 | 19.57 | -0.08 |
| 9/19/06 2:46 PM | 1546 | 19.57 | -0.08 |
| 9/19/06 2:48 PM | 1548 | 19.57 | -0.08 |
| 9/19/06 2:50 PM | 1550 | 19.57 | -0.08 |
| 9/19/06 2:52 PM | 1552 | 19.57 | -0.08 |
| 9/19/06 2:54 PM | 1554 | 19.57 | -0.08 |
| 9/19/06 2:56 PM | 1556 | 19.57 | -0.08 |
| 9/19/06 2:58 PM | 1558 | 19.57 | -0.08 |
| 9/19/06 3:00 PM | 1560 | 19.57 | -0.08 |
| 9/19/06 3:05 PM | 1565 | 19.57 | -0.08 |
| 9/19/06 3:10 PM | 1570 | 19.57 | -0.08 |
| 9/19/06 3:15 PM | 1575 | 19.57 | -0.08 |
| 9/19/06 3:20 PM | 1580 | 19.57 | -0.08 |
| 9/19/06 3:25 PM | 1585 | 19.57 | -0.08 |
| 9/19/06 3:30 PM | 1590 | 19.57 | -0.08 |
| 9/19/06 3:35 PM | 1595 | 19.56 | -0.09 |
| 9/19/06 3:40 PM | 1600 | 19.55 | -0.10 |
| 9/19/06 3:45 PM | 1605 | 19.55 | -0.10 |
| 9/19/06 3:50 PM | 1610 | 19.55 | -0.10 |
| 9/19/06 3:55 PM | 1615 | 19.55 | -0.10 |
| 9/19/06 4:00 PM | 1620 | 19.55 | -0.10 |
| 9/19/06 4:10 PM | 1630 | 19.55 | -0.10 |

September 18 - 21, 2006
BELLEFONTE NUCLEAR SITE
SCOTTSBORO, JACKSON COUNTY, AL
TERRA-SOLVE PROJECT NO. 06575

TEST TYPE: Variable Discharge
REFERENCE POINT: TOC
STATIC DEPTH TO WATER: 19.65 feet
WELL TOTAL DEPTH: 33.45 feet
WELL DIAMETER: 2 -inch
ASSOCIATED WITH PUMPING WELL: MW-1217B
DISTANCE FROM PUMPING WELL: 77.00 feet

| | |
|--------------------------|--------------|
| OBSERVATION WELL: | OW-10 |
|--------------------------|--------------|

| | | | |
|-----------------|------|-------|-------|
| 9/19/06 4:20 PM | 1640 | 19.55 | -0.10 |
| 9/19/06 4:30 PM | 1650 | 19.55 | -0.10 |
| 9/19/06 4:40 PM | 1660 | 19.54 | -0.11 |
| 9/19/06 4:50 PM | 1670 | 19.54 | -0.11 |
| 9/19/06 5:00 PM | 1680 | 19.54 | -0.11 |
| 9/20/06 8:10 AM | 2590 | 19.43 | -0.22 |
| 9/20/06 2:47 PM | 2987 | 19.34 | -0.31 |
| 9/21/06 8:16 AM | 4036 | 19.24 | -0.41 |

Pump off after 1500 minutes.

PUMPING TEST FIELD DATA

September 18 - 21, 2006

BELLEFONTE NUCLEAR SITE

SCOTTSBORO, JACKSON COUNTY, AL

TERRA-SOLVE PROJECT NO. 06575

TEST TYPE: Variable Discharge
 REFERENCE POINT: TOC
 STATIC DEPTH TO WATER: 18.10 feet
 WELL TOTAL DEPTH: 32.92 feet
 WELL DIAMETER: 2 -inch
 ASSOCIATED WITH PUMPING WELL: MW-1217B
 DISTANCE FROM PUMPING WELL: 90.50 feet

| | |
|--------------------------|--------------|
| OBSERVATION WELL: | OW-11 |
|--------------------------|--------------|

| Date | Time (min) | Depth to Water (feet) | Drawdown (feet) |
|-----------------|------------|-----------------------|-----------------|
| 9/18/06 1:00 PM | 0 | 18.10 | |
| 9/18/06 1:02 PM | 2 | 18.10 | 0.00 |
| 9/18/06 1:04 PM | 4 | 18.10 | 0.00 |
| 9/18/06 1:06 PM | 6 | 18.10 | 0.00 |
| 9/18/06 1:08 PM | 8 | 18.10 | 0.00 |
| 9/18/06 1:10 PM | 10 | 18.10 | 0.00 |
| 9/18/06 1:12 PM | 12 | 18.10 | 0.00 |
| 9/18/06 1:14 PM | 14 | 18.10 | 0.00 |
| 9/18/06 1:16 PM | 16 | 18.10 | 0.00 |
| 9/18/06 1:18 PM | 18 | 18.10 | 0.00 |
| 9/18/06 1:20 PM | 20 | 18.10 | 0.00 |
| 9/18/06 1:22 PM | 22 | 18.10 | 0.00 |
| 9/18/06 1:24 PM | 24 | 18.10 | 0.00 |
| 9/18/06 1:26 PM | 26 | 18.10 | 0.00 |
| 9/18/06 1:28 PM | 28 | 18.11 | 0.01 |
| 9/18/06 1:30 PM | 30 | 18.11 | 0.01 |
| 9/18/06 1:32 PM | 32 | 18.12 | 0.02 |
| 9/18/06 1:34 PM | 34 | 18.12 | 0.02 |
| 9/18/06 1:36 PM | 36 | 18.12 | 0.02 |
| 9/18/06 1:38 PM | 38 | 18.12 | 0.02 |
| 9/18/06 1:40 PM | 40 | 18.12 | 0.02 |
| 9/18/06 1:42 PM | 42 | 18.12 | 0.02 |
| 9/18/06 1:44 PM | 44 | 18.13 | 0.03 |
| 9/18/06 1:46 PM | 46 | 18.13 | 0.03 |
| 9/18/06 1:48 PM | 48 | 18.13 | 0.03 |
| 9/18/06 1:50 PM | 50 | 18.13 | 0.03 |
| 9/18/06 1:52 PM | 52 | 18.13 | 0.03 |
| 9/18/06 1:54 PM | 54 | 18.13 | 0.03 |
| 9/18/06 1:56 PM | 56 | 18.14 | 0.04 |
| 9/18/06 1:58 PM | 58 | 18.14 | 0.04 |
| 9/18/06 2:00 PM | 60 | 18.14 | 0.04 |
| 9/18/06 2:05 PM | 65 | 18.14 | 0.04 |
| 9/18/06 2:10 PM | 70 | 18.15 | 0.05 |
| 9/18/06 2:15 PM | 75 | 18.15 | 0.05 |
| 9/18/06 2:20 PM | 80 | 18.15 | 0.05 |
| 9/18/06 2:25 PM | 85 | 18.16 | 0.06 |
| 9/18/06 2:30 PM | 90 | 18.16 | 0.06 |
| 9/18/06 3:00 PM | 120 | 18.20 | 0.10 |
| 9/18/06 3:30 PM | 150 | 18.23 | 0.13 |
| 9/18/06 4:00 PM | 180 | 18.25 | 0.15 |

September 18 - 21, 2006
 BELLEFONTE NUCLEAR SITE
 SCOTTSBORO, JACKSON COUNTY, AL
 TERRA-SOLVE PROJECT NO. 06575

TEST TYPE: Variable Discharge
 REFERENCE POINT: TOC
 STATIC DEPTH TO WATER: 18.10 feet
 WELL TOTAL DEPTH: 32.92 feet
 WELL DIAMETER: 2 -inch
 ASSOCIATED WITH PUMPING WELL: MW-1217B
 DISTANCE FROM PUMPING WELL: 90.50 feet

OBSERVATION WELL: OW-11

| | | | |
|------------------|------|-------|------|
| 9/18/06 4:30 PM | 210 | 18.28 | 0.18 |
| 9/18/06 5:00 PM | 240 | 18.31 | 0.21 |
| 9/18/06 5:30 PM | 270 | 18.33 | 0.23 |
| 9/18/06 6:00 PM | 300 | 18.35 | 0.25 |
| 9/18/06 6:30 PM | 330 | 18.35 | 0.25 |
| 9/18/06 7:00 PM | 360 | 18.39 | 0.29 |
| 9/18/06 8:00 PM | 420 | 18.41 | 0.31 |
| 9/18/06 9:00 PM | 480 | 18.42 | 0.32 |
| 9/18/06 10:00 PM | 540 | 18.44 | 0.34 |
| 9/18/06 11:00 PM | 600 | 18.46 | 0.36 |
| 9/19/06 12:00 AM | 660 | 18.43 | 0.33 |
| 9/19/06 1:00 AM | 720 | 18.43 | 0.33 |
| 9/19/06 2:00 AM | 780 | 18.43 | 0.33 |
| 9/19/06 3:00 AM | 840 | 18.43 | 0.33 |
| 9/19/06 4:00 AM | 900 | 18.43 | 0.33 |
| 9/19/06 5:00 AM | 960 | 18.43 | 0.33 |
| 9/19/06 6:00 AM | 1020 | 18.43 | 0.33 |
| 9/19/06 7:00 AM | 1080 | 18.38 | 0.28 |
| 9/19/06 8:00 AM | 1140 | 18.36 | 0.26 |
| 9/19/06 9:00 AM | 1200 | 18.32 | 0.22 |
| 9/19/06 10:00 AM | 1260 | 18.31 | 0.21 |
| 9/19/06 11:00 AM | 1320 | 18.29 | 0.19 |
| 9/19/06 12:00 PM | 1380 | 18.26 | 0.16 |
| 9/19/06 1:00 PM | 1440 | 18.23 | 0.13 |
| 9/19/06 2:00 PM | 1500 | 18.21 | 0.11 |
| 9/19/06 2:02 PM | 1502 | 18.21 | 0.11 |
| 9/19/06 2:04 PM | 1504 | 18.21 | 0.11 |
| 9/19/06 2:06 PM | 1506 | 18.20 | 0.10 |
| 9/19/06 2:08 PM | 1508 | 18.20 | 0.10 |
| 9/19/06 2:10 PM | 1510 | 18.20 | 0.10 |
| 9/19/06 2:12 PM | 1512 | 18.20 | 0.10 |
| 9/19/06 2:14 PM | 1514 | 18.20 | 0.10 |
| 9/19/06 2:16 PM | 1516 | 18.19 | 0.09 |
| 9/19/06 2:18 PM | 1518 | 18.19 | 0.09 |
| 9/19/06 2:20 PM | 1520 | 18.18 | 0.08 |
| 9/19/06 2:22 PM | 1522 | 18.18 | 0.08 |
| 9/19/06 2:24 PM | 1524 | 18.18 | 0.08 |
| 9/19/06 2:26 PM | 1526 | 18.18 | 0.08 |
| 9/19/06 2:28 PM | 1528 | 18.17 | 0.07 |
| 9/19/06 2:30 PM | 1530 | 18.17 | 0.07 |
| 9/19/06 2:32 PM | 1532 | 18.17 | 0.07 |
| 9/19/06 2:34 PM | 1534 | 18.17 | 0.07 |
| 9/19/06 2:36 PM | 1536 | 18.16 | 0.06 |

September 18 - 21, 2006
 BELLEFONTE NUCLEAR SITE
 SCOTTSBORO, JACKSON COUNTY, AL
 TERRA-SOLVE PROJECT NO. 06575

TEST TYPE: Variable Discharge
 REFERENCE POINT: TOC
 STATIC DEPTH TO WATER: 18.10 feet
 WELL TOTAL DEPTH: 32.92 feet
 WELL DIAMETER: 2 -inch
 ASSOCIATED WITH PUMPING WELL: MW-1217B
 DISTANCE FROM PUMPING WELL: 90.50 feet

OBSERVATION WELL: OW-11

| | | | |
|-----------------|------|-------|-------|
| 9/19/06 2:38 PM | 1538 | 18.16 | 0.06 |
| 9/19/06 2:40 PM | 1540 | 18.16 | 0.06 |
| 9/19/06 2:42 PM | 1542 | 18.16 | 0.06 |
| 9/19/06 2:44 PM | 1544 | 18.16 | 0.06 |
| 9/19/06 2:46 PM | 1546 | 18.16 | 0.06 |
| 9/19/06 2:48 PM | 1548 | 18.15 | 0.05 |
| 9/19/06 2:50 PM | 1550 | 18.15 | 0.05 |
| 9/19/06 2:52 PM | 1552 | 18.15 | 0.05 |
| 9/19/06 2:54 PM | 1554 | 18.15 | 0.05 |
| 9/19/06 2:56 PM | 1556 | 18.14 | 0.04 |
| 9/19/06 2:58 PM | 1558 | 18.14 | 0.04 |
| 9/19/06 3:00 PM | 1560 | 18.14 | 0.04 |
| 9/19/06 3:05 PM | 1565 | 18.12 | 0.02 |
| 9/19/06 3:10 PM | 1570 | 18.12 | 0.02 |
| 9/19/06 3:15 PM | 1575 | 18.11 | 0.01 |
| 9/19/06 3:20 PM | 1580 | 18.11 | 0.01 |
| 9/19/06 3:25 PM | 1585 | 18.11 | 0.01 |
| 9/19/06 3:30 PM | 1590 | 18.10 | 0.00 |
| 9/19/06 3:35 PM | 1595 | 18.10 | 0.00 |
| 9/19/06 3:40 PM | 1600 | 18.09 | -0.01 |
| 9/19/06 3:45 PM | 1605 | 18.09 | -0.01 |
| 9/19/06 3:50 PM | 1610 | 18.08 | -0.02 |
| 9/19/06 3:55 PM | 1615 | 18.08 | -0.02 |
| 9/19/06 4:00 PM | 1620 | 18.06 | -0.04 |
| 9/19/06 4:10 PM | 1630 | 18.06 | -0.04 |
| 9/19/06 4:20 PM | 1640 | 18.06 | -0.04 |
| 9/19/06 4:30 PM | 1650 | 18.06 | -0.04 |
| 9/19/06 4:40 PM | 1660 | 18.06 | -0.04 |
| 9/19/06 4:50 PM | 1670 | 18.05 | -0.05 |
| 9/19/06 5:00 PM | 1680 | 18.05 | -0.05 |
| 9/20/06 8:13 AM | 2593 | 17.67 | -0.43 |
| 9/20/06 2:44 PM | 2984 | 17.38 | -0.72 |
| 9/21/06 8:15 AM | 4035 | 17.06 | -1.04 |

Pump off after 1500 minutes.

PUMPING TEST FIELD DATA

September 18 - 21, 2006
BELLEFONTE NUCLEAR SITE
SCOTTSBORO, JACKSON COUNTY, AL
TERRA-SOLVE PROJECT NO. 06575

TEST TYPE: Variable Discharge
REFERENCE POINT: TOC
STATIC DEPTH TO WATER: 19.42 feet
WELL TOTAL DEPTH: 32.95 feet
WELL DIAMETER: 2 -inch
ASSOCIATED WITH PUMPING WELL: MW-1217B
DISTANCE FROM PUMPING WELL: 78.60 feet

OBSERVATION WELL: OW-12

| Date | Time (min) | Depth to Water (feet) | Drawdown (feet) |
|-----------------|------------|-----------------------|-----------------|
| 9/18/06 1:00 PM | 0 | 19.42 | |
| 9/18/06 1:02 PM | 2 | 19.42 | 0.00 |
| 9/18/06 1:04 PM | 4 | 19.42 | 0.00 |
| 9/18/06 1:06 PM | 6 | 19.42 | 0.00 |
| 9/18/06 1:08 PM | 8 | 19.42 | 0.00 |
| 9/18/06 1:10 PM | 10 | 19.42 | 0.00 |
| 9/18/06 1:12 PM | 12 | 19.42 | 0.00 |
| 9/18/06 1:14 PM | 14 | 19.44 | 0.02 |
| 9/18/06 1:16 PM | 16 | 19.45 | 0.03 |
| 9/18/06 1:18 PM | 18 | 19.46 | 0.04 |
| 9/18/06 1:20 PM | 20 | 19.46 | 0.04 |
| 9/18/06 1:22 PM | 22 | 19.47 | 0.05 |
| 9/18/06 1:24 PM | 24 | 19.48 | 0.06 |
| 9/18/06 1:26 PM | 26 | 19.49 | 0.07 |
| 9/18/06 1:28 PM | 28 | 19.50 | 0.08 |
| 9/18/06 1:30 PM | 30 | 19.50 | 0.08 |
| 9/18/06 1:32 PM | 32 | 19.51 | 0.09 |
| 9/18/06 1:34 PM | 34 | 19.51 | 0.09 |
| 9/18/06 1:36 PM | 36 | 19.52 | 0.10 |
| 9/18/06 1:38 PM | 38 | 19.52 | 0.10 |
| 9/18/06 1:40 PM | 40 | 19.53 | 0.11 |
| 9/18/06 1:42 PM | 42 | 19.54 | 0.12 |
| 9/18/06 1:44 PM | 44 | 19.55 | 0.13 |
| 9/18/06 1:46 PM | 46 | 19.56 | 0.14 |
| 9/18/06 1:48 PM | 48 | 19.57 | 0.15 |
| 9/18/06 1:50 PM | 50 | 19.58 | 0.16 |
| 9/18/06 1:52 PM | 52 | 19.58 | 0.16 |
| 9/18/06 1:54 PM | 54 | 19.58 | 0.16 |
| 9/18/06 1:56 PM | 56 | 19.60 | 0.18 |
| 9/18/06 1:58 PM | 58 | 19.60 | 0.18 |
| 9/18/06 2:00 PM | 60 | 19.61 | 0.19 |
| 9/18/06 2:05 PM | 65 | 19.63 | 0.21 |
| 9/18/06 2:10 PM | 70 | 19.65 | 0.23 |
| 9/18/06 2:15 PM | 75 | 19.68 | 0.26 |
| 9/18/06 2:20 PM | 80 | 19.69 | 0.27 |
| 9/18/06 2:25 PM | 85 | 19.71 | 0.29 |
| 9/18/06 2:30 PM | 90 | 19.72 | 0.30 |
| 9/18/06 3:00 PM | 120 | 19.83 | 0.41 |
| 9/18/06 3:30 PM | 150 | 19.90 | 0.48 |
| 9/18/06 4:00 PM | 180 | 19.95 | 0.53 |

September 18 - 21, 2006
 BELLEFONTE NUCLEAR SITE
 SCOTTSBORO, JACKSON COUNTY, AL
 TERRA-SOLVE PROJECT NO. 06575

TEST TYPE: Variable Discharge
 REFERENCE POINT: TOC
 STATIC DEPTH TO WATER: 19.42 feet
 WELL TOTAL DEPTH: 32.95 feet
 WELL DIAMETER: 2 -inch
 ASSOCIATED WITH PUMPING WELL: MW-1217B
 DISTANCE FROM PUMPING WELL: 78.60 feet

| | |
|--------------------------|--------------|
| OBSERVATION WELL: | OW-12 |
|--------------------------|--------------|

| | | | |
|------------------|------|-------|-------|
| 9/18/06 4:30 PM | 210 | 19.99 | 0.57 |
| 9/18/06 5:00 PM | 240 | 20.03 | 0.61 |
| 9/18/06 5:30 PM | 270 | 20.09 | 0.67 |
| 9/18/06 6:00 PM | 300 | 20.10 | 0.68 |
| 9/18/06 6:30 PM | 330 | 20.10 | 0.68 |
| 9/18/06 7:00 PM | 360 | 20.11 | 0.69 |
| 9/18/06 8:00 PM | 420 | 20.11 | 0.69 |
| 9/18/06 9:00 PM | 480 | 20.11 | 0.69 |
| 9/18/06 10:00 PM | 540 | 20.09 | 0.67 |
| 9/18/06 11:00 PM | 600 | 20.03 | 0.61 |
| 9/19/06 12:00 AM | 660 | 19.98 | 0.56 |
| 9/19/06 1:00 AM | 720 | 19.94 | 0.52 |
| 9/19/06 2:00 AM | 780 | 19.87 | 0.45 |
| 9/19/06 3:00 AM | 840 | 19.81 | 0.39 |
| 9/19/06 4:00 AM | 900 | 19.73 | 0.31 |
| 9/19/06 5:00 AM | 960 | 19.65 | 0.23 |
| 9/19/06 6:00 AM | 1020 | 19.56 | 0.14 |
| 9/19/06 7:00 AM | 1080 | 19.48 | 0.06 |
| 9/19/06 8:00 AM | 1140 | 19.40 | -0.02 |
| 9/19/06 9:00 AM | 1200 | 19.30 | -0.12 |
| 9/19/06 10:00 AM | 1260 | 19.25 | -0.17 |
| 9/19/06 11:00 AM | 1320 | 19.16 | -0.26 |
| 9/19/06 12:00 PM | 1380 | 19.11 | -0.31 |
| 9/19/06 1:00 PM | 1440 | 19.04 | -0.38 |
| 9/19/06 2:00 PM | 1500 | 18.97 | -0.45 |
| 9/19/06 2:02 PM | 1502 | 18.97 | -0.45 |
| 9/19/06 2:04 PM | 1504 | 18.97 | -0.45 |
| 9/19/06 2:06 PM | 1506 | 18.97 | -0.45 |
| 9/19/06 2:08 PM | 1508 | 18.97 | -0.45 |
| 9/19/06 2:10 PM | 1510 | 18.95 | -0.47 |
| 9/19/06 2:12 PM | 1512 | 18.95 | -0.47 |
| 9/19/06 2:14 PM | 1514 | 18.95 | -0.47 |
| 9/19/06 2:16 PM | 1516 | 18.94 | -0.48 |
| 9/19/06 2:18 PM | 1518 | 18.94 | -0.48 |
| 9/19/06 2:20 PM | 1520 | 18.93 | -0.49 |
| 9/19/06 2:22 PM | 1522 | 18.92 | -0.50 |
| 9/19/06 2:24 PM | 1524 | 18.92 | -0.50 |
| 9/19/06 2:26 PM | 1526 | 18.91 | -0.51 |
| 9/19/06 2:28 PM | 1528 | 18.91 | -0.51 |
| 9/19/06 2:30 PM | 1530 | 18.89 | -0.53 |
| 9/19/06 2:32 PM | 1532 | 18.89 | -0.53 |
| 9/19/06 2:34 PM | 1534 | 18.88 | -0.54 |
| 9/19/06 2:36 PM | 1536 | 18.88 | -0.54 |

September 18 - 21, 2006
 BELLEFONTE NUCLEAR SITE
 SCOTTSBORO, JACKSON COUNTY, AL
 TERRA-SOLVE PROJECT NO. 06575

TEST TYPE: Variable Discharge
 REFERENCE POINT: TOC
 STATIC DEPTH TO WATER: 19.42 feet
 WELL TOTAL DEPTH: 32.95 feet
 WELL DIAMETER: 2 -inch
 ASSOCIATED WITH PUMPING WELL: MW-1217B
 DISTANCE FROM PUMPING WELL: 78.60 feet

OBSERVATION WELL: OW-12

| | | | |
|-----------------|------|-------|-------|
| 9/19/06 2:38 PM | 1538 | 18.87 | -0.55 |
| 9/19/06 2:40 PM | 1540 | 18.86 | -0.56 |
| 9/19/06 2:42 PM | 1542 | 18.85 | -0.57 |
| 9/19/06 2:44 PM | 1544 | 18.84 | -0.58 |
| 9/19/06 2:46 PM | 1546 | 18.84 | -0.58 |
| 9/19/06 2:48 PM | 1548 | 18.83 | -0.59 |
| 9/19/06 2:50 PM | 1550 | 18.82 | -0.60 |
| 9/19/06 2:52 PM | 1552 | 18.81 | -0.61 |
| 9/19/06 2:54 PM | 1554 | 18.80 | -0.62 |
| 9/19/06 2:56 PM | 1556 | 18.80 | -0.62 |
| 9/19/06 2:58 PM | 1558 | 18.79 | -0.63 |
| 9/19/06 3:00 PM | 1560 | 18.78 | -0.64 |
| 9/19/06 3:05 PM | 1565 | 18.76 | -0.66 |
| 9/19/06 3:10 PM | 1570 | 18.75 | -0.67 |
| 9/19/06 3:15 PM | 1575 | 18.72 | -0.70 |
| 9/19/06 3:20 PM | 1580 | 18.70 | -0.72 |
| 9/19/06 3:25 PM | 1585 | 18.69 | -0.73 |
| 9/19/06 3:30 PM | 1590 | 18.67 | -0.75 |
| 9/19/06 3:35 PM | 1595 | 18.65 | -0.77 |
| 9/19/06 3:40 PM | 1600 | 18.64 | -0.78 |
| 9/19/06 3:45 PM | 1605 | 18.62 | -0.80 |
| 9/19/06 3:50 PM | 1610 | 18.61 | -0.81 |
| 9/19/06 3:55 PM | 1615 | 18.59 | -0.83 |
| 9/19/06 4:00 PM | 1620 | 18.57 | -0.85 |
| 9/19/06 4:10 PM | 1630 | 18.52 | -0.90 |
| 9/19/06 4:20 PM | 1640 | 18.51 | -0.91 |
| 9/19/06 4:30 PM | 1650 | 18.48 | -0.94 |
| 9/19/06 4:40 PM | 1660 | 18.45 | -0.97 |
| 9/19/06 4:50 PM | 1670 | 18.42 | -1.00 |
| 9/19/06 5:00 PM | 1680 | 18.40 | -1.02 |
| 9/20/06 8:13 AM | 2593 | 17.63 | -1.79 |
| 9/20/06 2:42 PM | 2982 | 17.49 | -1.93 |
| 9/21/06 8:10 AM | 4030 | 17.38 | -2.04 |

Pump off after 1500 minutes.

**Waterloo Hydrogeologic, Inc.**

460 Philip Street - Suite 101

Waterloo, Ontario, Canada

Phone: +1 519 746 1798

Slug Test Data Report

Project: Bellefonte Nuclear Site Bail Test

Number: 06575

Client: ENERCON

Page 1

Test Well: MW-1203B**Slug Test: 1203B BAIL TEST**

Test Well: MW-1203B

Depth to Static WL: 13.34 [ft]

Casing radius: 0.17 [ft]

Location: Scottsboro, Jackson County, AL

Boring radius: 0.34 [ft]

Recorded by: PWE

Screen length: 10 [ft]

Date: 9/20/2006

Aquifer Thickness: 19.21 [ft]

| | Time [min] | Depth to WL [ft] | Drawdown [ft] |
|----|------------|------------------|---------------|
| 1 | 15 | 32.06 | 18.72 |
| 2 | 25 | 32.00 | 18.66 |
| 3 | 30 | 31.96 | 18.62 |
| 4 | 35 | 31.94 | 18.60 |
| 5 | 40 | 31.91 | 18.57 |
| 6 | 45 | 31.89 | 18.55 |
| 7 | 50 | 31.87 | 18.53 |
| 8 | 55 | 31.85 | 18.51 |
| 9 | 60 | 31.82 | 18.48 |
| 10 | 65 | 31.80 | 18.46 |
| 11 | 70 | 31.78 | 18.44 |
| 12 | 75 | 31.77 | 18.43 |
| 13 | 80 | 31.75 | 18.41 |
| 14 | 85 | 31.73 | 18.39 |
| 15 | 90 | 31.72 | 18.38 |
| 16 | 95 | 31.71 | 18.37 |
| 17 | 100 | 31.69 | 18.35 |
| 18 | 105 | 31.68 | 18.34 |
| 19 | 110 | 31.67 | 18.33 |
| 20 | 115 | 31.66 | 18.32 |
| 21 | 120 | 31.65 | 18.31 |
| 22 | 125 | 31.64 | 18.30 |
| 23 | 130 | 31.63 | 18.29 |
| 24 | 1090 | 30.37 | 17.03 |

In-Situ Inc. Troll 9000 Pro XP
Report generated: 9/21/2006 15:59:12
Report from file: ...\\SN45065 2006-09-18 131417 bellefonte 1.bin
Win-Situ@ Version 4.57.0.0

Serial number: 45065
Firmware Version 2
Unit name: Troll 9000

Test name: bellefonte 1

Test defined on: 9/17/2006 19:00:05
Test started on: 9/18/2006 13:14:17
Test stopped on: 9/19/2006 14:11:10

Data gathered using Linear testing
Time between data points: Seconds.
Number of data samples: 300

TOTAL DATA SAMPLES 300

Channel number [1]
Measurement type: Temperature
Channel name:

Channel number [3]
Measurement type: Barometric Pressure
Channel name:

Channel number [5]
Measurement type: Battery Voltage
Channel name:

Channel number [11]
Measurement type: ORP
Channel name:

Channel number [12]
Measurement type: pH
Channel name:

Channel number [25]
 Measurement type: Dissolved Oxygen
 Channel name:

Channel number [25]
 Measurement type: Dissolved Oxygen %Saturation
 Channel name:

Channel number [45]
 Measurement type: Conductivity, Low Range
 Channel name:

| Date | Time | ET (sec) | Chan[1] Temperature Fahrenheit | Chan[3] Barometric Inches Hg | Chan[5] Battery Volts | Chan[11] ORP millivolts | Chan[12] pH pH | Chan[25] Clark DO microgram | Chan[25] Clark DO Sat %Saturation | Chan[45] Conductivity microSiemens/cm Actual Conductivity |
|-----------|----------|----------|--------------------------------------|------------------------------------|-----------------------------|-------------------------------|----------------------|-----------------------------------|---|--|
| 9/18/2006 | 13:14:17 | 0 | 68.58 | 29.234 | 2.785 | 146 | 6.97 | 763 | 8.6871 | 1436.04 |
| 9/18/2006 | 13:19:17 | 300 | 68.51 | 29.352 | 2.785 | 137 | 6.98 | 574 | 6.5068 | 1434.28 |
| 9/18/2006 | 13:24:17 | 600 | 68.48 | 29.277 | 2.785 | 133 | 6.99 | 538 | 6.1123 | 1434.42 |
| 9/18/2006 | 13:29:17 | 900 | 68.45 | 29.233 | 2.811 | 130 | 6.99 | 569 | 6.4704 | 1435.09 |
| 9/18/2006 | 13:34:17 | 1200 | 68.42 | 29.208 | 2.811 | 127 | 7 | 597 | 6.7892 | 1433.43 |
| 9/18/2006 | 13:39:17 | 1500 | 68.41 | 29.202 | 2.811 | 126 | 7 | 604 | 6.877 | 1431.92 |
| 9/18/2006 | 13:44:17 | 1800 | 68.37 | 29.188 | 2.785 | 125 | 7 | 600 | 6.8336 | 1433.1 |
| 9/18/2006 | 13:49:17 | 2100 | 68.33 | 29.191 | 2.785 | 124 | 7 | 654 | 7.4384 | 1431.28 |
| 9/18/2006 | 13:54:17 | 2400 | 68.33 | 29.185 | 2.785 | 124 | 7 | 666 | 7.5783 | 1430.79 |
| 9/18/2006 | 13:59:17 | 2700 | 68.31 | 29.18 | 2.785 | 122 | 7 | 687 | 7.8134 | 1429.88 |
| 9/18/2006 | 14:04:17 | 3000 | 68.92 | 29.169 | 2.785 | 67 | 7.09 | 10659 | 121.8848 | 860.35 |
| 9/18/2006 | 14:09:17 | 3300 | 68.97 | 29.171 | 2.785 | 334 | 7.23 | 9472 | 108.0539 | 1.43 |
| 9/18/2006 | 14:14:17 | 3600 | 68.98 | 29.175 | 2.811 | 356 | 7.24 | 7378 | 84.1728 | 1.43 |
| 9/18/2006 | 14:19:17 | 3900 | 69.01 | 29.181 | 2.785 | 389 | 7.26 | 8072 | 92.0973 | 1.43 |
| 9/18/2006 | 14:24:17 | 4200 | 68.99 | 29.189 | 2.811 | 427 | 7.28 | 9342 | 106.5303 | 1.43 |
| 9/18/2006 | 14:29:17 | 4500 | 68.97 | 29.191 | 2.785 | 461 | 7.27 | 9403 | 107.1954 | 1.43 |
| 9/18/2006 | 14:34:17 | 4800 | 68.97 | 29.191 | 2.785 | 468 | 7.26 | 9399 | 107.1499 | 1.43 |
| 9/18/2006 | 14:39:17 | 5100 | 68.98 | 29.197 | 2.811 | 487 | 7.27 | 9405 | 107.2067 | 1.43 |
| 9/18/2006 | 14:44:17 | 5400 | 68.98 | 29.2 | 2.785 | 389 | 7.24 | 9385 | 106.9651 | 1.43 |
| 9/18/2006 | 14:49:17 | 5700 | 68.97 | 29.211 | 2.785 | 180 | 7.14 | 4727 | 53.9471 | 583.18 |
| 9/18/2006 | 14:54:17 | 6000 | 68.99 | 29.212 | 2.785 | 299 | 7.22 | 7586 | 86.4317 | 1.43 |
| 9/18/2006 | 14:59:17 | 6300 | 68.96 | 29.201 | 2.785 | 177 | 7.14 | 8083 | 92.282 | 582.53 |
| 9/18/2006 | 15:04:17 | 6600 | 68.96 | 29.219 | 2.811 | 153 | 7.14 | 8801 | 100.4136 | 581.88 |
| 9/18/2006 | 15:09:17 | 6900 | 68.97 | 29.22 | 2.759 | 144 | 7.14 | 8426 | 96.1415 | 581.31 |

| Date | Time | ET (sec) | Chan[1] Temperature Fahrenheit | Chan[3] Barometric Inches Hg | Chan[5] Battery Volts | Chan[11] ORP millivolts | Chan[12] pH pH | Chan[25] Clark DO microgram: | Chan[25] Clark DO Sat %Saturation | Chan[45] Conductivity microSiemens/cm Actual Conductivity |
|-----------|----------|----------|--------------------------------------|------------------------------------|-----------------------------|-------------------------------|----------------------|------------------------------------|---|--|
| 9/18/2006 | 15:14:17 | 7200 | 68.96 | 29.219 | 2.811 | 138 | 7.15 | 8053 | 91.8735 | 581.95 |
| 9/18/2006 | 15:19:17 | 7500 | 68.96 | 29.221 | 2.785 | 135 | 7.15 | 7693 | 87.7567 | 582.09 |
| 9/18/2006 | 15:24:17 | 7800 | 68.95 | 29.212 | 2.811 | 134 | 7.14 | 7337 | 83.7197 | 581.59 |
| 9/18/2006 | 15:29:17 | 8100 | 68.96 | 29.202 | 2.811 | 133 | 7.14 | 7020 | 80.1293 | 581.09 |
| 9/18/2006 | 15:34:17 | 8400 | 68.96 | 29.183 | 2.811 | 133 | 7.14 | 6718 | 76.7419 | 581.02 |
| 9/18/2006 | 15:39:17 | 8700 | 68.97 | 29.148 | 2.785 | 133 | 7.13 | 6440 | 73.6657 | 581.45 |
| 9/18/2006 | 15:44:17 | 9000 | 68.97 | 29.104 | 2.785 | 133 | 7.13 | 6168 | 70.6651 | 582.45 |
| 9/18/2006 | 15:49:17 | 9300 | 68.97 | 29.057 | 2.785 | 133 | 7.13 | 5928 | 68.0216 | 581.88 |
| 9/18/2006 | 15:54:17 | 9600 | 68.96 | 29.026 | 2.785 | 133 | 7.13 | 5721 | 65.7147 | 582.09 |
| 9/18/2006 | 15:59:17 | 9900 | 68.97 | 29.014 | 2.785 | 133 | 7.13 | 5510 | 63.3311 | 581.45 |
| 9/18/2006 | 16:04:17 | 10200 | 68.96 | 29.005 | 2.785 | 133 | 7.13 | 5313 | 61.072 | 580.23 |
| 9/18/2006 | 16:09:17 | 10500 | 68.96 | 29.003 | 2.785 | 133 | 7.13 | 5121 | 58.8643 | 579.8 |
| 9/18/2006 | 16:14:17 | 10800 | 68.96 | 29.006 | 2.811 | 134 | 7.13 | 4940 | 56.7857 | 579.87 |
| 9/18/2006 | 16:19:17 | 11100 | 68.96 | 29.008 | 2.785 | 134 | 7.13 | 4776 | 54.8941 | 579.51 |
| 9/18/2006 | 16:24:17 | 11400 | 68.97 | 29.008 | 2.811 | 134 | 7.13 | 4614 | 53.0386 | 579.51 |
| 9/18/2006 | 16:29:17 | 11700 | 68.96 | 29.009 | 2.785 | 135 | 7.13 | 4464 | 51.3016 | 579.51 |
| 9/18/2006 | 16:34:17 | 12000 | 68.96 | 29.01 | 2.785 | 135 | 7.13 | 4307 | 49.5029 | 580.23 |
| 9/18/2006 | 16:39:17 | 12300 | 68.95 | 29.013 | 2.785 | 137 | 7.13 | 4136 | 47.5229 | 579.66 |
| 9/18/2006 | 16:44:17 | 12600 | 68.96 | 29.013 | 2.785 | 137 | 7.14 | 3971 | 45.6289 | 579.51 |
| 9/18/2006 | 16:49:17 | 12900 | 68.95 | 29.016 | 2.785 | 137 | 7.13 | 3823 | 43.926 | 579.59 |
| 9/18/2006 | 16:54:17 | 13200 | 68.96 | 29.014 | 2.785 | 137 | 7.13 | 3674 | 42.2198 | 579.37 |
| 9/18/2006 | 16:59:17 | 13500 | 68.96 | 29.013 | 2.811 | 138 | 7.13 | 3546 | 40.7527 | 579.23 |
| 9/18/2006 | 17:04:17 | 13800 | 68.96 | 29.011 | 2.785 | 137 | 7.14 | 3434 | 39.4616 | 579.02 |
| 9/18/2006 | 17:09:17 | 14100 | 68.96 | 29.012 | 2.785 | 138 | 7.14 | 3338 | 38.3585 | 579.09 |
| 9/18/2006 | 17:14:17 | 14400 | 68.95 | 29.016 | 2.785 | 138 | 7.14 | 3246 | 37.2974 | 578.94 |
| 9/18/2006 | 17:19:17 | 14700 | 68.96 | 29.023 | 2.811 | 139 | 7.14 | 3161 | 36.3164 | 578.59 |
| 9/18/2006 | 17:24:17 | 15000 | 68.97 | 29.024 | 2.785 | 139 | 7.14 | 3084 | 35.4352 | 578.38 |
| 9/18/2006 | 17:29:17 | 15300 | 68.96 | 29.026 | 2.785 | 140 | 7.14 | 3017 | 34.6564 | 578.45 |
| 9/18/2006 | 17:34:17 | 15600 | 68.95 | 29.025 | 2.811 | 140 | 7.14 | 2954 | 33.9287 | 578.45 |
| 9/18/2006 | 17:39:17 | 15900 | 68.96 | 29.028 | 2.785 | 141 | 7.14 | 2889 | 33.1807 | 578.38 |
| 9/18/2006 | 17:44:17 | 16200 | 68.95 | 29.031 | 2.785 | 140 | 7.15 | 2830 | 32.4961 | 578.45 |
| 9/18/2006 | 17:49:17 | 16500 | 68.95 | 29.033 | 2.785 | 141 | 7.15 | 2770 | 31.8028 | 578.52 |
| 9/18/2006 | 17:54:17 | 16800 | 68.96 | 29.032 | 2.785 | 141 | 7.15 | 2709 | 31.109 | 578.59 |
| 9/18/2006 | 17:59:17 | 17100 | 68.95 | 29.031 | 2.785 | 142 | 7.15 | 2662 | 30.5643 | 578.24 |
| 9/18/2006 | 18:04:17 | 17400 | 68.94 | 29.027 | 2.785 | 143 | 7.15 | 2638 | 30.2956 | 578.02 |
| 9/18/2006 | 18:09:17 | 17700 | 68.95 | 29.024 | 2.759 | 138 | 7.15 | 2629 | 30.2024 | 577.81 |
| 9/18/2006 | 18:14:17 | 18000 | 68.93 | 29.023 | 2.785 | 137 | 7.15 | 2667 | 30.6291 | 577.6 |
| 9/18/2006 | 18:19:17 | 18300 | 68.92 | 29.024 | 2.785 | 137 | 7.14 | 3205 | 36.8026 | 577.67 |

| Date | Time | ET (sec) | Chan[1] Temperature Fahrenheit | Chan[3] Barometric Inches Hg | Chan[5] Battery Volts | Chan[11] ORP millivolts | Chan[12] pH pH | Chan[25] Clark DO microgram: | Chan[25] Clark DO Sat %Saturation | Chan[45] Conductivity microSiemens/cm Actual Conductivity |
|-----------|----------|----------|--------------------------------------|------------------------------------|-----------------------------|-------------------------------|----------------------|------------------------------------|---|--|
| 9/18/2006 | 18:24:17 | 18600 | 68.93 | 29.024 | 2.811 | 266 | 7.16 | 8806 | 100.934 | 1.47 |
| 9/18/2006 | 18:29:17 | 18900 | 68.95 | 29.022 | 2.785 | 298 | 7.17 | 6877 | 78.846 | 1.43 |
| 9/18/2006 | 18:34:17 | 19200 | 68.93 | 29.021 | 2.785 | 275 | 7.11 | 8280 | 94.9186 | 1.43 |
| 9/18/2006 | 18:39:17 | 19500 | 69.01 | 29.02 | 2.785 | 334 | 7.12 | 8299 | 95.2281 | 1.43 |
| 9/18/2006 | 18:44:17 | 19800 | 68.94 | 29.018 | 2.785 | 287 | 7 | 8279 | 94.9205 | 1.43 |
| 9/18/2006 | 18:49:17 | 20100 | 68.94 | 29.016 | 2.785 | 149 | 7.09 | 8225 | 94.3171 | 1.43 |
| 9/18/2006 | 18:54:17 | 20400 | 68.94 | 29.013 | 2.785 | 160 | 7.07 | 8162 | 93.6023 | 1.75 |
| 9/18/2006 | 18:59:17 | 20700 | 68.94 | 29.012 | 2.785 | 145 | 7.07 | 7988 | 91.62 | 2.34 |
| 9/18/2006 | 19:04:17 | 21000 | 68.94 | 29.01 | 2.811 | 207 | 7.05 | 7331 | 84.0858 | 2.08 |
| 9/18/2006 | 19:09:17 | 21300 | 68.99 | 29.01 | 2.785 | 181 | 7.08 | 4996 | 57.3339 | 1.43 |
| 9/18/2006 | 19:14:17 | 21600 | 68.96 | 29.007 | 2.811 | 169 | 7.14 | 7929 | 91.1313 | 575.64 |
| 9/18/2006 | 19:19:17 | 21900 | 68.96 | 29.004 | 2.785 | 165 | 7.14 | 7636 | 87.7806 | 575.07 |
| 9/18/2006 | 19:24:17 | 22200 | 68.96 | 29.001 | 2.785 | 163 | 7.14 | 7219 | 82.9943 | 574.92 |
| 9/18/2006 | 19:29:17 | 22500 | 68.97 | 28.999 | 2.785 | 162 | 7.15 | 6821 | 78.4293 | 574.36 |
| 9/18/2006 | 19:34:17 | 22800 | 68.97 | 28.997 | 2.785 | 161 | 7.15 | 6455 | 74.2347 | 574.08 |
| 9/18/2006 | 19:39:17 | 23100 | 68.98 | 28.994 | 2.785 | 160 | 7.15 | 6110 | 70.2791 | 573.45 |
| 9/18/2006 | 19:44:17 | 23400 | 69.04 | 28.99 | 2.785 | 158 | 7.16 | 5674 | 65.3225 | 584.47 |
| 9/18/2006 | 19:49:17 | 23700 | 68.96 | 28.985 | 2.811 | 157 | 7.15 | 5321 | 61.2034 | 574.43 |
| 9/18/2006 | 19:54:17 | 24000 | 68.96 | 28.981 | 2.811 | 157 | 7.14 | 5007 | 57.6093 | 574.15 |
| 9/18/2006 | 19:59:17 | 24300 | 68.96 | 28.979 | 2.785 | 157 | 7.13 | 4728 | 54.3928 | 573.52 |
| 9/18/2006 | 20:04:17 | 24600 | 68.95 | 28.977 | 2.811 | 156 | 7.14 | 4484 | 51.5942 | 573.24 |
| 9/18/2006 | 20:09:17 | 24900 | 68.95 | 28.974 | 2.785 | 156 | 7.14 | 4260 | 49.0188 | 572.75 |
| 9/18/2006 | 20:14:17 | 25200 | 68.94 | 28.973 | 2.785 | 157 | 7.14 | 4044 | 46.5359 | 572.27 |
| 9/18/2006 | 20:19:17 | 25500 | 68.96 | 28.971 | 2.785 | 157 | 7.15 | 3855 | 44.3611 | 571.64 |
| 9/18/2006 | 20:24:17 | 25800 | 68.95 | 28.97 | 2.785 | 157 | 7.15 | 3691 | 42.4737 | 570.95 |
| 9/18/2006 | 20:29:17 | 26100 | 68.96 | 28.97 | 2.811 | 156 | 7.15 | 3546 | 40.8121 | 570.81 |
| 9/18/2006 | 20:34:17 | 26400 | 68.96 | 28.972 | 2.785 | 157 | 7.14 | 3429 | 39.4678 | 570.88 |
| 9/18/2006 | 20:39:17 | 26700 | 68.96 | 28.971 | 2.785 | 157 | 7.15 | 3325 | 38.2718 | 570.54 |
| 9/18/2006 | 20:44:17 | 27000 | 68.96 | 28.972 | 2.785 | 157 | 7.15 | 3225 | 37.1166 | 570.26 |
| 9/18/2006 | 20:49:17 | 27300 | 68.96 | 28.97 | 2.785 | 157 | 7.16 | 3125 | 35.9686 | 570.33 |
| 9/18/2006 | 20:54:17 | 27600 | 68.96 | 28.967 | 2.785 | 157 | 7.16 | 3041 | 35.0015 | 570.19 |
| 9/18/2006 | 20:59:17 | 27900 | 68.97 | 28.967 | 2.811 | 158 | 7.16 | 2968 | 34.1673 | 570.05 |
| 9/18/2006 | 21:04:17 | 28200 | 68.97 | 28.968 | 2.785 | 159 | 7.16 | 2896 | 33.335 | 569.71 |
| 9/18/2006 | 21:09:17 | 28500 | 68.97 | 28.968 | 2.785 | 158 | 7.16 | 2824 | 32.5095 | 569.43 |
| 9/18/2006 | 21:14:17 | 28800 | 68.97 | 28.966 | 2.811 | 158 | 7.16 | 2744 | 31.5877 | 569.37 |
| 9/18/2006 | 21:19:17 | 29100 | 68.95 | 28.97 | 2.811 | 160 | 7.17 | 2693 | 30.9966 | 569.37 |
| 9/18/2006 | 21:24:17 | 29400 | 68.94 | 28.969 | 2.785 | 161 | 7.17 | 2678 | 30.8171 | 568.75 |
| 9/18/2006 | 21:29:17 | 29700 | 68.94 | 28.969 | 2.785 | 160 | 7.16 | 2718 | 31.2782 | 568.47 |

| Date | Time | ET (sec) | Chan[1] Temperature Fahrenheit | Chan[3] Barometric Inches Hg | Chan[5] Battery Volts | Chan[11] ORP millivolts | Chan[12] pH pH | Chan[25] Clark DO microgram: | Chan[25] Clark DO Sat %Saturation | Chan[45] Conductivity microSiemens/cm Actual Conductivity |
|-----------|----------|----------|--------------------------------------|------------------------------------|-----------------------------|-------------------------------|----------------------|------------------------------------|---|--|
| 9/18/2006 | 21:34:17 | 30000 | 68.93 | 28.971 | 2.785 | 159 | 7.13 | 3473 | 39.8807 | 1.43 |
| 9/18/2006 | 21:39:17 | 30300 | 68.97 | 28.972 | 2.785 | 274 | 7.15 | 7929 | 91.0961 | 1.43 |
| 9/18/2006 | 21:44:17 | 30600 | 68.99 | 28.972 | 2.811 | 309 | 7.16 | 8348 | 95.932 | 1.43 |
| 9/18/2006 | 21:49:17 | 30900 | 69.06 | 28.973 | 2.811 | 329 | 7.16 | 8157 | 93.7912 | 1.43 |
| 9/18/2006 | 21:54:17 | 31200 | 69.09 | 28.974 | 2.811 | 327 | 7.16 | 8152 | 93.7707 | 1.43 |
| 9/18/2006 | 21:59:17 | 31500 | 69.09 | 28.973 | 2.759 | 337 | 7.18 | 7969 | 91.6704 | 1.43 |
| 9/18/2006 | 22:04:17 | 31800 | 69.08 | 28.974 | 2.785 | 351 | 7.17 | 7640 | 87.8731 | 1.43 |
| 9/18/2006 | 22:09:17 | 32100 | 69.04 | 28.973 | 2.785 | 355 | 7.17 | 6739 | 77.4723 | 1.43 |
| 9/18/2006 | 22:14:17 | 32400 | 69.04 | 28.972 | 2.811 | 358 | 7.16 | 5180 | 59.5589 | 1.43 |
| 9/18/2006 | 22:19:17 | 32700 | 69 | 28.972 | 2.811 | 364 | 7.17 | 5718 | 65.7143 | 1.43 |
| 9/18/2006 | 22:24:17 | 33000 | 69.01 | 28.971 | 2.785 | 367 | 7.16 | 5908 | 67.9104 | 1.43 |
| 9/18/2006 | 22:29:17 | 33300 | 69.01 | 28.972 | 2.785 | 369 | 7.15 | 5729 | 65.843 | 1.43 |
| 9/18/2006 | 22:34:17 | 33600 | 69.03 | 28.971 | 2.785 | 363 | 7.15 | 4950 | 56.9071 | 1.43 |
| 9/18/2006 | 22:39:17 | 33900 | 69.05 | 28.968 | 2.785 | 366 | 7.14 | 5390 | 61.9857 | 1.43 |
| 9/18/2006 | 22:44:17 | 34200 | 69.03 | 28.966 | 2.785 | 366 | 7.16 | 5145 | 59.1589 | 1.43 |
| 9/18/2006 | 22:49:17 | 34500 | 69.03 | 28.967 | 2.785 | 370 | 7.18 | 5624 | 64.6713 | 1.43 |
| 9/18/2006 | 22:54:17 | 34800 | 69.04 | 28.969 | 2.785 | 370 | 7.18 | 6522 | 74.9929 | 1.43 |
| 9/18/2006 | 22:59:17 | 35100 | 69.04 | 28.969 | 2.811 | 372 | 7.16 | 6375 | 73.2984 | 1.43 |
| 9/18/2006 | 23:04:17 | 35400 | 69.06 | 28.97 | 2.811 | 374 | 7.22 | 7037 | 80.9303 | 1.43 |
| 9/18/2006 | 23:09:17 | 35700 | 69.07 | 28.97 | 2.785 | 362 | 7.22 | 7147 | 82.2044 | 1.43 |
| 9/18/2006 | 23:14:17 | 36000 | 69.06 | 28.971 | 2.785 | 362 | 7.15 | 7696 | 88.509 | 1.43 |
| 9/18/2006 | 23:19:17 | 36300 | 69.05 | 28.971 | 2.785 | 378 | 7.16 | 7423 | 85.356 | 1.43 |
| 9/18/2006 | 23:24:17 | 36600 | 69.05 | 28.971 | 2.785 | 368 | 7.17 | 7663 | 88.1158 | 1.43 |
| 9/18/2006 | 23:29:17 | 36900 | 69.05 | 28.97 | 2.785 | 385 | 7.14 | 6940 | 79.8037 | 1.43 |
| 9/18/2006 | 23:34:17 | 37200 | 69.03 | 28.968 | 2.811 | 383 | 7.15 | 6247 | 71.8361 | 1.43 |
| 9/18/2006 | 23:39:17 | 37500 | 69.04 | 28.967 | 2.785 | 388 | 7.19 | 6839 | 78.6397 | 1.43 |
| 9/18/2006 | 23:44:17 | 37800 | 69 | 28.967 | 2.811 | 339 | 7.16 | 6554 | 75.3372 | 1.43 |
| 9/18/2006 | 23:49:17 | 38100 | 69.03 | 28.964 | 2.785 | 380 | 7.14 | 6664 | 76.6353 | 1.43 |
| 9/18/2006 | 23:54:17 | 38400 | 69.04 | 28.962 | 2.785 | 371 | 7.19 | 6135 | 70.5584 | 1.43 |
| 9/18/2006 | 23:59:17 | 38700 | 69.03 | 28.962 | 2.811 | 384 | 7.2 | 5925 | 68.1373 | 1.43 |
| 9/19/2006 | 0:04:17 | 39000 | 68.96 | 28.963 | 2.811 | 250 | 7.1 | 7556 | 86.8217 | 1.43 |
| 9/19/2006 | 0:09:17 | 39300 | 68.97 | 28.964 | 2.785 | 250 | 7.12 | 6760 | 77.6878 | 1.43 |
| 9/19/2006 | 0:14:17 | 39600 | 68.99 | 28.964 | 2.785 | 322 | 7.11 | 8493 | 97.6208 | 1.43 |
| 9/19/2006 | 0:19:17 | 39900 | 69.01 | 28.965 | 2.811 | 341 | 7.12 | 8512 | 97.8543 | 1.43 |
| 9/19/2006 | 0:24:17 | 40200 | 68.95 | 28.966 | 2.785 | 354 | 7.12 | 8601 | 98.8044 | 2.09 |
| 9/19/2006 | 0:29:17 | 40500 | 68.95 | 28.966 | 2.785 | 346 | 7.09 | 8624 | 99.0741 | 1.43 |
| 9/19/2006 | 0:34:17 | 40800 | 68.95 | 28.966 | 2.785 | 259 | 7.12 | 8647 | 99.347 | 1.43 |
| 9/19/2006 | 0:39:17 | 41100 | 68.95 | 28.963 | 2.811 | 192 | 7.11 | 8685 | 99.7811 | 1.43 |

| Date | Time | ET (sec) | Chan[1] Temperature Fahrenheit | Chan[3] Barometric Inches Hg | Chan[5] Battery Volts | Chan[11] ORP millivolts | Chan[12] pH pH | Chan[25] Clark DO microgram: | Chan[25] Clark DO Sat %Saturation | Chan[45] Conductivity microSiemens/cm Actual Conductivity |
|-----------|---------|----------|--------------------------------------|------------------------------------|-----------------------------|-------------------------------|----------------------|------------------------------------|---|--|
| 9/19/2006 | 0:44:17 | 41400 | 68.94 | 28.959 | 2.785 | 168 | 7.12 | 8646 | 99.342 | 1.43 |
| 9/19/2006 | 0:49:17 | 41700 | 68.95 | 28.956 | 2.785 | 162 | 7.1 | 7779 | 89.3989 | 1.43 |
| 9/19/2006 | 0:54:17 | 42000 | 68.95 | 28.954 | 2.785 | 158 | 7.09 | 6456 | 74.2044 | 1.43 |
| 9/19/2006 | 0:59:17 | 42300 | 68.95 | 28.953 | 2.785 | 157 | 7.12 | 5754 | 66.1426 | 1.43 |
| 9/19/2006 | 1:04:17 | 42600 | 68.95 | 28.951 | 2.759 | 156 | 7.13 | 5586 | 64.2149 | 1.43 |
| 9/19/2006 | 1:09:17 | 42900 | 68.95 | 28.948 | 2.785 | 158 | 7.13 | 8705 | 100.066 | 1.43 |
| 9/19/2006 | 1:14:17 | 43200 | 68.94 | 28.944 | 2.759 | 209 | 7.06 | 6041 | 69.4507 | 1.43 |
| 9/19/2006 | 1:19:17 | 43500 | 69 | 28.941 | 2.785 | 267 | 7.09 | 5658 | 65.0979 | 1.43 |
| 9/19/2006 | 1:24:17 | 43800 | 68.99 | 28.939 | 2.759 | 296 | 7.04 | 5296 | 60.9293 | 1.43 |
| 9/19/2006 | 1:29:17 | 44100 | 69.01 | 28.939 | 2.785 | 321 | 7.11 | 5240 | 60.3021 | 1.43 |
| 9/19/2006 | 1:34:17 | 44400 | 69 | 28.937 | 2.785 | 335 | 7.15 | 5585 | 64.2725 | 1.43 |
| 9/19/2006 | 1:39:17 | 44700 | 69.01 | 28.935 | 2.785 | 344 | 7.14 | 5920 | 68.1348 | 1.43 |
| 9/19/2006 | 1:44:17 | 45000 | 69 | 28.934 | 2.785 | 355 | 7.13 | 5425 | 62.4378 | 1.43 |
| 9/19/2006 | 1:49:17 | 45300 | 69 | 28.935 | 2.759 | 358 | 7.15 | 7434 | 85.5466 | 1.43 |
| 9/19/2006 | 1:54:17 | 45600 | 69.02 | 28.936 | 2.759 | 361 | 7.17 | 6754 | 77.74 | 1.43 |
| 9/19/2006 | 1:59:17 | 45900 | 69.01 | 28.933 | 2.811 | 369 | 7.1 | 5985 | 68.8814 | 1.43 |
| 9/19/2006 | 2:04:17 | 46200 | 68.98 | 28.932 | 2.785 | 371 | 7.14 | 5605 | 64.4943 | 1.43 |
| 9/19/2006 | 2:09:17 | 46500 | 68.94 | 28.933 | 2.759 | 372 | 7.15 | 5621 | 64.6442 | 1.43 |
| 9/19/2006 | 2:14:17 | 46800 | 68.94 | 28.933 | 2.759 | 379 | 7.15 | 8378 | 96.3562 | 1.43 |
| 9/19/2006 | 2:19:17 | 47100 | 68.95 | 28.934 | 2.811 | 385 | 7.16 | 8767 | 100.8385 | 1.43 |
| 9/19/2006 | 2:24:17 | 47400 | 68.94 | 28.935 | 2.759 | 385 | 7.15 | 8815 | 101.3685 | 1.72 |
| 9/19/2006 | 2:29:17 | 47700 | 68.96 | 28.934 | 2.785 | 286 | 7.15 | 8788 | 101.0944 | 1.43 |
| 9/19/2006 | 2:34:17 | 48000 | 68.97 | 28.933 | 2.811 | 297 | 7.13 | 8759 | 100.7635 | 1.43 |
| 9/19/2006 | 2:39:17 | 48300 | 68.96 | 28.932 | 2.785 | 261 | 7.14 | 5512 | 63.4124 | 1.43 |
| 9/19/2006 | 2:44:17 | 48600 | 68.94 | 28.93 | 2.785 | 239 | 7.11 | 8793 | 101.1454 | 1.43 |
| 9/19/2006 | 2:49:17 | 48900 | 68.96 | 28.929 | 2.811 | 259 | 7.11 | 8784 | 101.0647 | 1.43 |
| 9/19/2006 | 2:54:17 | 49200 | 68.95 | 28.928 | 2.811 | 226 | 7.1 | 8793 | 101.1515 | 1.43 |
| 9/19/2006 | 2:59:17 | 49500 | 68.95 | 28.926 | 2.759 | 215 | 7.12 | 8760 | 100.7851 | 1.43 |
| 9/19/2006 | 3:04:17 | 49800 | 68.96 | 28.923 | 2.785 | 192 | 7.11 | 8777 | 101.001 | 1.43 |
| 9/19/2006 | 3:09:17 | 50100 | 68.96 | 28.921 | 2.785 | 196 | 7.12 | 5425 | 62.4298 | 1.43 |
| 9/19/2006 | 3:14:17 | 50400 | 68.98 | 28.92 | 2.785 | 283 | 7.09 | 8820 | 101.5241 | 1.43 |
| 9/19/2006 | 3:19:17 | 50700 | 68.99 | 28.919 | 2.785 | 311 | 7.12 | 8820 | 101.5529 | 1.43 |
| 9/19/2006 | 3:24:17 | 51000 | 69 | 28.916 | 2.785 | 329 | 7.11 | 8837 | 101.7685 | 1.43 |
| 9/19/2006 | 3:29:17 | 51300 | 69 | 28.914 | 2.785 | 337 | 7.11 | 8871 | 102.154 | 1.43 |
| 9/19/2006 | 3:34:17 | 51600 | 69 | 28.913 | 2.759 | 346 | 7.11 | 8884 | 102.3035 | 1.43 |
| 9/19/2006 | 3:39:17 | 51900 | 69 | 28.911 | 2.785 | 354 | 7.13 | 8868 | 102.125 | 1.43 |
| 9/19/2006 | 3:44:17 | 52200 | 69 | 28.91 | 2.785 | 360 | 7.12 | 8866 | 102.1197 | 1.43 |
| 9/19/2006 | 3:49:17 | 52500 | 68.99 | 28.908 | 2.811 | 367 | 7.12 | 8872 | 102.1883 | 1.43 |

| Date | Time | ET (sec) | Chan[1] Temperature Fahrenheit | Chan[3] Barometric Inches Hg | Chan[5] Battery Volts | Chan[11] ORP millivolts | Chan[12] pH pH | Chan[25] Clark DO microgram: | Chan[25] Clark DO Sat %Saturation | Chan[45] Conductivity microSiemens/cm Actual Conductivity |
|-----------|---------|----------|--------------------------------------|------------------------------------|-----------------------------|-------------------------------|----------------------|------------------------------------|---|--|
| 9/19/2006 | 3:54:17 | 52800 | 69 | 28.907 | 2.785 | 367 | 7.12 | 8869 | 102.1721 | 1.43 |
| 9/19/2006 | 3:59:17 | 53100 | 69 | 28.905 | 2.785 | 374 | 7.12 | 8885 | 102.3624 | 1.43 |
| 9/19/2006 | 4:04:17 | 53400 | 68.99 | 28.904 | 2.785 | 372 | 7.12 | 8852 | 101.972 | 1.43 |
| 9/19/2006 | 4:09:17 | 53700 | 68.99 | 28.904 | 2.811 | 373 | 7.12 | 8821 | 101.6121 | 1.43 |
| 9/19/2006 | 4:14:17 | 54000 | 68.99 | 28.903 | 2.785 | 376 | 7.13 | 8780 | 101.1459 | 1.43 |
| 9/19/2006 | 4:19:17 | 54300 | 69 | 28.901 | 2.785 | 378 | 7.11 | 8819 | 101.6028 | 1.43 |
| 9/19/2006 | 4:24:17 | 54600 | 68.99 | 28.9 | 2.759 | 382 | 7.12 | 8773 | 101.0725 | 1.43 |
| 9/19/2006 | 4:29:17 | 54900 | 69 | 28.899 | 2.759 | 381 | 7.12 | 8772 | 101.0653 | 1.43 |
| 9/19/2006 | 4:34:17 | 55200 | 69 | 28.896 | 2.785 | 383 | 7.13 | 8692 | 100.1523 | 1.43 |
| 9/19/2006 | 4:39:17 | 55500 | 68.99 | 28.895 | 2.811 | 383 | 7.12 | 8721 | 100.4894 | 1.43 |
| 9/19/2006 | 4:44:17 | 55800 | 68.98 | 28.892 | 2.785 | 384 | 7.11 | 8728 | 100.5643 | 1.43 |
| 9/19/2006 | 4:49:17 | 56100 | 68.99 | 28.89 | 2.785 | 388 | 7.14 | 8809 | 101.518 | 1.43 |
| 9/19/2006 | 4:54:17 | 56400 | 69 | 28.886 | 2.785 | 383 | 7.11 | 8937 | 103.0294 | 1.43 |
| 9/19/2006 | 4:59:17 | 56700 | 68.99 | 28.883 | 2.785 | 395 | 7.1 | 8989 | 103.625 | 1.43 |
| 9/19/2006 | 5:04:17 | 57000 | 69.01 | 28.878 | 2.785 | 381 | 7.12 | 8984 | 103.6059 | 1.43 |
| 9/19/2006 | 5:09:17 | 57300 | 69 | 28.876 | 2.785 | 384 | 7.16 | 9007 | 103.8605 | 1.43 |
| 9/19/2006 | 5:14:17 | 57600 | 68.99 | 28.876 | 2.811 | 402 | 7.16 | 9021 | 104.0147 | 1.43 |
| 9/19/2006 | 5:19:17 | 57900 | 68.99 | 28.875 | 2.785 | 401 | 7.17 | 9029 | 104.113 | 1.43 |
| 9/19/2006 | 5:24:17 | 58200 | 68.99 | 28.873 | 2.811 | 393 | 7.19 | 9053 | 104.3982 | 1.43 |
| 9/19/2006 | 5:29:17 | 58500 | 68.98 | 28.873 | 2.785 | 399 | 7.19 | 9059 | 104.4557 | 1.43 |
| 9/19/2006 | 5:34:17 | 58800 | 68.99 | 28.871 | 2.811 | 419 | 7.18 | 9068 | 104.5824 | 1.43 |
| 9/19/2006 | 5:39:17 | 59100 | 68.99 | 28.864 | 2.785 | 393 | 7.12 | 9069 | 104.6133 | 1.43 |
| 9/19/2006 | 5:44:17 | 59400 | 68.99 | 28.861 | 2.785 | 386 | 7.14 | 9086 | 104.819 | 1.43 |
| 9/19/2006 | 5:49:17 | 59700 | 68.99 | 28.858 | 2.785 | 399 | 7.14 | 9069 | 104.6384 | 1.43 |
| 9/19/2006 | 5:54:17 | 60000 | 68.99 | 28.856 | 2.785 | 390 | 7.12 | 9074 | 104.6998 | 1.43 |
| 9/19/2006 | 5:59:17 | 60300 | 68.98 | 28.853 | 2.759 | 401 | 7.13 | 9085 | 104.8246 | 1.43 |
| 9/19/2006 | 6:04:17 | 60600 | 68.99 | 28.849 | 2.785 | 402 | 7.19 | 9101 | 105.0394 | 1.43 |
| 9/19/2006 | 6:09:17 | 60900 | 68.97 | 28.848 | 2.785 | 402 | 7.18 | 9094 | 104.9429 | 1.43 |
| 9/19/2006 | 6:14:17 | 61200 | 68.99 | 28.845 | 2.785 | 402 | 7.18 | 9086 | 104.878 | 1.43 |
| 9/19/2006 | 6:19:17 | 61500 | 68.96 | 28.842 | 2.785 | 403 | 7.19 | 9092 | 104.9331 | 1.43 |
| 9/19/2006 | 6:24:17 | 61800 | 68.97 | 28.84 | 2.759 | 407 | 7.19 | 9098 | 105.0172 | 1.43 |
| 9/19/2006 | 6:29:17 | 62100 | 68.96 | 28.837 | 2.785 | 407 | 7.19 | 9101 | 105.0507 | 1.43 |
| 9/19/2006 | 6:34:17 | 62400 | 68.98 | 28.833 | 2.785 | 409 | 7.18 | 9093 | 104.9895 | 1.43 |
| 9/19/2006 | 6:39:17 | 62700 | 68.97 | 28.832 | 2.759 | 413 | 7.2 | 9118 | 105.2763 | 1.43 |
| 9/19/2006 | 6:44:17 | 63000 | 68.99 | 28.827 | 2.785 | 416 | 7.19 | 9104 | 105.1644 | 1.43 |
| 9/19/2006 | 6:49:17 | 63300 | 68.98 | 28.824 | 2.785 | 416 | 7.19 | 9112 | 105.2465 | 1.43 |
| 9/19/2006 | 6:54:17 | 63600 | 68.99 | 28.82 | 2.785 | 418 | 7.2 | 9118 | 105.3376 | 1.43 |
| 9/19/2006 | 6:59:17 | 63900 | 68.94 | 28.819 | 2.785 | 422 | 7.2 | 9126 | 105.3861 | 1.43 |

| Date | Time | ET (sec) | Chan[1] Temperature Fahrenheit | Chan[3] Barometric Inches Hg | Chan[5] Battery Volts | Chan[11] ORP millivolts | Chan[12] pH pH | Chan[25] Clark DO microgram: | Chan[25] Clark DO Sat %Saturation | Chan[45] Conductivity microSiemens/cm Actual Conductivity |
|-----------|----------|----------|--------------------------------------|------------------------------------|-----------------------------|-------------------------------|----------------------|------------------------------------|---|--|
| 9/19/2006 | 7:04:17 | 64200 | 68.93 | 28.815 | 2.785 | 422 | 7.2 | 9121 | 105.3262 | 1.43 |
| 9/19/2006 | 7:09:17 | 64500 | 68.96 | 28.814 | 2.785 | 422 | 7.21 | 9091 | 105.0115 | 1.43 |
| 9/19/2006 | 7:14:17 | 64800 | 68.97 | 28.813 | 2.785 | 423 | 7.21 | 9087 | 104.988 | 1.43 |
| 9/19/2006 | 7:19:17 | 65100 | 68.97 | 28.81 | 2.811 | 420 | 7.19 | 9115 | 105.3261 | 1.43 |
| 9/19/2006 | 7:24:17 | 65400 | 68.97 | 28.807 | 2.759 | 419 | 7.2 | 9115 | 105.336 | 1.43 |
| 9/19/2006 | 7:29:17 | 65700 | 68.97 | 28.803 | 2.785 | 420 | 7.2 | 9123 | 105.4385 | 1.43 |
| 9/19/2006 | 7:34:17 | 66000 | 68.97 | 28.799 | 2.785 | 423 | 7.19 | 9126 | 105.4903 | 1.43 |
| 9/19/2006 | 7:39:17 | 66300 | 68.97 | 28.795 | 2.759 | 427 | 7.23 | 9130 | 105.5569 | 1.43 |
| 9/19/2006 | 7:44:17 | 66600 | 68.99 | 28.791 | 2.785 | 429 | 7.25 | 9132 | 105.6184 | 1.43 |
| 9/19/2006 | 7:49:17 | 66900 | 68.99 | 28.788 | 2.785 | 431 | 7.25 | 9128 | 105.5842 | 1.43 |
| 9/19/2006 | 7:54:17 | 67200 | 69.02 | 28.786 | 2.759 | 433 | 7.26 | 9113 | 105.4498 | 1.43 |
| 9/19/2006 | 7:59:17 | 67500 | 69.03 | 28.784 | 2.811 | 432 | 7.21 | 9134 | 105.7129 | 1.43 |
| 9/19/2006 | 8:04:17 | 67800 | 69.03 | 28.78 | 2.759 | 432 | 7.2 | 9103 | 105.3629 | 1.43 |
| 9/19/2006 | 8:09:17 | 68100 | 69.03 | 28.778 | 2.759 | 441 | 7.2 | 9115 | 105.509 | 1.43 |
| 9/19/2006 | 8:14:17 | 68400 | 69.02 | 28.774 | 2.785 | 432 | 7.2 | 9113 | 105.4886 | 1.43 |
| 9/19/2006 | 8:19:17 | 68700 | 69.03 | 28.772 | 2.759 | 422 | 7.21 | 9111 | 105.4879 | 1.43 |
| 9/19/2006 | 8:24:17 | 69000 | 69.04 | 28.772 | 2.759 | 374 | 7.19 | 9140 | 105.8342 | 1.43 |
| 9/19/2006 | 8:29:17 | 69300 | 69.02 | 28.773 | 2.759 | 435 | 7.12 | 9125 | 105.6345 | 1.43 |
| 9/19/2006 | 8:34:17 | 69600 | 69.03 | 28.774 | 2.785 | 435 | 7.18 | 9122 | 105.6114 | 1.43 |
| 9/19/2006 | 8:39:17 | 69900 | 69.02 | 28.781 | 2.759 | 392 | 7.18 | 9126 | 105.6144 | 1.43 |
| 9/19/2006 | 8:44:17 | 70200 | 69.01 | 28.786 | 2.759 | 429 | 7.16 | 9120 | 105.5148 | 1.43 |
| 9/19/2006 | 8:49:17 | 70500 | 69 | 28.79 | 2.785 | 428 | 7.17 | 9143 | 105.7543 | 1.43 |
| 9/19/2006 | 8:54:17 | 70800 | 69.02 | 28.794 | 2.811 | 424 | 7.17 | 9138 | 105.6999 | 1.43 |
| 9/19/2006 | 8:59:17 | 71100 | 69.03 | 28.807 | 2.759 | 418 | 7.15 | 9161 | 105.9428 | 1.43 |
| 9/19/2006 | 9:04:17 | 71400 | 68.94 | 28.828 | 2.785 | 417 | 7.18 | 9160 | 105.7404 | 1.43 |
| 9/19/2006 | 9:09:17 | 71700 | 68.96 | 28.829 | 2.759 | 415 | 7.18 | 9133 | 105.4492 | 1.43 |
| 9/19/2006 | 9:14:17 | 72000 | 68.98 | 28.831 | 2.759 | 424 | 7.19 | 9148 | 105.6388 | 1.43 |
| 9/19/2006 | 9:19:17 | 72300 | 69 | 28.838 | 2.811 | 414 | 7.18 | 9155 | 105.7131 | 1.43 |
| 9/19/2006 | 9:24:17 | 72600 | 69 | 28.842 | 2.811 | 413 | 7.18 | 9103 | 105.0923 | 1.43 |
| 9/19/2006 | 9:29:17 | 72900 | 69 | 28.838 | 2.759 | 401 | 7.23 | 8995 | 103.8628 | 1.43 |
| 9/19/2006 | 9:34:17 | 73200 | 68.99 | 28.845 | 2.785 | 401 | 7.2 | 9112 | 105.1881 | 1.43 |
| 9/19/2006 | 9:39:17 | 73500 | 69.01 | 28.844 | 2.811 | 403 | 7.18 | 9136 | 105.4841 | 1.43 |
| 9/19/2006 | 9:44:17 | 73800 | 69.01 | 28.849 | 2.785 | 405 | 7.18 | 9167 | 105.8273 | 1.43 |
| 9/19/2006 | 9:49:17 | 74100 | 69.01 | 28.852 | 2.759 | 403 | 7.19 | 8936 | 103.1455 | 1.43 |
| 9/19/2006 | 9:54:17 | 74400 | 69.02 | 28.848 | 2.785 | 406 | 7.18 | 8978 | 103.6507 | 1.43 |
| 9/19/2006 | 9:59:17 | 74700 | 69.01 | 28.846 | 2.759 | 406 | 7.19 | 8968 | 103.536 | 1.43 |
| 9/19/2006 | 10:04:17 | 75000 | 69.02 | 28.847 | 2.785 | 416 | 7.19 | 9162 | 105.7789 | 1.43 |
| 9/19/2006 | 10:09:17 | 75300 | 68.92 | 28.837 | 2.785 | 408 | 7.17 | 6898 | 79.5896 | 1.43 |

| Date | Time | ET (sec) | Chan[1] Temperature Fahrenheit | Chan[3] Barometric Inches Hg | Chan[5] Battery Volts | Chan[11] ORP millivolts | Chan[12] pH pH | Chan[25] Clark DO microgram: | Chan[25] Clark DO Sat %Saturation | Chan[45] Conductivity microSiemens/cm Actual Conductivity |
|-----------|----------|----------|--------------------------------------|------------------------------------|-----------------------------|-------------------------------|----------------------|------------------------------------|---|--|
| 9/19/2006 | 10:14:17 | 75600 | 68.93 | 28.833 | 2.759 | 406 | 7.13 | 8882 | 102.5004 | 1.43 |
| 9/19/2006 | 10:19:17 | 75900 | 68.94 | 28.848 | 2.759 | 408 | 7.12 | 9076 | 104.6932 | 1.43 |
| 9/19/2006 | 10:24:17 | 76200 | 68.93 | 28.859 | 2.759 | 412 | 7.15 | 9081 | 104.709 | 1.43 |
| 9/19/2006 | 10:29:17 | 76500 | 68.93 | 28.848 | 2.759 | 411 | 7.1 | 9155 | 105.5924 | 1.43 |
| 9/19/2006 | 10:34:17 | 76800 | 68.93 | 28.871 | 2.759 | 397 | 7.13 | 9071 | 104.5384 | 1.43 |
| 9/19/2006 | 10:39:17 | 77100 | 68.94 | 28.891 | 2.785 | 404 | 7.18 | 9068 | 104.4358 | 1.43 |
| 9/19/2006 | 10:44:17 | 77400 | 68.94 | 28.905 | 2.785 | 391 | 7.18 | 9091 | 104.6577 | 1.43 |
| 9/19/2006 | 10:49:17 | 77700 | 68.94 | 28.926 | 2.785 | 407 | 7.19 | 9124 | 104.9553 | 1.43 |
| 9/19/2006 | 10:54:17 | 78000 | 68.94 | 28.941 | 2.785 | 405 | 7.18 | 9124 | 104.9013 | 1.43 |
| 9/19/2006 | 10:59:17 | 78300 | 68.92 | 28.958 | 2.759 | 406 | 7.15 | 9151 | 105.1391 | 1.43 |
| 9/19/2006 | 11:04:17 | 78600 | 68.94 | 28.95 | 2.785 | 400 | 7.13 | 9138 | 105.0395 | 1.43 |
| 9/19/2006 | 11:09:17 | 78900 | 68.93 | 28.961 | 2.785 | 417 | 7.1 | 9079 | 104.2956 | 1.43 |
| 9/19/2006 | 11:14:17 | 79200 | 68.92 | 28.965 | 2.785 | 414 | 7.12 | 9024 | 103.6454 | 1.43 |
| 9/19/2006 | 11:19:17 | 79500 | 68.96 | 28.961 | 2.785 | 421 | 7.04 | 8985 | 103.2571 | 1.43 |
| 9/19/2006 | 11:24:17 | 79800 | 68.97 | 28.969 | 2.785 | 425 | 7.06 | 9078 | 104.3082 | 1.43 |
| 9/19/2006 | 11:29:17 | 80100 | 68.96 | 28.975 | 2.759 | 431 | 7.06 | 9033 | 103.7583 | 1.43 |
| 9/19/2006 | 11:34:17 | 80400 | 68.96 | 28.983 | 2.785 | 433 | 7.05 | 8876 | 101.9285 | 1.43 |
| 9/19/2006 | 11:39:17 | 80700 | 68.97 | 28.982 | 2.759 | 433 | 7.06 | 9026 | 103.6673 | 1.43 |
| 9/19/2006 | 11:44:17 | 81000 | 68.96 | 28.99 | 2.759 | 430 | 7.04 | 9026 | 103.6196 | 1.43 |
| 9/19/2006 | 11:49:17 | 81300 | 68.97 | 29.001 | 2.785 | 441 | 7.09 | 8919 | 102.361 | 1.43 |
| 9/19/2006 | 11:54:17 | 81600 | 68.97 | 29.002 | 2.811 | 432 | 7.06 | 9024 | 103.5569 | 1.43 |
| 9/19/2006 | 11:59:17 | 81900 | 68.96 | 28.998 | 2.785 | 421 | 7.09 | 8956 | 102.793 | 1.43 |
| 9/19/2006 | 12:04:17 | 82200 | 68.97 | 28.999 | 2.759 | 418 | 7.1 | 8747 | 100.3961 | 1.43 |
| 9/19/2006 | 12:09:17 | 82500 | 68.97 | 29.002 | 2.759 | 415 | 7.12 | 8702 | 99.8663 | 1.43 |
| 9/19/2006 | 12:14:17 | 82800 | 68.97 | 29.001 | 2.785 | 423 | 7.12 | 9006 | 103.3665 | 1.43 |
| 9/19/2006 | 12:19:17 | 83100 | 68.97 | 29.002 | 2.785 | 413 | 7.08 | 9026 | 103.5884 | 1.43 |
| 9/19/2006 | 12:24:17 | 83400 | 68.97 | 29.006 | 2.785 | 419 | 7.1 | 8968 | 102.8982 | 1.43 |
| 9/19/2006 | 12:29:17 | 83700 | 68.97 | 29.005 | 2.785 | 418 | 7.1 | 8987 | 103.125 | 1.43 |
| 9/19/2006 | 12:34:17 | 84000 | 68.96 | 29.011 | 2.759 | 419 | 7.09 | 9016 | 103.4355 | 1.43 |
| 9/19/2006 | 12:39:17 | 84300 | 68.96 | 29.338 | 2.785 | 424 | 7.1 | 8996 | 102.029 | 1.43 |
| 9/19/2006 | 12:44:17 | 84600 | 68.9 | 29.338 | 2.759 | 430 | 4.98 | 9013 | 102.1482 | 1.43 |
| 9/19/2006 | 12:49:17 | 84900 | 68.9 | 29.337 | 2.811 | 452 | 5.15 | 9037 | 102.4242 | 1.43 |
| 9/19/2006 | 12:54:17 | 85200 | 68.95 | 29.335 | 2.785 | 413 | 6.99 | 9011 | 102.1956 | 1.43 |
| 9/19/2006 | 12:59:17 | 85500 | 68.93 | 29.334 | 2.785 | 507 | 6.88 | 8928 | 101.2374 | 1.43 |
| 9/19/2006 | 13:04:17 | 85800 | 68.9 | 29.332 | 2.811 | 497 | 5.81 | 9013 | 102.1677 | 1.43 |
| 9/19/2006 | 13:09:17 | 86100 | 68.9 | 29.329 | 2.785 | 510 | 7.37 | 8898 | 100.8721 | 1.43 |
| 9/19/2006 | 13:14:17 | 86400 | 68.91 | 29.33 | 2.811 | 515 | 7.34 | 8922 | 101.1588 | 1.43 |
| 9/19/2006 | 13:19:17 | 86700 | 68.95 | 29.326 | 2.811 | 571 | 7.19 | 8964 | 101.6912 | 1.43 |

| Date | Time | ET (sec) | Chan[1] Temperature Fahrenheit | Chan[3] Barometric Inches Hg | Chan[5] Battery Volts | Chan[11] ORP millivolts | Chan[12] pH pH | Chan[25] Clark DO microgram: | Chan[25] Clark DO Sat %Saturation | Chan[45] Conductivity microSiemens/cm Actual Conductivity |
|-----------|----------|----------|--------------------------------------|------------------------------------|-----------------------------|-------------------------------|----------------------|------------------------------------|---|--|
| 9/19/2006 | 13:24:17 | 87000 | 68.92 | 29.324 | 2.785 | 525 | 7.41 | 8920 | 101.163 | 1.43 |
| 9/19/2006 | 13:29:17 | 87300 | 68.91 | 29.323 | 2.785 | 529 | 7.14 | 8935 | 101.3224 | 1.43 |
| 9/19/2006 | 13:34:17 | 87600 | 68.9 | 29.321 | 2.811 | 533 | 6.96 | 8965 | 101.6678 | 1.43 |
| 9/19/2006 | 13:39:17 | 87900 | 68.91 | 29.321 | 2.811 | 536 | 6.67 | 9000 | 102.0662 | 1.43 |
| 9/19/2006 | 13:44:17 | 88200 | 68.92 | 29.318 | 2.785 | 549 | 6.97 | 8944 | 101.4587 | 1.43 |
| 9/19/2006 | 13:49:17 | 88500 | 68.91 | 29.32 | 2.811 | 541 | 6.83 | 8926 | 101.2432 | 1.43 |
| 9/19/2006 | 13:54:17 | 88800 | 68.92 | 29.319 | 2.785 | 551 | 6.87 | 8852 | 100.4079 | 1.43 |
| 9/19/2006 | 13:59:17 | 89100 | 68.93 | 29.319 | 2.811 | 547 | 7.04 | 8866 | 100.5768 | 1.43 |
| 9/19/2006 | 14:04:17 | 89400 | 68.92 | 29.318 | 2.811 | 529 | 7.41 | 8872 | 100.6387 | 1.43 |
| 9/19/2006 | 14:09:17 | 89700 | 68.91 | 29.318 | 2.785 | 521 | 7.34 | 8912 | 101.0764 | 1.43 |

ASSOCIATED BLN COL APPLICATION REVISIONS ATTACHMENTS

**Bellefonte Nuclear Plant, Units 3 & 4
COL Application
Part 2, FSAR**

TABLE 2.4.12-206 (Sheet 1 of 2)
MONTHLY GROUNDWATER HYDRAULIC GRADIENT AND FLOW VELOCITY

BLN COL 2.4-5

Groundwater Velocity and Travel Time from BLN Unit 3 to Town Creek Embayment

| Date | 07/11/06 | 08/31/06 | 09/21/06 | 10/26/06 | 11/13/06 | 12/11/06 | 01/04/07 | 02/01/07 | 03/05/07 | 04/17/07 | 05/08/07 |
|---|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|
| Elevation High (E_H) (ft) | 598.08 | 600.07 | 599.97 | 601.38 | 601.69 | 599.23 | 602.31 | 602.14 | 602.09 | 601.94 | 600.84 |
| Elevation Low (E_L) (ft) | 595.18 | 594.65 | 593.94 | 594.51 | 594.68 | 593.98 | 594.94 | 594.11 | 594.06 | 594.57 | 594.81 |
| Hydraulic Gradient (E_H-E_L)/L | 1.81x10 ⁻³ | 3.39x10 ⁻³ | 3.77x10 ⁻³ | 4.29x10 ⁻³ | 4.38x10 ⁻³ | 3.28x10 ⁻³ | 4.61x10 ⁻³ | 5.02x10 ⁻³ | 5.02x10 ⁻³ | 4.61x10 ⁻³ | 3.77x10 ⁻³ |
| Velocity (V) (ft/day) | 1.20 | 2.24 | 2.49 | 2.84 | 2.90 | 2.17 | 3.05 | 3.32 | 3.32 | 3.05 | 2.49 |
| Travel Time (T) (years) | 3.65 | 1.96 | 1.76 | 1.54 | 1.51 | 2.02 | 1.44 | 1.32 | 1.32 | 1.44 | 1.76 |

Assumptions:

Hydraulic gradient is between MW-1217b (E_H) and SW-4 Town Creek embayment surface (E_L).

Pathway distance (L) = 1600 ft.

Hydraulic conductivity (K_h) = 4.2x10⁻³ cm/s

porosity (η) = 0.018

Equation for velocity: $V = (K_h \times [E_H - E_L]/L)/\eta$ (Darcy equation for average linear velocity).

Equations for travel time: $T = L/V$.

Conversions: 1 day = 86,400 sec.; 1 ft. = 30.48 cm; 1 year = 365.25 days

**Bellefonte Nuclear Plant, Units 3 & 4
COL Application
Part 2, FSAR**

TABLE 2.4.12-206 (Sheet 2 of 2)
MONTHLY GROUNDWATER HYDRAULIC GRADIENT AND FLOW VELOCITY

BLN COL 2.4-5

Groundwater Velocity and Travel Time from BLN Unit 4 to the Intake Structure Channel

| Date | 07/11/06 | 08/31/06 | 09/21/06 | 10/26/06 | 11/13/06 | 12/11/06 | 01/04/07 | 02/01/07 | 03/05/07 | 04/17/07 | 05/08/07 |
|---|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|
| Elevation High (E_H) (ft) | 608.10 | 608.57 | 608.05 | 610.58 | 610.48 | 607.99 | 612.15 | 609.99 | 610.25 | 610.40 | 608.28 |
| Elevation Low (E_L) (ft) | 595.07 | 593.69 | 593.97 | 594.37 | 594.58 | 594.17 | 594.70 | 594.09 | 593.95 | 594.55 | 594.66 |
| Hydraulic Gradient (E_H-E_L)/L | 5.01x10 ⁻³ | 5.72x10 ⁻³ | 5.42x10 ⁻³ | 6.23x10 ⁻³ | 6.12x10 ⁻³ | 5.32x10 ⁻³ | 6.71x10 ⁻³ | 6.12x10 ⁻³ | 6.27x10 ⁻³ | 6.10x10 ⁻³ | 5.24x10 ⁻³ |
| Velocity (V) (ft/day) | 3.31 | 3.79 | 3.58 | 4.12 | 4.04 | 3.52 | 4.44 | 4.04 | 4.15 | 4.03 | 3.46 |
| Travel Time (T) (years) | 2.15 | 1.88 | 1.99 | 1.73 | 1.76 | 2.02 | 1.60 | 1.76 | 1.72 | 1.77 | 2.05 |

Assumptions:

Hydraulic gradient is between MW-1204c (E_H) and SW-2 Intake Structure surface (E_L).

Pathway distance (L) = 2600 ft.

Hydraulic conductivity (K_h) = 4.2x10⁻³ cm/s

porosity (η) = 0.018

Equation for velocity: $V = (K_h \times [E_H - E_L]/L)/\eta$ (Darcy equation for average linear velocity).

Equations for travel time: $T = L/V$.

Conversions: 1 day = 86,400 sec.; 1 ft. = 30.48 cm; 1 year = 365.25 days