ENCLOSURE 2

INSERVICE TESTING PROGRAM FOR PUMPS AND VALVES WATTS BAR NUCLEAR POWER PLANT UNIT 1

1.0 INTRODUCTION

Under the provisions of 10 CFR 50.55a, in-service testing of safety-related pumps and valves will be performed in accordance with Section XI of the ASME Boiler and Pressure Vessel (B&PV) Code and applicable Addenda. As specified in 10 CFR 50.55a(b), the effective edition of Section XI with regard

to this program is the 1983 edition through the summer 1983 addenda. This program identifies the pump and valve inservice testing that will be performed at the Watts Bar Nuclear Power Plant (WBN) to comply with the requirements of 10 CFR 50.55a for operation of unit 1.

2.0 PUMP INSERVICE TESTING PROGRAM

The pump test program shall be conducted in accordance with Subsection # IWP of Section XI of the 1983 Edition of the ASME Boiler and Pressure

* Vessel Code through summer 1983 addenda, except for relief requested under the provisions of 10CFR50.55a(g) (5) (iii). Appendix A details the in-service testing program for all safety related pumps at WBN. Each parameter to be measured, as well as reference to specific relief requests, are also listed. Relief requests are listed numerically in Appendix C.

2.1 Pump Bearing Temperature

Subsection IWP-3300 requires pump bearing temperatures be measured at least once every year. Industry experience demonstrates that bearing temperatures rise only minutes prior to failure. Any bearing failure predicted by a yearly recording of bearing temperature would be a random event and, thus, yearly measurement of bearing temperatures does not increase the level of confidence in component reliability. The expense of adding the additional testing is, therefore, not justified.

Further, IWP-3500(b) specifies that pumps be run until bearing temperatures stablize as determined by three measurements at 10-minute intervals. Clearly the pump would have to be run in excess of one-half hour to obtain these readings. The pump degradation caused by this requirement does not justify the very limited assurance it might provide.

Quarterly measurements of vibration velocity will provide meaningful indication of bearing reliability due to the increased sensitivity of velocity to higher frequency bearing vibration. Additionally, vibration velocity will begin to increase much earlier in bearing failure than temperature will. Data trending will also be more useful utilizing these vibration measurements.

Vibration data taken on a quarterly basis will be trended and significant increases in these data may necessitate further vibration measurements, including vibration analysis, to define the source of the increase. This request for relief should apply for all bearings presently required to be temperature tested.

3.0 VALVE IN-SERVICE TESTING PROGRAM

The valve test program shall be conducted in accordance with Subsection

** IWV of Section XI of the 1983 edition of the ASME B&PV Code through the

** summer 1983 addenda, except for relief requested under the provisions of

** 10 CFR 50a(g) (5) (iii). All valves in safety-related systems were reviewed

** and categorized. Valves which were categorized as active in any category

** and passive valves categorized in Category A are listed in Appendix B.

Relief requests are identified by number in the column labeled RELIEF and listed numerically in Appendix C. Justifications for testing in cold shutdown in lieu of during operation are listed in Appendix D and identified by number in the column labeled ALTER.

3.1 Category A Valves

Valves for which seat leakage is important may generally be classified as pressure isolation valves (PSIV), containment isolation valves (CIV), or both pressure and containment isolation valves.

3.1.1 <u>CIV</u>

Containment isolation valves falling within the scope of ASME Section XI are tested in accordance with the Section XI requirements of IWV-3410, Category A with the exception of the seat leakage tests (IWV-3420). The seat leakage testing of these valves meets the intent of Section XI, but the actual test procedures shall be in accordance with the 10 CFR 50, Appendix J, Type C, CIV test program. For valves performing a containment isolation function, individual valve leak rates are not in themselves significant. The only pertinent leak rate criterion for CIVs is that the total leak rate for all penetrations and valves be less than that allowed by Appendix J. In recognition of the fact that a single valve should not be allowed to approach

the Appendix J limit, working guidelines have been established to ensure that a single valve does not become the predominate source of leakage. The Watts Bar plant was designed to perform the Appendix J, Type C test, not the individual Category A leak test (i.e., some penetration test connections test more than one valve at a time). Accordingly, all CIV seat leak testing shall be performed in accordance with the requirements of 10 CFR 50, Appendix J, Type C, in lieu of the Category A requirements of Section XI.

3.1.2 PSIV

Pressure isolation valves (PSIV), falling within the scope of IWV-3421, shall be tested in accordance with Subsection IWV of Section XI of the 1983 edition of the ASME B&PV Code through the summer 1983 addenda except for the relief requested under the provisions of 10 CFR 50a(g)(iii). In addition to the requirements of Subsection IWV, these valves will also be tested in accordance with surveillance requirement 4.4.6.2.2 of the Watts Bar Technical Specifications regarding permissible leakage from the reactor coolant system.

3.2 Thermal Relief Valves

Many safety-related systems, particularly those with heat exchangers, have been provided with relief valves. These relief valves are thermal relief valves (TRV) of small capacity intended to relieve pressure due to thermal expansion of fluid in a "bottled-up" condition. Experience has shown that failure of these valves will not result in failure of a system to fulfill its safety-related function. Thus, the thermal relief valve is not safety-related and such valves have not been included in the program.

3.3 Thermal Relief Check Valves

Several penetrations have been fitted with small spring-loaded check valves designed to relieve pressure due to thermal expansion of fluid in the penetration. These valves will be leak tested in the closed position at each refueling: however, these valves do not have a safety-related function to open. The reasoning is similar to that for the thermal relief valves in that the only occasion that would require the opening function of these valves is when both CIVs are absolutely tight with zero leakage. On that occasion, the thermally induced pressure increase will be stabilized, since only a minute amount of leakage past any barrier would stabilize the penetration pressure. Watts Bar views these valves as safety-related only in the closed position to provide containment isolation function.

3.4 Corrective Action

Relief is requested from the corrective action requirements of Paragraph IWV-3417 of Section XI. The requirement for corrective action of components in safety systems is adequately covered in the Limiting Conditions for Operation (LCO) contained in the present Watts Bar Technical Specifications.

IWV-3417 requires that if a Category A or B valve fails to test satisfactorily (valve exercising) corrective action be taken immediately; if the condition is not corrected within 24 hours, the valve should be declared inoperable. If repairs are necessary due to CSD testing, the repairs shall be made prior to startup. A retest showing acceptable operation shall be run following any repairs before returning the valves to service.

Watts Bar Technical Specifications regarding corrective actions are more restrictive than those identified in IWV-3417. By the technical specification definition of OPERABLE, no grace period is allowed before a device that is not capable of performing its specified function is declared inoperable. LCO 3.0.4 and specific LCOs adequately address changes in OPERATIONAL MODES with inoperable equipment to ensure against entry into a condition without required safety-related equipment. The definition of OPERABLE again requires an acceptable retest to prove the component capable of performing its intended function prior to declaring the component (i.e., valve) operable.

IWV-3523 requires the same corrective actions for Category C CVs as described above for Category A and B valves. The same discussion as presented above for IWV-3417 applies for IWV-3523.

3.5 Systems Out of Service

Relief is requested from the requirements for testing valves in systems which are out of service before returning those systems to operable status in accordance with IWV-3416 of Section XI. These testing requirements are adequately covered in the Watts Bar Technical Specifications and Plant Procedures.

IWV-3416 states for a valve in a system declared inoperable or not required to be operable, the exercising test schedule need not be followed. Within 30 days prior to return of the system to operable status, the valves shall be exercised and the schedule resumed in accordance with requirements of this Article.

If a system is declared inoperable for the reason of a failure of a valve, then the valve will be exercised and tested satisfactorily prior to returning the system to operable status. This is provided for by the technical specifications definition of OPERABLE. If, however, a system is declared inoperable or is not required to be operable for some reason other than valve problems, e.g., a pump is tagged for maintenance, then the system valves do not have to be exercised prior to returning the system to operable status provided the valve exercising schedule is in the required frequency. In this case, the applicable pump test would be run to determine operability of the system. For an extended outage or period for which the system is not operable or required to be operable, the respective valve exercising must only be in frequency prior to declaring the system operable. Relief is therefore requested only from the 30-day requirement, i.e., valve exercising must only be in frequency (e.g., exercised within 90 days) prior to returning the system operable.

3.6 Emergency Diesel Systems

The in-service operability testing of pumps and valves associated with the emergency diesels, excluding the diesel oil transfer system and diesel air start system, are excluded from the enclosed test programs. These components are an integral part of the emergency diesel system and are functionally tested monthly. Thus, the functional operability testing of the pumps and valves is performed at a frequency greater than that required by Section XI for either pumps or valves. Additionally, the failure of a pump or valve to perform its intended function will be identified by the failure of the associated emergency diesel to meet its functional requirements. The diesel fuel oil transfer pumps and air start valves are included in the enclosed test program.

The Watts Bar emergency power system has a spare diesel generator set. Test frequency of the spare diesel generator need not be maintained when that diesel generator is not required to meet standby emergency power requirements. Prior to declaring the spare diesel operable and utilizing it to meet standby emergency power requirements, Watts Bar will either verify that all required Section XI tests have been performed within the previous three months or perform such tests prior to making the spare diesel operable.

3.7 Fail-Safe Actuators

All those valves which have a fail-safe actuator are exercised normally using that actuator. Thus, the fail-safe actuator is regularly tested when the valve is tested.

3.8 Valve Timing and Remote Indication

During each full-stroke test of a power-operated valve, the full-stroke time shall be measured in accordance with Section XI Article IWV-3413 except for those valves which stroke in less than two seconds. For these fast-acting valves (i.e., stroke time less than two seconds) observation that valve cycling was completed in not more than two seconds will be required. In addition, each valve with a remote indicator shall be stroke

* timed using that indicator. Proper indication of valve position will be

verified not less often than once every two years in accordance with Section XI,

*Article IWV-3300, except where relief has been granted.

3.9 Passive Valve

These valves, which have no Section XI testing requirements, are valves in safety-related systems which are not required to change position in order to accomplish their required safety function. Watts Bar has included as B-Passive all manually operated valves which are required by procedure to be maintained in their safety-related position. Any valves which are locked-open or locked-closed in their safety-related position are also considered Category B-Passive. Due to the lack of testing requirements, these valves have been excluded from Appendix B.

3.10 Cold Shutdown Testing

♣ Unless otherwise stated in Appendix C or D, reference to testing at cold
♣ shutdown in lieu of during operation implies that Watts Bar will commence
testing as soon as the cold shutdown condition is achieved but not later

★ than 48 hours after cold shutdown and will continue in a normal manner
until all tests are complete or the plant is ready to return to power.

Any testing not completed at one cold shutdown will be performed during

★ subsequent cold shutdowns starting from the last test performed at the

★ previous cold shutdown. Therefore, a unit shall not be required to remain
in cold shutdown to complete cold shutdown testing. For planned cold
shutdowns, where Watts Bar will complete all the tests identified in the
IST program for the cold shutdown mode, exception to the above 48-hour start
time may be taken (refueling, etc.). In the case of frequent cold shutdowns,

★ valve testing will not be performed more often than once every three months.

★ valve testing will not be performed more often than once every three months.

■ valve testing will not be performed more often than once every three months.

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4.0 ABBREVIATIONS AND SYSTEM IDENTIFICATION

4.1 Abbreviations Used In Summary Listing of Inservice Test Program

ACT - Valve actuator type

ANG - Angle body valve
BUT - Butterfly valve

BT - Bench test of safety or relief valve to determine setpoint

CATGRY - ASME Section XI category applicable to the valve listed

CK - Self-actuating checkvalve

CV - Full stroke exercising of a checkvalve performed quarterly

except for valves where relief has been requested.

COORD - Drawing coordinates at which the valve is shown.

The coordinates listed are for the unit 1 valves for drawings which show both units.

CYL - Air, hydraulic, or high pressure fluid cylinder actuator

DIA - Diaphragm body valve (when listed in TYPE column)DIA - Diaphragm actuator (when listed in ACT column)

DP - Differential pressure developed by a pump during stable operation.

DWG No.- TVA drawing number. The number listed is the last segment of the complete drawing number. To obtain the complete number, the type and size identifier 47W should be added. For example, the complete number of a drawing listed as. 801.1 is 47W801.1

GA - Gate valve
GL - Globe valve

LT - Seat leakage measurement test

MOT - Motor operated actuator

N. POS - Normal position of valve. The position listed corresponds to the position the valve is usually in. Some valves which are usually closed, and must close to fulfill their function, are listed as active valves because they may be opened as part of normal plant operation, thus, placing an active requirement to close on them.

OLP - Lubricating oil level or pressure

PLUG - Plug valve

PNU - Pneumatically operated valve

PS - Part stroke

Volumetric flow rate (when listed as a column headings in Appendix A)

Appendix A)

O - Quarterly (when listed in the parameter columns of Appendix A)

QT - Full stroke exercising of a power-operated valve performed quarterly except for valves where relief has been requested

REL - Safety or relief valve

RELIEF - Identification of the specific relief request applicable to the valve listed

RD - Rupture disk

SIZE - Nominal valve diameter in inches

SLF - Self actuated valve

SOL - Solenoid valve

SPF - Final suction pressure during stable pump operation

SPI - Initial suction pressure measured prior to pump start

SYS - TVA system identification number. See 4.2 below for listing of system numbers and names.

TB - Bearing temperatures

TESTS - Type of testing required by Section XI for valves of the category listed

TYPE - Valve body type
V - Vibration level

4.2 SYSTEM NUMBER IDENTIFICATION

- 01 Main Steam
- 02 Condensate System
- 03 Main and Auxiliary Feedwater
- 18 Fuel Oil System
- 26 High Pressure Fire Protection
- 30 Ventilation
- 31 Air-Conditioning
- 32 Control Air
- 43 Sampling
- 52 System Testing Facility
- 61 Ice Condenser
- 62 Chemical and Volume Control
- 63 Safety Injection
- 67 Essential Raw Cooling Water
- 68 Reactor Coolant
- 70 Component Cooling
- 72 Containment Spray
- 74 Residual Heat Removal
- 77 Waste Disposal
- 78 Spent Fuel Cooling
- 81 Primary Water
- 82 Diesel Air Start
- 87 Upper Heat Injection
- 90 Radiation Monitoring

APPENDIX-A PUMP INSERVICE TESTING PROGRAM SUMMARY

LIST P PUMPS		.SPC LPTR .NUMBER.					.CP.	.VIE.	.OLP.	.Te	REMARK	
0671	ESSENTIAL RAW CCCLING	A - A -	NR	RR.04	Q .	RR.05	RR.05	RR.02	N R	RR.01	OIL LEVEL OR PRESSURE IS	
	WATER										BEARINGS ARE NOT CUTSIDE	
											THE FLOW PATH. BEARINGS	
											ARE WATER LUBED SLEEVE	
						· · · · · · · · · · · · · · · · · · ·					TYPE LOCATED IN THE MAIN FLOW PATH. SPEED NOT	
											PEQUIRED FOR SYNCHRONGUS	
		·									OR INDUCTION MOTOR	
						<u>-</u>	· · · · · ·				DRIVEN PUMPS.	
1472 _	ESSENTTAL	c - A	N: P	PR-04	o.	RP_05	PP-05	88.C2	N R	RR.01	OIL LEVEL OR PRESSURE	
131.2	RAW COCLING				· · · · · · · · · · · · · · · · · · ·			RR.C3			NOT REQUIRED BECAUSE	
	WATER										BEARINGS ARE NOT CUTSIDE	
											THE FLOW PATH. BEARINGS	
											ARE WATER LUBED SLEEVE TYPE LOCATED IN THE MAIN	
											FLOW PATH. SPEED NOT	
											REGUIRED FOR SYNCHRONOUS	
											OR INDUCTION MOTOP	
	•										DRIVEN PUMPS.	
0673	ESSENTIAL	C = A	NR	RR.04	- C	RP.05	RR.05	RR.G2	NR	RR.01	OIL LEVEL OR PRESSURE IS	
	RAW COOLING							RR C3			NOT REQUIRED BECAUSE	
	WATER										BEARINGS ARE NOT CUTSIDE	
											THE FLOW FATH. BEARINGS ARE WATER LUBED SLEEVE	
									1		TYPE LOCATED IN THE MAIN	
											FLOW PATH. SPEED NOT	
											REQUIRED FOR SYNCHRONOUS	
											OR INDUCTION MOTOR DRIVEN PUMPS.	
0674	ESSENTIAL	D-A	NR	RR.04	Q	RP.05	RF.05		NR	RR.01	OIL LEVEL OR PRESSURE IS	
	RAW COCLING							RR.03			NOT REQUIRED BECAUSE BEARINGS ARE NOT OUTSIDE	_
	WATER										THE FLOW FATH. BEARINGS	
											ARE WATER LUBED SLEEVE	
											TYPE LOCATED INSIDE THE	
											MAIN FLOW PATH. SPEED NOT REQUIRED FOR	
											SYNCHRONOUS OR INDUCTION	
			<u> </u>								MOTOR DRIVEN PUMPS.	
0475	F 2 F F 3 T T 4 I	F-2	N.O.	20.07		20 OF	RR.05	20 03	NI D	ED 04	OIL LEVEL OR PRESSURE IS	
0675	ESSENTIAL RAW CCOLING	E-5	NR	RR.04	u	K = U 3	K R • U J	RR - 02		~ N • U I	NOT REQUIRED BECAUSE	
	WATER .										BEARINGS ARE NOT CUTSIDE	
											THE FLOW PATH. BEARINGS	
							•				ARE WATER LUBED SLEEVE	
							<u>-</u>			······································	TYPE LOCATED INSIDE THE MAIN FLOW PATH. SPEED	
								·				

IST P		.SPC LPTR .NUMBER.					DP	.vie.	.OLP.	.TB	REMARK
UNFS		31101 0211									
											NOT REQUIRED FOR SYNCHRONOUS OR INDUCTION
											MOTOR DRIVEN PUMPS.
676	ESSENTIAL	f-8	NR	RR.04	Q	RR.05	RR.05	RR.C2	NR	RR.01	
	RAW CCCLING							PP_D3			NOT REQUIRED BECAUSE BEARINGS ARE NOT CUTSIDE
	WATER										THE FLOW PATH. BEARINGS
- ,											ARE WATER LUBED SLEEVE
											TYPE LOCATED INSIDE THE
	•										MAIN FLOW PATH. SPEED NCT REQUIRED FOR
											SYNCHRONOUS OR INDUCTION
											MOTOR DRIVEN PUMPS.
1477	FSSENTIAL		N 2	8P.04	a	RR . 05	22.05	RR.C2	NR	RR - 01	OIL LEVEL OR PRESSURE
	RAW COCLING							RR.03			NOT REQUIRED BECAUSE
	WATER										BEARINGS ARE NOT CUISIDE
											THE FLOW FATH. BEARINGS ARE WATER LUBED SLEEVE
											TYPE LOCATED INSIDE THE
				<u> </u>		· · · · · · · · · · · · · · · · · · ·					MAIN FLOW PATH. SPEED
											NOT REQUIRED FOR SYNCHRONOUS OR INDUCTION
									-		MOTOR DRIVEN PUMPS.
			N R	RR.04		P.P. 0.5	pp 05	RR.02	N D	RR.01	OIL LEVEL OR PRESSURE
578	ESSENTIAL RAW COOLING	H_=3	N K	KK - 04	· ·	4K.0J	K 4 . U J	RR 03			NOT REQUIRED BECAUSE
	WATER										BEARINGS ARE NOT OUTSIDE
<u> </u>		·							······································		THE FLOW PATH. BEARINGS ARE WATER LUBED SLEEVE
											TYPE LOCATED INSIDE THE
						 					MAIN FLOW PATH. SPEED
								····			NOT REQUIRED FOR SYNCHRONOUS OR INDUCTION
											MOTOR DRIVEN PUMPS.
	COMPONENT	c-s	NR	20.07	G	80.05	BD 05	RR.C2	۵.	RP - 01	SPEED NOT REQUIRED FOR
701	COCLING	<u> </u>	N.3	<u> </u>		77.02	KKIOJ	KKECL			SYNCHRONOUS OR INDUCTION
				 							MCTOR DRIVEN PUMPS.
1931	AUXILIARY	1 4 - 4	NR	Q	Q	C	Q	RR.02	G	RR.01	SPEED NCT REQUIRED FOR
	FEEDWATER										SYNCHRONOUS OR INDUCTION
	PUMP				···						MOTOR DRIVEN PUMPS.
1332	AUXILIARY	15-5	NR	Q	<u> </u>	0	Q	RR.C2	Q	RR.01	SPEED NOT REQUIRED FOR
	FEEDWATER										SYNCHRONOUS OR INDUCTION
	PUYP					-		······································			MOTOR DRIVEN PUMPS.
1033	AUXILIARY	1A-S	<u> </u>	9	G	<u> </u>	Q	RR.CZ	Q	RR.01	
	FEEDWATER						÷				
							<u> </u>		-,		

<u>IST P</u> UMPS		.NUMBER.				AGE	DP.	VIE.	.OLP.	.19	REMARK
	PUMP									·	
181	FUEL CIL	1.61	NR	RR.09	RR.09	RR.10	RR.10	RR.02	RR.11	RR.01	SPEED NOT REQUIRED FOR
···	TRANSFER PUMP						······································				SYNCHRONOUS OR INDUCTION MOTOR DRIVEN PUMPS.
82	FUEL CIL	1 A Z	NR	ER.09	RR.C9	RR.10	RR.10	RR.C2	RR.11	RR.01	SPEED NOT REQUIRED FOR
	TRANSFER PUMP	······································			 						SYNCHRONOUS OR INDUCTION MOTOR DRIVEN PUMPS.
1 8 3	FUEL CIL	181	N R	RR.09	PR.09	RR.10	RR.10	RR.G2	RP.11	RP.01	SPEED NOT REQUIRED FOR
	TRANSFER PUMP										SYNCHRONOUS OR INDUCTION MOTOR DRIVEN PUMPS.
154	FUEL OIL	1 is 2	N R	RR.09	RR.C9	RR.10	RR.10	RR.02	RR.11	RR.01	SPEED NOT REQUIRED FOR
	TRANSFER PUMP										SYNCHRONOUS OR INDUCTION MOTOR DRIVEN PUMPS.
621	CENTRIFUSAL	1 A - A	NR		Q.	G.	Q	RR.02	Q	RR.01	SPEED NOT REQUIRED FOR
	CHARGING							· · · · · · · · · · · · · · · · · · ·			SYNCHRONOUS OR INDUCTION MOTOR DRIVEN PUMPS.
622	CENTRIFUGAL	15-E	N.R.	Q	G	Q	Q	RR.C2	Q	RR.01	SPEED NOT REQUIRED FOR
	CHARGING						···				SYNCHRONOUS OR INDUCTION MOTOR DRIVEN PUMPS.
 5 2 3	BORIC ACID	1 A-A	<u> </u>			80.48	Q	RP.02	Q	PR.01	
	TRANSFER PUMP										
624	EDRIC ACID	19-8	Q	Q	Q	RR.09	<u> </u>	RR.G2	Q	RP.01	
	TRANSFEP PUMP						·				
631	SAFETY	1 A - A	NR	Q	Q	a	Q	RR.C2	0	RR.01	SPEED NOT REQUIRED FOR
·····	INJECTION ·									······································	SYNCHRONOUS OR INDUCTION MOTOR DRIVEN PUMPS.
532	SAFETY	18-8	NR	Q	<u> </u>	G	Q	RR.C2	0	RR.01	SPEED NOT REQUIRED FOR
	INJECTION					······································		_	 		SYNCHRONOUS OR INDUCTION MOTOR DRIVEN PUMPS.
701	COMPONENT	1 A - A	NR	RR.06	Q	RR.05	RR.05	RR.C2	Q	RR.01	SPEED NOT REQUIRED FOR
	COCLING										SYNCHRONOUS OR INDUCTION MOTOR DRIVEN PUMPS.
702	COMPONENT	18-6	NR	RR.06		RR. 05	RR.05	RR.02	Q	RR.01	SPEED NOT REQUIRED FOR
	EOCLING										SYNCHRONOUS OR INDUCTION MOTOR DRIVEN PUMPS.
721	TAINMENT	1 A - A	NR	Q	Q	G	Q	RR.02	Q	RR - 01	SPEED NOT REQUIRED FOR
	COTTAINFERT	10.0	(11)			<u> </u>					

UMPS	UMPS T DBL	.NUMBER.	SPEED	.SPI.	.SPF.	Q	. DP	.vie.	.OLP.	.TB	REMARK
·	SPRAY										SYNCHRONOUS OR INDUCTION MOTOR DRIVEN PUMPS.
722	CONTAINMENT SPRAY	18-8	NR			C		RR.C2		_RR.01	SPEED NOT REQUIRED FOR SYNCHRONOUS OR INDUCTION MOTOR DRIVEN PUMPS.
741	RESIDUAL HEAT REMOVAL	1 A=A						R9.02_	_ G	_RR.01_	SPEED NOT REQUIRED FOR SYNCHRONOUS OR INDUCTION MOTOR DRIVEN PUMPS.
742	RESIDUAL HEAT REMOVAL	1e=e	NR NR			c		RR.02		_RR.01_	SPEED NOT REQUIRED FOR SYNCHRONOUS OR INDUCTION MOTOR DRIVEN PUMPS.
2181	FUEL CIL TRANSFER PUMP	2.41	NR	RR.09	<u> </u>	RP.1C_	_ = 2 . 10	98.02		RR.01	SPEED NOT REQUIRED FOR SYNCHRONOUS OR INDUCTION MOTOR DRIVEN PUMPS.
1.62	FUEL CIL TRANSFER PUMP	SAS	NR	_RR.09	RR.C9_	RR.10_	_ RR_10	RE.02	P.P11	_RR-01	SPEED NOT REQUIRED FOR SYNCHRONOUS OR INDUCTION MCIOR DRIVEN PUMPS.
21 8 3	FUEL OIL TRANSFER PUMP	2 P 1	ns —	RR.09	_ FR. C2	32.1C	RP.10	RR.02_	_R.R11_	P.R01	SPEED NOT REQUIPED FOR SYNCHRONOUS OR INDUCTION MOTOR DRIVEN PUMPS.
2184	FUEL OIL TRANSFER PUMP	252	NR		PP.C9	RR.1C		RR.C2	_ 28.11_	FR.01	SPEED NCT REQUIRED FOR SYNCHRONOLS OR INDUCTION MOTOR DRIVEN PUMPS.
32 REC	CORDS LISTED.										
			,								
									·		

APPENDIX-B VALVE INSERVICE TESTING PROGRAM SUMMARY

IST VALVES	SY 5	CLASS	DWG.NC	COORD	86 PAGE CATGRY	SIZE	TYPE	- A C T	N.POS	TESTS	ALTER-	RELIEF		
FCV01.004T		2	801.1	C - 4	B.ACT	- 32	G A	-CYL-	-0	- QT	- CS - O1 - PS	· · · · · · · · · · · · · · · · · · ·		
FCV01.011T	01	2	301.1	E • 4	B.ACT	32	G A	CYL	0	QT	CS.01			
FCV01.022T		-2-	301.1	G . 4	B.ACT	- 32	G A	CYL	0	9 T	- CS - O1 PS			
FCV01.029T	01	2	801.1	A - 4	B.ACT	32	G A	CYL	0	GT	CS.01			
FCV01.147A	01		801.1	C.4	E.ACT	2 -	GL	DIA	- c -	-01				
FCV01-1485	- c1 -	5		E . 4	B.ACT		GL-	DIA	- c	-QT				
FCV01.149A	01	Ž	301.1	G . 4	5.ACT		GL .	DIA	c	GT			· · · · · · · · · · · · · · · · · · ·	
FCV01.1508	- 61	2	801.1	A . 4	B.ACT	2	GL	DIA	-с	- Q T		···		
PCV01.0057	01		801.1	c.3	E.ACT	- 5	-G L	DIA	c	- GT-	cs.02			
PCV01.012T	C1	-2	331.1	E . 3	B.ACT	- 6 -	GL	DIA	-c	QT	- cs.02		<u> </u>	
PCV01.023T	01	2	391.1	F.3	B.ACT	-6	GL	DIA	- c	QT	cs.02			
PCV01.030T	- 01		801.1	A - 3	B.ACT	-6	GL	DIA	с		- cs02			
3 F V 01 - 51 2	- 81	- 2	801.1	F.2	C.ACT	-6	REL	-SLf-	- ε	- 21			·	
SFV01.513	C1	-2	891.1	-F - 2	C.ACT	6	REL	SLF	-c	-6 T				
SFV01.514	01	2	881.1	F.3	C - A C T	6	FEL	SLF		- 8 T				
SFV01.515	C1	2	801.1	F.3	С.АСТ	6	REL	SLF		вт				
SFV01.516	C1	2	801.1	F = 3	C.ACT	ó	REL	SLF	е	sT				
SFV01.517	-01	-2	301.1	D . 2	C.ACT	-6	REL	SLF	- c	-BT			· · · · · · · · · · · · · · · · · · ·	
SFV01.518	- 61 -	2	801.1	D.2	C.ACT	6	REL	SLF	c	- 5 T		· · · · · · · · · · · · · · · · · · ·		
SFV01.519	01	2	8 C1 - 1	0.3	C.ACT	6	REL	SLF	е	87				
SFV01.520		2	201.1	D.3	C.ACT	- 6	REL	SLF-	-с	- 51	· · · · · · · · · · · · · · · · · · ·			
SFV31.521	- 31	-2	€91 .1	0.3	C.ACT	-5	REL	SLF		21				<u></u>
SFV01.522	-01	-2	201.1		- C-ACT	6	REL	SLF		- 6 7				7 A.
SFV01.523	- 01		801.1	t.3	CACT	6	REL	SLF		- 3 T			9,7,7	

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VALVES	37S	CLASS		04-11-	-86 PAGE CATGRY	\$17E	TYPE	ACT	N.POS	TESTS	ALTER	RELIEF			
1 S F V O 1 • 52 4	01	2	801.1	C • 3	C.ACT	6	REL	SLF	С	ВТ					
1 S F V O 1 • 5 2 5	01	2	301.1	C.3	C.ACT	6	REL	SLF	С	BT					
1SFV01.526	C1	2	801.1	c.3	C.ACT	6	REL	SLF	С	вт					
1SFV01.527	01	2	801.1	A 🕽 3	C.ACT	6	REL	SLF	С	вт					
1\$FV01.528	01	2	801.1	A.3	C.ACT	6 .	REL	SLF	С	эт					
1SFV01.529	01	2	801.1	A . 3	C.ACT	6	REL	SLF	С	вт					
1SFV01.530	01	2	801.1	A.3	C.ACT	6	REL	SLF	С	вт					
18FV01.531	01	2	301.1	A . 3	C.ACT	6	REL	SLF	С	вт					
1FCV01.0078	C1	2	801.2	c.3	B.ACT	2	G A	SOL	0	91 -		RR.21			
1FCV01.014A	C1	2	801.2	E.3	B.ACT	2	G A	SOL	0	QT		RR.21			
1 F C V O 1 . 0 2 5 3	C1	2	801.2	G.3	B.ACT	2	G A	SOL	0	QT		RR.21			
1 F C V O 1 . O 3 2 A	01	2	801.2	A.3	B.ACT	2	G A	SOL	0	QТ		RR.21			
1 F C V O 1 . 181 A	C1	2	801.2	C • 2	B.ACT	2	G A	SOL	0	QT		RR.21			
1FCV01.1828	C1	2	801.2	E.2	B.ACT	2	G A	SOL	0	QT		RR.21			
1FCV01.183A	01	2	801.2	G.2	B.ACT	2	G A	SOL	0	QT		RR.21			
1 F C V O 1 . 184 B	01	2	801.2	4.2	B.ACT	2	G A	SOL	0	QT		RR.21			
1 FCV01.015A	01	2	803.2	в.9	E.ACT	4	' G A	том	0	QT.					
1 F C V O 1 . O 1 6 A	C1	2	803.2	A.9	B.ACT	4	G A	MOT	0	QT					
1 FCV01.017A	01	3	803.2	8.8	B.ACT	4	G A	MOT	0	QT	cs.03				
1 F C V O 1 • O 1 8 B	C1	2	803.2	B.8	E.ACT	4	G A	MOT	0	QT	cs.03				
1 CK VO 2 . 667	02	3	804.1	G.3	C.ACT	2.5	cĸ	SLF	С	cv					
1CKV03.508	03	2	803.1	E • 2	C.ACT	16	CK	SLF	0	CV	cs.04	RF.28			
1CKV03.509	G 3	2	803.1	D.2	C.ACT	16	СК	SLF	0	c v	cs.04	RR.28			
1CKV03.51C	C 3	2	803.1	c.2	C.ACT	16	cĸ	SLF	0	cv	cs.04	RR.28			
1 CKV03.511	03	2	803.1	B.2	C.ACT	16	CK	SLF	0	CV	cs.04	RR-28			

LIST VALVES &			TR 07:27:18	04-11-8	36 PAGE Catgry	SIZE	TYPE	ACT	N.POS	- TESTS -	ALTER	RELIEF		
1003.638	<u>C3</u>	2	803.1	A . 3	CLACT	6 .	ск	SLF	0	CV	cs.05			
1CKV03.652	03	2	303.1	C . 3	C.ACT	6	ск	SLF	0	e v	cs.05			
108703.659	C 3	2	803.1	0.2	C.ACT	ó	ck	SLF	0	<u>cv</u>	cs.05			
1CKV03.678	C3	2	503.1	F • 2	CACT	6	cĸ	SLF	0	CV	cs.05	·		
1FCV03.033A	C3	2	803.1	C . 3	B.ACT	16	G A	MOT	0	- от	cs.04			
1FCV03.0478	<u> </u>	2	803.1	E.3	S.ACT	- 16	G A	тсм		QT	cs.04			
1FCV03.087A	03	2	803.1	G.3	E.ACT	16	G A	мот	0	GT	CS.04			
1FCV03.1005	C 3	2	803.1	3.3	P.ACT	16 · · ·	G A	мот	0	- Q T	cs.04			
1FCV03.185	03	2	803.1	C . 2	B.ACT		G A	DIA	c	GT	CS • O ć			
1FCVG3.186	03	2	803.1	£.2	E.ACT	2	G A	DIA	C	QT	<u>cs.05</u>		•	
1FCV03.187	03	2	803.1	e . 2	B.ACT	2	G A	DIA	- с	er -	CS.06			
1FCV03.188	C3	2	803:1	F • 2	9.ACT	2	- G A	DIA	c	- 0 T 	€8.86	· · · · · · · · · · · · · · · · · · ·		
1FCV03.236	23	2	803.1	C.3	B.ACT	6	G A	DIA	0	37	cs.07			
1FCV03.239	 	2	803.1	0.3	B.ACT	6	G A	DIA	0	QT	-cs.07			
1 F C V O 3 . 2 4 2		-2	503.1	F.3	E ACT	- 6 ,	ŚA	DIA-	-0	Q T	- cs - 07			
1FCV03.245	03	2	803.1	A . 3	B.ACT	6	G A	DIA	-0	QT	cs.07			
1¢KV03.805A	C3	-3	803.2	- F • 5	C.ACT	-8	C K	SLF-	с	C V	CS.OS PS			
1CKV03.806B	C3	3	803.2	F.6	C.ACT	8	CK	SLF	c	cv	cs.08			
1ckv03.810s	63	3	803.2	-G . 4	C.ACT	-10	c ĸ	SLF		c v	- PS - 08 - PS	:		
1CKV03.814A	03	3	803.2	F.5	C.ACT	1.5	CK	SLF	С	C V		- · · · · · · · · · · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·
1CKV03.8158	C3	3	803.2	F.6	C.ACT	1.5	CK	SLF	С	c v				
10KV03.812\$	03	3	803.2	G.6	C.ACT	1.5	εĸ	SLF	С	c v				
1 CKV03.820A	03	3	803.2	F.5	C.ACT	6	ск	SLF	С	cv	CS.09			
1CKV03.8218	C3	3	803.2	F.6	C.ACT .	6	CK	SLF	С	cv	CS.09	***************************************		

	IST VALVES OF		L.SPC LPT	TR 07:27:18	04-11-	86 PAGE Catery	SIZE	TYPE	ACT	N.POS	TESTS	ALTER RELIEF
-	TCKV03.8308	03	2	803.2	F.8	C.ACT	4 .	cĸ —	SLF		CA	CS-09
-	1CKV03.831A	03	2	803.2	E . 8	C.ACT	4	CK	SLF	C	cv	cs.09
-	TCKV03.832A	03		803.2	8.0	C.ACT	4	CK	SLF	С	CV	cs.09
	1CKV03.5338	C 3	2	803.2	E . 8	C.ACT	4	tk	SLF	τ	cv	CS.C9
	1CKV03.8618	C3	2	803.2	G.10	C.ACT	4	· cĸ	SLF	С	cv	£\$.09
_	1CKV03.8625	C3	2	303.2	E.10	C.ACT	4	-ck	SLF	С	- c v	CS-09
_	1CKV03.8645	C3	3	803.2	6.6	CACT	6	cĸ	SLF	с	-cv	cs.10
	1CKV03-871A	03	2	803.2	F.8	C.ACT-	4	-cĸ	SLF	С —	C V	cs-10
_	1CKV03.8729	C3	2	803.2	0.8	C.ACT	4	CK	SEF	С	cv	cs-10
_	1CKV03.8738	03	-2	803.2	C.8	C.ACT	4	СК	SLF	с	c∨	CS.10
_	1CKV03.874A	C3	2	803.2	A . 8	C.ACT	-4	- cĸ	SLF	с	c v	-cs.10
_	1CKVG3.891S	03	-2	803.2	8.8	C.ACT	4	ск	SLF	c —	€V	- CS.11 PS
_	1ckv03.892s	03	2	803.2	A . 8	C.ACT	4	CK	SLF	C ,	cv	CS.11
_	1CKV03.921S	- c 3		803.2	-6.10-	CACT	4	-ск	SLF-	С	-cv	- cs.09
_	1CKV03.9228	-03		503.2	£.10	C.ACT	4	- c k	SL.F	-	c v	- CS - 09
	1FCV03.116A.A	03	-3	803.2	F.5	B.ACT	- 4	GA	тем	С	QT	
_	1FCV03=1165.A	03	- 3	803.2	F.5	B.ACT	4		MOT	-с	- QT	
_	1FCV03.126A.B	C3	-3	803.2	F . 7	E.ACT	4	G A-	TCM		QT	
_	1FCV03.1252.8	- C3	3	803.2	F.7	B.ACT	- 4	G A	MOT	c	-07	
_	1FCV03-136A.A	03		803.2	G.5	E.ACT	-6	- G A	MOT	-с	QT	
_	1FCV03.136B.A	03	3	803.2	6.5	- P.ACT	6	G A	MOT	c —	QT -	
_	1FCV03.179A.E	C 3		803.2	н.5	- E . A C-T	-6	- S A	MOT		Q T	<u> </u>
_	1fcv03.1798.8	- 63	-3	863.2	H-5	B.ACT	- 6	G A	- 401 -	- с	97	
_	1LCV03.148.8	03	-3	603.2	- f . 8	- E - A C T		-6L	- D I 4 -	-c	-0.T	
_	1LCV03.148A.E	-63	-3	803.2	F.8-	S.ACT	2	-ANG	-DIA-	- 6	· QT	

VALVES	. 5YS		PTR 07:27:18	04-11-1 COORD	CATERY	SIZE	TYPE	ACT	N.POS	TESTS	ALTER	RELIEF	
1FCV26.244B	76		DED 6			•						RR.13	
	26	3	850.9	G.1	2.ACT	4	GA	MOT		. QT			
1FCV26.245A	26	3	650.9	6.1	E-ACT	4	G A	MOT	0	GT			
1FCV30.007A	30	2	856.1	C.2	A.ACT	24	EUT	CYL	C	QT.LT	AJ	RR.12 RR.13	
1 F C V 3 0 . 00 8 B	30	. 2	366.1	C.2	A.ACT	24	BUT	CYL.	С	QT.LT	AJ	RR.12	
1FCV30-0098	30	2	865.1	C.2	A.ACT	- 24	801	CYL				RR • 13	
					nene:				· ·	QT.LT	AJ	RR.12 RR.13	
1 F C V 3 0 . 0 1 0 A	30	2	566.1	Ç.2	A.ACT	24	BUT	CYL	<u> </u>	QT.LT	AJ	RR.12 RR.13	
1FCV30.014A	30		556.1	E . 2	A.ACT	24	BUT	CYL		QT.LT	AJ	RR.12	
												RR.13	
1FCV30.0158	30	2	866.1	E.2	A.ACT	24	BUT	CYL	С	QT.LT	AJ	RR.12 RR.13	
1FCV30.016	- 30		355.1	F . 2	A.ACT	24	вит	CYL		QT.LT	- A I	RR.12	
										W la L l		RR.13	
1FCV30.017	- 30	2	866.1	F • 2	A.ACT	24	BUT	CYL	С	QT.LT	AJ	RR.12	
1 F C V 3 0 - 01 9 8	30-	2	666.1	6.2	A . A C T	24.	BUT	CYL	- c		— A J — —	RR:12	
												RR.13	
1 F C V 3 O . O 2 O A	30	2	866.1	G • 2	A.ACT	24	BUT	CYL	<u> </u>	QT.LT	AJ	RR.12	
 	30	-2	865.1	D.10	A . Á C T	- 24	9UT -	CYL	С	QT.LT		RR.12	
												RR.13	
1FCV30.040	30	2	866.1	D.10	A.ACT	24	BUT	CYL	С	QT.LT	AJ	RR.12 RR.13	
1FCV30.05GE	30		856.1	c.10	A.ACT	24	- 801	CYL		QT.LT	AJ	RR.12	
										W1.L1		RR.13	-
1FCV30.051A	30	2	866.1	c.10	A.ACT	24	aut	CYL	С	QT.LT	AJ	RR.12 RR.13	
1FCV30.052A	30		- 856.1	-c.16	A.ACT		- eut -	CYL	·	- 01.LT -	<u> </u>	PR.12	
***										TWITE L	- NJ	RR.13	

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) .	LIST VALVES		L.SPC		B 04-11-	86 PAGE	7 S17E	TYPE	ACT	N.POS	TESTS	ALTER	RELIEF
1	1FCV30.0533	30	2	355.1	c.10	A.ACT	-24 .	SUT	CYL	· · · · · ·	QT.LT		RR.12 RR.13
) [']	1FCV30.056A	30	2	866.1	E.10	A.ACT	24	BUT	CYL	С	QT.LT	AJ	RR.12
٠	1fcv30:0578	30		866.1	E-19	- A.ACT	24	SUT	CYL		37. LT	AJ	FF.12 RR.13
•	1FCV30.0588	30	2	866.1	6.10	A.ACT	24	BUT	CYL	С	QT.LT	AJ	RR.12
	1FCV30.059A	30-	2 -	955.1	G.10	A.ACT	- 24	SUT	CYL	- с	GT.LT	- AJ	RR.12 RR.13
•	1FSV30.134	30	2	866.1	F. 9	A • A C T	0.5	PLUG	SOL	0	QT.LT	AJ	RR.12
)													RR.13 FR.21
	1fSV30.135	30	2	866.1	F.10	A.ACT	0.5	PLUG	SOL	0	QT.LT	AJ	RR.12 RR.13 RR.21
•	1FCV31.305B	31	2	865.5	B.7	A.ACT	2	G A	DIA	0	QT.LT	AJ	RR.12
•	1FCV31.306A	31		865.5	- B • 8	A.ACT		G A	- DIA -	- 0	QT.LT	A J	RR.12
•	1FCV31.308A	31	2	865.5	C.8	A.ACT	2	G A	DIA	0	QT.LT	AJ	RR.12
-	1fcv31.3098	31		865.5		- A . A C T	5	G A	DIA	-0	GT.LT	AJ	RR.12 RR.13
	1FCV31.326A	31	2	865.5	E.7	A.ACT	2	G A	DIA	0	QT.LT	AJ	RR.12 RR.13
•	1FCV31.3278	31	2	865.5		A.ACT			DIA	•	GT.LT	AJ	RR.12 RR.13
•	1fCV31.329B	31	2	865.5	F.8	A - A C T	2	G A	DIA	0	QT.LT	AJ	RR.12 RR.13
	1FCV31.330A	31		865.5	F • 7	A • A CT	- 2	- G A	DIA		01.LT-	AJ	RR.12 RR.13
	116031.3378	31	2	865.5	F.8	AC.PAS	0.5	СК	SLF	С	LT	AJ	RR.12
	118031.3392	- 31 -		365.5	E . 8	AC.PAS	0.5	ск	- SLF	E	LT	- A J	<u>R</u> R.12
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<u>.</u>	LIST VALVES TO		L.SPC LP	TR 07:27:18	04-11-	86 PAGE CATGRY	8 SIZE	TYPE	ACT	N.POS	TESTS	ALTER	RELIEF
)						 	•		· · · · · · · · · · · · · · · · · · ·				RR.13
)	118031.3407	31	2	865.5	C.S	AC.PAS	0.5	C K	SLF	C	LT	AJ	RR.12 RR.13
•	118031.3421	31	2	865.5	P.8	AC.PAS	0.5	cĸ	SLF	С	LT	AJ	PR-12 RR-13
)	18YV32.288	32	2	548.1	C.9	A.PAS	2	GL	MAN	С	LT	AJ	RR.12 RR.13
)	18YV32.298A	32	2	848.1	в.9	A.PAS	2	GL	MAN	С	LT	AJ	RR.12 RR.13
)	1BYV32.3088	32	2	546.1	0.9	A.PAS	2	GL	MAN	τ	LT	AJ	RR.12 RR.13
3	1CKV32.293A	32	2	848.1	5.10	AC.ACT	2	CK	SLF	0	CV.LT	CS.12	RR.12 RR.13
)	1 CKV32.303A	32	2	843.1	c.10	ACAACT	2	C K	SLF	0	CV.LT	CS.12 AJ	RR.12 RR.13
)	1ckv32.3138	32	2	648.1	D.10	AC.ACT	2	CK	SLF	0	CV.LT	CS.12	RR.12
)	-1FCV32.080A	32	-2	548.1	.9	A . A CT	-2	G A	DIA	0	QT.LT	C3.12 AJ	RR.12
)	1FCV32.102B	32	2	845.1	D.9	A.ACT	2	G A	DIA	0	QT.LT	CS.12	RR.12 RR.13
)	1FCV32.110A	32	2	848.1	A . 9	A . A C T	- 2	G A · · ·	- DIA -	0	07.LT		RR.12 RR.13
•	1 CKV33.714	33	2	846.2	F.6	AC.PAS	3	СК	SLF	С	LT	AJ	RR.12 RR.13
•	118V33.713	33		345.2	F.6	A.PAS	2	DIA	MAN	-с	<u>L</u> Ŧ	AJ	RR.12 RR.13
)	1 FCV43.002B	43	5	625.01	0.3	A.ACT	.375	G A	DIA	С	QT.LT	AJ	RR.12 RR.13
ز	1FCV43.0118	43		625.01	3.2	A . A C T	.375	G A	DIA	- c .	GT.LT	A J	RR.12 RR.13
<u>;</u>	1FCV43.022B	43	2	625.01	F.5	A.ACT	.375	G A	DIA	0	QT.LT	AJ	RR.12 RR.13
<u>.</u>	1fcv-3.023A	43		625.01	0.5	A.ACT	.375	- GA	DIA	0	• • • • • • • • • • • • • • • • • • •	AJ	- RR.12
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	LIST VALVES ECM						9 - 317E	T YPE	ACT	N.POS	- TESTS	ALTER	RELIEF
	1FCV43.0348	43	2	625.02	3.2	A . A C T	.375	G A	DIA	С	QT.LT	AJ	RR.12 PR.13
	1FCV43.035A	43	2	625.02	C _ 4	A.ACT	.375	G A	DIA	С	QT.LT	AJ	RR.12 RR.13
	1FCV43.0540.B	43	2	625.02	C.7	A.ACT	.375	- G A	DIA	0	QT.LT	L A	RR.12 RR.13
_	1FCV43.055A	43	2	625.02	C • 6	A.ACT	.375	G A	DIA	0	QT.LT	AJ	RR.12 RR.13
	1 F C V 4 3 - 05 6 0 - 8	43		625.02	- C = 8	A.ACT	.375	G A	DIA	0	97.LT	AJ	RR.12 RR.13
	1FCV43.058A	43	2	625.02	c . 7	A.ACT	.375	G A	DIA	0	QT.LT	AJ	RR.12
_	1 F C V 4 3 . 0 5 F D . B	43	2	625.02	0.8	A.ACT	.375	G A	DIA	0	GT.LT	AJ	RP.12 RR.13
_	1FCV43.061A	43	2	625.02	D.8	A.ACT	.375	G A	DIA	0	aT.LT	AJ	RR.12 RR.13
	1FCV43-0630-E	43	-2	625.02	D • 9	- A - A C T	- 375	G A	DIA	0 '	- 01 LT -	—AJ	RR.12
_	1 FCV43.064A	43	2	625.02	8. d	A.ACT	.375	G A	DIA	0	GT.LT	AJ	FR.12 RR.13
_	1FCV43.075	43	-2	625.07	E . 7	A.ACT	. 375	G-A	DIA	 	9T.LT	- AJ	FR.12 RR.13
	1FCV43.077A	43	2	625.07	E.8	A.ACT	.375	G A	DIA	С	QT.LT	AJ	RR.12 RR.13
_	1FCV43.201A	43	2	625.11	H-5	- A . A C T	.375	G A	DIA	0	GT.LT	AJ .	PR.12 RR.13
	1FCV43.202A	43	2	625.11	G.5	A.ACT	.375	G A	DIA	0	QT.LT	AJ	RR.12 RR.13
	1FCV43.2078	43	2	025.11	€.7	A . A CT	. 37-5	G A	DIA		QT.LT	- AJ	RR.12 RR.13
	1FCV43.2088	43	2	625.11	D.7	A.ACT	.375	G A	DIA	0	QT.LT	AJ	RR.12 PR.13
	10KV43.N0001	43	2	625.15	e.4	AC.ACT	•375	c ×	SLF	-c	LT	cs.13	RR.12

	 					4.0)
VALVES					86 PAGE CATGRY	10 \$12E	TYPE	A CT-	N.POS	TESTS	ALTER	RELIEF		•
								· · ·			ĀJ	RR.13		
1CKV43.N0002	43	2	625.15	æ.10	AC.ACT	.375	-ск	SLF	С	LT	CS.13 AJ	RR.12 RR.13	:	
1 CKV43.NOC26	43	2	625.15	B.10	AC.ACT	.375	ск	SLF	С	LT	CS.13	RR.12 PR.13	:	
1CKV43.N0030	43	- 2	625.15	н.4	AC.ACT	.375	<u>.</u> ск	SLF	-с	LT	- CS.13 AJ	RR.12 RR.13	:	· · · · · · · · · · · · · · · · · · ·
1FSV43.250	43	2	625.15	D.1	A.ACT	.375	PLUG	SOL	С	LT	CS.13	RR.12 RR.13	;	
												RR.21		
1FSV43.251	43	2	625.15	c - 1	A.ACT	.375	PLUG	SOL	С	LT	CS.13	RR.12 RR.13 RP.21	<u></u>	
1FSV43.287	43	2	625.15	c.9	A.ACT	. 375	PLUG	SOL	С	LT	CS.13	RR.12		
												RR.21		
1FSV43.288	43	2	625.15	3.9	A.ACT	.375	PLUG	SOL	С	LT	CS.13	RR.12 RR.13 RR.21		
1FSV43.307	43	2	625.15	c.10	A.ACT	.375	PLUG	SOL	С	ĻT	CS.13	RR.12		
												<u>RP.21</u>		
1FSV43.309	43	2	625.15	D • 2	A . A C T	-375	PLUG	SOL	С	LT	CS.13	RR.12 RR.13 RR.21		
1FSV43.310	43	2	625.15	C • 2	A.ACT	.375	PLUG	SOL	С	LT	CS.13	RR.12 .RR.13		
1FSV43.318	43	2	625.15	C.9	A.ACT	.375	PLUG	SOL		LT	cs.13	RR-12		
											AJ-	PR.13 PR.21		
1FSV43.319	43	2	625.15	B.9	A.ACT	.375	PLUG	SOL	С	LT	CS.13	RR.12 RR.13		
1FSV43.325	43	2	625.15	c.10	A . A C T	.375	PLUG	SOL		LT	cs.13	PR.21 RR.12		
											A J	RR.13 RR.21		

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	VALVES					-86 PAGE	11 5175	TYPE	ACT	N.POS	TESTS	ALTER	RELIEF
•	1FSV43.341	43		625.15	н.5	A.ACT	- 375,	PLUG	SOL	c	LT	- cs.13 - AJ	RR.12
0		· · · · · · · · · · · · · · · · · · ·		*****									RR.21
	165743.342	43	2	525.15	6.5	A.ACT	.375	PLUG	SOL	c -	LT -	CS.13 AJ	RR.12 RR.13
3	1FCV43.003A	43	2	652.01	C.5	A.ACT	.375	G A	DIA	_c	GT.LT	AJ	RR.12
:)	1FCV43.012A	43	2	652 .01	8.4	A.ACT	. 375	G A	DIA	С	QT.LT	AJ	RR.13
<u>.</u>	115852.500	52		331.3	н.4	A.PAS	0.75	G.A.	MAN		LT.		RR.13
. ,									r: AN		L 1	AJ	RR.13
)	113852.501	52	2	331.3	H . 4	A.PAS	0.75	G A	MAN	С	LT	AJ	RR.12
)	11\$852.502	52	-2	331.3	-н.4	A.PAS	0.75	G A	MAN	с	LT	AJ	RR.12
:)	118852.503	52	2	331.3	н.4	A.PAS	0.75	G A	MAN	С	LT	AJ	RR.12
O	118B52-504	52		331.3	H.4	A.PAS	0.75	- G A	MAN -	· ·	LT	AJ	RR-12 RR-13
O	1ISB52.505	52	2	331.3	H • 4	A.PAS	0.75	G A	MAN	С	LT	AJ	PR.12
O	118852.506	52		331.3	H.4	A.PAS	-0.75-	G A	MAN	-с	LT-	AJ	PR.12 RR.13
o j	118852.507	52	2	331.3	н.4	A.PAS	0.75	G A	MAN	С	LT	AJ	RR.12
0	118V59.522	59	-2	856.1	F.3	A.PAS		- CA	MAN	- c	LT	- AJ	RR.12
O.	1ISV59.698	59	2	856.1	F.3	A.PAS	2	DIA	MAN	С	LT	AJ	RR.12 RR.13
G	1CKV61.533		 2	814.2	A . 5	AC.PAS	• 3 7 5	-cĸ -	SLF-	- C	LT	LA	RR.12 RR.13
C	1CKV61.68C	61	2	814.2	A . 6	AC.PAS	.375	СК	SLF	С	LT	AJ	RR.12
C	1CKV61.692	- 61	-2	814.2	F.10	AC.PAS	.375	ск	SLF	c	LT	AJ	RR-12
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	LIST VALVES.	MIT DB'	L.SPC LPT	TR 07:27:18	04-11-5	36 PAGE	12						
-	VALVES	SYS	CLASS	DWG.NO		CATGRY	SIZE	TYPE	ACT	N.POS	TESTS	ALTER	RELIEF
						· ·		1 _		7.7			RR.13
_	1CKV61.745	61		814.2	H.1C	AC.PAS	±375	CK	SLF	С	LT	AJ	RR.12 RR.13
_	1FCV61.096A	61	2	814.2	F.10	A.ACT	2	DIA	DIA	0	QT.LT	AJ	RR.12 RR.13
-	1FCV61.097B	61	- 2	314.2	F.10	A.ACT	2	DIA -	DIA	-0	QT.LT	AJ -	RR.12
-	1FCV61.110A	61	2	314.2	н.10	A.ACT	2	DIA	DIA	0	QT.LT	AJ	RR.12 PR.13
_	1FCV61.122B	61	2	814.2	н.10	A.ACT	2 -	DIA -	DIA	0	QT.LT	A_J	RR.12 RR.13
_	1FCV61.191A	61		814.2	A . 5	A.ACT	4	DIA	DIA	0	QT.LT	AJ	RR.12 RR.13
_	1FCV61.1928	- 61	-2	314.2	A . 6	A.ACT	4	DIA	DIA	0 -	- - GT.LT	— A J	RR.12 RR.13
_	1FCV61.193A	61	2	314.2	A • 5	A.ACT	4	DIA	DIA	0	QT.LT	AJ	RR.12 RR.13
_	1FCV61.1949	c1	2	814.2	A • 6	A.ACT -	-4	DIA	- DIA -		ùT.LT	— A J	PR.12 RR.13
_	1 CK V 62.504 S	62	2	309.1	н.10	C.ACT	8	СК	SLF	С	CV	PS.RR	RR-14
	1CKV62.519S	62	2	309.1	F.9	C.ACT	3	CK	SLF	0	CV		RR.27
	1 C K V 62 . 523 A	62	2	809.1	н. 9	C.ACT	2	CK	SLF	С	CV		,
	1CKV62.525A	62	2	309.1	н.9	C.ACT	4	cĸ	SLF	C -	cv	PS.RR	RR.15
	1CKV62.5308	62 .	-2	909.1	6.9	C.ACT	-2	- ск	SLF	-c			
-	106762.5328	<u>62</u>	2	809.1	6.9	C.ACT	4	- ек	3LF	-c		F3.RR	RR.15
_1	1 CKV62.639S	- 62	2	809.1	C.7	AC.PAS	0.75	СК	SLF	С	LT	AJ	RR.12 RR.13
_	1FCV82.0819	02	2	209.1	2.7	A.ACT	4	G A	мот	-9	37.LT	CS.14	RR.12 RR.13
_	1 F C V 6 2 . 0 6 3 A	62	2	809.1	3.8	A.ACT	4	GA	мот	0 .	QT.LT	CS.14	RR.12

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TALVES	375		TR 07:27:18	CCORD	86 PAGE CATERY	13 ⁻ SIZE-	TYPE	ACT	- N.POS-	TESTS-	ALTER-	RELISE		
1FCV62.072A	62	2	809.1	A . 5	A.ACT	2 .	GL	DIA	С	QT.LT	AJ	RR.12		***************************************
1FCV62.073A	62	2	309.1	A . 4	A.ACT	-5	GL	DIA	0 -	QT.LT	A J	RR.13 RR.12 RR.13	:	. ,
1FCV62.074A	62	2	809.1	A • 4	A.ACT	2	. GL	DIA	C	OT.LT	AJ	RR.12		
1FCV62.076A	62	2	809.1	A ± 5	A.ACT	2	GL	DIA	0	QT.LT	AJ	RR.13 RR.12		
1FCV62.077B	62	2	809.1	A.7	A.ACT	2	GL	DIA	0	QT.LT	AJ	RR.12		-
1FCV62.090A	62		809.1	0.7	B.ACT	_3	G A	MOT	0	QT		- RR.13		
1FCV62.0913 1LCV62.132A	62 62	2	809.1	D.8 ε.10	E.ACT	3	G A	MOT		QT				
1LCV62.1338 -	- 52 -	- 2	809.1	E.10	B.ACT	4	GA.	- MOT -	0	- Q T	- CS . 1 6 -			
1LCV62.135A	62		809.1	н.10	B.ACT	8 -	G A	MOT	-c	01	- 03.16 - - 05.17 -		,	
LCV62.1368	62-	- 2	839.1	H=10	B.ACT	- e	G A	MOT	- c - '	- 6 T	CS.17			
RFV62.505	- 62 -	-2	809.1	-F.10	- C . A C T	-1 -	REL	-SLF-		- 75	· <u>.</u>		<u> </u>	
RFV62.6498	62	- 2	309.1	- C . 9	- C.ACT	- 2	REL	-SLF		- 8 T				
RFV62.6628	62		809 .1	— A . 3 ——	AC.ACT	-2	REL	SLF		87.LT	—AJ	RR.12 RR.13		
RFV62.675S	62	2	809.1	A - 10	C.ACT	2	REL	SLF	С	BT				
RFV62.688S	62	2	809.1	D.9	C.ACT	3	REL	SLF	С	вт			·. :	
SFV62.518	62	2	809.1	E.9	C.ACT	. 75	REL	SLF	С	ЭТ			· ·	
FCV62.138B	62	2	509.2	8.4	B.ACT	3	GL	MOT		QT				
CKV63.5028	63	2	811.1	f.10	C.ACT	12	CK	SLF	С	CV	PS.RR	RR.16	:	
CKV63.51CS	63	2	311.1	D.10	C.ACT	8	CK	SLF	С	cv	PS.RR	RR.17		
CKV63.524A	63	2	811.1	ē.8	C.ACT	4	CK	SLF	С	CV	PS.RR	RR.27 RR.34)	

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		<u> </u>				· ·										
Ċ	LIST VALVES		L.SPC LP	TR 07:27:18	04-11-	86 PAGE	14		***	- ** - ** - • • • • • • • • • • • • • • • • • •	· 	·				
•)						CAIGRY	SIZE	TYPE	ACT	N.POS	TESTS	ALTER	RELIEF	r 1	, -	` '
•	1¢KV63.526B	63		811.1	D.8	C.ACT	4	CK	SLF	Ć ·	cv	PS.RR	RR.27 FR.34	<u>.</u>		
_	TCKV63.528A	63	2	511.1	E-8	CACT	0.75	ск	SLF	с —	c v 					
n	1CKV63.53CB	63	2	E11.1	0.8	C.ACT	0.75	CK	SLF	c	cv			1		
C	1CKV63.543A	63	1	811.1	F . 4	ACART	2	-cĸ	SLF	·c	CV-LT	PS.RR	RR - 18	<u> </u>		
	1CKV63.545A	63	1	<u>ε11.1</u>	E.4	AC.ACT	2	CK	SLF	с —	CV.LT	PS.RR	FR.18	-{	<u> </u>	
9	1CKV63.5478	63	1	611.1	0 - 4	AC.ACT	2	CK	SLF	c	CV.LT	PS.RR	RR.18			
O.	1CKV63.549B	63	1	811.1	E . 4	ACTACT	-2 -	CK-	SLF	. c	CV-LT	PS.RR	RR.18			
_	1003.5515	63	1	811.1	6.1	AC.ACT	2	cĸ	SLF	c	CV.LT	PS.RR	RR.18			
จ	1CKV63.5535	63		311.1	н.3	AC.ACT	2	-cĸ	SLF	С	CV-LT	PS.RR	RR.13			
C	1CKV63.5555	63	1	811.1	6.3	AC.ACT	-2	- ск	SLF	с	-CV.LT	PS.RR	RR.18 ,			
Δ.	10KV63.5578	£3	1 :	811:1	G . 2	AC.ACT	2	ck	SLF	-с	CV.LT	PS.RR	-RR.18		· · · · · · · · · · · · · · · · · · ·	
'	-1ckv63.5588	63	1	811.1	E . 2	AC.ACT	6	ск	SLF	-с	CV.LT	FS.RR	RR.18			
0	10KV63.5598	ć3	1'	811.1	D.1	AC.ACT	-6 -	c K	SLF	<u> </u>	CV.LT	PS.RR	RR.18			
	10KV63.5608	63	1	811.1	₹.1	AC.ACT	10	-ск`	SLF	е	CV.LT		<u>RR.20</u>			<u> </u>
o	10KV63.561S	- 63	-1	311.1	D . 2	AC.ACT	10	ск	- St-F-	с —	CV.LT		RR. 20			
O .	10KV63.5628	63	1	811.1	0.3	AC.ACT	10	-ск	SLF	е	-cv.LT		RR. 20			 -
	1 CKV63.5638	63	-1	811.1	F . 2	AC.ACT	10 -	-ск	SLF	е	CV.LT		-RR.20			
O .	1CKV63.5818	63	1	811.1	5.7	C.ACT	3 -	- ск	SLF-	с	- c v	PS.RR				<u> </u>
0	1CKV63.5868	63	1	311.1	E-1	CACT	1.5	ск	SLF	С	c v ·	PS.RR	RR.19			
	1CKV63.5878	c 3	-1	311.1	0.2	C.ACT	1.5	c ĸ-	SLF	С	- c ∨	FS.RR	RR.19			
0 .	1CKV63.588\$	63	-1	311.1	0.2	CACT	1.5	ск	SLF	С	cv	PS.RR	RR-19			
e ·	1CKV63.589S	£5	1	811.1	E . 2	C.ACT	1.5	-ск	SLF	-с	- c v	PS.RR	RR.19			
,	1CKV53.6225	c 3	1	511.1	c.1	AC.ACT	10	ck -	- SLF	е	CV.LT	-PS	PR.20	· · · · · · · · · · · · · · · · · · ·		
C	1CKV63.623S	- 63 -	1	811.1		ACAACT	10	-c×	SLF	-c	- (P 5	- 20			
C	1CKV63.6245	63	1	311.1		AC.ACT	10	ск	SLF	-е	CV.L7-		- RR - 20			
																
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	ALVES	MIT DBI	CLASS	TR 07:27:18	04-11-1	36 PAGE CATGRY	15 312E	TYPE	A C T	N.POS	TESTS	ALTER	RELIEF	
1	CKV63.625\$	63	1	811.1	C.3	AC.ACT	10	ск	SLF	C	CV.LT	PS	RR.20	· · · · · · · · · · · · · · · · · · ·
1	CKV63.632A	63	1	811.1	G.3	AC.ACT	6	CK	SLF	С	CV.LT	CS.18		
1	CKV63.633B	63	1	811.1	G.2	AC.ACT	6	CK	SLF	С	CV-LT	CS.18		
1	CKV63.634A	63	1	811.1	G.3	AC.ACT	6	. CK	SLF	С	CV-LT	CS.18		
1	CKV63.635B	63	1	811.1	G • 2	AC.ACT	6	CK	SLF	c ·	CV.LT	cs.18		
1	CKV63.640S	63	1	811.1	F . 4	AC.ACT	8	СК	SLF	С	CV.LT		RR.35	
_1	CKV63.641S	63	1	811.1	f.4	AC.ACT	8	C K	SLF	С	CV.LT		RR.18	
_1	CKV63.643S	63	1	811.1	F - 4	AC.ACT	3	CK	SLF	С	CV.LT		RR.35	
_1	CKV63.644S	63	1	311.1	D.2	AC.ACT	6	CK	SLF	С	CV.LT		RR.18	
_1	FCV63.001A	63	2	B11.1	E.10	B.ACT	14	G A	MOT	0	QT	cs.19		,
1	FCV63.003A	63	2	311.1	D.8	B.ACT	2	GL	MOT	0	QT -	C\$.20		
1	FCV63.004B	63	2	311.1	D.8	B.ACT	2	GL	мот	0	QT			
1	FCV63.005B	ć 3	2	§11.1	D.10	B.ACT	8	G A	MOT	0	QT	cs.21		
1	FCV63.006B	63	2	811.1	F • 10	E.ACT	4	G A	MOT	С	QT			
1	FCV63.007A	63	2	811.1	F.10	B.ACT	4	G A	MOT	С	QT			
1	FCV63.008A	63	2	811.1	н.9	B.ACT	8	G A	MOT	С	QT	CS.22		
1	FCV63.011B	63	2	811.1	E . 9	B.ACT	8	G A	MOT	c	Q T	CS.22		
1	FCV63.022B	63	2	811.1	0.6	9.ACT	4	G A	MOT	0	QT	CS.23		
1	FCV63.023B	63	2	311.1	D.7	A - ACT	1	GL	DIA	С	QT.LT	AJ	FR.12	
							· · · · · · · · · · · · · · · · · · ·						RR.13	
	FCV63.025B	63		811:1	A • 7	BACT	4	G A	MOT	- c	- GT			
	FCV63.026A	0.5	2	911.1	8.7	E.ACT	- 4	G A	MOT	- c	GT			
	FCV63-047A	63		\$11.1	E.10	B.ACT	6	G A	MOT	0	- 9T		<u> </u>	
	FCV03.0488	- 63	2	811.1	0.10	BACT	- 6	G A	MOT	•	QT			
-1	FCV63.071A	- 63	-2	611.1	C . 6	A.ACT	0.75	GL	DIA		- QT.LT-	AJ	RR.12	
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VALVES		CEASS	PTR 07:27:18	04-11-	86 PAGE Catgry	16 SIZE	TYPE	ACT	N.POS	TESTS	ALTER	RELIEF	· , \		
1FCV63.072A	- 63	- 2	811.1	н.6	S.ACT	18	G A	мот	С	QT	CS.24				-
TFCV63.0738	63	2	811.1	н.б	B.ACT	18	GA '	MOT	С	QT	CS.24				
TFCV63.0348	63	2	811.1	t.6	ATACT	0.75	GL	DIA	c	QT.LT	AJ	RR.12 RR.13			
1FCV63.093A	63	2	811.1	6.7	E.ACT	8	, G A	MOT	0	QT	<u></u>	88613			
1 F C V 63 . C 9 4 B	63	2	811.1	G.7	B.ACT	8	G A	MOT	0	Q T			•		
1 F C V 63 . 152 A	63	2	311.1	E.7	B.ACT	4	G A	MOT	0	QT					
1FCV63.1538	63	2	311.1	D.7	B.ACT	4	G A	MOT	0	QT					
1FCV63.156A	63	2	811.1	E.6	P.ACT	4	G A	MOT	С	QT					
1FCV63.157B	63	2	811.1	D.6	B.ACT	4	G A	MOT	С	ОТ	· · · · · · · · · · · · · · · · · · ·				
1FCV63.172B	63	2	811.1	F.6	B.ACT	12	G A	MOT	С	QT					
1FCV63.175B	63	2	811.1	D . S	B.ACT	2	GL	MOT	0	QT					
1 F C V 6 3 . 177 A	63	2	311.1	F.10	B.ACT	4	G A	MOT	0	QT					
1RFV63.511A	63	2	811.1	D.10	C.ACT	0.75	REL	SLF	С	8 T					
1RFV63.534A	63	2	811.1	E.7	C.ACT	0.75	REL	SLF	С	вт					
RFV63.5358	63	2	311.1	D.7	C.ACT	0.75	REL	SLF	С	вт					
IRFV63.536B	63	2	811.1	D.7	C.ACT	0.75	REL	SLF	С	вт					
RFV63.5778	63	2	811.1	A - 8	C.ACT	0.75	REL	SLF	С	вт					
RFV63.602S	63	2	811.1	A - 1	C.ACT	1	REL	SLF	С	вт					
RFV63.603S	63	2	811.1	A . 3	C.ACT	1	REL	SLF	С	вт				· · · · · · · · · · · · · · · · · · ·	
RFV63.604S	63	2	811.1	A . 4	C.ACT	1	REL	SLF	С	вт					
RFV63.605\$	63	2	811.1	A • 5	C.ACT	1	REL	SLF	С	вт					
RFV63.625A	63	2	811.1	6.7	C.ACT	2	REL	SLF	С	БТ					
RFV63.627B	63	2	811.1	e.7	C.ACT	2	REL	SLF	С	ЭТ_		· · · · · · · · · · · · · · · · · · ·			
RFV63.6378	63	2	311.1	F.7	C.ACT	0.75	REL	SLF	С	вт					
FCV63.064A	63	2	830.6	a.5	A.ACT	1	GL	DIA	С	QT.LT	AJ	RR.12			

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LIST VALVES at	MIT DBL	SPC LPT	R 07:27:18	04-11-8	6 PAGE CATGRY	17 SIZE	TYPE	A C T	N.POS	TESTS	ALTER	RELIEF	
OCKV67.503A.A	67	3	845.1	E.9	C.ACT	20 .	CK	SLF	c	cv		RR.27 ·	
OCKV67.503B.A	67	3	345.1	E.8	C.ACT	20	CK	SLF	С	cv		RR.27	
OCKV67.503C.A	67	3	845.1	F.8	C.ACT	20	CK	SLF	С	cv		RR.27	
OCKV67.503D.A	67	3	845.1	F • 9	C.ACT	20	CK	SLF	С	cv		RR.27	
OCKV67.503E.B	67	3 .	845.1	F • 6	C.ACT	20	CK	SLF	С	cv		RR.27	
OCKV67.503F.B	67	3	845.1	F.7	C.ACT	20	CK	SLF	С	C.V		RR.27	
OCKV67.503G.B	67	3	845.1	E.7	C.ACT	20	CK	SLF	С	c v		RR.27	
OCKV67.503H.B	67	3	345.1	E,•6	C.ACT	20	CK	SLF	С	CV		RR.27	
1CKV67.508A.A	67	3	845.1	C.10	C.ACT	8	СК	SLF	С	cv			
1CKV67.5088.E	67	3	845.1	C.6	C.ACT	δ	CK	SLF	С	cv			
1CKV67.513A.A	67	3	345.1	C.10	C.ACT	8	CK	SLF	С	cv			
1ckv67.5138.8	67	3	845.1	C.6	C.ACT	8	CK	SLF	С	cv			
1FCV67.022	67	3	845.1	6.9	B.ACT	24	BUT	MOT	0	QT	cs.25		
1FCV67.024	67	3	845.1	F.6	B.ACT	24	au T	мот	0	GT	C\$.25		
1FCV67.065B	67	3	845.1	C.6	B.ACT	8	BUT	MOT	С	QT			
1FCV67.066A	67	3	845.1	c.10	B.ACT	8	BUT	MOT	С	· Q T			
1fCV67.067B	67	3	345.1	C.6	B.ACT	8	BUT	MOT	С	QT			
1FCV67.068A	67	3	845.1	c.10	B.ACT	8	EUT	MOT	С	QТ			
2CKV67.508A.A	67	3	845.1	C.8	C.ACT	8	CK	SLF	С	cv			
2CKV67.5083.B	67	3	845.1	C • 4	C.ÁCT	8	CK	SLF	С	c v			
2CKV67.513A.A	67	3	345.1	C.8	C.ACT	8	- CK	SLF	С	cv			
2CKV67.5138.8	67	3	845.1	C • 4	C.ACT	3	ÇK	SLF	С	cv			
2FCV67.022	67	3	845.1	F.9	B.ACT	24	BUT	MOT	0	QT	CS.25		
2FCV67.024	67	3	845.1	G • 6	B.ACT	24	BUT	MOT	0	QT	CS.25		
2FCV67.0653	67	3	845.1	C - 4	B.ACT	8	BUT	MOT	С	QT	•		

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VALVES	MIT DBL	CLASS	OTR 07:27:18	04-11-8	CATGRY	18 SIZE		ACT	N.POS	TESTS	ALTER	RELIEF
2FCV67.U86A	67	3	845.1	C.8	E.ACT	8	601	мот	С	QT		
2FCV67.067B	67	3	845.1	C.4	B.ACT	8	вит	мот		GT -		
2FCV67.065A	67	3	845.1	C.8	e.ACT	8	вит	мот	c	GT -		
0FCV67.1528	67	3	345.2	в.7	B.ACT	24	BUT	мот	-c	QT		
1FCV67.081A	67	3	845.2	н.9	B.ACT	24	BUT	MOT	0	QT	cs.25	
1FCV67.0828	67	3	845.2	н.9	6.ACT	-24	901	тот	-0	QT	CS.25	
1FCV67.123B	67	3	845.2	C.9	в. АСТ	18	PUT	MOT	-с	QT		
1FCV67.1248	67	3	845.2	0.8	E.ACT	18	BUT	мот	с —	- ст		
1FCV67.125A	67	3	845.2	C.8	B.ACT	18	907	тот		- ат		
1FCV67.126A	67	3	845.2	C.7	B.ACT	18	BUT	мот	c	ат		
1FCV67.146	67	-3	845.2	C.7	E.ACT	24	BUT	мот	-0	QT	CS.26	
1FCV67.223A	£7	3	845.2	A • 6	e.ACT	24	вит	MOT	c	QT		
1FCV67.458A	67	3	845.2	A . 9	5.ACT	24	вит	мот		- QT		
1FCV67.4788	67	3	845.2	e.7	E.ACT	24	5UT	MOT		QT	cs.26-	
2FCV67.081A	67	-3	845.2	H - 2	B.ACT	24	вит	MOT			cs.25	
2FCV67.082B	67	-3	845.2	н.2	e.act	24	BUT	MOT	0	- QT	CS.25	
2FCV67.146	67	- 5	845.2	C = 5	B.ACT	24	807	- MOT		- 9T	cs.26	
1CKV67.562A.A	67		345.3	G • 4	- AC.ACT	-6	c×	SLF		€V.LT	- cs.27 AJ	RR.12 RR.13
1.CKV67.5628.B	67	2	845.3	E.4	AC.ACT	6	cĸ	SLF	С	CV.LT	CS.27	RR.12
1CKV67.562C.A	-67	_2	845.3	F : 4	ACLACT	- 6	ск	SLF	-c	-CV-LT-	-	
1CKV67.562D.3	67	2	345.3	D = 4	AC.ACT	6	СК	SLF	С	CV.LT	CS.27	RR.12 RR.13
	- 67	-2	845.3	G . 4	AC.PAS	- 0.5	ск	SLF.			AJ	RR.12 RR.13
1CKV67.575A.A									С		AJ	RR.12

ANTARA	SYS	CLAS	LPTR 07:27:18	COORD		19 3128		ACT	N.POS	TE3T3	ALTER-	RELIEF	٠
1622/7 5754 4													-
1CKV67.575C.A			845.3	F.4	AC.PAS	0.5	CK	SLF	С	LT	AJ	RR.12	
1CKV67.5750.5	67	· 5	843.3	C • 4	AC.PAS	0.5	CK	SL F		LT	AJ	RR.12	
1 CKV 67.58 CA.A	67	2	845.3	c.3	AC.ACT	2	. CK	SLF	0	CV.LT	AJ	RR.12	
1CKV67.5808.8	- 67		545.3	9.3	AC. ACT	2 .	c ĸ	SLF	0	CV.LT	AJ	RR.13 RR.12 RR.13	
1CKV67.580C.A	67	5	845.3	E.3	AC.ACT	2	СК	SLF	0	CV.LT	AJ	RR.12	
10KV67.5800.8	c7		345.3	A.3	ACACT	-2	ск	SLF	-0	CV.LT-	AJ	RR.13 RR.12 RR.13	
1CKV67.585A.A	67	2	845.3	C _ 4	AC.PAS	0.5	СК	SLF	С	LT	AJ	RR.12	
1¢kv67.5858.8-			345.3	8.4	AC.PAS	0.5	- c K	SLF	-c	-L1	AJ	RR.12 RR.13	
1 CKV 67.585C.A	67	2	845.3	C - 4	AC.PAS	0.5	CK	SLF	С	LT	AJ	RR.12	
16KV67.5350.5	-67		845.3	-A.4	A C . P A S	-0.5	- C K	-SLF	- c	- LT	A J	RR.12 RR.13	
FCV67.083A	67	2	845.3	G - 4	A.ACT	6	BUT	MOT	0	QT.LT			
FCV67.087A	- 67		845.3	6.4	A . A CT	-6	- BUT -	MOT	-0	GT.LT	- AJ	RR.12 RR.13	
FCV67.088B	67	2	845.3	G • 4	A.ACT	6	BUT	мот	0	QT.LT	CS.27		
PCV67.091A	67	- 2	845.3	F. 4	A.ACT	-6	-SUT	<u> </u>	-0	-GT.LT	- CS. 27 AJ	RR.12 RR.13	
FCV67.095A	67	2	845.3	F.4	A.ACT	6	BUT	мот	0	QT.LT	CS.27	RR.12	
PCV87.0968	67	~	\$45.3		- A . A C T -	-5	SUT -	- MOT	- 0	-GT.LT	CS.27	RR.13 RR.12 RR.13	
FCV67.099B	67	2	845.3	E.4	A.ACT	6	BUT	мот	0	QT.LT	CS.27	RP. 12	

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LIS	T VALVES	MIT DE	L.SPC L	PTR 07:27:18	04-11-		20					· · · · · · · · · · · · · · · · · · ·			
VAL	VES	313	CLASS	DWG.NO	COORD	CATGRY	SIZE	TYPE	ACT	N.POS	TESTS	ALTER	RELIEF		
1FC	v67.1038	67	2	845.3	E . 4	A.ACT	6	вит	мот	0	QT.LT	CS.27	RR.12 RR.13		
	V67.104A	67	2	345.3	E.4	A.ÁCT	6	- SUT	MOT	0	QT.LT	CS:27 AJ	RR.12 RR.13		
1 F C	V67.107B	67	2	845.3	D.4	A . A CT	6	BUT	мот	0	QT.LT	CS.27	RR.12 RR.13		
1 F C	V67.1118	ε7	2	845.3	D.4	AACT	6	BUT	мот	0	च्या- धा	CS - 27 AJ	RR.12 RR.13		
1 F C	V67.112A	67	2	845.3	D.4	A.ACT	6	BUT	MOT	0	QT.LT	CS.27	RR.12		
	V67.130A	67	2	845.3	C - 4	A.ACT	2	PLUG	MOT	0	QT.LT	AJ	RR.12 RR.13	 .	
1 F C	v67.131B	67		845.3	C - 4	A.ACT	2	PLUG	MOT	0	QT.LT	AJ	RR.12		
150	V67.133A	67	- 2	845.3	9.4	A.ACT	- 2	PLUG	M0.T	0	QT.LT	AJ	RR.12 RR.13		
1 FC	/67.1349	67	2	845.3	C - 4	A.ACT	2	PLUG	том	0	QT.LT	AJ	RR.12 RR.13		
	/67.1388	-67	-2	845.3	3.4	-A.ACT	- 2	PLUG	MOT	0	- QT.LT	— A J	RR.12 RR.13		
1 F C V	167.139A	67	2	845.3	B • 4	A.ACT	2	PLUG	мот	0	GT.LT	AJ	RR.12 RR.13		
1 P C V	/67.1418	67	2 -	845.3	A . 4	A.ACT	2	PLUG	MOT .	0	QT.LT	- A J	RR.12 RR.13		
1 F C V	67.142A	67	2	845.3	A . 4	A.ACT	2	PLUG	мот	0	QT.LT	AJ	ER.12 RR.13		
1 FCV	/67.295A	67	2	845.3	C.4	A.ACT	- 2	PLUG	MOT	-0	- 07.LT -	AJ	RR.12 RR.13		
1 FCV	167.296A	67	2	845.3	C - 4	A.ACT	2	PLUG	мот	0	QT.LT	AJ	RR.12 RR.13		
1FCV	167.2972	67	2	345.3	5.4	A.ACT	2	PLUG	MOT		37.LT	AJ	RP.12 RR.13		
1 FCV	/67.2988	67	2	945.3	A.4	A.ACT	2	PLUG	мот	0	QT.LT	AJ	RR.12 RR.13		
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ALVES		CLASS	TR 07:27:18	04-11-1 	86 PAGE CATGRY	21 317E	TYPE	ACT	N.FOS	TESTS	ALTER	RELIEF	·		<u> </u>
FCV67.162	67	3	345.4	B.7	B.ACT	2 ·	G A	DIA	0	QT					
FCV67.164	67	3	845.4	B.9	B.ACT	2	G A	DIA	С	QT					
FCV67.176	67	3	845.4	D.7	B.ACT	1.5	G A	DIA	С	QT					
FCV67.182	67	3	345.4	D.9	E.ACT	1.5	. G A	DIA	С	QT					
FCV67.184	67	3 ·	345.4	D • 8	- B.ACT	1.5	G A	DIA	С	QT					
FCV67.186	67	3	845.4	D.9	B.ACT	1.5	G A	DIA	С	QT					
FCV67.213	67	3	845.4	B.7	B.ACT	1.5	G A	DIA	0	QT					
FCV67.215	67	3	345.4	E.9	E.ACT	1.5	G A	DIA	С	QT					•
FCV67.342	67	3	845.4	G.7	B.ACT	2	G A	DIA	0	QT					
FCV67.344	67	3	845.4	G . 8	B.ACT	2	GA	DIA	С	QT					
FCV67.346	67	3	845.4	E.8	B.ACT	1.5	G A	DIA	0	QT					
FCV67.348	67	3	845.4	E.9	B.ACT	1.5	G A	DIA	С	QT				******	
FCV67.350	67	3	845.4	F . 8	B.ACT	1.5	G A	DIA	0	QT					
FCV67.352	67	3	845.4	F.9	a.act	1.5	G A	DIA	С	QT	·				
FCV67.354	67	3	545.4	F.8	B.ACT	1.5	G A	DIA	0	QT					
FCV67.356	67	3	845.4	F.9	E.ACT	1.5	G A	DIA	С	QT					•
FCV67.217	67	3	845.4	8.2	B.ACT	2	G A	DIA	С	QT					
FCV67.219	67	3	845.4	C . 4	9.ACT	2	G A	DIA	0	QT	· · · · · · · · · · · · · · · · · · ·				
FCV67.336	67	3	845.4	A . 2	B.ACT	1	G A	DIA	С	QT					
FCV67.338	67	3	845.4	A - 4	B.ACT	1	G A	DIA	С	QT					
FCV67.205A	67	3	845.5	G • 2	B.ACT	4	BUT	MOT	0	QT					
FCV67.208B	67	3	845.5	6.2	E.ACT	4	вит	MOT	0	QT					
SFV67.671	67	3	845.5	E • 6	C.ACT	• 75	REL	SLF	С	ST					
SFV67.672	67	3	845.5	G . 7	C.ACT	.75	REL	SLF	С	вт			- ,		
FCV68.307A	63	2	625.8	6.2	A.ACT	.375	G A	DIA	С	QT.LT	AJ	RR.12			

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LIST VALVES L	SA2	CLASS	DWG.NO	04-11-	B6 PAGE CATGRY	SIZE	TYPE	ACT	N.POS	TESTS	ALTER	RELIEF	
1FCV68.308B	68	2	625.8	F.1	A.ACT	.375	G A	DIA	0	QT.LT	AJ	RR.12	 •
CKV68.559	68		813.1	E • 7	B.ACT	4	cĸ	SLF	 	- cv	· · · · · · · · · · · · · · · · · · ·	- RR.32	
FCV66.3328	68	1	813.1	8.2	B.ACT	3	G A	мот	0	QT			
FCV68.333A	63	1	313.1	E.1	S.ACT		G A	MOT		QT-		· · · · · · · · · · · · · · · · · · ·	
FSV88.394	ćS	2	813.1	F.7	B.ACT	1	PLUG	SOL		- 97	CS.36	RR.21	
FSV68.395	68	2	813.1	F.7.	B.ACT	1	PLUG	SOL	с	QT	CS.36	RR.21	
FSV68.396	68	2	813.1	F.5	B.ACT	1	PLUG	SCL		QT	<u> </u>	RR.21	
FSV68.397	6.8	-2	813.1	ř.ó	E.ACT	1	PLUG	SOL -	-с	QT	<u> </u>	RR. 21	
PCV68.334	63		313.1	8.1	S.ACT	3	GL	SOL	с	QT	CS.36	RR.21	
PCV68.340A.A	ć8	-1	813.1	8.1	B.ACT	3 .	- GL	-sot-	-с	- 2T	<u>cs.36</u>	RR-21	
RFV08.5035	c 5	-1	813.1	A • 3	C.ACT	- 6	REL	SLF	-с	87			
RFV68.5648	- 8	-1	813.1	A . 2	C . ACT	6	- REL	SLF	С	87	····		
RFV68.5658	68	1	813.1	A . 1	C.ACT	6	REL	- SLF-		- 3 T			
PCV68.305A	63	2	330.6	6.6	A.ACT	0.75	GL	DIA	•	QT.LT	AJ	RR.12 RR.13	 <u></u>
ICKV70.504B	70	3	859.1	E . 8	C.ACT	16	CK	SLF	С	cv			
CKV70.753	70	3	859.1	F.10	C.ACT	8	СК	SLF	0	CV		<u> </u>	
FCV70.194B	70	3	259.1	8.4	B.ACT	20	BUT	MOT	0	QT			
FCV70.2068	70	3	859.1	G.10	E.ACT	10	BUT	мот	0	QT			
FCV70-208A	70	3	859.1	B.1	B.ACT	10	BUT	мот	0	QT		-	
CKV70.504A.A	70	3	859.1	C . 8	C.ACT	16	CK	SLF	С	cv		RR - 27	
CKV70.5048.A	70	3	859.1	D.8	C.ACT	16	εĸ	SLF	С	cv		RR.27	
FCV70.066	70	3	359.1	E.3	B.ACT	2	ANG	DIA	0	QT			
FCV70.2079	70	3	859.1	A.2	B.ACT	10	BUT	мот	0	QT			
RFV70.538	70	3	859.1	E.3	C.ACT	3	REL	SLF	С	ВТ			

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VALVES	SYS	CLASS	PTR 07:27:18	04-11-	-86 PAGE Catery-	23 512E	TYPE	ACT	N.POS	TESTS			
1CKV70.679A	70	2	259.2	Н.4	ACTACT	3 .	ск	SLF	0	CV.LT	CS.28	RELIEF RR.12	
1CKV70.687A	70	2	859.2	G . 9	AC.PAS	0.5	CK	SLF		LT	LA LA	RR.13	
1CKV70.692A	70	2	859.2	6.3	AC.ACT	6	c K	SLF	.0	CV LT	CS - 29	RR.12 RR.13	
1 CKV70.698A	70	2	359.2	E.9	AC.PAS	0.5	СК	SLF	С	LT	AJ	RR.12	
1FCV70.085B	70	- 2-	859.2	D.10	A.ACT	6	BUT	DIA	0	QT.LT	AJ	RR.12 RR.13	
1FCV70.0878	70	2	859.2	G.9	A.ACT	3	G A	MOT	0	GT.LT	CS.28	RR.12	
1FCV70.0898	70	 	859.2	Ε.9	A . A CT	6	вит	MOT.	0	GT.LT	CS.29 AJ	RR.12 RR.13	-
1FCV70.090A	70	2	859.2	E.10	A.ACT	3	G A	мот	0	QT.LT	CS.28	RR.12	
1FCV70.092A	73	2	359.2	0.10	A.ACT	- 6	- 5 UT	MOT	0	QT.LT	C3.29 AJ	RR.12 RR.13	
1FCV70.134B	70	2	859.2	н.3	A.ACT	3	G A	мот	0	QT.LT	CS.28	RR.12	
1FCV70.1408	70	-2	359.2	6.3	A.ACT	6	вит	MOT	0	QT.LT	CS.29 AJ	RR.12 RR.13	
FCV70.143A	70	2	859.2	E.3	A.ACT	6	BUT	мот	0	QT.LT	ĄJ	RR.12	
RFV70.703	70	2	359.2	0.5	AC.ACT	- 3	REL	SLF		BT.LT	AJ	RR.12 RR.13	
FCV70.1538	70	3	859.4	F.3	B.ACT	18	BUT	мот	С	QT			
FCV70.156A	70	3	859.4	F.4	B.ACT	18	BUT	MOT	С	QT			
CKV72.506A	72	2	812.1	8.11	C.ACT	12	СК	SLF	С	c v			
CKV72.5078	72	2	812.1	0.11	C.ACT	12	СК	SLF	С	cv			
CKV72.524A	72	2	512.1	0.7	C.ACT	10	CK	SLF	С	CV			***************************************
CKV72.525B	72	2	812.1	8.7	C.ACT	10	CK	SLF	C .	CV.	•		

LIST VALVES &C				COORD	B6 PAGE CATGRY	SIZE	TYPE	ACT	N.POS	TESTS	ALTER	RELIEF	
1CKV72.548A	72	- 2	812.1	0.3	C.ACT	10 .	- ск	SLF	С	cv	PS.RR	RF. 22	
1CKV72.549B	72	2	512.1	8.3	C.ACT	10	cĸ	SLF	С	cv	PS.RR	RR • 22	
TCKV72.562A	72	2	812.1	F.3	CLACT	-5	ск	SLF	-c	cv	PS.RR	RR.22	
TCKV72.563B	72	2	812.1	E • 3	C.ACT		- cĸ	SLF		cv	PS.RR	RP.22	
1FCV72.002B	72,	2	812.1	B.4	A.ACT	10 .	G A	мот	-c	GT.LT	AJ	RR.12 RR.13	
1FCV72.0136	72	2	812.1	B.6	B.ACT	3	G A	MOT	С	ÇТ			
1FCV72.0218	72	2	312.1	9.10	B.ACT	12	G A	MOT	0	QT		<u></u>	
1FCV72.022A	72	2	612.1	c.10	P.ACT	12	G A	мот	0	QT			
1FCV72.034A	72	2	812.1	C.6	B.ACT	3	G A	MOT	С	QT			
1FCV72.039A	72	2	812.1	D.4	A. A C T	10	G A	MOT		QT.LT	AJ	RR • 12	
1FCV72.040A	72		812.1	F.5	BART	8 -	G A	- MOT		QT	cs.39		
1FCV72.0413	72		812.1	E.5	B.ACT		G A	MOT	- c		<u>cs.30</u>		
1FCV72.044A	72	2	812.1	G . 4	- E.ACT	12	G A	MOT			cs.24		·.
18cv72.0458	72		812.1	H • 4	9.ACT	12	G A	MOT		- QT	cs.24		
1RFV72.508	. 72 —	2	812.1	., 9	C.ACT	3.75	REL	SLF	-c	- 76			
1RFV72.509	72		814.1	A . 9	C.ACT	0.75	REL	- SLF		- 81	····		
10KV74.514A	74		810.1	£.7	C.ACT		ск	SLF			 CS . 31 PS	RR.27	,,,
1CKV74_515B	74	2	810 .1	c.7	C.ACT	8	СК	SLF	c ·	c v	CS.31	RR.27	
1FCV74=001A	74		810.1	6.3	A.ACT	14	G A	MOT		QT.LT	- cs.32		
1FCV74.8028	74	1	910.1	G.3	A.ACT	14	<u>—6 А</u>	мот	— с	QT.LT	- cs.32-	RR = 2-3	
1FCV74.003A	74	2 -	81 C. 1	- 5 - 9	B.ACT	14	G A	MOT	-0	9.7		·	
1FCV74.808A	-74-		. 31 C . 1	- F.3	A.ACT	- 10	G A	MOT		@T.LT	- cs.32-		
1FCV74.0098	 74	1	\$10.1	-6.3	A.ACT	-10	GA-	- MOT		- QT.LT-	- cs.32	RR.23	
1FCV74.012A	74-		810.1	- F.5	B.ACT	2	G A	мот		- QT	•		

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ာ ့ ့	LIST VALVES	MIT DB	L.SPC LP1	TR 07:27:18	04-11-8	CATGRY	25 SIZE	TYPE	ACT	N.POS	TESTS	ALTER	RELIEF			
	1 FCV74.016	74	2	810.1	E.4	B.ACT	8 .	BUT	DIA	0	QT					`
;)	1FCV74.0218	74	2	810.1	C.9	B.ACT	14	G A	MOT	0	QT					
5	1FCV74.G248	74	2	810.1	8.5	'E.ACT	2	G A	MOT	0	QT	_				
4	1FCV74.028	.74	2	31C.1	C.4	B.ACT	8	BUT	DIA	0	QT					
C	1FCV74.033A	74	2	810.1	E-4	B.ACT	8	G A	МОТ	0	QT	<u>cs.35</u>				
છ	1FCV74.035B	74	2	810.1	C - 4	B.ACT	8	G A	мот	0	QT	<u>cs.35</u>				
.)	1RFV74.505S	74	2	81C.1	G • 3	C.ACT	3	REL	SLF	С	5 T					
	1FCV77.009B	77	2	830.1	D.1	A.ACT	3	DIA	DIA	0	QT.LT	AJ	RR.12 			
o	- 1 F C V 77 - 01 0 A	77	2	330.1	E • 1	A:ACT	3	DIA	DIA	0	QT.LT	AJ	PR.12 FR.13			
)	1FCV77.016B	77	2	830.1	8.5	A.ACT	0.75	DIA	DIA	0	QT.LT	AJ	RR.12		7145 VEST 18	
~	1FCV77.017A	-77 -	2	830.1	3.6	-A.ACT	0.75	DIA	DIA	¢	- QT.LT	AJ	RR.12 RR.13			
0	1FCV77.018B	77	2	830.1	B.5	A.ACT	1	DIA	DIA	0	QT.LT	LA	RR.12			
	1FCV77.019A	77	2	830.1	3.6	A . A C T	-1	DIA	DIA	0	OT.LT	AJ	RR.12 RR.13	-		
O	1 FCV77.020A	77	2	830.1	C.6	A.ACT	1	DIA	DIA	С	QT.LT	AJ	RR.12			
	1CKV77.349	77	2	830.6	G • 6	AC.ACT-	0.75	ск	SLF	e	CV.LT	CS.33 AJ	RR.13 RR.12			
$\mathbb{R}^{\mathbf{V}_{p^{n}}}$	1CKV77.868	77	2	830.6	8.6	AC.ACT	1	CK	SLF	С	CV.LT	CS.33	RR.12	-		
	1FCV77.1278	77	2 .	851.1	F.7	A.ACT	-2	DIA	DIA	0	- QT.LT	AJ	RR.12 RR.13			
0	1FCV77.128A	77	2	851.1	F . 7	A.ACT	2	DIA	DIA	0	QT.LT	AJ	RR.12			
ပ ေ	118778.557	73	2	855.1	6.8	A.PAS	4	DIA	MAN	- C	LT	AJ	RR.12 RR.13			
		 														
. C								····		·						

<i>i .</i>	•					J.							
)	LIST VALVES DE				04-11-		26				· · · · · · · · · · · · · · · · · · ·		
•)	VALVES	- SYS	CLASS	DWG.NO	COORD	CATGRY	SIZE	TYPE	ACT	N.POS	TESTS	ALTER	RELIEF
	118078.558	78	2	855.1	G.8	A.PAS	4	DIA	MAN	С	LT	ÂĴ	RR.12 RR.13
) i	11SV78.560	78	2	855.1	G • 3	A.PAS	6	DIA	MAN	С	LT	AJ	RR.12
n .	118078.561	78	2	855.1	G.8	A.PAS	5	DIA	MAN	· · ·	<u>LT</u>	AJ	RR.12 RR.13
9	1CKV81.502	81	2	819.1	F • 4	AC.ACT	3	СК	SLF	С	CV.LT	CS.34	RR.12
.	1FCV81.012A	81	2	819.1	F . 4	A.ACT	3	DIA	DIA	0	QT.LT	AJ	RR.12 RR.13
0	1CKV82.502A.A	82	3	839.1	E.2	C.ACT	1.5	CK	SLF	С	c v		
ີ	1CKV82.502A.B	82	3	839.1	E • 2	C.ACT	1.5	CK	SLF	С	CV		
4.	1CKVS2.505A.A	82	3	539.1	3.2	C.ACT	1.5	CK	SLF	С	C V		
ာ	1CKV82.505A.B	82	3	839.1	B.2	C.ACT	1.5	CK	SLF	С	cv		
•	1CKV82:536B.A	82	3 .	839.1	P.11	C.ACT	1.5	СК	SLF	С	cv		
	1CKV82.5368.8	82	3	839.1	8.11	C.ACT	1.5	CK	SLF	С	CV		
0	1CKV82.539B.A	82	3	839.1	E.11	C.ACT	1.5	CK	SLF	С	CV		
0	1CKV82.5398.B	82	3	839.1	E.11	C.ACT	1.5	CK	SLF	С	cv		
	1FCV82.16CA.A	٤2	3	839.1	E.4	B.ACT	1.5	DIA	PNU	C	QT		RR.31
O	1FCV82.161B.A	82	3	839.1	E.9	B.ACT	1.5	DIA	PNU	С	QT		RR.31
0	1FCV82.170A.A	82	3	839.1	C - 4	E.ACT	1.5	DIA	PNU	С	QT		RR - 31
	1FCV82.171B.A	82	3	839.1	C.9	B.ACT	1.5	DIA	PNU	c ·	QТ		RR.31
0	1FCV82.190A.B	82	3	839.1	E.4	B.ACT	1.5	DIA	PNU	С	QT		RR.31
0	1FCV82.1918.B	82	3	839.1	E.9	B.ACT	1.5	DIA	PNU	С	QT		RR.31
· -	1FCV82.200A.B	8.2	3	839.1	C - 4	B.ACT	1.5	DIA	PNU	С	QT		RR-31
(; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ;	1FCV82.2018.B	82	3	839.1	C.9	B.ACT	1.5	DIA	PNU	С	QT		RR.31
U.	2CKV82.502A.A	82	3	839.1	E.2	C.ACT	1.5	ск	SLF	С	cv		
-	2CKV82.502A.B	82	3	839.1	E.2	C.ACT	1.5	СК	SLF	<u> </u>	cv		
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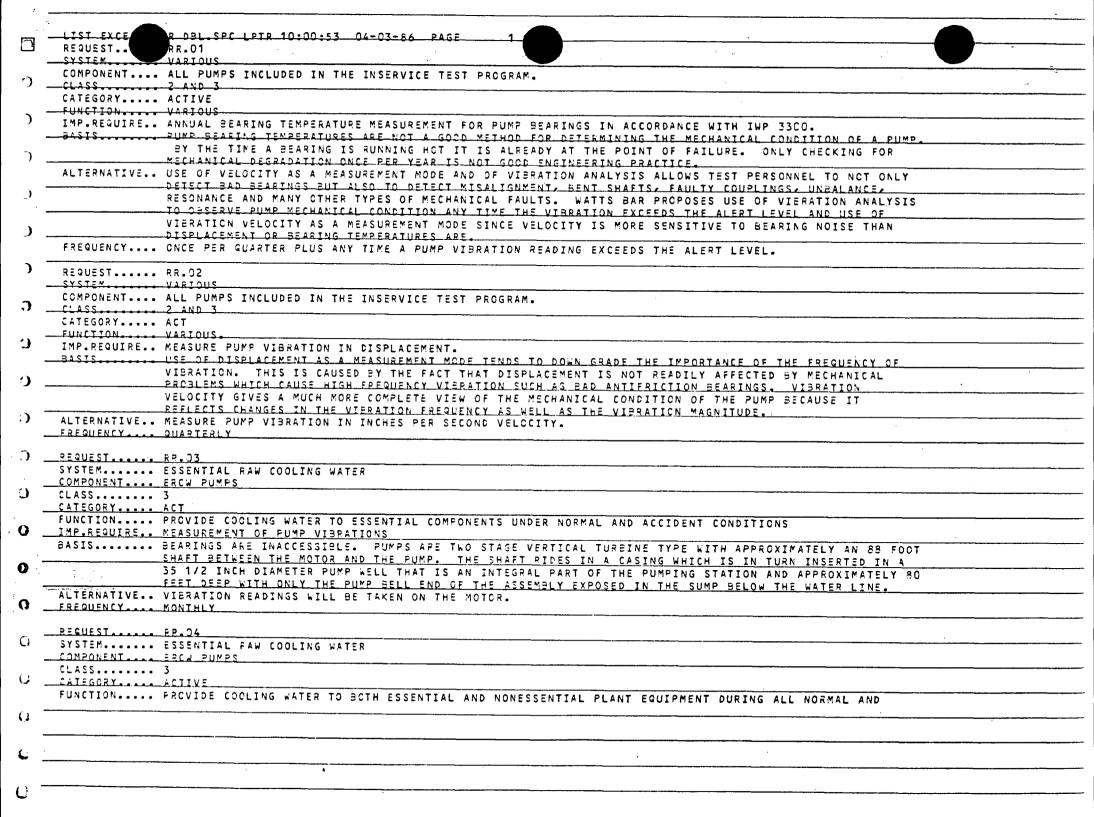
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VALVES		CLASS	TR 07:27:18		B6 PAGE	27 312E	TYPE	ACT-	N.POS	TESTS ALTER	RELIEF
- 2CKV82.505A.A	82	3	839.1	5.2	CART	1.5	-ск	SLF	-с	cv	
2CKV82.505A.E	82	3	839.1	8.2	C.ACT	1.5	- cĸ -	SLF	-с	ev	
2CKV82.536E.#	82	-3	239.1	S.11	C.ACT	1.5	ек	SLF-	-с	ev	
2CKV82.5363.E	82	3	£39.1	8.11	C.ACT	1.5	ск	SLF	С		
2CKV82.5392.A	82	3	839.1	- E - 11	C.ACT	1.5	. cĸ	SLF	с	CV	
- 2CKV82.5398.5	82	3	337.1	E . 11	CRACT	1.5	ск	SLF	е	ev	· · · · · · · · · · · · · · · · · · ·
2FCV82.220A.A	82	3	839.1	- E . 4	B.ACT	1.5	DIA	PNU	-с	QT	RR.31
2fCV82.221B.A	- 82	3	839.1	E . 9	B.ACT	1.5	DIA	PNU	-с	QT	RR - 31
2FCV82.230A.A	62	3	839.1	C = 4	B.ACT	1.5	DIA	PNU	-с	QT	PR.31
2fCV82.2319.A	- 82	3	839.1	- C • 9	B.ACT	1.5	DIA	PNU	-с	QT	RR.31
2fCV82.250A.E	82	3	839.1	E - 4	B.ACT	1.5	DIA	PNU	-c	QT	RR.31
2FCV82.2513.8	82		839.1	 	E.ACT	1.5	DIA	PNU	с	QT	RR.31
2FCV82.260A.B	82		339.1	C - 4	e.Act	1.5	DIA	PNU	-с	QT	RR.31
2FCV82.2618.B	- 82	-3	839.1	.,9	B.ACT	1.5	DIA	PNU	-с	GT	RR.31
- 00KV82.561	- 82 -	3	839.2	- E - 2	C.ACT	-1.5	 c K	SLF	- €		
00KV82.562	82	 3	839.2	8.11	- C . A C T	1.5	- c k	SLF	е	€ V	·
0CKV82.567	82 —	3	839.2	-8 . 2 -	C.ACT	1.5	— ск	SLF		c v	
- 0ckv82.570	62-	3	639.2	E.11	C.ACT	1.5	- ск	SLF	-с	£ V	
OFCV82.300	82-	3	339.2	E . 4	-S.ACT	1.5	DIA	PNU	-с	— Q Т	RR.31
OFCV82.301	82	-3	639.2	- E . 9	B.ACT	1.5	- DIA	PNU	- C	QT	
OFCV82.310	ε2	-3 -	239.2	C - 4	B. ACT	1.5	DIA	PNU	-е	Q.T	RR.31
OF CV6 2.311	82	3	839.2	C . 9	S.ACT	1.5	DIA	PNU	.	QT	RR.31
11\$V84.530\$	£4		±09.7	- f.3	A.PAS	1	G A	MAN	.	LT AJ	RR.13
1CKV87.558\$	87	1	811.2	E.1	AC.ACT	8	CK	SLF	С	CV.LT	RR.20
1CKV87.5598	٤٦	1	811.2	-F.2	AC.ACT	-8	-cĸ	SLF	с		

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)	LIST VALV	MIT D	91 S2C 15	PTR 07:27:18	0/-11-	94 0465							
.	VALVES	SYS		DWG.NO.	04-11- COORD	86 PAGE CATERY	SIZE	TYPE	ACT	N.POS	TESTS	ALTER	RELIEF
<u>)</u>	1CKV87.560\$	87	1	811.2	F.2	AC.ACT	8	ск	SLF	c	CV.LT		RR.23 RR.20 RR.23
၁	1CKV87.561S	87	1	811.2	G.2	AC.ACT	. 8	СK	SLF	С	CV.LT		RR.20
c	1CKV87.5628	87		811.2	E.4	AC.ACT	12	·cĸ	SLF	c	CV.LT		RR.20 RR.23
')	1CKV87.563\$	87	1	811.2	F.3	AC.ACT	12	ск	SLF	С	CV.LT		RR.20
-)	1FCV87.007A	£7-	1	811.2	E • 3	A.ACT	2	GA .	DIA	- c	QT.LT	AJ	RR.12 RR.13
จ	1FCV87.008A	87	1	811.2	E.3	A.ACT	2	GL	DIA	С	QT.LT	AJ	RR.12
3	1FCV87.009B	87	2	811.2	E . 4	A.ACT	2	G A	DIA	с	QT.LT	AJ	RR.12 RR.13
)	1fCV87.0106	87	2	811.2	F . 5	B.ACT	0.75	G A	DIA	С	QT		,
)	1 FC V87.011B	87	2	811.2	F.5	B.ACT	2	G A	DIA	С	Q T		
.•	1FCV87.021D	87	2	811.2	E . 6	E.ACT	12	G A	CYL	0	QT		RR. 24
)	1FCV87.022E	87	2	811.2	E.7	B.ACT	12	G A	CYL	0	GT -		RR.24
)	1FCV87.023F	87	2	811.2	F . 6	B.ACT	12	G A	CYL	0	QT		RR.24
	1 F C V 87 . 024 G	87	2	811.2	F.7	B.ACT	12	G A	CYL	0	QT		RR.24
•	1RFV87.556S	87	2	811.2	C.10	C.ACT	1.5	REL	SLF	С	ет		
<u>,</u>	1RFV87.557S	87	2	311.2	0.8	C.ACT	1.5	REL	SLF	С	вт		
· .	RUPTURE DISK	87	2	811.2	B.7	D.ACT	12	RD	SLF	С	RD	· · · · · · · · · · · · · · · · · · ·	
)	1FCV90.107A	90	2	610.90.3	A.9	A.ACT	1.5	G A	DIA	0	QT.LT	AJ	RR.12
; -	1FCVY0.1088	90	2	610.90.3	. 9	A.ACT	1.5	G A	DIA	0	QT.LT	AJ	RR.12 RR.13
	1FCV90.109B	90	2	610.90.3	C.9	A.ACT	1.5	G A	DIA	0	QT.LT	AJ	RR.12 RR.13
: -	1FCV90.1108	90	2	610.93.3	c.9	A.ACT	1.5	G A	DIA	-0	QT.LT	AJ	FR-12
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	VALVES			R 07:27:18			29 S12E	TYPE	ACT-	N.POS	TESTS	ALTER					3
9			· · · · · · · · · · · · · · · · · · ·		<u>.</u>				·			· · · · · · · · · · · · · · · · · · ·	RR.13				
ð	1FCV90.111A	90	2	ć10.90.3	C.9	ALACT	1.5	GA ···	DIA	0	01.L7	- AJ	RR.12 RR.13	·			
Э	1FCV90.113A	90	2	610.90.3	A.6	A.ACT	1.5	G A	DIA	0	QT.LT	AJ	RR.12 				
Ċ	1FCV90.1148	- 90	2	610.90.3	- c . 5	A . A C T	1.5	G A	DIA	0	QT.LT	- AJ	RR.12 RR.13				
•	1FCV90.115B	90	2	610.90.3	C • 5	A_ACT	1.5	G A	DIA	0	QT.LT	LA	RR.12 RR.13				
•	1FCV90.1165	90	- 2	610.90.3	C . 5	A.ACT	-1.5	G A	DIA	0	QT.LT-	AJ	RR.12 RR.13				
o .	1FCV90.117A	90	2	610.90.3	D.6	A.ACT	1.5	G A	DIA	0	QT.LT	AJ	RR.12 RR.13		· ·		
c	601 RECORDS LIS	STED.								<u></u>	· · · <u>·</u> · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·					
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APPENDIX-C RELIEF REQUESTS SUMMARY



DRI SPC 1 PTR : 10+00+53 - 04-03-86 - PAGE ITCT EVER CCIDENT CONDITIONS. THE REQUIRE - MEASURE PUMP SUCTION PRESSURE BOTH BEFORE AND AFTER PUMP START DURING THE INSERVICE TEST. BASIS..... THESE ARE VERTICAL TURBINE PUMPS WHICH SIT IN AN OPEN PUMP PIT. THEY ARE SEPARATED FROM THE RIVER ONLY BY A TRAVELING SCREEN. ALTERNATIVE. DETERMINE RIVER LEVEL BEFORE THE TEST REGINS TO ENSURE ADEQUATE SUBMERGENCE AND MEASURE THE DIFFERENTIAL PRESSURE ACROSS THE TRAVELING SCREENS DUPING PUMP CPERATION TO ENSURE THAT THE SCREENS ARE NOT BLOCKED TO A DEGREE WHICH WOULD DEPRIVE THE PUMPS OF ADEQUATE SUBMERGENCE. EDECHERCY CHARTERLY REQUEST..... RP. 05 SYSTEM..... ESSENTIAL RAW COOLING WATER AND COMPONENT COOLING SYSTEMS COMPONENT. ... ERCW AND CCS PUMPS CATEGORY.... ACT FUNCTION..... PROVIDE COCLING WATER TO ESSENTIAL PLANT EQUIPMENT DURING NORMAL AND ACCIDENT CONDITIONS. IMPLREGULTER. PROVIDE A FIXED POINT OF OPERATION FOR FLOW AND DIFFERENTIAL PRESSURE MEASUREMENT. BASIS..... THESE PUMPS ARE NOT EQUIPPED WITH RECIRCULATION TEST LINES. THE NATURE OF THE SYSTEM THEY FEED MAKES IT IMPOSSIBLE TO SPECIFY A PARTICULAR FLOW PATH THAT CAN ALWAYS BE REPEATED. VARIOUS COMPONENTS WHICH THEY FEED WILL SOMETIMES REQUIRE COOLING WATER AND SOMETIMES NOT. ALTERNATIVE.. INITIALLY ESTABLISH AN INSITU PUMP CURVE WHICH ESTABLISHES THE RELATIONSHIP BETWEEN FLOW AND DIFFERENTIAL PRESSURE IN A BAND COVERING THE SYSTEM OPERATING CONDITIONS. SUESEQUENT INSERVICE **3** TESTS WOULD THEN COMPARE TEST DATA TO THIS CURVE. FREQUENCY... QUARTERLY 1) REQUEST.... RR.06 SYSTEM.... COMPONENT COOLING WATER SYSTEM COMPONENT.... COMPONENT COOLING PEMPS FOR TRAIN A ONLY • __CLAS5.....3 CATEGORY.... ACT <u>FUNCTION..... PROVIDE COCLING WATER TO ESSENTIAL PLANT EQUIPMENT DURING NORMAL AND ACCIDENT CONDITIONS.</u> IMP_REQUIRE__ MEASURE STATIC PUMP SUCTION PRESSURE PRIOR TO STARTING PUMP BASIS...... TO OBTAIN TRUE STATIC PRESSURE WOULD REQUIRE STOPPING BOTH TRAIN A PUMPS SINCE THEY SHARE A COMMON SUCTION HEADER. THIS IS IMPRACTICAL FROM AN OPERATIONAL STANDPOINT DUE TO THE SUBSEQUENT LOSS OF COCLING TO EQUIPMENT SERVED BY THESE PUMPS. NORMAL OPERATION INCLUDING PLANT SHUTDOWN REQUIRES AT LEAST ONE TRAIN A PUMP IN SERVICE. ALTERNATIVE.. MEASURE SUCTION PRESSURE WITH ONLY ONE PUMP RUNNING, NOT THE PUMP TO BE TESTED, START THE PUMP TO BE TESTED AND MEASURE SUCTION PRESSURE, STCP THE PUMP NOT BEING TESTED AND CONTINUE TESTING BY FIPST MEASURING THE SUCTION PRESSURE FOR THE PUMP UNDER TEST. THIS WILL PROVIDE REFERENCE TO BOTH NORMAL AND ACCIDENT CONDITIONS. FREQUENCY.... QUARTERLY REQUEST.... RR.07 SYSTEM.... COMPONENT COOLING SYSTEM COMPONENT.... COMPONENT COOLING PUMPS FOR TRAIN B ONLY C CATEGORY ACT FUNCTION.... PROVIDE COCLING WATER TO ESSENTIAL PLANT EQUIPMENT DURING NORMAL AND ACCIDENT CONDITIONS IMP_REQUIRE.. MEASURE STATIC PUMP SUCTION PRESSURE PFIOR TO STARTING PUMP. BASIS..... THIS IS THE ONLY PUMP ON B TRAIN AND CONSEQUENTLY IS IN NEAR CONTINUOUS SERVICE. STOPPING THE PUMP HOULD REQUIRE REMOVING AN ENTIRE TRAIN FROM SERVICE AND FAILURE OF THE PUMP TO RESTART WOULD LEAVE SOTH UNITS WITH ONLY ONE TRAIN OF COMPONENT COOLING WATER. ALTERNATIVE. MEASURE STATIC SUCTION PRESSURE ONLY WHEN THE PUMP IS NOT ALREADY IN SERVICE AND IS ONLY BEING STARTED FOR TESTING PURPOSES.

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ES	LIST EXCE. DBL-SPC LPTR 10:C0:53 04-C3-86 PAGE 3	
	FREQUENCY. QUARTERLY	
	REQUEST RR.D8	
1	SYSTEM BORIC ACID	
	COMPONENT BORIC ACID TRANSFER (BAT) PUMPS	
,	- CLASS - V-V-V- 3	
)	CATEGORY ACT	
	FUNCTION SUPPLIES BORIC ACID FOR EMERGENCY ECRATION.	
7	IMP.REQUIRE MEASURE PUMP FLOW RATE	
	BASIS THE BORON INJECTION TANK (BIT) IS NO LONGER REQUIRED TO BE MAINTAINED AT 20,000 PPM BORON	
	CONCENTRATION. IN ORDER TO INCORPORATE THIS CHANGE AT WATTS BAR, THE BIT ISOLATION VALVES ARE TO BE MAINTAINED IN A CLOSED AND DEENERGIZED CONDITION WHICH ISOLATES THE ONLY FLOW ELEMENT AVAILABLE	
3	TO MEASURE BAT PUMP FLOW. THERE IS NOT SUFFICIENT TIME TO PROCURE AND INSTALL A FLOW ELEMENT PRIOR	
	TO LICENSING.	
.)	ALTERNATIVE TEST THE BAT PUMPS ON A FIXED RESISTANCE FLOW LOOP MEASURING THE DEVELOPED DIFFERENTIAL PRESSURE	
,	- ONLY -	
	FREQUENCY QUARTERLY	
.)	REQUEST RR.09	
	SYSTEM DIESEL FUEL CIL	
~~	COMPONENT FUEL OIL TRANSFER PUMPS	-
Э	-CLASS3	
	CATEGORY ACTIVE	
3	- FUNCTION TRANSFER FUEL OIL FEOM THE SEVEN DAY STORAGE TANK TO THE DIESEL ENGINE SKID MOUNTED DAY TANK Imp.require Measure suction pressure both before and after pump start.	
	BASIS NO PRESSURE INSTRUMENTATION EXISTS SETWEEN THE PUMP AND THE TANK FROM WHICH IT TAKES SUCTION	
	ALTERNATIVE DETERMINE PRIOR TO PUMP START THAT THE SEVEN DAY STORAGE TANK HAS A LEVEL WHICH IS SUBSTITED TO	
•)	PROVIDE ADEQUATE SUCTION TO THE FUEL OIL TRANSFER PUMPS.	
	FREQUENCY QUARTERLY	
:O:	REQUEST RR.10	
	SYSTEM DIESEL FUEL OIL	
~	COMPONENT FUEL OIL TRANSFER PUMPS	
o .	CLASS	
	CATEGORY ACT	
o '	FUNCTION TRANSFER FUEL OIL FROM THE SEVEN DAY STORAGE TANK TO THE DIESEL ENGINE SKID MOUNTED DAY TANK. IMP.REQUIRE MEASURE DIFFERENTIAL PRESSURE AND FLOW.	
	BASIS NO INSTRUMENTATION EXISTS FOR EITHER PRESSURE OR FLOW. THE TANK TO WHICH THE PUMPS DELIVER FUEL	
	OIL IS NOT INSTRUMENTED TO ALLOW MEASUREMENT OF LEVEL CHANGE WITH SUFFICIENT ACCURACY TO OBTAIN	
0.	FLOW WITHIN 2%,	
	ALTERNATIVE. DETERMINE FLOW BY MEASUREMENT OF LEVEL CHANGE TO BE AT LEAST 10 GALLONS PER MINUTE. THIS IS	
C ·	APPROXIMATELY TWICE THE RATE AT WHICH THE DIESELS CONSUME FUEL AND IS SUFFICIENT TO DEMONSTRATE OPERABILITY OF THE PUMP. THE ABILITY OF THE PUMP TO DELIVER FUEL OIL TO THE DAY TANK DEMONSTRATES	
-	SUFFICIENT DIFFERENTIAL PRESSURE TO FULFILL ITS FUNCTION. THE WATTS BAR DIESEL FUEL OIL TRANSFER	
	PURPS ARE SUREW TYPE POSITIVE DISPLACEMENT PHIMPS. MEASURING DIFFERENTIAL PROCESURE ON A DOCTTON	
О.	TRISPLACEMENT PUMP DOES NOT PROVIDE MEANINGFUL INFORMATION AS INTENDED BY THE 1500.	
	FREQUENCY GUARTERLY	
•	REQUEST RR.11	
	SYSTEMA DIESEL FUEL OIL	
	COMPONENT FUEL DIL TPANSFER PUMPS	
·	CLASS.	
	CATEGORY ACTIVE	
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LIST FXCER 1 091 SPC 19TR 10-00-53 04-03-86 PAGE TRANSFER FUEL OIL FROM THE SEVEN DAY STORAGE TAN FUNCTION. THE DIESEL ENGINE SKID MOUNTED DAY TANK. THE REQUIRE. OR SERVE OR VERTEY LUBE OIL LEVEL OR PRESSURE. BASIS..... 90TH THE PUMP AND THE MOTOR HAVE SELF CONTAINED SEARINGS WHICH DO NOT REQUIRE EXTERNAL LUBRICATION 1 AND ARE NOT FOULTPED WITH ANY MEANS TO SUPPLY EXTERNAL LUBRICATION. ALTERNATIVE. USE OF VIBRATION VELOCITY AS A MEASUREMENT MODE FOR VIBRATION WILL ALLOW ANY LACK OF LUBRICATION TO BE IMMEDIATELY DETECTED. FREQUENCY ... QUARTERLY REQUEST.... RR.12 SYSTEM ... VARTOUS COMPONENT.... VARIOUS. INDIVIDUAL VALVES FOR WHICH THIS SELIFE REQUEST APPLIES ARE IDENTIFIED IN THE VALVES PRINTOUT BY ROLLD IN THE DELTEE COLUMN 1 CLASS CATEGORY FUNCTION.... CONTAINMENT ISOLATION VALVES (CIV'S). - TMP_REDUTRE __ CATEGORY A LEAK RATE TESTING. BASIS..... MAINTAINING TWO SEPERATE LEAK TEST PROGRAMS FOR THE SAME VALVES IS NOT ECONOMICALLY JUSTIFIED NOR DOES IT ADD TO THE SAFETY OF THE PLANT. THE SECTION XI CATEGORY A LEAK TESTS ARE INTENDED FOR . VALVES WHICH PERFORM A PRESSURE ISOLATION TYPE FUNCTION AND NOT FOR APPENDIX J TYPE TESTS WHICH ARE <u>INTENDED TO DEMONSTRATE CONTAINMENT LEAK TIGHTNESS. SINCE THESE VALVES ARE CATEGORY A BECAUSE OF</u> THEIR CONTAINMENT ISOLATION FUNCTION. THE APPROPRIATE LEAK TEST METHOD IS ONE WHICH COMPLIES WITH . 10CFR50 APPENDIX J. ALTERNATIVE. ALL CIV SEAT LEAK TESTING SHALL BE PERFORMED IN ACCORDANCE WITH THE REQUIREMENTS OF 10CFR50 APPENDIX J TYPE C IN LIEU OF THE CATEGORY A REQUIREMENTS OF SECTION XI. THE SEAT LEAKAGE TESTING 4 OF THESE VALVES MEETS THE INTENT OF SECTION XI BUT THE ACTUAL TEST PROCEDURES SHALL BE IN ACCORDANCE WITH THE 10CFR50 APPENDIX J TYPE C CIV TEST PROGRAM. FREQUENCY.... ONCE PER REFUELING. 4 REQUEST.... RR.13 SYSTEM ---- VARIOUS CONTAINMENT ISOLATION COMPONENT.... ALL CONTAINMENT ISCLATION VALVES (CIV) CATEGORY.... A AND AC \mathbf{o} - FUNCTION.... CONTAINMENT ISOLATION IMP.REQUIRE.. ANALYSIS OF LEAKAGE RATES PER IWV-3426 BASIS...... THE REQUIREMENTS OF APPENDIX I WHICH ALSO GOVERN ANALYSIS OF LEAKAGE RATES OF CIV'S DO NOT MATCH THE REQUIREMENTS OF SECTION XI. IN THIS CASE, THE REQUIREMENTS OF APPENDIX J. APPLIED IN ACCORDANCE WITH THE BELOW LISTED ALTERNATIVE, ARE MORE CONSERVATIVE. ALTERNATIVE. . CIV'S WHICH ARE LEAK TESTED IN ACCORDANCE WITH THE REQUIREMENTS OF 10CFR50, APPENDIX J. ARE <u>ASSIGNED</u> CONSERVATIVE REFERENCE LEAK RATES BASED UPON THE VALVE SIZE AND THE TOTAL ALLOWABLE CONTAINMENT PENETRATION LEAKAGE, O.6 LA. THE TOTAL OF ALL OF THE REFERENCE LEAK RATES IS SET EQUAL TO APPROXIMATELY 40% OF THE TOTAL ALLOWABLE CONTAINMENT LEAKAGE, I.E., 40% OF (0.6 LA); THIS PROVIDES A COMFORTABLE MARGIN EVEN IF ALL VALVES ARE LEAKING THEIR RESPECTIVE REFERENCE LEAK RATES. IF A MAXIMUM PERMISSIBLE LEAK RATE IS NOT SPECIFIED BY THE OWNER (LICENSEE), IWV-3426, AS A GUIDELINE, RECOMMENDS A PERMISSIBLE LEAK RATE EQUIVALENT TO 0.3125 SCFH PER INCH VALVE SIZE; THE REFERENCE LEAK RATE ASSIGNED TO CIV'S FROM THE PRECEDING METHODOLOGY CORRESPONDS TO 0.06 SCFH PER INCH VALVE SIZE, LESS THAN ONE FIFTH THE CODE GUIDELINE. DURING REFUELING OUTAGES MAINTENANCE IS <u>PERFORMED, IE REQUIRED,</u> IN AN ATTEMPT TO RESTORE ALL CIV'S TO BELOW THEIR REFERENCE LEAK RATES AND AS CLOSE TO ZERO LEAKAGE AS REASONABLY ACHIEVABLE; THIS ENSURES THE ABILITY OF THE CONTAINMENT <u>SYSIEM TO SATISFY THE INTEGRATED LEAK RATE TESTING CRITERIA AND TO PROVIDE ADEQUATE MARGIN FOR</u> VALVE DEGRADATION OVER THE NEXT FUEL CYCLE. WHILE EVERY ATTEMPT IS MADE TO MAINTAIN CIV'S AT ZERO LEAKAGE OR RELOW THEIR REFERENCE LEAK FATES AT ALL TIMES, A VALVE LEAKING IN EXCESS OF ITS REFERENCE VALUE MAY REMAIN OPERABLE AND LEFT "AS IS" IN CERTAIN SITUATIONS, PROVIDED THAT AN

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ت ا	EVALUATION BY AN ENGINEER CERTIFIED TO LEVEL III CONTAINMENT LEAKAGE RATE TESTING IN ACCORDANCE	•		_
	WITH ASNIT-TC-1A FINDS IT ACCEPTABLE. AN EXAMPLE OF SUCH A SITUATION WOULD BE A VALVE FOUND TO BE		•_	
2)	LEAKING IN EXCESS OF 115 REFERENCE LEAK RATE IN MID FUEL CYCLE, AND FOR WHICH ALL DEACONABLE			_
,	ON-LINE MAINTENANCE EFFORTS HAVE FEEN MADE. SUCH EVALUATION SHALL BE BASED UPON CONSIDERATION OF			
	THE EFFECTS ON OVERALL CONTAINMENT LEAKAGE AND POSSIBLE EFFECTS ON ADJACENT PIPING AND COMPONENTS,			
•	AS WELL AS CONSIDERATION OF TIME, COST, UNIT OPERATIONS, AND RADIOLOGICAL EXPOSURE REQUIRED FOR			
'	CORRECTIVE MEASURES. WHILE THE MAXIMUM PERMISSIBLE LEAK RATE AT THIS TIME WOULD, BY PLANT	7		
	TECHNICAL SPECIFICATIONS, BE LIMITED TO THE CHERENT MARGIN BETWEEN OVERALL CONTAINMENT LEAKAGE AND			
7	U.O LAZ MAXIMUM SINGLE PENETRATION LEAKAGE IS AT ALL TIMES ADMINISTRATIVELY LIMITED TO A VALUE THAT			
'	AS LOW AS REASONABLY ACHIEVABLE AND CONSISTENT WITH THE EVALUATION BY THE LEVEL TIT TESTED AND			
	SOUM VALVE, WOULD BE REPAIRED OR REPLACED NO LATER THAN THE NEXT REFLIELTING OUTAGE OF EVEN DURING			
(1)	THE NEXT COLD SHUTDOWN OF SUFFICIENT DURATION IF PRACTICAL. THE ABOVE DESCRIBED METHODOLOGY FOR			
. .	SELLING AND MAINTAINING ULTRA CONSERVATIVE MAXIMUM LEAK RATES ENGURES SYSTEM OPERARTITY AND			
	PROVIDES REASONABLE ASSURANCE OF VALVE LEAK-TIGHT INTEGRITY INTENDED BY THE CODE. AT THE SAME TIME			
•	PLEXIBILITY IS PROVIDED TO PRUDENTLY OPERATE UNTIL THE NEXT REFUGITING OUTSIGE (OR LENGTHY COLD			
. •	SHUTDOWN). FOR THESE REASONS RELIEF AS REQUESTED WILL NOT ENDANGER LIFE OR PROPERTY OR THE COMMON			
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.)	FREQUENCY AS REQUIRED BY IMV-3422 AND APPENDIX J. WHICHEVER IS MODE RESTRICTIVE.			
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	SYSTEM CHEMICAL AND VOLUME CONTROL			
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	FUNCTION OPENS TO ADMIT FLOW FROM REFUELING WATER STORAGE TANK TO THE CENTRIFUGAL CHARGING PUMPS. CLOSES TO	-		
	PREVENT REVERSE FLOW TO RWST IMP.REQUIRE. EXERCISE QUARTERLY.		· · · · · · · · · · · · · · · · · · ·	
9	AMPERENDIKE. EXERCISE QUARTERLY.			
	SASTS CHARGING PUMPS CANNOT BE RUN TAKING SUCTION FROM THE REST WITHOUT CAUSING UNDESTRABLE RCS			
	TEMPERATURE AND OR BORON CONCENTRATION CHANGES RESULTING IN CHANGES IN REACTIVITY DURING OPERATION			
0	ALTERNATIVE SYCERCISE AT THE FIRST TRIP. LETDOWN CAPACITY WILL NOT ALLOW FULL FLOW TESTING DURING MODE 5.			
-	ALTERNATIVE. EXCERCISE AT FULL FLOW AT REFUELING AND AT PART FLOW DURING COLD SHUTDOWN. VERIFY VALVE IS 54CKSEATED GUARTERLY.			
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0	BASIS THE CENTRIFUGAL CHARGING PUMPS CANNOT BE RUN AT FULL FLOW DURING OPERATION FOR CHARGING OR THROUGH	·		
_	THE COLD LEG INJECTION LINES DUE TO UNDESIRABLE TEMPERATURE AND OR BORON CONCENTRATION TRANSIENTS	*		
_	AND INSUFFICIENT LETDOWN CAPACITY. INSUFFICIENT LETDOWN CAPACITY PRECLUDES FULL FLOW TESTING IN			
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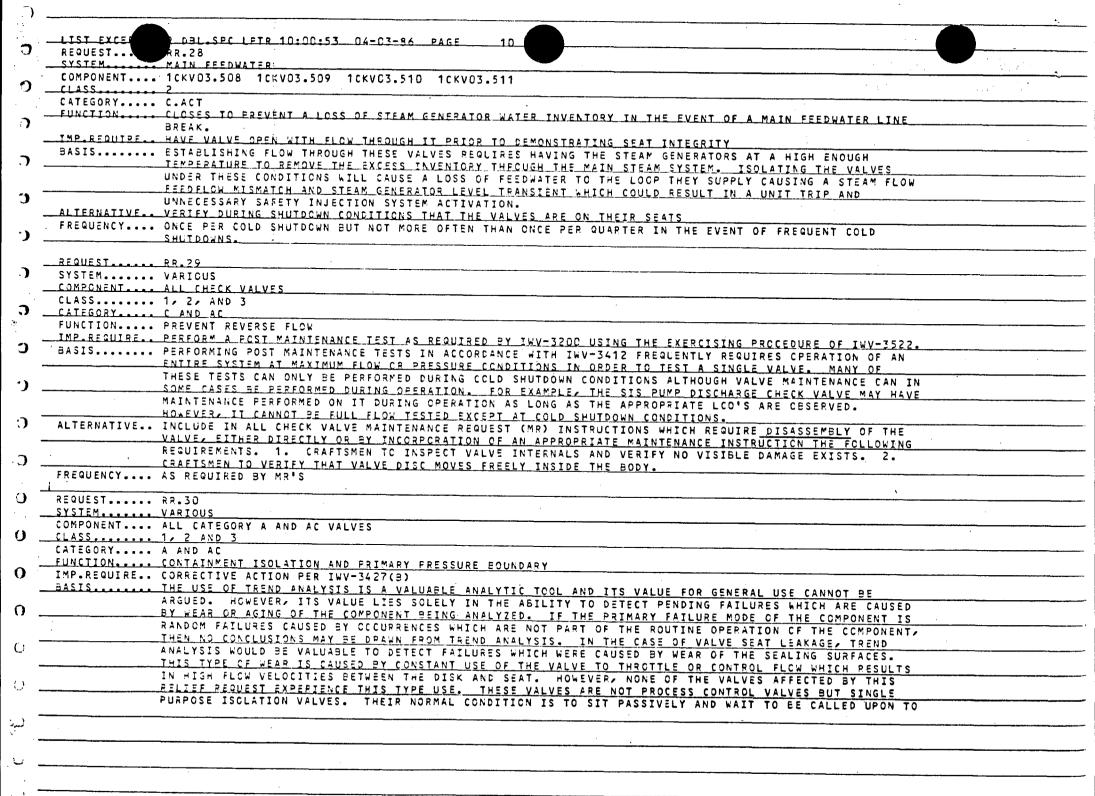
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ITST FYCE R DBL_SPC LPTR 10:00:53 04-03-86 PAGE CLASS CATEGORY FUNCTION.... OPENS TO ADMIT FLOW FROM RWST TO THE RHR PUMPS DURING SAFETY INJECTION. CLOSES TO PREVENT FLOW TO THE RUST DURING ECCS RECTROULATION IMP.REQUIRE. EXERCISE VALVE DURING OPERATION. BASIS.... THE RHR PUMPS DO NOT DEVELOP SUFFICIENT HEAD TO PUMP TO THE REACTOR AT NORMAL OPERATING PRESSURES. THE PUMP RECIRCULATION FLOW PATH DOES NOT INCLUDE THIS CHECK VALVE. CAPABILITIES OF THE LETDOWN SYSTEM PRECLUDE TESTING DURING COLD SHUTDOWN. BACKSEATING DURING OPERATION WOULD REQUIRE CLOSURE OF 1FCV63_GO1A WHICH WOULD CAUSE INOPERABILITY OF BOTH TRAINS OF RESIDUAL HEAT REMOVAL. ALTERNATIVE .. EXERCISE AT REFUELING OUTAGES AT FULL FLOW. VERIFY THE VALVE HAS EACKSEATED DURING COLD SHUTDOWN. FREQUENCY... FULL STROKE AT REFUELING AND VERIFY THE VALVE HAS BACKSEATED EACH COLD SHUTDOWN BUT NOT MORE OFTEN THAT ONCE PER GHARTER IN THE EVENT OF FREQUENT COLD SHUTDOWNS. ^) REQUEST RP.17 SYSTEM.... SAFETY INJECTION COMPONENT 10KV63-5109 CLASS..... 2 CATEGORY C.ACT FUNCTION.... CPENS TO ADMIT FLOW FROM RWST TO THE REACTOR THROUGH THE SIS PUMPS DURING SAFETY INJECTION. CLOSES ID PROVIDE DOUBLE ISOLATION DURING RECIRCULATION MODE. IMP_REQUIRE_. EXERCISE VALVE DURING OPERATION AT FULL FLOW. . BASIS..... SIS PUMPS DO NOT DEVELOP SUFFICIENT HEAD TO PUMP TO THE RCS AT NORMAL OPERATING PRESSURES AND THE PUMP RECIRCULATION LINE WILL NOT PASS FULL FLOW. CAPABILITIES OF THE LETDOWN SYSTEM PRECLUDE FULL FLCW TESTING DURING COLD SHUTDOWN. ALTERNATIVE.. CYCLE VALVE AT REDUCED FLOW ONCE PER QUARTER DURING SIS PUMP TEST AND AT FULL FLOW ONCE PER 1 REFUELING. VERIEY VALVE HAS BACKSBATED ONCE PER COLD SHUTDOWN. FREQUENCY.... PART STRCKE QUARTERLY. FULL STRCKE ONCE PER REFUELING. VERIFY VALVE HAS BACKSEATED ONCE PER COLD SHUTDOWN BUT NOT MORE CRIEN THAN ONCE PER COLD SHUTDOWN IN THE EVENT OF FREQUENT COLD SHUTDOWNS. REQUEST. ... RR.18 SYSTEM..... SAFETY INJECTION SYSTEM COMPONENT... 10KV63.543A 10KV63.545A 10KV63.547B 10KV63.549B 10KV63.5518 10KV63.5538 10KV63.5558 10KV63.5578 1CKV63.558B 1CKV63.559B 1CKV63.641S 1CKV63.644S Э CLASS..... 1 CATEGORY AC.ACT FUNCTION.... OPENS TO ADMIT FLOW FROM SIS PUMPS TO RCS DURING LOCA. IMP.REQUIRE.. EXERCISE QUARTERLY AT FULL FLOW BASIS..... SIS PUMPS DO NOT DEVELOP SUFFICIENT HEAD TO OVERCOME NORMAL RCS PRESSURE. VALVES ARE NOT IN RECIRCULATION FLOW PATH. CAPABILITIES OF THE LETDOWN SYSTEM PRECLUDES FULL FLOW TESTING DURING COLD SHUTDOWN. TECH SPEC 4.4.6.2.2 REQUIRES THESE VALVES TO BE LEAK TESTED FOLLOWING VALVE ACTUATION AND DURING COLD SHUTDOWN IF THEY HAVE NOT BEEN LEAK TESTED IN THE LAST NINE MONTHS. THEREFORE, RELIEF IS REQUESTED TO ALLOW PARTIAL STROKING OF THESE VALVES DURING COLD SHUTDOWN NOT TO EXCEED ONCE PER NINE MONTHS AND FULL STRCKE EXERCISING DURING REFUELING OUTAGES. VALVE CLOSURE WILL BE VERIFIED DURING COLD SHUTDOWN, NOT TO EXCEED ONCE PER NINE MONTHS WHEN THE PRESSURE ISCLATION EOUNDARY LEAK TEST REQUIRED BY SR 4.4.5.2.2 IS PERFORMED. ALTERNATIVE. EXERCISE VALVE AT REFUELING AT FULL FLOW AND AT PART FLOW DURING COLD SHUTDOWN. LEAK TEST AS REQUIRED BY SR 4.4.6.2.2. FREQUENCY... PART STROKE EVERY COLD SHUTDOWN NOT TO EXCEED ONCE PER NINE MONTHS AND FULL STROKE EACH REFUELING GUTAGE. LEAK TEST AT THE FREQUENCIES REQUIRED BY SR 4.4.6.2.2. REQUEST.... RR.19 SYSTEM. SAFETY INJECTION COMPONENT.... 1CKV63.581S 1CKV63.586S 1CKV63.587S 1CKV63.588S 1CKV63.589S

DBL SPC LPTR 10:00:53 04-03-86 PAGE LIST FXCE CLASS.... CATEGORY C ACT FUNCTION..... OPEN TO ADMIT FLOW FROM BORON INJECTION TANK TO THE RCS DURING SAFETY INJECTION. - IMP RECUIRE - EXERCISE VALVE ON A GUARTERLY RASIS BASIS..... CYCLING THE VALVES WOULD CAUSE AN UNDESTRAELE TEMPERATURE AND OR BORON CONCENTRATION CHANGES AND UNSTABLE CHARGING AND LETDOWN CONDITIONS WHICH COULD RESULT IN A SAFETY INJECTION OR UNIT TRIP. CAPABILITIES OF THE LETDOWN SYSTEM PRECLUDE FILL FLOW TESTING DURING COLD SHUTDOWNS. ALTERNATIVE - EXERCISE VALVE AT FULL FLOW DURING REFUELING AND AT PART FLOW DURING COLD SHUTDOWN. FREQUENCY.... FULL STROKE AT REFUELING AND PART STROKE FACH COLD SHUTDOWN BUT NOT MORE OFTEN THAN ONCE PER 7 CUARTER IN THE EVEAT OF FREQUENT COLD SHUTDOWNS. REQUEST RR 20 4 SYSTEM----- SAFETY INJECTION AND UPPER HEAD INJECTION COMPONENT 10KV63 6228 10KV63 6238 10KV63 6248 10KV63 6258 10KV87 5588 10KV87 5598 10KV87 5608 10KV87 5618 1CKV87-5628 1CKV87-5638 1CKV63-5608 1CKV63-5618 1CKV63-5628 1CKV63-5638 CATEGORY ---- AC-ACT - FUNCTION: ... OPENS TO ADMIT FLOW FROM ACCUMULATORS TO THE PCS DURING DEPRESSURIZATION. IMP_REQUIRE__ EXERCISE AT FILL FLOW AND DURING OPERATION_ BASTS THE ACCUMULATORS ARE PASSIVE AND DE THEMSELVES DO NOT HAVE SUFFICIENT PRESSURE TO OVERCOME RCS PRESSURE. THE SIS PUMPS DO NOT DEVELOP SUFFICIENT HEAD TO OPEN THE COLD LEG ACCUMULATOR VALVES AT NORMAL PRESSURE BY USING THE CHECK VALVE TEST LINE. THE RECIPROCATING CHARGING PUMP COULD BE USED TO OPEN THE UPPER HEAD INJECTION CHECKS BUT THIS WOULD CREATE AN UNDESTRABLE REACTIVITY EXCURSION DUE TO THE ADDITION OF COLD WATER INTO THE VESSEL HEAD. NEITHER OF THE TWO METHODS OF OPENING THE CHECKS WILL REACH FULL FLOW DUE TO THE HIGH RESISTANCE OF THE CHECK VALVE TEST LINE. THE CHECK VALVE TEST LINE IS THE ONLY MEANS AVAILABLE TO CREW THESE VALVES AND IT WILL NOT PASS FULL FLOW. THE ONLY WAY TO REACH FULL FLOW ON THESE LINES IS TO COMPLETELY UNICAD THE CORE. REMOVE THE INTERNALS FACKAGES, INSTALL TEMPORARY IMPINGEMENT PLATES AND DRAIN THE REACTOR COCLANT SYSTEM. THE RESULTANT EXTENDED DOWN TIME DUE TO THE ADDITIONAL FUEL MOVEMENT AND STORAGE PROBLEMS AND WATER CHEMISTRY CLEAN UP AND REFILL GRERATIONS PRESENT AN UNUSUALLY LARGE FINANCIAL SURDEN WITHOUT A CORRESPONDING INCREASE IN THE LEVEL OF SAFETY. TECHNICAL SPECIFICATION 4.4.6.2.2 REQUIRES THESE <u>VALVES TO BE LEAK TESTED FOLLOWING VALVE ACTUATION AND DURING COLD SHUTDOWN IF THEY HAVE NOT BEEN </u> LEAK TESTED IN THE LAST NINE MONTHS. THEREFORE, RELIEF IS REQUESTED TO ALLOW PARTIAL STROKING OF THESE VALVES DURING COLD SHUTDOWN NOT TO EXCEED ONCE PER NINE MONTHS. VALVE CLOSURE WILL BE VERIFIED DURING COLD SHUTDOWN, NOT TO EXCEED ONCE PER NINE MONTHS WHEN THE PRESSURE ISOLATION POUNDARY LEAK TEST REQUIRED BY SR 4.4.6.2.2 IS PERFORMED. ALTERNATIVE. EXERCISE AT THE MAXIMUM FLOW AVAILABLE THROUGH THE CHECK VALVE TEST LINE DURING COLD SHUTDOWNS. LEAK TEST AS REQUIRED BY SR 4.4.6.2.2. O FREQUENCY.... PART STROKE EVERY COLD SHUTDOWN NOT TO EXCEED ONCE PER NINE MONTHS. LEAK TEST AT THE FREQUENCIES REQUIFED BY SR4.4.6.2.2. IREQUEST. SYSTEM..... MAIN STEAM, SAMPLING, REACTOR COOLANT, VENTILATION COMPONENT.... 1 FCV01.0078 1 FCV01.0148 1 FCV01.025 1 FCV01.0328 1 FCV01.1818 1 FCV01.1828 1 FCV01.1838 1 FCV01.1848 1FSV43.250 1FSV43.251 1FSV43.267 1FSV43.288 1FSV43.307 1FSV43.309 1FSV43.310 1FSV43.318 1FSV43.319 <u> 158V43.325 168V43.341 168V43.342 16CV68.334 16CV68.340A.A 16SV68.394 16SV68.395 16SV68.396</u> (; 1FSV69.397 1FSV30.134 1FSV30.135 2 FOR ALL EXCEPT THE SYSTEM 69 VALVES WHICH ARE CLASS 1 CATEGORY.... ALACT FOR ALL EXCEPT THE SYSTEM 68 VALVES WHICH ARE BLACT FUNCTION. ... CONTAINMENT ISOLATION, EXCEPT FOR THE SYSTEM 68 VALVES. THE SYSTEM 68 PCV'S ARE POWER OPERATED RELIEF VALVES LOCATED ON THE PRESSURIZER. THE SYSTEM 68 FSV'S ARE REACTOR COOLANT HEAD VENT VALVES.

IN PARALLEL WILL BE HELD TO THE MINIMUM POSSIBLE WITH THE INSTALLED SYSTEM. WHERE TWO OR MORE VALVES MUST BE TESTED IN PARALLEL ALL MEASURED LEAKAGE WILL BE ASSUMED TO BE COMING FROM ONE VALVE. FREQUENCY AS REQUIRED BY SURVEILLANCE REQUIREMENT 4.4.6.2.2. REQUEST RR.24 SYSTEM UPPER HEAD INJECTION COMPONENT 1FCV87.C21D 1FCV87.022E 1FCV87.C23F 1FCV87.C24G CLASS 2	
AASIS. VALUES RE IOTALLY ENCISED SOLEMOID OPERATED VALUES WHICH HAVE NO EXTERNAL MOVING PARTS CAPABLE OF SIGN USED TO VERIFY VALVE POSITION. ALTERNATIVE. VERIEY, VALVE POSITION OF VEST AVAILABLE MEANS. WHERE A SIGNIFICANT TEMPERATURE OR PRESSURE OF ARADADE IN DOWNSTREAR THE PREFATURE OR PRESSURE MAY BE USED. WHERE THE CARABILITY TO VERIEY, FLOW EXISTS, THE PRESSINCE AND ABSENCE OF FLOW MAY BE USED. WHERE NO FEDERAL WAS ARRESTED ON SAVALLABLE, ACOUSTIC MONITORING OF VALVE OPERATION MAY BE USED. WHERE NO FEDERAL WAS SELECT. REQUEST. 8.2.2 SYSTEM CONTAINMENT SPRAY COMPANIENT. LIVEZ. SARA ICKYZZ. SAZR ICKYZZ. SAZR ICKYZZ. SAZR COMPANIENT. LIVEZ. SAZR ICKYZZ. SAZR ICKYZZ. SAZR ICKYZZ. SAZR COMPANIENT. LIVEZ. SAZR ICKYZZ. SAZR ICKYZZ. SAZR ICKYZZ. SAZR CLASS	
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REQUEST. SR.22 SYSTEM. CONTAINMENT SPRAY CAMPANENT. 16xV72.5484 16xV72.5498 16xV72.5624 16xV72.5638 CLASS. 2 CATEGORY. CLACT CHASS. 2 CATEGORY. CLACT SPANIE STREET	· · · · · · · · · · · · · · · · · · ·
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DESIGNED TO CLOSE A 12 INCH VALVE AGAINST EXTREMELY HIGH FLOW RATES AND PRESSURES IN 3.5 SECONDS.	
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I IST EXCER DPL SPC LPTR 10:00:53 04-03-86 PAGE HE INCREASED DENSITY OF WATER AT UHI OPERATING SURES COMBINED WITH THE VELOCITY AT WHICH THESE VALVES CLOSE CREATE AN EMORMOUSLY HIGH ENERGY WATER STREAM TO BE EJECTED FROM BETWEEN THE VALVE DISK AND SEAT. THIS IN TURN CREATES A HIGH POTENTIAL FOR EROSION OF SEAT AND DISK TO THE EXTENT • THAT THE VALVES COULD EVENTUALLY LOSE THEIR PHYSICAL INTEGRITY. ALTERNATIVE.. TEST THE VALVES USING THE MAINTENANCE CPERATOR, WHICH FUNCTIONS AT A SLOWER SPEED, ON A QUARTERLY BASIS AND WITH THE NORMAL CPERATOR DURING REFUELING OUTAGES. FREQUENCY.... PART SPEED STROKE GUARTERLY AND FULL SPEED STRCKE AT REFUELINGS. REQUEST.... RR.25 - SYSTEM VARIOUS COMPONENT VARIOUS CLASS 1. 2. AND 3 CATEGORY.... A.ACT AND B.ACT FUNCTION. VARIOUS IMP.REQUIRE.. EVALUATING IN GUANTITATIVE TERMS THE STROKE TIMES OF FAST ACTING CATEGORY A AND B VALVES. BASIS.... IT IS IMPRACTICAL TO ATTEMPT TO QUANTIEY STROKE TIMES OF VALVES WITH VERY SHORT STROKE TIMES (1.5. < 2 SECONDS). SOLENCID OPERATED VALVES, FOR EXAMPLE, TYPICALLY HAVE FULL STROKE TIMES OF MUCH LESS</p> THAN ONE SECOND. FOR THESE SHORT STROKE TIMES, VARIANCES OF 50% OR MORE CAN OCCUR IN THE MEASURED $\mathbf{\cdot}$ STROKE TIME FOR REASONS THAT ARE IN NO WAY RELATED TO VALVE PERFORMANCE, FOR EXAMPLE, OPERATOR REACTION TIMES. IN THESE CASES, VERIEVING THAT THE VALVE'S STROKE TIME DOES NOT EXCEED 2 SECONDS WOULD BE SUFFICIENT TO EVALUATE VALVE CONDITION. 3 ALTERNATIVE. VERIEY VALVES STROKE IS NOT GREATER THAN 2 SECONDS. FREQUENCY.... EACH VALVE TEST. 3 REQUEST..... RR.26 W - ITEDRAM N 1) SYSTEM. COMPONENT.... CI ASS. O CATEGORY..... FUNCTION.... IMP.REQUIRE.. 0 ALTERNATIVE.. FREQUENCY.... 0 REQUEST.... FR.27 SYSTEM..... VARIOUS, INCLUDES ALL ACTIVE PUMPS WHICH DELIVER TO A COMMON DISCHARGE HEADER O COMPONENT.... VARIOUS. SPECIFIC COMPONENT IDENTIFIED BY RR.27 IN THE RELIEF COLUMN. CLASS..... 2 AND 3 CATEGORY.... C.ACT FUNCTION.... VALVES MUST OPEN TO DELIVER FLOW AND RECLOSE TO PREVENT RECIRCULATION THROUGH THE SHUTDOWN PUMP. IMP_REQUIRE. HAVE VALVE OPEN WITH FLOW THROUGH IT PRIOR TO DEMONSTRATING SEAT INTEGRITY BASIS..... OPENING THE VALVES WITH PUMP FLOW AT THE TIME THE SEAT INTEGRITY OF THE VALVE IS VERIFIED WOULD REQUIRE EXCESSIVE FUMP STARTS, WOULD FREQUENTLY REQUIRE REMOVING SAFETY RELATED PUMPS FROM SERVICE. AND IN THE CASE OF THE CHARGING PUMPS AND SIS PUMPS IT WOULD REQUIRE VIOLATION OF MODE 4, 5 OR 6 TECHNICAL SPECIFICATIONS REGARDING THE NUMBER OF PUMPS WHICH MAY BE OPERABLE AT A GIVEN TIME. ALTERNATIVE.. EXERCISE VALVE OPEN DURING THE PUMP TEST FOR THE PUMP WITH WHICH THE VALVE IS ASSOCIATED. VERIFY THE VALVE HAS CLOSED SUFFICIENTLY TIGHT TO PRECLUDE EXCESS LEAKAGE DURING THE PUMP TEST OF EACH OF THE OTHER PUMPS WHICH FEED THE SAME HEADER. FREQUENCY... SUARTERLY



R DRL_SPC LPTR 10:00:53 04-03-86 PAGE FREORM THEIR ISOLATION FUNCTION. THEREFORE, I NOT ANTICIPATED THAT SEAT AND DISK WEAR WILL BE A SIGNIFICANT CONTRIBUTOR TO VALVE LEAK RATE FATLURES. WE ANTICIPATE AND IT HAS BEEN OUR EXPERIENCE, THAT THE PRIMARY CAUSE OF EXCESSIVE LEAKAGE IN CIV'S AND PRESSURE BOUNDARY VALVES IS INCLUSION OF FOREIGN PARTICLES RETWEEN THE DISK AND SEAT CAUSING THE SEATING SURFACE TO FITHER BE HELD APART OR SUSTAIN A SCRATCH WHICH PENETRATES FROM SEAT LIP TO SEAT LIP. GTHER MAJOR CONTRIBUTORS TO VALVE LEAKAGE FATILIRES ARE FAILURE OF THE VALVE OPERATOR OR EXCESSIVE LIGHTNESS OF PACKING. NONE OF THESE FAILURE MODES CAN BE DETECTED OR PREDICTED BY TREND ANALYSIS. ADDITIONALLY, TREND ANALYSIS REQUIRES THAT THE UPPER LIMIT BE SET SUBERCIENTLY HIGH THAT RANDOM DATA SCATTER DOES NOT CAUSE PREMATURE FAILURE OF THE MCNITORED CRITERIA. IT HAS BEEN OUR EXPERIENCE THAT WITH THE DEPER LIMITS OF LEAKAGE SET AS LOW AS WE HAVE THEM RANDOM DATA SCATTER CONSUMES ALL THE AVAILABLE CEILING BETWEEN THE TREND AND THE UPPER LIMIT AND CAUSES TREND ANALYSIS TO ERRONEOUSLY PREDICT EARLY FAILURES CAUSING EXCESSIVE MAINTENANCE AND TESTING TO BE PERFORMED WITH A RESULTANT INCREASE IN COST OF DCLLARS AND MAN/REM WITHOUT A CORRESPONDING INCREASE IN THE LEVEL OF SAFETY. ADDITIONALLY THE LEAK TESTING SYSTEMS FOR PRIMARY PRESSURE BOUNDARY VALVES IS SUCH THAT IN MOST CASES IT IS IMPOSSIBLE TO AVOID MORE THAN ONE VALVE BEING TESTED AT A TIME. FURTHERMORE, THE LEAK TEST SYSTEM IS SUCH THAT MANY LEAK TEST LINES MAY FEED INTO THE LEAKAGE PATH. THEREFORE A LEAKING TEST SYSTEM VALVE COULD ADD TO THE MEASURED LEAKAGE; THAT IS, THE LEAK RATE COULD BE COMING FROM THE TESTED VALVE, FROM TEST LINE VALVES OR BOTH. IF THE COMBINED LEAKAGE IS LESS THAN 1 GPM THEN TECHNICAL SPECIFICATIONS ARE GUARANTEED SATISFIED FOR THE INDIVIDUAL VALVES; A LEAK PATE FOR EACH VALVE, HOWEVER, CANNOT BE DETERMINED. FOR THESE REASONS, TRENDING OF LEAKBATES IS MEANINGLESS FOR THE PURPOSE OF MONITORING FOR VALVE DEGRADATION. SEE RELIEF REQUEST RR.13 FOR ADDITIONAL INFORMATION RESARDING CONTAINMENT ISOLATION VALVES. ALTERNATIVE. . APPLY CORRECTIVE ACTION PER INV-3427(A) AND RR.13 FREQUENCY ... AS REQUIRED BY INV-3422 OR APPENDIX J . WHICH EVER IS THE MORE FREQUENT. SYSTEM..... DIESEL GENERATOR AIR START SYSTEM COMPONENT ... DIESEL ENGINE AIR START VALVES CLASS..... 3 CATEGORY PACT FUNCTION.... OPENS TO APPLY AIR PRESSURE TO THE DIESEL ENGINE AIR START MOTORS. IMP REQUIRE. MEASURING STROKE TIME IN ACCORDANCE WITH THE REQUIREMENTS OF SECTION XI. BASIS..... THE STROKE TIME OF THE AIR START VALVES CANNOT BE MEASURED AS THERE IS NO VISIBLE STEM MOVEMENT OR **C** INDICATION. VALVES ARE AIR OPERATED STEMLESS DIAPHRAGM VALVES. THE ONLY MOVING PART IS THE DIAPHRAGM ITSELF WHICH IS TOTALLY ENCLOSED WITHIN THE VALVE. ALTERNATIVE. VERIFY THAT THE ASSOCIATED DIESEL COMES UP TO SPEED IN LESS THAN OR EQUAL TO 10 SECONDS. THIS 3 DEMONSTRATES THAT THE VALVE HAS FUNCTIONED ADEQUATELY. FREQUENCY... AS REQUIRED BY TABLE 4.8-1 OF THE WATTS BAR TECHNICAL SPECIFICATIONS WHICH LISTS A MAXIMUM NOMINAL TEST FREQUENCY OF ONCE PER 31 DAYS. O REQUEST.... RR.32 SYSTEM..... REACTOR COCLANT O COMPONENT 1CKV68.559 CATEGORY.... S.ACT Ω FUNCTION.... CPENS TO ALLOW FLOW FROM FELIEF VALVE VENT HEADER TO ENTER THE PRESSURIZER RELIEF TANK. CLOSES TO PROVIDE CONTAINMENT BOUNDARY. IMP. REQUIRE. EXERCISE THE VALVE. \mathbf{C} BASIS..... SIGNIFICANT PROBLEMS EXIST FOR FULL FLOW EXERCISING THIS CV IN ACCORDANCE WITH THE REQUIREMENTS OF SECTION XI. FULL FLOW EXERCISING, IS NOT POSSIBLE DUE TO THE NATURE OF THE SYSTEM, I.E., CANNOT LIFT ALL RELIEF VALVES AT SETPOINT PRESSURES. PARTIAL STRCKE EXERCISING WOULD PRESENT UNACCEPTABLE PERSONNEL HAZAFOS UNLESS ALL INTERACTING SYSTEMS WERE REMOVED FROM SERVICE; THESE SYSTEMS INCLUDE RCS, CVCS CHARGING/SEAL FLCW/LETDOWN, RHR, SIS, AND CS SYSTEMS. REMOVAL FROM SERVICE OF THE

LIST EXCE R DBL.SPC LPTR 10:00:53 04-03-86 PAGE AFFECTED SYSTEMS WOULD REQUIRE ENTRY INTO LCOS ' N CVERALL DEGRADED PLANT CONDITION REGARDLESS OF OPERATING MODE. FOR THESE REASONS THE LICENSEE IS PEQUESTING RELIEF FROM VALVE EXERCISING REGUIREMENTS OF PARAGRAPH IWV-3520 CF SECTION XI. THIS CV IS A CIV BUT IS NOT APPENDIX J TESTED 1) SECAUSE: 1) ANY LEAKAGE WOULD BE INTO A CLOSED, QUALIFIED SYSTEM, 2) THE INJECTED PRESSURE WOULD ALWAYS EXCEED 1.1 PA, AND 3) A GUARANTEED 3C-DAY WATER SUPPLY IS PROVIDED FOR SIS, CCP AND CS PUMPS. ACCORDINGLY, THIS VALVE IS NOT REQUIRED TO BE LEAK TESTED IN ACCORDANCE WITH THE • REGUIREMENTS OF SECTION XI. LIERNATIVE NONE FREQUENCY... NONE 7 REQUEST..... RR.33 SYSTEM.... SAFETY INJECTION 7 COMPONENT.... 1CKV63.5865 1CKV63.5875 1CKV63.5885 1CKV63.5395 1CKV63.5475 1CKV63.549B 1CKV63.543A 1CKV63.545A 1CKV63_6435 1CKV63_6405 CLASS..... 1 CATEGORY ... A ACT AND E ACT FUNCTION.... OPENS TO PERMIT FLOW TO THE REACTOR VESSEL FROM VARIOUS PUMPS IN THE SAFETY INJECTION SYSTEM. VALVES CATEGORIZED AS A ACT ALSO CLOSE TO PROVIDE PRIMARY PRESSURE BOUNDARY. IMP.REQUIRE.. VERIFY INDIVIDUAL VALVE STROKE DURING PART STOKE IN LIEU OF FULL STROKE TESTING. BASIS THESE VALVES ARE INSTALLED IN PARALLEL HEADERS WITH FROM TWO TO FOUR VALVES BEING FED FROM THE SAME SOURCE. WHEN PERFORMING THE PART STROKE TEST AT A MUCH REDUCED FROM FULL FLOW, IT IS IMPOSSIBLE TO Э DETERMINE WHETHER BOTH VALVES HAVE IN FACT LEFT THEIR SEAT. ALTERNATIVE. . VERIFY THAT AT LEAST ONE VALVE IN EACH PARALLEL FLOW PATH OPENS DURING EACH PART STROKE TEST. FREQUENCY... AS STATED IN PR. 18, FR. 19, AND RR. 20 1) 1REQUEST..... RR.34 SYSTEM..... SAFETY INJECTION COMPONENT ... 1CKV63.5246 1CKV63.5263 CLASS..... 2 CATEGORY.... C.AST FUNCTION.... OPENS TO ALLOW FLOW FROM THE RESPECTIVE SAFETY INJECTION PUMP TO ENTER THE REACTOR COOLANT SYSTEM DURING VARIOUS ACCIDENT SITUATIONS. IMP.REQUIRE.. STROKE TEST VALVE ON A QUARTERLY BASIS. BASIS SAFETY INJECTION PUMPS DO NOT PROVIDE SUFFICIENT HEAD TO OPEN THE VALVES DURING OPERATION. INSUFFICIENT LET DOWN CAPACITY PRECLUDES FULL FLOW TESTING DURING COLD SHUTDOWN. VALVES ARE NOT IN THE PUMP RECIRCULATION LINE. \odot ALTERNATIVE.. PART STROKE VALVES AT REDUCED FLOW AT EACH COLD SHUTDOWN BUT NOT MORE OFTEN THAN ONCE PER THREE MONTHS IN THE EVENT OF FREGUENT COLD SHUTDOWNS. FULL STROKE VALVE AT EACH REFUELING. FREQUENCY.... PART STROKE AT EACH COLD SHUTDOWN, BUT NOT MORE OFTEN THAN ONCE PER THREE MONTHS IN THE EVENT OF () FREQUENT COLD SHUTDOWNS. FULL STROKE AT EACH REFUELING. REQUEST.... RR.35 SYSTEM.... SAFETY INJECTION COMPONENT ... 1CKV63.6405 1CKV63.6435 CLASS...... 1 O CATEGORY ACACT FUNCTION.... CPENS TO ADMIT FLOW FROM THE RHR PUMPS TO THE REACTOR COCLANT SYSTEM DURING THE HOT LEG RECIFCULATION PORTION OF ACCIDENT RECOVERY. PRIMARY PRESSURE BOUNDARY ISOLATION. () IMP.REQUIRE.. FULL STROKE EXERCISE VALVE ON A QUARTERLY EASIS. BASIS..... FAR PUMPS DO NOT DEVELOP SUFFICIENT PRESSURE TO INJECT TO THE VESSEL DURING OPERATION. TESTING EACH COLD SHUTDOWN NOT ONLY UNNECESSARILY CHALLENGES THE ABILITY OF THE VALVE TO SEAT AND PROVIDE 1.7 ITS ISCLATION FUNCTION BUT ALSO CAUSES OTHER VALVES IN THE SAFETY INJECTION SYSTEM TO BE CHALLENGED WITH THE RESULTANT NECESSITY TO LEAK TEST ALL OF THE CHALLENGED VALVES IN ACCORDANCE WITH SR

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	LIST EXCER 2 DBL SPC LPTR 10:00:53 04-03-86 PAGE 13	
	4.4.6.2.2. ALIERNATIVE FULL STROKE TEST AT EACH COLD SHUTDOWN AT WHICH 5-4.4.6.2.2 REQUIRES LEAK TESTING OF THE PRIMARY	
^	PRESSURE BOUNDARY ISOLATION VALVES. MAXIMUM FREQUENCY FOR SR 4.4.6.2.2 IS ONCE PER COLD SHUTDOWN	
)	PROVIDING 9 MONTHS HAS PASSED SINCE THE LAST LEAK TEST. FREQUENCY SAME FREQUENCY AS SPECIFIED IN SR 4.4.6.2.2	
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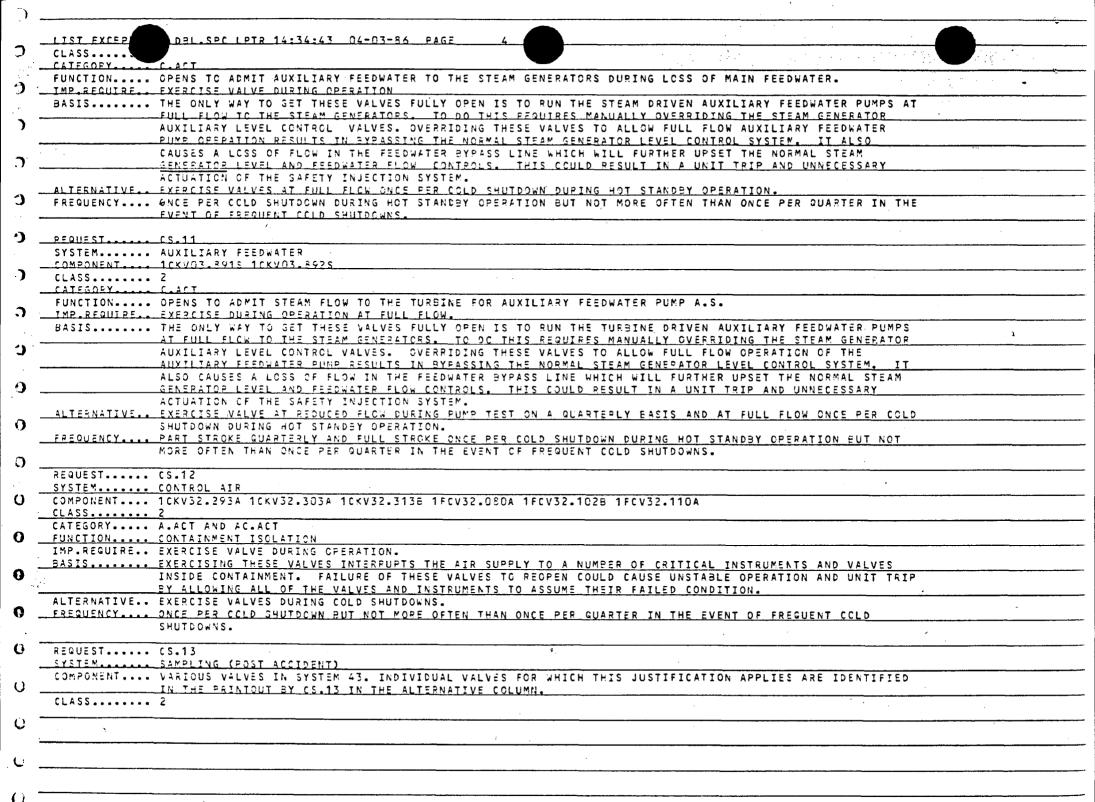
APPENDIX-D COLD SHUTDOWN JUSTIFICATIONS SUMMARY

DEL SPC LPTR 14:34:43 04-03-86 PAGE ITST FXCEPT REQUEST... 5.01 MATH STEAM. SYSTEM. COMPONENT.... 1FCV01.004T 1FCV01.011T 1FCV01.022T 1FCV01.029T CATEGORY B.ACT FUNCTION. ... CLOSES DURING MAIN STEAM LINE EREAK DOWNSTREAM CE VALVE TO PREVENT UNCONTROLLED STEAM GENERATOR BLOWDOWN. EXERCISE VALVE DURING OPERATION BASIS..... VALVES CANNOT BE FULL STROKE TESTED DURING POWER OPERATION DUE TO LOSS OF MAIN STEAM FLOW TO ONE STEAM GENERATOR CRUSING HIGH STEAM LINE DIFFERENTIAL, STEAM FLOW FEED FLOW MISMATCH, AND STEAM Э GENERATOR LEVEL TRANSIENTS, ANY OF WHICH COULD CAUSE A UNIT TRIP AND SAFETY INJECTION. VALVES CAN CHLY BE PART STROKED DURING OPERATION ALTERNATIVE.. FULL STROKE DURING COLD SHUTDOWNS AND FART STROKE DURING OPERATION. PART STROKE QUARTERLY AND FULL STROKE AT COLD SHUTDOWNS BUT NOT MORE OFTEN THAN ONCE PER QUARTER IN FREQUENCY THE EVENT OF FREQUENT COLD SHUTDOWNS. 4) REQUEST..... CS.02 SYSTEM MAIN STEAM COMPONENT.... 1PCV01.C05T 1PCV01.012T 1PCV01.023T 1PCV01.C3CT C1 455 ... CATEGORY S.ACT FUNCTION.... CPENS TO PREVENT SEVERE OVERPRESSURE TRANSIENTS IN THE STEAM GENERATOR IN THE EVENT OF MAIN STEAM PRESSURE TRANSIENTS. IMP RECUTEE - EXERCISE VALVES DURING OPERATION. BASIS..... OPENING THESE VALVES DURING POWER OPERATION MAY CAUSE A STEAM GENERATOR LEVEL TRANSIENT OR MAIN STEAM LINE DIFFERENTIAL PRESSURE TRANSFERT OR STEAM FLOW FEED FLOW MISMATCH. FITHER OF THESE COULD RESULT IN A UNIT TRIP AND UNNECESSARY INITIATION OF THE SAFETY INJECTION SYSTEM. ALTERNATIVE . EXERCISE VALVE DURING COLD SHUTDOWN. FREQUENCY.... ONCE PER COLD SHUTDOWN BUT NOT MORE OFTEN THAN ONCE PER QUARTER IN THE EVENT OF FREQUENT COLD SHLTDOWNS. \mathbf{O} REQUEST.... CS.03 SYSTEM..... MAIN STEAM COMPONENT... 1FCV01.017A 1FCV01.G18B CLASS 2 AND 3 CATEGORY ... B.ACT FUNCTION.... CLOSES TO PREVENT BLOWDOWN OF MAIN STEAM IN THE EVENT OF FAILURE OF THE STEAM DRIVEN AUXILIARY FEEDWATER PUMP OR OF THE MAIN STEAM PIPING TO THE PUMP. IMP.REQUIRE. . EXERCISE VALVE DURING CPERATION. BASIS..... TESTING THESE VALVES TO CLOSE COMPLETELY ISOLATES THE STEAM DRIVEN AUXILIARY FEEDWATER PUMPFROM ITS SOURCE OF STEAM. FAILURE OF EITHER VALVE IN THE CLOSED POSITION WILL CAUSE A LOSS OF HEAT SINK FOR THE LOSS OF ALL AC POWER ACCIDENT. ALTERNATIVE.. TEST AT COLD SHUTDOWNS. FREQUENCY... ONCE PER COLD SHUTDOWN BUT NOT MORE OFTEN THAN ONCE PER QUARTER IN THE EVENT OF FREQUENT COLD SHUTDOWNS. O REQUEST.... CS.04 SYSTEM ... FEEDWATER COMPONENT.... 1 FCV03.033A 1 FCV03.0478 1 FCV03.027A 1 FCV03.100B 1 CKV03.508 1 CKV03.509 1 CKV03.510 1 CKV03.511 CATEGORY.... E.ACT AND C.ACT FUNCTION.... CLOSES TO INTERPUPT MAIN FEEDWATER TO FREVENT A RAPID PRIMARY SIDE COOLDOWN IN THE EVENT OF A MAIN STEAM LINE BREAK AND OR TO PREVENT LOSS OF STEAM GENERATOR WATER INVENTORY IN THE EVENT OF A BREAK ()

A THE WALL RESPONDED THAT ESPENDATE IN THE SERVER THE ISOLATION . JAME PROJUTES PREPENTS MAINES DURING CRESSITION . ASSIS		t t
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CLOSE ALTERNATIVE. EXERCISE VALVE DURING COLD SHUTDOWNS. FREQUENCY GNCF FACH COLD SHUTDOWN BUT NOT MORE OFTEN THAN ONCE PER QUARTER IN THE EVENT OF FREQUENT COLD SHUTDOWNS. REQUEST CS.37 SYSTEM FEEDWATER		ALLOW THE VALVES TO BE TESTED REFORE THE POINT IN OPERATION AT WHICH THEY MAY BE DESCRIBED TO AUTO
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FREQUENCY ONCE FACH COLD SHUTDOWN BUT NOT MORE OFTEN THAN ONCE PER QUARTER IN THE EVENT OF FREQUENT COLD SHUTDOWNS. REQUEST CS.J7 SYSTEM FEEDWATER	ALTERNATIVE -	
REQUEST CS.J7 SYSTEM FEEDWATER		. INCRESE THE FOLD SHITDOWN DIE NOT MODE OFTEN THAN ONCE DED OUADTED IN THE THERE OF FREQUENT AGE.
REQUEST CS.07		SHUTDOWAS.
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STETAMCEE "ETENCEE	REQUEST	CS_07
	CONTURENT	- 110403.630 170403.634 170403.642 170403.643

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DEL_SPC | PTR 14.34:43 | 04-03-86 | PAGE ITST EYCEP 7 CLASS.... CATEGORY ... PACT FUNCTION.... CLOSES TO PREVENT LCSS OF STEAM GENERATOR WATER INVENTORY IN THE EVENT OF A FEEDWATER BYPASS LINE SPEAK -IMP.REQUIRE.. EXERCISE VALVE DURING OPERATION. BASIS EXERCISING VALVE DURING OPERATION WILL CAUSE A PARTIAL LOSS OF FEEDWATER FLOW RESULTING IN PROBABLE STEAM GENERATOR LEVEL TRANSIENTS AND SUBSEQUENT UNIT TRIP AND SAFETY INJECTION SYSTEM ACTUATION. ALTERNATIVE . EXERCISE VALVE DURING COLD SHITDOWNS FREQUENCY ... ONCE PER COLD SHUTDOWN BUT NOT MORE OFTEN THAN ONCE PER QUARTER IN THE EVENT OF FREQUENT COLD SHUTDOWKS. REQUEST CS-08 SYSTEM.... AUXILIARY FEEDWATER COMPONENT 10KVG3 ROSA 10KVO3 ROAR 10KVO3 RIOS CATEGORY C ACT FUNCTION.... OPENS TO ALLOW AUXILIARY FEEDWATER PUMPS TO TAKE SUCTION FROM THE CONDENSATE STORAGE TANK, CLOSES THE COT IS EXHAUSTED TO PROVIDE FLOW BOUNDRY FOR ERCH IMP.REGUIRE.. EXERCISE VALVE DURING OPERATION AT FILL FICE. BASIS THE ONLY WAY TO GET THESE VALVES FULLY OPEN IS TO RUN THE AUXILITARY FEEDWATER PUMPS AT FULL FLOW TO THE STEAM GENERATORS. TO DO THIS REQUIRES MANUALLY OVERRIDING THE STEAM GENERATOR AUXILIARY LEVEL . CONTROL VALVES. CVERRIDING THESE VALVES TO ALLOW FULL FLOW AUXILITARY FEEDWATER PUMP OPERATION RESULTS IN EYPASSING THE NORMAL STEAM GENERATOR LEVEL CONTROL SYSTEM. IT ALSO CAUSES A LOSS OF FLOW IN THE RESDWATER BYPASS LINE WHICH WILL FURTHER UPSET THE NORMAL STEAM GENERATOR LEVEL AND FEEDWATER FLOW CONTROLS. THIS COULD RESULT IN A UNIT TFIP AND UNNECESSARY ACTUATION OF THE SAFETY ALTERNATIVE.. EXERCISE VALVE AT REDUCED FLOW ONCE PER QUARTER DURING THE PUMP TEST AND EXERCISE AT FULL FLOW EACH COLD SHUTDOWN. TEST VALVE TO BACKSEAT GUARTERLY. FREQUENCY.... PART STROKE QUARTERLY AND FULL STROKE AT COLD SHUTDOWN BUT NOT MORE OFTEN THAN ONCE PER QUARTER IN THE EVENT OF EFFCUENT COLD SHUTDOWNS. TEST VALVE TO BACKSEAT QUARTERLY. \circ REQUEST. ... CS.09 SYSTEM.... AUXILIARY FEEDWATER COMPONENT.... 1CKV03.820A 1CKV03.821B 1CKV03.830B 1CKV03.831A 1CKV03.832A 1CKV03.833B 1CKV03.861S 1CKV03.862S 1CKV03.9218 1CKV03.9228 CLASS..... 2 EXCEPT FCR 1CKV03.8618 1CKV03.82CA AND 1CKV03.8213 WHICH ARE CLASS 3. CATEGORY C.ACT FUNCTION.... OPENS TO ADMIT AUXILIARY FEEDWATER TO THE STEAM GENERATORS DURING LOSS OF MAIN FEEDWATER. IMP.REQUIRE.. EXERCISE VALVE DURING OPERATION. BASIS..... THE ONLY WAY TO GET THESE VALVES FULLY OPEN IS TO RUN THE MOTOR DRIVEN AUXILIARY FEEDWATER PUMPS AT FULL FLOW TO THE STEAM GENERATORS. TO DO THIS REQUIRES MANUALLY OVERRIDING THE STEAM GENERATOR AUXILIARY LEVEL CONTROL VALVES. OVERRIDING THESE VALVES TO ALLOW FULL FLOW AUXILIARY FEEDWATER PUMP OPERATION RESULTS IN EYPASSING THE NORMAL STEAM GENERATOR LEVEL CONTROL SYSTEM. IT ALSO CAUSES A LOSS OF FLOW IN THE FEEDWATER BYPASS LINE WHICH WILL FURTHER UPSET THE NORMAL STEAM GENERATOR LEVEL AND FEEDWATER FLOW CONTROLS. THIS COULD RESULT IN A UNIT TRIP AND UNNECESSARY O ACTUATION OF THE SAFETY INJECTION SYSTEM. ALTERNATIVE.. EXERCISE VALVES AT FULL FLOW ONCE PER COLD SHUTDOWN. FREQUENCY.... ONCE PER COLD SHUTDOWN BUT NOT MORE OFTEN THAN ONCE PER QUARTER IN THE EVENT OF FREQUENT COLD SHUTDOWN'S. REQUEST.... CS.10 SYSTEM.... AUXILIARY FEEDWATER COMPONENT.... 1CKVG3.2045 1CKVG3.871A 1CKVC3.372B 1CKVG3.873B 1CKVG3.874A



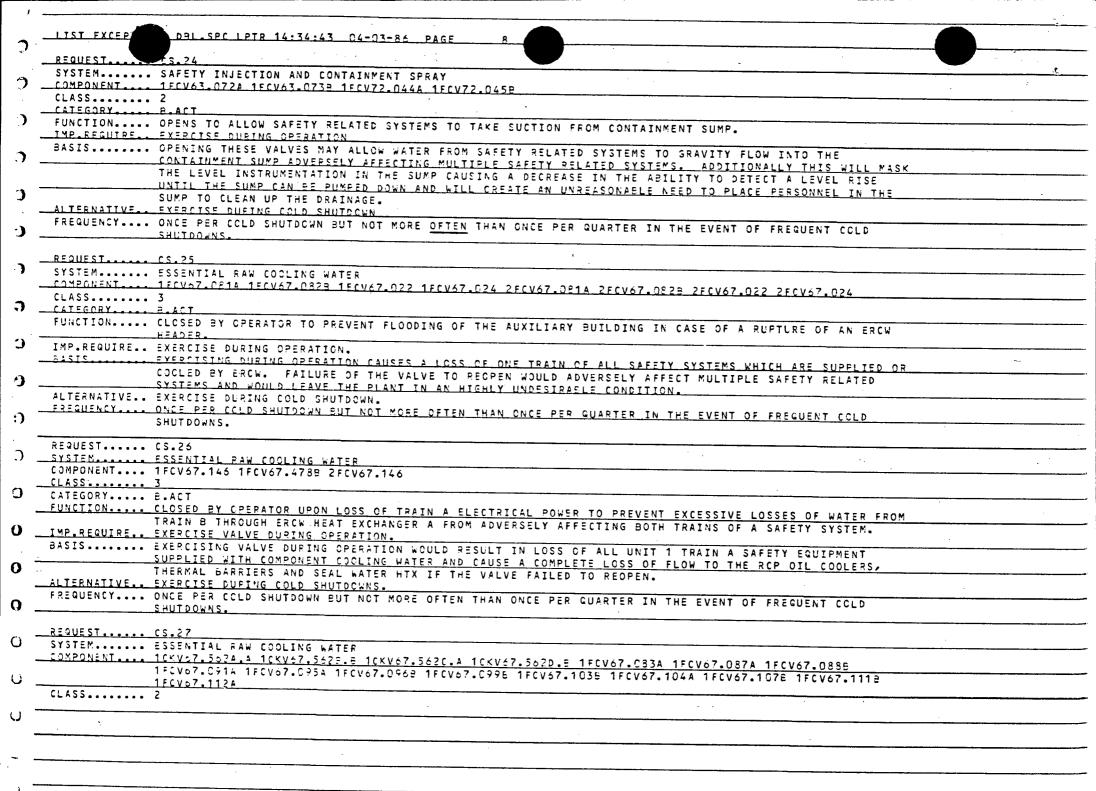
	LIST EXCER	DEL.SPC LPTR 14:34:43 04-03-86 PAGE 5
	CATEGORY	ACT AND AC.ACT
	_FUNCTION	VALVES ARE NORMALLY CLOSED AND MAINTAINED IN THE GLOSED CONDITION FOR CONTAINMENT ISOLATION
o .	• •	PURPOSES. VALVES ARE REQUIRED TO OPEN TO PASS SAMPLE FLOW FROM THE REACTOR BUILDING TO THE POST
•	IMP.REQUIRE	ACCIDENT SAMPLING FACTLITY FOR ANALYSTS OF POST ACCIDENT WATER GUALITY AND CONTENT. EXERCISE THE VALVES DURING OPERATION.
a		THESE VALVES ARE NOT EQUIPPED WITH A CONTAINMENT ISOLATION SIGNAL AND ARE NORMALLY MAINTAINED IN A
• •		DEENERGIZED AND CLOSED CONDITION. TESTING THE VALVES DURING OPERATION WOULD REQUIRE RESTORING BOWER
•		TO THEM AND COULD CONCEIVABLY RESULT IN A VALVE BEING LEFT OPEN CAUSING A BREACH OF CONTAINMENT INTEGRITY.
.	ALTERNATIVE	EXERCISE DURING COLD SHUTDOWNS.
	FREQUENCY	ONCE PER COLD SHUTDOWN NOT TO EXCEED ONCE PER GUARTER IN THE EVENT OF FREQUENT COLD SHUTDOWNS.
)	REQUEST	rs.14
		CHEMICAL AND VOLUME CONTROL
	COMPONENT	1FCV62.0618 1FCV62.063A
•)	CATEGORY	
		CLOSES TO ISOLATE SEAL WATER RETURN ON CONTAINMENT ISOLATION.
•	IMP.REQUIRE	EXERCISE VALVE DURING OPERATION.
		EXERCISING WALVES DURING OPERATION WOULD CAUSE LOSS OF SEAL WATER RETURN AND DAMAGE THE REACTOR
o	ALTEDRATIVE	COCLANT PUMP SEALS CAUSING HIGH SEAL LOSSES WITH CONTAMINATION AND CLEAN UP PROBLEMS. EXERCISE VALVES DURING COLD SHUTDOWNS.
	FREQUENCY	ONCE PER COLD SHUTDOWN BUT NOT MORE OFTEN THAN ONCE PER QUARTER IN THE EVENT OF FREQUENT COLD
		SHUTDOWNS.
o	RECHEST	, , , , , , , , , , , , , , , , , , , ,
•		CS-15 CHEMICAL AND VOLUME CONTROL
') ,	COMPONENT	1FCV62.098A 1FCV62.6993
	CLASS	
o :	CATEGORY	
	1011011011111	CLOSED BY OPERATOR TO ESTABLISH DISCHARGE FLOW FOUNDARY FOR CENTRIFUGAL CHARGING PUMPS DURING ACCIDENT CONDITIONS ONCE IT HAS BEEN ESTABLISHED THAT THE RCS PRESSURE HAS DECAYED TO THE POINT
0		THAT THE CHARGING PUMPS WILL NOT BE DEAD HEADED.
.,	HASTS	EXERCISE VALVE DURING OPERATION.
_		FAILURE OF EITHER VALVE TO REOPEN WOULD AFFECT BOTH TRAINS OF A SAFETY SYSTEM BY ISOLATING THE RECIRCULATION FLOW PATH TO BOTH CHARGING PUMPS. DUPING A SECONDARY SIDE HIGH ENERGY LINE BREAK
)		CONCURRENT WITH FAILURE OF THE REACTOR COCLANT SYSTEM FOWER OPERATED RELIFE VALVES PRIMARY SIDE
-		PRESSURE MAY EXCEED SHUT OFF HEAD OF THE CHARGING FUMPS. IF NO FLOW PATH IS AVAILABLE ROTH PUMPS
0	ALTERNATIVE	COULD SUFFER DAMAGE. REFERENCE NRC IE BULLETIN 39.18. EYERCISE VALVES DURING COLD SHUTDOWNS.
_	FREQUENCY	ONCE PER COLD SHUTDOWN BUT NOT MORE OFTEN THAN ONCE PER QUARTER IN THE EVENT OF FREQUENT COLD
o -		SAWCOTUHS.
•	REQUEST	CC 44
-		CHEMICAL AND VOLUME CONTROL
3 _	COMPONENT	11 CV 62 . 132A 11 CV 62 . 133B
	CLASS	
<u>.</u> -	CATEGORY	
_	IMPEREQUIPE	CLCSES TO ISOLATE VCLUME CONTROL TANK FROM CHARGING PUMP SUCTION DURING SAFETY INJECTION. EXERCISE VALVES DURING OPERATION.
1	5ASIS	EXERCISING VALVES DURING OPERATION RESULTS IN MAKING UP LETDOWN FLOW FROM THE REACTOR COOLANT
<i>•</i> _		SISTEM WITH BITHER CONCENTRATED BORIC ACID OR PRIMARY WATER. EITHER OF THESE MAY CHANGE THE BORON
_		CONCENTRATION IN THE REACTOR CAUSING UNSTABLE UNIT OPERATION.
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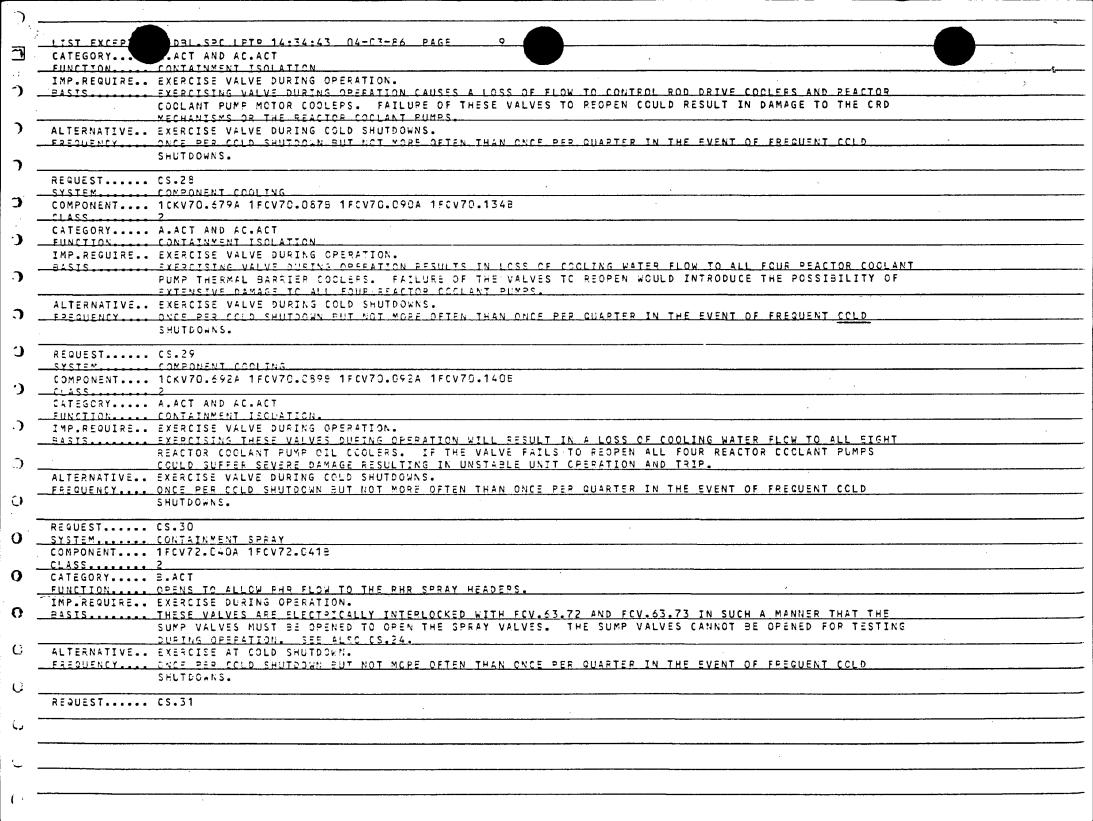
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T VALVES &C	MIT DRI	SPC LPT	TR 07:27:18	04-11-8	36 PAGE	5							
ALVES	3YS	CLASS	DWS.NO	- ccorp	CATGRY	- 517É -	TYPE	A C T	N.POS	TESTS	- ALT'ER-	RELIEF	
LCV03.156.A	03	3	803.2	D.8	B.ACT	4	GL	DIA	С	QT		····	
LCV03.156A.A	03	3	803.2	D.8	B.ACT	2	ANG	DIA	С	QT			
LCV03.164.A	03	3	503.2	C.8	B.ACT	4	GL	DIA	С	QT .		:	
LCV03.164A.A	C 3	3	803.2	C.8	B.ACT	2	ANG	DIA	С	QT			
LCV03.171.B	C3	3	803.2	A . 8	B.ACT	4	GL	DIA	С	QT			
LCV03.171A.E	03	3	803.2	A . 8	3.ACT	2	ANG	DIA	С	QT			
ILCV03.172A	03	3	803.2	F.8	B.ACT	3	GL	DIA	C	QT			
LCV03.173B	03	3	803.2	p.8	P.ACT	3	GL	DIA	С	QT			
LCV03.174E	03	3	803.2	C.8	e.act	3	GL	DIA	С	QT			
ILCV03.175A	C 3	3	803.2	A . 8	5.ACT	3	GL	DIA	С	GT			i
CKV18.556A.A	18	3	840.1	C.2	C.ACT	1.5	CK	SLF	С	cv		RR.27	
CKV18.556A.B	18	3	540 .1	C.2	C.ACT	1.5	CK	SLF	С	CV		RR.27	
CKV18.557E.A	18	3 .	34G.1	C . 2	C.ACT	1.5	CK	SLF	С	cv		RR.27	
CKV18.5573.E	18	3	8401	C • 2	C.ACT	1.5	C K	SLF	С	cv		RP.27	
CKV18.556A.A	18	3	840.1	C • 2	C.ACT	1.5	CK	SLF	С	cv		PR.27	
CKV18.556A.B	18	3	340.1	C • 2	C.ACT	1.5	CK	SLF	С	cv		RR.27	
CKV18.557B.A	18	3	840.1	C • 2	C.ACT	1.5	CK	SLF	С	C V		RR.27	
CKV18.5578.B	18	3	840.1	C . 2	C.ACT	1.5	CK	SLF	С	cv		RR.27	
CKV26.1260	26	2	850.9	A . 9	AC.PAS	4	CK	SLF	С	LT	AJ	PR.12 RR.13	
CKV26.1296	25	2	250.9	3.3	AC.PAS		ск	SLF		 L T	AJ	RR.13	v i ll ′
FCV26.240A	25	2	350.9	A.9	A.ACT	4	G A	MOT	0	QT.LT	AJ	PR.12	
fcv26.2413	-26	-3	- 350.9	0.7	3.ACT	4	- GA	- MCT-	-0				
FCV26.242A	- 26				-B.ACT			MOT		- QT -			
FCV26.243A	-26		850.9							<u> </u>		R.P 1 2	

LIST EXCEP DBL.SPC LPTR 14:34:43 04-03-86 PAGE ALTERNATIV XERCISE VALVES DURING COLD SHUTDOWN. FREQUENCY... ONCE PER COLD SHUTDOWN BUT NOT MORE OFTEN THAN ONCE PER QUARTER IN THE EVENT OF PREQUENT COLD SHUTDOWNS. 9 REQUEST.... CS.17 SYSTEM.... CHEMICAL AND VOLUME CONTROL COMPONENT.... 1LCV62.135A 1LCV62.136B C! ASS CATEGORY B.ACT FUNCTION ---- OPENS TO ALLOW CHARGING PUMPS TO TAKE SUCTION FROM RWST IMP.REQUIRE.. EXERCISE DURING OPERATION BASIS CYCLING THESE VALVES DURING OPERATION RESULTS IN ALLOWING THE CHARGING PUMPS TO TAKE SUCTION FROM THE RWST FOR NORMAL CHARGING REQUIREMENTS. THIS WILL RESULT IN ADDITION OF BORATED WATER WHICH HAS A DIFFERENT SORON CONCENTRATION THAN THAT IN THE PEACTOR COOLANT SYSTEM SINCE THE LIKELYHOOD OF BOTH THE RWST AND THE RCS BEING AT THE SAME BORON CONCENTRATION AT THE SAME TIME IS VERY SMALL. THE CHANGE IN BORON CONCENTRATION IN THE RCS CAUSED BY MAKEUP FROM THE RWST DURING TESTING WOULD CAUSE UNSTABLE UNIT OPERATION, ESPECIALLY IF EITHER OF THE VALVES FAILED TO RECLOSE. ALTERNATIVE .. EXERCISE DURING COLD SHUTDOWNS. FREQUENCY.... ONCE PER COLD SHUTDOWN BUT NOT MORE OFTEN THAN ONCE PER QUARTER IN THE EVENT OF FREQUENT COLD SHUTDOWNS • PEQUEST.... CS.18 SYSTEM..... SAFETY INJECTION COMPONENT.... 1CKV63.632A 1CKV63.633B 1CKV63.634A 1CKV63.635B CATEGORY AC ACT FUNCTION.... OPENS TO ADMIT FLOW FROM RHR PUMPS TO REACTOR DURING LOCA OR POST LOCA RECOVERY. IMP_REQUIRE. EXERCISE DURING OPERATION. BASIS..... THESE VALVES ARE IN THE RESIDUAL HEAT REMOVAL FUMP INJECTION LINES AND THE RHR PUMPS DO NOT DEVELOP SUFFICIENT HEAD TO CPEN THE VALVES DURING CPERATION. Ω ALTERNATIVE.. CYCLE VALVES DURING COLD SHUTDOWN. FREQUENCY.... ONCE PER COLD SHUTDOWN BUT NOT MORE OFTEN THAN ONCE PER QUARTER IN THE EVENT OF FREQUENT COLD SHUTDOWNS. 0 REQUEST.... CS-19 SYSTEM..... SAFETY INJECTION COMPONENT.... 1FCV63.CO1A CLASS..... 2 CATEGORY B.ACT FUNCTION.... CLOSED WHEN RESIDUAL HEAT PEMOVAL SYSTEM SUCTION IS TRANSFERRED TO THE CONTAINMENT SUMP FOLLOWING A LOCA. IMP.REQUIRE. EXERCISE VALVE DURING OPERATION. BASIS..... EXERCISING VALVE DURING OPERATION RESULTS IN LOSING SUCTION FROM RWST TO BOTH TRAINS OF RESIDUAL HEAT REMOVAL. IF VALVE FAILS TO REOPEN BOTH TRAINS OF A SAFETY SYSTEM WOULD BE MADE INOPERABLE. ALTERNATIVE.. EXERCISE VALVE DURING COLD SHUTDOWN. FREQUENCY.... ONCE PER COLD SHUTDOWN BUT NOT MORE OFTEN THAN ONCE PER QUARTER IN THE EVENT OF FREQUENT COLD. SHUTDOWNS. REQUEST.... CS.20 SYSTEM.... SAFETY INJECTION COMPONENT.... 1FCVoE.CG3A CATEGORY.... B.ACT Q

LIST EXCE DRI SPC | PTR 14-34-43 D4-03-86 PAGE FUNCTION. VALVE IS CLOSED TO PREVENT CONTAMINATION OF RWST N ST PUMP SUCTION IS TRANSFERRED TO RHR PUMP DISCHARGE FOLLOWING A LOCA WITH RHR TAKING SUCTION FROM CONTAINMENT SUMP IMP.REQUIRE.. EXERCISE VALVE DURING OPERATION. EXERCISING VALVE DURING OPERATION RESULTS IN ISOLATING THE RECIRCULATION LINE TO BOTH TRAINS OF SAFETY INJECTION PUMPS. FAILURE OF THE VALVE TO REOPEN WOULD MAKE BOTH TRAINS OF A SAFETY SYSTEM THORFRARIE ALTERNATIVE.. EXERCISE VALVE DURING COLD SHUTDOWNS. FREQUENCY. ONCE PER COLD SHUTDOWN BUT NOT MORE OFTEN THAN ONCE PER GUARTER IN THE EVENT OF EDECHENT COLD SHUTDOWNS 7 REQUEST.... CS.21 SYSTEM ... SAFETY INTECTION ~ COMPONENT ... 1 FCV63 - DOSE 2 2 2 2 CATEGORY B.ACT FUNCTION - - - CLOSED WHEN THE SAFETY INJECTION PUMP SUCTION IS TRANSFERRED TO THE RESIDUAL HEAT REMOVAL PUMP DISCHARGE FOLLOWING A LOCAL IMP REQUIRE. EXERCISE VALVE DURING OPERATION. BASIS..... EXERCISING VALVE DURING OPERATION EFFECTS BOTH TRAINS OF A SAFETY SYSTEM. FAILURE OF THE VALVE TO RECPEN WHILD CAUSE A TOTAL LOSS OF SYSTEM FUNCTION. ALTERNATIVE.. EXERCISE VALVE DURING COLD SHUTDOWN. FREQUENCY ... ONCE PER COLD SHUTDOWN BUT NOT MORE OFTEN THAN ONCE PER QUARTER IN THE EVENT OF FREQUENT COLD SHUTDOWNS. REQUEST.... CS.22 SAFFTY THIFTTON CYCTEM COMPONENT.... 1FCV63.008A 1FCV63.011B 22413 CATEGORY.... B.ACT FUNCTION.... CRENED TO ESTABLISH SUCTION FLOW PATH TO SAFETY INJECTION AND OR CENTRIFUGAL CHARGING PUMPS DURING THE RECIRCULATION FROM CONTAINMENT SUMP PHASE OF POST LOCA RECOVERY. IMP. REQUIRE. - EXERCISE VALVES DURING OPERATION. BASIS..... BOTH VALVES ARE ELECTRICALLY INTERLOCKED WITH THE SAFETY INJECTION PUMP RECIRCULATION ISOLATION VALVES 1FCV63.003A 1FCV63.C045 AND 1FCV63.175B IN SUCH A MANNER THAT BOTH TRAINS OF SAFETY INJECTION PUMPS MUST HAVE THEIR RECIRCULATION FLOW PATH ISCLATED TO CYCLE 1FCV63.0C8A OR 1FCV63.0116. ISCLATION OF THESE RECIRCULATION PATHS ADVERSELY AFFECTS BOTH TRAINS OF A SAFETY SYSTEM AND COULD CAUSE FAILURE OF BOTH TRAINS. SEE ALSO CS.20. ALTERNATIVE. EXERCISE AT COLD_SHUTDOWN. FREQUENCY... ONCE PER COLD SHUTDOWN BUT NOT MORE OFTEN THAN ONCE PER QUARTER IN THE EVENT OF FREQUENT COLD __ SHUTDOWNS. REQUEST. CS.23 SYSTEM..... SAFETY INJECTION SYSTEM COMPONENT 1 FCV63 C225 CLASS..... 2 __CATEGORY.... B.ACT FUNCTION.... CLOSED WHEN SAFETY INJECTION PUMPS ARE PLACED ON HOT LEG RECIRCULATION AFTER A LOCA. IMP_BEQUIRE. EXERCISE VALVE DUBING OPERATION. SASIS..... EXERCISING VALVE DURING OPERATION ISCLATES BOTH TRAINS OF SAFETY INJECTION FROM THEIR NORMAL FLOW PATH TO THE COLD LEGS. FAILURE OF THE VALVE TO REOPEN RESULTS IN TOTAL LOSS OF SYSTEM FUNCTION. ALTERNATIVE.. EXERCISE VALVE DURING COLD SHUTDOWNS. FREQUENCY... SUCE PER COLD SHUTDOWN BUT NOT MORE OFTEN THAN ONCE PER GUARTER IN THE EVENT OF FREQUENT COLD SHUTDOWNS.





DBL.SPC LPTR 14:34:43 04-03-86 PAGE ITST FYCEP ESTRUAL HEAT REMOVAL SYSTEM COMPONENT ... 1 CKYZ4 - 5144 1 CKYZ4 - 5152 CLASS.... 2 CATEGORY C.ACT FUNCTION OPENS TO ADMIT FLOW FROM RHR PUMPS TO THE REACTOR COLD LEGS DURING LOCA-THE PECULTER SYRECTSE VALVE CHRING OPERATION AT FULL FLOW. BASIS..... RHR PUMPS DO NOT DEVELOP SUFFICIENT HEAD TO INJECT TO VESSEL AT OPERATING PRESSURES. FULL FLOW CANNOT BE ACHTEVED ON PUMP RECTROULATION LINES. ALTERNATIVE. PART STROKE VALVE GUARTERLY DURING PUMP TEST ON RECIRCULATION LINE. FULL STROKE AT COLD SHUTDOWN. FREQUENCY ... PART STECKE ONCE PER QUARTER AND FULL STRCKE CHCE PER COLD SHUTDOWN BUT NOT MORE CETEN THAN ONCE PER QUARTER IN THE EVENT OF FREQUENT COLD SHUTDOWNS. 4 REQUEST.... CS.32 SYSTEM RESIDUAL HEAT PEMOVAL COMPONENT.... 1FCV74.CO1A 1FCV74.CO29 1FCV74.GO8A 1FCV74.CO98 CATEGORY ---- A.ACT FUNCTION.... CLOSES TO ISOLATE LOW PRESSURE ARR PIPING FROM HIGH PRESSURE OF THE REACTOR COOLANT SYSTEM. IMPLREQUIREL. EXERCISE VALVE DURING OPERATION. BASIS..... VALVES HAVE INTERLOCKS TO PREVENT OPENING THEM WHEN RCS IS ABOVE THE RHR DESIGN PRESSURE. EXERCISING THE VALVES DURING OPERATION RESULTS IN OVERFPESSURIZING RHR CAUSING A LCSS OF BCTH . TRAINS OF A SAFETY SYSTEM. ALTERNATIVE. EXERCISE DURING COLD SHUTDOWNS. FREQUENCY.... ONCE PER COLD SHUTDOWN BUT NOT MORE OFTEN THAN ONCE PER QUARTER IN THE EVENT OF FREQUENT COLD 1 SHUTDOWNS REQUEST.... CS.33 SYSTEM..... WASTE DISPOSAL COMPONENT.... 1CKV77.849 1CKV77.868 CATEGORY AC.ACT FUNCTION.... CLOSES TO PREVENT OUTLEAKAGE FROM REACTOR BUILDING THPOUGH THE PRESSURIZER RELIEF TANK OR STEAM GENERATOR LAYUF OR COLD LEG ACCUMULATOR NITROGEN SUPPLY LINES. O IMP. REQUIRE. EXERCISE DUFING OPERATION. BASIS..... CYCLING THESE VALVES DURING POWER OPERATION INTERPUPTS THE NITROGEN SUPPLY INSIDE CONTAINMENT TO A NUMBER OF COMPONENTS AND SYSTEMS. ADDITIONALLY PERSONNEL RADIATION EXPOSURE AND VALVE INACCESSIBILITY ALSO PROHIBIT QUARTERLY EXERCISING OF THESE VALVES. ALTERNATIVE.. EXERCISE AT COLD SHUTDOWN. FREQUENCY.... ONCE PER COLD SHUTDOWN NOT TO EXCEED ONCE PER QUARTER IN THE EVENT OF FREQUENT COLD SHUTDOWNS. G REQUEST.... CS.34 SYSTEM.... PRIMARY WATER COMPONENT 1 CKVE1 . 502 CATEGORY.... AC.ACT FUNCTION. ... CLOSES TO PREVENT OUTLEAKAGE FROM PEACTOR BUILDING THROUGH THE REACTOR COOLANT PUMP STANDPIPE AND PRESSURIZER RELIEF TANK SPRAY HEADER SUPPLY LINE. IMPUREGUIRE. EXSECTSE OURTHO OPERATION. BASIS..... EXERCIBING THIS VALUE PESULTS IN LOSS OF PRIMARY WATER TO THE RCP STANDPIPES AND PRT. PERSONNEL RESISTION EXPOSURES AND VALVE INACCESSIFILITY ALSO PROMIPIT EXERCISING THIS VALVE GUARTERLY. ALTERNATIVE. . EXERCISE DUAING COLD SHUTDOWN. FREQUENCY ... SINCE PER COLD SHUTDOWN NOT TO EXCEED ONCE PER GUAPTER IN THE EVENT OF FREQUENT COLD SHUTDOWNS.

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1	LIST EXCER	DSI SPC 1PTR 14:34:43 D4-03-84 PAGE 11					
5	REQUEST	RESIDUAL HEAT REMOVAL					·
์ ก		. 1FCV74.033A 1FCV74.035B			-	3	
· ·	CATEGORY	B.ACT CREN DURING ECCS INJECTION MODE TO ALLOW EITHER TRAIN RHE					
o	FUNC+ LUNG	INJECTION LINES. CLOSED DURING RECIRCULATION MODE AFTER A ALLOW ONE TRAIN INJECTION AND OTHER TRAIN SUPPLYING FOCS	ACCIDENT TO HAVE TRAIN SEPARABILITY	<u>FCUR RHR</u> f TO			
o .	IMP.REQUIRE	EXERCISE VALVE DURING OPERATION.					
• • •	[THE RESIDUAL HEAT REMOVAL SYSTEM WAS DESIGNED AND ANALYZE FOUR COLD LEGS. CLOSURE OF EITHEP OF THESE VALVES CAUSES	OPERATION IN AN UNANALYZED CONDIT	I TO ALL			
o -		ISCLATING TWO GE THE FOUR COLD LEGS. EXERCISE DURING COLD SHUTDOWN.				 	
o .	FREQUENCY	ONCE PER COLD SHUTDOWN PUT NOT MORE OFTEN THAN ONCE PER S SHUTDOWNS.	QUARTER IN THE EVENT OF FREQUENT CO	:LD	<u> </u>		
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•		- REACTOR COCLANT SYSTEM - 1FSV68.394 1FSV68.395 1FSV68.396 1FSV68.397 1PCV68.340A.A	A 1PCV68.334				
٠ .	CATEGORY						
O.	FUNCTION	PCV'S ARE POWER ORERATED RELIEF VALVES ON THE PRESSURITER CONDITIONS DURING START-UP AND SHUT DOWN.	3 WHICH FUNCTION TO CONTROL OVERPRE	SSURE			
o -	JMP.REQUIRE	. EXERCISE VALVE GUARTERLY. . THESE ARE TARGET ROCK SOLENOID OPERATED VALVES AND HAVE A	A REPUTATION FOR STICKING CPEN. TH		`		
- -		CONSEQUENCES OF A VALVE STICKING OPEN ARE CONSIDERABLE. WOULD DEPRIVE THE PLANT OF ONE TRAIN OF OVERPRESSURIZATION	<u>IE A PORV STICKS CPEN DURING OPERA</u> ON PROTECTION WHICH WOULD BE REQUIS	ATION IT			
) .		DUFING THE SUBSECUENT SHUTDOWN FOR REPAIR. FAILURE OF A DEGRADE THE ABILITY TO CONTROL RCS HEAD VENTING DURING PO	OST ACCIDENT CONDITIONS.	EVERELY			
O -	FREQUENCY	PORV'S TO BE TESTED AT EACH COLD SHUTDOWN PROVIDING THREE	MONTHS HAVE PASSED SINCE THE PREV	IOUS			
_		TEST. PORY'S WILL NOT BE SHELLECT TO THE SEQUENTIAL TEST! ACCOMPANYING NARRATIVE BUT WOULD BE TESTED AT EACH COLD S	SHUTDOWN PROVIDED THREE MONTHS HAD	PASSED			
O _		SINCE THE FREVIOUS TEST. HEAD VENT VALVES WOULD BE TESTE ACCOMPANYING NARRATIVE.	D IN ACCORDANCE WITH PARAGRAPH 3.1	C OF THE			
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