CHAPTER 10 STEAM AND POWER CONVERSION

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CHAPTER 10

STEAM AND POWER CONVERSION

10.1 SUMMARY DESCRIPTION

This section of the referenced DCD is incorporated by reference with the following departures and/or supplements.

10.1.3 COMBINED LICENSE INFORMATION ON EROSION - CORROSION MONITORING

Add the following text at the end of DCD Subsection 10.1.3.

10.1.3.1 Erosion-Corrosion Monitoring

STD COL 10.1-1

The flow accelerated corrosion (FAC) monitoring program analyzes, inspects, monitors and trends those nuclear power plant components that are potentially susceptible to erosion-corrosion damage such as carbon steel components that carry wet steam. In addition, the FAC monitoring program considers the information of Generic Letter 89-08 and industry guidelines.

10.1.3.1.1 Analysis

An industry-sponsored program is used to identify the most susceptible components and to evaluate the rate of wall thinning for components and piping potentially susceptible to FAC. Each susceptible component is tracked in a database and is inspected, based on susceptibility. Analytical methods utilize the results of plant-specific inspection data to develop plant-specific correction factors. This correction accounts for uncertainties in plant data, and for systematic discrepancies caused by plant operation. For each piping component, the analytical method predicts the wear rate, and the estimated time until it must be re-inspected, repaired, or replaced. Carbon steel piping (ASME III and B31.1) that is used for single or multi-phase high temperature flow are the most susceptible to erosion-corrosion damage and receive the most critical analysis.

10.1.3.1.2 Industry Experience

Review and incorporation of industry experience provides a valuable supplement to plant analysis. Industry experience is used to update the program by identifying susceptible components or piping features.

10.1.3.1.3 Inspections

Wall thickness measurements establish the extent of wear in a given component, provide data to help evaluate trends, and provide data to refine the predictive

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model. Components are inspected for wear using ultrasonic techniques (UT), radiography techniques (RT), or by visual observation. The initial inspections are used as a baseline for later inspections. Each subsequent inspection determines the wear rate for the piping and components and the need for inspection frequency adjustment for those components.

10.1.3.1.4 Training and Engineering Judgement

The FAC program is administered by both trained and experienced personnel. Task specific training is provided for plant personnel that implement the monitoring program. Specific non-destructive examination (NDE) is carried out by personnel qualified in the given NDE method. Inspection data is analyzed by engineers or other experienced personnel to determine the overall effect on the system or component.

10.1.3.1.5 Long-Term Strategy

This strategy focuses on reducing wear rates and performing inspections on the most susceptible locations.

10.1.3.2 Procedures

10.1.3.2.1 Generic Plant Procedure

The FAC monitoring program is governed by procedure. This procedure contains the following elements:

- A requirement to monitor and control FAC.
- Identification of the tasks to be performed and associated responsibilities.
- Identification of the position that has overall responsibility for the FAC monitoring program at each plant.
- Communication requirements between the coordinator and other departments that have responsibility for performing support tasks.
- Quality Assurance requirements.
- Identification of long-term goals and strategies for reducing high FAC wear rates.
- A method for evaluating plant performance against long-term goals.

10.1.3.2.2 Implementing Procedures

The FAC implementing procedures provide guidelines for controlling the major tasks. The plant procedures for major tasks are as follows:

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- Identifying susceptible systems.
- Performing FAC analysis.
- Selecting and scheduling components for initial inspection.
- Performing inspections.
- Evaluating degraded components.
- Repairing and replacing components when necessary.
- Selecting and scheduling locations for the follow-on inspections.
- Collection and storage of inspections records.

10.1.3.3 Plant Chemistry

The responsibility for system chemistry is under the purview of the plant chemistry section. The plant chemistry section specifies chemical addition in accordance with plant procedures.

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10.2 TURBINE-GENERATOR

This section of the referenced DCD is incorporated by reference with the following departures and/or supplements.

10.2.2 SYSTEM DESCRIPTION

Add the following sentence at the end of the second paragraph of DCD Subsection 10.2.2.

STD SUP 10.2-1 Subsection 3.5.1.3 addresses the probability of generation of a turbine missile for AP1000 plants in a side-by-side configuration.

Add the following statement at the end of DCD Subsection 10.2.2.

STD SUP 10.2-4 Preoperational and startup tests provide guidance to operations personnel to ensure the proper operability of the turbine generator system.

10.2.3 TURBINE ROTOR INTEGRITY

Add the following statement at the end of DCD Subsection 10.2.3.

Operations and maintenance procedures mitigate the following potential degradation mechanisms in the turbine rotor and buckets/blades: pitting, stress corrosion cracking, corrosion fatigue, low-cycle fatigue, erosion, and erosion-corrosion.

10.2.3.6 Maintenance and Inspection Program Plan

Add the following at the end of the third bullet of DCD Subsection 10.2.3.6.

STD SUP 10.2-2 The main steam stop and control valves are exercised at a frequency recommended by the turbine vendor or valve manufacturer.

Add the following at the end of DCD Subsection 10.2.3.6.

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The inservice inspection (ISI) program for the turbine assembly provides assurance that rotor flaws that lead to brittle fracture of a rotor are detected. The ISI program also coincides with the ISI schedule during shutdown, as required by the ASME Boiler and Pressure Vessel Code, Section XI, and includes complete inspection of all significant turbine components, such as couplings, coupling bolts, turbine shafts, low-pressure turbine blades, low-pressure rotors, and high-pressure rotors. This inspection consists of visual, surface, and volumetric examinations required by the code.

10.2.6 COMBINED LICENSE INFORMATION ON TURBINE MAINTENANCE AND INSPECTION

Replace the text in DCD Subsection 10.2.6 with the following:

A turbine maintenance and inspection program will be submitted to the NRC staff for review prior to fuel load. The program will be consistent with the maintenance and inspection program plan activities and inspection intervals identified in DCD Subsection 10.2.3.6. Plant-specific turbine rotor test data and calculated toughness curves, that support the material property assumptions in the turbine rotor analysis after the fabrication of the turbine, will be available for review prior to fuel load.

10.2-2 Revision 0

10.3 MAIN STEAM SUPPLY SYSTEM

This section of the referenced DCD is incorporated by reference with the following departures and/or supplements. 10.3.2.2.1 Main Steam Piping Add the following at the end of DCD Subsection 10.3.2.2.1. Operations and maintenance procedures include adequate precautions to avoid STD SUP 10.3-1 steam hammer and relief valve discharge reaction load occurrences. 10.3.5.4 Chemical Addition Add the following at the end of DCD Subsection 10.3.5.4. Alkaline chemistry supports maintaining iodine compounds in their nonvolatile STD SUP 10.3-2 form. When iodine is in its elemental form, it is volatile and free to react with organic compounds to create organic iodine compounds, which are not assumed to remain in solution. It is noted that no significant level of organic compounds is expected in the secondary system. The secondary water chemistry, thus, does not directly impact the radioactive iodine partition coefficients. 10.3.6.2 Material Selection and Fabrication Add the following at the end of DCD Subsection 10.3.6.2. Appropriate operations and maintenance procedures provide the necessary STD SUP 10.3-3 controls during operation to minimize the susceptibility of components made of

stainless steel and nickel-based materials to intergranular stress-corrosion cracking by controlling chemicals that are used on system components.

10.3-1 Revision 0

10.4 OTHER FEATURES OF STEAM AND POWER CONVERSION SYSTEM

This section of the referenced DCD is incorporated by reference with the following departures and/or supplements.

10.4.2.2.1 General Description

Revise the first sentence of the third paragraph of DCD Subsection 10.4.2.2.1 to remove the brackets.

VCS CDI

The circulating water system (CWS), or water supplied by the raw water system (RWS) when the CWS is not in operation, provides the cooling water for the vacuum pump seal water heat exchangers.

10.4.2.2.2 Component Description

Revise the fourth sentence of the first paragraph of DCD Subsection 10.4.2.2.2 to remove the brackets.

VCS CDI

Seal water flows through the shell side of the seal water heat exchanger and circulating water, or water supplied by the RWS when the CWS is not in operation, flows through the tube side.

Subsection 10.4.5 is modified using full text incorporation to provide site specific information to replace the DCD conceptual design information (CDI).

DCD

- 10.4.5 CIRCULATING WATER SYSTEM
- 10.4.5.1 Design Basis
- 10.4.5.1.1 Safety Design Basis

The circulating water system (CWS) serves no safety-related function and therefore has no nuclear safety design basis.

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10.4.5.1.2 Power Generation Design Basis

VCS CDI

The CWS supplies cooling water to remove heat from the main condenser. The CWS or makeup water from the RWS supplies cooling water to the turbine building closed cooling water system (TCS) heat exchangers and the condenser vacuum pump seal water heat exchangers under varying conditions of power plant loading and design weather conditions.

DCD

10.4.5.2 System Description

10.4.5.2.1 General Description

Classification of components and equipment in the circulating water system is given in Section 3.2.

VCS COL 10.4-1

The CWS provides a heat sink for the waste heat exhausted from the steam turbine to the main condenser and dissipates this waste heat to the atmosphere using cooling towers. The CWS also provides cooling for the TCS heat exchangers and the condenser vacuum pump seal water heat exchangers. The CWS is shown in Figure 10.4-201. CWS design parameters are provided in Table 10.4-201 and Table 10.4-202.

VCS CDI

The CWS consists of three 33-1/3-percent-capacity circulating water pumps, two mechanical-draft cooling towers, and associated piping, valves, and instrumentation.

DCD

Makeup water to the CWS is provided by the raw water system (RWS). In addition, water chemistry is controlled by the turbine island chemical feed system (CFS).

10.4.5.2.2 Component Description

Circulating Water Pumps

VCS CDI

The three circulating water pumps are vertical, wet pit, single-stage, mixed-flow pumps driven by electric motors. The pumps are mounted in an intake structure

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connected to the cooling tower basins by open flumes. The three pump discharge lines combine in a single main header at the intake structure. This main header with two supply lines to the turbine building forms a common header which connects to the two inlet water boxes of the condenser and may also supply cooling water to the TCS and condenser vacuum pump seal water heat exchangers. Each pump discharge line has a motor-operated butterfly valve located between the pump discharge and the main header. This permits isolation of one pump for maintenance and allows two-pump operation.

Cooling Towers

VCS COL 10.4-1

Two mechanical induced-draft, counterflow cooling towers are sized to reject a single unit's full-load waste heat to the atmosphere and cool the circulating water to less than 91°F based on an entering wet-bulb temperature of 79.4°F. Heat is rejected to the atmosphere primarily through evaporative cooling as circulating water returned from the condenser drops through the tower fill to the tower basins from which it is returned through open flumes to the CWS pump intake structure.

Cooling Tower Makeup and Blowdown

DCD

The circulating water system makeup is provided by the raw water system.

VCS CDI

Makeup to and blowdown from the CWS is controlled by the makeup and blowdown control valves. These valves, along with the CFS, provide chemistry control in the circulating water in order to maintain a noncorrosive, nonscale-forming condition and limit biological growth in CWS components.

Makeup water may be used as a source of cooling water for the TCS and condenser vacuum pump seal water heat exchangers.

DCD Piping and Valves

VCS CDI

The underground portions of the CWS piping are constructed of prestressed concrete pressure piping. The remainder of the piping is carbon steel and is coated internally with a corrosion-resistant compound.

DCD	Motor-operated butterfly valves are provided in each of the circulating water lines at their inlet to and exit from the condenser shell to allow isolation of portions of the condenser.
VCS CDI	Control valves provide regulation of cooling tower blowdown and makeup.
DCD	The circulating water system is designed to withstand the maximum operating discharge pressure of the circulating water pumps.
VCS CDI	Piping includes the expansion joints, butterfly valves, condenser water boxes, and tube bundles.
VCS COL 10.4-1	The design pressure of the condenser portions of the piping is identified in DCD Table 10.4.1-1. The design pressure of the remaining piping is 100 psig.
DCD	Circulating Water Chemical Injection
	Circulating water chemistry is maintained by the turbine island chemical feed system.
VCS CDI	Turbine island chemical equipment injects the required chemicals into the circulating water downstream of the CWS pumps. Chemicals can also be injected at the cooling towers separate from the CFS.
DCD	This maintains a noncorrosive, nonscale-forming condition and limits the biological film formation that reduces the heat transfer rate in the condenser and the heat exchangers supplied by the circulating water system.
VCS COL 10.4-1	The specific chemicals used within the system are based on site water conditions as determined by plant chemistry.

DCD	The chemicals can be divided into six categories based upon function: biocide, algaecide, pH adjuster, corrosion inhibitor, scale inhibitor, and a silt dispersant. The pH adjuster, corrosion inhibitor, scale inhibitor, and dispersant are metered into the system continuously or as required to maintain proper concentrations. The biocide application frequency may vary with seasons.	
VCS CDI	The algaecide is applied, as necessary, to control algae formation on the cooling towers.	
VCS COL 10.4-1	The following chemicals are used to control circulating water chemistry:	
	Biocide - Sodium hypochlorite	
	Algaecide – Quaternary amine	
	pH Adjuster – Sulfuric acid	
	Corrosion Inhibitor – Ortho/polyphosphate	
	Scale Inhibitor – Phosphonate	
	Silt Dispersant – Polyacrylate	
DCD	Addition of biocide and water treatment chemicals is performed by turbine island chemical feed injection metering pumps and is adjusted as required.	
VCS CDI	Chemical concentrations are measured through analysis of grab samples from the CWS.	
DCD	Residual chlorine is measured to monitor the effectiveness of the biocide treatment.	

10.4.5.2.3 System Operation

VCS CDI	The three circulating water pumps take suction from the circulating water pump pit and circulate the water through the tube side of the main condenser, with smaller flows to the TCS and the condenser vacuum pump seal water heat exchangers, and back through the piping discharge network to the cooling towers. See Figure 10.4-201. The cooling towers cool the circulating water by discharging the water above the tower fill material, through which the water then falls to the basins beneath the towers and, in the process, rejects heat to the atmosphere. Circulating water flow to the cooling towers can be diverted directly to the basins, bypassing the cooling towers' internals, by opening the bypass valves. The bypass can be used during plant startup or partial load or to maintain CWS temperatures above 40°F while operating during periods of cold weather.
V00 0DI	The row water evetem cumplies makeup water to the cooling tower basins to
VCS CDI	The raw water system supplies makeup water to the cooling tower basins to replace water losses due to evaporation, drift, and blowdown. Connections are provided to supply water from the RWS to fill the CWS piping and supply cooling for the TCS and condenser vacuum pump seal water heat exchangers when the CWS is not in operation.
DCD	A condenser tube cleaning system is installed to clean the circulating water side of the main condenser tubes.
VCS CDI	Blowdown from the CWS is taken from the discharge of the CWS pumps and is discharged to the plant outfall.
DCD	The circulating water system is used to supply cooling water to the main condenser to condense the steam exhausted from the main turbine.
VCS CDI	If the CWS malfunctions such that condenser backpressure rises above the maximum allowable value, the main condenser will no longer be able to adequately support unit operation.

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DCD

Cooldown of the reactor may be accomplished by using the power-operated atmospheric steam relief valves or safety valves rather than the turbine bypass system when the condenser is not available.

Passage of condensate from the main condenser into the circulating water system through a condenser tube leak is not possible during power generation operation, since the circulating water system operates at a greater pressure than the condenser.

VCS CDI

Turbine building closed cooling water in the TCS heat exchangers is maintained at a higher pressure than the circulating water or raw water to prevent leakage of the circulating water or raw water into the closed cooling water system.

Cooling water to the condenser vacuum pump seal water heat exchangers is supplied from the circulating water or raw water system. Cooling water flow from the circulating water system is normally maintained through all four heat exchangers to facilitate placing the spare condenser vacuum pump in service.

DCD

Isolation valves are provided for the condenser vacuum pump seal water heat exchanger cooling water supply lines to facilitate maintenance.

Small circulating water system leaks in the turbine building will drain into the waste water system. Large circulating water system leaks due to pipe failures will be indicated in the control room by a loss of vacuum in the condenser shell. The effects of flooding due to a circulating water system failure, such as the rupture of an expansion joint, will not result in detrimental effects on safety-related equipment since there is no safety-related equipment in the turbine building and the base slab of the turbine building is located at grade elevation. Water from a system rupture will run out of the building through a relief panel in the turbine building west wall before the level could rise high enough to cause damage. Site grading will carry the water away from safety-related buildings.

VCS CDI

The cooling towers are located to prevent adverse interactions with structures, systems, and components (SSCs) required for safe shutdown of the plant in case of a collapse of the towers or failure of their basins and flumes.

DCD

10.4.5.3 Safety Evaluation

The circulating water system has no safety-related function and therefore requires no nuclear safety evaluation.

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10.4.5.4 Tests and Inspections

Components of the circulating water system are accessible as required for inspection during plant power generation.

The circulating water pumps are tested in accordance with standards of the VCS CDI Hydraulic Institute.

DCD Performance, hydrostatic, and leakage tests associated with preinstallation and preoperational testing are performed on the circulating water system. The system performance and structural and leaktight integrity of system components are demonstrated by continuous operation.

> 10.4.5.5 Instrumentation Applications

VCS CDI Instrumentation provided indicates the open and closed positions of motoroperated butterfly valves in the circulating water piping. The motor-operated valve at each pump discharge is interlocked with the pump so that the pump trips if the discharge valve fails to reach the full-open position shortly after starting the pump.

> Local grab samples are used to periodically test the circulating water quality to limit harmful effects to the system piping and valves due to improper water chemistry.

Pressure indication is provided on the circulating water pump discharge lines.

A differential pressure transmitter is provided between one inlet and outlet branch to the condenser. This differential pressure transmitter is used to determine the frequency of operating the condenser tube cleaning system (CES).

Temperature indication is supplied on the common CWS inlet header to the TCS heat exchanger trains. This temperature is also representative of the inlet cooling water temperature to the main condenser.

A flow element is provided for the common discharge line from the TCS heat exchangers to allow monitoring of the total flow through the TCS heat exchangers. Flow measurement for the raw water makeup to the cooling towers and for CWS blowdown is also provided.

VCS CDI

DCD

VCS CDI	Level instrumentation provided in the circulating water pump intake structure and cooling tower basins controls makeup flow from the RWS to the cooling tower basins and annunciates on low-water level at the pump intake structure and on high-water level in the cooling tower basins.	
VCS COL 10.4-1	The circulating water chemistry is controlled by CWS blowdown and chemical addition to maintain the circulating water with an acceptable Langelier Index as specified in plant chemistry procedures. The system accomplishes this by regulating the blowdown valve. This regulation causes the cooling tower basin water levels to fluctuate. The fluctuation is sensed by level controllers that operate the cooling tower makeup valves.	
DCD	The control approach is to allow the makeup water to concentrate naturally to its upper limit. Provisions are made to add chemicals for pH control.	
VCS CDI	The cycles of concentration at which the cooling towers is operated are dependent on the quality of the cooling tower makeup water. Blowdown is directed to the waste water system (blowdown sump) and dechlorinated as needed before discharge at the plant outfall.	
DCD	Monitoring of the circulating water system is performed through the data display and processing system. Control functions are performed by the plant control system. Appropriate alarms and displays are available in the control room. See Chapter 7.	
	10.4.7.2.1 General Description	
	Replace the last sentence of the sixth paragraph of DCD Subsection 10.4.7.2.1 as	

follows.

VCS COL 10.4-2	The oxygen scavenger agent is hydrazine or carbohydrazide and the pH control agent is ammonia (ammonium hydroxide) or morpholine.	
STD SUP 10.4-1	Add new paragraph at the end of the DCD Subsection 10.4.7.2.1: Operations and maintenance procedures include appropriate precautions to avoid steam/water hammer occurrences.	
	10.4.12.1 Circulating Water System	
VCS COL 10.4-1	This COL Item is addressed in Subsection 10.4.5 with specific discussion of CWS configuration in Subsection 10.4.5.2.1, design pressure and cooling towers in Subsection 10.4.5.2.2, and specific chemicals and chemistry in Subsections 10.4.5.2.2 and 10.4.5.5.	
	10.4.12.2 Condensate, Feedwater and Auxiliary Steam System Chemistry Control.	
VCS COL 10.4-2	This COL Item is addressed in Subsection 10.4.7.2.1.	
	10.4.12.3 Potable Water	
VCS COL 10.4-3	This COL item is duplicated in the Subsection 9.2.12.1 COL Item and is addressed as stated in that subsection.	

TABLE 10.4-201 SUPPLEMENTAL MAIN CONDENSER DESIGN DATA

Condenser Data

VCS CDI Circulating water flow

600,000 gpm

Note: This table supplements DCD Table 10.4.1-1.

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VCS COL 10.4-1

TABLE 10.4-202 SUPPLEMENTAL DESIGN PARAMETERS FOR MAJOR CIRCULATING WATER SYSTEM COMPONENTS

Circulating Water Pump	
Quantity	Three per unit
Flow rate (gal/min)	211,267
Mechanical Draft Cooling Tower	
Quantity	Two per unit
Approach temperature (°F)	10.7
Inlet temperature (°F)	114.8
Outlet temperature (°F)	90.1
Approximate Temperature range (°F)	24.7
Flow rate (gal/min)	309,400
Heat transfer (Btu/hr)	3,815 x 10 ⁶
Wind velocity design (mph) Seismic design criteria per Uniform Building Code	110

Note: This table supplements DCD Table 10.4.5-1.