TABLE 5.1
TESTING SUMMARY - OBSERVATION WELLS
EXELON TEXAS COL (Victoria) PROJECT
MACTEC PROJECT NO: 6468-07-1777
POWER BLOCK

Well Number	Drilling Method	Well Depth (ft)	Screen Interval (ft bgs)	Coordinates				Well Diameter (I.D. in.)	Testing		
				Northing	Easting	TOC Elevation	Pad Elevation		Slug Testing	24-hour Pump Testing	Sampling for Chemistry
OW-2150L	mud rotary	151.15	140 - 150	13412552.91	2599585.12	82.45	80.87	2	✓		
OW-2150U	mud rotary	66.15	55 - 65	13412568.08	2599582.77	82.78	80.91	2	✓		
OW-2169L	mud rotary	101	90 - 100	13412356.74	2599930.20	81.72	80.04	2	✓		✓
OW-2169U	mud rotary	66	55 -65	13412343.77	2599945.85	81.77	80.11	2	✓		✓
OW-2181L	mud rotary	101	90 - 100	13412138.42	2600071.96	81.32	79.88	2	✓		
OW-2181U	mud rotary	51	40 - 50	13412147.38	2600052.86	81.31	80.01	2	✓		
OW-2185L	mud rotary	101	90 - 100	13412314.47	2600815.69	81.36	79.76	2	✓		
OW-2185U	mud rotary	76	65 - 75	13412328.07	2600801.11	81.45	79.89	2	✓		
OW-2253L	mud rotary	146	135 - 145	13413591.55	2600474.37	82.66	81.17	2	✓		
OW-2253U	mud rotary	66	55 -65	13413584.76	2600494.74	82.82	81.18	2	✓		
OW-2269L	mud rotary	141.15	130 - 140	13413123.29	2600574.23	82.55	80.89	2	✓		✓
OW-2269U	mud rotary	91.15	80 - 90	13413110.10	2600589.08	82.43	80.75	2	✓		✓
OW-2284L	mud rotary	111.06	100 - 110	13413063.71	2600939.04	82.74	80.98	2	✓		
OW-2284U	mud rotary	76.07	65 - 75	13413055.14	2600956.60	82.62	80.97	2	✓		

ft bgs = feet below ground surface
Northings and Eastings provided in US feet (NAD83)
Elevations in feet (NAVD88)

Prepared by: [illegible] Date: 7-10-08

Checked by: KAW Date: 7-10-08

TABLE 5.2
SUMMARY OF GROUNDWATER FIELD MEASUREMENTS
OBSERVATION WELLS
EXELON TEXAS COL (Victoria) PROJECT
MACTEC PROJECT NO: 6468-07-1777
POWER BLOCK

Well ID	Sample Date	Temperature (°C)	pH	Dissolved Oxygen (mg/L)	Specific Conductivity ($\mu S/cm^2$)	Turbidity (NTU)	O.R.P. (mv)
OW-2169U	2/18/2008	22.85	6.91	1.46	1179	10	135.9
OW-2169L	2/18/2008	22.54	7.31	5.12	1373	2	46.5
OW-2269L	2/18/2008	23.10	6.83	0.95	1358	116	55.1
OW-2269U	2/18/2008	22.79	7.06	5.72	1492	6	104.9

Observation wells purged in accordance with ASTM D 6452-99. Field parameters reported for the final stablization reading.

Prepared by: LWS Date: 7-10-08

Checked by: KAW Date: 7.10.08

TABLE 5.3
SUMMARY OF GROUNDWATER TEST RESULTS
OBSERVATION WELLS
EXELON TEXAS COL (Victoria) PROJECT
MACTEC PROJECT NO: 6468-07-1777
POWER BLOCK

Analytical Method →		160.1	6020C								300.0						310.1 - Alkalinity			350.1	SM18 1030F & API
Constituent →		TDS	Calcium	Iron	Magnesium	Manganese	Potassium	Silica	Silicon	Sodium	Bromide	Chloride	Fluoride	Sulfate	Nitrate	Nitrite	Bicarbonate	Carbonate	Total	Ammonia*	Ion Balance Difference
Well ID	Date Collected	mg/L	µg/L								mg/L						mg/L			µg/L	%
OW-2169 U	2/18/2008	642	53,200 N	<500	14,000	<20	2,620	44,300	20,700 N	194,000	0.26	77.0	1.1	74.6	0.53	<0.020	397	<5.0	397	22.7 B, J	2.3
OW-2169 L	2/18/2008	780	65,500 N	<500	16,000	9.8 B	2,680	45,200	21,100 N	218,000	0.36	119	1.1	122	0.47	<0.020	398	<10.0	398	22.7 B, J	0.78
OW-2269 U	2/18/2008	801	116,000 N	<500	17,800	<20	4,050	36,000	16,800 N	181,000	0.72	224	0.45	105	0.59	<0.020	339	<5.0	339	22.7 B, J	0.080 B
OW-2269 L	2/18/2008	872	209,000 N	873	2,740	14.3 B	16,100	17,800	8,320 N	160,000	0.57	214	0.38	23.9	0.097	0.19	<25.0	324	592	72.8	0.28

* = Test conducted on Nitrogen, as Ammonia.
< # = Indicates analyte not detected at or above the method detection limit.
N = Spiked analyte recovery is outside stated control limits. Method performance confirmed using Laboratory Control Spike sample results.
B = Estimated result. Result is less than the reporting limit.
J = Method blank contamination. The associated method blank contains the target analyte at a reportable level. Therefore, these data should not be relied upon.

Prepared by: WSL Date: 7-10-08

Checked by: KAW Date: 7-10-08

MACTEC Engineering and Consulting, Inc.
Raleigh, NC

TABLE 5.4
IN-SITU SLUG TEST RESULTS SUMMARY (ASTM D 4044-96(02))
EXELON TEXAS COL (Victoria) PROJECT
MACTEC PROJECT NO: 6468-07-1777
POWER BLOCK

				Falling Head Test Results in ft/day		Rising Head Test Results in ft/day		
Slug Test ID	Well Depth (ft bgs)	TOC Elevation (ft NAVD88)	Screen Interval (ft bgs)	Bouwer & Rice	Butler	Bouwer & Rice	Butler	Notes
OW-2150 U	67	82.78	55 - 65	5.45E-02	8.47E-02	2.46E+00	4.46E+00	Well screen exposed to SM (3.5 ft), SC (5.6 ft), and CH (0.9 ft), in increasing depth.
OW-2150 L	152	82.45	140 - 150	*Probe moved during test*		8.67E+00	1.64E+01	Well screen exposed to CH (8.5 ft) and SP-SM (1.5 ft), in increasing depth.
OW-2169 U	67	81.77	55 - 65	1.45E+01	3.02E+01	2.84E+01	3.09E+01	Well screen exposed to SM (3.5 ft), SP (5 ft), and SC (1.5 ft), in increasing depth.
OW-2169 L	102	81.72	90 - 100	1.07E+00	1.33E+00	3.62E+01	3.65E+01	Well screen exposed to SC (10 ft).
OW-2181 U	52	81.31	40 - 50	4.08E+00	1.35E+01	8.95E+00	1.28E+01	Well screen exposed to SC (10 ft).
OW-2181 L	102	81.32	90 - 100	5.79E-3 (Late Time)	3.44E-02	1.30E-02	3.44E-02	Well screen exposed to CH (4.8 ft), SC (5 ft), and SP-SC (0.2 ft), in increasing depth.
OW-2185 U	77	81.45	65 - 75	9.92E+00	1.52E+01	1.08E+01	1.39E+01	Well screen exposed to CH (3 ft), SP-SC (5 ft), and CH (2 ft) in increasing depth.
OW-2185 L	102	81.36	90 - 100	6.17E+00	8.10E+00	1.94E+01	2.73E+01	Well screen exposed to SW (4.6 ft) and SP (5.4 ft), in increasing depth.
OW-2253 U	67	82.82	55 - 65	1.08E+01	1.16E+01	1.25E+01	1.54E+01	Well screen exposed to SC (3.5 ft), SP (5 ft) and CH (1.5 ft) in increasing depth.
OW-2253 L	147.00	82.66	135 - 145	1.01E+02	1.05E+02	7.73E+01	8.79E+01	Well screen exposed to SC (3.5 ft), and SP-SM (6.5 ft) in increasing depth.
OW-2253 LB	147.00	82.66	135 - 145	9.98E+01	1.15E+02	NT	NT	Well screen exposed to SC (3.5 ft), and SP-SM (6.5 ft) in increasing depth, no rising head test conducted.
OW-2253 L2	147.00	82.66	135 - 145	1.38E+02	1.48E+02	NT	NT	Well screen exposed to SC (3.5 ft), and SP-SM (6.5 ft) in increasing depth, no rising head test conducted.
OW-2269 U	92	82.43	80 - 90	7.93E-01	1.13E+00	2.49E+00	3.41E+00	Well screen exposed to CL (0.4 ft) and SC (9.6 ft), in increasing depth.
OW-2269 UB	92	82.43	80 - 90	1.57E+00	2.25E+00	NT	NT	Well screen exposed to CL (0.4 ft) and SC (9.6 ft), in increasing depth, no rising head test conducted.
OW-2269 L	143	82.55	130 - 140	6.34E-01	1.26E+00	1.17E+00	1.50E+00	Well screen exposed to CH (0.4 ft), and SC-SM (9.6 ft) in increasing depth.
OW-2284 U	77	82.62	65 - 75	8.53E-01	9.52E-01	1.37E+00	1.82E+00	Well screen exposed to SP-SC (3.5 ft), and CH (6.5 ft) in increasing depth.
OW-2284 UB	77	82.62	65 - 75	5.79E-01	3.04E+00	NT	NT	Well screen exposed to SP-SC (3.5 ft), and CH (6.5 ft) in increasing depth, no rising head test conducted.
OW-2284 L	112	82.74	100 - 110	2.62E+01	3.89E+01	2.39E+01	3.58E+01	Well screen exposed to SP (10 ft).

NT = not tested
No data = no data received as of 3/14/2008
ft bgs = feet below ground surface

Prepared by: [illegible] Date: 7-10-08

Checked by: KAW Date: 7-10-08

FINAL DATA REPORT Rev 0
GEOTECHNICAL EXPLORATION AND TESTING

EXELON TEXAS COL PROJECT
VICTORIA COUNTY, TEXAS
POWER BLOCK

July 10, 2008

VOLUME 1
Figures

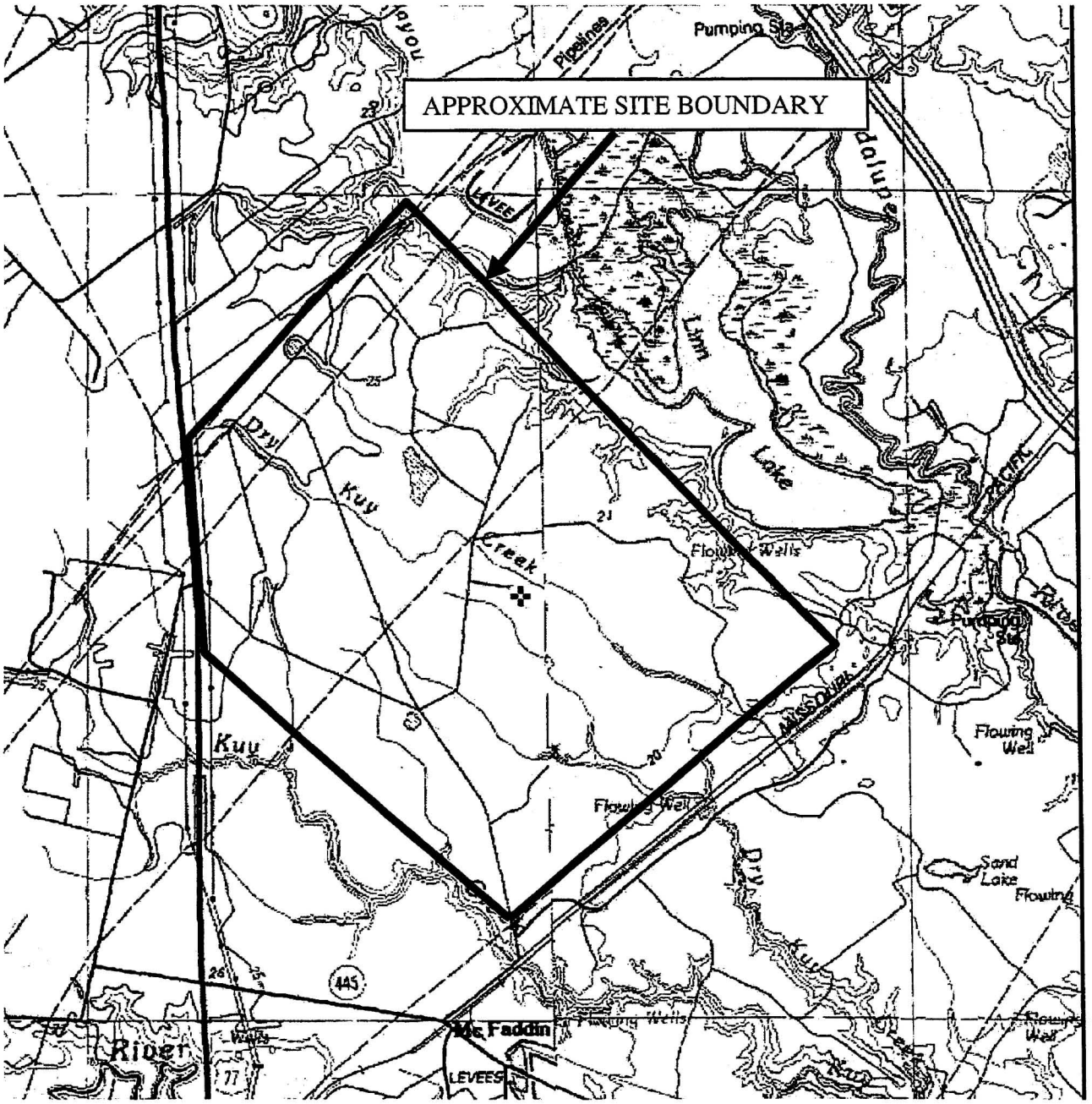
Prepared By:

MACTEC Engineering and Consulting, Inc.
Raleigh, North Carolina

MACTEC Project No. 6468-07-1777

Prepared For:

Bechtel Power Corporation
Subcontract No. 25352-102-HC4-CY00-00001



0 1 2 3 4 5 km

0 0.8 1.6 2.4 3.2 4 mi

UTM 14 695259E 3165327N (NAD83/WGS84)

USGS McFaddin (TX) Quadrangle

Projection is UTM Zone 14 NAD83 Datum

NORTH

NOTE: SITE LOCATION IS APPROXIMATE

MACTEC

MACTEC ENGINEERING AND CONSULTING, INC.
3301 ATLANTIC AVENUE
RALEIGH, NORTH CAROLINA 27604

SITE VICINITY MAP
EXELON COL PROJECT
VICTORIA, TEXAS

DRAWN:	WSG	DATE:	APRIL 2008	FIGURE
ENG CHECK:	CBS	SCALE:	AS SHOWN	1
APPROVAL:	KAW 4.30.08	JOB:	6468-07-1777	

FINAL DATA REPORT Rev 0
GEOTECHNICAL EXPLORATION AND TESTING

EXELON TEXAS COL PROJECT
VICTORIA COUNTY, TEXAS
POWER BLOCK

July 10, 2008

VOLUME 1
Appendix A – Survey Report

Prepared By:

MACTEC Engineering and Consulting, Inc.
Raleigh, North Carolina

MACTEC Project No. 6468-07-1777

Prepared For:

Bechtel Power Corporation
Subcontract No. 25352-102-HC4-CY00-00001

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Final Survey Report
As-built Survey for All Geotechnical Investigatory Sites
McCan Ranch Site, Victoria, Texas

Introduction

SURVCON INC. (Houston, Texas) in accordance with instructions directed by MACTEC Engineering and Consulting Inc. performed an As-built Survey to locate geotechnical borings previously staked at the McCan Ranch Site in Victoria County, Texas. These borings were assigned grid coordinate values in a *Boring Location Plan* issued by the Bechtel Corporation (Frederick, Maryland), Job No. 25352, Drawing No. 000-CY-0010-00002 and 000-CY-0010-00003, issued October 31, 2007. The pre-determined grid coordinate values assigned to each boring were in the Texas Coordinate System South Central Zone 4204, North American Datum 1983. SURVCON INC. established horizontal and vertical control monuments within the subject site utilizing GPS static observation techniques. Geotechnical borings were then located in the field with GPS; however, not all boring locations were staked by SURVCON INC. The MACTEC geotechnical team staked and marked boring locations in the proposed cooling pond area of the McCan Ranch Site. After all boring locations were staked on the ground, the MACTEC boring team proceeded to bore all investigatory borings as referenced from the *Boring location Plan*. This survey report chronicles the geospatial locations of all as-built boreholes on the McCan Ranch Site.

As the as- built locations were located in the field, the raw GPS data was sent to the Houston office via FTP and processed. Error analyses were calculated for collected coordinate data sets and every borehole location were assigned averaged state plane coordinate values. These values were then compared to the borehole stakeout locations in comparison with the planned geospatial locations of the geotechnical borings defined by the *Boring Location Plan*. All professional surveying services were done in accordance with the guidelines and instructions outlined in a document titled, *Work Instructions No. 208*, Project No. 6468-07-1777, issued to both Adam Salazar III, and Luther Hensley by email from Kathryn A. White of MACTEC. Bill Deobald, Senior Geologist at MACTEC made additional checks for inclusion of all geotechnical investigation sites.

Datum and Accuracy Standards

Horizontal datum	North American Datum 1983 (NAD83)
Vertical Datum	North American Vertical Datum 1988 (NAVD88)

All horizontal coordinates for the geotechnical borings are reported in Grid, NAD83. Vertical elevations are reported in NAVD88 and are orthometric heights. These heights are derived from the equation: ellipsoid height – (geoid height). Coordinates may be modified to surface values to calculate surface horizontal distances, by dividing by the average combined scale factor of 0.999941186. Horizontal accuracy to locate the borings exceeded the required third order accuracy (1:5000). Vertical accuracy for all boring locations met or exceeded the required accuracy of 0.10 feet.

Establishment of Horizontal and Vertical Control

Two control points were established on the McCann Ranch Site, Victoria, County, Texas by GPS static observation techniques. Two L1/L2 GPS receivers were plumbed over the five-foot long 5/8" iron rods set in the ground at the Victoria County Site. Continuous static observations of more than 3 hours were then performed. The data set accumulated through the duration of the static observation time was sent via internet to the National Geodetic Survey (NGS) Online Position User Service (OPUS) to establish horizontal and vertical control on one of the control points although a solution for both control points were derived. Once it was established that the error constraints for the control points were within tolerance, one control point was held fixed and assigned primary control point status. A baseline solution with the 3 hours of observed static data was processed using Leica Geomatics Office to determine the horizontal and vertical coordinates for the secondary control point using a least squares technique. This solution was then compared to the OPUS solution as a check. The Primary and Secondary Control Points' horizontal and vertical coordinates are as follows:

Description	Grid Northing NAD83 TXSC US Ft.	Grid Easting NAD83 TXSC US Ft.	Orthometric Elevation NAVD88 US Ft.
Primary Control Pt. No. 1	13,414,408.22	2,606,561.05	76.75
Secondary Control Pt. No. 2	13,414,975.99	2,605,255.34	76.37

Methodology

Accuracy standards were achieved by collecting spatial data using Real Time Kinematic-Global Positioning Satellite (RTK-GPS) techniques. The Leica GPS System 1200 was used to collect all field data and observations, and Leica Geomatics Office Version 2.0 was used to process all GPS data. As stated, all data collected for the spatial locations of geotechnical borings were done in a manner to achieve accuracy in the horizontal component to met or exceeded a third order accuracy of 1:5,000 and all data collected for the spatial locations of geotechnical borings in the vertical component met or exceeded an accuracy of 0.10 feet (except for those noted in the following spread sheets).

Three observations were made on each geotechnical spatial location using RTK-GPS. The RTK-GPS observations were made at different time periods and different days to

ensure independent satellite geometry for each respective boring. The independent observations were then processed through Leica Geomatics Office and a least squares adjustment and error analysis were performed in order to check the accuracy of the collected geospatial locations of the geotechnical borings. The processed coordinate values for the as-built geotechnical borings and their standard deviations from the mean coordinate values are as follows:

BOREHOLE	AVERAGE AS-BUILT GRID NORTHING NAD83 TXSC US FT.	AVERAGE AS-BUILT GRID EASTING NAD83 TXSC US FT.	AVERAGE ORTHOMETRIC ELEVATION NAVD88 US FT.	σ N	σ E	σ ELEV.
B-01	13404257.08	2606680.96	71.46	0.01	0.01	0.05
B-02	13411511.00	2607865.77	74.68	0.02	0.03	0.06
B-03	13414926.74	2609291.47	74.89	0.05	0.01	0.03
B-04	13414277.17	2607437.06	78.97	0.01	0.02	0.08
B-05	13414770.02	2605821.89	77.56	0.03	0.02	0.10
B-06	13415884.18	2604971.12	78.98	0.03	0.01	0.10
B-07	13418366.17	2606567.82	77.39	0.01	0.05	0.03
B-08	13415809.85	2598937.51	81.71	0.04	0.01	0.05
B-09	13414943.90	2604897.77	77.36	0.02	0.01	0.05
B-10	13418474.15	2604736.80	77.69	0.01	0.03	0.05
B-11	13411479.49	2607866.27	74.47	0.00	0.00	0.01
B-12	13418446.37	2606546.46	76.70	0.01	0.01	0.01
B-2150	13412560.45	2599590.93	80.44	0.13	0.11	0.01
B-2151	13412636.54	2599654.12	80.41	0.05	0.03	0.08
B-2152	13412705.76	2599720.24	80.26	0.08	0.09	0.05
B-2153	13412821.99	2599842.54	80.23	0.10	0.06	0.06
B-2154	13412450.91	2599619.83	80.54	0.04	0.03	0.07
B-2155	13412471.13	2599698.69	80.36	0.10	0.16	0.01
B-2156	13412548.01	2599760.77	80.25	0.11	0.06	0.09
B-2157	13412623.72	2599823.05	80.07	0.00	0.02	0.08
B-2158	13412749.59	2599928.77	80.45	0.11	0.05	0.01
B-2159	13412476.54	2599788.95	80.40	0.13	0.06	0.07
B-2160	13412180.67	2599627.24	80.43	0.12	0.06	0.07
B-2161	13412263.41	2599698.18	80.49	0.04	0.11	0.13
B-2162 A	13412385.92	2599799.34	80.16	0.08	0.04	0.09
B-2162 A Offset	13412378.65	2599792.16	80.05	0.04	0.04	0.07
B-2163	13412463.50	2599862.07	79.85	0.11	0.07	0.09
B-2164	13412537.94	2599925.58	80.38	0.05	0.10	0.11
B-2165	13412661.24	2600035.28	80.13	0.11	0.05	0.01
B-2166	13412109.03	2599713.14	80.50	0.06	0.15	0.02
B-2167	13412192.20	2599781.27	80.19	0.09	0.08	0.05
B-2168	13412294.30	2599891.10	80.12	0.04	0.06	0.04
B-2169	13412350.21	2599938.43	79.47	0.06	0.03	0.03

BOREHOLE	AVERAGE AS-BUILT GRID NORTHING NAD83 TXSC US FT.	AVERAGE AS-BUILT GRID EASTING NAD83 TXSC US FT.	AVERAGE ORTHOMETRIC ELEVATION NAVD88 US FT.	σ N	σ E	σ ELEV.
B-2170	13412413.86	2599989.72	79.68	0.11	0.03	0.10
B-2170 R	13412396.19	2599989.32	79.18	0.12	0.06	0.04
B-2171	13412488.43	2600092.96	80.03	0.08	0.06	0.01
B-2171 R	13412479.95	2600074.23	79.97	0.10	0.10	0.01
B-2172	13412096.23	2599829.90	80.10	0.13	0.09	0.03
B-2173	13412224.54	2599944.52	79.59	0.05	0.04	0.01
B-2174 A	13412299.46	2600000.64	80.11	0.07	0.07	0.06
B-2174 A Offset	13412316.51	2599991.79	79.28	0.02	0.05	0.03
B-2174 UD	13412276.56	2600005.51	79.58	0.07	0.03	0.03
B-2174 UDR	13412303.29	2600012.41	78.98	0.01	0.00	0.02
B-2175	13412370.49	2600062.81	80.12	0.17	0.07	0.05
B-2176 A	13412511.69	2600175.17	79.81	0.07	0.12	0.02
B-2176 A Offset	13412522.55	2600178.10	79.99	0.04	0.08	0.02
B-2177	13412196.92	2600000.49	79.61	0.10	0.05	0.03
B-2178	13412315.43	2600107.27	79.53	0.06	0.10	0.00
B-2179	13412424.96	2600168.71	79.78	0.05	0.05	0.03
B-2180	13412247.39	2600062.56	78.85	0.06	0.10	0.03
B-2181	13412143.28	2600062.56	79.24	0.10	0.10	0.05
B-2182 A	13412219.77	2600133.20	79.69	0.02	0.01	0.01
B-2182 A Offset	13412209.92	2600137.01	79.70	0.05	0.04	0.06
B-2182 UD	13412207.39	2600143.80	79.47	0.07	0.08	0.09
B-2183	13412265.91	2600166.16	79.63	0.07	0.03	0.02
B-2184	13412295.45	2600305.41	79.71	0.04	0.05	0.05
B-2185	13412320.56	2600808.84	79.48	0.02	0.02	0.02
B-2250	13413327.46	2600233.62	81.05	0.07	0.07	0.01
B-2251	13413404.52	2600297.97	80.79	0.07	0.06	0.05
B-2252	13413478.24	2600360.51	80.74	0.07	0.03	0.07
B-2253	13413587.94	2600484.98	80.86	0.08	0.06	0.02
B-2254	13413216.45	2600262.92	80.54	0.07	0.08	0.03
B-2255	13413238.32	2600340.81	80.67	0.06	0.09	0.04
B-2256	13413314.37	2600403.14	80.26	0.07	0.05	0.08
B-2257	13413389.48	2600466.52	80.78	0.08	0.08	0.03
B-2258	13413515.61	2600571.48	80.75	0.10	0.05	0.04
B-2259	13413243.36	2600432.64	80.35	0.03	0.07	0.02
B-2260	13412945.84	2600269.60	80.71	0.02	0.05	0.03
B-2261	13413029.99	2600340.99	80.50	0.08	0.07	0.09
B-2262 A	13413146.75	2600442.41	80.42	0.06	0.03	0.08
B-2262 A Offset	13413146.80	2600433.53	80.57	0.01	0.02	0.04
B-2263	13413227.48	2600506.73	80.43	0.08	0.07	0.06
B-2264	13413303.45	2600569.40	80.51	0.06	0.06	0.03

BOREHOLE	AVERAGE AS-BUILT GRID NORTHING NAD83 TXSC US FT.	AVERAGE AS-BUILT GRID EASTING NAD83 TXSC US FT.	AVERAGE ORTHOMETRIC ELEVATION NAVD88 US FT.	σ N	σ E	σ ELEV.
B-2265	13413424.28	2600677.27	80.60	0.09	0.07	0.13
B-2266	13412873.85	2600353.67	80.67	0.09	0.06	0.03
B-2267	13412957.87	2600424.20	80.74	0.10	0.03	0.10
B-2268	13413056.37	2600528.54	80.58	0.04	0.05	0.10
B-2269	13413117.17	2600582.50	80.45	0.07	0.03	0.06
B-2269 UD	13413092.19	2600593.55	80.06	0.04	0.02	0.03
B-2270	13413179.24	2600633.41	80.62	0.08	0.06	0.05
B-2271	13413253.44	2600735.25	80.46	0.07	0.04	0.05
B-2272	13412863.17	2600472.73	80.22	0.03	0.08	0.01
B-2273	13412991.36	2600585.49	80.69	0.04	0.07	0.05
B-2274 A	13413066.32	2600642.98	80.86	0.01	0.06	0.04
B-2274 A Offset	13413070.52	2600633.47	80.34	0.02	0.02	0.04
B-2274 UD	13413047.70	2600652.45	80.41	0.06	0.05	0.03
B-2275	13413133.62	2600702.31	80.49	0.08	0.06	0.04
B-2276 A	13413276.30	2600822.55	80.53	0.07	0.10	0.05
B-2276 A Offset	13413289.36	2600817.99	80.63	0.02	0.02	0.04
B-2277	13412961.61	2600644.66	80.60	0.04	0.05	0.03
B-2278	13413084.23	2600745.84	80.69	0.10	0.09	0.04
B-2279	13413192.06	2600811.88	80.28	0.07	0.08	0.01
B-2280	13413014.25	2600704.09	80.57	0.05	0.07	0.04
B-2281	13412908.71	2600705.43	80.42	0.09	0.01	0.09
B-2282 A	13412970.74	2600757.69	80.31	0.05	0.00	0.01
B-2282 A Offset	13412962.40	2600766.39	80.46	0.02	0.04	0.05
B-2283	13413031.52	2600808.58	80.40	0.08	0.06	0.05
B-2284	13413060.61	2600948.44	80.42	0.13	0.07	0.06
B-2285	13412682.80	2600322.38	80.35	0.08	0.05	0.04
B-2301 A	13414429.68	2596278.37	81.23	0.01	0.03	0.05
B-2301	13414414.60	2596251.62	80.79	0.08	0.07	0.07
B-2302 A	13407371.01	2598389.30	80.32	0.00	0.00	0.02
B-2302	13407401.61	2598386.93	80.00	0.04	0.04	0.07
B-2302 UD	13407373.35	2598406.10	80.00	0.06	0.04	0.03
B-2303 A	13402308.03	2600478.63	75.36	0.07	0.02	0.01
B-2303	13402314.55	2600497.11	75.56	0.11	0.06	0.03
B-2304 A	13396556.48	2608686.75	68.33	0.01	0.03	0.05
B-2304	13396541.80	2608710.01	68.12	0.03	0.01	0.04
B-2304 UD	13396571.12	2608693.06	68.46	0.04	0.01	0.06
B-2305 A	13406652.71	2621646.04	65.45	0.03	0.03	0.08
B-2305	13406649.21	2621680.51	65.58	0.02	0.05	0.03
B-2306 A	13411450.19	2615249.64	64.28	0.03	0.02	0.01
B-2306	13411472.15	2615253.02	64.68	0.01	0.01	0.00

BOREHOLE	AVERAGE AS-BUILT GRID NORTHING NAD83 TXSC US FT.	AVERAGE AS-BUILT GRID EASTING NAD83 TXSC US FT.	AVERAGE ORTHOMETRIC ELEVATION NAVD88 US FT.	σ N	σ E	σ ELEV.
B-2307 A	13420888.12	2603157.79	76.75	0.03	0.03	0.07
B-2307	13420917.89	2603184.91	76.38	0.06	0.02	0.09
B-2308	13404197.77	2599333.56	76.39	0.06	0.01	0.05
B-2309 P	13405492.18	2600431.73	76.19	0.07	0.02	0.08
B-2309 P-L	13405491.59	2600445.06	76.13	0.07	0.07	0.04
B-2309 P-U	13405492.30	2600435.20	76.25	0.10	0.07	0.06
B-2310	13406601.70	2601353.57	75.95	0.03	0.04	0.03
B-2311 P	13407700.78	2602286.18	75.78	0.01	0.01	0.01
B-2311 P-L	13407702.98	2602296.89	75.33	0.07	0.04	0.07
B-2311 P-U	13407705.71	2602287.63	75.71	0.06	0.04	0.04
B-2312 P	13410697.79	2604163.84	75.71	0.01	0.03	0.02
B-2312 P-L	13410694.32	2604153.23	75.50	0.02	0.01	0.05
B-2312 P-U	13410699.82	2604161.16	75.46	0.08	0.03	0.03
B-2313 P	13412119.71	2605602.60	77.96	0.03	0.01	0.01
B-2313 P-L	13412115.55	2605606.11	77.97	0.01	0.02	0.03
B-2313 P-U	13412117.40	2605610.94	77.86	0.03	0.02	0.04
B-2314 P	13413943.94	2607786.59	76.01	0.02	0.02	0.04
B-2314 P-L	13413940.68	2607782.57	75.42	0.01	0.00	0.01
B-2314 P-U	13413937.97	2607776.49	75.48	0.02	0.01	0.03
B-2315	13416228.72	2609409.27	47.06	0.04	0.01	0.01
B-2316	13413189.22	2608491.76	75.17	0.04	0.01	0.03
B-2317	13410598.40	2600511.90	76.73	0.00	0.02	0.02
B-2318	13401612.98	2601154.61	75.31	0.03	0.03	0.06
B-2319	13403601.01	2603048.72	74.16	0.02	0.01	0.02
B-2319 UD	13403595.98	2603062.86	74.16	0.12	0.05	0.10
B-2320	13407573.79	2606839.75	71.46	0.04	0.02	0.09
B-2321	13410953.82	2610037.97	71.62	0.01	0.01	0.01
B-2321 UD	13410937.49	2610017.10	71.81	0.01	0.01	0.02
B-2322	13413528.90	2612528.69	68.53	0.07	0.02	0.04
B-2324	13416308.77	2612208.94	24.47	0.02	0.02	0.04
B-2325 P	13401292.55	2603700.67	73.83	0.02	0.03	0.03
B-2325 P-L	13401292.30	2603696.51	73.85	0.02	0.03	0.08
B-2325 P-U	13401288.29	2603699.18	73.79	0.05	0.03	0.04
B-2326 P	13403071.71	2605620.06	70.92	0.02	0.02	0.03
B-2326 P-L	13403074.73	2605620.44	70.76	0.07	0.08	0.06
B-2326 P-U	13403069.23	2605616.46	70.97	0.07	0.05	0.12
B-2327 P	13404716.72	2607391.55	71.31	0.04	0.04	0.05
B-2327 P-L	13404712.18	2607384.02	70.81	0.02	0.01	0.10
B-2327 P-U	13404711.41	2607393.78	71.24	0.23	0.05	0.07
B-2328 P	13406227.52	2609018.21	68.55	0.06	0.02	0.07

BOREHOLE	AVERAGE AS-BUILT GRID NORTHING NAD83 TXSC US FT.	AVERAGE AS-BUILT GRID EASTING NAD83 TXSC US FT.	AVERAGE ORTHOMETRIC ELEVATION NAVD88 US FT.	σ N	σ E	σ ELEV.
B-2328 P-L	13406222.90	2609021.23	68.42	0.02	0.02	0.04
B-2328 P-U	13406233.26	2609021.31	68.13	0.02	0.02	0.02
B-2329 P	13407870.29	2610791.91	67.98	0.02	0.03	0.04
B-2329 P-L	13407871.37	2610784.65	68.06	0.03	0.03	0.05
B-2329 P-U	13407877.98	2610791.88	68.07	0.04	0.02	0.05
B-2330 P	13410093.19	2613189.45	68.19	0.05	0.04	0.09
B-2330 P-L	13410088.73	2613185.03	68.18	0.00	0.02	0.09
B-2330 P-U	13410096.27	2613183.99	67.89	0.01	0.04	0.09
B-2331	13409862.54	2612278.74	69.37	0.03	0.04	0.04
B-2332	13414435.21	2603735.80	78.68	0.07	0.02	0.03
B-2333	13398864.77	2603981.87	76.07	0.01	0.00	0.04
B-2334	13400634.86	2606130.71	71.85	0.03	0.02	0.04
B-2335	13404183.94	2610412.10	66.75	0.06	0.02	0.04
B-2336	13409474.40	2616874.85	68.00	0.01	0.01	0.02
B-2337	13407263.05	2614846.26	67.23	0.07	0.06	0.05
B-2338	13398220.80	2606385.80	68.15	0.04	0.03	0.04
B-2339 P	13399913.99	2608670.98	68.89	0.07	0.03	0.01
B-2339 P-L	13399911.22	2608674.69	68.63	0.05	0.03	0.03
B-2339 P-U	13399916.45	2608670.14	68.75	0.04	0.01	0.04
B-2340	13400762.63	2609812.65	68.09	0.04	0.02	0.02
B-2341 P	13401608.46	2610954.27	65.22	0.07	0.03	0.04
B-2341 P-L	13401617.83	2610954.24	65.53	0.01	0.01	0.01
B-2341 P-U	13401610.51	2610947.05	64.98	0.01	0.02	0.01
B-2342 P	13402771.26	2612522.81	67.22	0.00	0.03	0.06
B-2342 P-L	13402761.03	2612526.25	67.34	0.02	0.05	0.06
B-2342 P-U	13402788.89	2612523.26	67.61	0.02	0.04	0.06
B-2343 P	13404151.56	2614382.47	64.51	0.02	0.01	0.08
B-2343 P-L	13404159.35	2614395.88	64.95	0.04	0.01	0.10
B-2343 P-U	13404159.36	2614386.73	64.62	0.04	0.04	0.08
B-2344	13404997.85	2615527.11	65.78	0.01	0.00	0.02
B-2345 P	13405844.69	2616666.65	67.81	0.01	0.02	0.03
B-2345 P-L	13405831.44	2616657.32	67.79	0.06	0.02	0.04
B-2345 P-U	13405835.31	2616662.51	67.91	0.03	0.09	0.08
B-2346	13407540.56	2618951.51	67.09	0.00	0.01	0.01
B-2348	13409626.85	2621653.06	50.63	0.04	0.00	0.01
B-2349	13417352.46	2607239.49	76.66	0.03	0.02	0.01
B-2350	13395764.08	2610122.62	65.25	0.02	0.04	0.01
B-2351	13398915.88	2613285.96	63.73	0.03	0.03	0.06
B-2352	13402480.47	2617531.27	62.91	0.01	0.02	0.04
B-2352 UD	13402493.35	2617543.73	62.84	0.01	0.05	0.07

BOREHOLE	AVERAGE AS-BUILT GRID NORTHING NAD83 TXSC US FT.	AVERAGE AS-BUILT GRID EASTING NAD83 TXSC US FT.	AVERAGE ORTHOMETRIC ELEVATION NAVD88 US FT.	σ N	σ E	σ ELEV.
B-2353	13406185.70	2620582.19	65.60	0.01	0.03	0.00
B-2354	13418119.59	2607884.13	76.83	0.03	0.02	0.04
B-2355	13412008.12	2611224.44	71.04	0.01	0.01	0.00
B-2356	13409147.49	2614293.88	67.71	0.01	0.02	0.01
B-2357	13404654.33	2620736.11	65.67	0.06	0.01	0.03
B-2358	13402101.51	2611620.85	66.47	0.01	0.02	0.01
B-2359	13417294.57	2605500.03	77.57	0.01	0.03	0.02
B-2359 UD	13417325.03	2605493.44	77.35	0.08	0.01	0.06

CPT NO.	AVERAGE AS-BUILT GRID NORTHING NAD83 TXSC US FT.	AVERAGE AS-BUILT GRID EASTING NAD83 TXSC US FT.	AVERAGE ORTHOMETRIC ELEVATION NAVD88 US FT.	σ N	σ E	σ ELEV.
C-2101	13412774.10	2599705.86	80.12	0.05	0.04	0.01
C-2102 S	13412550.23	2599702.26	80.17	0.06	0.09	0.05
C-2103	13412715.32	2599852.09	77.68	0.03	0.03	0.07
C-2104 S	13412187.52	2599704.22	80.10	0.08	0.03	0.01
C-2105	13412269.09	2599774.92	80.19	0.06	0.06	0.01
C-2106	13412291.55	2599955.62	79.59	0.00	0.00	0.01
C-2106 S	13412296.36	2599958.27	79.51	0.04	0.06	0.03
C-2107	13412304.73	2600042.26	79.96	0.00	0.03	0.02
C-2108	13412425.89	2600105.91	79.78	0.07	0.00	0.02
C-2109 S	13412545.94	2600138.83	79.93	0.06	0.05	0.03
C-2110	13412478.15	2600217.10	80.00	0.03	0.02	0.02
C-2111	13412225.65	2600089.78	78.04	0.01	0.01	0.02
C-2111 A	13412224.80	2600089.84	78.14	0.06	0.06	0.02
C-2111 B	13412225.10	2600087.29	78.28	0.04	0.06	0.02
C-2111 C	13412238.89	2600087.16	78.04	0.05	0.05	0.02
C-2111 D	13412212.18	2600086.06	79.22	0.05	0.06	0.00
C-2112	13412358.60	2600185.71	79.55	0.03	0.04	0.03
C-2113	13412251.45	2600231.11	79.31	0.05	0.01	0.02
C-2201	13413541.97	2600349.92	80.62	0.03	0.06	0.04
C-2202 S	13413315.91	2600345.61	80.42	0.00	0.02	0.05
C-2203	13413489.00	2600490.16	80.56	0.05	0.02	0.01
C-2204 S	13412953.12	2600347.76	80.35	0.05	0.04	0.00
C-2204 SA	13412954.25	2600354.46	80.30	0.08	0.06	0.00
C-2204 SB	13412963.86	2600351.20	80.18	0.05	0.02	0.05
C-2205	13413036.37	2600417.96	80.39	0.08	0.04	0.06
C-2206	13413081.83	2600615.27	80.22	0.03	0.04	0.01

CPT NO.	AVERAGE AS-BUILT GRID NORTHING NAD83 TXSC US FT.	AVERAGE AS-BUILT GRID EASTING NAD83 TXSC US FT.	AVERAGE ORTHOMETRIC ELEVATION NAVD88 US FT.	σ N	σ E	σ ELEV.
C-2206 S	13413071.11	2600604.08	80.63	0.04	0.03	0.09
C-2207	13413071.18	2600687.06	80.39	0.10	0.04	0.00
C-2208	13413191.48	2600748.18	80.54	0.08	0.04	0.03
C-2209 S	13413311.92	2600780.51	80.27	0.05	0.05	0.06
C-2210	13413244.43	2600858.74	80.30	0.07	0.06	0.01
C-2210 A	13413246.80	2600860.38	79.87	0.04	0.01	0.04
C-2211	13412992.38	2600730.80	80.20	0.12	0.03	0.04
C-2212	13413123.28	2600827.18	80.44	0.10	0.06	0.05
C-2213	13413017.49	2600874.63	80.46	0.13	0.06	0.03
C-2214	13412587.86	2600280.45	79.86	0.05	0.02	0.03
C-2215	13412539.13	2600425.19	79.83	0.07	0.04	0.02
C-2216	13414151.27	2600733.87	80.54	0.01	0.05	0.10
C-2301 S	13408989.39	2599158.23	79.08	0.02	0.04	0.03
C-2301 SA	13408982.41	2599162.20	78.70	0.00	0.02	0.02
C-2302	13412519.49	2602124.85	77.49	0.05	0.04	0.04
C-2303 S	13416428.66	2605405.65	76.79	0.04	0.03	0.08
C-2304	13418878.70	2607463.62	74.85	0.07	0.08	0.04
C-2305	13408849.43	2603251.14	75.47	0.02	0.04	0.02
C-2306	13411148.27	2605179.25	77.54	0.09	0.01	0.05
C-2307	13414685.38	2608147.28	74.88	0.06	0.05	0.05
C-2308	13415348.90	2610567.73	58.02	0.08	0.05	0.06
C-2309	13405587.95	2604945.49	72.92	0.08	0.05	0.06
C-2310	13409556.77	2608738.56	70.88	0.05	0.01	0.09
C-2311	13413231.26	2613049.76	41.70	0.01	0.04	0.04
C-2311 A	13413277.55	2612969.43	50.49	0.03	0.05	0.06
C-2312	13397971.98	2606226.92	64.99	0.01	0.01	0.03
C-2313	13399066.96	2607529.09	71.17	0.00	0.03	0.01
C-2314	13402413.42	2608270.67	69.45	0.06	0.01	0.08
C-2315	13405943.12	2612535.56	66.35	0.03	0.03	0.00
C-2316	13407731.74	2614700.43	68.23	0.01	0.00	0.04
C-2317	13408493.37	2617901.20	45.17	0.01	0.00	0.03
C-2318	13403305.07	2613240.79	66.39	0.02	0.00	0.04
C-2319	13406689.77	2617807.82	65.56	0.02	0.00	0.01
C-2321 S	13397141.61	2611187.71	65.80	0.01	0.00	0.03
C-2321 SA	13397149.37	2611182.17	65.90	0.03	0.01	0.02
C-2322	13400701.15	2615409.91	62.19	0.01	0.03	0.04
C-2323 S	13404257.20	2619650.56	65.67	0.02	0.03	0.01
C-2324	13406320.31	2622094.07	63.58	0.03	0.02	0.04
C-2328	13395274.28	2609720.08	65.62	0.02	0.05	0.02

OBSERVATION WELL NO.	AVERAGE AS-BUILT GRID NORTHING NAD83 TXSC US FT.	AVERAGE AS-BUILT GRID EASTING NAD83 TXSC US FT.	AVERAGE ORTHOMETRIC ELEVATION NAVD88 US FT.	σ N	σ E	σ ELEV
OW-01 L	13404252.09	2606686.52	73.74	0.03	0.03	0.03
OW-01 L TOP CONC	13404252.72	2606685.58	72.22	0.05	0.03	0.03
OW-01 U	13404253.64	2606666.85	73.65	0.02	0.03	0.01
OW-01 U TOP CONC	13404254.49	2606666.07	72.16	0.06	0.06	0.03
OW-02 L	13411520.51	2607869.30	76.53	0.03	0.05	0.01
OW-02 L TOP CONC	13411521.57	2607868.98	75.07	0.06	0.02	0.05
OW-02 U	13411502.39	2607862.19	76.74	0.04	0.03	0.05
OW-02 U TOP CONC	13411503.36	2607861.75	75.25	0.08	0.01	0.01
OW-03 L	13414918.69	2609286.61	76.67	0.02	0.01	0.05
OW-03 L TOP CONC	13414918.42	2609285.47	75.21	0.01	0.03	0.07
OW-03U	13414934.48	2609294.86	77.05	0.02	0.01	0.05
OW-03 U TOP CONC	13414934.52	2609293.72	75.60	0.04	0.05	0.04
OW-04 L	13414268.74	2607440.23	80.67	0.03	0.01	0.01
OW-04 L TOP CONC	13414269.01	2607439.15	79.13	0.04	0.05	0.01
OW-04 U	13414280.51	2607428.57	81.08	0.02	0.01	0.02
OW-04 U TOP CONC	13414280.58	2607427.43	79.61	0.04	0.00	0.00
OW-05 L	13414774.22	2605813.28	79.90	0.02	0.03	0.07
OW-05 L TOP CONC	13414775.20	2605812.65	78.26	0.01	0.01	0.03
OW-05 U	13414770.21	2605832.08	79.55	0.02	0.01	0.06
OW-05 U TOP CONC	13414771.22	2605831.64	78.07	0.02	0.00	0.03
OW-06 L	13415889.64	2604964.90	81.55	0.09	0.09	0.00
OW-06 L TOP CONC	13415890.25	2604964.02	79.49	0.08	0.08	0.08
OW-06 U	13415875.58	2604966.94	80.77	0.07	0.06	0.02
OW-06 U TOP CONC	13415876.40	2604966.04	79.46	0.03	0.10	0.06
OW-07 L	13418420.52	2606531.28	79.04	0.06	0.05	0.03
OW-07 L TOP CONC	13418421.26	2606530.50	77.47	0.05	0.07	0.02
OW-07 U	13418421.40	2606542.01	79.02	0.07	0.05	0.02
OW-07 U TOP CONC	13418422.28	2606541.26	77.32	0.05	0.07	0.07
OW-08 L	13415818.85	2598942.49	84.07	0.07	0.04	0.00
OW-08 L TOP CONC	13415818.87	2598943.53	82.56	0.02	0.05	0.03
OW-08 U	13415801.21	2598934.58	83.88	0.05	0.05	0.02
OW-08 U TOP CONC	13415801.21	2598935.76	82.38	0.02	0.13	0.05
OW-09 L	13414937.42	2604893.58	80.00	0.06	0.01	0.10
OW-09 L TOP CONC	13414938.28	2604892.97	77.86	0.10	0.04	0.06
OW-09 U	13414956.05	2604894.51	79.24	0.08	0.08	0.05
OW-09 U TOP CONC	13414955.40	2604895.32	77.91	0.02	0.06	0.00
OW-10 L	13418486.44	2604760.99	79.88	0.01	0.05	0.03
OW-10 L TOP CONC	13418487.53	2604761.06	78.07	0.01	0.05	0.06
OW-10 U	13418474.37	2604768.43	79.53	0.08	0.04	0.05
OW-10 U TOP CONC	13418475.58	2604768.57	78.09	0.00	0.05	0.03

OBSERVATION WELL NO.	AVERAGE AS-BUILT GRID NORTHING NAD83 TXSC US FT.	AVERAGE AS-BUILT GRID EASTING NAD83 TXSC US FT.	AVERAGE ORTHOMETRIC ELEVATION NAVD88 US FT.	σ N	σ E	σ ELEV
OW-2150 L	13412552.91	2599585.12	82.45	0.08	0.05	0.01
OW-2150 L TOP CONC	13412554.00	2599585.62	80.87	0.07	0.03	0.02
OW-2150 U	13412568.08	2599582.77	82.78	0.11	0.05	0.05
OW-2150 U TOP CONC	13412569.02	2599583.62	80.91	0.06	0.08	0.03
OW-2169 L	13412356.74	2599930.20	81.72	0.08	0.04	0.01
OW-2169 L TOP CONC	13412357.98	2599930.15	80.04	0.03	0.03	0.00
OW-2169 U	13412343.77	2599945.85	81.77	0.07	0.04	0.02
OW-2169 U TOP CONC	13412344.89	2599945.62	80.11	0.05	0.04	0.01
OW-2181L	13412138.42	2600071.96	81.32	0.09	0.06	0.07
OW-2181 L TOP CONC	13412139.35	2600071.54	79.88	0.05	0.02	0.03
OW-2181 U	13412147.38	2600052.86	81.31	0.07	0.06	0.03
OW-2181 U TOP CONC	13412148.36	2600052.29	80.01	0.03	0.03	0.02
OW-2185 L	13412314.47	2600815.69	81.36	0.02	0.02	0.02
OW-2185 L TOP CONC	13412315.64	2600815.86	79.76	0.04	0.04	0.04
OW-2185 U	13412328.07	2600801.11	81.45	0.02	0.02	0.03
OW-2185 U TOP CONC	13412329.14	2600800.87	79.89	0.02	0.01	0.02
OW-2253 L	13413584.76	2600494.74	82.82	0.07	0.06	0.05
OW-2253 L TOP CONC	13413585.74	2600494.29	81.18	0.07	0.06	0.03
OW-2253 U	13413591.55	2600474.37	82.66	0.07	0.06	0.02
OW-2253 U TOP CONC	13413592.61	2600473.94	81.17	0.08	0.04	0.03
OW-2269 L	13413123.29	2600574.23	82.55	0.04	0.01	0.01
OW-2269 L TOP CONC	13413124.53	2600574.10	80.89	0.07	0.07	0.02
OW-2269 U	13413110.10	2600589.08	82.43	0.07	0.05	0.04
OW-2269 U TOP CONC	13413111.38	2600589.01	80.75	0.09	0.05	0.01
OW-2284 L	13413063.71	2600939.04	82.74	0.05	0.06	0.09
OW-2284 U TOP CONC	13413064.86	2600938.54	80.97	0.11	0.10	0.05
OW-2284U	13413055.14	2600956.60	82.62	0.06	0.06	0.08
OW-2284 L TOP CONC	13413056.14	2600956.28	80.98	0.05	0.05	0.04
OW-2301 L	13414429.77	2596268.29	83.19	0.02	0.05	0.17
OW-2301 L TOP CONC	13414430.11	2596268.35	81.89	0.12	0.03	0.04
OW-2301 U	13414430.08	2596288.46	83.27	0.02	0.02	0.05
OW-2301 U TOP CONC	13414430.39	2596288.71	81.77	0.02	0.03	0.03
OW-2302 L	13407382.11	2598388.94	81.95	0.02	0.02	0.06
OW-2302 L TOP CONC	13407382.70	2598388.05	80.46	0.04	0.04	0.04
OW-2302 U	13407361.50	2598388.47	81.99	0.03	0.02	0.03
OW-2302 U TOP CONC	13407362.26	2598387.74	80.52	0.03	0.03	0.01
OW-2304 L	13396528.12	2608678.06	69.73	0.03	0.03	0.05
OW-2304 L TOP CONC	13396528.37	2608678.09	68.88	0.00	0.03	0.01
OW-2304-U	13396542.39	2608679.35	70.10	0.02	0.05	0.02
OW-2304-U TOP CONC	13396542.58	2608679.36	68.80	0.00	0.04	0.04

OBSERVATION WELL NO.	AVERAGE AS-BUILT GRID NORTHING NAD83 TXSC US FT.	AVERAGE AS-BUILT GRID EASTING NAD83 TXSC US FT.	AVERAGE ORTHOMETRIC ELEVATION NAVD88 US FT.	σ N	σ E	σ ELEV
OW-2307 L	13420879.09	2603152.12	78.56	0.05	0.07	0.04
OW-2307 L TOP CONC	13420880.36	2603152.11	76.91	0.05	0.03	0.11
OW-2307 U	13420896.73	2603164.23	78.59	0.07	0.03	0.13
OW-2307 U TOP CONC	13420897.85	2603164.32	77.07	0.03	0.03	0.08
OW-2319 L	13403611.30	2603051.83	76.05	0.02	0.01	0.02
OW-2319 L TOP CONC	13403612.25	2603051.49	74.68	0.01	0.02	0.04
OW-2319 U	13403590.40	2603046.21	75.97	0.03	0.01	0.03
OW-2319 U TOP CONC	13403590.49	2603047.46	74.33	0.03	0.05	0.06
OW-2320 L	13407580.88	2606834.36	73.19	0.06	0.04	0.01
OW-2320 L TOP CONC	13407581.88	2606833.72	71.76	0.03	0.05	0.02
OW-2320 U	13407569.51	2606849.70	73.50	0.04	0.02	0.08
OW-2320 U TOP CONC	13407570.41	2606850.68	71.80	0.05	0.03	0.02
OW-2320 U1	13407445.66	2607080.05	72.90	0.03	0.05	0.01
OW-2320 U1 TOP CONC	13407446.90	2607079.84	71.36	0.01	0.02	0.04
OW-2320 U2	13407436.76	2607093.25	72.92	0.02	0.03	0.03
OW-2320 U2 TOP CONC	13407437.85	2607093.17	71.36	0.07	0.04	0.06
OW-2320 U3	13407448.17	2607121.37	72.84	0.01	0.03	0.03
OW-2320 U3 TOP CONC	13407449.28	2607121.38	71.36	0.03	0.09	0.08
OW-2320 U4	13407466.49	2607138.42	72.91	0.01	0.02	0.02
OW-2320 U4 TOP CONC	13407466.35	2607137.26	71.42	0.01	0.03	0.05
OW-2321 L	13410955.46	2610027.59	73.54	0.01	0.01	0.01
OW-2321 L TOP CONC	13410955.77	2610026.59	71.99	0.00	0.01	0.01
OW-2321 U	13410943.58	2610040.96	73.27	0.01	0.00	0.04
OW-2321 U TOP CONC	13410943.88	2610039.88	71.79	0.00	0.03	0.01
OW-2324 L	13416300.52	2612217.00	26.27	0.02	0.03	0.05
OW-2324 L TOP GND	13416300.92	2612216.76	24.85	0.01	0.01	0.06
OW-2324 U	13416316.54	2612203.23	26.17	0.02	0.01	0.02
OW-2324 U TOP GND	13416317.04	2612203.55	24.67	0.01	0.05	0.04
OW-2348 L	13409617.75	2621644.36	52.70	0.02	0.02	0.02
OW-2348 L TOP CONC	13409617.95	2621643.16	51.21	0.01	0.00	0.01
OW-2348 U	13409636.31	2621660.58	52.12	0.03	0.02	0.01
OW-2348 U TOP CONC	13409636.43	2621659.33	50.56	0.02	0.02	0.03
OW-2352 L	13402468.45	2617518.54	64.60	0.01	0.02	0.02
OW-2352 L TOP CONC	13402468.79	2617518.57	63.33	0.01	0.00	0.00
OW-2352 U	13402470.61	2617538.69	64.47	0.03	0.04	0.02
OW-2352 U TOP CONC	13402470.92	2617538.74	63.17	0.02	0.03	0.04
OW-2359 L1	13417263.65	2605470.56	79.36	0.00	0.03	0.02
OW-2359 L1 TOP CONC	13417263.98	2605469.40	78.08	0.00	0.02	0.01
OW-2359 L2	13417259.76	2605433.37	78.93	0.01	0.06	0.08
OW-2359 L2 TOP CONC	13417260.94	2605433.42	77.56	0.03	0.04	0.04

OBSERVATION WELL NO.	AVERAGE AS-BUILT GRID NORTHING NAD83 TXSC US FT.	AVERAGE AS-BUILT GRID EASTING NAD83 TXSC US FT.	AVERAGE ORTHOMETRIC ELEVATION NAVD88 US FT.	σ N	σ E	σ ELEV
OW-2359 L3	13417278.58	2605416.18	78.83	0.06	0.03	0.13
OW-2359 L3 TOP CONC	13417279.01	2605415.10	77.26	0.02	0.01	0.01
OW-2359-U1	13417252.64	2605460.64	79.29	0.03	0.00	0.04
OW-2359-U1 TOP CONC	13417253.02	2605459.59	77.66	0.02	0.02	0.01
TW-2320 U	13407428.59	2607105.51	72.72	0.02	0.01	0.00
TW-2320 U TOP CONC	13407429.59	2607105.40	71.50	0.03	0.01	0.02
TW-2359 L	13417241.41	2605450.48	79.88	0.03	0.07	0.09
TW-2359 L TOP CONC	13417242.94	2605450.87	77.69	0.01	0.01	0.02

RESISTIVITY	AVERAGE AS-BUILT GRID NORTHING NAD83 TXSC US FT.	AVERAGE AS-BUILT GRID EASTING NAD83 TXSC US FT.	AVERAGE ORTHOMETRIC ELEVATION NAVD88 US FT.	σ N	σ E	σ ELEV.
R-2101 A	13412761.28	2599119.76	80.81	0.03	0.03	0.03
R-2101 D	13412177.28	2599801.44	79.88	0.00	0.00	0.03
R-2101/ R-2102 CENTER POINT	13412470.72	2599460.82	80.53	0.02	0.03	0.05
R-2102 A	13412813.73	2599752.01	79.50	0.03	0.06	0.01
R-2102 D	13412127.65	2599169.54	80.79	0.01	0.00	0.02
R-2201 A	13413688.62	2599921.76	80.69	0.01	0.00	0.07
R-2201 D	13413110.41	2600611.49	80.28	0.06	0.00	0.08
R-2201/ R-2202 CENTER POINT	13413399.51	2600266.58	80.66	0.05	0.07	0.01
R-2202 A	13413039.50	2599964.52	80.52	0.07	0.03	0.03
R-2202 D	13413744.28	2600555.69	80.79	0.07	0.03	0.03

TEST PIT	AVERAGE AS-BUILT GRID NORTHING NAD83 TXSC US FT.	AVERAGE AS-BUILT GRID EASTING NAD83 TXSC US FT.	AVERAGE ORTHOMETRIC ELEVATION NAVD88 US FT.	σ N	σ E	σ ELEV.
TP-2101	13412437.27	2599756.15	80.43	0.01	0.02	0.04
TP-2102	13412124.00	2599818.54	80.35	0.05	0.03	0.04
TP-2103	13411950.60	2600103.92	79.70	0.05	0.02	0.04
TP-2104	13412451.21	2600288.03	80.20	0.03	0.04	0.03
TP-2201	13413198.85	2600399.35	79.85	0.03	0.03	0.05
TP-2202	13412889.65	2600464.19	80.60	0.04	0.01	0.03
TP-2203	13412717.50	2600741.27	80.26	0.07	0.04	0.03
TP-2204	13413215.93	2600931.80	80.84	0.03	0.03	0.07

TEST PIT	AVERAGE AS-BUILT GRID NORTHING NAD83 TXSC US FT.	AVERAGE AS-BUILT GRID EASTING NAD83 TXSC US FT.	AVERAGE ORTHOMETRIC ELEVATION NAVD88 US FT.	σ N	σ E	σ ELEV.
TP-2310	13406614.56	2601358.66	75.57	0.09	0.04	0.02
TP-2314	13413935.46	2607799.59	74.70	0.02	0.02	0.03
TP-2317	13410595.30	2600492.45	76.76	0.07	0.02	0.06
TP-2319	13403607.12	2603037.74	74.25	0.09	0.07	0.05
TP-2320	13407598.78	2606824.54	71.41	0.01	0.02	0.01
TP-2321	13410972.16	2610031.41	70.82	0.01	0.02	0.01
TP-2332	13414422.39	2603751.85	78.22	0.03	0.02	0.02
TP-2334	13400632.04	2606110.32	72.41	0.09	0.09	0.08
TP-2335	13404163.77	2610401.63	66.82	0.08	0.05	0.05
TP-2337	13407266.15	2614864.54	66.92	0.02	0.01	0.04
TP-2351	13398902.07	2613286.15	63.91	0.00	0.02	0.01
TP-2352	13402479.96	2617531.97	62.97	0.02	0.01	0.06

Conclusion

The as-built geospatial locations for all geotechnical borings on the Victoria County Site as defined by the *Boring Location Plan* issued by the Bechtel Corporation (Frederick, Maryland), Job No. 25352, Drawing No. 000-CY-0010-00002 and 000-CY-0010-00003, issued October 31, 2007 were located within the accuracies as defined by *Work Instructions No.208* being produced by MACTEC Engineering and Consulting Inc. and assigned MACTEC Project No. 6468-07-1777.

Compiled by Adam Salazar III, RPLS
Project Surveyor
SURVCON INC.
Houston, Texas
April 4, 2008
Revised: 04/07/08
Revised: 05/13/08

STATE OF TEXAS REGISTERED ADAM SALAZAR III 5965 PROFESSIONAL LAND SURVEYOR

05/13/2008

FINAL DATA REPORT Rev 0
GEOTECHNICAL EXPLORATION AND TESTING

EXELON TEXAS COL PROJECT
VICTORIA COUNTY, TEXAS
POWER BLOCK

July 10, 2008

VOLUME 1
Appendix B – Geotechnical Field Data

Prepared By:

MACTEC Engineering and Consulting, Inc.
Raleigh, North Carolina

MACTEC Project No. 6468-07-1777

Prepared For:

Bechtel Power Corporation
Subcontract No. 25352-102-HC4-CY00-00001

Contents

Geotechnical Boring Logs
Test Pit Logs
SPT Report

MACTEC

GEOTECHNICAL BORING LOG

Prepared By JPA Date 6-12-08

Checked By KAW Date 7.10.08

SHEET 1 OF 3

BECHTEL PROJECT NO.: 25352		COUNTY Victoria	GEOLOGIST C. Gandy
SITE DESCRIPTION Exelon COL Project (Victoria Site)		MACTEC PROJECT NO.: 6468-07-1777	GROUND WATER (ft)
BORING NO. B-2150	DRILL METHOD: Mud Rotary	SAMPLE METHODS: SPT	0 HR. ND
GROUND SURFACE ELEV. 80.4 ft (NAVD88)	NORTHING 13,412,560 US ft (NAD83)	EASTING 2,599,591 US ft (NAD83)	24 HR. ND
TOTAL DEPTH 150.0 ft	DRILL MACHINE CME-55 LC	DRILLER: D. White/O. Smith	HAMMER (ID) 140 lb. Auto (MEC 02)
DATE STARTED 11/8/07	COMPLETED 11/9/07	CASING DEPTH: N/A	BITS USED: 2 7/8" Wing Bit

ELEV. (ft)	DEPTH (ft)	BLOW COUNT 0.5ft	0.5ft	0.5ft	BLOWS PER FOOT (0 20 40 60 80 100)	SAMP. NO.	MOI	LOG	SOIL AND ROCK DESCRIPTION
80.4					Ground Surface				80.4 / 0.0
80.4	0.0	2	3	4	7	SS-1			FAT CLAY (CH), very dark gray (5YR3/1), firm, moist, few fine sands, no HCl reaction, roots
76.9	3.5	3	7	9	16	SS-2			3.5ft: dark gray (7.5YR4/1), very stiff, little sand, no HCl reaction, carbonate and iron nodules, slightly mottled
74.4	6.0	6	6	7	13	SS-3			74.4 / 6.0 LEAN CLAY with sand (CL), pale brown (10YR6/3), stiff, carbonate nodules, strong HCl reaction, thinly laminated, organics
71.9	8.5	4	5	6	11	SS-4			8.5ft: very pale brown (10YR7/3), weak HCl reaction, iron staining
69.4	11.0	7	12	13	25	SS-5			11.0ft: light gray (10YR7/2), very stiff, few sand, thinly laminated
66.9	13.5	6	8	8	16	SS-6			13.5ft: very pale brown (10YR7/3), strong HCl reaction,
61.9	18.5	4	4	6	10	SS-7			18.5ft: stiff, weak HCl reaction
56.9	23.5	4	5	6	11	SS-8			56.9 / 23.5 FAT CLAY (CH), reddish yellow (7.5YR7/8), mottled light greenish gray (10Y8/1), stiff, few sand, strong HCl reaction, trace carbonate nodules
51.9	28.5	4	6	8	14	SS-9			28.5ft: mottled yellow (10YR7/8), little sand, trace organics
46.9	33.5	5	6	8	14	SS-10			33.5ft: few sand
41.9	38.5	4	5	6	11	SS-11			38.5ft: brownish yellow (10YR6/6), mottled light greenish gray (10Y8/1), iron staining
36.9	43.5	5	8	12	20	SS-12			36.9 / 43.5 FAT CLAY with sand (CH), brownish yellow (10YR6/6), mottled very pale brown (10YR7/4), very stiff, little sand, weak HCl reaction
31.9	48.5	5	7	10	17	SS-13			48.5ft: no HCl reaction
26.9	53.5	7	10	9	19	SS-14			26.9 / 53.5 Silty SAND (SM), pale yellow (2.5Y7/3), firm, wet, little fines, iron staining, no HCl reaction

EXELON COL BORE EXELON-2.GPJ EXELON COL.GDT 6/12/08

MACTEC

BECHTEL PROJECT NO.: 25352	COUNTY Victoria	GEOLOGIST C. Gandy	
SITE DESCRIPTION Exelon COL Project (Victoria Site)	MACTEC PROJECT NO.: 6468-07-1777		GROUND WATER (ft)
BORING NO. B-2150	DRILL METHOD: Mud Rotary	SAMPLE METHODS: SPT	0 HR. ND
GROUND SURFACE ELEV. 80.4 ft (NAVD88)	NORTHING 13,412,560 US ft (NAD83)	EASTING 2,599,591 US ft (NAD83)	24 HR. ND
TOTAL DEPTH 150.0 ft	DRILL MACHINE CME-55 LC	DRILLER: D. White/O. Smith	HAMMER (ID) 140 lb. Auto (MEC 02)
DATE STARTED 11/8/07	COMPLETED 11/9/07	CASING DEPTH: N/A	BITS USED: 2 7/8" Wing Bit

ELEV. (ft)	DEPTH (ft)	BLOW COUNT 0.5ft	0.5ft	0.5ft	BLOWS PER FOOT (0 20 40 60 80 100)	SAMP. NO.	MOI	LOG	SOIL AND ROCK DESCRIPTION
24.3					Continued from previous page				
21.9	58.5								Silty SAND (SM), pale yellow (2.5Y7/3), firm, wet, little fines, iron staining, no HCl reaction *(continued)* 21.9 — 58.5
16.9	63.5	19	28	25	53	SS-15			Clayey SAND (SC), light gray (10YR7/2), very dense, moist, weak HCl reaction, carbonate nodules 63.5ft: reddish yellow (7.5YR7/6), wet, no HCl reaction 16.3 — 64.1
11.9	68.5	3	7	8	15	SS-16A/B			FAT CLAY (CH), light yellowish brown (10YR6/4), mottled light greenish gray (10Y8/1), stiff, moist, few sands, trace carbonate nodules, weak HCl reaction
6.9	73.5	5	6	8	14	SS-17			68.5ft: brownish yellow (10YR6/6), mottled light greenish gray (10YR8/1) 73.5ft: light gray (10YR7/2), very stiff, little sand, no HCl reaction, iron staining, thinly laminated
1.9	78.5	6	7	10	17	SS-18			1.9 — 78.5
-3.1	83.5	7	9	11	20	SS-19			Clayey SAND (SC), light gray (10YR7/2), firm, wet, little fines, no HCl reaction, carbonate nodules, organics -3.1 — 83.5
-8.1	88.5	39	50/0.4		89/0.9	SS-20			POORLY GRADED SAND with silt (SP-SM), very pale brown (10YR8/2), very dense, wet, few fines, strong HCl reaction, thin lenses of cemented sand -8.1 — 88.5
-13.1	93.5	8	8	11	19	SS-21			FAT CLAY (CH), light gray (10YR7/2), mottled yellowish brown (10YR5/8), very stiff, moist, no HCl reaction, carbonate nodules, iron staining, thinly laminated
-18.1	98.5	8	12	24	36	SS-22			93.5ft: very pale brown (10YR8/3), hard, some sand, strong HCl reaction -18.1 — 98.5
-28.1	108.5	48	50/0.5		98/1.0	SS-23			POORLY GRADED SAND (SP), very pale brown (10YR7/4), very dense, wet, fine to medium grained, few fines, strong HCl reaction -28.1 — 108.5
		7	10	12	22	SS-24			FAT CLAY with sand (CH), very pale brown (10YR7/4), very stiff, moist, little sand, weak HCl reaction, trace iron staining, trace mottling, thinly laminated

EXELON COL BORE EXELON-2.GPJ EXELON COL.GDT 6/12/08

MACTEC

BECHTEL PROJECT NO.: 25352	COUNTY Victoria	GEOLOGIST C. Gandy
SITE DESCRIPTION Exelon COL Project (Victoria Site)	MACTEC PROJECT NO.: 6468-07-1777	GROUND WATER (ft)
BORING NO. B-2150 / DRILL METHOD: Mud Rotary	SAMPLE METHODS: SPT	0 HR. ND
GROUND SURFACE ELEV. 80.4 ft (NAVD88) / NORTHING 13,412,560 US ft (NAD83)	EASTING 2,599,591 US ft (NAD83)	24 HR. ND
TOTAL DEPTH 150.0 ft / DRILL MACHINE CME-55 LC	DRILLER: D. White/O. Smith	HAMMER (ID) 140 lb. Auto (MEC 02)
DATE STARTED 11/8/07 / COMPLETED 11/9/07	CASING DEPTH: N/A	BITS USED: 2 7/8" Wing Bit

ELEV. (ft)	DEPTH (ft)	BLOW COUNT 0.5ft	0.5ft	0.5ft	BLOWS PER FOOT (0 20 40 60 80 100)	SAMP. NO.	MOI	LOG	SOIL AND ROCK DESCRIPTION
-31.8					Continued from previous page				
									FAT CLAY with sand (CH), very pale brown (10YR7/4), very stiff, moist, little sand, weak HCl reaction, trace iron staining, trace mottling, thinly laminated *(continued)*
-38.1	118.5								
		8	10	11	21	SS-25			118.5ft: light gray (10YR7/2), few sand, organics, trace carbonate nodules
-48.1	128.5								
		7	7	18	25	SS-26			128.5ft: light gray (5Y7/1), little sand, 2 sand seams each 0.3'-thick
-58.1	138.5								-58.1 / 138.5
		6	12	13	25	SS-27A/B			-58.8 / 139.2 Clayey SAND (SC), very pale brown (10YR8/2), very firm, wet, some fines, strong HCl reaction
									FAT CLAY (CH), very pale brown (10YR8/2), very stiff, moist, few sand, strong HCl reaction, iron staining, carbonate nodules
-68.1	148.5								-68.1 / 148.5
		8	20	30	50	SS-28			-69.6 / 150.0 POORLY GRADED SAND with silt (SP-SM), very pale brown (10YR7/3), dense, wet, few fines, no HCl reaction
									Boring Terminated at Elevation -69.6 ft

EXELON COL BORE EXELON~2.GPJ EXELON COL.GDT 6/12/08

MACTEC

GEOTECHNICAL BORING LOG

Prepared By WBD Date 6-16-08

Checked By KAW Date 7-10-08

BECHTEL PROJECT NO.: 25352	COUNTY Victoria	GEOLOGIST J. Liles	
SITE DESCRIPTION Exelon COL Project	MACTEC PROJECT NO.: 6468-07-1777	GROUND WATER (ft)	
BORING NO. B-2151	DRILL METHOD: Mud Rotary	SAMPLE METHODS: SPT	0 HR. ND
GROUND SURFACE ELEV. 80.4 ft (NAVD88)	NORTHING 13,412,637 US ft (NAD83)	EASTING 2,599,654 US ft (NAD83)	24 HR. ND
TOTAL DEPTH 200.0 ft	DRILL MACHINE CME-550	DRILLER: L. Carter/C. Harden	HAMMER (ID) 140 lb. Auto (MEC 03)
DATE STARTED 12/13/07	COMPLETED 12/14/07	CASING DEPTH: 3.5 ft	BITS USED: 2 15/16" Drag Bit

ELEV. (ft)	DEPTH (ft)	BLOW COUNT 0.5ft	0.5ft	0.5ft	BLOWS PER FOOT (0 20 40 60 80 100)	SAMP. NO.	MOI	LOG	SOIL AND ROCK DESCRIPTION
80.4					Ground Surface				
80.4	0.0	3	5	8	13	SS-1			FAT CLAY with sand (CH), very dark gray (2.5Y3/1), stiff, moist, fine to medium grained sand, no HCl reaction, organics
76.9	3.5	14	16	15	31	SS-2			Sandy LEAN CLAY (CL), dark gray (2.5Y4/1), hard, fine to coarse grained sand, fine gravel, strong HCl reaction, carbonate nodules
74.4	6.0	4	6	7	13	SS-3			FAT CLAY with sand (CH), light brownish gray (2.5Y6/2), stiff, moist, fine to medium grained sand, strong HCl reaction, organics
71.9	8.5	10	10	13	23	SS-4			LEAN CLAY with sand (CL), light brown gray (2.5Y6/2), very stiff, wet, fine to medium grained sand
69.4	11.0	7	11	13	24	SS-5			Sandy LEAN CLAY (CL), light brownish gray, very stiff, moist, fine to medium grained sand, strong HCl reaction
66.9	13.5	10	13	17	30	SS-6			
60.9	19.5	7	7	12	19	SS-7			FAT CLAY (CH), light gray (2.5Y7/1), very stiff, moist, fine to medium grained sand, no HCl reaction, few carbonate nodules, organics
55.9	24.5	6	6	9	15	SS-8			24.5ft: brownish yellow (10YR6/6), stiff, moist, strong HCl reaction
50.9	29.5	7	9	11	20	SS-9			29.5ft: light yellowish brown (10YR6/4), very stiff, organics
45.9	34.5	6	8	10	18	SS-10			34.5ft: strong brown (7.5YR5/6)
40.9	39.5	5	6	9	15	SS-11			39.5ft: stiff, organics
35.9	44.5	5	7	9	16	SS-12			44.5ft: light yellowish brown (10YR6/4 to 2.5Y6/3), very stiff
30.9	49.5	7	9	11	20	SS-13			LEAN CLAY with sand (CL), light yellowish brown (10YR6/4), very stiff, moist, fine to coarse grained sand, no HCl reaction, few carbonate nodules, organics
25.9	54.5	13	12	12	24	SS-14			Clayey SAND (SC), light gray (2.5Y7/1), very firm, moist, fine to medium grained sand

EXELON COL BORE EXELON-2.GPJ EXELON COL.GDT 6/16/08

MACTEC

BECHTEL PROJECT NO.: 25352		COUNTY Victoria	GEOLOGIST J. Liles
SITE DESCRIPTION Exelon COL Project		MACTEC PROJECT NO.: 6468-07-1777	GROUND WATER (ft)
BORING NO. B-2151	DRILL METHOD: Mud Rotary	SAMPLE METHODS: SPT	0 HR. ND
GROUND SURFACE ELEV. 80.4 ft (NAVD88)	NORTHING 13,412,637 US ft (NAD83)	EASTING 2,599,654 US ft (NAD83)	24 HR. ND
TOTAL DEPTH 200.0 ft	DRILL MACHINE CME-550	DRILLER: L. Carter/C. Harden	HAMMER (ID) 140 lb. Auto (MEC 03)
DATE STARTED 12/13/07	COMPLETED 12/14/07	CASING DEPTH: 3.5 ft	BITS USED: 2 15/16" Drag Bit

ELEV. (ft)	DEPTH (ft)	BLOW COUNT 0.5ft	0.5ft	0.5ft	BLOWS PER FOOT (0 20 40 60 80 100)	SAMP. NO.	MOI	LOG	SOIL AND ROCK DESCRIPTION
24.3					Continued from previous page				
20.9	59.5								Clayey SAND (SC), light gray (2.5Y7/1), very firm, moist, fine to medium grained sand *(continued)*
15.9	64.5	8	10	10	20	SS-15			59.5ft: firm, fine to coarse grained sand, fine gravel, strong HCl reaction, organics
10.9	69.5	33	25	22	47	SS-16			64.5ft: light brownish gray (2.5Y6/2), dense, wet, carbonate nodules, no HCl reaction, (visual)
5.9	74.5	6	7	9	16	SS-17			10.9 — 69.5: FAT CLAY (CH), light brownish gray (10YR6/2), very stiff, moist, fine to medium grained sand, carbonate nodules, strong HCl reaction, organics
0.9	79.5	7	11	12	23	SS-18			5.9 — 74.5: LEAN CLAY (CL), light brownish gray (10YR6/2), very stiff, moist, fine to medium grained sand, carbonate nodules, strong HCl reaction
-4.1	84.5	5	10	11	21	SS-19			0.9 — 79.5: Clayey SAND (SC), light gray (2.5Y7/2), very firm, moist, fine to medium grained sand, no HCl reaction (visual)
-9.1	89.5	12	13	14	27	SS-20			84.5ft: light gray (2.5Y7/2), wet, fine to coarse grained sand, no HCl reaction (visual)
-14.1	94.5	6	11	14	25	SS-21			-9.1 — 89.5: Sandy LEAN CLAY (CL), light gray (2.5Y7/2), very stiff, moist, fine to medium grained sand, carbonate nodules, strong HCl reaction, organics
-19.1	99.5	41	37	39	76	SS-22			94.5ft: hard, fine to coarse grained sand (visual)
-29.1	109.5	35	49	50/0.3	99/0.8	SS-23			-19.1 — 99.5: Clayey SAND (SC), pale yellow (2.5Y7/3), very dense, wet, fine to medium grained sand, strong HCl reaction (visual)
									-20.6 — 101.0: FAT CLAY (CH) light gray (5Y7/2), very stiff, moist, fine to medium grained sand, carbonate nodules, strong to no HCl reaction
		7	8	11	19	SS-24			

EXELON COL BORE EXELON-2.GPJ EXELON COL.GDT 6/16/08

MACTEC

BECHTEL PROJECT NO.: 25352	COUNTY Victoria	GEOLOGIST J. Liles	
SITE DESCRIPTION Exelon COL Project	MACTEC PROJECT NO.: 6468-07-1777	GROUND WATER (ft)	
BORING NO. B-2151	DRILL METHOD: Mud Rotary	SAMPLE METHODS: SPT	0 HR. ND
GROUND SURFACE ELEV. 80.4 ft (NAVD88)	NORTHING 13,412,637 US ft (NAD83)	EASTING 2,599,654 US ft (NAD83)	24 HR. ND
TOTAL DEPTH 200.0 ft	DRILL MACHINE CME-550	DRILLER: L. Carter/C. Harden	HAMMER (ID) 140 lb. Auto (MEC 03)
DATE STARTED 12/13/07	COMPLETED 12/14/07	CASING DEPTH: 3.5 ft	BITS USED: 2 15/16" Drag Bit

ELEV. (ft)	DEPTH (ft)	BLOW COUNT 0.5ft	0.5ft	0.5ft	BLOWS PER FOOT (0 20 40 60 80 100)	SAMP. NO.	MOI	LOG	SOIL AND ROCK DESCRIPTION
-31.8					Continued from previous page				
									FAT CLAY (CH) light gray (5Y7/2), very stiff, moist, fine to medium grained sand, carbonate nodules, strong to no HCl reaction *(continued)*
-39.1	119.5								-39.1 — 119.5
		8	8	12	20	SS-25			FAT CLAY with sand (CH), light gray (5Y7/2), very stiff, moist, fine to medium grained sand, carbonate nodules, strong HCl reaction
-44.1	124.5								LEAN CLAY with sand (CL), light gray (5Y7/2), hard, moist, fine to medium grained sand
-49.1	129.5								
		7	8	25	33	SS-26			-50.3 — 130.7 Field notes do not indicate that SS-26 was split into separate jars
									POORLY GRADED SAND with clay (SP-SC), light gray (2.5Y7/2), dense, wet, fine to medium grained sand, no HCl reaction (visual)
-59.2	139.6								
		19	26	24	50	SS-27			
-69.2	149.6								
		6	13	14	27	SS-28			149.6ft: very firm, wet, fine gravel, carbonate nodules, strong HCl reaction, organics
-79.2	159.6								-79.2 — 159.6
		24	34	38	72	SS-29			POORLY GRADED SAND (SP), light gray (10YR7/2), very dense, wet, fine grained, trace fines, no HCl reaction, trace ferrous flakes (visual)

EXELON COL BORE EXELON-2.GPJ EXELON COL.GDT 6/16/08