

Detailed Contents of US-APWR DCD Revision

June 25, 2008 Mitsubishi Heavy Industries, LTD.

MITSUBISHI HEAVY INDUSTRIES, LTD.

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- 2. Scope of DCD Revision
- 3. Updates to Detailed Engineering Design (Closed session due to SRI)
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Background and Purpose



- MHI is planning to submit a revision to the US-APWR DCD (in August 2008) prior to the Reference-COLA submittal in September 2008.
- MHI believes that the revisions in the DCD are minor; therefore, the DCD revision will not impact the NRC's review schedule of the DCD.
- MHI will present additional detailed information on the contents of the DCD revision as well as on the required adjustment of the plant arrangement based on the progress of the detailed engineering design.

Scope of DCD Revision



- 1. Incorporation of customer preference items appropriate for the DCD
- 2. Updates to the detailed engineering design

➔ closed session due to SRI

- 3. Incorporation of NRC comments and responses to NRC questions
- 4. Incorporation of recently submitted technical reports using references and/or summaries
- 5. Change of description related COL information

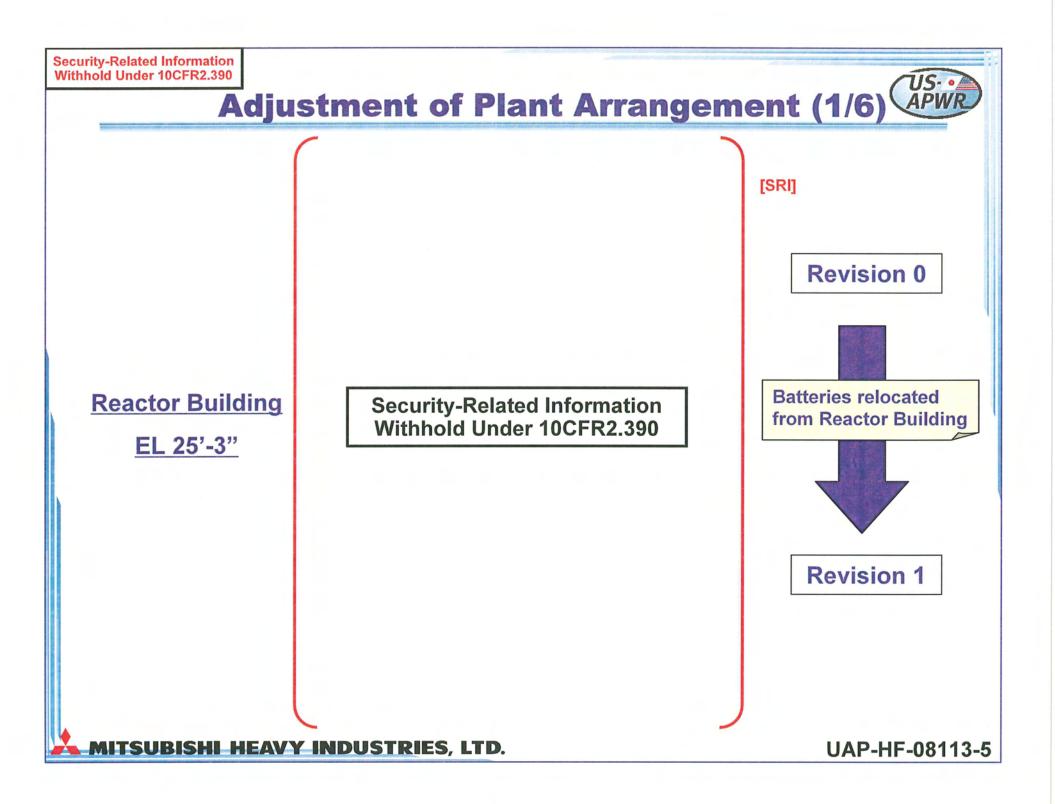
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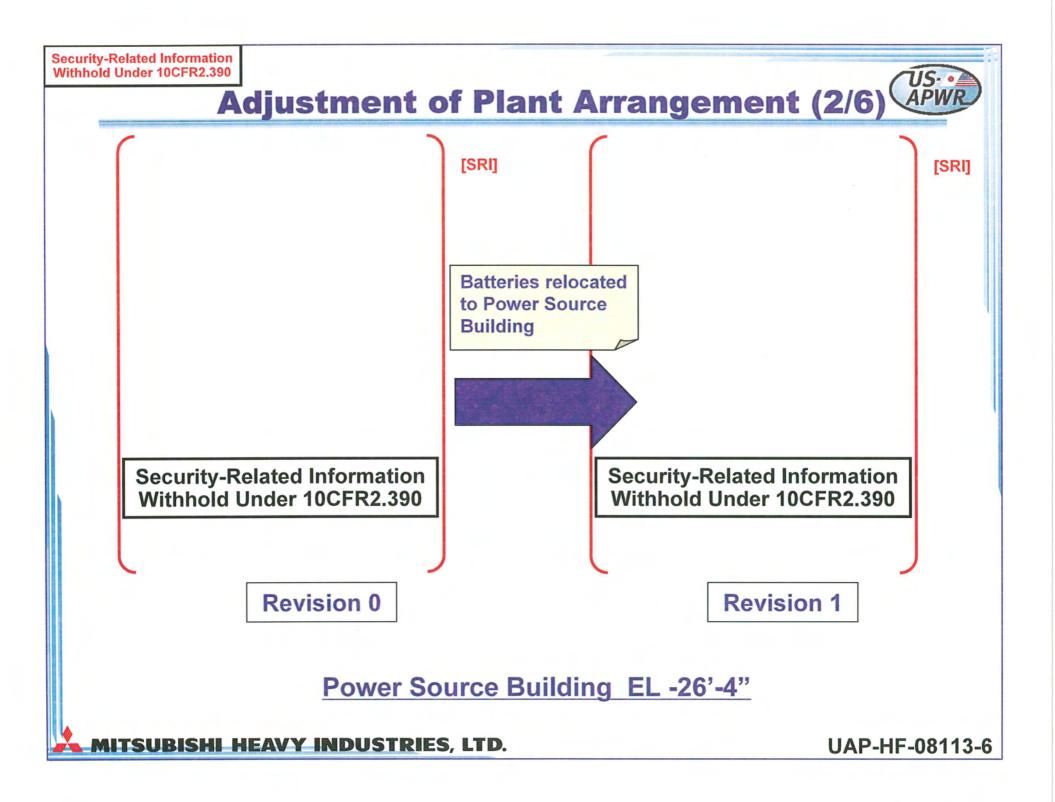
Updates to Detailed Engineering Design

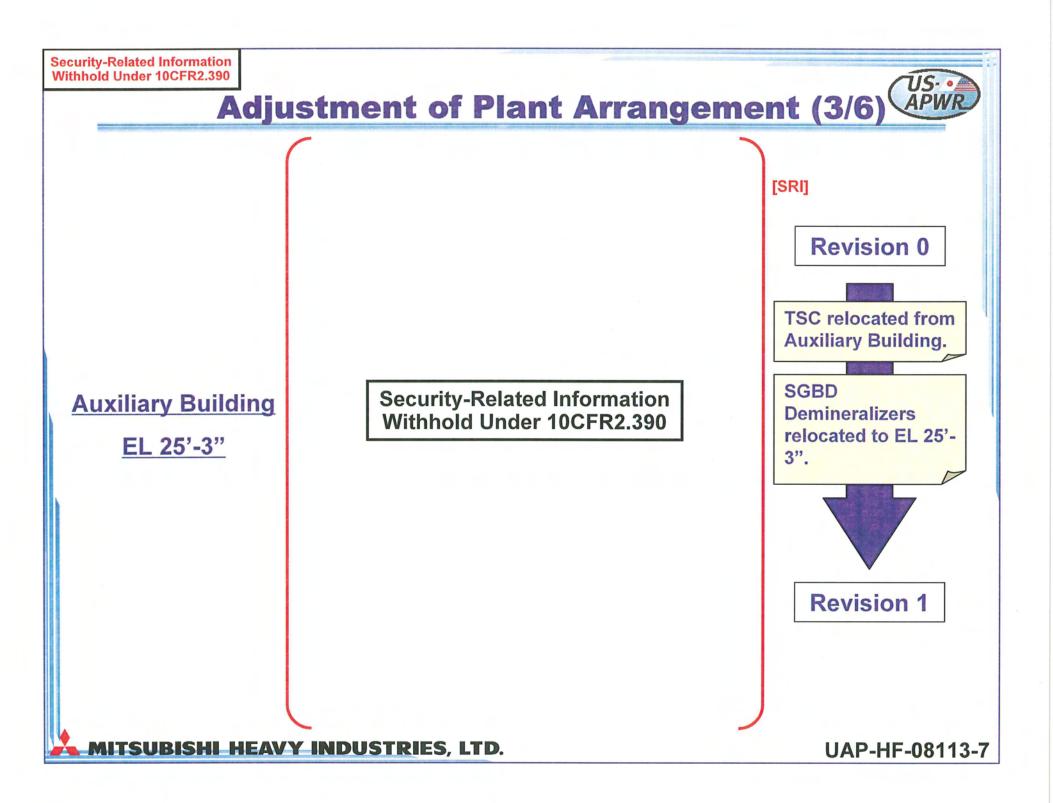


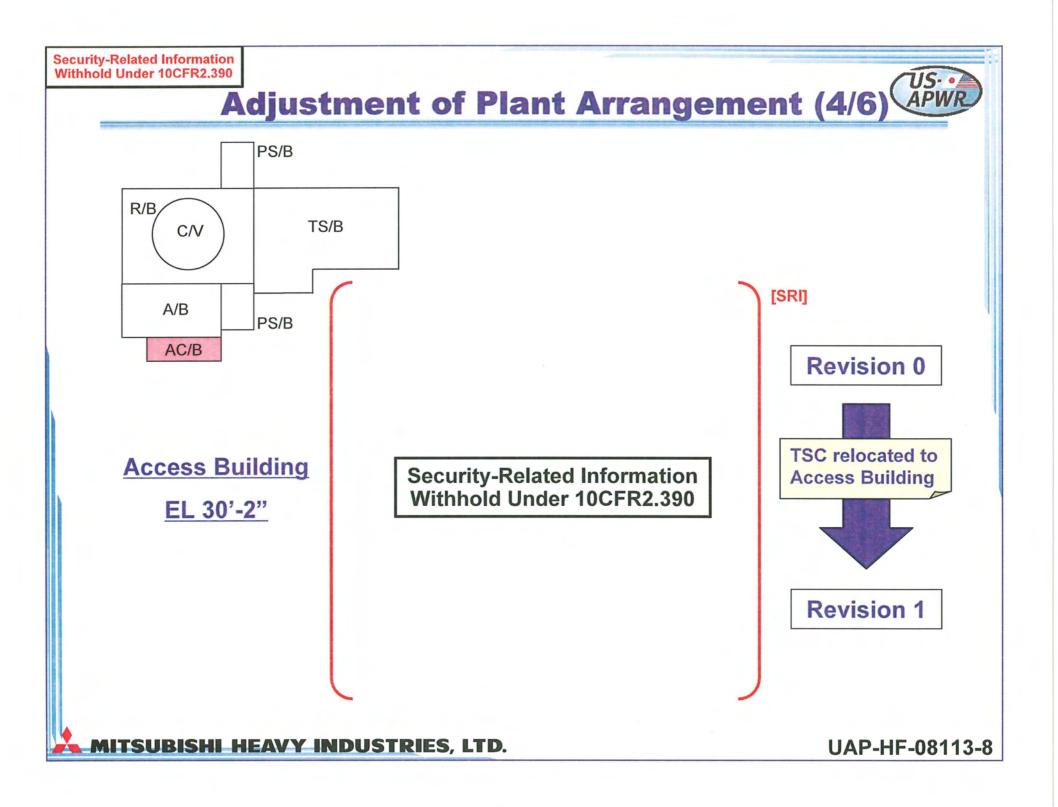
- > Changes to the plant arrangement:
 - 1. Relocation of the battery room from the Reactor Building to the Power Source Building due to re-evaluation of the battery capacity necessary for the required electrical loads
 - 2. Relocation of the TSC (Technical Support Center) from the Auxiliary Building to the Access Building
 - 3. Relocation of the remote shutdown console to a more protected area
 - 4. Relocation of Waste and SGBD (Steam Generator Blowdown) Demineralizers, addition of Mobile Waste System
- Impact on the DCD (described in detail in the later slides):
 - => Revision of drawings and descriptive information
 - => Minor revision of the fire hazard analysis
 - => Minor revision of the internal fire and internal flooding PRA

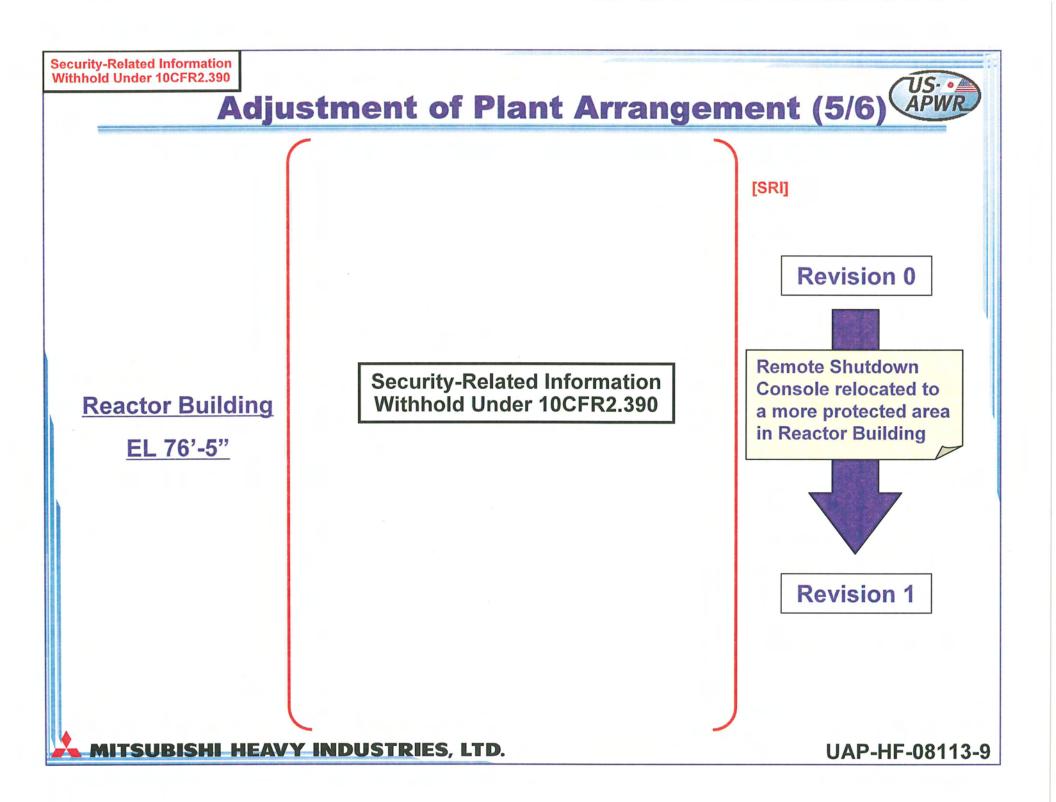
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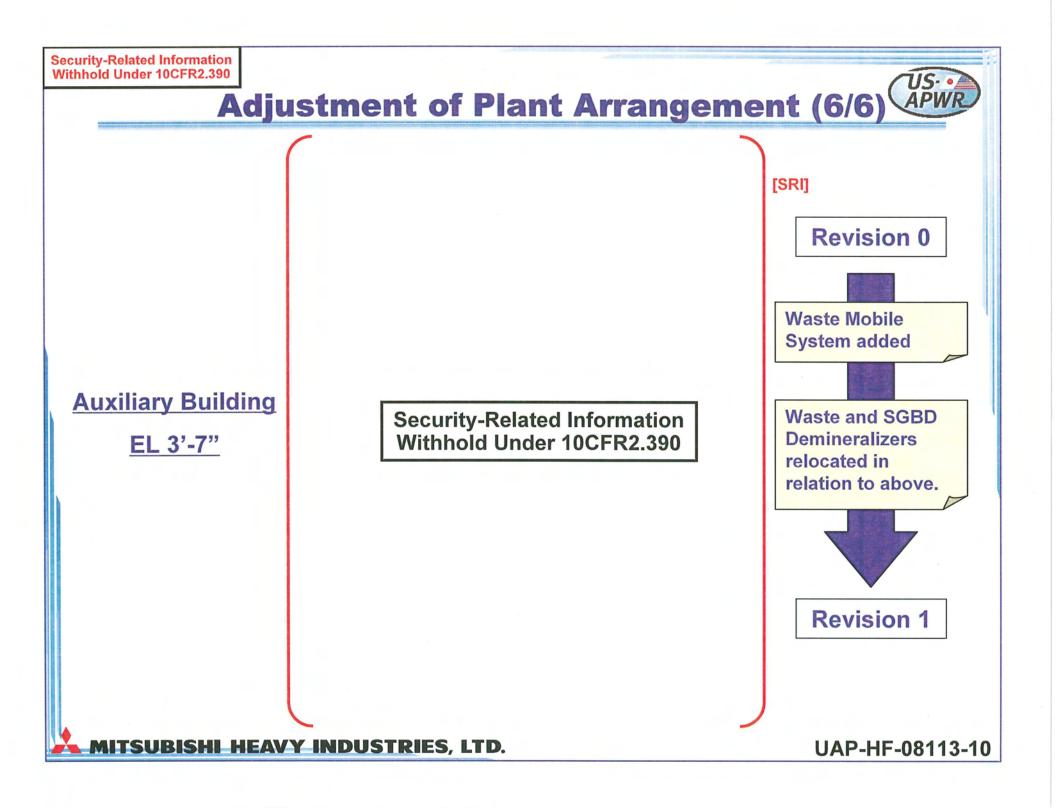




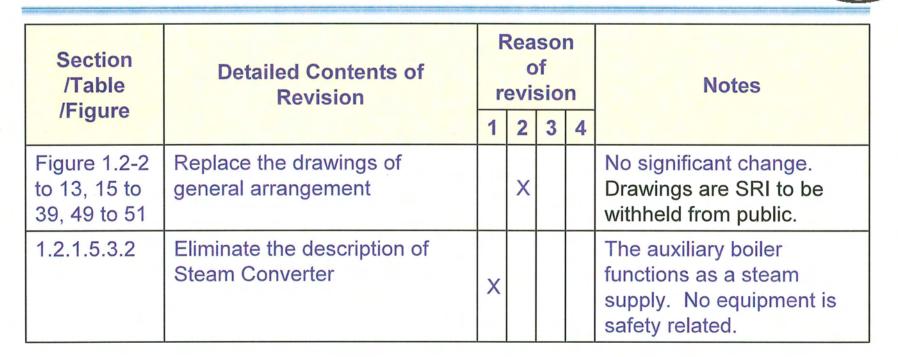








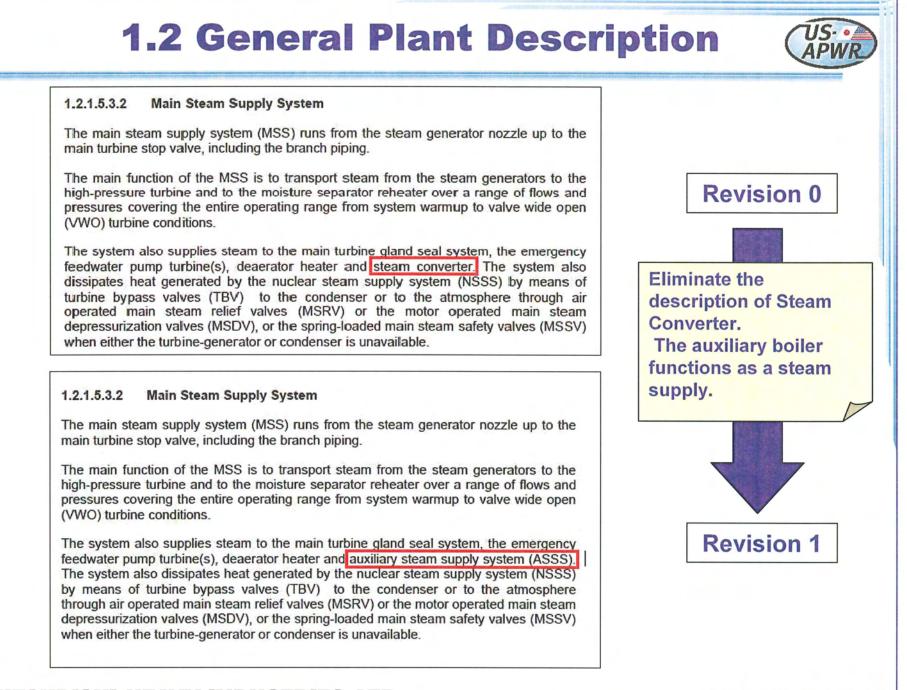
DCD Chapter 1 Revision



Reason of Revision:

- 1. Incorporation of customer preference items appropriate for the DCD
- 2. Update of the detailed engineering design
- 3. Incorporation of NRC comments and responses to NRC questions
- 4. Incorporation of recently submitted technical reports by references and/or summaries

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DCD Chapter 2 Revision

Section /Table	Detailed Contents of Revision		Reason of revision			Notes	
/Figure		1	2	3	4		
2.0	Update the x/Q values for Main Control Room due to the changes of general arrangement		×			No significant change. See Chapter 15 Revision.	
2.0	Use the exact values at key site parameter			x		No significant change.	
2.1 to 2.5	Simplify the description of Site Parameters, incorporating the NRC comments			×		The requirements of RG 1.206 are to be summarized. No significant change.	

Reason of Revision:

- 1. Incorporation of customer preference items appropriate for the DCD
- 2. Update of the detailed engineering design
- 3. Incorporation of NRC comments and responses to NRC questions
- 4. Incorporation of recently submitted technical reports by references and/or summaries

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Chapter 2 Site Characteristics (1/2)

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Table 2.0-1 Key Site Parameters							
Parameter Description	Parameter Value						
Subsurface stability – mean minimum shear wave velocity at SSE input at ground surface	~ 1,000 ft/s						
Subsurface stability – mean shear wave velocity for defining firm rock	≧ 3,500 ft/s						
Subsurface stability – mean shear wave velocity for defining firm to hard rock	∼ 6,500 ft/s						
Subsurface stability – mean shear wave velocity for defining hard rock	≧ 8,500 ft/s						

Table 2.0-1 Key Site Parameters

Parameter Description	Parameter Value
Subsurface stability –minimum shear wave velocity at SSE input at ground surface	1,000 ft/s
Subsurface stability –shear wave velocity for defining firm rock	3,500 ft/s
Subsurface stability –shear wave velocity for defining firm to hard rock	6,500 ft/s
Subsurface stability –shear wave velocity for defining hard rock	8,500 ft/s



Exact values for the shear wave velocity



Revision 1

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Chapter 2 Site Characteristics (2/2)

Revision 0

US-APWR Design Cortrol Document

2. SITE CHARACTERISTICS

2.4 Hydrologic Engineering

The LS-APWR is designed for a groundwater elevation of 1 ft. below plant grade as well as a maximum level for flood or tsunami of 1 ft. below plant grade. The US-APWR is designed for a maximum local intense precipitation of 19.4 in./inr. The COL Applicant is to provide sufficient information as outlined in SRPs 2.4.1 through 2.4.14 (References 2.4-1 through 2.4-14) and as outlined below to verify that hydrologic related events will not affect the safety-basis for the US-APWR. Table 2.0-1 contains standard plant design input for hydrology.

An independent hydrologic angineering review of hydrologically related site characteristics, performance requirements, and bases for operation of SSCs important to safety, is to consider the following pheromena or conditions.

- 1. Probable maximum precipitation, on site and on the contributing drainage area
- Runoff floods for streams, reservoirs, adjacent drainage areas, and site drainage, and flood waves resulting from dam failures induced by runoff floods
- 3. Surges, seiches, and wave action
- 4. Tsunami
- Nonrunoff-induced flood waves attributable to dam failures or landslides, and floods attributable to failure of onsite or near-site water control structures
- 6. Blockage of cooling water sources by natural events
- 7. Ice jam flooding
- 8. Combinations of flood types
- Low water and/or drought effects (including setdown resulting from surges, seiches, frazi and anchor ics, or tsumami) on safety-relatec cooling water supplies and their dependability
- 10. Channel diversions of safety-related cooling water sources
- 11. Capacity requirements for safety-related cooling water sources
- 12. Dilution and dispersion of severe accidental releases to the hydrosphere relating to existing and potential future users of surface water and ground water resources.

2.4.1 Hydrologic Description

2.4.1.1 Site and Facilities

The site topographic map is to be provided that shows any proposed changes to natural drainage features. In addition, all safety-related elevations, structures, exterior accesses, equipment, and systems are to be described from the standpoint of hydrologic considerations, both surface and subsurface.

2.4.1.2 Hydrosphere

The location, size, shape, and other hydrologic characteristics of streams, lakes, shore regions, and ground water environments influencing plant siting are to be described, and

Revision 0

Revision 0 of Section 2.1 through 2.5 described in detail the type of site-specific information that a COL Applicant should include to satisfy SRP requirements. **MITSUBISHI HEAVY INDUSTRIES, LTD.**

Description of Site Parameters was simplified. (Example of Section 2.4)

Revision 1

2. SITE CHARACTERISTICS

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US-APWR Design Control Document

Hydrologic Engineering

The US-APWR is designed for a maximum ground water elevation of 1 ft. below plant grade as well as a maximum level for flood or tsunami of 1 ft. below plant grade. The US-APWR is designed for a maximum local intense precipitation of 19.4 in./hr. Table 2.0-1 contains standard plant design input for hydrology.

The COL Applicant is to provide sufficient information to verify that hydrologic related events will not affect the safety-basis for the US-APWR,

Non safaty-related structures and certain safety-related structures whose flooding would not prevent safe operation of the plant need not be designed for the effects of high water or ice. Examples of safety-related structures that may not be adversely affected by flooding or icing include water intake structures and ultimate heat sink basins.

2.4.1 Hydrologic Description

Major external hydrologic considerations for safety operation of the plant include both surface and subsurface sources. The hydrologic description includes the location, size, ahape, and other hydrologic characteristics of streams, lakes, shore regions, and ground water environments influencing plant siting, and includes a description of existing and proposed water control structures, both upstream and downstream, that may influence conditions at the site.

2.4.2 Floods

The site-specific design of flood protection for safety-related components and structures of the plant is based on the highest calculated flood water level elevations and flood wave effect (site-characteristic flood) resulting from analyses of several different hypothetical causes. The site-specific design for local probable maximum precipitation demonstrates the capability of site drainage facilities to prevent flooding of safety-related facilities.

2.4.3 Probable Maximum Flood

The site-specific probable maximum flood (PMF) is based on the nearby streams and rivers contribution to the design basis flooding. Any nexervoir and channel routing assumptions are addressed for site-specific impact, including coefficients and their bases with appropriate discussion of initial conditions, outlat works (controlled and uncontrolled), and spilways (controlled and uncontrolled).

A site-specific flood enalysis also includes the translation of the estimated peak probable maximum pracipitation (PMP) discharge to elevation using applicable site profile and precipitation data.

2.4.4 Potential Dam Failures

A site-specific evaluation considers the potential hazard to the plant's safety-related facilities as a result of the seismically induced failures of upstream and downstream water control structures. The avaluation also describes the worst combination failure (domino or simultaneous) that affects the site with respect to the maximum flood.

2.4-1

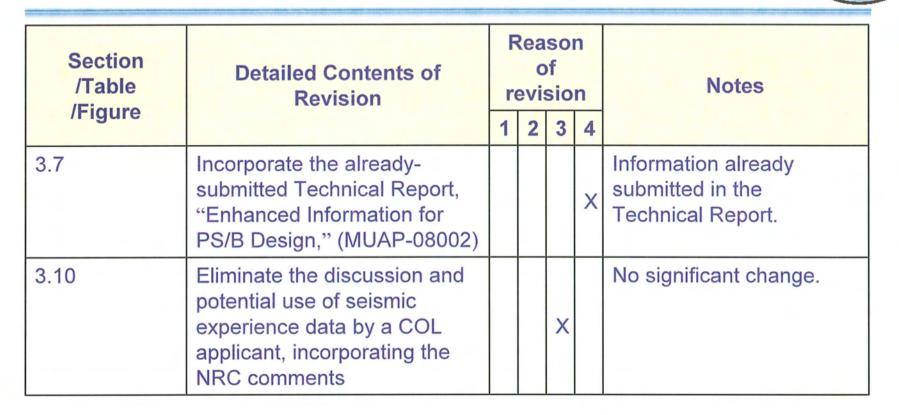
Tier 2

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Revision 1

Revision 1 simply identifies site-specific information requirements without additional detail.

DCD Chapter 3 Revision (1/2)



Reason of Revision:

- 1. Incorporation of customer preference items appropriate for the DCD
- 2. Update of the detailed engineering design
- 3. Incorporation of NRC comments and responses to NRC questions
- 4. Incorporation of recently submitted technical reports by references and/or summaries

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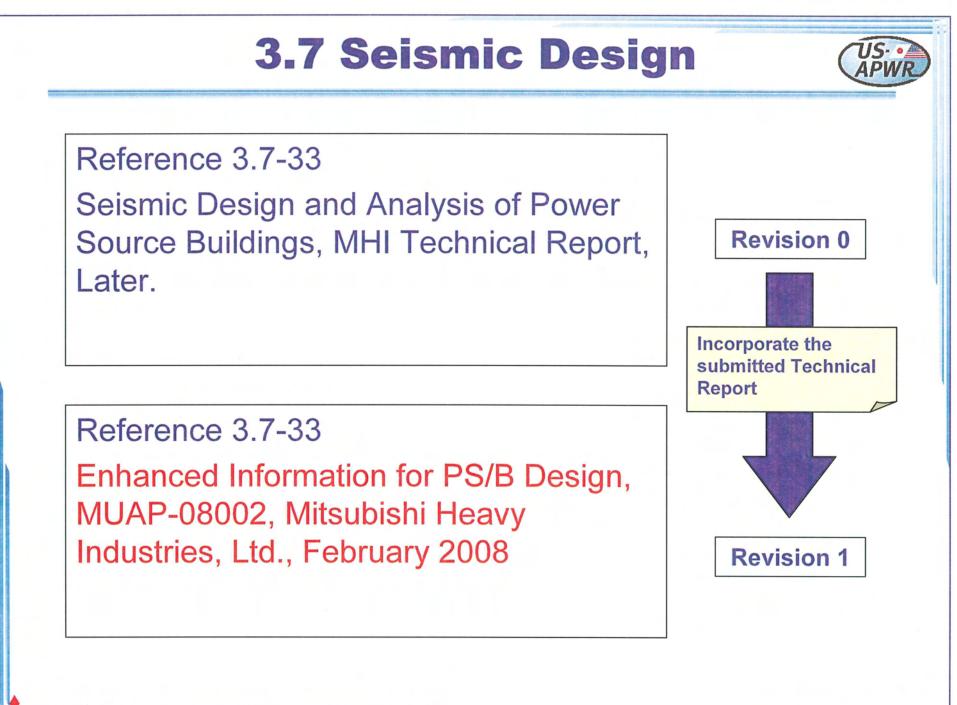
DCD Chapter 3 Revision (2/2)

Section /Table	Detailed Contents of Revision		Reason of revision			Notes	
/Figure		1	2	3	4		
Table 3D-2	Update the location of Battery in the Environmental Qualification Equipment List		X			Relocation of the Battery room from the Reactor Building to the Power Source Building. Both of the buildings categorized as Seismic Category I. No safety related change.	

Reason of Revision:

- 1. Incorporation of customer preference items appropriate for the DCD
- 2. Update of the detailed engineering design
- 3. Incorporation of NRC comments and responses to NRC questions
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3.10 Seismic and Dynamic Qualification of Mechanical and Electrical Equipment



Experience-based qualification is eliminated in Rev.1.

Descriptions in Revision 0	Descriptions in Revision 1
3.10.1.1 Qualification Standards This method of qualification of safety-related seismic category I equipment using experience data is not used in the DCD. This is an optional method that can be used after the DCD by the COL Applicant. If used by the COL Applicant, it is to be documented in the equipment qualification file (and EQSDS) and readily available for review. This methodology is also discussed in Subsection 3.10.4.2.	Experience-based qualification is not used for any equipment.
 3.10.2 Methods and Procedures for Qualifying Mechanical and Electrical Equipment and Instrumentation Qualify the equipment through the use of experience data (optional) (This item is one of the methods for seismic qualification of equipment.) 	(This item is deleted)
 3.10.4 Test and Analyses Results and Experience Database Qualification by an experience-based approach, identification of the type of experience and the source of experience database, if applicable. (This item is one of the items should be included in EQSDSs) 	(This item is deleted)
3.10.4.2 Experience Based Qualification <i>The whole of paragraph</i>	Experience-based qualification is not used for any equipment.

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APPENDIX 3D US-APWR EQUIPMENT QUALIFICATION LIST

Table 3D-2 Environmental Qualification List (Example) Equipment Location Purpose Description Tag RT, ESF A-Class 1E Battery Charger **BCP-A** R/B **Revision 0** RT, ESF DCC-A A-Class 1E DC Switchboard R/B RT, ESF DCC-A1 A1-Class 1E DC Switchboard R/B **Relocate the Battery** Room from R/B to PS/B Description Purpose Equipment Location Tad

rag					
BCP-A	A-Class 1E Battery Charger	PS/B	RT, ESF	Revision 1	
DCC-A	A-Class 1E DC Switchboard	PS/B	RT, ESF		
DCC-A1	A1-Class 1E DC Switchboard	PS/B	RT, ESF		

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UAP-HF-08113-20

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DCD Chapter 5 Revision

Section /Table /Figure	Detailed Contents of Revision		Reason of revision		of	
rigure		1	2	3	4	
5.2.3.2.3	Add the description of metallic insulation, incorporating a future submittal Technical Report related to "Sump Strainer"				x	The assumption of the debris generation to decrease the debris head loss (as described in the letter dated April 16, 2008 UAP-HF-08080).

Reason of Revision:

- 1. Incorporation of customer preference items appropriate for the DCD
- 2. Update of the detailed engineering design
- 3. Incorporation of NRC comments and responses to NRC questions
- 4. Incorporation of recently submitted technical reports by references and/or summaries

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5.2.3 Reactor Coolant Pressure Boundary Materials

Added the description of metallic insulation to Subsection 5.2.3.2.3, incorporating a Technical Report related to "Sump Strainer."

(Revision 0) No information about metallic insulation.

(Revision 1) Added the following description in the first sentence of Subsection 5.2.3.2.3.

The US-APWR design utilizes the reflective metal insulation (RMI), to the great extent practical, for the pipe lines and components subject to jet impingement from a high-energy line break, in order to mitigate the generation of insulation debris. RMI is made of stainless steel and applied to most part of the RCS components and piping.

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DCD Chapter 6 Revision

Section/ Table/Figure	Detailed Contents of Revision		Reason of revision		of		of			Notes
		1	2	3	4					
6.2.2.2	Incorporate the already- submitted Technical Report, "Sump Strainer Performance," MUAP- 080001				х	Information already submitted in the Technical Report.				

Reason of Revision:

- 1. Incorporation of customer preference items appropriate for the DCD
- 2. Update of the detailed engineering design
- 3. Incorporation of NRC comments and responses to NRC questions
- 4. Incorporation of recently submitted technical reports by references and/or summaries

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6.2.2 Containment Heat Removal Systems (1/5)

<u>Added</u> new information about the technical report of the US-APWR Sump Strainer Performance and <u>revised</u> the description about sump strainer in Section 6.2

(Revision 0) No subsection 6.2.2.2.6 ECC/CS Strainers

(Revision 1) Added following subsection :

6.2.2.2.6 ECC/CS Strainers

These components are included in the ECCS. Figures 6.2.2-8 and 6.2.2-9 show four independent sets of ECC/CS strainers located in the RWSP. The strainer design includes redundancy, a large surface area to account for potential debris blockage and maintain safety performance, corrosion resistance, and a strainer hole size to minimize downstream effects. Additional design attributes are described in the US-APWR Sump Strainer Performance document (Ref 6.2-34).

As described in Chapter 3, the ECC/CS strainers are Equipment Class 2, Seismic Category I.

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6.2.2 Containment Heat Removal Systems (2/5)

(Revision 0) Including the excessive information duplicated with the Sump Strainer Performance Evaluation document in Subsection 6.2.2.2.5 "Refueling Water Storage Pit"

(Revision 1) Deleted following sentence in Subsection 6.2.2.2.5 "Refueling Water Storage Pit"

The ECC/CS strainers are a passive disc, fin, or cassette-type design with a large "footprint" that presents a surface area of approximately 2,150 ft², sufficient to preclude debris clogging. The ECC/CS strainers are made of stainless steel, and use perforated plates in a layered disc design to limit the maximum "pass through" debris size to 0.071 in. Important design features of the US-APWR and CS/RHR and SI suction piping ECC/CS strainers include the following:

- Active portion of strainer above the RWSP floor
- Strainer support base acts as a curb against potential debris
- Fully submerged with recirculation sufficient to preclude flow vortexing
- Maximum debris size "pass through" is 0.071 in.

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6.2.2 Containment Heat Removal Systems (3/5)

(Revision 0) Including excessive information and COL Item duplicated with the Sump Strainer Performance Evaluation document in Subsection 6.2.2.3 "Design Evaluation" and table 6.2.2-2

(Revision 1) Referred and summarized "the Sump Strainer Performance Evaluation document" in subsection 6.2.2.3 "Design Evaluation"

The Sump Strainer Performance Evaluation document (Ref. 6.2-34) evaluates parameters described in NEI 04-07 (Ref. 6.2-24). Additional detailed evaluation of these parameters are provided in reference 6.2-34 and are summarized below:

- Identification of insulation types and coating systems used and restricted in the US-APWR and associated potential for debris generation and differential pressure across the strainer
- Break selection criteria and bounding break locations
- Debis generation, characterization and transport assumptions associated with affected insulation, coatings, and latent debris

6.2.2 Containment Heat Removal Systems (4/5)

(Cont.)

- Total strainer head loss associated with fibrous and particulate debris, "chemical effect"
- Net Positive Suction Head associated with total strainer head loss, hydraulic head loss of the equipment and piping, including uncertainty margins
- Upstream effects including hold up volumes conservative drainage flow path and capacity assumptions
- Downtream effects potentially impacting the safety functions associated with pumps, valves, heat exchangers, instrumentation (sensing lines and flow measuring devices), spray nozzles, reactor vessel flow paths

6.2.2 Containment Heat Removal Systems (5/5)

(Revision 0) Including COL Item 6.2(1) about the sump strainer performance in Subsection 6.2.8 No Reference document about US-APWR Sump Strainer Performance in Subsection 6.2.9

(Revision 1) Deleted COL Item 6.2(10)

"Performance characteristics and effectiveness of the ECCS/CS strainer is evaluated by the COL applicant. The evaluation includes the effects of debris, hydraulic resistance, debris transport and vendor test data. "

(Revision 1) Added following document as Reference <u>US-APWR Sump Strainer Performance</u>, MUAP-080001-P, Rev. 1(Proprietary), and MUAP-080001-NP, Rev. 1(Non-Proprietary), September 2008.

DCD Chapter 7 Revision

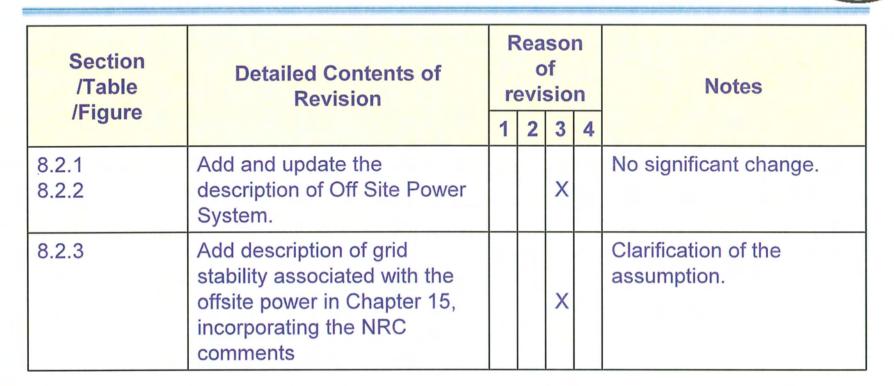
Section /Table /Figure	Detailed Contents of Revision		Reason of revision			Notes	
nigure		1	2	3	4		
7.5.1.6.1 Figure 7.5-3	Update the description and layout of the Technical Support Center (TSC)		X			No significant change of the facilities of the TSC and the distance from Main Control Room. The drawing is SRI to be withheld from public.	

Reason of Revision:

- 1. Incorporation of customer preference items appropriate for the DCD
- 2. Update of the detailed engineering design
- 3. Incorporation of NRC comments and responses to NRC questions
- 4. Incorporation of recently submitted technical reports by references and/or summaries

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DCD Chapter 8 Revision (1/2)



Reason of Revision:

- 1. Incorporation of customer preference items appropriate for the DCD
- 2. Update of the detailed engineering design
- 3. Incorporation of NRC comments and responses to NRC questions
- 4. Incorporation of recently submitted technical reports by references and/or summaries

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DCD Chapter 8 Revision (2/2)



Section /Table /Figure	Detailed Contents of Revision		Reason of revision			Notes
rigure		1	2	3	4	
Table 8.3.1-9	Update the location of Electrical Equipment in Electrical Equipment Location List		X			Relocation of the Battery room from the Reactor Building to the Power Source Building. Both of the buildings categorized as Seismic Category I. No safety related change.
Figure 8.3.1-4	Update the Class 1E Electrical Equipment layout		X			Ditto The drawings are SRI to be withheld from public.

Reason of Revision:

- 1. Incorporation of customer preference items appropriate for the DCD
- 2. Update of the detailed engineering design
- 3. Incorporation of NRC comments and responses to NRC questions
- 4. Incorporation of recently submitted technical reports by references and/or summaries

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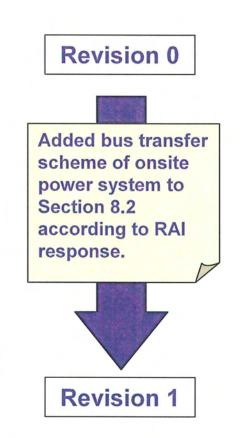
8.2 Off Site Power System (1/5)

8.2.1.2 Offsite Power System

XXXXXXX. For all these MV buses, if power is lost from one source, it is automatically transferred to the other source. XXXXX

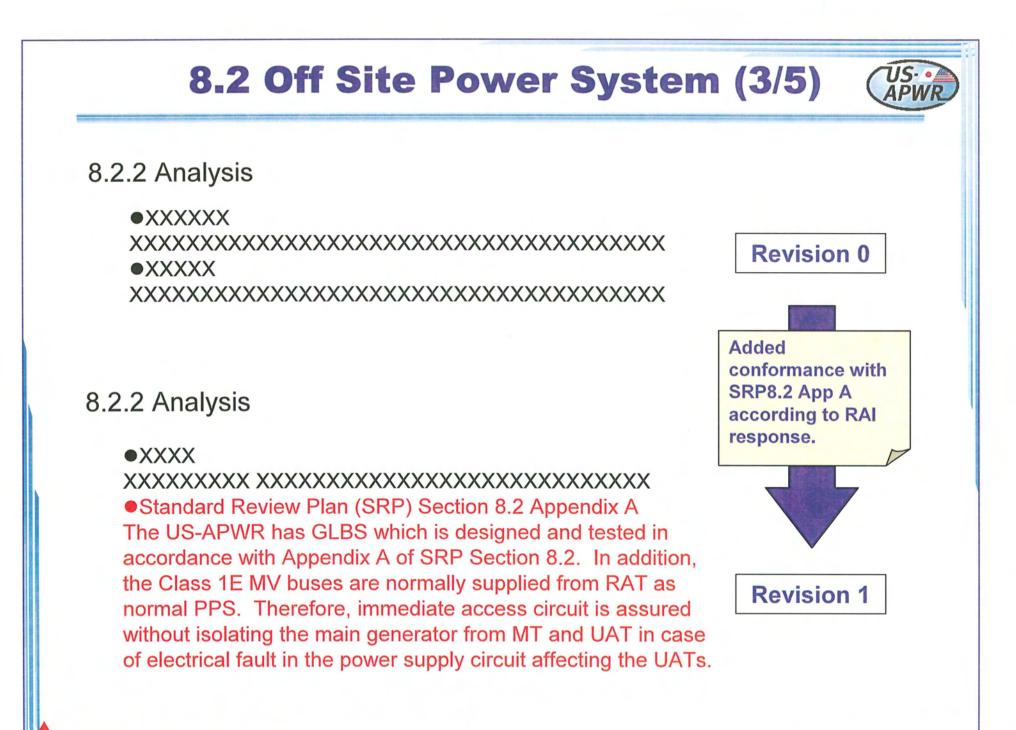
8.2.1.2 Offsite Power System

XXXXXXX. For all these MV buses, if power is lost from one source, the buses are automatically transferred to the other source by fast or slow transfer scheme. At that time, if bus voltage is adequate, fast transfer is initiated. If this is not the case, slow transfer is initiated. Detail explanation of bus transfer scheme is described in Subsection 8.3.1.1.2.4.XXXXX



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8.2 Off Site Power System (2/5) 8.2.1.2 Offsite Power System **Revision 0** The UATs and RATs are provided with differential and over-current protection schemes. The MT is provided with **Changed description of** a differential current protection scheme. transformer protection according to RAI response. 8.2.1.2 Offsite Power System The MTs, UATs and RATs have differential, over-current, **Revision 1** sudden pressure and ground over-current protection schemes per IEEE Std 666 MITSUBISHI HEAVY INDUSTRIES, LTD. **UAP-HF-08113-33**



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8.2 Off Site Power System (4/5)

8.2.2.1 Applicable Criteria

• GDC 2

XXXXX. The effects of natural phenomena are considered in designing the offsite power system, but it not specifically designed to withstand earthquakes, tornadoes or floods. XXXXXXX.

8.2.2.1 Applicable Criteria

• GDC 2

XXXXX. The effects of natural phenomena are considered in designing the offsite power system to withstand without loss of capability to perform their intended functions within the conditions as provided in Chapter 2 such as high and low atmospheric temperatures, high wind, rain, ice and snow, but it not specifically designed to withstand earthquakes, tornadoes or floods. Lightning protection of the offsite power system is described in conformance with RG 1.204. XXXXX

Changed description of conformance with GDC 2 according to RAI response.

Revision 0



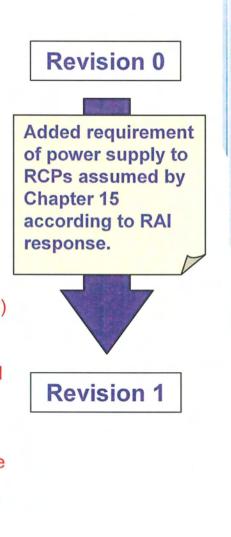
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8.2 Off Site Power System (5/5)

8.2.3 Design Bases Requirement

8.2.3 Design Bases Requirement

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US-8.3.1 AC Power System Name Bldg/F Elevation Room A-Class 1E Battery R/B 2F EL 25'-3" A-Class 1E Battery Room **Revision 0** A-Class 1E Battery A-Class 1E Battery Charger and **R/B 2F** EL 25'-3" **UPS** Room Charger A-Class 1E DC A-Class 1E Battery Charger and **DC** power equipment EL 25'-3" R/B 2F Switchboard **UPS Room** relocated from **Reactor Building to Power Source** Building. Bldg/F Elevation Name Room PS/B EL -26'-4" A-Class 1E Battery A-Class 1E Battery Room B1F A-Class 1E Battery PS/B **Revision 1** EL -14'-2" A-Class 1E Battery Charger Room B1MF Charger A-Class 1E DC PS/B EL -14'-2" A-Class 1E Battery Charger Room Switchboard B1MF Table 8.3.1-9 **Electrical Equipment Location List**

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DCD Chapter 9 Revision

Section /Table /Figure Detailed Contents of Revision		Reason of revision				Notes	
, iguio		1	2	3	4		
9A	Update the description and results of Fire Hazard Analysis in entire Appendix		×			No change of the fire scenarios in the risk evaluation. Minor updates of the analysis results.	

Reason of Revision:

- 1. Incorporation of customer preference items appropriate for the DCD
- 2. Update of the detailed engineering design
- 3. Incorporation of NRC comments and responses to NRC questions
- 4. Incorporation of recently submitted technical reports by references and/or summaries

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Appendix 9A Fire Hazard Analysis (1/9)



- 1. Technical Revision
- **Reflect the changes of plant general arrangement.**

e.g. Relocation of Battery Room, Remote Shutdown Console.

> Reflect the other engineering progress.

e.g. Progress of Cable Raceway Route

- 2. Editorial Revision
- > Unification and correction of description in FHA.

Appendix 9A Fire Hazard Analysis (2/9)



Fire Hazard Analysis of each fire area includes:

- 1. The explanation of fire area
- 2. Fire Detection and Suppression Features
- 3. Smoke Control Features
- 4. Fire Protection Adequacy Evaluation
- 5. Fire Protection System Integrity
- 6. Safe Shutdown Evaluation
- 7. Radioactive Release to Environment Evaluation

Note ; Red character sections may be revised to reflect technical and editorial revision.

Green character sections may be revised to reflect editorial revision.

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Appendix 9A Fire Hazard Analysis (3/9)



This room is changed from battery charger room" to UPS room", because of the relocation of battery room.

9A.3.38 FA2-302 A-Class 1E UPS Room

The FA2-302 train A Class 1E UPS room fire area is located on the 2F floor level on the east side of the nonradiologically controlled access portion of the reactor building as depicted in Figures 9A-5 and 9A-6. The room, which is designated as a single fire zone, FA2-302-01, contains the train A Inverter Unit, UPS for MOV, Solenoid Distribution Panel, and Safety AC120V Switch Board and so forth. The fire loading due to this combustible content is not expected to exceed 3.9E+04 Btu/ft2.

Revision 1

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Appendix 9A Fire Hazard Analysis (4/9)



Change the description of adjacent area to refer Table 9A-3. Add the description of associated train for each fire area.

(continued)

The borders of this fire area are constructed using construction techniques and material which results in fire resistance that provides at least a 3-hour ASTM E-119 fire rating. The adjacent fire zone for each fire zone is presented in Table 9A-3. Openings and penetrations into this fire area are protected with fire protection features provide at least 3-hour fire resistance.

The area is identified as being associated with safety train A.

Revision 1

Appendix 9A Fire Hazard Analysis (5/9)

US-APWR

Modify the description of reactor transients to reflect the technical revision. • Change of GA

Progress of design

(continued)

Safe Shutdown Evaluation

A fire in this area could initiate reactor transients as follows.

- Rod Cluster Control Assembly Misalignment (System Malfunction or Operator Error)
- Complete Loss of Forced Reactor Coolant Flow / (Loss of Non Emergency AC Power
- to the Station Auxiliaries / Partial Loss of Forced Reactor Coolant Flow)
- Loss of Normal Feedwater Flow
- Inadvertent Operating of a Pressurizer safety or Relief Valve
- XXXXXXXXXXXXXXXXXXXXXX

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Revision 1

Appendix 9A Fire Hazard Analysis (6/9)



Change description to reflect the design progress. Add the description of the potential to damage the systems for mitigation functions and safe shutdown functions.

(continued)

A fire in this fire area has the potential to damage the following typical systems of mitigation functions and safe shutdown functions associated with safety train A.

- A-Safety Inverter Unit
- A-Class 1E I&C Power Transformer
- A-MOV Inverter

Since this fire area is separated from the Train B, C, and D areas by 3-hour fire rated barriers, two safety trains of equipment in other fire areas can achieve and maintain safe shutdown from full power, and the fire in this fire area, therefore, will not adversely impact the ability of achieving safe shutdown.

Revision 1

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Appendix 9A Fire Hazard Analysis (7/9)

Change the description, if the building of fire area is changed .

(continued)

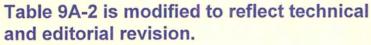
Radioactive Release to Environment Evaluation

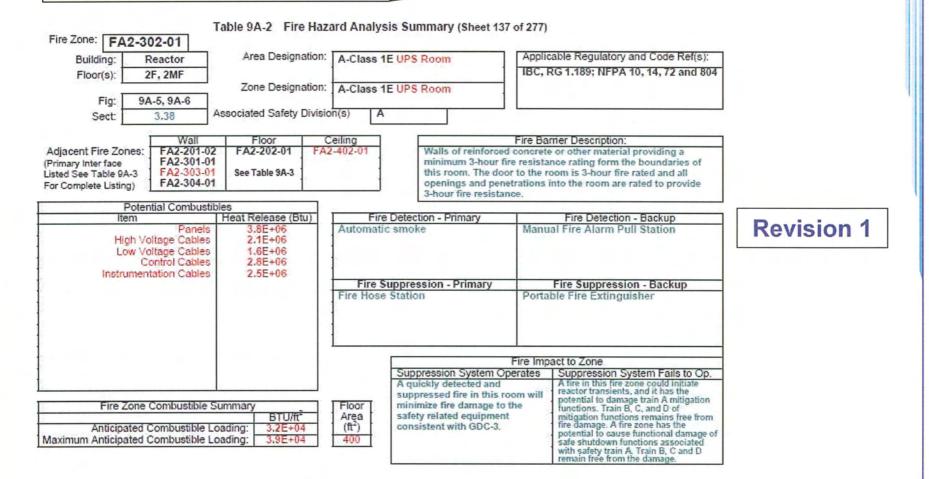
This area is located in the south reactor building portion of the plant which is within the nonradiologically controlled access area of the reactor building. Radiological material is not allowed within this building area by administrative controls. There are no piping systems in the area that could contain fluids with radiological content. As such, a fire in this area is not deemed credible of causing a radioactive release to the environment.

Revision 1

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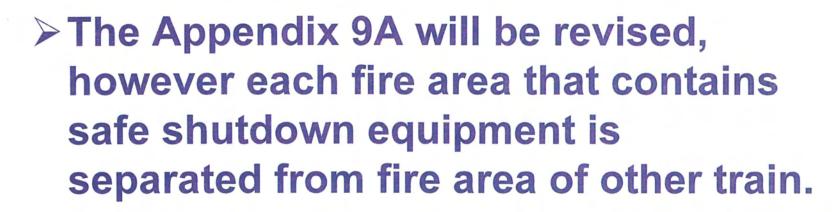
Appendix 9A Fire Hazard Analysis (8/9)





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Appendix 9A Fire Hazard Analysis (9/9)



There is no impact on the plant in terms of safe shutdown capability.

DCD Chapter 10 Revision

Section /Table	Detailed Contents of Revision		C	so of sio		Notes
/Figure			2	3	4	
10.4.10	Change the pH controller of secondary side coolant from ammonia to morpholine, and add the components related chemical controller.	x				No safety related equipment
.10.4.11	Eliminate the description and figures related to Steam Converter from "Auxiliary Steam Supply System" Section	x				The auxiliary boiler functions as a steam supply. No safety related equipment

Reason of Revision:

- 1. Incorporation of customer preference items appropriate for the DCD
- 2. Update of the detailed engineering design
- 3. Incorporation of NRC comments and responses to NRC questions
- 4. Incorporation of recently submitted technical reports by references and/or summaries

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10.4.10 Chemical Injection System

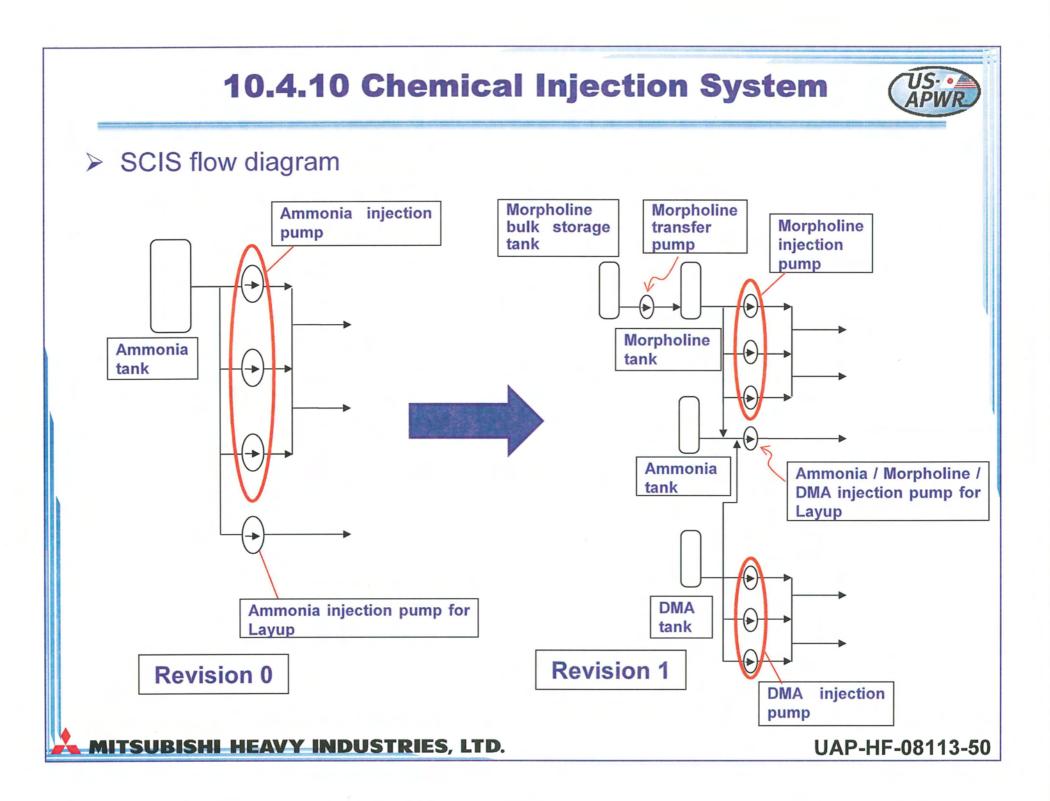


Change of pH controller from ammonia to morpholine and DMA

Addition of components relating morpholine and DMA (chemical tank, injection pump, etc)

 Incorporated bulk chemical system from COL item into standard design

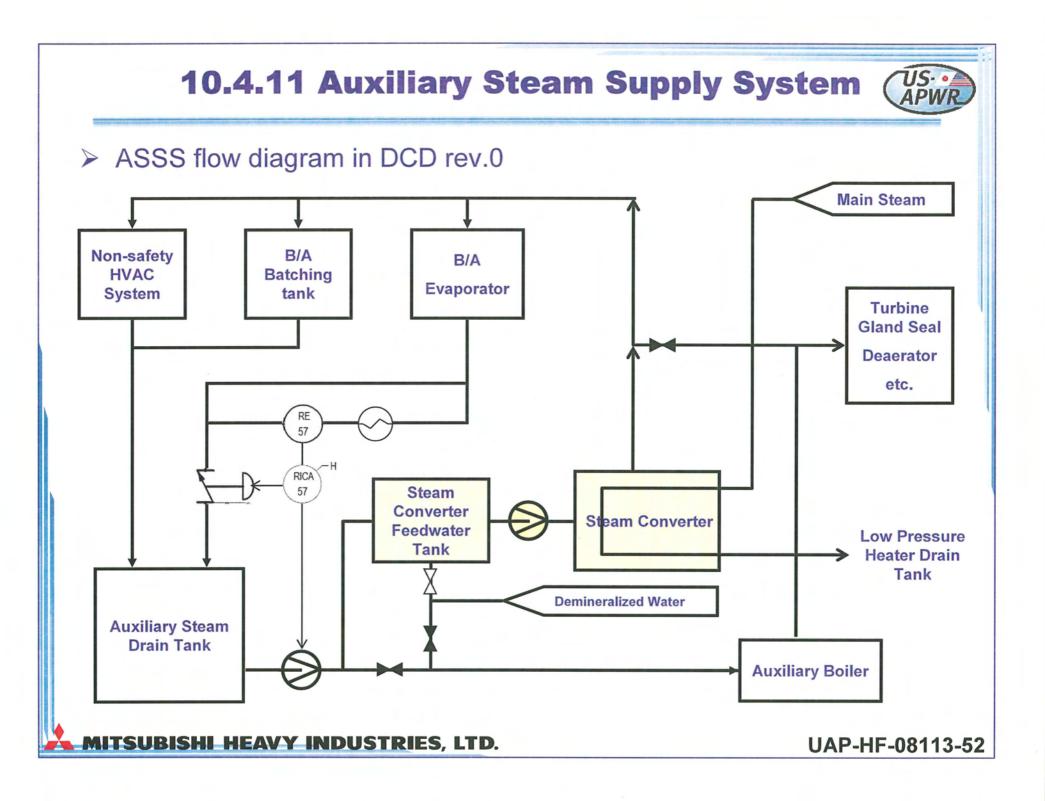
Addition of components relating bulk chemical system (bulk storage tank, transfer pump, etc)

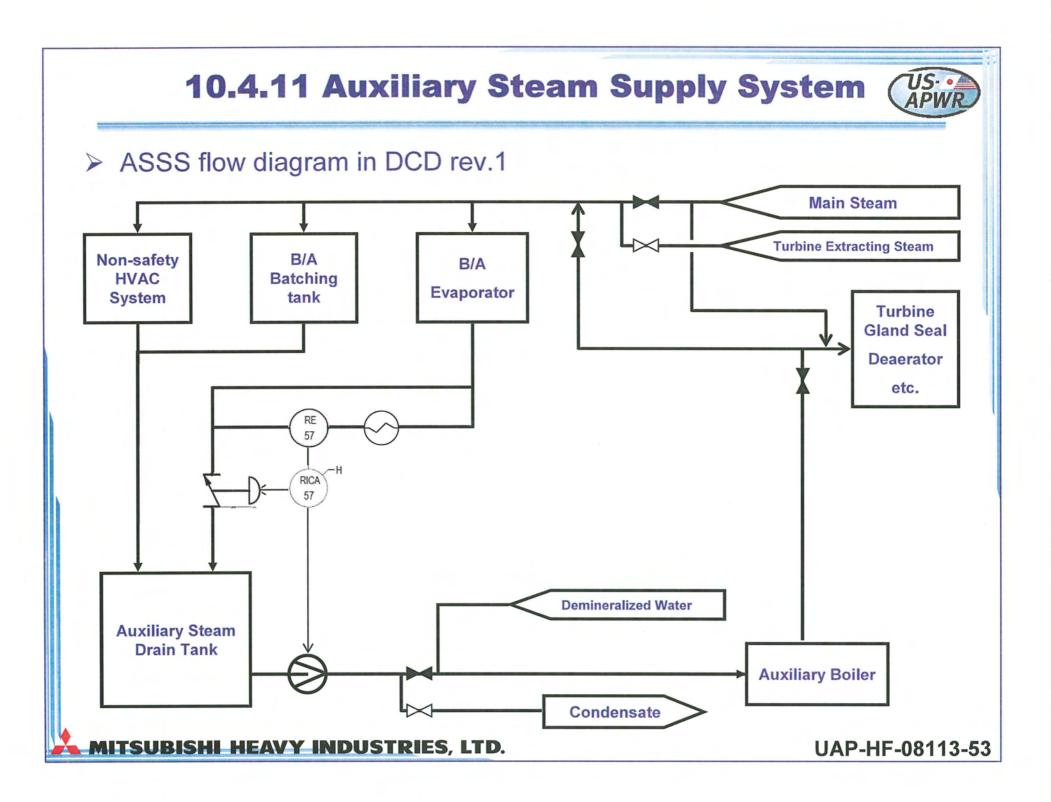


10.4.11 Auxiliary Steam Supply System

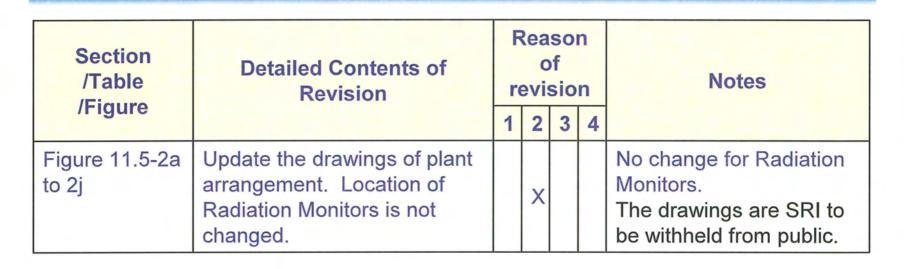


- Elimination of the steam converter
- Elimination of components relating the steam converter elimination (pump, piping, valves, instruments)
- Auxiliary steam source change to the main steam or turbine extracting steam





DCD Chapter 11 Revision



Reason of Revision:

- 1. Incorporation of customer preference items appropriate for the DCD
- 2. Update of the detailed engineering design
- 3. Incorporation of NRC comments and responses to NRC questions
- 4. Incorporation of recently submitted technical reports by references and/or summaries

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DCD Chapter 12 Revision

Section /Table /Figure	Detailed Contents of Revision		Reason of revision			Notes
// igure		1	2	3	4	
Figure 12.3-1 to 6	Update the drawings of plant arrangement. Radiation Zone is not changed on the Map.		X			No change for Radiation Zone. The drawings are SRI to be withheld from public.

Reason of Revision:

- 1. Incorporation of customer preference items appropriate for the DCD
- 2. Update of the detailed engineering design
- 3. Incorporation of NRC comments and responses to NRC questions
- 4. Incorporation of recently submitted technical reports by references and/or summaries

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DCD Chapter 13 Revision

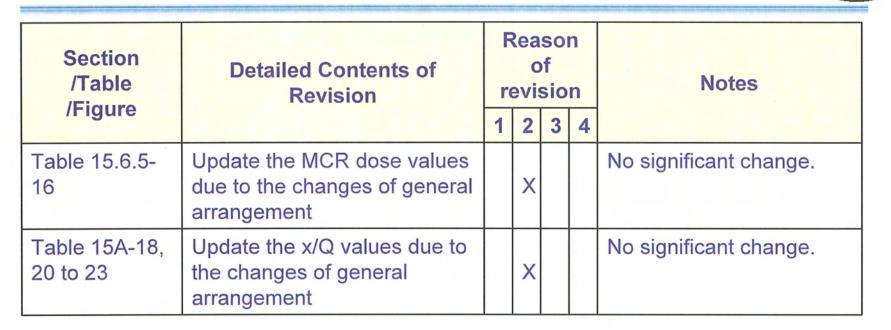
Section /Table /Figure	Detailed Contents of Revision		Reason of revision			Notes	
Technical Report	Update the drawings of general arrangement in "Physical Security Element Review"		×			No significant change. The drawings are SRI to be withheld from public.	

Reason of Revision:

- 1. Incorporation of customer preference items appropriate for the DCD
- 2. Update of the detailed engineering design
- 3. Incorporation of NRC comments and responses to NRC questions
- 4. Incorporation of recently submitted technical reports by references and/or summaries

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DCD Chapter 15 Revision



Reason of Revision:

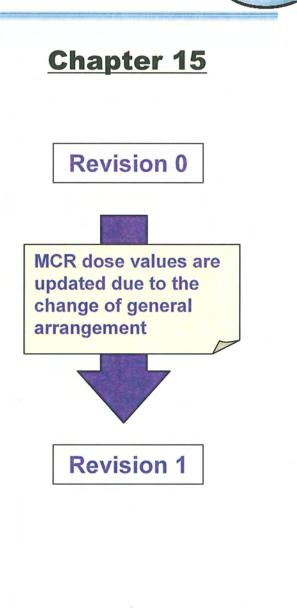
- 1. Incorporation of customer preference items appropriate for the DCD
- 2. Update of the detailed engineering design
- 3. Incorporation of NRC comments and responses to NRC questions
- 4. Incorporation of recently submitted technical reports by references and/or summaries

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Chapter 15 MCR dose values

Table 15.6.5-16 Radiological Consequences of the LOCA **TEDE Dose (rem) Dose Location** EAB (0.5 to 2.5 hours) 13 LPZ outer boundary 13 MCR dose Airborne activity entering the MCR 4.5 8.2×10-3 Direct radiation from the containment 2.1×10-4 Direct radiation from the radioactive plume 9.2×10⁻³ Direct radiation from the recirculation filters Total 4.5

Dose Location	TEDE Dose (rem)				
EAB (0.5 to 2.5 hours)	13				
LPZ outer boundary	13				
MCR dose					
Airborne activity entering the MCR	4.4				
Direct radiation from the containment	8.2×10 ⁻³				
Direct radiation from the radioactive plume	2.1×10 ⁻⁴				
Direct radiation from the recirculation filters	9.2×10 ⁻³				
Total	4.5				

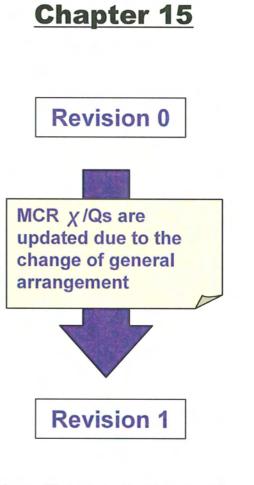


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Chapter 15 χ /Q values

Acc	idents	LOCA						
Sources		Plant vent		Ground Level containment release point				
		Intake	Inleak	Intake	Inleak			
Receptors		MCR HVAC Intake	Reactor building Door	MCR HVAC intake	Class 1E electrical room HVAC intake			
Horizontal Distance (m)		56	37	32	27			
	Distance (m)	52	60	32	33			
0-8 hr		1.1 × 10 ⁻³	1.3 × 10 ⁻³	2.2×10^{-3}	2.4×10^{-3}			
X/Q	8-24 hr	6.6 × 10 ⁻⁴	7.8×10^{-4}	1.3 × 10 ⁻³	1.4 × 10 ⁻³			
(s/m^3)	24-96 hr	4.2×10^{-4}	4.9 × 10 ⁻⁴	8.3×10 ⁻⁴	9.1 × 10 ⁻⁴			
	96-720 hr	1.9×10-4	2.2 × 10 ⁻⁴	3.6×10^{-4}	4.0×10^{-4}			

Acc	idents	LOCA							
Sources			ant ent	Ground level containment release point					
		Intake	Inleak	Intake	Inleak				
Rec	ceptors	MCR HVAC intake	Reactor building door	MCR HVAC intake	Class 1E electrical room HVAC intake				
	al Distance (m)	56	37	32	27				
	I Distance (m)	52	60	32	33				
	0-8 hr	1.1×10^{-3}	1.3 × 10 ⁻³	2.2×10^{-3}	2.4×10^{-3}				
X/Q	8-24 hr	6.6 × 10 ⁻⁴	7.7 × 10 ⁻⁴	1.3×10^{-3}	1.4 × 10 ⁻³				
(s/m ³)	24-96 hr	4.2×10^{-4}	4.9 × 10 ⁻⁴	8.3 × 10 ⁻⁴	9.1 × 10 ⁻⁴				
	96-720 hr	1.9 × 10 ⁻⁴	2.2 × 10 ⁻⁴	3.6×10 ⁻⁴	4.0×10^{-4}				



Note: These χ /Qs are input for MCR dose evaluation

Tables 15A-18, 15A-20, 15A-21 and 15A-23 are also updated by the same token.

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DCD Chapter 16 Revision

Section /Table	e Detailed Contents of Revision		Reason of revision			Notes	
/Figure			2	3	4		
Entire	Increase the number of the components applied for Initiative 4b (currently, 9 LCOs included)	X				Additional information.	
Entire	Incorporate Initiative 5b	Х				Additional information.	

Reason of Revision:

- 1. Incorporation of customer preference items appropriate for the DCD
- 2. Update of the detailed engineering design
- 3. Incorporation of NRC comments and responses to NRC questions
- 4. Incorporation of recently submitted technical reports by references and/or summaries

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Chapter 16 Technical Specifications (1/5)

Risk-Informed Tech. Specs.: Revision 0

- DCD Rev.0 applied Risk-Informed Tech. Specs. Initiative 4b (Risk Managed Tech. Specs.: RMTS) to 9 LCOs*.
 - The program which allows Completion Time to be flexibly determined on site by a licensee using PRA result based on the real time plant configuration.

Other Initiatives such as 5b (Surveillance Frequency Control Program), 1 (Modified End States) and 7 (inoperable barriers) may be implemented in the future.

*LCO: Limiting Condition for Operation

Chapter 16 Technical Specifications (2/5)

Risk-Informed Tech. Specs.: Revision 1

Initiative 4b

- Increase the LCOs (SSCs*) to which initiative 4b is applied.
- Initiative 5b (Surveillance Frequency Control Program: SFCP)
 - Incorporate initiative 5b into the Technical Specifications to the extent allowed by regulation.
 - This program relocates Surveillance Frequencies (SFs) to licensee control.

* SSCs: Structures, Systems, and Components

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Chapter 16 Technical Specifications (3/5)

Revision 0 to Revision 1

- > Based on the Customer's Preference
- Extension of Initiative 4b
 - SSCs modeled by PRA
 - As many as possible unless justified to be excluded by other reasons
- > Incorporation of Initiative 5b
 - Time based SF, NOT Event based
 - Exclude SFs that reference other programs (ex. IST)
 - Followed TSTF-425 Rev.2

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Chapter 16 Technical Specifications (4/5)

Initiative 4b applied SSCs

Rev.0	Rev.1
Safety Injection System	RTS Instrumentation
Containment Spray System	ESFAS Instrumentation
CCW System	PAM Instrumentation
ESW System	SDVs
Main Control Room HVAC System	Accumulators
AC Sources	Safety Injection System
DC Sources (Operating and Shutdown)	RWSP
Inverters	Containment Air Locks
	Containment Isolation Valves
	Containment Spray System
	MSIVs
	MSDVs
	EFW Pit
	CCW System
	ESW System
	AC Sources
	DC Sources (Operating)
	Inverters
	Distribution Systems

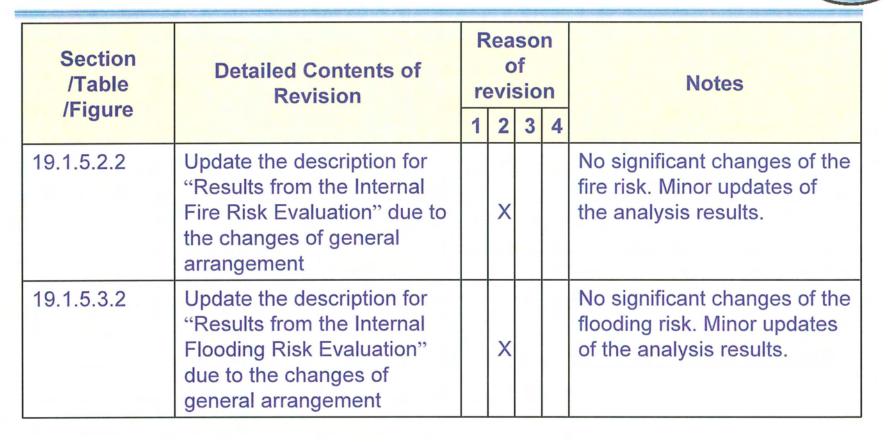
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Chapter 16 Technical Specifications (5/5)

Incorporation of Initiative 5b

- Time based Surveillance Frequency for each surveillance Requirement is described as follows (example):
 - ex. [xx hours OR In accordance with Surveillance Frequency Control Program]
- Definition of SFCP is provided in Administrative Control Section
 Followed TSTF-425 Rev.2

DCD Chapter 19 Revision (1/3)

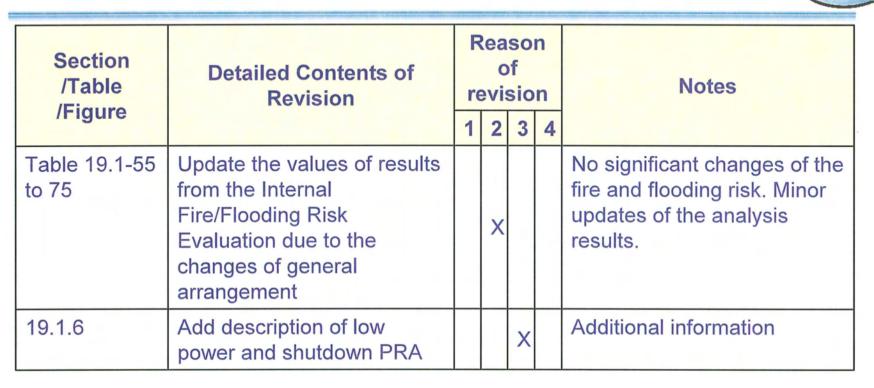


Reason of Revision:

- 1. Incorporation of customer preference items appropriate for the DCD
- 2. Update of the detailed engineering design
- 3. Incorporation of NRC comments and responses to NRC questions
- 4. Incorporation of recently submitted technical reports by references and/or summaries

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DCD Chapter 19 Revision (2/3)

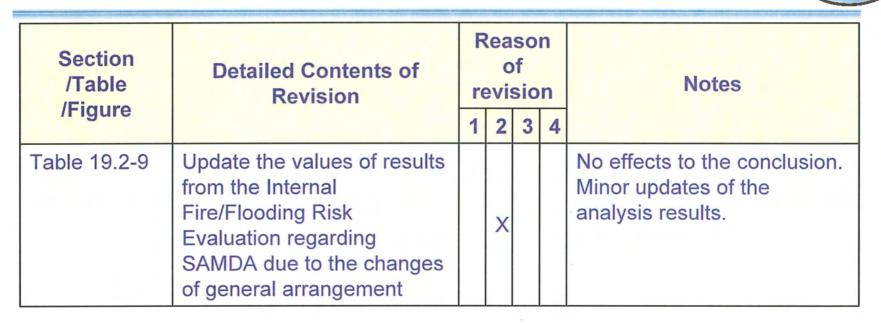


Reason of Revision:

- 1. Incorporation of customer preference items appropriate for the DCD
- 2. Update of the detailed engineering design
- 3. Incorporation of NRC comments and responses to NRC questions
- 4. Incorporation of recently submitted technical reports by references and/or summaries

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DCD Chapter 19 Revision (3/3)



Reason of Revision:

- 1. Incorporation of customer preference items appropriate for the DCD
- 2. Update of the detailed engineering design
- 3. Incorporation of NRC comments and responses to NRC questions
- 4. Incorporation of recently submitted technical reports by references and/or summaries

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Chapter 19 PRA and SA (1/6)



Internal Fire and Internal Flood PRA(1/4)

- Reflect plant arrangement & design changes on Internal Fire PRA and Internal Flood PRA (Subsection 19.1.5.2 and 19.1.5.3)
 - Fire: Fire Compartment Areas & Equipment, Fire Barriers, Cable Routings
 - Flood: Flood Compartment Area & Equipment, Watertight Barriers, Piping lengths, and Water inventories
- Primary impact comes from design changes in the reactor building
- No changes in the methodologies
- No changes in the event trees and fault trees

Chapter 19 PRA and SA (2/6)



Internal Fire and Internal Flood PRA(2/4)

- Effects the results of internal fire PRA
 - ♦ Total risk of internal fire
 - No significant changes in the total CDF & LRF
 - ♦ Dominant scenarios of internal fire
 - Major fire scenarios in the yards are unchanged
 - 1. Yard (Switchyard) fire (70% of CDF)
 - 2. FA6-101-04 (Yard adjacent to T/B) fire (10% of CDF)
 - Changes in the ranking of other scenarios
 - Individual scenario frequencies are very low (<~10⁻⁷/RY)
 » Fire impact is limited in local areas in the reactor building
 » Only simultaneous random failures of intact trains lead to core damage

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Chapter 19 PRA and SA (3/6)



Internal Fire and Internal Flood PRA(3/4)

Effects the results of internal flood PRA

- ♦Total risk of internal flood
 - No significant changes in the total CDF & LRF
- ♦ Dominant scenarios of internal flood
 - No particular major scenarios
 - No significant change in the risk profile
 - Changes in the scenario rankings in the reactor building
 - Individual scenario frequencies are very low (<~10⁻⁷/RY)
 - » Flooding impact is limited in East / West side in the reactor building
 - » Only simultaneous random failures of intact areas lead to core damage

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Chapter 19 PRA and SA (4/6)



Internal Fire and Internal Flood PRA(4/4)

Insignificant changes in the DCD

- •19.1.5.2 Internal Fires Risk Evaluation
- •19.1.5.2.1 Description of the Internal Fires Risk Evaluation
 - -19.1.5.2.2 Results from the Internal Fires Risk Evaluation
- •19.1.5.3 Internal Flooding Risk Evaluation
 - -19.1.5.3.1 Description of the Internal Flooding Risk Evaluation

–19.1.5.3.2 Results from the Internal Flooding Risk Evaluation

Insignificant changes in the Technical Report

♦ US-APWR Probabilistic Risk Assessment, MUAP-07030

Chapter 22 and Chapter 23

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Chapter 19 PRA and SA (5/6)



Response to RAI

- The following are incorporated in the low power and shutdown PRA, subsection 19.1.6, reflecting RAI No.1 question 7
 - Description of initiating events, failures, and coredamage sequences for each POS (12 pages)
 - Revised tables of important human actions and SSCs for each POS (18 tables)
 - Description of the methodology used to evaluate other POSs than mid-loop operation (1 page)
- > Additional descriptions are based on information provided in Technical Report, MUAP-07030

Chapter 19 PRA and SA (6/6)



SAMDA

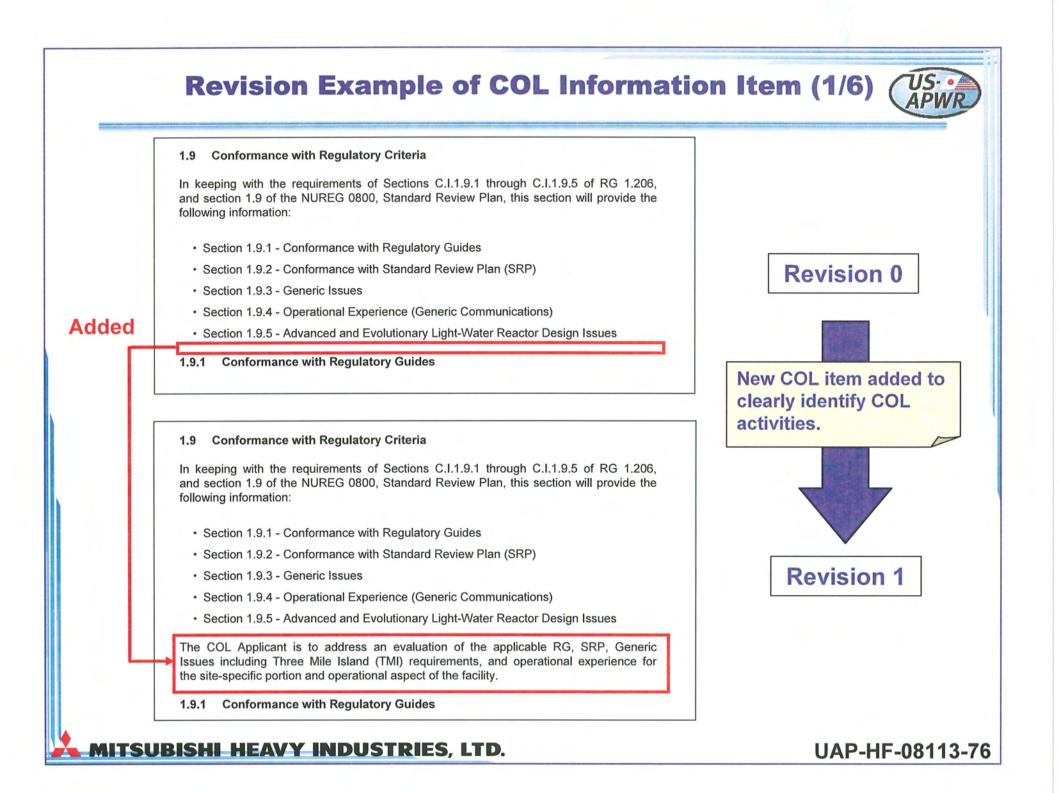
> Update of SAMDA Analysis (Subsection 19.2.6)

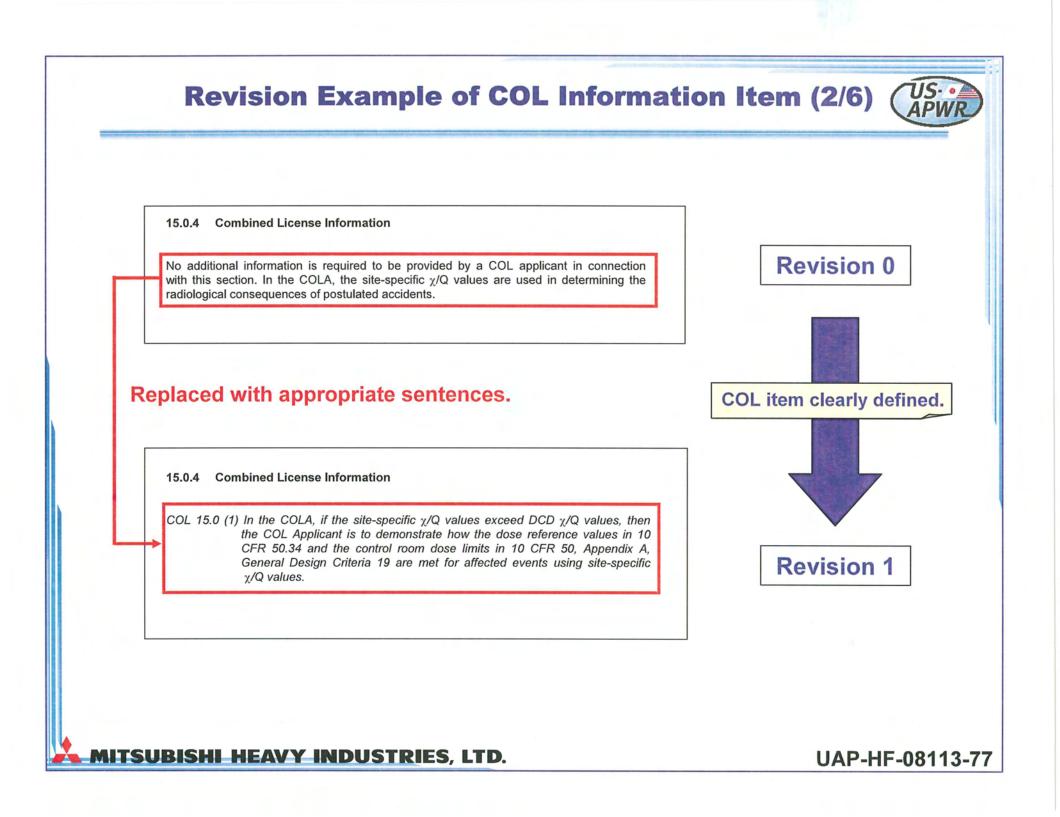
- SAMDA analysis will be updated reflecting the internal fire/flood risk re-evaluation.
- Insignificant impact on cost evaluation and conclusion.
- Environmental Report will be revised accordingly.

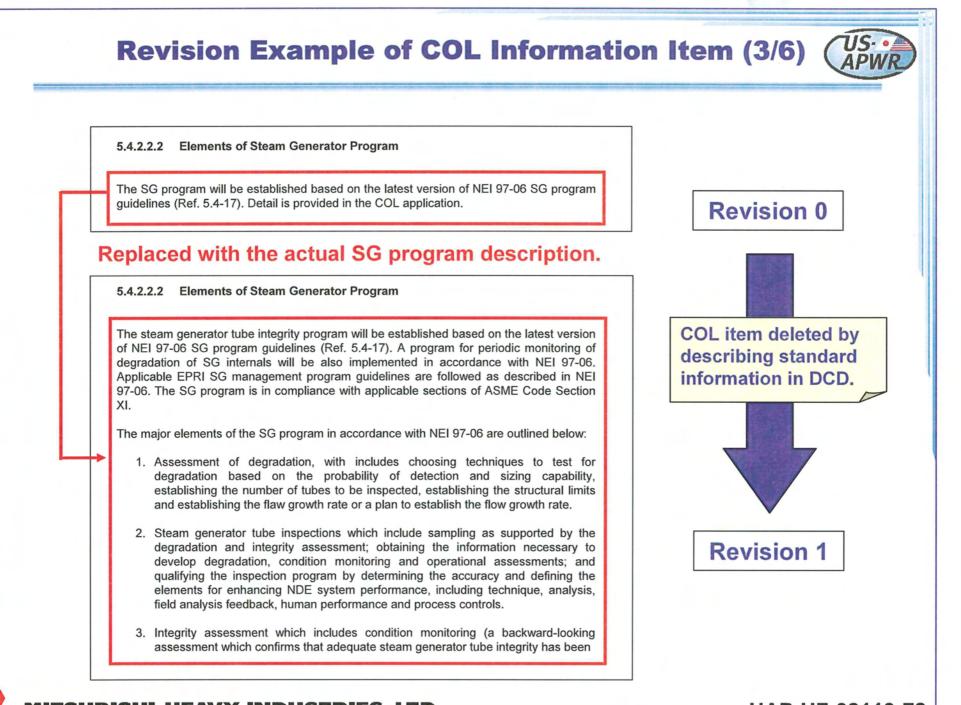
> Resolution of Open Item (Subsection 19.3.1)

 Open item of chapter 19 for DCD Rev.0, "The Level 3 PRA in Section 19.1, and Subsection 19.2.6 and subsections will be completed within March 2008. There will be no open items associated with this Chapter on March 2008." has been resolved so that issuance of the Level 3 PRA technical report, MUAP-08004, was completed in March 2008. **Revision of COL Information Items** (\mathcal{J}_{AP}^{US})

- 1. Updated (revised and/or added)
 - Mainly adjusted with COLA FSAR (i.e., minimize unidentified supplemental information)
- 2. Eliminated
 - Replacement with Standard Information from COLA FSAR
 - Duplicated COL items (e.g. same as ITAAC, technical specification etc.)
 - ✓ Consolidation with the COL item







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Revision Example of COL Information Item (4/6)

Low power and power ascension testing verifies integrated core physics plant operation that is limited to specified power plateaus. The results of all tests associated with each power plateau are reviewed and approved prior to moving to the next, higher power plateau. A full test of ESFs is performed from cold conditions and a reduced flow test is performed from hot conditions prior to fuel load, in accordance with the guidance provided by RG 1.79 (Ref. 6.3-5). The testing under maximum startup loading conditions is performed to verify the adequacy of the electric power supply. Maximum startup loading conditions testing is described in Chapter 14, subsection 14.2.12.1

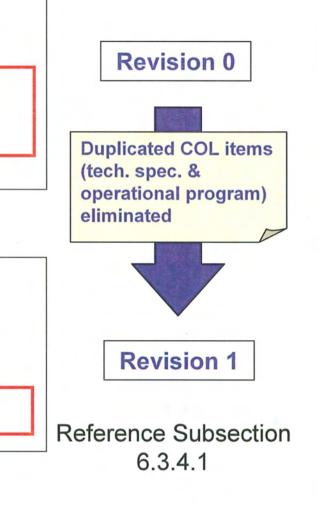
The COL Applicant provides the based for ECCS surveillance requirements for ECCS performance such as motor operated valve and pump performance testing.

The COL Applicant prepares a suitable initial test program consistent with DCD Chapter 14 in accordance with RG 1.68 (Ref. 6.3.-7) to ensure operational readiness.

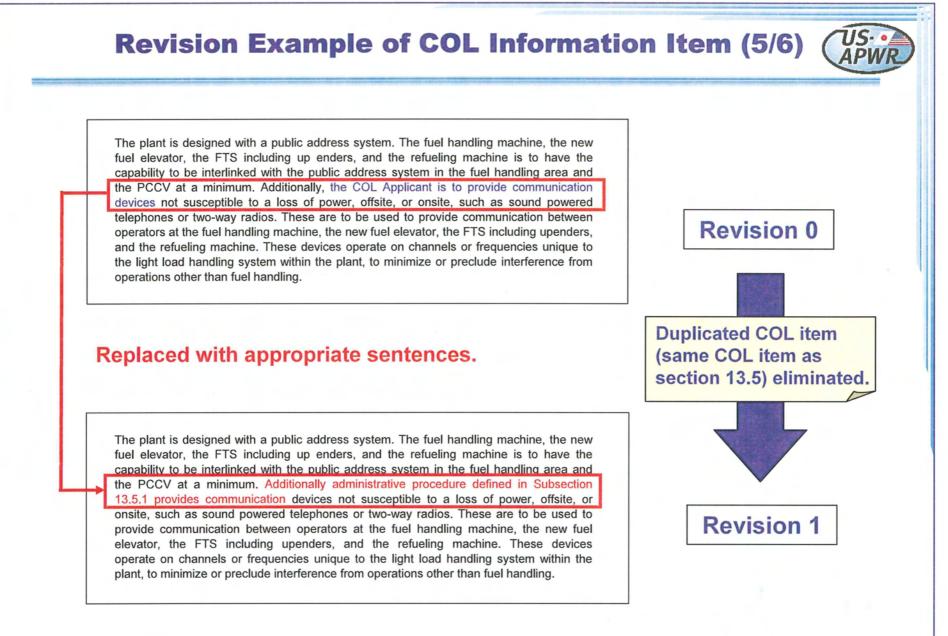
Replaced with appropriate sentences.

Low power and power ascension testing verifies integrated core physics plant operation that is limited to specified power plateaus. The results of all tests associated with each power plateau are reviewed and approved prior to moving to the next, higher power plateau. A full test of ESFs is performed from cold conditions and a reduced flow test is performed from hot conditions prior to fuel load, in accordance with the guidance provided by RG 1.79 (Ref. 6.3-5). The testing under maximum startup loading conditions is performed to verify the adequacy of the electric power supply. Maximum startup loading conditions testing is described in Chapter 14, subsection 14.2.12.1

LCOs, surveillances, and surveillance bases for the ECCS pumps and valves are provided in Subsections 3.5, B 3.5 and 16.1.1.2 of the Technical Specifications

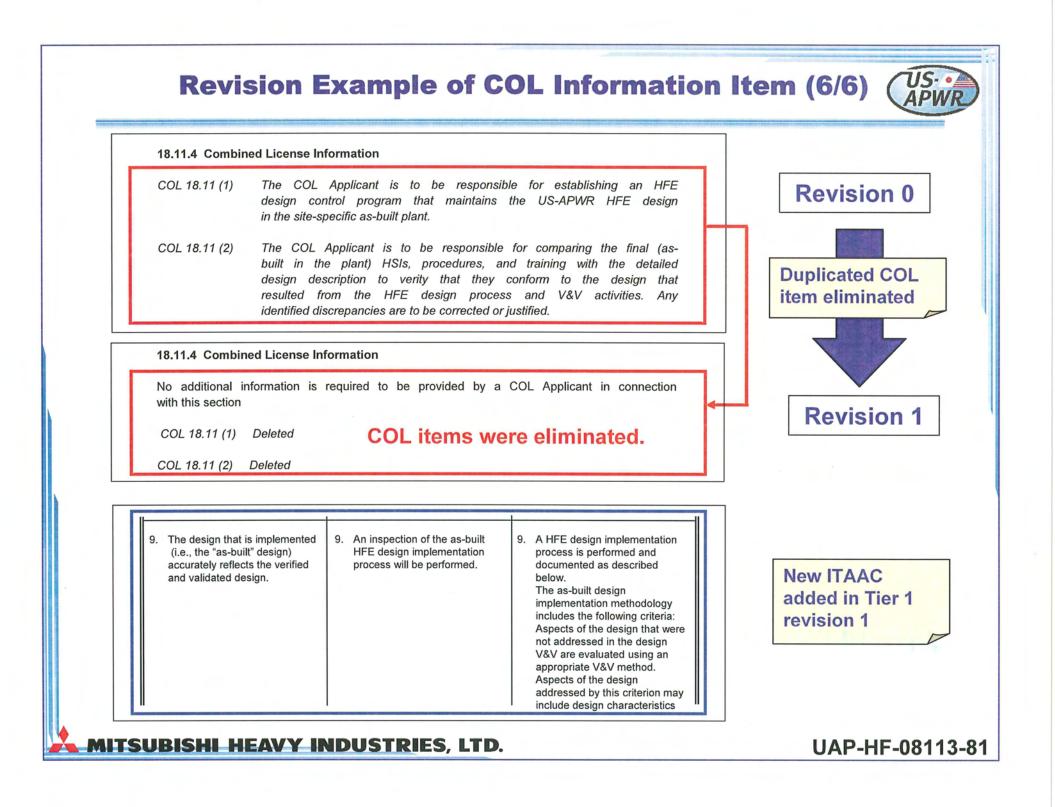






Reference Subsection 9.1.4.5





Summary



- MHI plans to revise the DCD in August 2008. Certain Tier 2 revision will be incorporated to Tier 1. In addition to DCD Rev.1, Environmental Report including SAMDA will be revised.
- The revision will be used for the Reference-COL Application to be submitted in September 2008.
- The presented detail information on the DCD revision will facilitate the NRC's understanding of the DCD revision plan.
- Because the scope of the revisions is minor, these revisions should not impact the NRC's review schedule.
- > These revisions will be clearly identified in the revised DCD.

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