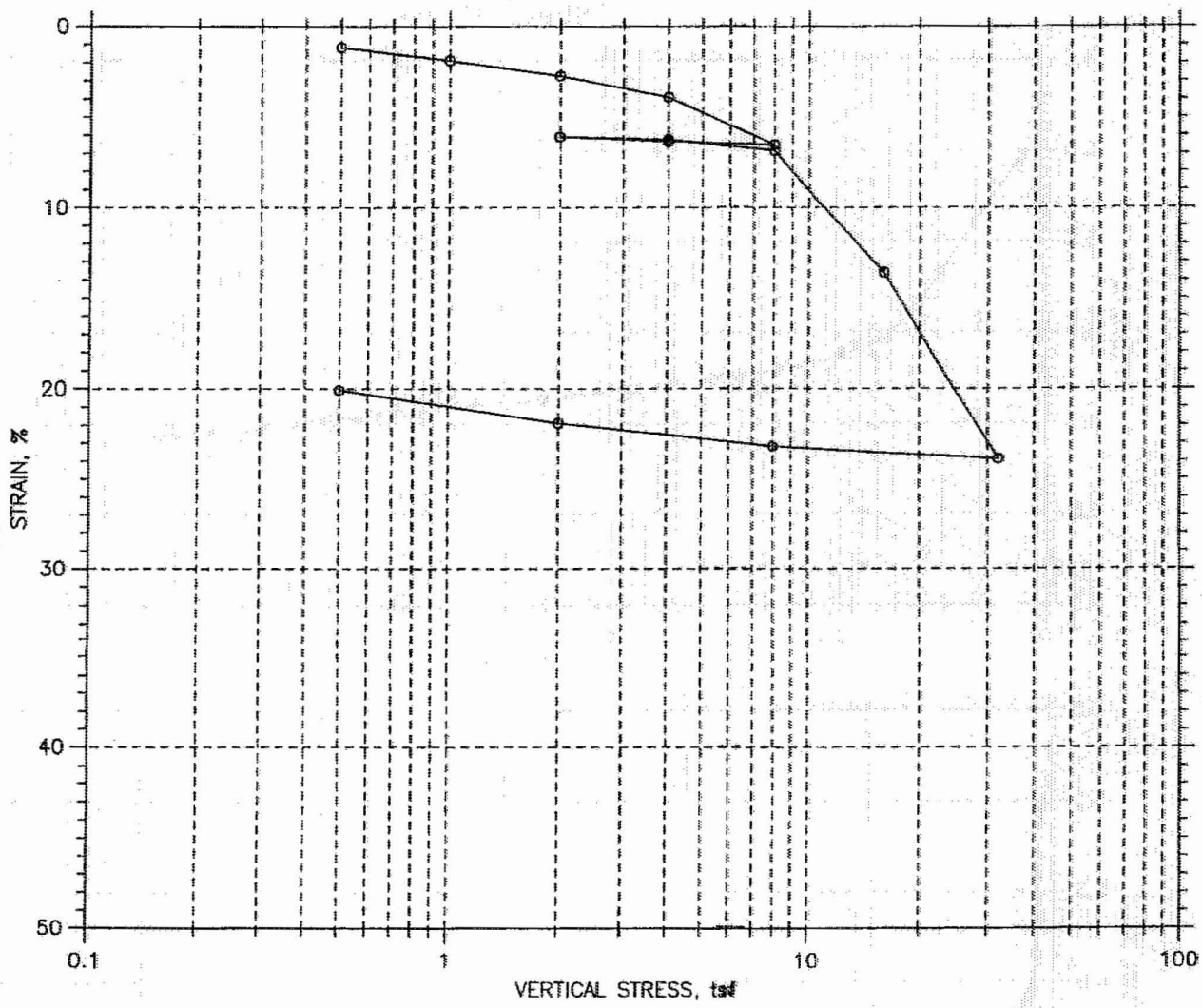
# CONSOLIDATION TEST DATA

SUMMARY REPORT




| | | | | | Before Test | After Test |
|---|---|---|---|---|---|---|
| Overburden Pressure: --- | | | | Water Content, % | 44.40 | 37.22 |
| Preconsolidation Pressure: 10 tsf | | | | Dry Unit Weight, pcf | 67.94 | 84.99 |
| Compression Index: --- | | | | Saturation, % | 79.76 | 100.00 |
| Diameter: 2.5 in | | Height: 1 in | | Void Ratio | 1.54 | 1.03 |
| LL: 72 | PL: 45 | PI: 27 | GS: 2.76 | | | |

| | | | |
|---|---|---|---|
| GeoTesting express, a subsidiary of Geocomp Corporation | Project: Calvert Cliffs Nuclear | Location: Calvert County, MD | Project No.: GTX-6880 |
| | Boring No.: B-328 | Tested By: md | Checked By: njh |
| | Sample No.: S-28 | Test Date: 09/09/06 | Depth: 123.5-125.1 |
| | Test No.: C-6 | Sample Type: tube | Elevation: --- |
| | Description: Moist, olive gray silt with sand (MH), 83% passing #200 sieve, inundated @ 0.5 tsf | | |
| | Remarks: System G - Compression Ratio: 0.38, Recompression Ratio: 0.02 | | |

Thu, 09-NOV-2006 16:17:04

# CONSOLIDATION TEST DATA

Project: Calvert Cliffs Nuclear
Boring No.: B-328
Sample No.: S-28
Test No.: C-6

Location: Calvert County, MD
Tested By: md
Test Date: 09/09/06
Sample Type: tube

Project No.: GTX-6880
Checked By: njh
Depth: 123.5-125.t
Elevation: ---

Soil Description: Moist, olive gray silt with sand (MH), 83% passing #200 sieve, inundated @ 0.5 tsf
Remarks: System G - Compression Ratio: 0.38, Recompression Ratio: 0.02

Measured Specific Gravity: 2.76
Initial Void Ratio: 1.54
Final Void Ratio: 1.03

Liquid Limit: 72
Plastic Limit: 45
Plasticity Index: 27

Initial Height: 1.00 in
Specimen Diameter: 2.50 in

| | Before Consolidation | | After Consolidation | |
|---|---|---|---|---|
| | Trimmings | Specimen+Ring | Specimen+Ring | Trimmings |
| Container ID | 1225 | RING | | 1111 |
| Wt. Container + Wet Soil, gm | 172.09 | 342.88 | 336.6 | 127.46 |
| Wt. Container + Dry Soil, gm | 121.87 | 304.02 | 304.02 | 95.07 |
| Wt. Container, gm | 8.37 | 216.48 | 216.48 | 8.05 |
| Wt. Dry Soil, gm | 113.5 | 87.537 | 87.537 | 87.02 |
| Water Content, % | 44.25 | 44.40 | 37.22 | 37.22 |
| Void Ratio | --- | 1.54 | 1.03 | --- |
| Degree of Saturation, % | --- | 79.76 | 100.00 | --- |
| Dry Unit Weight, pcf | --- | 67.936 | 84.99 | --- |

# CONSOLIDATION TEST DATA

Project: Calvert Cliffs Nuclear
Boring No.: B-328
Sample No.: S-28
Test No.: C-6

Location: Calvert County, MD
Tested By: md
Test Date: 09/09/06
Sample Type: tube

Project No.: GTX-6880
Checked By: njh
Depth: 123.5-125.t
Elevation: ---

Soil Description: Moist, olive gray silt with sand (MH), 83% passing #200 sieve, inundated @ 0.5 tsf
Remarks: System G - Compression Ratio: 0.38, Recompression Ratio: 0.02

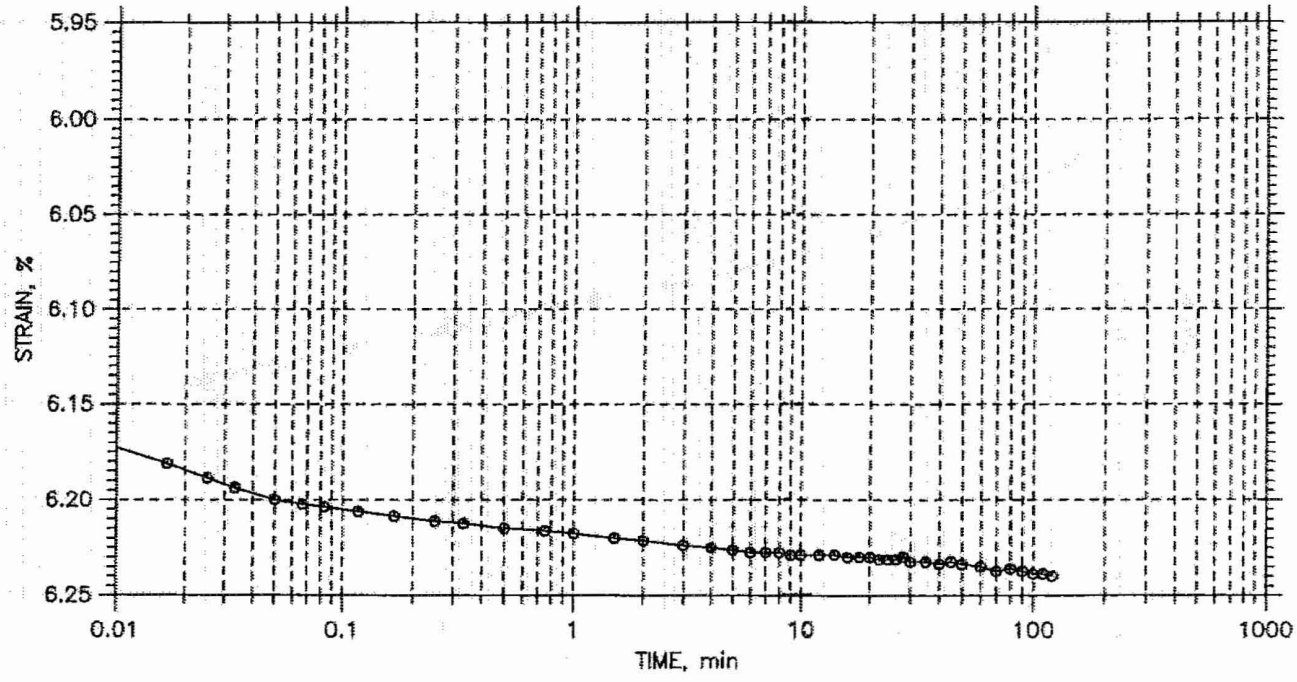
| | Applied Stress tsf | Final Displacement in | Void Ratio | Strain at End % | T50 Fitting Sq.Rt. min | T50 Fitting Log min | Coefficient of Consolidation Sq.Rt. in^2/sec | Coefficient of Consolidation Log in^2/sec | Coefficient of Consolidation Ave. in^2/sec |
|---|---|---|---|---|---|---|---|---|---|
| 1 | 0.5 | 0.01171 | 1.507 | 1.17 | 0.0 | 0.0 | 2.77e-002 | 0.00e+000 | 2.77e-002 |
| 2 | 1 | 0.01889 | 1.488 | 1.89 | 0.0 | 0.0 | 2.06e-002 | 3.21e-002 | 2.51e-002 |
| 3 | 2 | 0.02737 | 1.467 | 2.74 | 0.0 | 0.0 | 5.02e-002 | 4.00e-002 | 4.45e-002 |
| 4 | 4 | 0.03904 | 1.437 | 3.90 | 0.0 | 0.0 | 2.18e-002 | 5.35e-002 | 3.10e-002 |
| 5 | 8 | 0.06528 | 1.371 | 6.53 | 0.1 | 0.0 | 7.44e-003 | 4.97e-002 | 1.29e-002 |
| 6 | 4 | 0.06356 | 1.375 | 6.36 | 0.0 | 0.0 | 1.67e-001 | 0.00e+000 | 1.67e-001 |
| 7 | 2 | 0.061 | 1.382 | 6.10 | 0.0 | 0.0 | 7.35e-002 | 0.00e+000 | 7.35e-002 |
| 8 | 4 | 0.0624 | 1.378 | 6.24 | 0.0 | 0.0 | 1.47e-001 | 0.00e+000 | 1.47e-001 |
| 9 | 8 | 0.06856 | 1.362 | 6.86 | 0.7 | 0.0 | 9.70e-004 | 0.00e+000 | 9.70e-004 |
| 10 | 16 | 0.136 | 1.191 | 13.60 | 0.3 | 0.0 | 2.27e-003 | 1.92e-002 | 4.06e-003 |
| 11 | 32 | 0.2389 | 0.930 | 23.89 | 0.6 | 0.3 | 8.66e-004 | 1.71e-003 | 1.15e-003 |
| 12 | 8 | 0.2319 | 0.948 | 23.19 | 0.0 | 0.0 | 6.63e-002 | 0.00e+000 | 6.63e-002 |
| 13 | 2 | 0.2189 | 0.981 | 21.89 | 0.7 | 0.0 | 7.08e-004 | 0.00e+000 | 7.08e-004 |
| 14 | 0.5 | 0.2007 | 1.027 | 20.07 | 2.9 | 3.4 | 1.78e-004 | 1.52e-004 | 1.64e-004 |

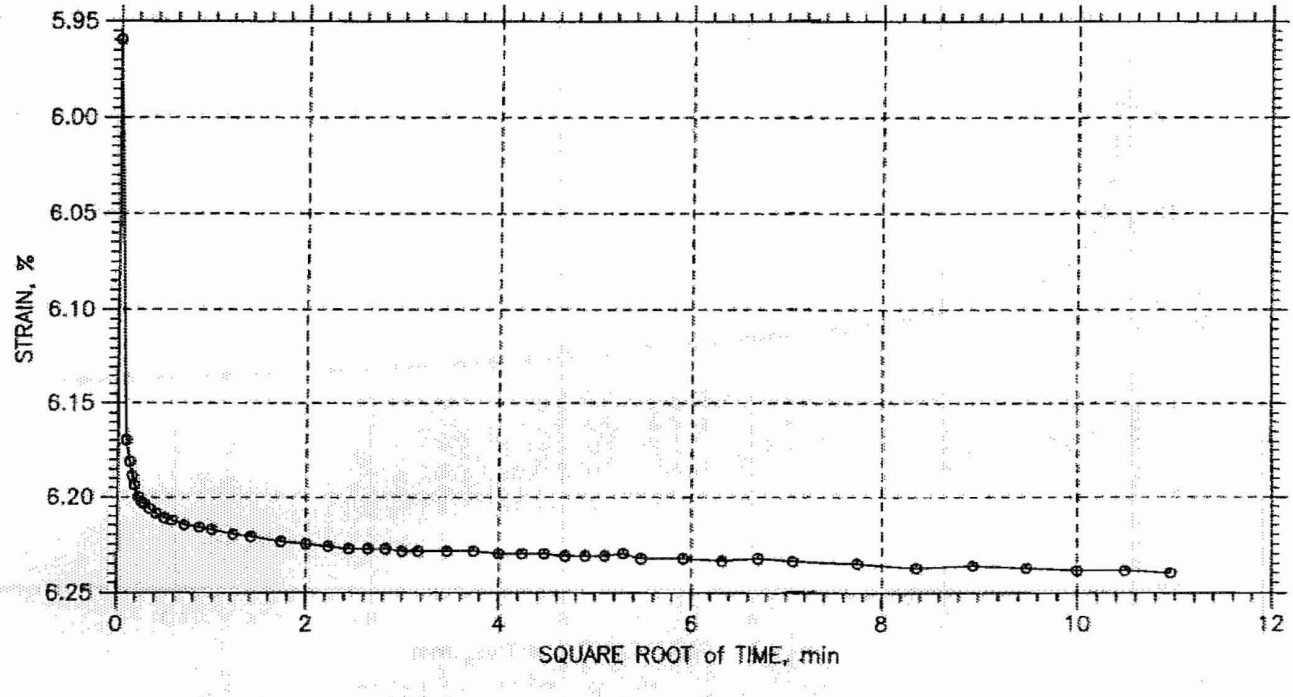
# CONSOLIDATION TEST DATA

TIME CURVES

Constant Load Step: 8 of 14

Stress: 4. tsf




| | | | |
|---|---|---|---|
| GeoTesting express<br>a subsidiary of Geocomp Corporation | Project: Calvert Cliffs Nuclear | Location: Calvert County, MD | Project No.: GTX-6880 |
| | Boring No.: B-328 | Tested By: md | Checked By: njh |
| | Sample No.: S-28 | Test Date: 09/09/06 | Depth: 123.5-125.t |
| | Test No.: C-6 | Sample Type: tube | Elevation: --- |
| | Description: Moist, olive gray silt with sand (MH), 83% passing #200 sieve, inundated @ 0.5 tsf | | |
| | Remarks: System G - Compression Ratio: 0.38, Recompression Ratio: 0.02 | | |

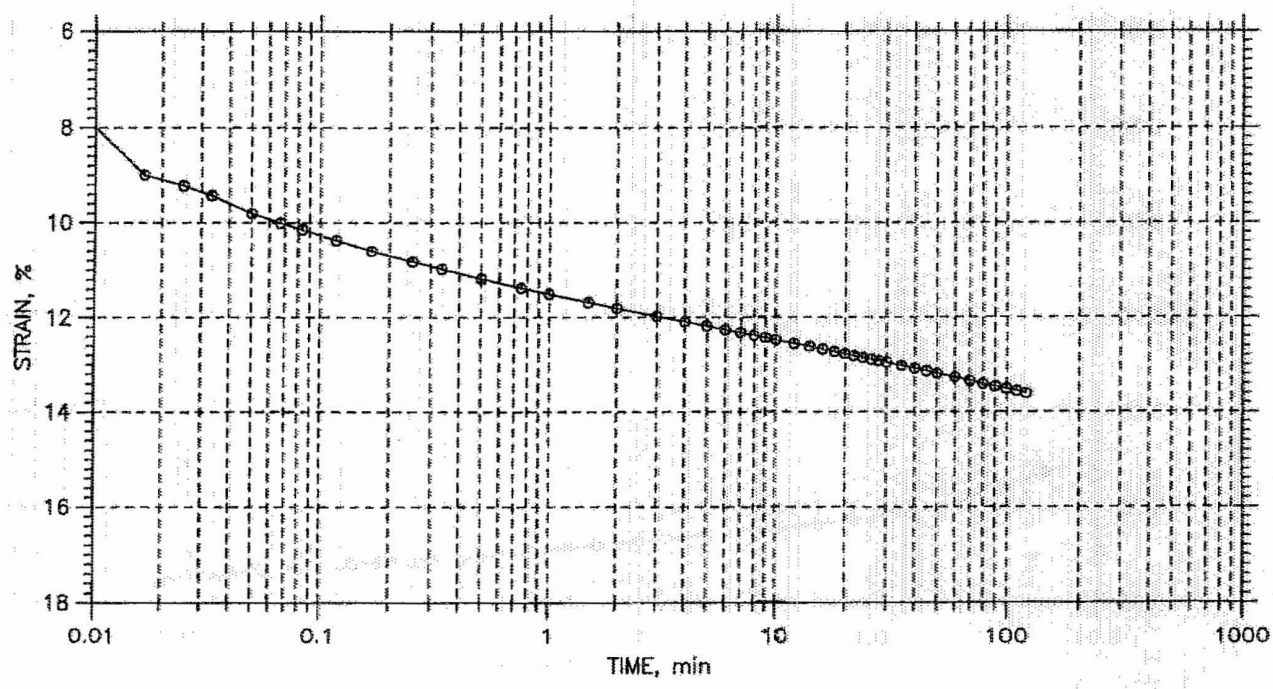
Thu, 09-NOV-2006 16:17:23

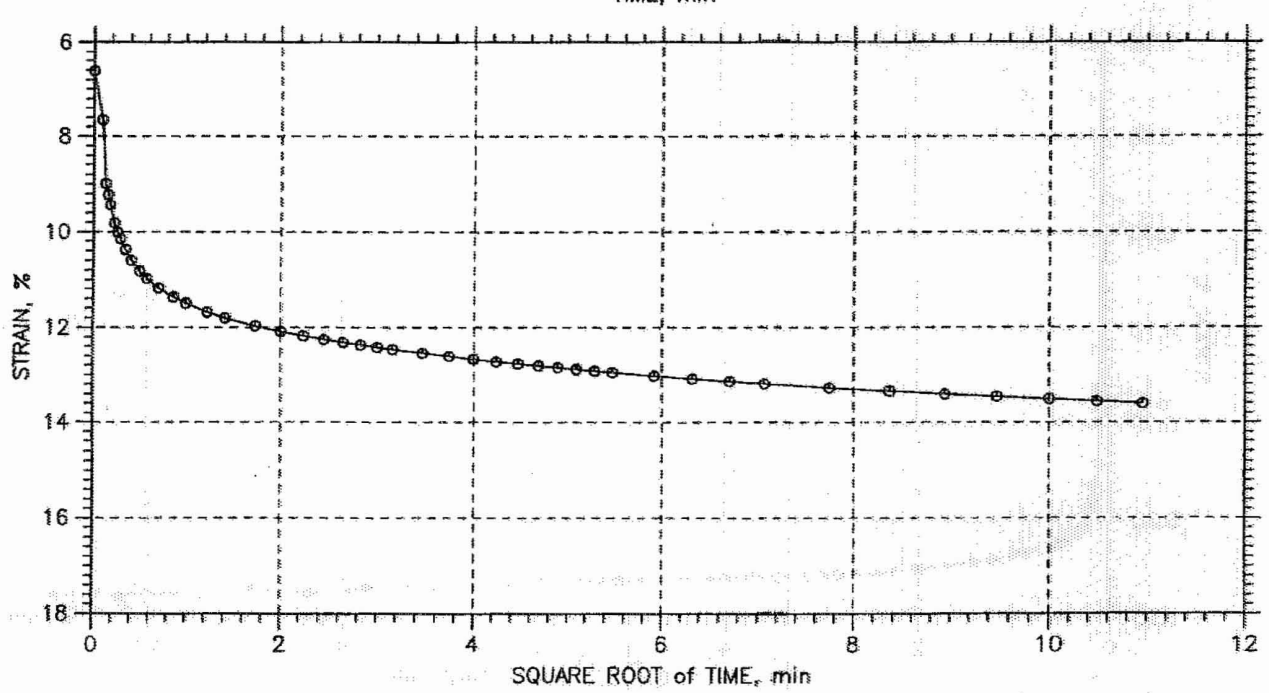
# CONSOLIDATION TEST DATA

TIME CURVES

Constant Load Step: 10 of 14

Stress: 16. tsf




| | | | |
|---|---|---|---|
| GeoTesting express<br>a subsidiary of Geocomp Corporation | Project: Calvert Cliffs Nuclear | Location: Calvert County, MD | Project No.: GTX-6880 |
| | Boring No.: B-328 | Tested By: md | Checked By: njh |
| | Sample No.: S-28 | Test Date: 09/09/06 | Depth: 123.5-125.1 |
| | Test No.: C-6 | Sample Type: tube | Elevation: --- |
| | Description: Moist, olive gray silt with sand (MH), 83% passing #200 sieve, inundated @ 0.5 tsf | | |
| | Remarks: System G - Compression Ratio: 0.38, Recompression Ratio: 0.02 | | |

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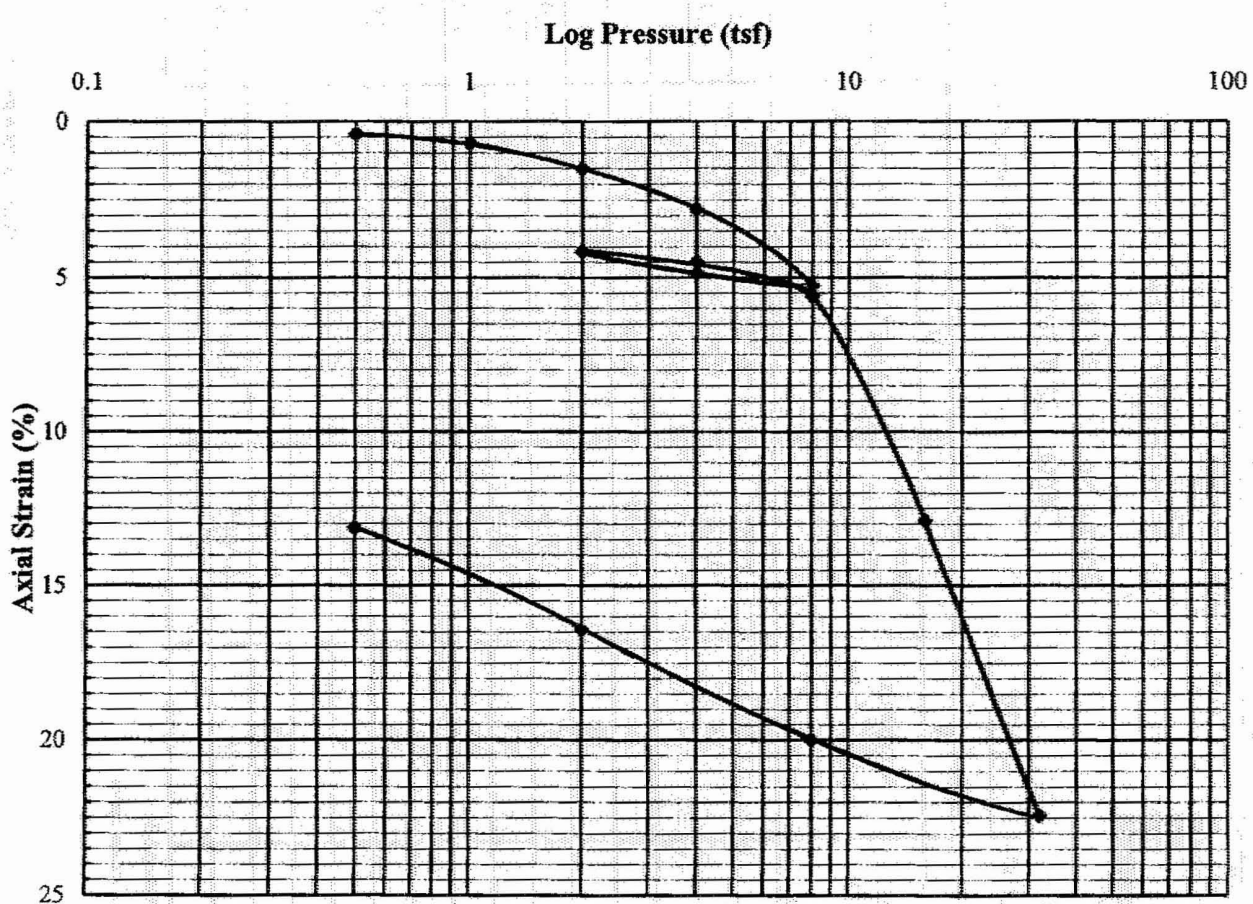


REVISED FORM FOR
NCR NO. 25237-NCR-028
2/12/2007

| | | | | | |
|---|---|---|---|---|---|
| **Probable Preconsolidation Pressure (Pp), tsf:** | *9.3* | | | **Recompression Ratio (Cεr):** | *0.021* |
| **Type of Specimen:** | *Tube Sample* | | | **Compression Ratio (Cεc):** | *0.316* |
| **Description:** | *FAT CLAY with sand (CH) - gray* | | | | **Initial** / **Final** |
| | | | | **Water Content, %** | *39.5* / *31.4* |
| **LL:** *52* | **PI:** *33* | **Gs:** *2.82* | **$P_o'$ (tsf):** *1.15* | **Void Ratio** | *1.15* / *0.87* |
| **% < No. 200:** | *85.3* | **Test Method:** | *ASTM D2435 Method A* | **Saturation, %** | *97* / *100* |
| **Test Condition:** | *Inundated @ 2 tsf* | | | **Dry Unit Weight, pcf** | *81.7* / *94.0* |

**Remarks:** Coefficient of Consolidation, Cv, equals 196 and 17 ft2/yr at average pressures of 3 and 12 tsf (square root of time method).

**Average Water Content of Trimmings, %:** *37.4*

**Project:** Calvert Cliffs Nuclear Power Plant

| | | | |
|---|---|---|---|
| **Location:** | *Calvert County, MD* | | |
| **Boring:** | *B-333* | **Schnabel No.:** | *06120048* |
| **Depth:** | *28.5-30.5ft.* | **Elevation:** | *61 to 59 ft* |
| **Date:** | *11/21/2006* | **Reviewed by:** | *CJS* |

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**Consolidation Test Report**

# Consolidation Test Data Sheet

Consolidometer ID: 3

11/21/06

REVISED FORM FOR
NCR NO. 25237-NCR-028
2/12/07

Schnabel Contract: *06120048*

Test Method: *ASTM D2435 Method A*

Project: *Calvert Cliffs Nuclear Power Plant*

Test Condition: *Inundated @ 2 tsf*

Initial Height of Specimen ($H_o$), in.: 0.7497

Boring No.: *B-333*

Height of Solids ($H_s$), in.: 0.3481

Depth: *28.5-30.5ft.*

Seating Press. (tsf): 0.05

Initial Dial Gauge Reading ($D_o$), in.: -0.0010

Reviewed by: CJS

| Pressure, P (tsf) | Time Readings Required | Date Load Applied | Time Load Applied | Load Applied By | A: Final[1] Dial Reading, $D_{fi}$ x $10^{-4}$ in. | B: Apparatus Correction[2], $D_{ci}$ x $10^{-4}$ in. | C: Cumulative Change in Height[3], $\Delta H_i$ in. | D: Height of Voids[4], $H_{vi}$ in. | Vertical Strain[5], $\varepsilon_i$ (%) | Void Ratio[6], $e_i$ |
|---|---|---|---|---|---|---|---|---|---|---|
| 0.5 | | 10/14/2006 | 9:25 | CJS | 29 | 8 | 0.0031 | 0.3985 | 0.41 | 1.145 |
| 1 | | 10/16/2006 | 9:00 | DWC | 56 | 13 | 0.0053 | 0.3963 | 0.71 | 1.138 |
| 2 | | 10/17/2006 | 9:00 | DWC | 120 | 17 | 0.0113 | 0.3903 | 1.51 | 1.121 |
| 4 | | 10/18/2006 | 9:00 | DWC | 224 | 25 | 0.0209 | 0.3807 | 2.79 | 1.094 |
| 8 | | 10/19/2006 | 9:00 | DWC | 424 | 39 | 0.0395 | 0.3621 | 5.27 | 1.040 |
| 4 | | 10/20/2006 | 9:00 | DWC | 379 | 25 | 0.0364 | 0.3652 | 4.86 | 1.049 |
| 2 | | 10/21/2006 | 9:00 | DWC | 319 | 17 | 0.0312 | 0.3704 | 4.16 | 1.064 |
| 4 | | 10/23/2006 | 9:00 | DWC | 352 | 25 | 0.0337 | 0.3679 | 4.50 | 1.057 |
| 8 | | 10/24/2006 | 9:00 | DWC | 450 | 39 | 0.0421 | 0.3595 | 5.62 | 1.033 |
| 16 | | 10/25/2006 | 9:00 | DWC | 1005 | 48 | 0.0967 | 0.3049 | 12.90 | 0.876 |
| 32 | | 10/26/2006 | 9:00 | DWC | 1727 | 56 | 0.1681 | 0.2335 | 22.42 | 0.671 |
| 8 | | 10/27/2006 | 9:00 | DWC | 1528 | 39 | 0.1499 | 0.2517 | 19.99 | 0.723 |
| 2 | | 10/30/2006 | 1:00 | DWC | 1239 | 17 | 0.1232 | 0.2784 | 16.43 | 0.800 |
| 0.5 | | 10/31/2006 | 1:00 | DWC | 983 | 8 | 0.0985 | 0.3031 | 13.14 | 0.871 |
| | | | | | | | | | | |

Notes:
1. "Final" based on test method; 24 hrs for Method A, end of primary for Method B.
2. Correction value, for the current pressure, from the consolidometer's calibration curve.
3. $\Delta H = D_{fi} - D_o - D_{ci}$ = Col. A - $D_o$ - Col. B
4. $H_{vi} = (H_o - H_s) - \Delta H$
5. $\varepsilon_i = (\Delta H / H_o) \times 100$ = (Col. C / $H_o$) x 100
6. $e_i = H_{vi} / Hs$ = Col. D / Hs

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# Load Time Readings

11/21/06

Project: Calvert Cliffs Nuclear Power Plant
Schnabel Contract: 06120048
Boring No.: B-333 Depth: 28.5-30.5ft.
Consol. ID: 3 Reviewed by: CJS

| Elapsed Time (min.) | Dial Guage Readings (inches) | | | | | |
|---|---|---|---|---|---|---|
| | 4 tsf Reload 10/23/2006 | 32 tsf Load 10/26/2006 | X tsf Load Date | X tsf Load Date | X tsf Load Date | X tsf Load Date |
| 0.1 | 0.0174 | 0.0441 | | | | |
| 0.25 | 0.0175 | 0.0457 | | | | |
| 0.5 | 0.0176 | 0.0473 | | | | |
| 1 | 0.0177 | 0.0496 | | | | |
| 2 | 0.0178 | 0.0525 | | | | |
| 4 | 0.0178 | 0.0561 | | | | |
| 8 | 0.0178 | 0.0608 | | | | |
| 15 | 0.0179 | 0.0657 | | | | |
| 30 | 0.0179 | 0.0715 | | | | |
| 60 | 0.0179 | 0.0770 | | | | |
| 120 | 0.0180 | 0.0817 | | | | |
| 240 | 0.0180 | 0.0856 | | | | |
| 480 | 0.0181 | 0.0890 | | | | |
| 720 | 0.0181 | 0.0907 | | | | |
| 960 | 0.0181 | 0.0918 | | | | |
| 1200 | 0.0181 | 0.0926 | | | | |
| 1440 | 0.0181 | 0.0933 | | | | |
| 1680 | | | | | | |
| 1920 | | | | | | |
| 2160 | | | | | | |
| 2400 | | | | | | |
| 2640 | | | | | | |
| 2880 | | | | | | |
| | | | | | | |
| | | | | | | |

Schnabel Engineering

# Consolidation Time Curves

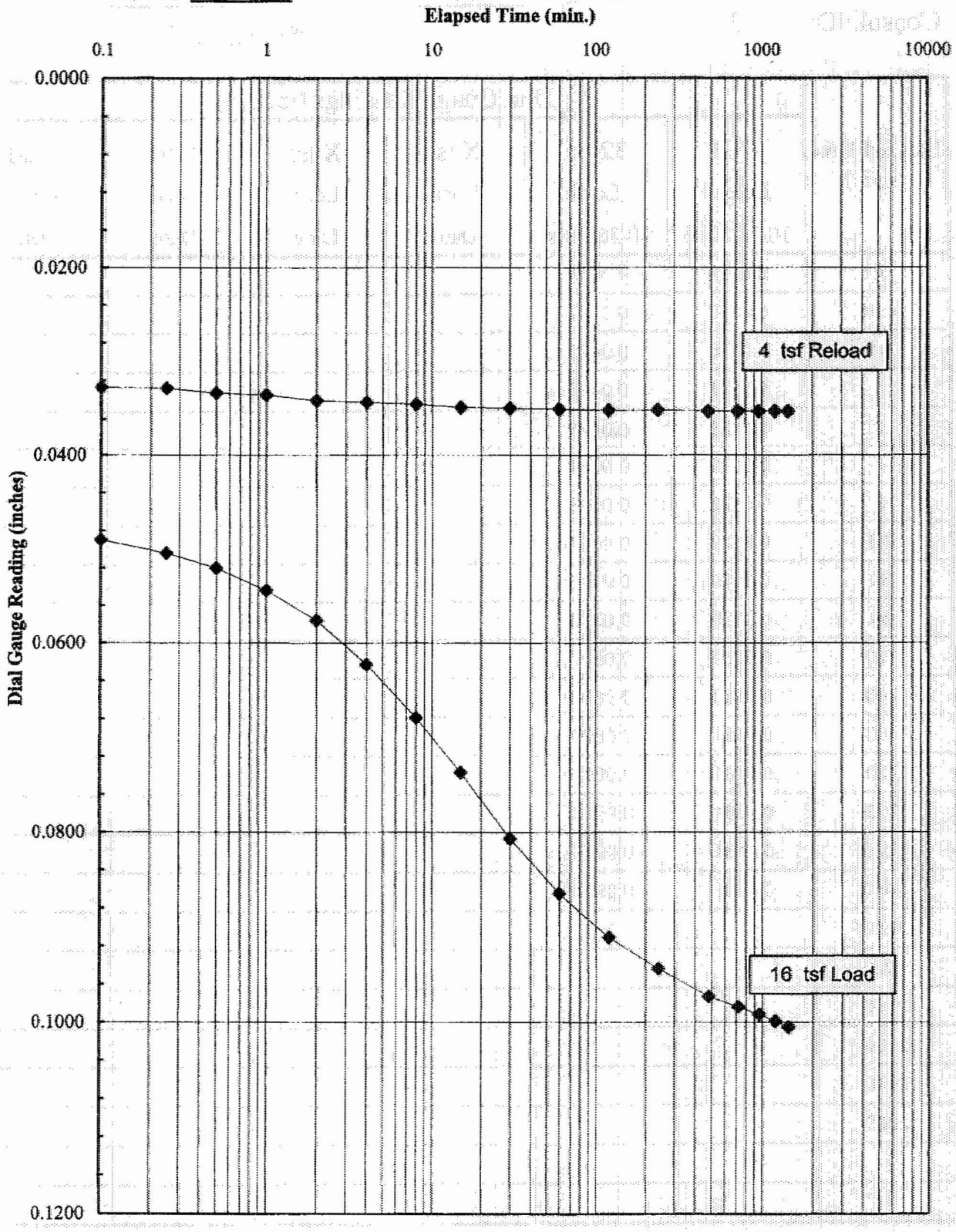
11/21/06

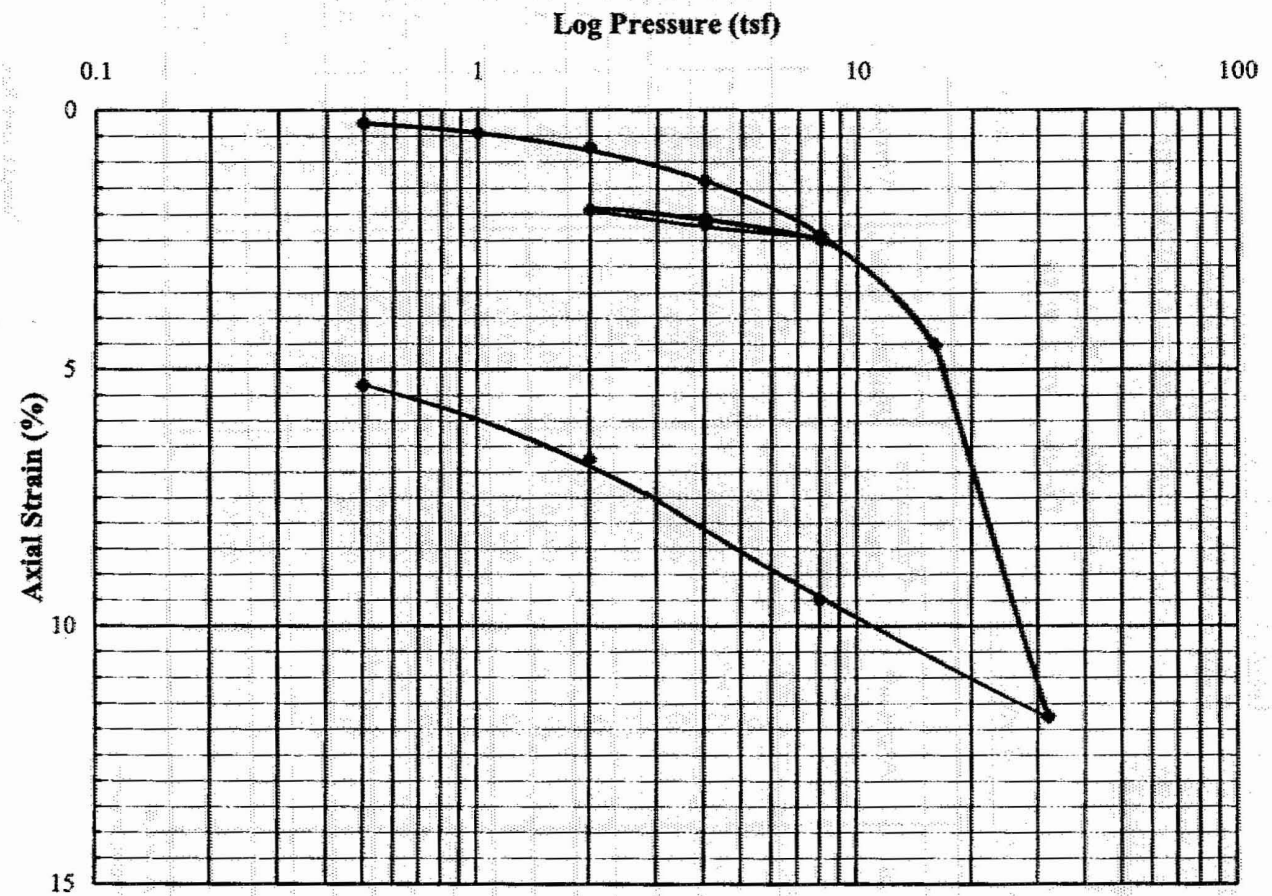
Project: Calvert Cliffs Nuclear Power Plant

Schnabel Contract: 06120048

Boring No.: B-333 Depth: 28.5-30.5ft.

Reviewed by: CJS






REVISED FORM FOR
NCR NO. 25237-NCR-028
2/12/07

| | | | | | |
|---|---|---|---|---|---|
| **Probable Preconsolidation Pressure (Pp), tsf:** | *15.2* | | | **Recompression Ratio (Cεr):** | *0.009* |
| **Type of Specimen:** | *Tube Sample* | | | **Compression Ratio (Cεc):** | *0.240* |
| **Description:** | *FAT CLAY (CH) - gray* | | | | **Initial** / **Final** |
| | | | | **Water Content, %** | *37.2* / *34.9* |
| **LL:** *61* | **PI:** *38* | **Gs:** *2.85* | **$P_c'$ (tsf):** *1.40* | **Void Ratio** | *1.10* / *0.99* |
| **% < No. 200:** *98.8* | | **Test Method:** | *ASTM D2435 Method A* | **Saturation, %** | *96* / *100* |
| **Test Condition:** | *Inundated @ 2.0tsf* | | | **Dry Unit Weight, pcf** | *84.6* / *89.3* |

**Remarks:** Coefficient of Consolidation, Cv, equals 279 and 34 ft2/yr at average pressures of 3 and 16 tsf (square root of time method).

**Average Water Content of Trimmings, %:** *32.8*

**Project:** Calvert Cliffs Nuclear Power Plant

| | | | |
|---|---|---|---|
| **Location:** | *Calvert County, MD* | | |
| **Boring:** | *B-333* | **Schnabel No.:** | *06120048* |
| **Depth:** | *38.5-40.5ft.* | **Elevation:** | *51 to 49 ft* |
| **Date:** | *11/21/2006* | **Reviewed by:** | *CJS* |

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**Consolidation Test Report**

# Consolidation Test Data Sheet

Consolidometer ID: 3

11/21/06

REVISED FORM FOR
NCR NO. 25237-NCR-028
2/12/2007

Schnabel Contract: *06120048*

Test Method: *ASTM D2435 Method A*

Project: *Calvert Cliffs Nuclear Power Plant*

Test Condition: *Inundated @ 2.0tsf*

Initial Height of Specimen ($H_o$), in.: 0.7504

Boring No.: *B-333*

Height of Solids ($H_s$), in.: 0.3569

Depth: *38.5-40.5ft.*

Seating Press. (tsf): 0.05

Initial Dial Gauge Reading ($D_o$), in.: -0.0002

Reviewed by: CJS

| Pressure, P (tsf) | TimeReadings Required | Date Load Applied | Time Load Applied | Load Applied By | A<br>Final[1] Dial Reading, $D_{fi}$ x $10^{-4}$ in. | B<br>Apparatus Correction[2], $D_{ci}$ x $10^{-4}$ in. | C<br>Cumulative Change in Height[3], $\Delta H_i$ in. | D<br>Height of Voids[4], $H_{vi}$ in. | Vertical Strain[5], $\varepsilon_i$ (%) | Void Ratio[6], $e_i$ |
|---|---|---|---|---|---|---|---|---|---|---|
| 0.5 | | 10/25/2006 | 9:10 | DWC | 23 | 6 | 0.0019 | 0.3916 | 0.25 | 1.097 |
| 1 | | 10/26/2006 | 9:10 | DWC | 44 | 13 | 0.0033 | 0.3902 | 0.44 | 1.093 |
| 2 | | 10/27/2006 | 9:10 | DWC | 72 | 20 | 0.0054 | 0.3881 | 0.72 | 1.087 |
| 4 | | 10/31/2006 | 9:10 | DWC | 127 | 27 | 0.0102 | 0.3833 | 1.36 | 1.074 |
| 8 | | 11/1/2006 | 9:10 | DWC | 214 | 36 | 0.0180 | 0.3755 | 2.40 | 1.052 |
| 4 | | 11/2/2006 | 9:10 | DWC | 190 | 27 | 0.0165 | 0.3770 | 2.20 | 1.056 |
| 2 | | 11/3/2006 | 9:10 | DWC | 162 | 20 | 0.0144 | 0.3791 | 1.92 | 1.062 |
| 4 | | 11/4/2006 | 9:10 | CJS | 181 | 27 | 0.0156 | 0.3779 | 2.08 | 1.059 |
| 8 | | 11/6/2006 | 9:10 | DWC | 221 | 36 | 0.0187 | 0.3748 | 2.49 | 1.050 |
| 16 | | 11/7/2006 | 9:10 | DWC | 382 | 44 | 0.0340 | 0.3595 | 4.53 | 1.007 |
| 32 | | 11/8/2006 | 9:10 | DWC | 933 | 53 | 0.0882 | 0.3053 | 11.75 | 0.855 |
| 8 | | 11/9/2006 | 9:10 | DWC | 746 | 36 | 0.0712 | 0.3223 | 9.49 | 0.903 |
| 2 | | 11/10/2006 | 9:10 | DWC | 525 | 20 | 0.0507 | 0.3428 | 6.76 | 0.961 |
| 0.5 | | 11/11/2006 | 9:10 | DWC | 402 | 6 | 0.0398 | 0.3537 | 5.30 | 0.991 |
| | | | | | | | | | | |

Notes:
1. "Final" based on test method; 24 hrs for Method A, end of primary for Method B.
2. Correction value, for the current pressure, from the consolidometer's calibration curve.
3. $\Delta H = D_{fi} - D_o - D_{ci}$ = Col. A - $D_o$ - Col. B
4. $H_{vi} = (H_o - H_s) - \Delta H$
5. $\varepsilon_i = (\Delta H / H_o) \times 100$ = (Col. C / $H_o$) x 100
6. $e_i = H_{vi} / Hs$ = Col. D / Hs

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Schnabel Engineering

# Load Time Readings

11/21/06

Project: Calvert Cliffs Nuclear Power Plant

Schnabel Contract: 06120048

Boring No.: B-333 Depth: 38.5-40.5ft.

Consol. ID: 3 Reviewed by: CJS

| Elapsed Time (min.) | Dial Guage Readings (inches) | | | | | |
|---|---|---|---|---|---|---|
| | 4 tsf Reload 11/4/2006 | 32 tsf Load 11/8/2006 | X tsf Load Date | X tsf Load Date | X tsf Load Date | X tsf Load Date |
| 0.1 | 0.0174 | 0.0441 | | | | |
| 0.25 | 0.0175 | 0.0457 | | | | |
| 0.5 | 0.0176 | 0.0473 | | | | |
| 1 | 0.0177 | 0.0496 | | | | |
| 2 | 0.0178 | 0.0525 | | | | |
| 4 | 0.0178 | 0.0561 | | | | |
| 8 | 0.0178 | 0.0608 | | | | |
| 15 | 0.0179 | 0.0657 | | | | |
| 30 | 0.0179 | 0.0715 | | | | |
| 60 | 0.0179 | 0.0770 | | | | |
| 120 | 0.0180 | 0.0817 | | | | |
| 240 | 0.0180 | 0.0856 | | | | |
| 480 | 0.0181 | 0.0890 | | | | |
| 720 | 0.0181 | 0.0907 | | | | |
| 960 | 0.0181 | 0.0918 | | | | |
| 1200 | 0.0181 | 0.0926 | | | | |
| 1440 | 0.0181 | 0.0933 | | | | |
| 1680 | | | | | | |
| 1920 | | | | | | |
| 2160 | | | | | | |
| 2400 | | | | | | |
| 2640 | | | | | | |
| 2880 | | | | | | |
| | | | | | | |
| | | | | | | |

Schnabel Engineering

# Consolidation Time Curves

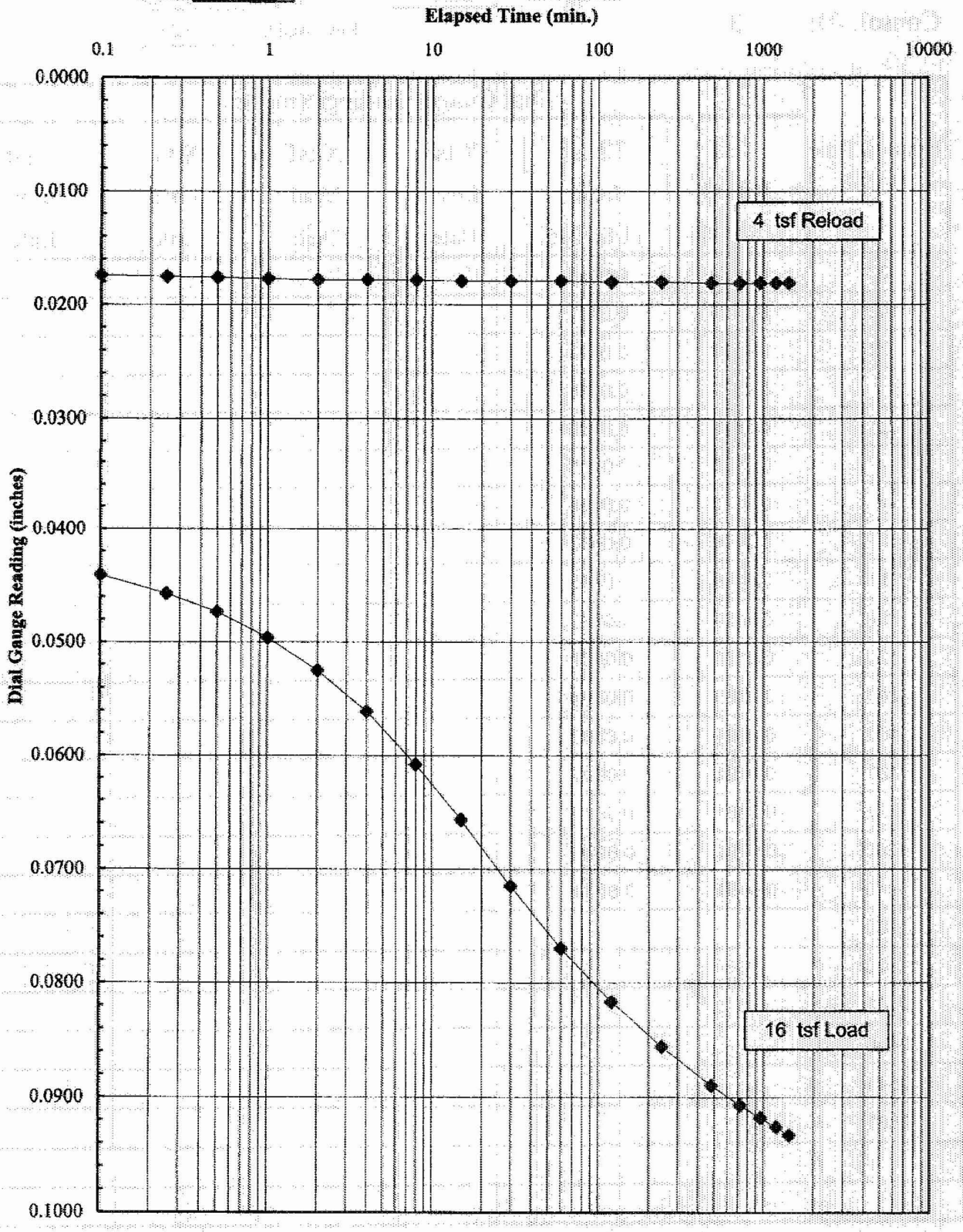
11/21/06

Project: Calvert Cliffs Nuclear Power Plant

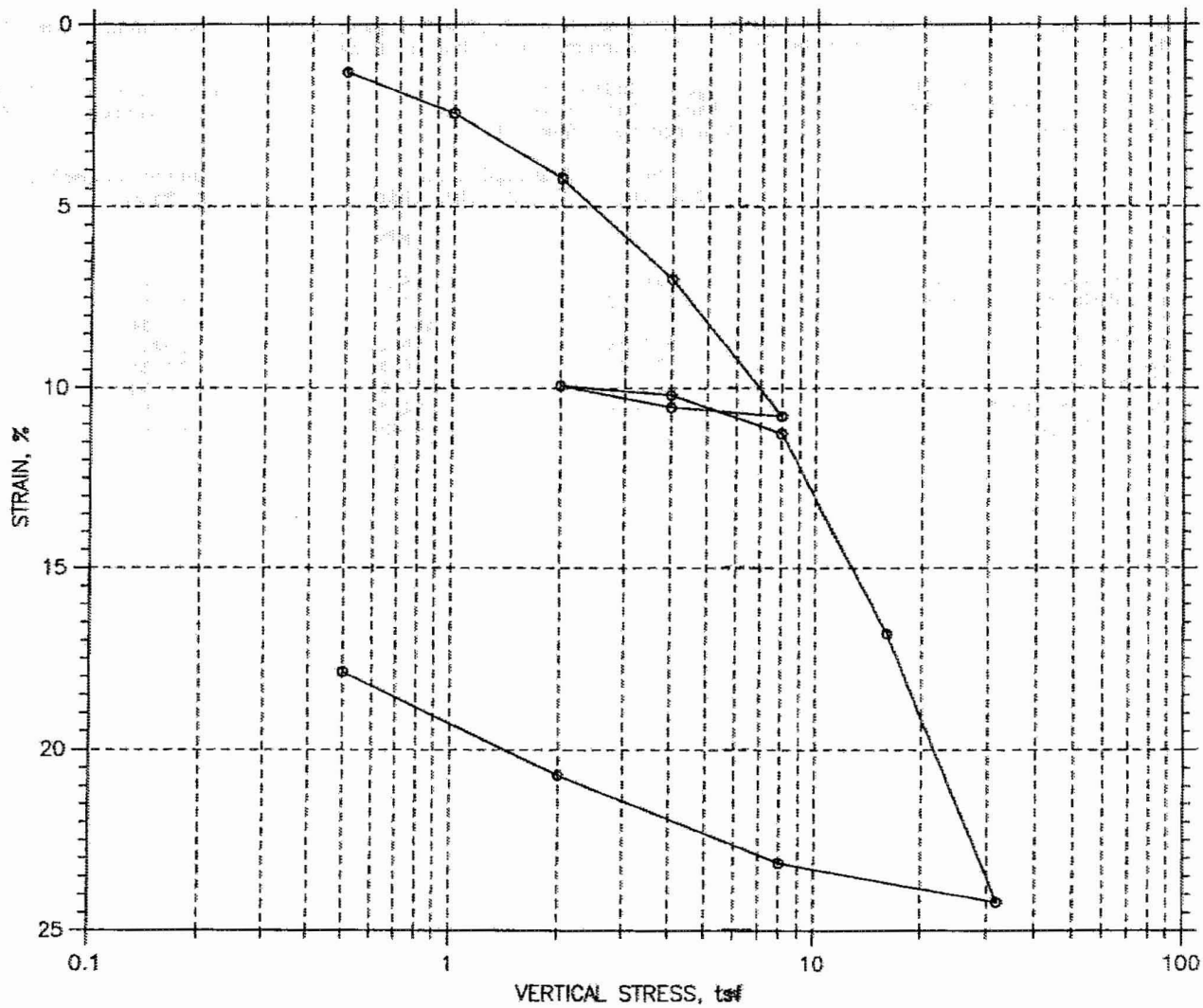
Schnabel Contract: 06120048

Boring No.: B-333 Depth: 38.5-40.5ft.

Reviewed by: CJS



# CONSOLIDATION TEST DATA
## SUMMARY REPORT




| | | | | | Before Test | After Test |
|---|---|---|---|---|---|---|
| Overburden Pressure: --- | | | | Water Content, % | 38.34 | 27.36 |
| Preconsolidation Pressure: 5.3 tsf | | | | Dry Unit Weight, pcf | 79.63 | 96.94 |
| Compression Index: --- | | | | Saturation, % | 92.70 | 99.99 |
| Diameter: 2.5 in | | Height: 1 in | | Void Ratio | 1.12 | 0.74 |
| LL: 51 | PL: 16 | PI: 35 | GS: 2.70 | | | |

| | | | |
|---|---|---|---|
| GeoTesting express<br>a subsidiary of Geocomp Corporation | Project: Calvert Cliffs Nuclear PP | Location: Calvert County | Project No.: GTX-6880 |
| | Boring No.: B-334 | Tested By: md | Checked By: jdt |
| | Sample No.: S-8 | Test Date: 09/11/2006 | Depth: 23-25 |
| | Test No.: C-9 | Sample Type: tube | Elevation: --- |
| | Description: Moist, dark greenish gray clay with sand (CH),79% passing #200 sieve,inundated@0.5 tsf | | |
| | Remarks: System T - Compression Ratio: 0.22 , Recompression Ratio: 0.02 | | |

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| | | |
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| | | |
|---|---|---|
| Measured Specific Gravity: 2.70 | Liquid Limit: 51 | Initial Height: 1.00 in |
| Initial Void Ratio: 1.12 | Plastic Limit: 16 | Specimen Diameter: 2.50 in |
| Final Void Ratio: 0.74 | Plasticity Index: 35 | |

| | Before Consolidation | | After Consolidation | |
|---|---|---|---|---|
| | Trimmings | Specimen+Ring | Specimen+Ring | Trimmings |
| Container ID | Six | RING | | 1729 |
| Wt. Container + Wet Soil, gm | 216.61 | 251.1 | 239.83 | 140.93 |
| Wt. Container + Dry Soil, gm | 164.26 | 211.76 | 211.76 | 112.48 |
| Wt. Container, gm | 7.95 | 109.16 | 109.16 | 8.49 |
| Wt. Dry Soil, gm | 156.31 | 102.6 | 102.6 | 103.99 |
| Water Content, % | 33.49 | 35.34 | 27.36 | 27.36 |
| Void Ratio | --- | 1.12 | 0.74 | --- |
| Degree of Saturation, % | --- | 92.70 | 99.99 | --- |
| Dry Unit Weight, pcf | --- | 79.626 | 96.942 | --- |

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Boring No.: B-334
Sample No.: S-8
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Location: Calvert County
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Sample Type: tube

Project No.: GTX-6880
Checked By: jdt
Depth: 23-25
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| | Applied Stress tsf | Final Displacement in | Void Ratio | Strain at End % | T50 Fitting Sq.Rt. min | T50 Fitting Log min | Coefficient of Consolidation Sq.Rt. in^2/sec | Coefficient of Consolidation Log in^2/sec | Coefficient of Consolidation Ave. in^2/sec |
|---|---|---|---|---|---|---|---|---|---|
| 1 | 0.5 | 0.01318 | 1.089 | 1.32 | 0.1 | 0.1 | 8.69e-003 | 1.03e-002 | 9.41e-003 |
| 2 | 1 | 0.02453 | 1.065 | 2.45 | 0.1 | 0.1 | 5.95e-003 | 8.32e-003 | 6.94e-003 |
| 3 | 2 | 0.04216 | 1.028 | 4.22 | 0.3 | 0.1 | 2.64e-003 | 9.60e-003 | 4.14e-003 |
| 4 | 4 | 0.06976 | 0.969 | 6.98 | 0.6 | 0.0 | 1.20e-003 | 0.00e+000 | 1.20e-003 |
| 5 | 8 | 0.1078 | 0.889 | 10.78 | 1.8 | 1.9 | 3.89e-004 | 3.54e-004 | 3.71e-004 |
| 6 | 4 | 0.1054 | 0.894 | 10.54 | 0.8 | 0.0 | 8.17e-004 | 0.00e+000 | 8.17e-004 |
| 7 | 2 | 0.09933 | 0.907 | 9.93 | 2.1 | 3.3 | 3.17e-004 | 2.02e-004 | 2.47e-004 |
| 8 | 4 | 0.102 | 0.901 | 10.20 | 0.6 | 0.0 | 1.13e-003 | 0.00e+000 | 1.13e-003 |
| 9 | 8 | 0.1126 | 0.878 | 11.26 | 1.9 | 1.9 | 3.40e-004 | 3.49e-004 | 3.44e-004 |
| 10 | 16 | 0.1681 | 0.761 | 16.81 | 6.4 | 10.5 | 9.43e-005 | 5.79e-005 | 7.18e-005 |
| 11 | 32 | 0.242 | 0.604 | 24.20 | 13.9 | 14.2 | 3.75e-005 | 3.67e-005 | 3.71e-005 |
| 12 | 8 | 0.2312 | 0.627 | 23.12 | 3.1 | 3.5 | 1.55e-004 | 1.36e-004 | 1.45e-004 |
| 13 | 2 | 0.207 | 0.679 | 20.70 | 12.8 | 0.0 | 3.93e-005 | 0.00e+000 | 3.93e-005 |
| 14 | 0.5 | 0.1786 | 0.739 | 17.86 | 56.0 | 0.0 | 9.57e-006 | 0.00e+000 | 9.57e-006 |

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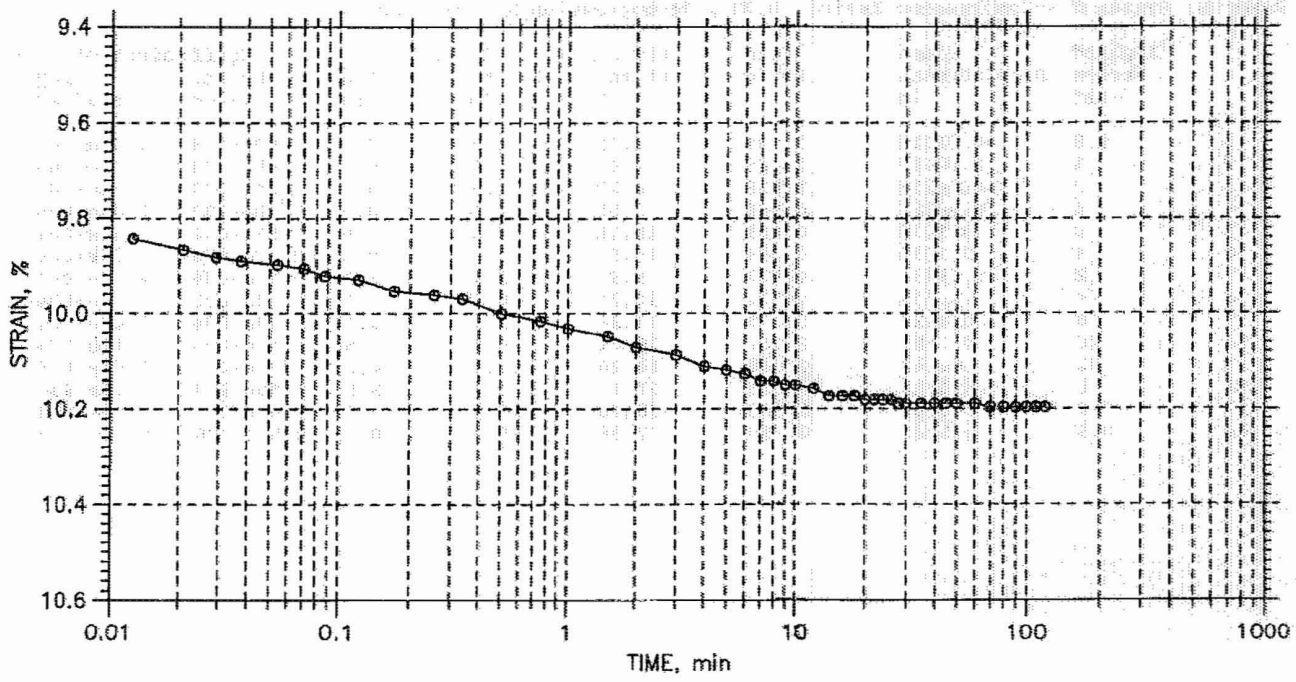
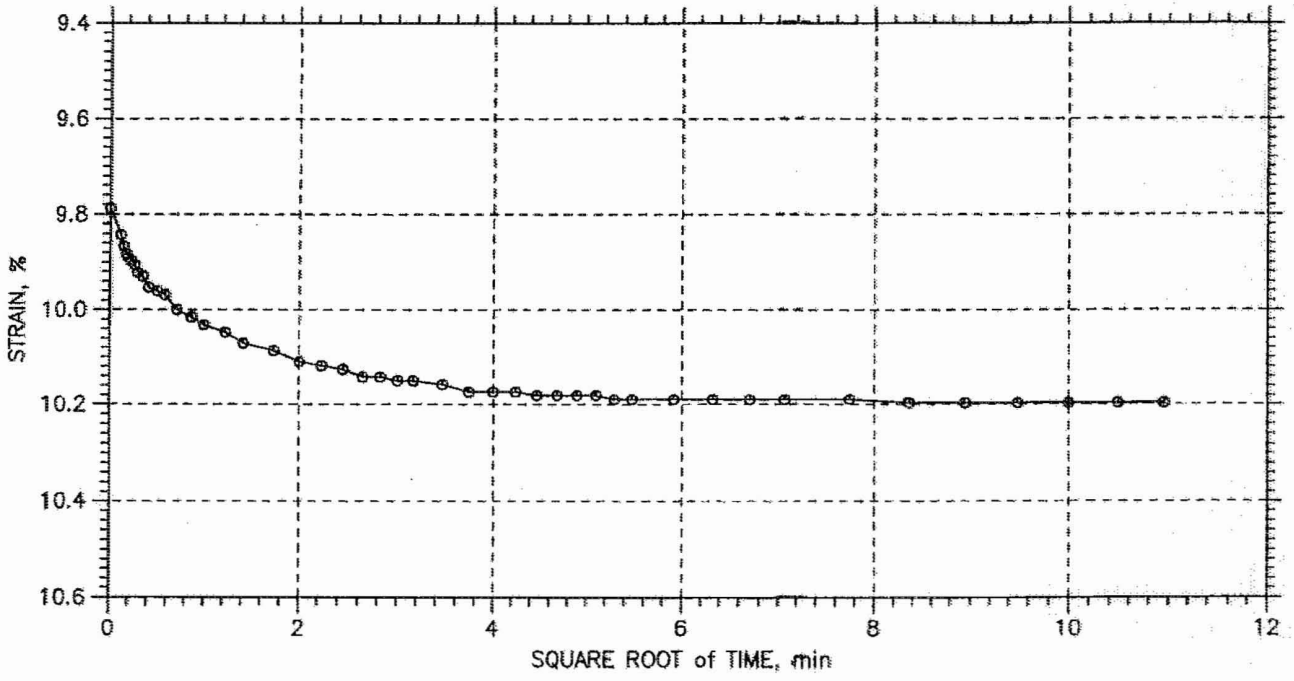
TIME CURVES

Constant Load Step: 8 of 14

Stress: 4. tsf

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