

## Jonathan Rowley - Re: Questions & Comments - January 8, 2008 meeting with VY/Entergy

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**From:** <Noverflo@aol.com>  
**To:** <JGR@nrc.gov>  
**Date:** 01/11/2008 12:26 PM  
**Subject:** Re: Questions & Comments - January 8, 2008 meeting with VY/Entergy  
**CC:** <KTYLER@SDKSLAW.com>, <dlochbaum@ucsusa.org>, <shadis@prexar.com>

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Hi Jonathan, thanks for the presentation slides

At the end of the subject meeting I submitted to you two hand written questions which I asked the SIA speaker who did not answer my questions. I am resubmitting these questions in case my handwriting was difficult to read.

At the meeting I also wanted to add a comment regarding Union of Concerned Scientists Dave Lochbaum's question relating to oxygen excursions but I was prevented from doing so by Entergy's lawyer who instructed Entergy not to reply to my questions.

My two questions are paraphrased below:

1. What data do you have, to support your statement that the heat transfer coefficients you used to determine the Green functions were conservative (slides 44 and 51) and what do you believe is the degree of conservatism?
2. Does the geometry of the nozzle in slide 9 represent the design geometry of the vessel nozzle or does it represent the "as installed geometry." You have indicated that the validity of the assumption that shear stresses can be neglected is very sensitive to the geometry. It is therefore important to ascertain that the dimensions you used to calculate pipe reactions and peak stress were obtained from the dimensionally correct construction documents and that they also reflect the dimensionally correct geometry at the onset of the extended life period.

### Comment Regarding Dave Lochbaum's Question.

A proper NRC reply to Dave's question is important for the following reasons:

1. The Environmental correction factor,  $F_{en}$ , varies exponentially with the oxygen content.
2. The experimental fit curve for  $F_{en}$  is based on only one data point at the very low end of the oxygen concentrations.
3. The fatigue usage of each transient is multiplied by its respective  $F_{en}$ . Since the final usage factors are a summation of these products for all transients over the 60 year period one must be assured that the correct oxygen for each transient was employed. This oxygen must reflect the correct concentration **at the surface of the given component** in question at the time of the transient. It is not clear at all the oxygen concentrations that are measured either daily or bi-weekly, at some point in the plant represent the correct value that should be used by the  $F_{en}$  equation in its present form.

I would be grateful if the NRC address the above in the FSAR.

Sincerely,

Joe Hopenfeld

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**Created By:** [Noverflo@aol.com](mailto:Noverflo@aol.com)

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prexar.com

shadis CC

ucsusa.org

dlochbaum CC

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