

EN DES CALCULATIONS

TITLE EVALUATION OF BASEPLATE RIGIDITY REQUIREMENTS				UNIT SYSTEM(S)	PLANT/UNIT <i>All units</i> SAR SECTION(S)
PREPARING ORGANIZATION CEB		REV R0	(FOR MEDS USE) <i>840229A0029</i>		MEDS ACCESSION NUMBER <i>CEB '84 0227 001</i>
APPLICABLE DESIGN DOCUMENTS DS-C1.7.1	BRANCH/PROJECT IDENTIFIERS <i>CSG-85-001</i>	REV R1	<i>840613C0022</i>		CEB '84 0522 011
		REV R2			B41 '85 0731 002
KEY NOUNS Baseplates Expansion Anchors		REV R3			
REV R0	REV R1	REV R2	REV R3	STATEMENT OF PROBLEM Civil Design Standard DS-C1.7.1 for General Anchorage to Concrete - Determination of Tensile Loads for Expansion Anchors - Evaluation of Plate Rigidity Requirement for Use of Rigid Baseplate Analysis	
DATE <i>2/24/84</i>	PREPARED <i>J.B. Ramsey</i>	SUBMITTED <i>J.H. Perry</i>	APPROVED <i>C. Hildreth</i>		
CHECKED <i>J.B. Ramsey</i>	SUBMITTED <i>J.H. Perry</i>	APPROVED <i>Mann G. Coney</i>	SUBMITTED <i>C. Hildreth</i>		
ATTACHMENTS MICROFILMED:					
LIST ALL PAGES * ADDED BY THIS REV:		PAGES 401 THRU 402			
LIST ALL PAGES * DELETED BY THIS REV:					
LIST ALL PAGES * CHANGED BY THIS REV:		PAGES 1-3			

ABSTRACT

To evaluate the requirements for use of rigid plate analysis given in DS-C1.7.1, four sizes of plates were analyzed. The plates were sized to produce edge distances from the face of the attachment of 4- and 6-plate thicknesses. A pattern of eight expansion anchors was used on all of the plates. Two load conditions, axial load only and bi-axial moments only, were applied to the plates through a centered attachment. Analysis was performed using the CASD BAP program (a rigid analysis program) and Baseplate II (a finite element flexible analysis program). The results were compared to show the requirements for rigid baseplate analysis given in design Design Standard DS-C1.7.1 are acceptable.

Computer output on microfilm roll # 50100

R1 Clarified statement on page 2

R2 ADDITIONAL CALCULATIONS WERE ADDED FOR THE EVALUATION OF THE EFFECTS OF COMBINED AXIAL (TENSION) AND BI-AXIAL BENDING ON THE REQUIREMENTS OF RIGID PLATE ANALYSIS.

Please return originals to NHL Perry (W9B108)

EVALUATION OF BASEPLATE RIGIDITY REQUIREMENTS

DS-C1.7.1

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| R2

SHEET 1 OF 40
EVALUATION OF BASEPLATE
RIGIDITY REQUIREMENTS
COMPUTED TBR DATE 7/30/85
CHECKED LS DATE 7-30-85

EVALUATION OF BASEPLATE RIGIDITY REQUIREMENTS

DS-C1.7.1

PURPOSE

To evaluate the baseplate rigidity requirements given in Design Standard DS-C1.7.1, and to show that the requirements for baseplate analysis give acceptable anchor loads.

ASSUMPTIONS

1. An average anchor stiffness of 100 k/in was assumed for a 3/4-inch-diameter expansion anchor. A stiffness of 300 k/in was also used in the evaluation.
2. 3/4-inch-diameter self-drilling expansion anchors were used for the rigid evaluation.

DISCUSSION

The plates were sized to give the required distance between the face of the attachment and the edge of the plate. An 8-bolt pattern was selected to obtain varied spacings between the attachment and the anchors. For the smaller plates, 10-inch and 13-inch, the closer anchor spacings would be unacceptable with respect to concrete capacity but are conservative with respect to anchor load distribution. The configurations of plate size, anchor spacings, attachment size, and applied loads were used only for this evaluation and do not represent actual designs. For some of the configurations, the stress in the plate and tube section exceeds normal allowables. However, for this comparative analysis plate, stresses do not affect the results.

Table 1 summarizes the results from the evaluation. The rigid method for plates loaded with moment gives conservative anchor loads for the 4t edge distance and a $K_t=100$ k/in. A 4t extension with an anchor stiffness of 300 k/in only under estimates the anchor load by 4 percent.

For the axial load condition, the flexible analysis will always give higher anchor loads than a rigid plate analysis unless all anchors are equidistant from the attachment. Even a smaller edge distance of 2t as given in the NCR 79-02 Bulletin will give an underestimation of the anchor loads by a few percent. For an anchor stiffness of 100 k/in, a rigid plate analysis for a plate with a 4t extension will result in an underestimation of the anchor load by only 5 percent.

| RI

CONCLUSION

Based on the above discussion, the 4t limitation for use of rigid plate analysis given in DS-C1.7.1 is acceptable for expansion anchors.

SHEET 2 OF 40
EVALUATION OF BASEPLATE
RIGIDITY REQUIREMENTS
COMPUTED TBL DATE 5/22/84
CHECKED Esk DATE 5/22/84

EVALUATION OF BASEPLATE RIGIDITY REQUIREMENTS

DS-C1.7.1

TABLE 1

Plate Size	Edge Dist.	CASDBAP	Maximum Anchor Loadings, kips			
			BASEPLATE II K = 100 k/in	*	BASEPLATE II K = 300 k/in	*
Bi-Axial Moment Loading						
10x10x3/4	4t	4.96	4.30	+15	4.78	+ 4
13x13x3/4	6t	4.46	4.44	-	4.51	- 1
16x16x1-1/2	4t	3.90	3.62	+ 8	4.06	- 4
22x22x1-1/2	6t	3.44	3.66	- 6	3.68	- 7
Axial Loading						
10x10x3/4	4t	2.50	2.62	- 5	2.82	-11
13x13x3/4	6t	2.88	3.35	-14	4.03	-29
16x16x1-1/2	4t	3.25	3.43	- 5	3.74	-13
22x22x1-1/2	6t	3.75	4.26	-12	5.03	-25
Combined Axial and Bi-axial Moment Loading						
10x10x3/4	4t	5.11	4.44	+15	4.91	+ 4
13x13x3/4	6t	3.58	3.53	+ 1	3.35	+ 7
16x16x1-1/2	4t	2.75	2.55	+ 8	2.83	- 3
22x22x1-1/2	6t	1.88	1.95	- 4	1.93	- 3

* % = ((Rigid-Flexible)/Flexible) x 100%

SHEET 3 OF 40EVALUATION OF BASEPLATERIGIDITY REQUIREMENTSCOMPUTED FBR DATE 7/30/85CHECKED LS DATE 7-30-85

EVALUATION OF BASEPLATE RIGIDITY REQUIREMENTS

DS-CI.7.1

REFERENCES

1. TVA Civil Design Standard DS-CI.7.1, Revision 1 Concrete Anchorages.
2. TVA Computer Program "CASDBAP" rigid baseplate analysis. TVA program identification number 262256.
3. Cybernet Services computer program "BASEPLATE II" finite element flexible plate analysis. BASEPLATE II User Manual Publication number 84002770.

SHEET 4 OF 40

EVALUATION OF BASEPLATE
RIGIDITY REQUIREMENTS
COMPUTED TBL DATE 2/10/84
CHECKED JSL DATE 2/13/84

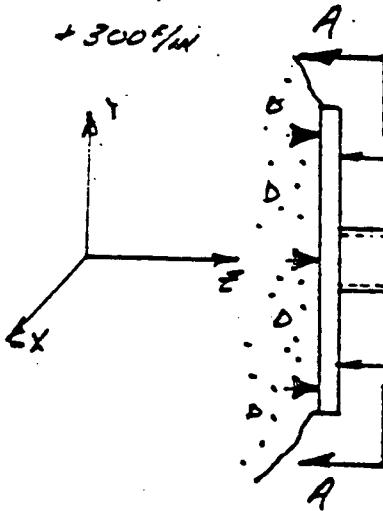
EVALUATION OF BASEPLATE RIGIDITY
REQUIREMENTS

5 of 40
DS-C1.7.1

COMPUTED TAR DATE 1/21/84
CHECKED G.H. DATE 1/31/84

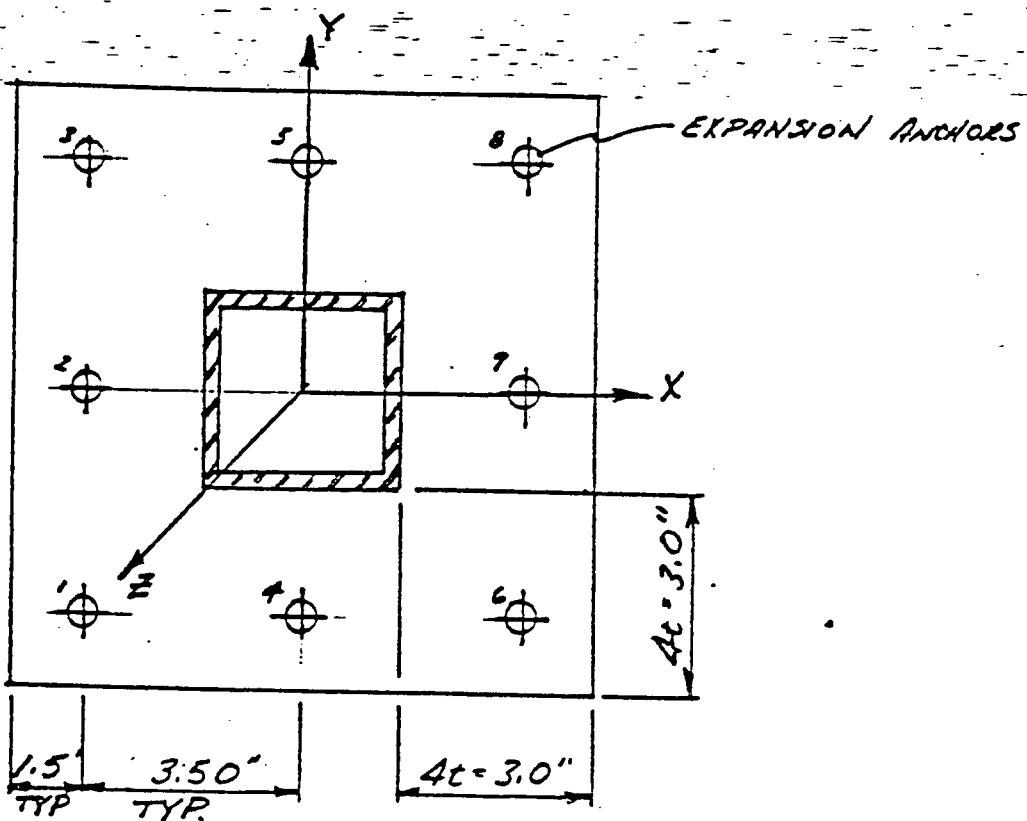
PLATE SIZE - 10" x 10" x 3/4"

$K_c = 100 \text{ kN}$
 $+ 300 \text{ kN}$



LOAD POINT

LOADS:
 $F_x = 1000 \text{ kN}$
 $F_y = -1000 \text{ kN}$
 $F_z = 0$



SECTION A-A

EVALUATION OF BASEPLATE RIGIDITY
REQUIREMENTS

DS-C1.7.1

COMPUTED TBR DATE 1/31/84
CHECKED PSL DATE 1/31/84

SUMMARY OF RESULTS
FOR PLATE SIZE 10"X10"X $\frac{3}{4}$ "

ANCHOR LOADS

ANCHOR NUMBER	RIGID KIPS	FLEXIBLE, KIPS	
		K _f = 100% _{min}	K _f = 300% _{min}
1	1.22	1.55	1.36
2	3.09	3.06	3.53
3	4.96	4.30	4.78
4	0	.34	0
5	3.09	3.06	3.53
6	0	0	0
7	0	.34	0
8	1.22	1.55	1.36

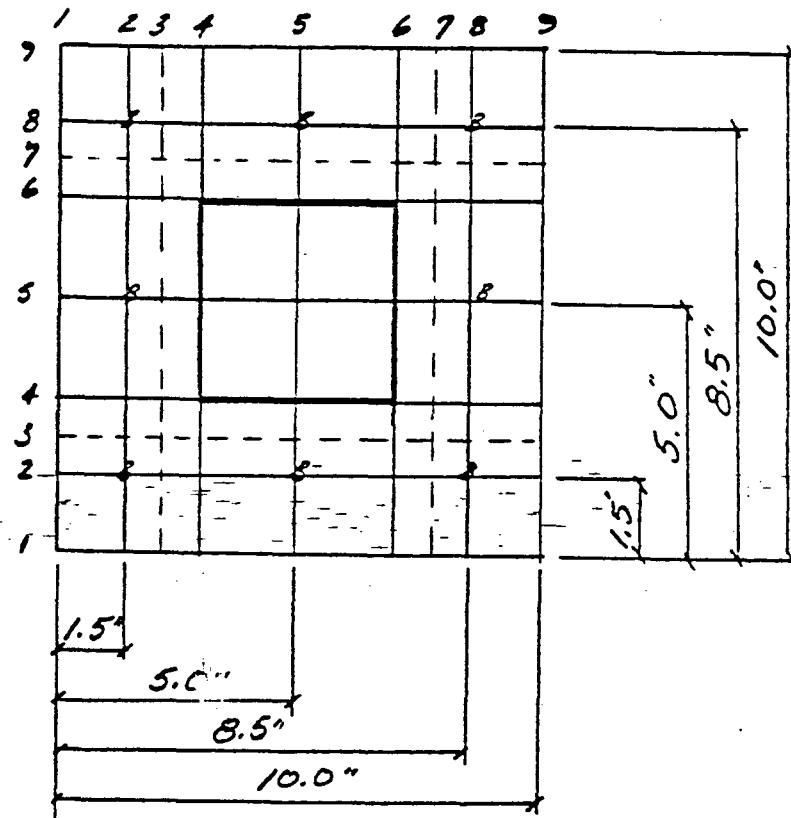
DS-CI.7.1

EVALUATION OF BASEPLATE RIGIDITY
REQUIREMENTS

COMPUTED TOR DATE 1/29/84
 CHECKED 9th DATE 1/31/84

BASEPLATE II (FINITE ELEMENT) MODEL

2 10x10" 3/4"
 $K_t = 100 \text{ k/in}, 300 \text{ k/in}$



1ST

84/01/21. 07.27.59.
PROGRAM DAP10

00100 1,4,UM,0
00110 3,9,NC,1,5
00120 10,10,1,1
00130 8
00140 SD,.75,1,5,1,5
00150 SD,.75,1,5,5,0
00160 SD,.75,1,5,8,5
00170 SD,.75,5,0,1,5
00180 SD,.75,5,0,8,5
00190 SD,.75,8,5,1,5
00200 SD,.75,8,5,5,0
00210 SD,.75,8,5,8,5
00220 4,4,S,5,5,0
00230 0,0,0,5,83,5,83,0
READY.

SHEET 8 OF 40

EVALUATION OF DESIGN

Boundary Requirements

COMPUTED TBE DATE 1/21/84

CHECKED AK DATE 1/3/84

READY.

84/01/31. 07.29.30.
PROGRAM CASDOUT

WIDTH OF PLATE = 10 INCHES
LENGTH OF PLATE = 10 INCHES
MODULAR RATIO = 9

ANCHOR NUMBER	AREA IN	X ORDINATE IN	Y ORDINATE IN
1	.334	1.5	1.5
2	.334	1.5	5
3	.334	1.5	8.5
4	.334	5	1.5
5	.334	5	8.5
6	.334	8.5	1.5
7	.334	8.5	5
8	.334	8.5	8.5

LOAD CONDITION NUMBER = 1

ATTACHMENT 1
VERT LOAD = 0 KIPS LOCATION X = 5 INCHES Y = 5 INCHES
APPLIED MOMENT ABOUT Y AXIS = 5.83 KIP FEET
APPLIED MOMENT ABOUT X AXIS = 5.83 KIP FEET

SUMMATION OF APPLIED LOADS FOR 1 ATTACHMENT(S) = 0 KIP(S)
TRANSLATED MOMENT CENTERLINE ABOUT Y AXIS = 5.83 KIP FEET
TRANSLATED MOMENT CENTERLINE ABOUT X AXIS = 5.83 KIP FEET

PARTIAL PRESSURE CASE

CONCRETE PRESSURE = (61)
C2 = -1.37

CONCRETE PRESSURE FORCE, CF = -13.6 KIPS
LOCATION IN X-DIRECTION = 6.07 INCHES
LOCATION IN Y-DIRECTION = 1.93 INCHES

FRICITION SHEAR CAPACITY, SF = 6.8 KIPS

PRESSURE BULB GEOMETRY
Z3 = 7.71
Z6 = 7.71

ANCHOR NUMBER	STRESS GROSS AREA (KSI)	LOAD KIPS
1	3.86	1.22
2	9.86	3.09
3	14.86	4.96
5	9.28	3.69
8	3.56	1.22

SHEET 9 OF 40
EVALUATION OF EXISTING
RIGIDITY REQUIREMENTS
COMPUTED BY DATE 1/21/84
CHECKED BY DATE 1/31/84

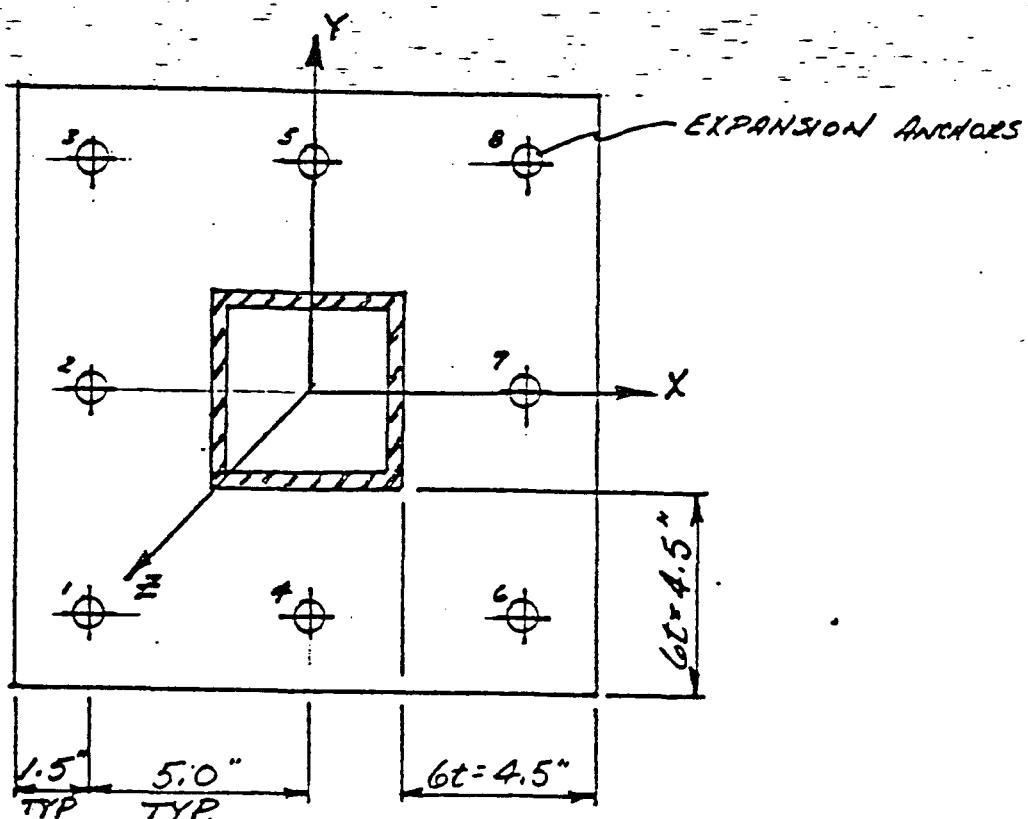
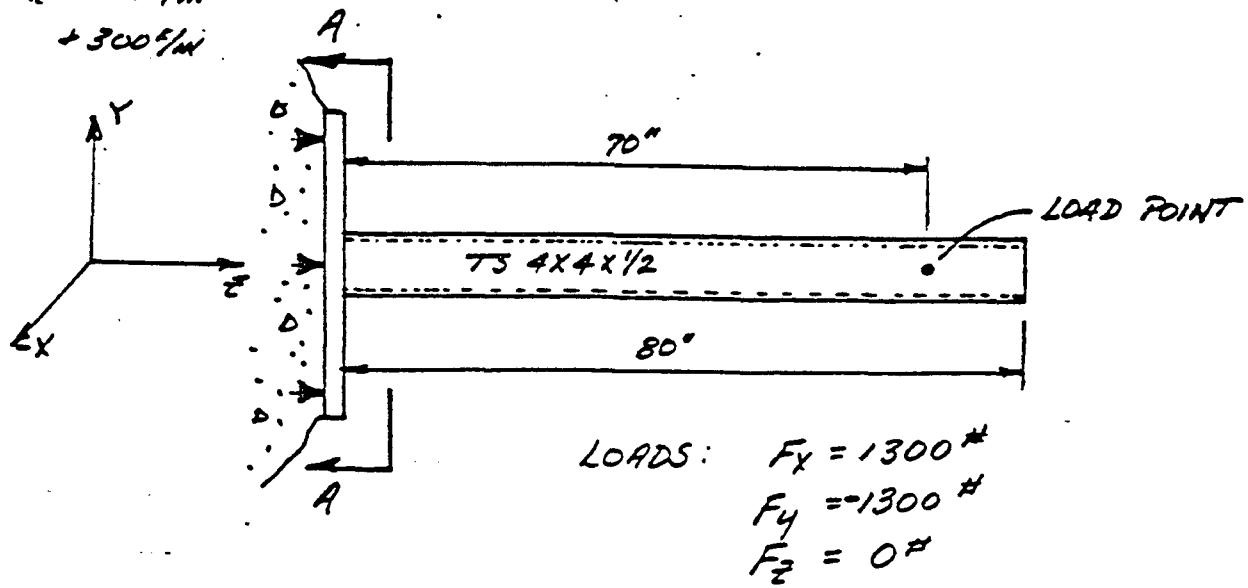
EVALUATION OF BASEPLATE RIGIDITY
REQUIREMENTS

10 \times 40
DS-CI.7.1

COMPUTED TBR DATE 1/31/84
CHECKED 95% DATE 1/31/84

PLATE SIZE - 13" x 13" x 3/4"

$K_c = 100 \text{ kN}$
 $+ 300 \text{ kN}$



EVALUATION OF BASEPLATE RIGIDITY
REQUIREMENTS

SHEET 11 OF 40

DS-C1.7.1

COMPUTED TBC DATE 1/31/8
CHECKED EAK DATE 1/31/8

SUMMARY OF RESULTS
FOR PLATE SIZE $13 \times 13 \times \frac{3}{4}$ "

ANCHOR LOADS

ANCHOR NUMBER	RIGID KIPS	FLEXIBLE, KIPS	
		$K_F = 100\%w$	$K_F = 300\%w$
1	1.28	1.27	.98
2	2.87	3.57	4.51
3	4.46	4.44	4.23
4	0	.21	.04
5	2.87	3.57	4.51
6	0	0	0
7	0	.21	.04
8	1.28	1.27	.98

EVALUATION OF BASEPLATE RIGIDITY
REQUIREMENTS

DS-CI-7.1

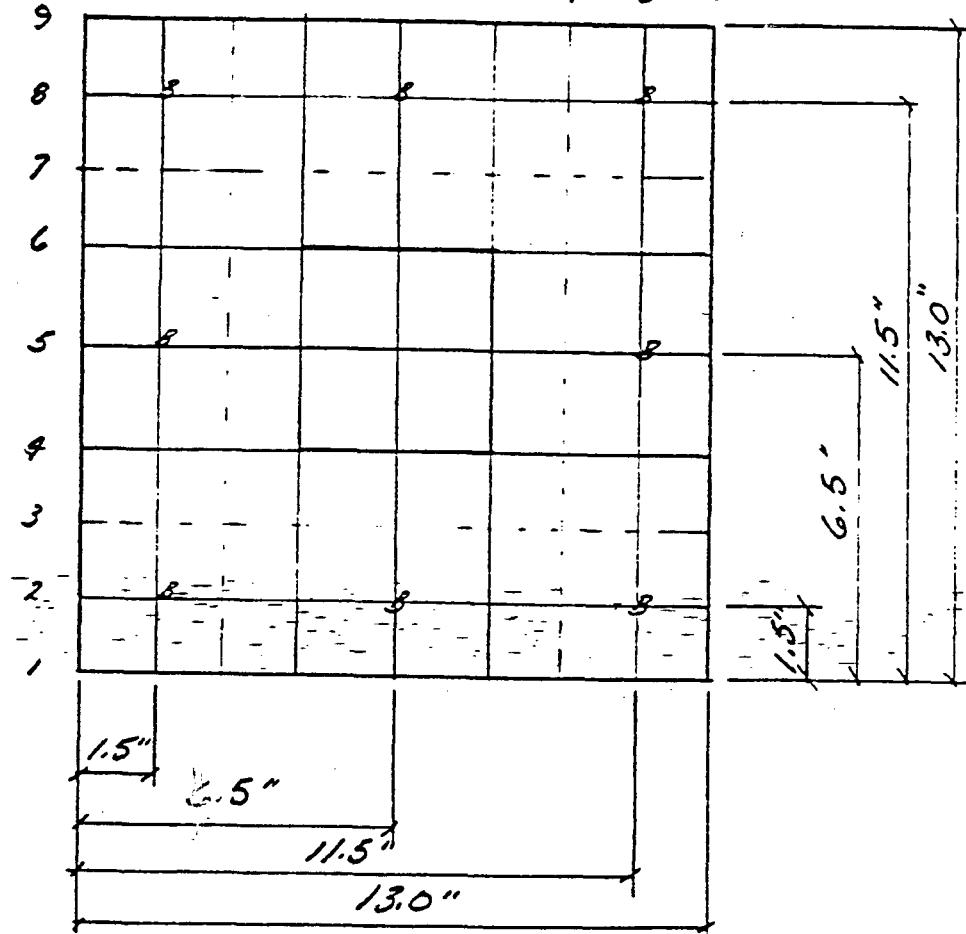
COMPUTED TSR DATE 1/20/84CHECKED PJL DATE 1/31/84

BASEPLATE II (FINITE ELEMENTS) MODEL

TP 13X13X 3/4"

Kt = 100 E/in, 300 E/in

1 2 3 4 5 6 7 8 9



LIS

04-01/21. 07.07.17.
PROGRAM RAPID

00102 1.4,UH,0
00110 3.9,HC,1.5
00120 13,13,1,1
00130 8
00140 SD,.75,1.5,1.5
00150 SD,.75,1.5,6.5
00160 SD,.75,1.5,11.5
00170 SD,.75,6.5,1.5
00180 SD,.75,6.5,11.5
00190 SD,.75,11.5,1.5
00200 SD,.75,11.5,8.5
00210 SD,.75,11.5,11.5
00220 4,4,6.5,6.5
00230 0,0,0,7.50,7.50,0
READY.

SHEET 13 OF 40
EVALUATION OF SYSTEM
Security Requirements
COMPUTED TBE DATE 1/31/84
CHECKED 9th DATE 1/31/84

21/21. 07.38.18.
PROGRAM CASTOUT

WIDTH OF PLATE = 13 INCHES
LENGTH OF PLATE = 13 INCHES
MODULAR RATIO = 9

ANCHOR NUMBER	AREA IN	X ORDINATE IN	Y ORDINATE IN
1	.334	1.5	1.5
2	.334	1.5	6.5
3	.334	1.5	11.5
4	.334	6.5	1.5
5	.334	6.5	6.5
6	.334	11.5	1.5
7	.334	11.5	6.5
8	.334	11.5	11.5

LOAD CONDITION NUMBER = 1

ATTACHMENT 1
VERT LOAD = 0 KIPS LOCATION X = 6.5 INCHES Y = 6.5 INCHES
APPLIED MOMENT ABOUT Y AXIS = 7.58 KIP FEET
APPLIED MOMENT ABOUT X AXIS = 7.58 KIP FEET

SUMMATION OF APPLIED LOADS FOR 1 ATTACHMENT(S) = 0 KIP(S)
TRANSLATED MOMENT CENTERLINE ABOUT Y AXIS = 7.58 KIP FEET
TRANSLATED MOMENT CENTERLINE ABOUT X AXIS = 7.58 KIP FEET

PARTIAL PRESSURE CASE

CONCRETE PRESSURE (KPS)
C2 = .95

CONCRETE PRESSURE FORCE, CF = -12.76 KIPS
LOCATION IN X-DIRECTION = 10.76 INCHES
LOCATION IN Y-DIRECTION = 8.24 INCHES

FRICITION SHEAR CAPACITY, SF = 6.38 KIPS

PRESSURE BULB GEOMETRY
Z3 = 8.98
Z6 = 8.98

ANCHOR NUMBER	STRESS CROSS AREA (KSI)	LOAD KIPS
1	3.87	1.20
2	8.59	2.87
3	13.38	4.46
5	8.59	2.87
8	3.89	1.28

SHEET 14 OF 40

RIGIDITY REQUIREMENTS

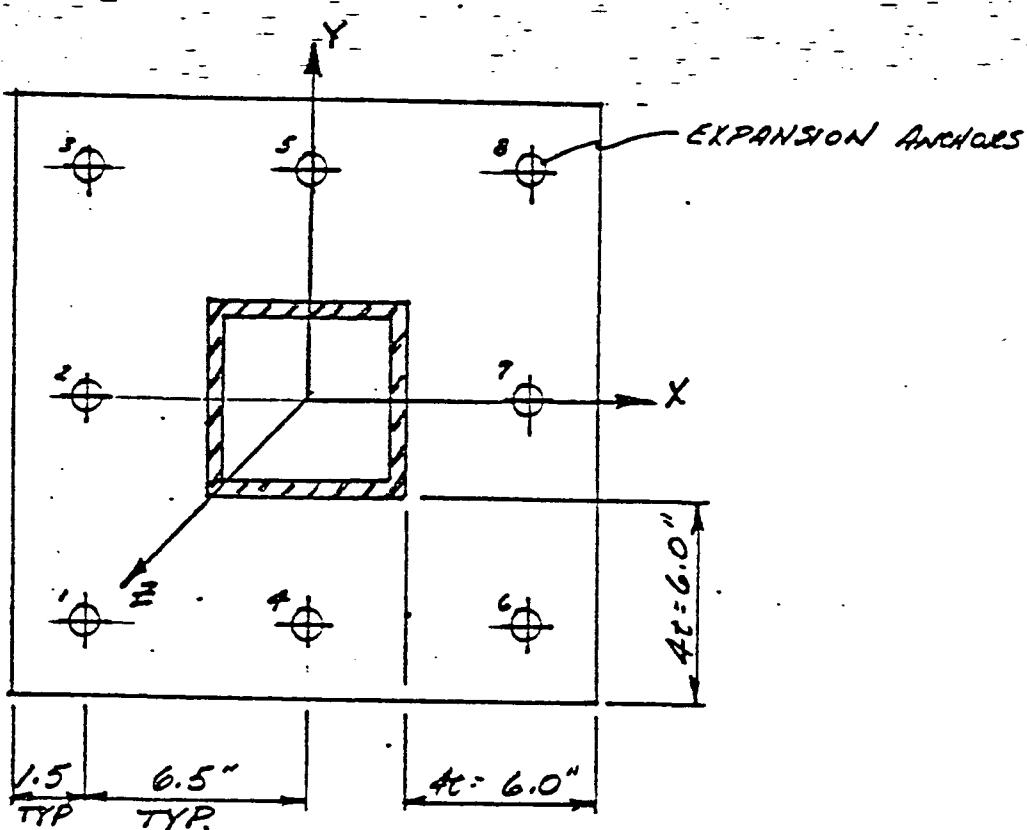
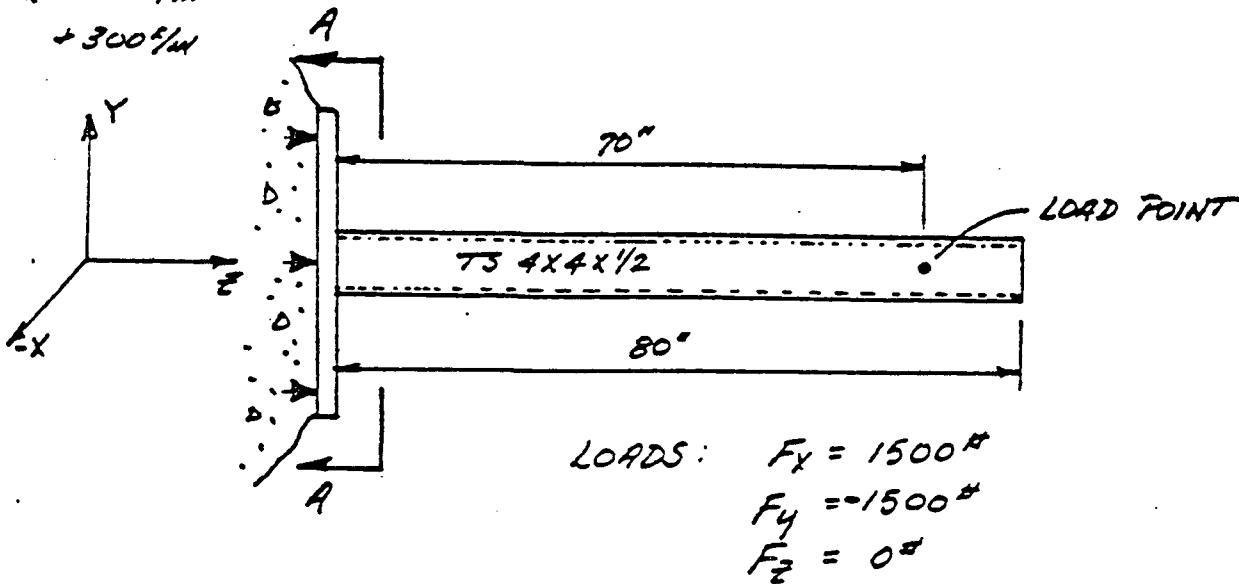
EVALUATION OF DESIGN

COMPUTED BY DATE 1/21/84

CHECKED Lsh DATE 1/21/84

EVALUATION OF BASEPLATE RIGIDITY
REQUIREMENTS

DS-C1.7.1

COMPLETED TSR DATE 1/31/84
CHECKED Psh DATE 1/31/84PLATE SIZE - 16" x 16" x 1 1/2" $K_x = 100 \text{ kN/m}$
 $+ 300 \text{ kN/m}$ 

SECTION A-A

EVALUATION OF BASEPLATE RIGIDITY
REQUIREMENTS

SHEET 16 OF 40

DS-C1.7.1

COMPUTED TBR DATE 1/31/84
CHECKED PJW DATE 1/31/84

**SUMMARY OF RESULTS
FOR PLATE SIZE 16X16X11/2"**

ANCHOR LOADS

ANCHOR NUMBER	RIGID KIPS	FLEXIBLE, KIPS	
		K _F = 100% K _F = 300%	K _F = 300% K _F = 300%
1	1.23	1.16	1.02
2	2.56	2.56	3.09
3	3.90	3.62	4.06
4	0	.19	0
5	2.56	2.56	3.09
6	0	0	0
7	0	.19	0
8	1.23	1.16	1.02

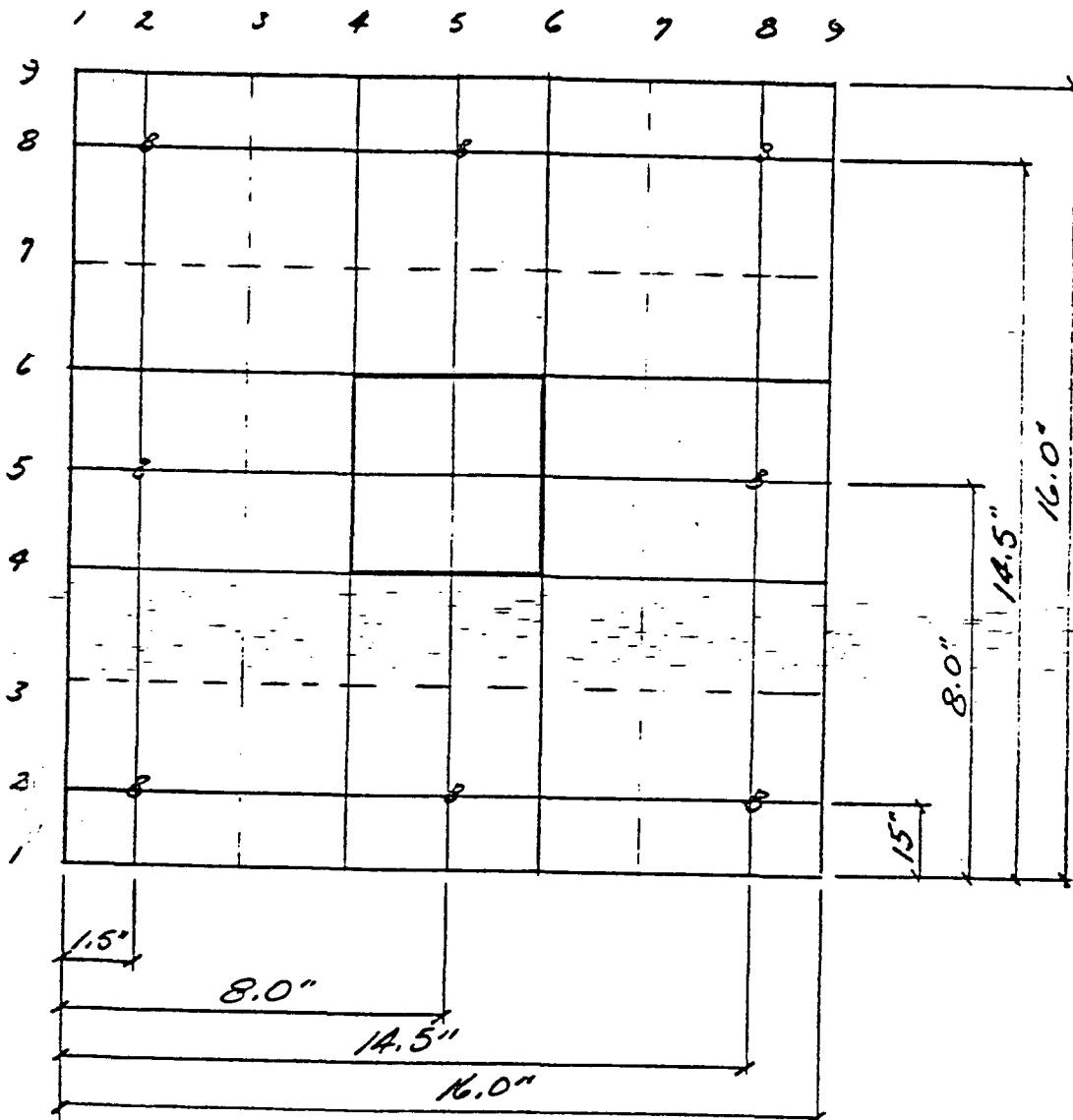
EVALUATION OF BASEPLATE REGIORITY
REQUIREMENTS

DS-C1.7.1

COMPUTED TBC DATE 1/20/84
 CHECKED PAC DATE 1/31/84

BASEPLATE II (FINITE ELEMENTS) MODEL

RE 16X16 X 1/2"
 $K_t = 100 \text{ k/in}, 300 \text{ k/in}$



15

84/01/21. 07.39.03.
PROGRAM BAP16

00100 1,4,0H,0
00110 3,9,HC,1,5
00120 16,16,1,1
00130 8
00140 SD,.75,1,5,1,5
00150 SD,.75,1,5,8,0
00160 SD,.75,1,5,14,5
00170 SD,.75,R,0,1,5
00180 SD,.75,8,0,14,5
00190 SD,.75,14,5,1,5
00200 SD,.75,14,5,8,0
00210 SD,.75,14,5,14,5
00220 4,4,8,0,8,0
00230 0,0,0,8,75,R,75,0
READY.

NET 18 or 40
EVALUATION of DISCRETE
DENSITY REQUIREMENTS
COMPUTED TBC DATE 1/21/84
CHECKED PMB DATE 1/31/84

84-01-21. 67.40.04.
PROGRAM CHSDOUT

WIDTH OF PLATE = 16 INCHES
LENGTH OF PLATE = 16 INCHES
MODULAR RATIO = 9

ANCHOR NUMBER	AREA IN	X ORDINATE IN	Y ORDINATE IN
1	.034	1.5	1.5
2	.034	1.5	0
3	.034	1.5	14.5
4	.034	0	1.5
5	.034	0	14.5
6	.034	14.5	1.5
7	.034	14.5	0
8	.034	14.5	14.5

LOAD CONDITION NUMBER = 1

ATTACHMENT 1
VERT LOAD = 0 KIPS LOCATION X = 8 INCHES V = 8 INCHES
APPLIED MOMENT ABOUT Y AXIS = 0.75 KIP FEET
APPLIED MOMENT ABOUT X AXIS = 0.75 KIP FEET

SUMMATION OF APPLIED LOADS FOR 1 ATTACHMENT(S) = 0 KIP(S)
TRANSLATED MOMENT CENTERLINE ABOUT Y AXIS = 0.75 KIP FEET
TRANSLATED MOMENT CENTERLINE ABOUT X AXIS = 0.75 KIP FEET

PARTIAL PRESSURE CASE

CONCRETE PRESSURE (KSI)
C2 = .68

CONCRETE PRESSURE FORCE = -11.47 KIPS
LOCATION IN X-DIRECTION = 13.49 INCHES
LOCATION IN Y-DIRECTION = 2.51 INCHES

FRICITION SHEAR CAPACITY, SF = 5.74 KIPS

FRESSNIE SHELL GEOMETRY
ZD = 10.03
ZB = 10.03

ANCHOR NUMBER	STRESS GROSS AREA (KSI)	LOAD KIPS
1	3.67	1.83
2	7.67	2.56
3	11.67	3.9
4	7.67	2.56
5	3.67	1.83

Sheet 19 or 40
Evaluation of Concrete
Prestressing Requirements
COMPUTED BY DATE 1/21/84
CHECKED BY DATE 1/31/84

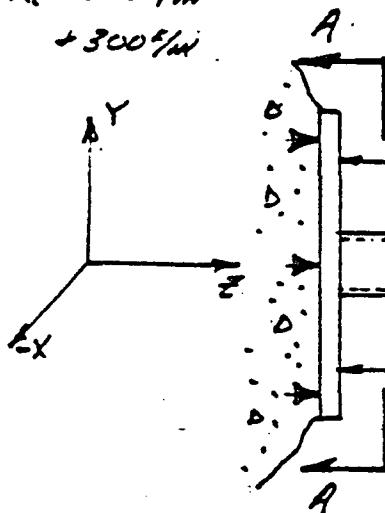
EVALUATION OF BASEPLATE RIGIDITY
REQUIREMENTS

DS-C1.7.1

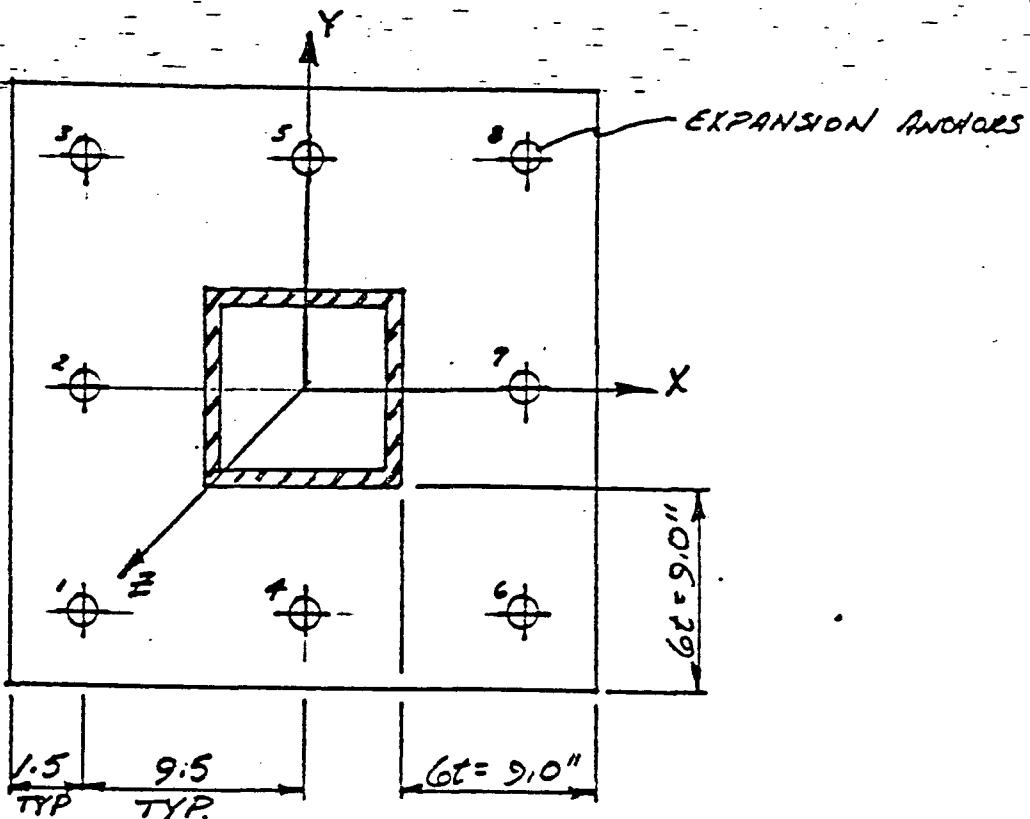
COMPLETED TSR DATE 1/31/84
CHECKED 9th DATE 1/31/84

PLATE SIZE - 22" x 22" x 1 1/2"

$K_x = 100 \text{ kN/m}$
 $+ 300 \text{ kN/m}$



LOADS: $F_x = 2000 \text{ lb}$
 $F_y = -2000 \text{ lb}$
 $F_z = 0 \text{ lb}$



SECTION A-A

EVALUATION OF BASEPLATE RIGIDITY
REQUIREMENTS

DS-C.I.7.1

COMPUTED TBR DATE 1/31/84
CHECKED PSL DATE 1/31/84SUMMARY OF RESULTS
FOR PLATE SIZE 22X22X1½"

ANCHOR LOADS

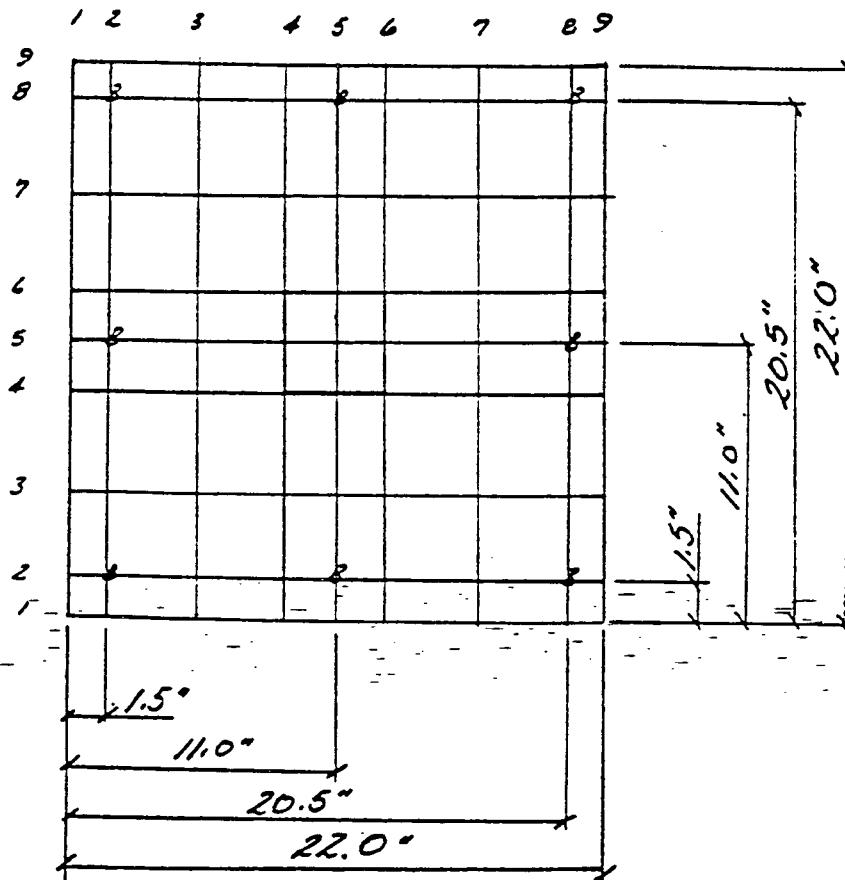
ANCHOR NUMBER	RIGID KIPS	FLEXIBLE, KIPS	
		K _F = 100% K _F = 300%	K _F = 100% K _F = 300%
1	1.20	.94	.75
2	2.32	2.77	3.56
3	3.44	3.66	3.68
4	.09	.07	0
5	2.32	2.77	3.56
6	0	0	0
7	.09	.07	0
8	1.20	.94	.75

EVALUATION OF BASEPLATE RIGIDITY
REQUIREMENTS

DS-C.1.7.1

COMPUTED TBC DATE 1/20/84
 CHECKED E.J.M. DATE 1/31/84

BASEPLATE II (FINITE ELEMENTS) MODEL

 $R = 22 \times 22 \times 1\frac{1}{2}$ " $K_t = 100 \text{ k/in}, 300 \text{ k/in}$ 

LIS

34/61/21. 07.46.45.
PROGRAM BAP22

00140 1,4,UM,0
00110 3,9,IC,1,5
00120 22,22,1,1
00130 8
00140 SD,.75,1.5,1.5
00150 SD,.75,1.5,11.0
00160 SD,.75,1.5,20.5
00170 SD,.75,11.0,1.5
00180 SD,.75,11.0,20.5
00190 SD,.75,20.5,1.5
00200 SD,.75,20.5,11.0
00210 SD,.75,20.5,20.5
00220 4,4,11.0,11.0
00230 0,0,0,11.66,11.66,0
READY.

Sheet 23 or 40
EVALUATION OF DISCREPANCY
Priority Requirements
COMPUTED TBC DATE 1/24/84
CHECKED JMK DATE 1/31/84

.42.48.
PROGRAM CASOUT

WIDTH OF PLATE = 22 INCHES
LENGTH OF PLATE = 22 INCHES
MODULAR RATIO = 9

ANCHOR NUMBER	AREA IN	X COORDINATE IN	Y COORDINATE IN
1	.334	1.5	1.5
2	.334	1.5	11
3	.334	1.5	20.5
4	.334	11	1.5
5	.334	11	20.5
6	.334	20.5	1.5
7	.334	20.5	11
8	.334	20.5	20.5

LOAD CONDITION NUMBER = 1

ATTACHMENT 1
VERT LOAD = 0 KIPS LOCATION X = 11 INCHES Y = 11 INCHES
APPLIED MOMENT ABOUT Y AXIS = 11.68 KIP FEET
APPLIED MOMENT ABOUT X AXIS = 11.68 KIP FEET

SUMMATION OF APPLIED LOADS FOR 1 ATTACHMENT(S) = 0 KIP(S)
TRANSLATED MOMENT CENTERLINE ABOUT Y AXIS = 11.68 KIP FEET
TRANSLATED MOMENT CENTERLINE ABOUT X AXIS = 11.68 KIP FEET

PARTIAL PRESSURE CASE

CONCRETE PRESSURE (KSI)
C2 = .45

CONCRETE PRESSURE / CPCE, CF = 10.57 KIPS
LOCATION IN X-DIRECTION = 19.06 INCHES
LOCATION IN Y-DIRECTION = 8.04 INCHES

FRICITION SHEAR CAPACITY, SF = 5.53 KIPS

PRESSURE BUILD GEOMETRY
Z1 = 11.78
Z6 = 11.78

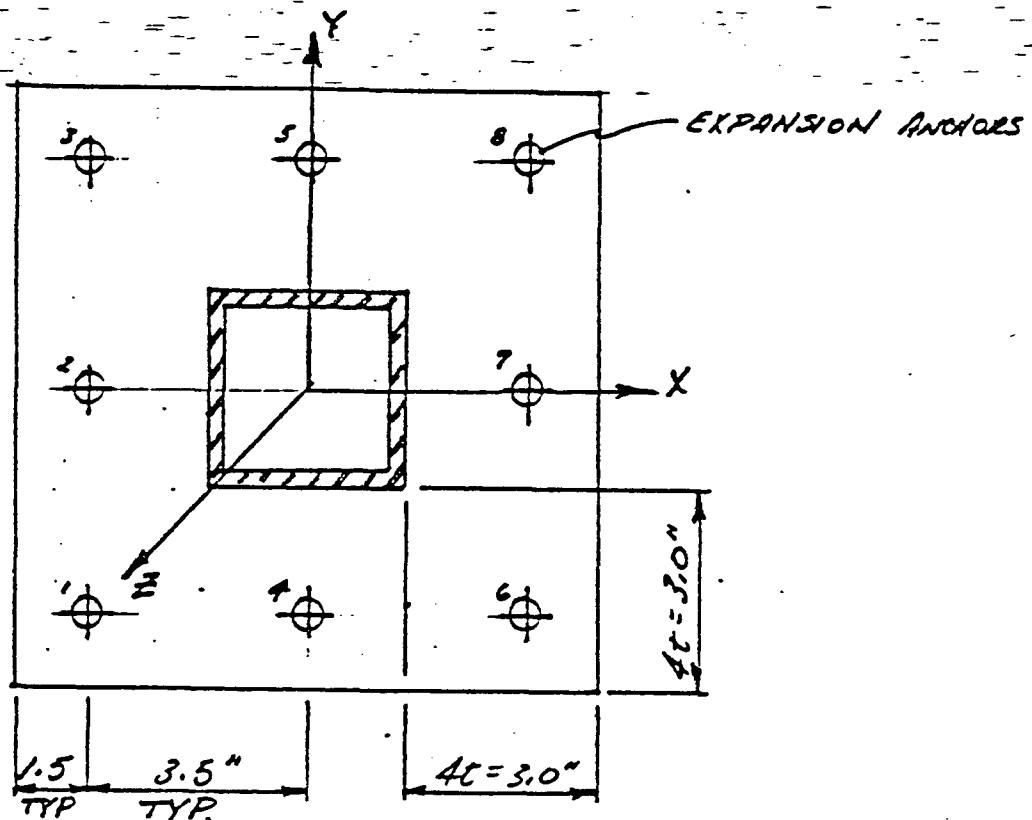
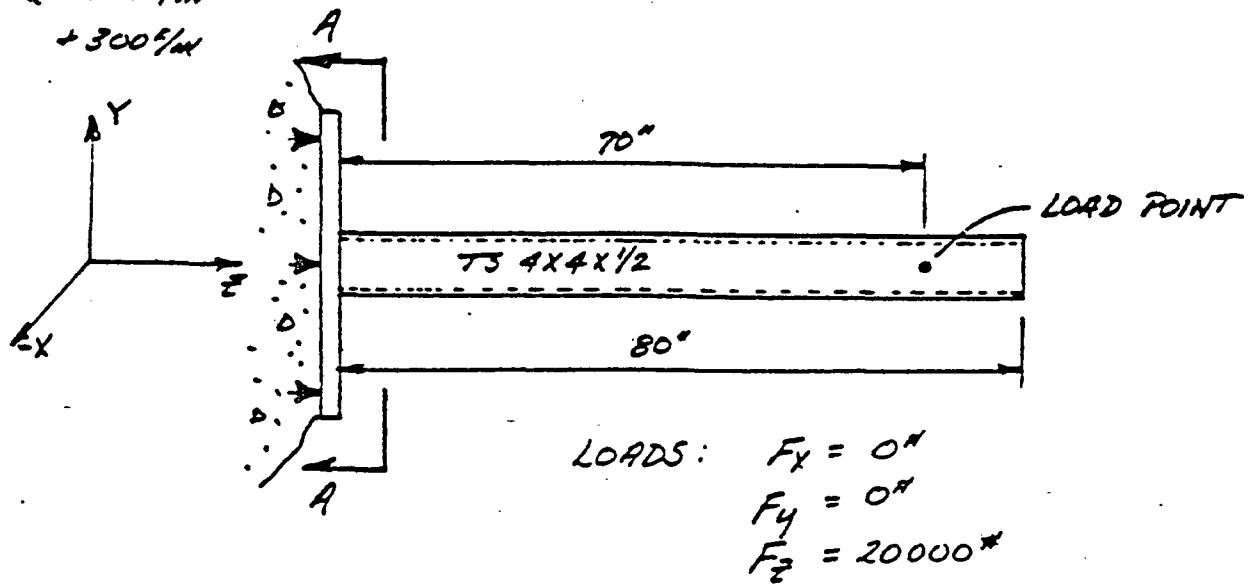
ANCHOR NUMBER	STRESS GROSS AREA (KSI)	LOAD KIPS
1	.61	1.2
2	6.96	2.32
3	16.31	3.44
4	.26	.09
5	6.96	2.32
7	.26	.09
8	.61	1.2

SHEET 24 OR 40
EVALUATION OF BASEMENT
SHEAR REQUIREMENTS
COMPUTED BY DATE 1/21/84
CHECKED P.M. DATE 1/31/84

EVALUATION OF BASEPLATE RIGIDITY
REQUIREMENTS

DS-C1.7.1

COMPUTED TBL DATE 1/31/84
 CHECKED PAW DATE 1/31/84

PLATE SIZE - 10" x 10" x 3/4"
 $K_x = 100 \text{ kN/m}$
 $\approx 300 \text{ kN/m}$


EVALUATION OF BASEPLATE RIGIDITY
REQUIREMENTS

SHEET 26 OF 40

DS-C1.7.1

COMPUTED TBR DATE 1/31/84
CHECKED PML DATE 1/31/84

SUMMARY OF RESULTS
FOR PLATE SIZE 10"X10"X 3/4"

ANCHOR LOADS

ANCHOR NUMBER	RIGID KIPS	FLEXIBLE, KIPS	
		K _F =100%W	K _F =300%W
1	2.5	2.39	2.19
2	2.5	2.61	2.81
3	2.5	2.39	2.19
4	2.5	2.62	2.82
5	2.5	2.62	2.82
6	2.5	2.39	2.18
7	2.5	2.61	2.81
8	2.5	2.39	2.18

READY.
L18

84/01/29, 10:30:10.
PROGRAM 54P10

00100 1,4,UN,0
00110 3,9,NO,1.5
00120 10,10,1,1
00130 9
00140 SD,.75,1.5,1.5
00150 SD,.75,1.5,5.0
00160 SD,.75,1.5,8.5
00170 SD,.75,5.0,1.5
00180 SD,.75,5.0,8.5
00190 SD,.75,8.5,1.5
00200 SD,.75,8.5,5.0
00210 SD,.75,8.5,8.5
00220 4,4,5.0,5.0
00230 0,0,20,0,0,0
READY.

27 of 40
EVALUATION OF BASEPLATE
RIGIDITY REQUIREMENTS
COMPUTED TBR DATE 1/23/84
CHECKED Pde DATE 1/31/84

DISCRETE
LIG-F=DISCRETE
ILLEGAL COMMAND
LIG,F=DISCRETE

34/01/84, 10.1.17.
PROGRAM: DISCRETE

SHEET 28 OF 40
EVALUATION OF BASEPLATE
RIGIDITY REQUIREMENTS
COMPUTED T82 DATE 1/23/84
CHECKED CJH DATE 1/31/84

WIDTH OF PLATE = 10 INCHES
LENGTH OF PLATE = 10 INCHES
MODULAR RATIO = 8

ANCHOR NUMBER	AREA IN	X ORDINATE IN	Y ORDINATE IN
1	.334	1.5	1.5
2	.334	1.5	5
3	.334	1.5	8.5
4	.334	5	1.5
5	.334	5	8.5
6	.334	8.5	1.5
7	.334	8.5	5
8	.334	8.5	8.5

LOAD CONDITION NUMBER = 1

ATTACHMENT 1

VERT LOAD = 20 KIPS LOCATION X = 5 INCHES Y = 5 INCHES
APPLIED MOMENT ABOUT Y AXIS = 0 KIP FEET
APPLIED MOMENT ABOUT X AXIS = 0 KIP FEET

SUMMATION OF APPLIED LOADS FOR 1 ATTACHMENT(S) = 20 KIPS
TRANSLATED MOMENT CENTERLINE ABOUT Y AXIS = 0 KIP FEET
TRANSLATED MOMENT CENTERLINE ABOUT X AXIS = 0 KIP FEET

UPLIFT CONDITION ON ANCHORS

ANCHOR NUMBER	STRESS KSI	TOTAL FORCE KIPS
1	7.49	2.5
2	7.49	2.5
3	7.49	2.5
4	7.49	2.5
5	7.49	2.5
6	7.49	2.5
7	7.49	2.5
8	7.49	2.5

READY.

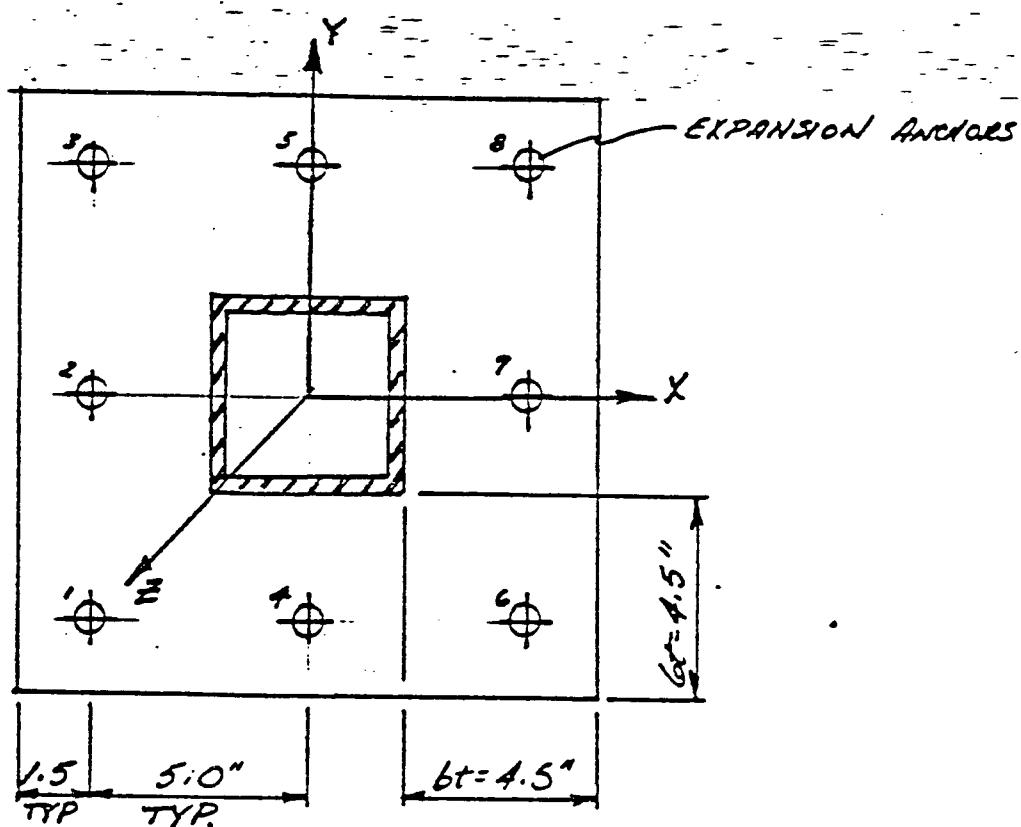
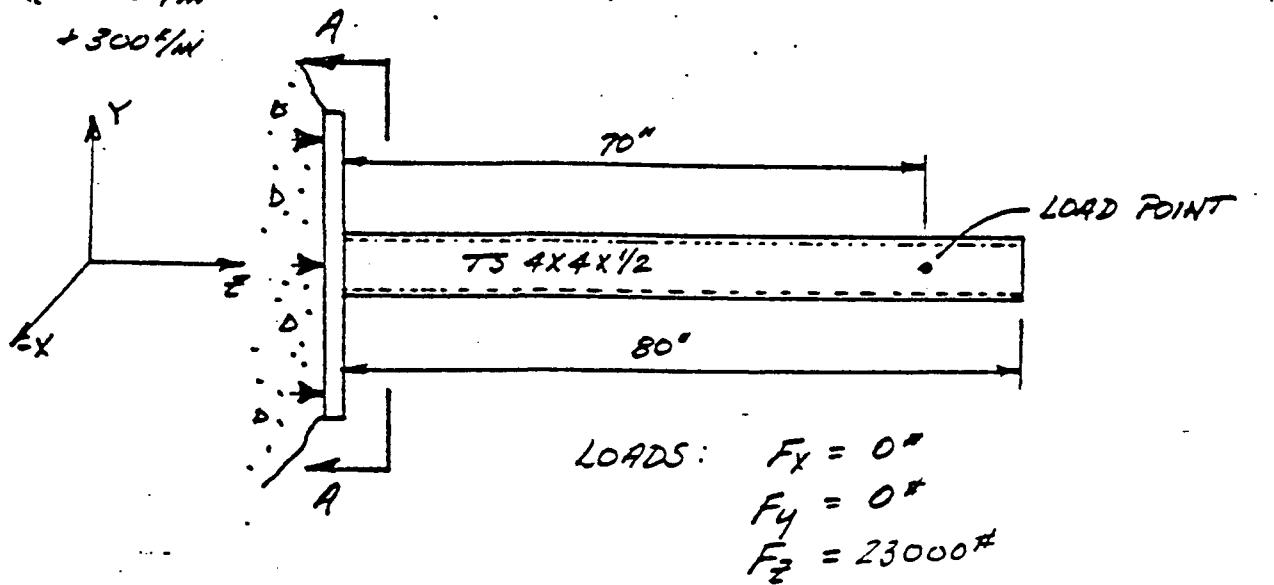
EVALUATION OF BASEPLATE RIGIDITY
REQUIREMENTS

DS-C1.7.1

COMPUTED T.S.R. DATE 1/31/84
CHECKED C.S.R. DATE 1/31/84

PLATE SIZE - 13" x 13" x 3/4"

$K_x = 100 \text{ kN/m}$
 $+ 300 \text{ kN/m}$



EVALUATION OF BASEPLATE RIGIDITY
REQUIREMENTS

SEE 30 OF 40
DS-C1.7.1

COMPUTED TBE DATE 1/31/8
CHECKED Etk DATE 1/31/8

SUMMARY OF RESULTS
FOR PLATE SIZE $13 \times 13 \times 3/4"$

ANCHOR LOADS

ANCHOR NUMBER	RIGID KIPS	FLEXIBLE, KIPS	
		$K_F = 100\text{ kips}$	$K_F = 300\text{ kips}$
1	2.88	2.40	1.91
2	2.88	3.35	4.02
3	2.88	2.40	1.91
4	2.88	3.35	4.03
5	2.88	3.35	4.03
6	2.88	2.40	1.91
7	2.88	3.35	4.02
8	2.88	2.40	1.91

DATA SHEET

READY.

L108

ALLEGED COMMAND.

L19

84/01/29. 10:15:17.
PROGRAM BAP13

00100 1,4,0N,0
00110 0,9,ND,1,5
00120 18,13,1,1
00130 6
00140 8D, .75,1,5,1,5
00150 8D, .75,1,5,1,5
00160 8D, .75,1,5,1,5
00170 8D, .75,1,5,1,5
00180 8D, .75,1,5,1,5
00190 8D, .75,1,5,1,5
00200 8D, .75,1,5,1,5
00210 8D, .75,1,5,1,5
00220 0,4,6,5,6,5
00230 0,0,23,0,0,0
READY.

SHEET

31

of 40

EVALUATION OF BASE RATE
RIGIDITY REQUIREMENTS

COMPUTED TBR DATE 1/23/84

CHECKED PM DATE 1/31/84

84/01/28. 10.04.16.
PROGRAM CADDO

WIDTH OF PLATE = 18 INCHES
LENGTH OF PLATE= 18 INCHES
MODULAR RATIO= 1

SHEET 2 OF 40
EVALUATION OF BASEPLATE
RIGIDITY REQUIREMENTS
COMPUTED TBR DATE 1/23/84
CHECKED PML DATE 1/31/84

ANCHOR NUMBER	AREA IN	X ORDINATE IN	Y ORDINATE IN
1	.384	1.5	1.5
2	.384	1.5	6.5
3	.384	1.5	11.5
4	.384	6.5	1.5
5	.384	6.5	11.5
6	.384	11.5	1.5
7	.384	11.5	6.5
8	.384	11.5	11.5

LOAD CONDUCTION NUMBER= 1

ATTACHMENT 1

VERT LOAD= 28 KIPS LOCATION X= 6.5 INCHES Y= 6.5 INCHES

APPLIED MOMENT ABOUT Y AXIS= 0 KIP·FEET

APPLIED MOMENT ABOUT X AXIS= 0 KIP·FEET

SUMMATION OF APPLIED LOADS FOR 1 ATTACHMENT(S)= 28 KIP(S)

TRANSLATED MOMENT CENTERLINE ABOUT Y AXIS= 0 KIP·FEET

TRANSLATED MOMENT CENTERLINE ABOUT X AXIS= 0 KIP·FEET

UPLIFT CONDITION ON ANCHORS

ANCHOR NUMBER	STRESS KSI	TOTAL FORCE KIPS
1	8.61	2.88
2	8.61	2.88
3	8.61	2.88
4	8.61	2.88
5	8.61	2.87
6	8.61	2.88
7	8.61	2.87
8	8.61	2.87

READY.

EVALUATION OF BASEPLATE RIGIDITY
REQUIREMENTS

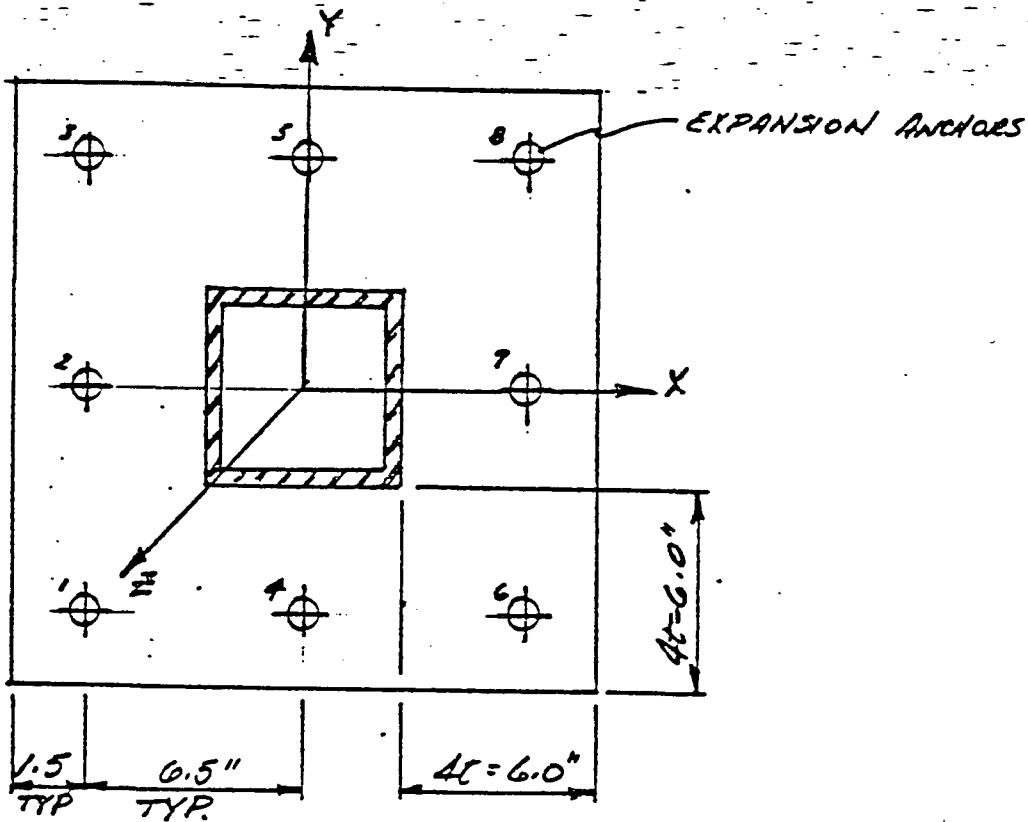
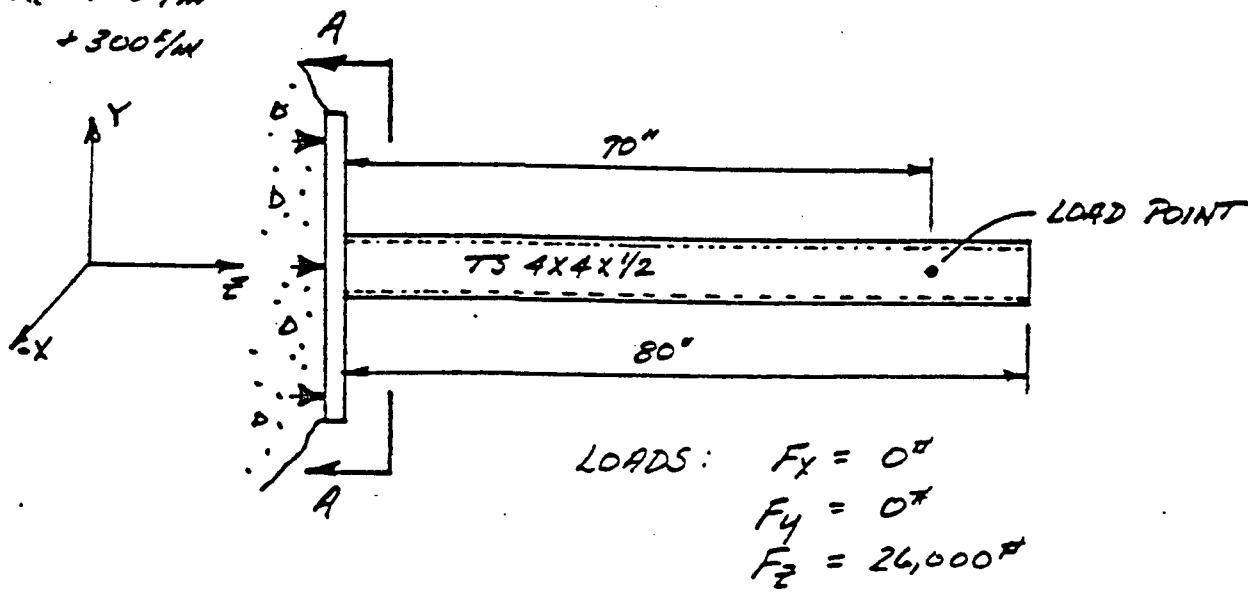
33 40

DS-C1.7.1

COMPLETED TBL DATE 1/31/84
CHECKED GAK DATE 1/31/84

PLATE SIZE - 16" x 16" x 1 1/2"

$K_x = 100 \text{ kN/m}$
 $+ 300 \text{ kN/m}$



SECTION A-A

EVALUATION OF BASEPLATE RIGIDITY
REQUIREMENTS

S-EE- 34 OF 40

DS-C1.7.1

COMPLETED TBR DATE 1/31/84
CHECKED PAB DATE 1/31/84

SUMMARY OF RESULTS
FOR PLATE SIZE 16"X16"X1 1/2"

ANCHOR LOADS

ANCHOR NUMBER	RIGID KIPS	FLEXIBLE, KIPS	
		K _F =100% _W	K _F =300% _W
1	3.25	3.08	2.77
2	3.25	3.42	3.73
3	3.25	3.08	2.77
4	3.25	3.43	3.74
5	3.25	3.43	3.74
6	3.25	3.08	2.76
7	3.25	3.42	3.73
8	3.25	3.08	2.76

READY.

LIS

64/01/23, 10.17.41.
PROGRAM PAP16

00100 1,4,UN,0
00110 3,9,ND,1,5
00120 16,16,1,1
00130 8
00140 SD,.75,1.5,1.5
00150 SD,.75,1.5,8.0
00160 SD,.75,1.5,14.5
00170 SD,.75,8.0,1.5
00180 SD,.75,8.0,14.5
00190 SD,.75,14.5,1.5
00200 SD,.75,14.5,8.0
00210 SD,.75,14.5,14.5
00220 4,4,8.0,8.0
00230 0,0,24,0,0,0
READY.

SHEET 35 OF 40
EVALUATION OF BASEPLATE
RIGIDITY REQUIREMENTS
COMPUTED TBR DATE 1/23/84
CHECKED PAK DATE 1/31/84

84/01/29. 10.15 S.
PROGRAM CADDET

SHEET 36 OF 40
EVALUATION OF BASEPLATE
RIGIDITY REQUIREMENTS
COMPUTED BY DATE 1/23/84
CHECKED 910 DATE 1/31/84

WIDTH OF PLATE = 16 INCHES
LENGTH OF PLATE= 16 INCHES
MODULAR RATIO= 3

ANCHOR NUMBER	AREA IN	X ORDINATE IN	Y ORDINATE IN
1	.334	1.5	1.5
2	.334	1.5	9
3	.334	1.5	14.5
4	.334	8	1.5
5	.334	8	14.5
6	.334	14.5	1.5
7	.334	14.5	8
8	.334	14.5	14.5

LOAD CONDITION NUMBER= 1

ATTACHMENT 1

VERT LOAD= 26 KIPS LOCATION X= 8 INCHES Y= 8 INCHES
APPLIED MOMENT ABOUT Y AXIS= 0 KIP FEET
APPLIED MOMENT ABOUT X AXIS= 0 KIP FEET

SUMMATION OF APPLIED LOADS FOR 1 ATTACHMENT(S)= 26 KIP(S)
TRANSLATED MOMENT CENTERLINE ABOUT Y AXIS= 0 KIP FEET
TRANSLATED MOMENT CENTERLINE ABOUT X AXIS= 0 KIP FEET

UPLIFT CONDITION ON ANCHORS:

ANCHOR NUMBER	STRESS KSI	TOTAL FORCE KIPS
1	9.73	3.25
2	9.73	3.25
3	9.73	3.25
4	9.73	3.25
5	9.73	3.25
6	9.73	3.25
7	9.73	3.25
8	9.73	3.25

READY.

EVALUATION OF BASEPLATE RIGIDITY
REQUIREMENTS

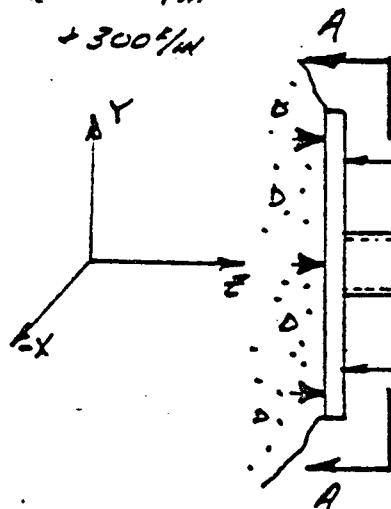
SET 37 or 40

DS-C1.7.1

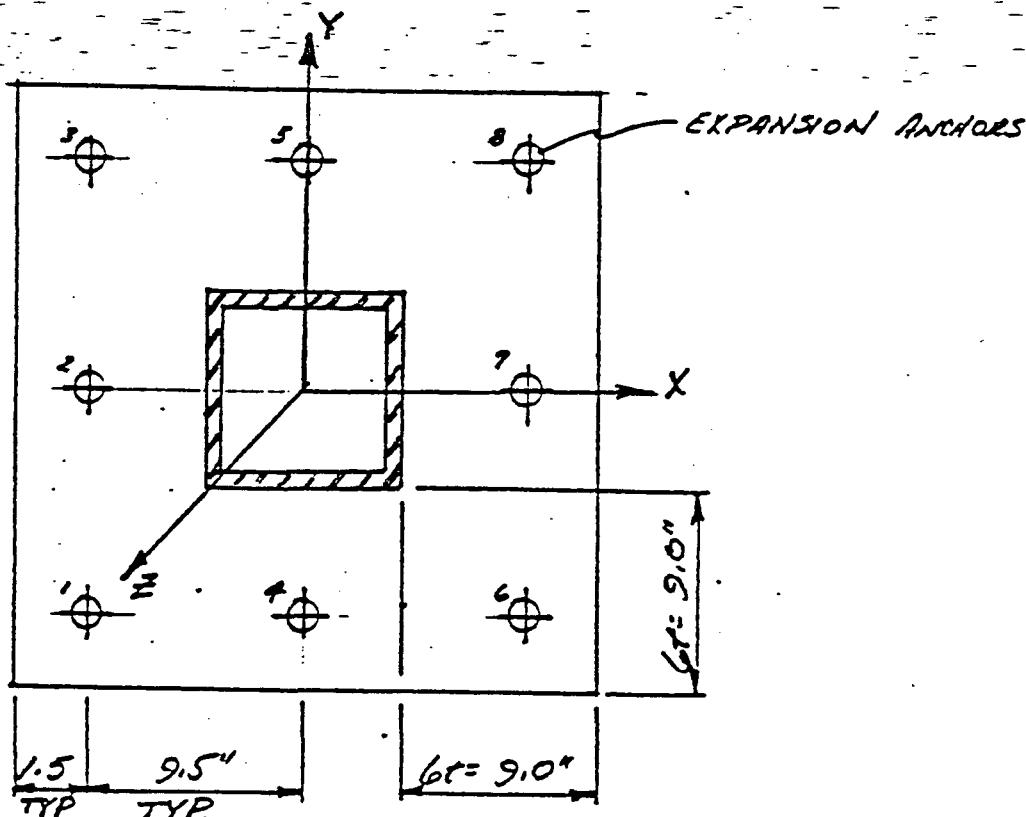
COMPUTED TBC DATE 1/31/8
 CHECKED P.M. DATE 1/31/8

PLATE SIZE - 22" x 22" x 1 1/2"

$K_x = 100 \text{ kN}$
 $+ 300 \text{ kN}$



LOADS: $F_x = 0^*$
 $F_y = 0^*$
 $F_z = 30000^*$



SECTION A-A

EVALUATION OF BASEPLATE RIGIDITY
REQUIREMENTS

DS-C1.7.1

COMPUTED TBL DATE 1/31/8
CHECKED PAB DATE 1/31/8

SUMMARY OF RESULTS
FOR PLATE SIZE 22X22X1 $\frac{1}{2}$

ANCHOR LOADS

ANCHOR NUMBER	RIGID KIPS	FLEXIBLE, KIPS	
		K _F =100% K _R =300%	K _F =300% K _R =100%
1	3.75	3.25	2.47
2	3.75	4.25	5.02
3	3.75	3.25	2.47
4	3.75	4.26	5.03
5	3.75	4.26	5.03
6	3.75	3.25	2.47
7	3.75	4.25	5.03
8	3.75	3.25	2.47

OLD, SAP22
READY.
LIS

84/01/29. 10.21.04.
PROGRAM SAP22

00100 1,4,UN,0
00110 3,7,NC,1,5
00120 22,22,1,1
00130 3
00140 SD,.75,1.5,1.5
00150 SD,.75,1.5,11.0
00160 SU,.75,1.5,20.5
00170 SD,.75,11.0,1.5
00180 SD,.75,11.0,20.5
00190 SD,.75,20.5,1.5
00200 SD,.75,20.5,11.0
00210 SU,.75,20.5,20.5
00220 4,4,11.0,11.0
00230 0,0,30,0,0,0
READY.

SET 39 OF 40
EVALUATION OF BASEPLATE
RIGIDITY REQUIREMENTS
COMPUTED TOK DATE 1/23/84
CHECKED PSL DATE 1/31/84

84301/29. 10.20.5.
PROGRAM CASOUT

SHEET 40 OF 40
EVALUATION OF BASEPLATE
RIGIDITY REQUIREMENTS
COMPUTED TOL DATE 1/23/84
CHECKED PW DATE 1/31/84

WIDTH OF PLATE = 22 INCHES
LENGTH OF PLATE= 22 INCHES
MODULAR RATIO= 9

ANCHOR NUMBER	AREA IN	X ORDINATE IN	Y ORDINATE IN
1	.334	1.5	1.5
2	.334	1.5	11
3	.334	1.5	20.5
4	.334	11	1.5
5	.334	11	20.5
6	.334	20.5	1.5
7	.334	20.5	11
8	.334	20.5	20.5

LOAD CONDITION NUMBER= 1

ATTACHMENT 1

VERT LOAD= 30 KIPS LOCATION X= 11 INCHES Y= 11 INCHES

APPLIED MOMENT ABOUT Y AXIS= 0 KIP FEET

APPLIED MOMENT ABOUT X AXIS= 0 KIP FEET

SUMMATION OF APPLIED LOADS FOR 1 ATTACHMENT(S)= 30 KIP(S)

TRANSLATED MOMENT CENTERLINE ABOUT Y AXIS= 0 KIP FEET

TRANSLATED MOMENT CENTERLINE ABOUT X AXIS= 0 KIP FEET

UPLIFT CONDITION ON ANCHORS

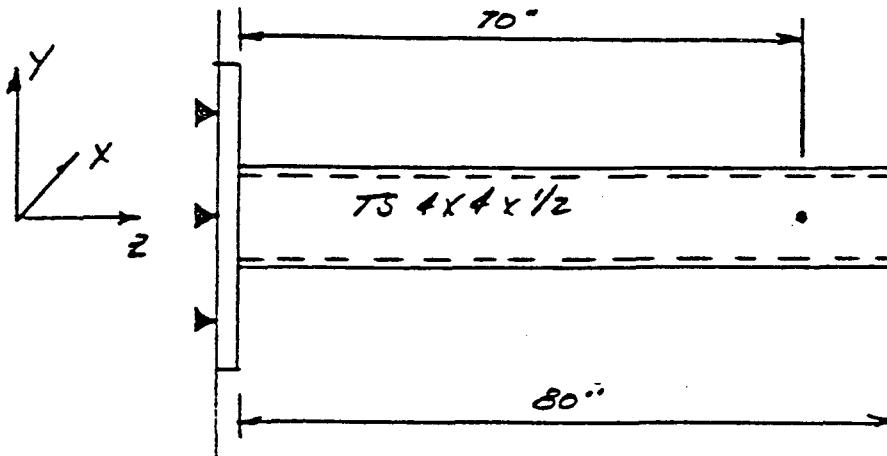
ANCHOR NUMBER	STRESS KSI	TOTAL FORCE KIPS
1	11.28	3.75
2	11.28	3.75
3	11.28	3.75
4	11.28	3.75
5	11.28	3.75
6	11.28	3.75
7	11.28	3.75
8	11.28	3.75

READY.

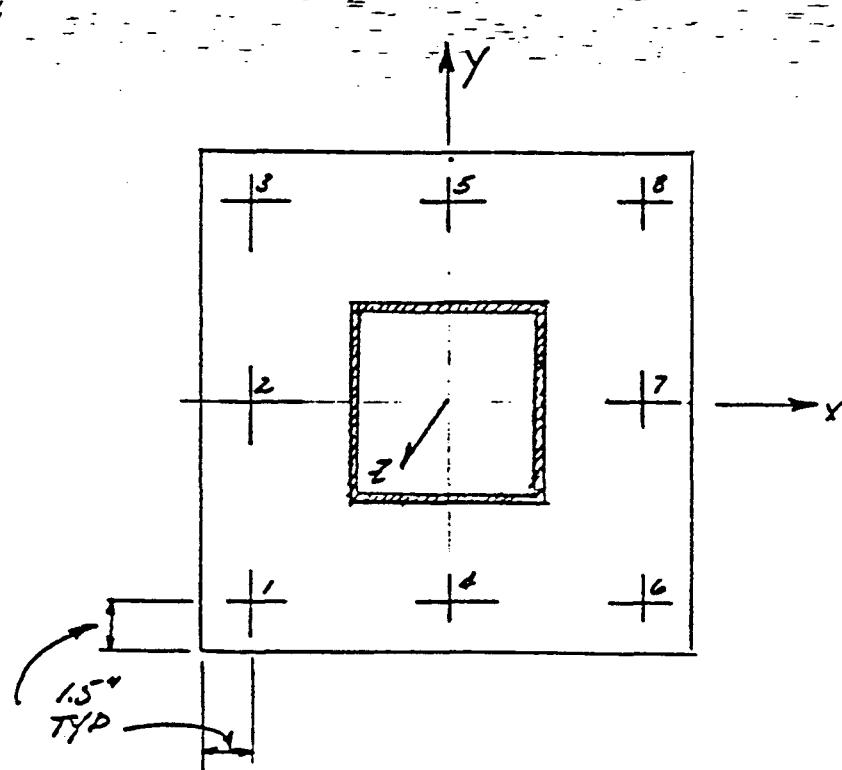
EVALUATION OF BASE PLATE RIGIDITY
REQUIREMENTS

 COMPUTED BY DATE 7/19/81
 CHECKED LS DATE 7-30-81

PLATE SIZE 10x10 x 3/4 w/ 8 - 3/4" # 550 ANCHORS LS.
 $L_1 = 100 \text{ in} + 300 \text{ in}$



LOADS
 $F_x = 1000 \text{ lb}$
 $F_y = -1000 \text{ lb}$
 $F_z = 1000 \text{ lb}$



85/07/19. 10.15.35.
PROGRAM CASIDOUT

PROGRAM CASIDBAP ID 262256 REV. 1 04/84

DATE = 85/07/19.
FILE = BAP10

TIME = 10.15.07.

SHEET 408 OF 40

800EARTH EX1074

PREPARED 100 DATE 7/30/85

CHECKED 100 DATE 7-30-85

ANCHORS TAKE NO COMPRESSION
WIDTH OF PLATE = 10 INCHES
LENGTH OF PLATE= 10 INCHES
MODULAR RATIO= 9

ANCHOR NUMBER	AREA IN	X ORDINATE IN	Y ORDINATE IN
1	.334	1.5	1.5
2	.334	1.5	5
3	.334	1.5	8.5
4	.334	5	1.5
5	.334	5	8.5
6	.334	8.5	1.5
7	.334	8.5	5
8	.334	8.5	8.5

LOAD CONDITION NUMBER= 1

ATTACHMENT 1

VERT LOAD= 1 KIPS LOCATION X= 5 INCHES Y= 5 INCHES

APPLIED MOMENT ABOUT Y AXIS= 5.83 KIP FEET

APPLIED MOMENT ABOUT X AXIS= 5.83 KIP FEET

1.83

SUMMATION OF APPLIED LOADS FOR 1 ATTACHMENT(S)= 1 KIP(S)

TRANSLATED MOMENT CENTERLINE ABOUT Y AXIS= 5.83 KIP FEET

TRANSLATED MOMENT CENTERLINE ABOUT X AXIS= 5.83 KIP FEET

PARTIAL PRESSURE CASE

CONCRETE PRESSURE (KSI)

C2=-1.3711

CONCRETE PRESSURE FORCE,CF=-13.16 KIPS

LOCATION IN X-DIRECTION= 8.1 INCHES

LOCATION IN Y-DIRECTION= 1.9 INCHES

FRICITION SHEAR CAPACITY,SF= 6.58 KIPS

PRESSURE BULB GEOMETRY

Z3= 7.5876

Z6= 7.5876

ANCHOR NUMBER	STRESS GROSS AREA (KSI)	LOAD KIPS
1	3.9234	1.3104
	9.6156	3.2116
	15.3077	5.1128
5	9.6156	3.2116
8	3.9234	1.3104

DS-C1.7.1

EVALUATION OF BASEPLATE RIGIDITY
REQUIREMENTSCOMPUTED TOL DATE 7/19/85
CHECKED LS DATE 7-30-85SUMMARY OF RESULTS
FROM PLATE SIZE 10X10X 3/4

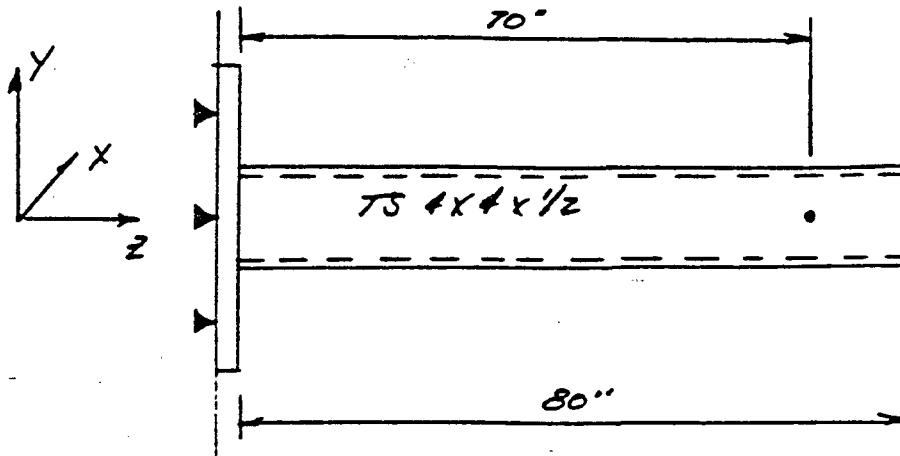
ANCHOR NUMBER	RIGID ANGL. KIPS	ANCHOR LOADS	
		*FLEXIBLE ANALYSIS, L1.05 $K_1 = 100 \text{ kN/m}$	$K_1 = 300 \text{ kN/m}$
1	1.31	1.62	1.42
2	3.21	3.18	3.66
3	5.11	4.44	4.91
4	0	.38	0
5	3.21	3.18	3.66
6	0	0	0
7	0	.38	0
8	1.31	1.62	1.42

F *for Flexible Analysis PLATE MODEL SEE chs. 7
8&9.

EVALUATION OF BASE PLATE RIGIDITY REQUIREMENTS

COMPUTED TBC DATE 7/7/85
CHECKED LS DATE 7-30-85

PLATE SIZE 13 X 13 X 3/4 W/ 8- 3/4" # 550 ANCHORS
 $K_L = 100 \text{ kN} + 300 \text{ kN}$

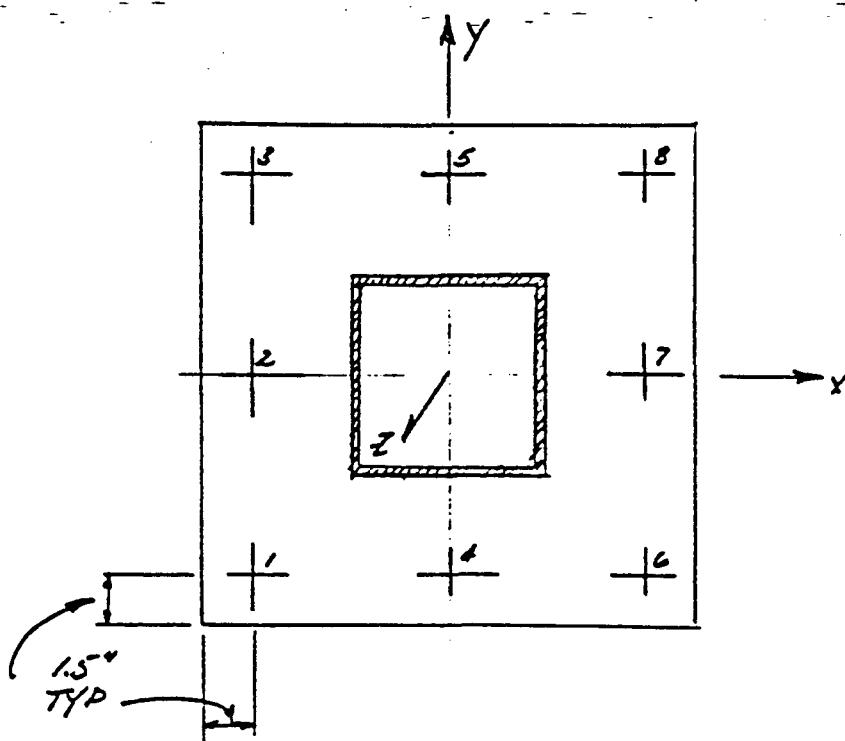


LOADS

$$F_x = 1000 \text{ lb}$$

$$F_y = -1000 \text{ lb}$$

$$F_z = 1000 \text{ lb}$$



LIS.F=CASDOUT

85/07/19. 10.18.27.
PROGRAM CASDOUT

PROGRAM CASDBAP ID 262256 REV. 1 04/84

DATE = 85/07/19.
FILE = BAP13

TIME = 10.18.00.

SHEET 40E OF 40

~~--DO NOT PLOT Priority~~

PREPARED 202 DATE 2/2/85

CHECKED LS DATE 2-30-85

ANCHORS TAKE NO COMPRESSION
WIDTH OF PLATE = 13 INCHES
LENGTH OF PLATE= 13 INCHES
MODULAR RATIO= 9

ANCHOR NUMBER	AREA IN	X ORDINATE IN	Y ORDINATE IN
1	.334	1.5	1.5
2	.334	1.5	6.5
3	.334	1.5	11.5
4	.334	6.5	1.5
5	.334	6.5	6.5
6	.334	11.5	11.5
7	.334	11.5	1.5
8	.334	11.5	6.5
			11.5

LOAD CONDITION NUMBER= 1

ATTACHMENT 1

APPLIED LOAD= 1 KIPS LOCATION X= 6.5-INCHES Y= 6.5 INCHES
APPLIED MOMENT ABOUT Y AXIS= 5.83 KIP FEET
APPLIED MOMENT ABOUT X AXIS= 5.83 KIP FEET

SUMMATION OF APPLIED LOADS FOR 1 ATTACHMENT(S)= 1 KIP(S)
TRANSLATED MOMENT CENTERLINE ABOUT Y AXIS= 5.83 KIP FEET
TRANSLATED MOMENT CENTERLINE ABOUT X AXIS= 5.83 KIP FEET

PARTIAL PRESSURE CASE

CONCRETE PRESSURE (KSI)
C2=-.7333

CONCRETE PRESSURE FORCE, CF=-9.37 KIPS
LOCATION IN X-DIRECTION= 10.81 INCHES
LOCATION IN Y-DIRECTION= 2.19 INCHES

FRICITION SHEAR CAPACITY, SF= 4.69 KIPS

PRESSURE BULB GEOMETRY
Z3= 8.7574
Z6= 8.7574

ANCHOR NUMBER	STRESS GROSS AREA (KSI)	LOAD KIPS
3	3.1973	1.0679
5	6.9653	2.3264
8	10.7333	3.5849
	6.9653	2.3264
	3.1973	1.0679

EVALUATION OF BASEPLATE RIGIDITY
REQUIREMENTSCOMPUTED TBL DATE 7/19/85
CHECKED LS DATE 7-30-85SUMMARY OF RESULTS
FROM PLATE SIZE 13X13 X 3/4

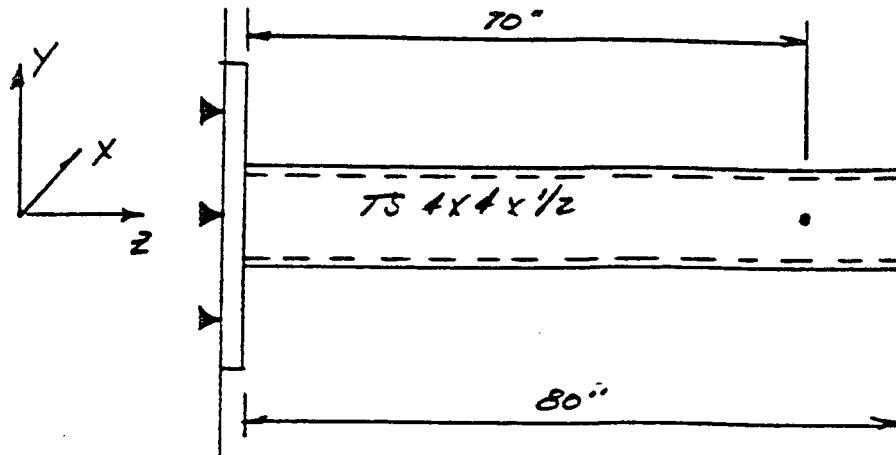
ANCHOR NUMBER	RIGID ANGL. KIPS	ANCHOR LOADS	
		*FLEXIBLE ANALYSIS, KIPS $K_1 = 100 \text{ kips/m}$	$K_1 = 300 \text{ kips/m}$
1	1.07	1.02	.80
2	2.33	2.85	3.61
3	3.58	3.53	3.35
4	0	.18	.07
5	2.33	2.85	3.61
6	0	0	0
7	0	.18	.07
8	1.07	1.02	.80

[* FOR FLEXIBLE ANALYSIS (BASED II) PLATE MODEL]
SEE SHEET 12. L.D.

EVALUATION OF BASE PLATE RIGIDITY
REQUIREMENTS

 COMPUTED TBC DATE 7/12/85
 CHECKED LS DATE 7-30-8

PLATE SIZE 16 x 16 x 1 1/2 W/ 8 - 3/4" ϕ 550 ANCHORS.
 $k_x = 100 \text{ k/in} + 300 \text{ k/in}$

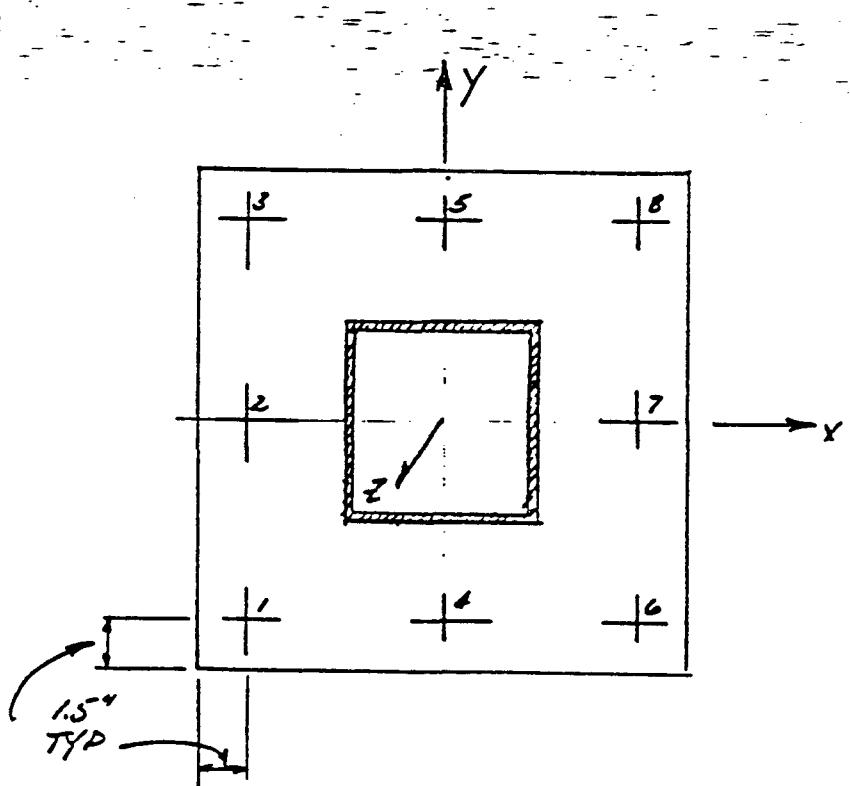


LOADS

$F_x = 1000 \text{ lb}$

$F_y = 1000 \text{ lb}$

$F_z = 1000 \text{ lb}$



85/07/19. 10.20.50.
PROGRAM CASDOUT

PREFEFAM CASDRAF ID 262256 REV. 1 04/84

DATE = 85/07/19.
FILE = BAP16

TIME = 10.20.22.

SHEET 40 OF 40

~~Emergency Priority~~

PREPARED JRC DATE 7/12/85

CHECKED LS DATE 7-30-85

ANCHORS TAKE NO COMPRESSION
WIDTH OF PLATE = 16 INCHES
LENGTH OF PLATE= 16 INCHES
MODULAR RATIO= 9

ANCHOR NUMBER	AREA IN	X ORDINATE IN	Y ORDINATE IN
1	.334	1.5	1.5
2	.334	1.5	8
3	.334	1.5	14.5
4	.334	8	1.5
5	.334	8	14.5
6	.334	14.5	1.5
7	.334	14.5	8
8	.334	14.5	14.5

LOAD CONDITION NUMBER= 1

ATTACHMENT 1

VERT LOAD= 1 KIPS LOCATION X= 8 INCHES Y= 8 INCHES
APPLIED MOMENT ABOUT Y AXIS= 5.83 KIP FEET
APPLIED MOMENT ABOUT X AXIS= 5.83 KIP FEET

SUMMATION OF APPLIED LOADS FOR 1 ATTACHMENT(S)= 1 KIP(S)
TRANSLATED MOMENT CENTERLINE ABOUT Y AXIS= 5.83 KIP FEET
TRANSLATED MOMENT CENTERLINE ABOUT X AXIS= 5.83 KIP FEET

PARTIAL PRESSURE CASE

CONCRETE PRESSURE (KSI)
C2=-.4601

CONCRETE PRESSURE FORCE, CF=-7.21 KIPS
LOCATION IN X-DIRECTION= 13.58 INCHES
LOCATION IN Y-DIRECTION= 2.42 INCHES

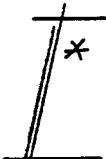
FRICITION SHEAR CAPACITY, SF= 3.6 KIPS

PRESSURE BULB GEOMETRY
Z3= 9.6943
Z6= 9.6943

ANCHOR NUMBER	STRESS GROSS AREA (KSI)	LOAD KIPS
1	2.6932	.8995
2	5.4695	1.8268
3	8.2457	2.7541
5	5.4695	1.8268
8	2.6932	.8995

EVALUATION OF BASEPLATE RIGIDITY
REQUIREMENTSCOMPUTED JBL DATE 7/19/85
CHECKED LS DATE 7-30-85SUMMARY OF RESULTS
FROM PLATE SIZE 16 X 16 X 1 1/2

ANCHOR NUMBER	RIGID ANGL. KIPS	ANCHOR LOADS	
		*FLEXIBLE ANALYSIS, L1,PS $K_1 = 100 \text{ kips/in}$	$K_1 = 300 \text{ kips/in}$
1	.90	.84	.73
2	1.83	1.82	2.17
3	2.75	2.55	2.83
4	0	.16	0
5	1.83	1.82	2.17
6	0	0	0
7	0	.16	0
8	.90	.84	.73

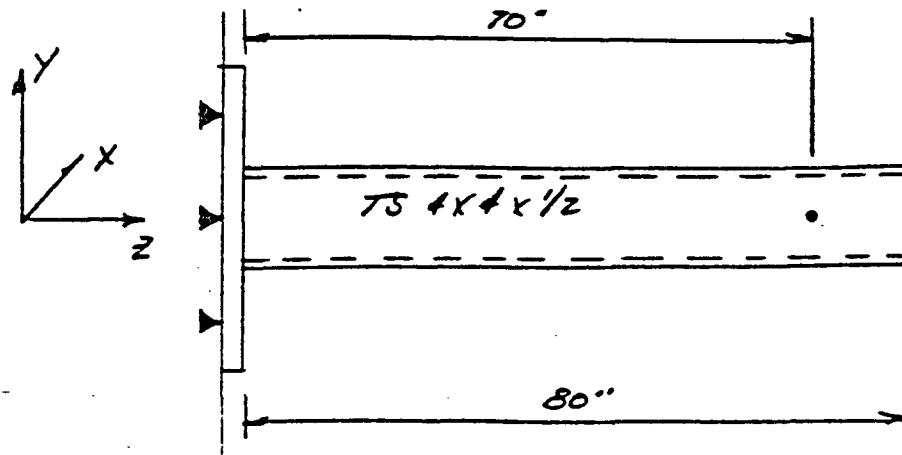
 * FOR FLEXIBLE ANALYSIS (BASEPLATE II) PLATE MODEL
 SEE SHEET 17.
 LS.

DS-C1.7.1

EVALUATION OF BASE PLATE RIGIDITY
REQUIREMENTS

COMPUTED TBL DATE 7/19/85
 CHECKED LS DATE 7-30-85

PLATE SIZE 22X22X1/2 W/8-3/4" # 350 ANCHORS.
 $L_1 = 100\text{ ft/in} + 300\text{ ft/in}$

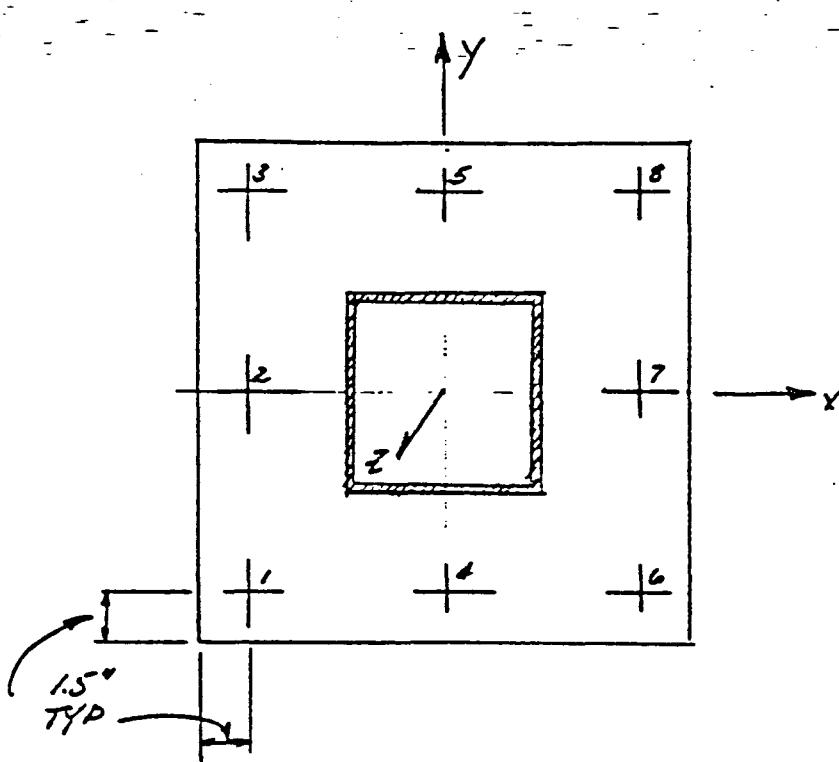


LOADS

$$F_x = 1000 \text{ lb}$$

$$F_y = -1000 \text{ lb}$$

$$F_z = 1000 \text{ lb}$$



85/07/19. 10.23.05.
PROGRAM CASIDOUT

PROGRAM CASIDBAP ID 262256 REV. 1 04/84

DATE = 85/07/19.
FILE = BAP22

TIME = 10.22.37.

SHEET 40 OF 40

~~BASEMENT P-10-01~~

PREPARED ZL DATE 2/2/85

CHECKED LS DATE 2-30-85

ANCHORS TAKE NO COMPRESSION
WIDTH OF PLATE = 22 INCHES
LENGTH OF PLATE= 22 INCHES
MODULAR RATIO= 9

ANCHOR NUMBER	AREA IN	X ORDINATE IN	Y ORDINATE IN
1	.334	1.5	1.5
2	.334	1.5	11
3	.334	1.5	20.5
4	.334	11	1.5
5	.334	11	20.5
6	.334	20.5	1.5
7	.334	20.5	11
8	.334	20.5	20.5

LOAD CONDITION NUMBER= 1

ATTACHMENT 1

VERT LOAD= 1 KIPS LOCATION X= 11 INCHES Y= 11 INCHES
APPLIED MOMENT ABOUT Y AXIS= 5.83 KIP FEET
APPLIED MOMENT ABOUT X AXIS= 5.83 KIP FEET

SUMMATION OF APPLIED LOADS FOR 1 ATTACHMENT(S)= 1 KIP(S)
TRANSLATED MOMENT CENTERLINE ABOUT Y AXIS= 5.83 KIP FEET
TRANSLATED MOMENT CENTERLINE ABOUT X AXIS= 5.83 KIP FEET

PARTIAL PRESSURE CASE

CONCRETE PRESSURE (KSI)
C2=-.2362

CONCRETE PRESSURE FORCE, CF=-4.97 KIPS
LOCATION IN X-DIRECTION= 19.19 INCHES
LOCATION IN Y-DIRECTION= 2.81 INCHES

FRICITION SHEAR CAPACITY, SF= 2.48 KIPS

PRESSURE BULB GEOMETRY

Z3= -11.2316

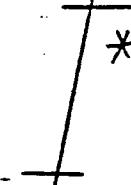
Z6= 11.2316

ANCHOR NUMBER	STRESS GROSS AREA (KSI)	LOAD KIPS
1	2.0378	.6806
2	3.8356	1.2811
3	5.6334	1.8816
4	.24	.0802
5	3.8356	1.2811
7	.24	.0802
8	2.0378	.6806

DS-C1.7.1

EVALUATION OF BASEPLATE RIGIDITY
REQUIREMENTSCOMPUTED JBL DATE 2/9/85
CHECKED LB DATE 7-30-85SUMMARY OF RESULTS
FROM PLATE SIZE 22X22X1 1/2

ANCHOR NUMBER	RIGID ANGL. KIPS	ANCHOR LOADS	
		*FLEXIBLE ANALYSIS, E.I.DS $K_f = 100 \text{ ft/lb}$	$K_f = 300 \text{ ft/lb}$
1	.68	.52	.40
2	1.28	1.50	1.90
3	1.88	1.95	1.93
4	.08	.06	0
5	1.28	1.50	1.90
6	0	0	0
7	.08	.06	0
8	.68	.52	.40


 * For Flexible Analysis (Base Plate II) Plate Model.
 SEE SHEET 22. Lb.