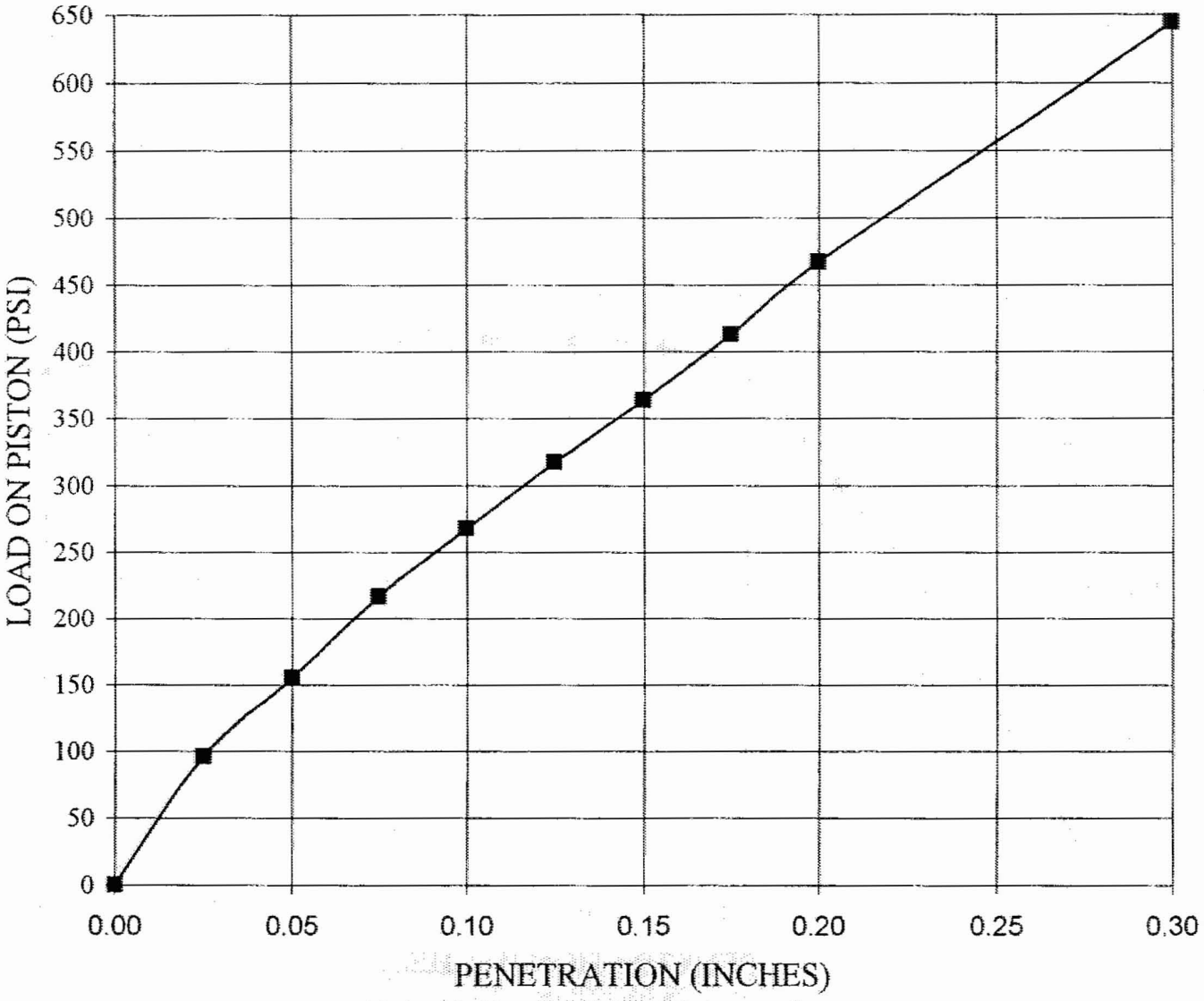
## UNSOAKED CBR




## CALIFORNIA BEARING RATIO

ASTM D-1883

| | | | | | |
|---|---|---|---|---|---|
| Project: | Constellation Energy Group COLA Project, Calvert Cliffs NuclearPower Plant (CCNPP), Calvert County, Maryland | Contract No.: | 06120048.00 | Date: | 9/29/2006 |

| Boring No. | Depth (ft) | Sample Description |
|---|---|---|
| TP-C-723 | 2.5-3.5 | Clayey SAND, dark brown |

| | | | |
|---|---|---|---|
| **CBR (Unsoaked):** | **26.8** | Soaking Time: | N/A |
| Surcharge: | 50 PSF | Swell: | N/A |

| DRY DENSITY, PCF | | MOISTURE CONTENT, % | |
|---|---|---|---|
| Before Soaking: | 126.3 | Before Soaking: | 7.2 |
| After Soaking: | N/A | After Soaking: | N/A |
| Max. Dry Density: | 132.8 | Optimum Moisture: | 7.3 |

Schnabel

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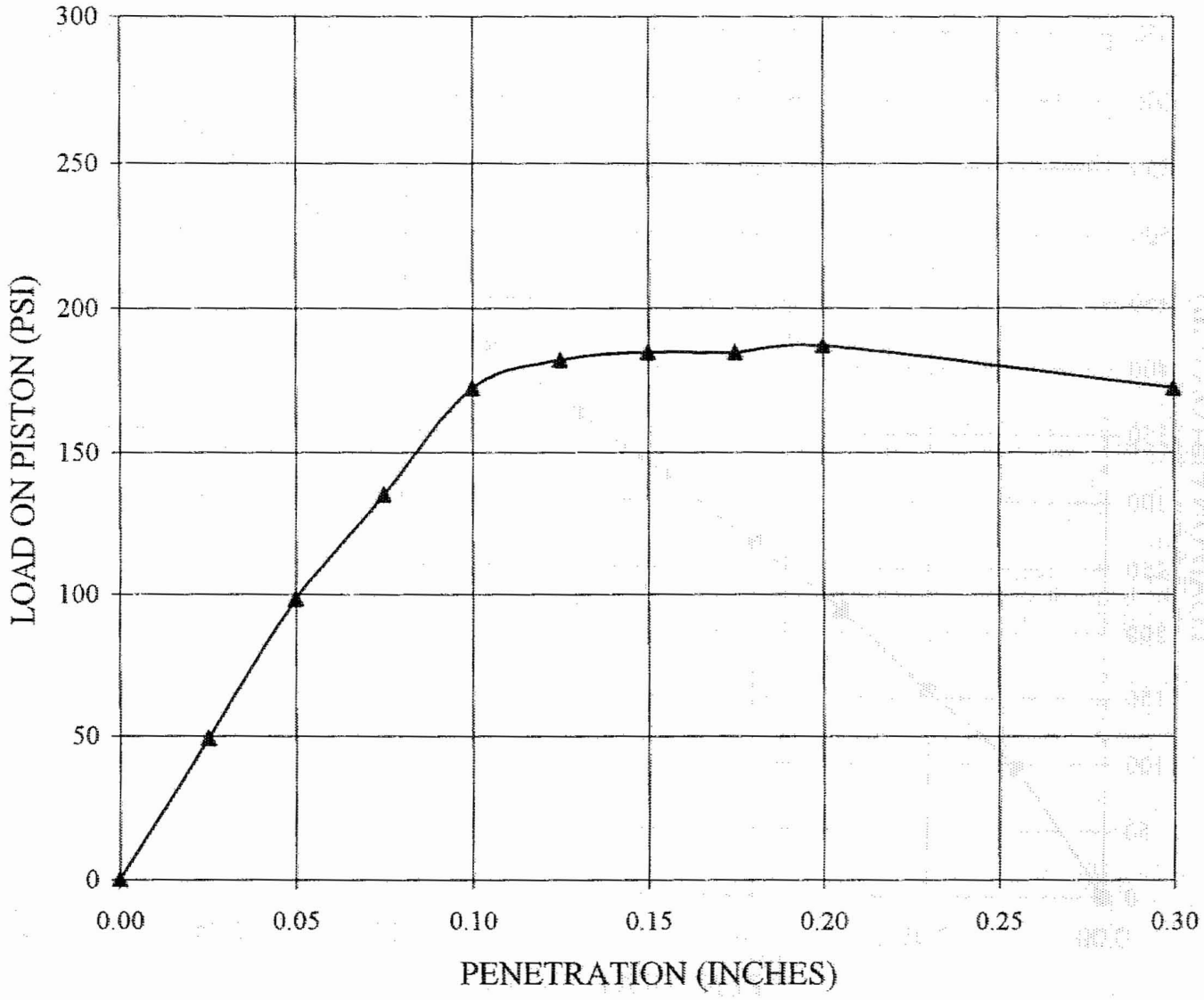
## SOAKED CBR




## CALIFORNIA BEARING RATIO

ASTM D-1883

| | | | | | |
|---|---|---|---|---|---|
| Project: | Constellation Energy Group COLA Project, Calvert Cliffs NuclearPower Plant (CCNPP), Calvert County, Maryland | Contract No.: | 06120048.00 | Date: | 9/29/2006 |

| Boring No. | Depth (ft) | Sample Description |
|---|---|---|
| TP-C-723 | 2.5-3.5 | Clayey SAND, dark brown |

| | | | |
|---|---|---|---|
| **CBR (Soaked):** | **17.2** | Soaking Time: | 4 Days |
| Surcharge: | 50 PSF | Swell: | 0.5% |

| DRY DENSITY, PCF | | MOISTURE CONTENT, % | |
|---|---|---|---|
| Before Soaking: | 126.3 | Before Soaking: | 7.2 |
| After Soaking: | 125.5 | After Soaking: | 9.2 |
| Max. Dry Density: | 132.8 | Optimum Moisture: | 7.3 |

Schnabel

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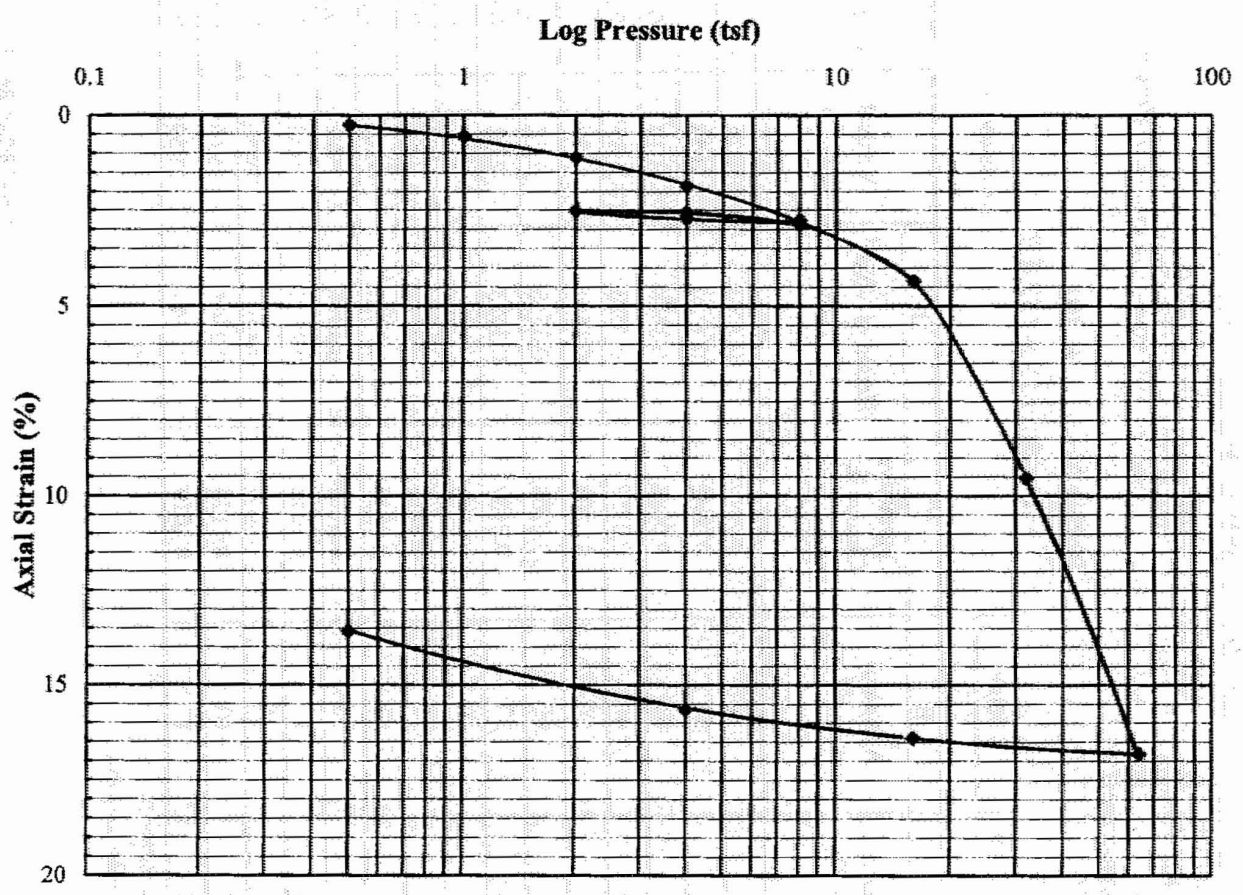
# CONSOLIDATION RESULTS




REVISED FORM FOR
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| | | | | | |
|---|---|---|---|---|---|
| **Probable Preconsolidation Pressure (Pp), tsf:** | *20* | | | **Recompression Ratio (Cεr):** | *0.005* |
| **Type of Specimen:** | *Tube Sample* | | | **Compression Ratio (Cεc):** | *0.243* |
| **Description:** | *FAT CLAY (CH), contains mica - gray* | | | | **Initial** / **Final** |
| | | | | **Water Content, %** | *36.4* / *28.6* |
| **LL:** *76* | **PI:** *46* | **Gs:** *2.68* | **$P_c'$ (tsf):** *5.15* | **Void Ratio** | *1.01* / *0.73* |
| **% < No. 200:** *99.5* | | **Test Method:** | *ASTM D2435 Method A* | **Saturation, %** | *97* / *100* |
| **Test Condition:** | *Inundated @ 1 tsf* | | | **Dry Unit Weight, pcf** | *83.3* / *96.4* |

**Remarks:** Coefficient of Consolidation, Cv, equals 2448, 591, and 1764 ft2/yr at average pressures of 6, 12, and 24 tsf (square root of time method).

**Average Water Content of Trimmings, %:** *35.3*

**Project:** Calvert Cliffs Nuclear Power Plant

| | | | |
|---|---|---|---|
| **Location:** | *Calvert County, MD* | | |
| **Boring:** | *B-301* | **Schnabel No.:** | *06120048* |
| **Depth:** | *158.5-159.6 ft* | **Elevation:** | *-61.7 to -62.8* |
| **Date:** | *10/13/2006* | **Reviewed by:** | *CJS* |

Schnabel
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**Consolidation Test Report**

# Consolidation Test Data Sheet

Consolidometer ID: 5

10/13/06

REVISED FORM FOR
NCR NO. 25237-NCR-028
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Schnabel Contract: *06120048*

Test Method: *ASTM D2435 Method A*

Project: *Calvert Cliffs Nuclear Power Plant*

Test Condition: *Inundated @ 1 tsf*

Initial Height of Specimen ($H_o$), in.: 0.7499

Boring No.: *B-301*

Height of Solids ($H_s$), in.: 0.3737

Depth: *158.5-159.6 ft*

Seating Press. (tsf): 0.05

Initial Dial Gauge Reading ($D_o$), in.: 0.0000

Reviewed by: CJS

| Pressure, P (tsf) | TimeReadings Required | Date Load Applied | Time Load Applied | Load Applied By | A<br>Final[1] Dial Reading, $D_{fi}$<br>x $10^{-4}$ in. | B<br>Apparatus Correction[2], $D_{ci}$<br>x $10^{-4}$ in. | C<br>Cumulative Change in Height[3], $\Delta H_i$<br>in. | D<br>Height of Voids[4], $H_{vi}$<br>in. | Vertical Strain[5], $\varepsilon_i$<br>(%) | Void Ratio[6], $e_i$ |
|---|---|---|---|---|---|---|---|---|---|---|
| 0.5 | | 9/13/2006 | 9:00 | DWC | 31 | 12 | 0.0019 | 0.3743 | 0.25 | 1.002 |
| 1 | | 9/14/2006 | 9:00 | DWC | 63 | 21 | 0.0042 | 0.3720 | 0.56 | 0.996 |
| 2 | | 9/15/2006 | 9:00 | DWC | 117 | 33 | 0.0084 | 0.3678 | 1.12 | 0.984 |
| 4 | | 9/16/2006 | 9:00 | CJS | 179 | 40 | 0.0139 | 0.3623 | 1.85 | 0.970 |
| 8 | | 9/18/2006 | 9:15 | CJS | 258 | 50 | 0.0208 | 0.3554 | 2.77 | 0.951 |
| 4 | | 9/19/2006 | 9:25 | CJS | 244 | 40 | 0.0204 | 0.3558 | 2.72 | 0.952 |
| 2 | | 9/20/2006 | 9:25 | CJS | 222 | 33 | 0.0189 | 0.3573 | 2.52 | 0.956 |
| 4 | | 9/21/2006 | 9:25 | CJS | 233 | 40 | 0.0193 | 0.3569 | 2.57 | 0.955 |
| 8 | | 9/22/2006 | 9:25 | CJS | 265 | 50 | 0.0215 | 0.3547 | 2.87 | 0.949 |
| 16 | | 9/25/2006 | 9:30 | DWC | 389 | 63 | 0.0326 | 0.3436 | 4.35 | 0.920 |
| 32 | | 9/26/2006 | 9:25 | DWC | 791 | 76 | 0.0715 | 0.3047 | 9.53 | 0.815 |
| 64 | | 9/27/2006 | 9:25 | DWC | 1349 | 87 | 0.1262 | 0.2500 | 16.83 | 0.669 |
| 16 | | 9/28/2006 | 9:25 | DWC | 1293 | 63 | 0.1230 | 0.2532 | 16.40 | 0.678 |
| 4 | | 9/29/2006 | 9:25 | DWC | 1214 | 40 | 0.1174 | 0.2588 | 15.66 | 0.693 |
| 0.5 | | 10/2/2006 | 9:25 | DWC | 1031 | 12 | 0.1019 | 0.2743 | 13.59 | 0.734 |

Notes:
1. "Final" based on test method; 24 hrs for Method A, end of primary for Method B.
2. Correction value, for the current pressure, from the consolidometer's calibration curve.
3. $\Delta H = D_{fi} - D_o - D_{ci}$ = Col. A - $D_o$ - Col. B
4. $H_{vi} = (H_o - H_s) - \Delta H$
5. $\varepsilon_i = (\Delta H / H_o) \times 100$ = (Col. C / $H_o$) x 100
6. $e_i = H_{vi} / Hs$ = Col. D / Hs

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# Load Time Readings

10/13/06

Project: Calvert Cliffs Nuclear Power Plant
Schnabel Contract: 06120048
Boring No.: B-301 Depth: 158.5-159.6 ft

Consol. ID: 5 Reviewed by: CJS

| Elapsed Time (min.) | Dial Guage Readings (inches) | | | | | |
|---|---|---|---|---|---|---|
| | 8 tsf Initial Load 9/18/2006 | 16 tsf Initial Load 9/25/2006 | 32 tsf Load 9/26/2006 | X tsf Load Date | X tsf Load Date | X tsf Load Date |
| 0.1 | 0.0229 | 0.0329 | 0.0521 | | | |
| 0.25 | 0.0232 | 0.0335 | 0.0550 | | | |
| 0.5 | 0.0234 | 0.0339 | 0.0568 | | | |
| 1 | 0.0237 | 0.0343 | 0.0586 | | | |
| 2 | 0.0238 | 0.0346 | 0.0603 | | | |
| 4 | 0.0240 | 0.0350 | 0.0621 | | | |
| 8 | 0.0242 | 0.0353 | 0.0638 | | | |
| 15 | 0.0244 | 0.0357 | 0.0655 | | | |
| 30 | 0.0246 | 0.0361 | 0.0675 | | | |
| 60 | 0.0247 | 0.0365 | 0.0694 | | | |
| 120 | 0.0250 | 0.0370 | 0.0715 | | | |
| 240 | 0.0252 | 0.0375 | 0.0737 | | | |
| 480 | 0.0254 | 0.0380 | 0.0761 | | | |
| 720 | 0.0254 | 0.0383 | 0.0770 | | | |
| 960 | 0.0255 | 0.0385 | 0.0778 | | | |
| 1200 | 0.0256 | 0.0386 | 0.0785 | | | |
| 1440 | 0.0258 | 0.0389 | 0.0791 | | | |
| 1680 | | | | | | |
| 1920 | | | | | | |
| 2160 | | | | | | |
| 2400 | | | | | | |
| 2640 | | | | | | |
| 2880 | | | | | | |
| | | | | | | |
| | | | | | | |

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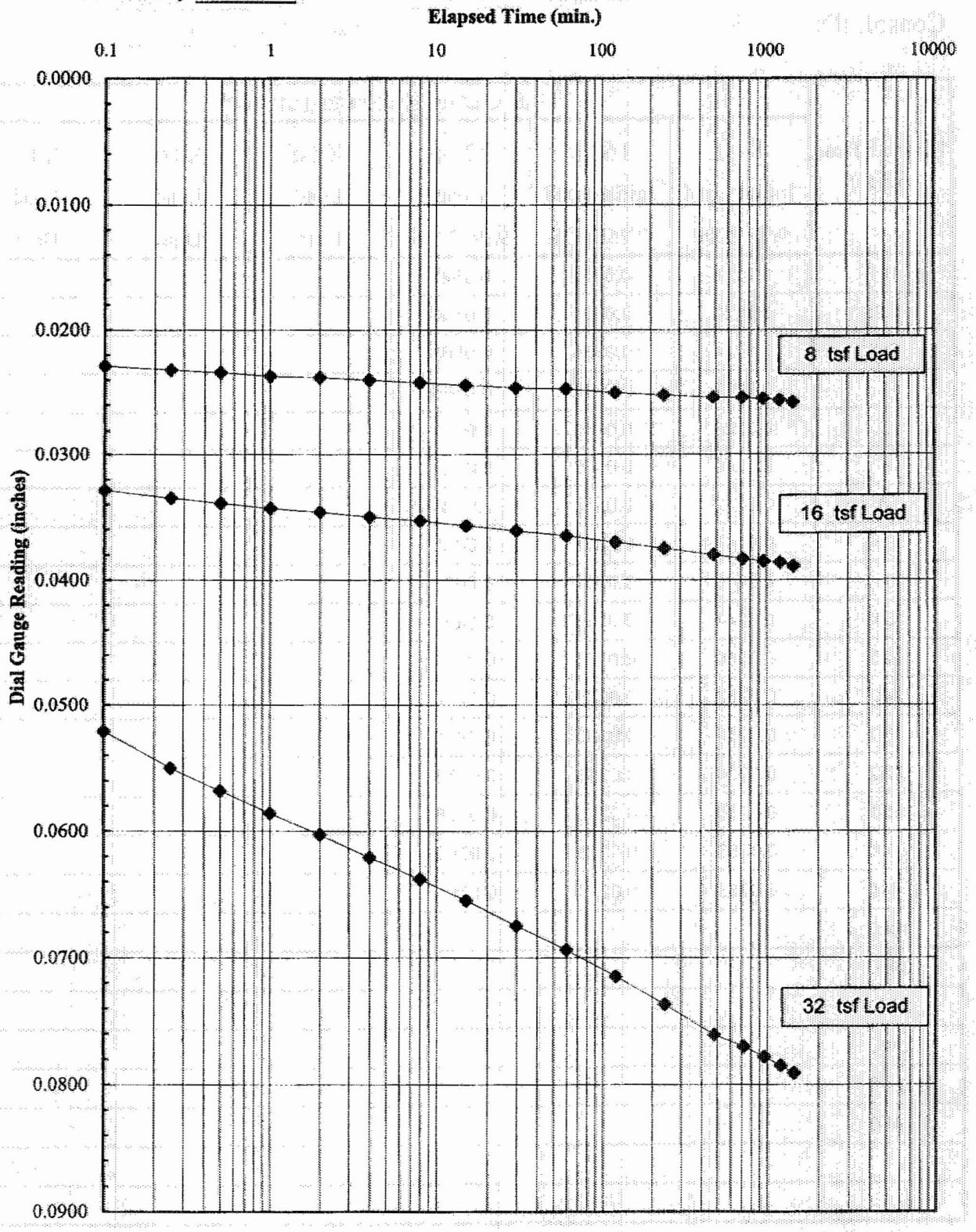
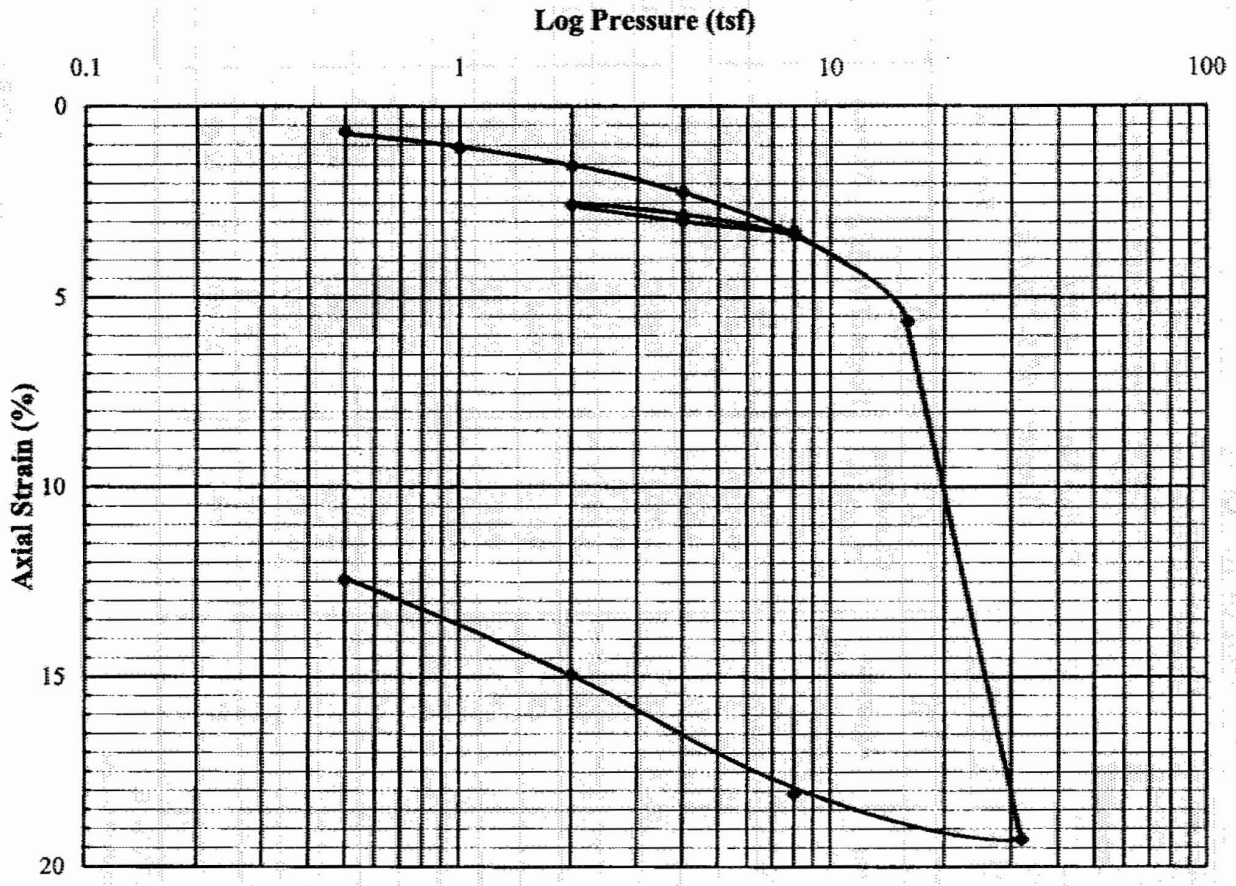
# Consolidation Time Curves

10/13/06

Project: Calvert Cliffs Nuclear Power Plant
Schnabel Contract: 06120048
Boring No.: B-301 Depth: 158.5-159.6 ft

Reviewed by: CJS



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2/12/07

| | | | |
|---|---|---|---|
| **Probable Preconsolidation Pressure (Pp), tsf:** | *16* | **Recompression Ratio (Cεr):** | *0.012* |
| **Type of Specimen:** | *Tube Sample* | **Compression Ratio (Cεc):** | *0.453* |
| **Description:** | *SANDY FAT CLAY (CH) - gray* | | |

| | Initial | Final |
|---|---|---|
| Water Content, % | 66.4 | 56.8 |
| Void Ratio | 1.82 | 1.46 |
| Saturation, % | 96 | 100 |
| Dry Unit Weight, pcf | 58.0 | 66.3 |

| | | | | | |
|---|---|---|---|---|---|
| **LL:** | *112* | **PI:** | *73* | **Gs:** | *2.62* |
| **$P_c'$ (tsf):** | *5.45* | | | | |
| **% < No. 200:** | *66.2* | **Test Method:** | *ASTM D2435 Method A* | | |
| **Test Condition:** | *Inundated @ 1 tsf* | | | | |

**Remarks:** Coefficient of Consolidation, Cv, equals 3037, 754, and 110 ft2/yr at average pressures of 3, 12, and 24 tsf (square root of time method).

**Average Water Content of Trimmings, %:** *64.9*

**Project:** Calvert Cliffs Nuclear Power Plant

| | | | |
|---|---|---|---|
| **Location:** | *Calvert County, MD* | | |
| **Boring:** | *B-301* | **Schnabel No.:** | *06120048* |
| **Depth:** | *168.5-170.4 ft* | **Elevation:** | *-71.7 to -73.6* |
| **Date:** | *10/14/2006* | **Reviewed by:** | *CJS* |

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# Consolidation Test Report

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# Consolidation Test Data Sheet

Consolidometer ID: 2

10/14/06

REVISED FORM FOR
NCR NO. 25237-NCR-028
2/12/2007

Schnabel Contract: *06120048*

Test Method: *ASTM D2435 Method A*

Project: *Calvert Cliffs Nuclear Power Plant*

Test Condition: *Inundated @ 1 tsf*

Initial Height of Specimen ($H_o$), in.: 0.7611

Boring No.: *B-301*

Height of Solids ($H_s$), in.: 0.2703

Depth: *168.5-170.4 ft*

Seating Press. (tsf): 0.05

Initial Dial Gauge Reading ($D_o$), in.: 0.0000

Reviewed by: CJS

| Pressure, P (tsf) | Time Readings Required | Date Load Applied | Time Load Applied | Load Applied By | A: Final[1] Dial Reading, $D_{fi}$ x $10^{-4}$ in. | B: Apparatus Correction[2], $D_{ci}$ x $10^{-4}$ in. | C: Cumulative Change in Height[3], $\Delta H_i$ in. | D: Height of Voids[4], $H_{vi}$ in. | Vertical Strain[5], $\varepsilon_i$ (%) | Void Ratio[6], $e_i$ |
|---|---|---|---|---|---|---|---|---|---|---|
| 0.5 | | 9/12/2006 | 9:15 | DWC | 61 | 11 | 0.0050 | 0.4858 | 0.66 | 1.797 |
| 1 | | 9/13/2006 | 9:15 | DWC | 97 | 15 | 0.0082 | 0.4826 | 1.08 | 1.785 |
| 2 | | 9/14/2006 | 9:15 | DWC | 139 | 21 | 0.0118 | 0.4790 | 1.55 | 1.772 |
| 4 | | 9/15/2006 | 9:15 | DWC | 198 | 28 | 0.0170 | 0.4738 | 2.23 | 1.753 |
| 8 | | 9/16/2006 | 9:15 | CJS | 283 | 36 | 0.0247 | 0.4661 | 3.25 | 1.724 |
| 4 | | 9/18/2006 | 9:20 | CJS | 255 | 28 | 0.0227 | 0.4681 | 2.98 | 1.732 |
| 2 | | 9/19/2006 | 9:30 | CJS | 216 | 21 | 0.0195 | 0.4713 | 2.56 | 1.744 |
| 4 | | 9/20/2006 | 9:30 | CJS | 244 | 28 | 0.0216 | 0.4692 | 2.84 | 1.736 |
| 8 | | 9/21/2006 | 9:30 | CJS | 290 | 36 | 0.0254 | 0.4654 | 3.34 | 1.722 |
| 16 | | 9/22/2006 | 9:35 | CJS | 474 | 45 | 0.0429 | 0.4479 | 5.64 | 1.657 |
| 32 | | 9/25/2006 | 9:35 | DWC | 1525 | 57 | 0.1468 | 0.3440 | 19.29 | 1.273 |
| 8 | | 9/27/2006 | 9:35 | DWC | 1412 | 36 | 0.1376 | 0.3532 | 18.08 | 1.307 |
| 2 | | 9/28/2006 | 9:30 | DWC | 1158 | 21 | 0.1137 | 0.3771 | 14.94 | 1.395 |
| 0.5 | | 9/29/2006 | 9:30 | DWC | 959 | 11 | 0.0948 | 0.3960 | 12.46 | 1.465 |
| | | | | | | | | | | |

Notes:
1. "Final" based on test method; 24 hrs for Method A, end of primary for Method B.
2. Correction value, for the current pressure, from the consolidometer's calibration curve.
3. $\Delta H = D_{fi} - D_o - D_{ci}$ = Col. A - $D_o$ - Col. B
4. $H_{vi} = (H_o - H_s) - \Delta H$
5. $\varepsilon_i = (\Delta H / H_o) \times 100 = (\text{Col. C} / H_o) \times 100$
6. $e_i = H_{vi} / Hs$ = Col. D / Hs

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Schnabel
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# Load Time Readings

10/14/06

Project: Calvert Cliffs Nuclear Power Plant
Schnabel Contract: 06120048
Boring No.: B-301 Depth: 168.5-170.4 ft

Consol. ID: 2 Reviewed by: CJS

| Elapsed Time (min.) | Dial Guage Readings (inches) | | | | | |
|---|---|---|---|---|---|---|
| | 4 tsf Reload 9/20/2006 | 16 tsf Load 9/22/2006 | 32 tsf Load 9/23/2006 | X tsf Load Date | X tsf Load Date | X tsf Load Date |
| 0.1 | 0.0235 | 0.0352 | 0.0591 | | | |
| 0.25 | 0.0239 | 0.0368 | 0.0638 | | | |
| 0.5 | 0.0239 | 0.0380 | 0.0686 | | | |
| 1 | 0.0239 | 0.0388 | 0.0745 | | | |
| 2 | 0.0240 | 0.0394 | 0.0816 | | | |
| 4 | 0.0240 | 0.0400 | 0.0895 | | | |
| 8 | 0.0240 | 0.0407 | 0.0977 | | | |
| 15 | 0.0240 | 0.0413 | 0.1055 | | | |
| 30 | 0.0241 | 0.0419 | 0.1137 | | | |
| 60 | 0.0241 | 0.0427 | 0.1216 | | | |
| 120 | 0.0242 | 0.0435 | 0.1293 | | | |
| 240 | 0.0242 | 0.0444 | 0.1365 | | | |
| 480 | 0.0245 | 0.0456 | 0.1434 | | | |
| 720 | 0.0245 | 0.0463 | 0.1467 | | | |
| 960 | 0.0244 | 0.0467 | 0.1490 | | | |
| 1200 | 0.0244 | 0.0471 | 0.1509 | | | |
| 1440 | 0.0244 | 0.0474 | 0.1525 | | | |
| 1680 | | 0.0478 | 0.1539 | | | |
| 1920 | | 0.0480 | 0.1551 | | | |
| 2160 | | 0.0481 | 0.1559 | | | |
| 2400 | | 0.0484 | 0.1567 | | | |
| 2640 | | 0.0487 | 0.1574 | | | |
| 2880 | | 0.0488 | 0.1580 | | | |
| | | | | | | |
| | | | | | | |

Schnabel Engineering

# Consolidation Time Curves

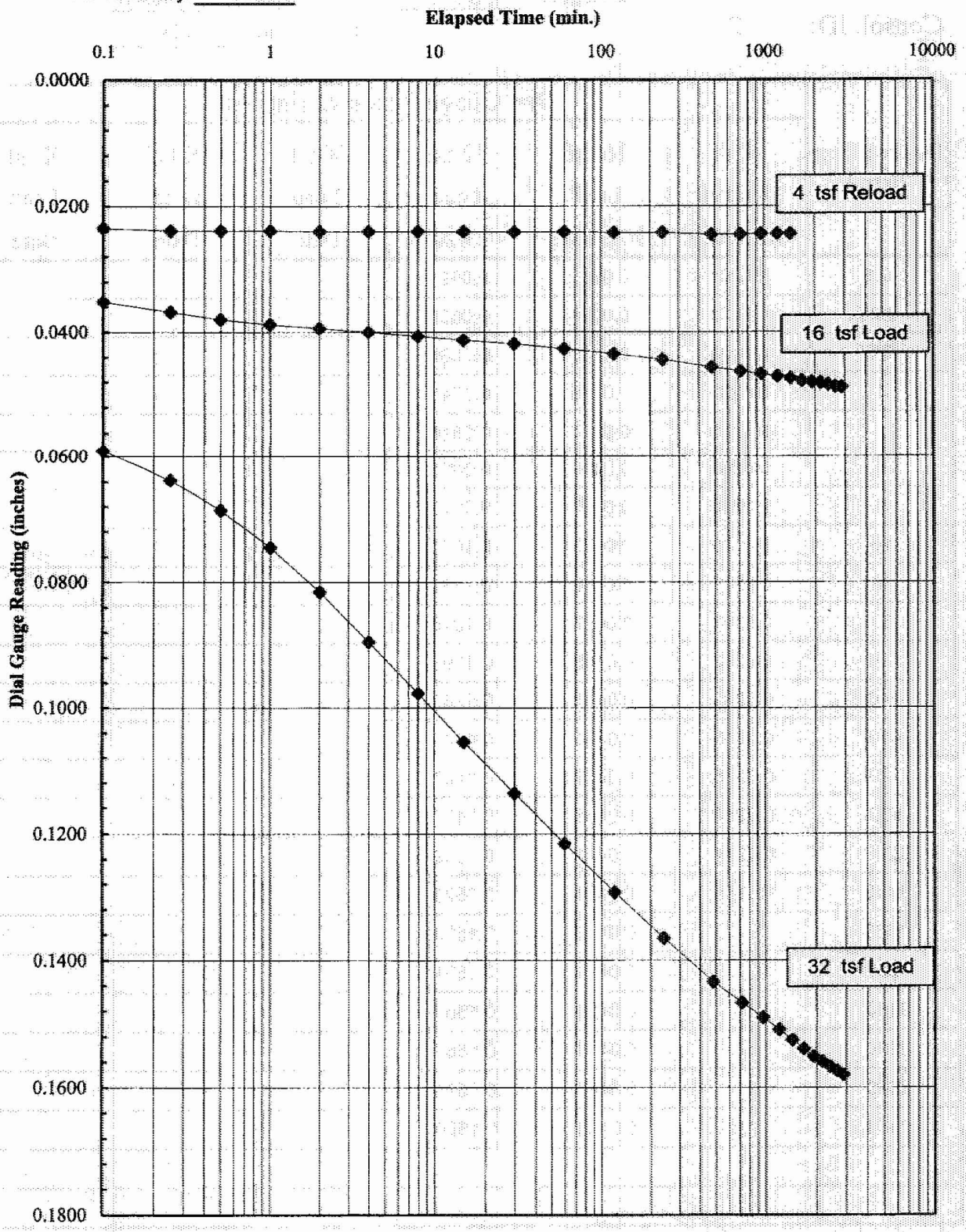
10/14/06

Project: Calvert Cliffs Nuclear Power Plant

Schnabel Contract: 06120048

Boring No.: B-301 Depth: 168.5-170.4 ft

Reviewed by: CJS

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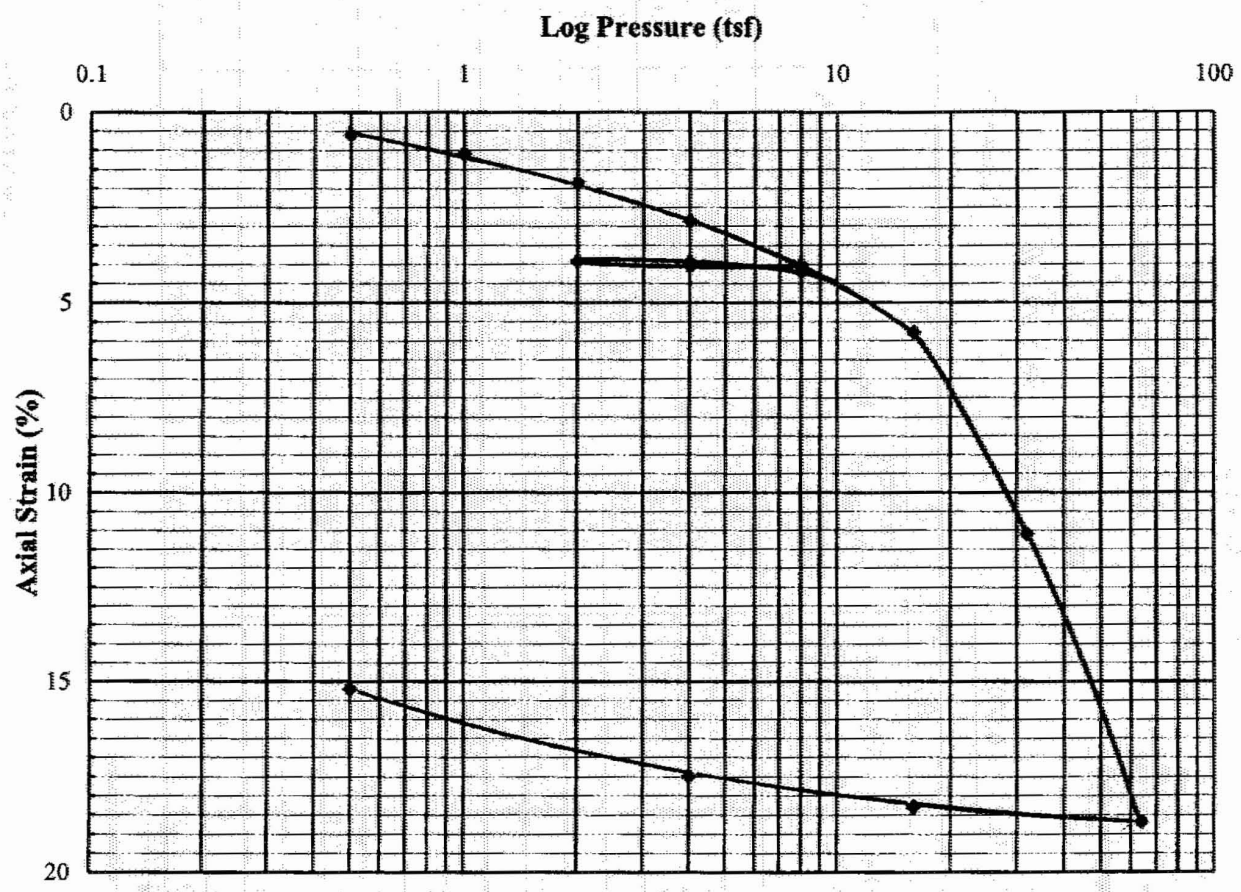


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| | | | | | |
|---|---|---|---|---|---|
| **Probable Preconsolidation Pressure (Pp), tsf:** | *20* | | | **Recompression Ratio (Cεr):** | *0.003* |
| **Type of Specimen:** | *Tube Sample* | | | **Compression Ratio (Cεc):** | *0.251* |
| **Description:** | *Fine CLAYEY SAND (SC), contains shell fragments - light gray* | | | | **Initial** / **Final** |
| **LL:** *79* | **PI:** *51* | **Gs:** *2.65* | **$P_c'$ (tsf):** *3.25* | **Water Content, %** | *37.7* / *28.9* |
| **% < No. 200:** | *47.3* | **Test Method:** | *ASTM D2435 Method A* | **Void Ratio** | *1.03* / *0.72* |
| **Test Condition:** | *Inundated @ 1 tsf* | | | **Saturation, %** | *97* / *100* |
| | | | | **Dry Unit Weight, pcf** | *81.6* / *96.2* |

**Remarks:** Coefficient of Consolidation, Cv, equals 2988 and 2703 ft2/yr at average pressures of 3 and 24 tsf (square root of time method).

**Average Water Content of Trimmings, %:** *37.2*

**Project:** Calvert Cliffs Nuclear Power Plant

| | | | |
|---|---|---|---|
| **Location:** | *Calvert County, MD* | | |
| **Boring:** | *B-304* | **Schnabel No.:** | *06120048* |
| **Depth:** | *98.5-99.5 ft* | **Elevation:** | *-30.5 to -31.5* |
| **Date:** | *10/17/2006* | **Reviewed by:** | *CJS* |

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**Consolidation Test Report**

# Consolidation Test Data Sheet

Consolidometer ID: 4

10/17/06

REVISED FORM FOR
NCR NO. 25237-NCR-028
2/12/2007

Schnabel Contract: *06120048*

Test Method: *ASTM D2435 Method A*

Project: *Calvert Cliffs Nuclear Power Plant*

Test Condition: *Inundated @ 1 tsf*

Initial Height of Specimen ($H_o$), in.: 0.7522

Boring No.: *B-304*

Height of Solids ($H_s$), in.: 0.3713

Depth: *98.5-99.5 ft*

Seating Press. (tsf): 0.05

Initial Dial Gauge Reading ($D_o$), in.: 0.0001

Reviewed by: CJS

| Pressure, P (tsf) | TimeReadings Required | Date Load Applied | Time Load Applied | Load Applied By | A<br>Final[1] Dial Reading, $D_{fi}$<br>x $10^{-4}$ in. | B<br>Apparatus Correction[2], $D_{ci}$<br>x $10^{-4}$ in. | C<br>Cumulative Change in Height[3], $\Delta H_i$<br>in. | D<br>Height of Voids[4], $H_{vi}$<br>in. | Vertical Strain[5], $\varepsilon_i$<br>(%) | Void Ratio[6], $e_i$ |
|---|---|---|---|---|---|---|---|---|---|---|
| 0.5 | | 9/16/2006 | 8:55 | CJS | 82 | 36 | 0.0045 | 0.3764 | 0.60 | 1.014 |
| 1 | | 9/18/2006 | 9:05 | CJS | 128 | 45 | 0.0082 | 0.3727 | 1.09 | 1.004 |
| 2 | | 9/19/2006 | 9:10 | CJS | 199 | 58 | 0.0140 | 0.3669 | 1.86 | 0.988 |
| 4 | | 9/20/2006 | 9:10 | CJS | 285 | 69 | 0.0215 | 0.3594 | 2.86 | 0.968 |
| 8 | | 9/21/2006 | 9:10 | CJS | 388 | 84 | 0.0303 | 0.3506 | 4.03 | 0.944 |
| 4 | | 9/22/2006 | 9:15 | CJS | 375 | 69 | 0.0305 | 0.3504 | 4.05 | 0.944 |
| 2 | | 9/25/2006 | 9:45 | DWC | 354 | 58 | 0.0295 | 0.3514 | 3.92 | 0.946 |
| 4 | | 9/26/2006 | 9:45 | DWC | 367 | 69 | 0.0297 | 0.3512 | 3.95 | 0.946 |
| 8 | | 9/27/2006 | 9:40 | DWC | 400 | 84 | 0.0315 | 0.3494 | 4.19 | 0.941 |
| 16 | | 9/28/2006 | 9:40 | DWC | 540 | 104 | 0.0435 | 0.3374 | 5.78 | 0.909 |
| 32 | | 9/29/2006 | 9:40 | DWC | 960 | 123 | 0.0836 | 0.2973 | 11.11 | 0.801 |
| 64 | | 10/2/2006 | 9:15 | DWC | 1549 | 143 | 0.1405 | 0.2404 | 18.68 | 0.647 |
| 16 | | 10/3/063 | 9:15 | DWC | 1481 | 104 | 0.1376 | 0.2433 | 18.29 | 0.655 |
| 4 | | 10/4/2006 | 9:15 | DWC | 1385 | 69 | 0.1315 | 0.2494 | 17.48 | 0.672 |
| 0.5 | | 10/5/2006 | 9:15 | DWC | 1180 | 36 | 0.1143 | 0.2666 | 15.20 | 0.718 |

Notes:
1. "Final" based on test method; 24 hrs for Method A, end of primary for Method B.
2. Correction value, for the current pressure, from the consolidometer's calibration curve.
3. $\Delta H = D_{fi} - D_o - D_{ci}$ = Col. A - $D_o$ - Col. B
4. $H_{vi} = (H_o - H_s) - \Delta H$
5. $\varepsilon_i = (\Delta H / H_o) \times 100$ = (Col. C / $H_o$) x 100
6. $e_i = H_{vi} / Hs$ = Col. D / Hs

Consol 8/2006 Rev. 1

Schnabel
Schnabel Engineering

# Load Time Readings

10/17/06

Project: Calvert Cliffs Nuclear Power Plant
Schnabel Contract: 06120048
Boring No.: B-304 Depth: 98.5-99.5 ft
Consol. ID: 4 Reviewed by: CJS

| Elapsed Time (min.) | Dial Guage Readings (inches) | | | | | |
|---|---|---|---|---|---|---|
| | 4 tsf Initial Load 9/20/2006 | 32 tsf Load 9/29/2006 | X tsf Load Date | X tsf Load Date | X tsf Load Date | X tsf Load Date |
| 0.1 | 0.0256 | 0.0687 | | | | |
| 0.25 | 0.0259 | 0.0711 | | | | |
| 0.5 | 0.0261 | 0.0728 | | | | |
| 1 | 0.0263 | 0.0744 | | | | |
| 2 | 0.0264 | 0.0759 | | | | |
| 4 | 0.0266 | 0.0776 | | | | |
| 8 | 0.0268 | 0.0793 | | | | |
| 15 | 0.0270 | 0.0811 | | | | |
| 30 | 0.0272 | 0.0832 | | | | |
| 60 | 0.0273 | 0.0853 | | | | |
| 120 | 0.0276 | 0.0877 | | | | |
| 240 | 0.0279 | 0.0902 | | | | |
| 480 | 0.0281 | 0.0926 | | | | |
| 720 | 0.0281 | 0.0939 | | | | |
| 960 | 0.0282 | 0.0948 | | | | |
| 1200 | 0.0283 | 0.0955 | | | | |
| 1440 | 0.0285 | 0.0960 | | | | |
| 1680 | | 0.0965 | | | | |
| 1920 | | 0.0969 | | | | |
| 2160 | | 0.0973 | | | | |
| 2400 | | 0.0976 | | | | |
| 2640 | | 0.0979 | | | | |
| 2880 | | 0.0983 | | | | |
| | | | | | | |
| | | | | | | |