



UNITED STATES
NUCLEAR REGULATORY COMMISSION
WASHINGTON, D. C. 20555

November 8, 1991

Docket Nos. 50-390
and 50-391

LICENSEE: TENNESSEE VALLEY AUTHORITY
FACILITY: WATTS BAR NUCLEAR PLANT, UNITS 1 AND 2
SUBJECT: OCTOBER 31, 1991 MEETING WITH THE TENNESSEE VALLEY AUTHORITY
REGARDING OUTSTANDING ISSUE 19(j) (TAC NOS. 79717 AND 80346)
References: Meeting Notice by P. S. Tam (NRC), dated October 22, 1991

The subject meeting was held on October 31, 1991, at NRC headquarters in Rockville, Maryland as a result of the staff's request. The purpose was to specifically address the concern of thermal evaluation of structural steel members, part of the Outstanding Issue 19(j) described in the Watts Bar SER Supplement 6. Enclosure 1 is the meeting attendance list.

The main topic of the discussion concerned allowable ductility ratio for a steel member when subjected to a severe loading combination that includes stresses induced by accident-related temperatures (such as temperatures as the result of a LOCA).

A discussion was held following the handout of documents which were provided by TVA (Enclosures 2-5 of this summary). Enclosure 3 shows that TVA has identified 204 cases of thermal concerns for structural members, of which, 15 cases have been analyzed to be the worst cases. The staff stated that Watts Bar, being a plant applying for an operating license (OL), is expected to follow closely the guidelines of the Standard Review Plan (SRP), specifically, Section 3.8.4; if necessary, and if the cost is not prohibitive, TVA should make suitable modifications to reduce thermal stresses on structural members. TVA personnel stated that they do not believe that Watts Bar is deviating from the SRP guidelines on this issue and while the cost to make modifications may amount to only \$500,000, they do not believe they need to make any modifications since Watts Bar is in compliance. A typical modification, according to TVA, would be an attempt to put in slotted holes to allow for thermal expansion.

The staff also pointed out that the ductility ratio of 3 alone does not provide the staff with the necessary information to make a safety determination; additional attributes such as limits of end rotation, deflection and maximum strain should be established at some acceptable predetermined values.

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E PDR

RFOL
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Meach
EJH

The staff summarized its concerns as follows:

1. TVA should provide experimental data demonstrating that the proposed ductility ratio of three does not mean a state of imminent structural instability (collapse) due to lateral loading, and represents the maintenance of sufficient margin. The experimental data should include, as a minimum, the following parameters:
 - a. beam-column effect,
 - b. compatability and comparability of transverse and axial loads tested to those of Watts Bar beams being evaluated,
 - c. dynamic response due to safe-shutdown earthquake in a post-inelastic region, and
 - d. combination of a. and c. above.

2. Since the ANSYS code is the primary tool to calculate the ductility of a member as well as the extent of the thermal axial load relaxation, there should be a verification of the code based on applicable experiments in an inelastic region. This should include comparison of the ANSYS results with experiments performed in 1. above, as well as numerical studies regarding error estimate and instability associated with the calculations.

The meeting was adjourned with the understanding that TVA will request another meeting with the staff when it is ready to address the concerns identified above.

Original signed by

Peter S. Tam, Senior Project Manager
Project Directorate II-4
Division of Reactor Projects - I/II
Office of Nuclear Reactor Regulation

Enclosures:

1. Attendance List
2. Outline of TVA Presentation
3. Flow Chart on Thermal Task
4. Various Graphs
5. Model of Induced Loads

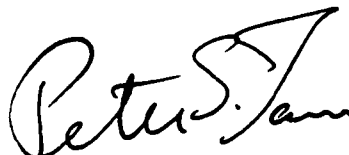
cc w/enclosures:
See next page

OFC	: PDII-4/LA	: PDII-4/PM	: PDII-4/D	: <i>ESGB</i>	:
NAME	: MSanders <i>ms</i>	: PTam:as <i>PST</i>	: FHebdon <i>BT</i>	: GBagchi	:
DATE	: 11/7/91	: 11/7/91	: 11/8/91	: 11/7/91	:

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cc w/enclosures:
See next page

ENCLOSURE 1

NRC-TVA MEETING ON

WATTS BAR NUCLEAR PLANT

OCTOBER 31, 1991

Attendee

Organization

R. K. Alexander	TVA - Watts Bar
Hans Ashar	NRC/NRR/ESGB
Goutam Bagchi	NRC/NRR/ESGB
S. J. Chen	EBASCO
Walter Grossman	Brookhaven National Laboratory
F. J. Hebdon	NRC/NRR/PDII-4
R. O. Hernandez	TVA - Watts Bar
John J. Hughes	TVA - Corporate Engineering
Roger W. Huston	TVA - Rockville Office
David C. Jeng	NRC/NRR/ESGB
Sang Bo Kim	NRC/NRR/ESGB
S. Alan Lin	EBASCO
Wayne A. Massie	TVA - Watts Bar Licensing
Peter S. Tam	NRC/NRR/PDII-4
Joe Williams	NRC/NRR/PDII-4

Enclosure 2

TENNESSEE VALLEY AUTHORITY

WATTS BAR NUCLEAR PLANT

**THERMAL EVALUATION OF
STRUCTURAL STEEL FEATURES**

OCTOBER 31, 1991
9:00 A.M.

NRC OFFICES - WASHINGTON

*THERMAL EVALUATION OF
STRUCTURAL STEEL FEATURES*

AGENDA

OVERVIEW

- SCOPE
- PROBLEM
- RESOLUTION
- IMPLEMENTATION METHODOLOGY

TECHNICAL DISCUSSION

**THERMAL EVALUATION OF
STRUCTURAL STEEL FEATURES**

SCOPE

- **EXTREME THERMAL LOADS**
- **IDENTIFICATION OF STRUCTURAL STEEL
FEATURES**

WATTS BAR NUCLEAR PLANT

*THERMAL EVALUATION OF
STRUCTURAL STEEL FEATURES*

PROBLEM: INCONSISTENT DESIGN PRACTICES

- **LACK OF DESIGN GUIDANCE**
- **EXPANSION CAPABILITY**
- **SELF-RELIEVING AND DUCTILE BEHAVIOR**

WATTS BAR NUCLEAR PLANT

*THERMAL EVALUATION OF
STRUCTURAL STEEL FEATURES*

RESOLUTION: EXPLICIT DESIGN GUIDANCE

- **SELF-RELIEVING BEHAVIOR**
- **DUCTILE BEHAVIOR**
- **LOAD COMBINATIONS**

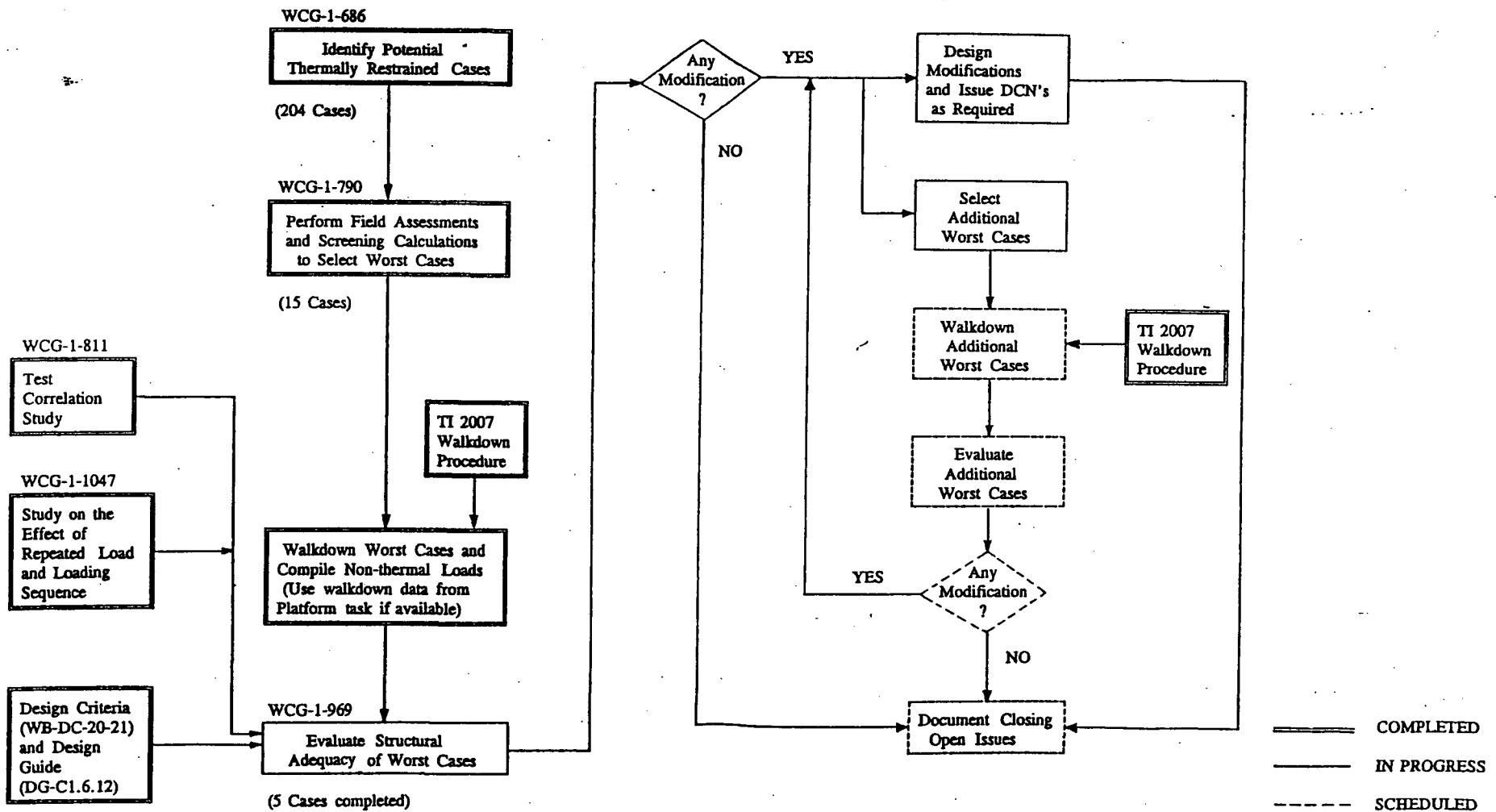
*THERMAL EVALUATION OF
STRUCTURAL STEEL FEATURES*

IMPLEMENTATION METHODOLOGY

- **IDENTIFICATION OF RESTRAINT CONDITIONS**
- **GROUPING OF STRUCTURES**
- **ANALYSIS AND EVALUATION**
- **ACCEPTANCE CRITERIA**
- **MODIFICATIONS**

THERMAL TASK OVERVIEW

September 1991

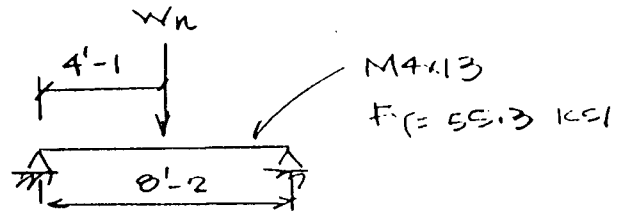
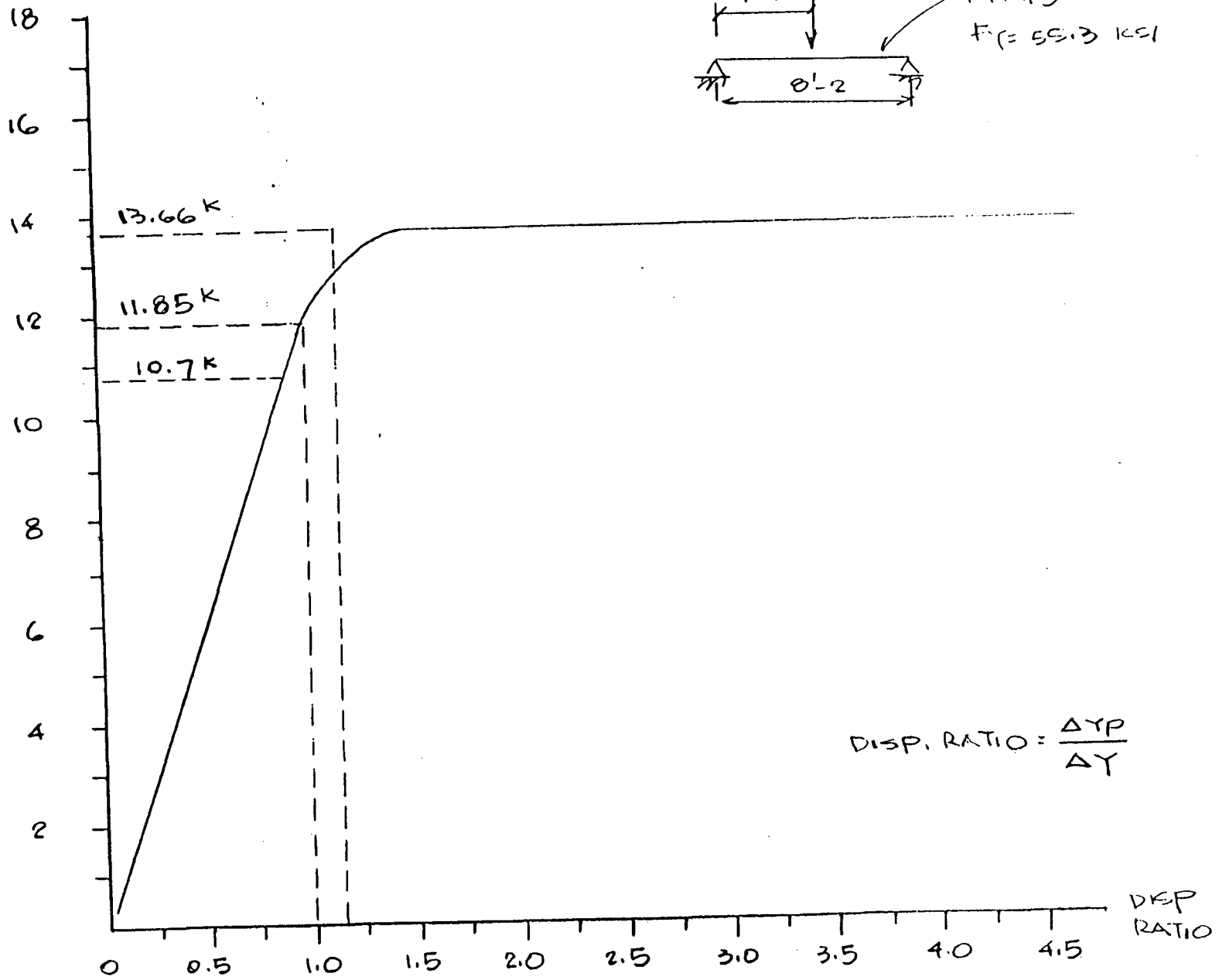


Enclosure 3

WORST CASE EVALUATION RESULTS

<u>Worst Case</u>	<u>Ductility Ratio/Calculation</u>	<u>Remarks</u>
1 - 11	$\mu < 1$ (WCG-1-969)	Linear
1 - 22	$\mu = 2.9$ (Preliminary)	Potential Modification
1 - 23	$\mu = 1.9$ (Preliminary)	Potential Modification
1 - 26	$\mu < 1$ (WCG-1-970)	Linear
1 - 28	$\mu = 4.4$ (Preliminary)	Modification Projected
2 & 3 - 2 (D)	$\mu = 2.1$ (WCG-1-970)	
1 - 37 2 & 3 - 5(H)	$\mu > 3$ (Preliminary) $1 < \mu < 3$ (Preliminary)	Modification Projected
1 - 38 2 & 3 - 6(J)	$\mu = 5.1$ (WCG-1-970) $\mu = 2.1$ (WCG-1-970)	Modification/Additional Case Potential Modification
2 & 3 - 7(I)	$\mu = 2$ (WCG-1-970)	
2 & 3 - 8(G)	$\mu < 1$ (WCG-1-969)	Linear
1 - 27	$\mu = 3.3$ (WCG-1-969)	Modification/Additional Case
2 & 3 - 9(C)	$\mu < 1$ (WCG-1-969)	Linear
5 - 7	$\mu < 1$ (WCG-1-969)	Linear

EQUIVALENT
LATERAL FORCE IN KIP

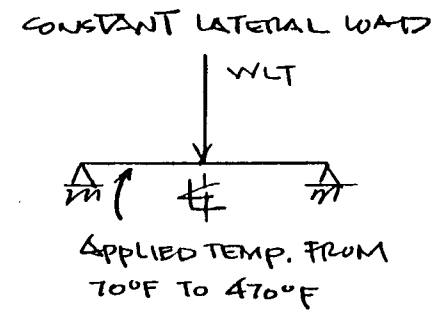
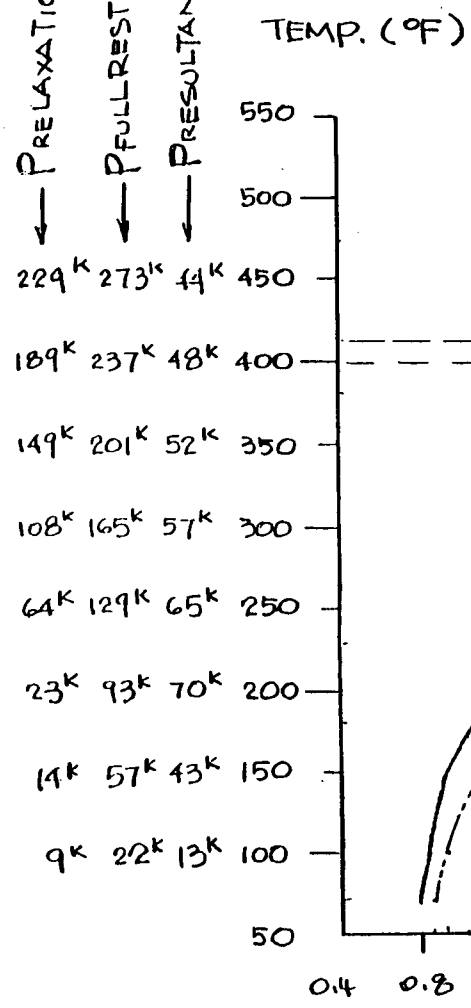


EBASCO SERVICES INCORPORATED

Enclosure 4

WLT = 8.2 K

PRELAXATION*
FULL RESTRAINT
PRESULTANT

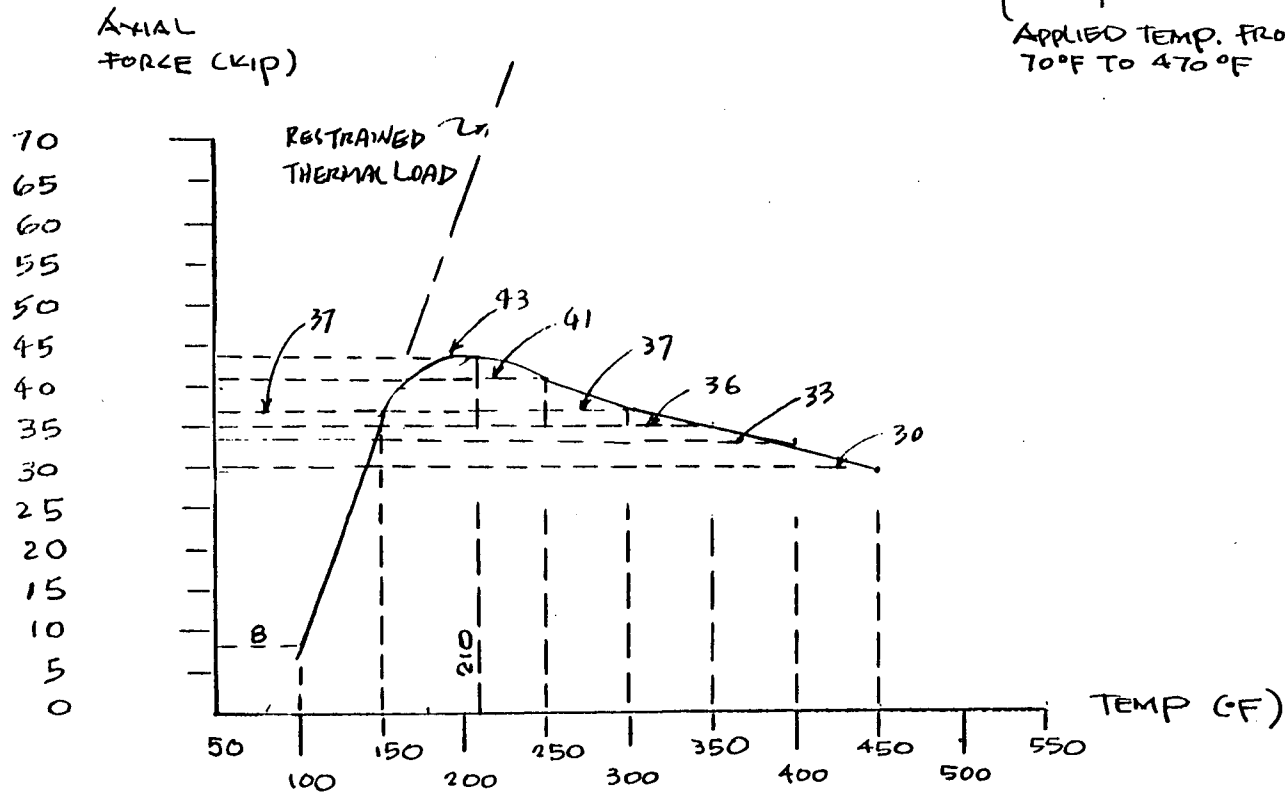
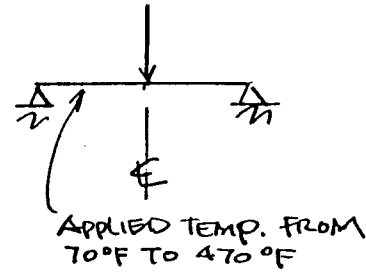


* RELAXATION DUE TO YIELDING AND CURVATURE.

$$\text{DISP. RATIO} = \frac{\text{ACTUAL LATERAL DISP.}}{\text{LATERAL DISP. @ YIELD}}$$

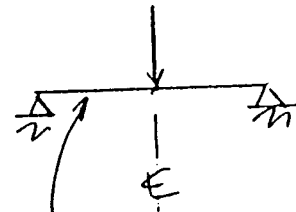
EBASCO SERVICES INCORPORATED

CONSTANT LATERAL LOAD = 10.7 K



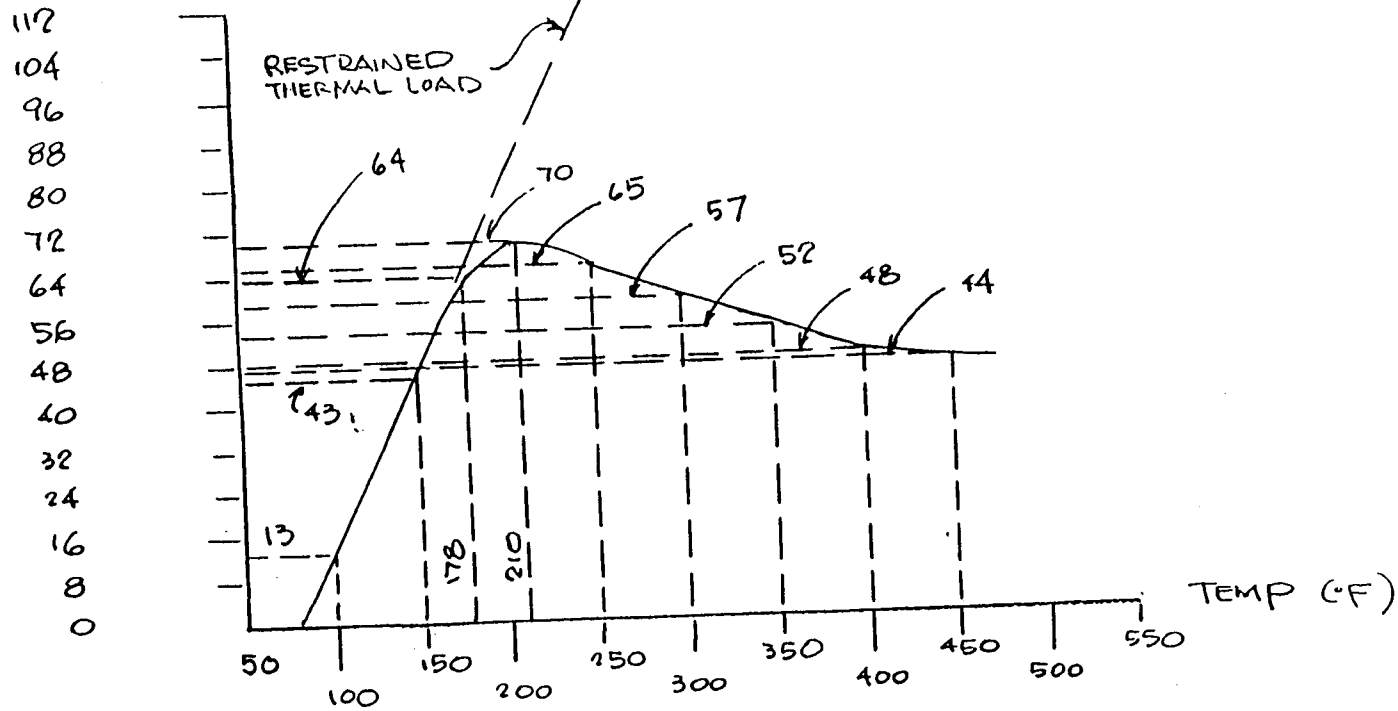
EBASCO SERVICES INCORPORATED

CONSTANT LATERAL LOAD = 8.2 K

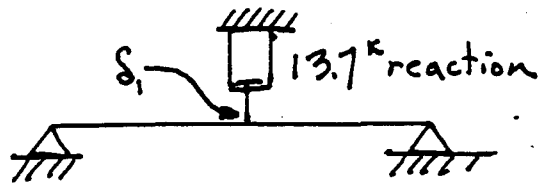


APPLIED TEMP. FROM 70°F TO 470°F

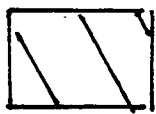
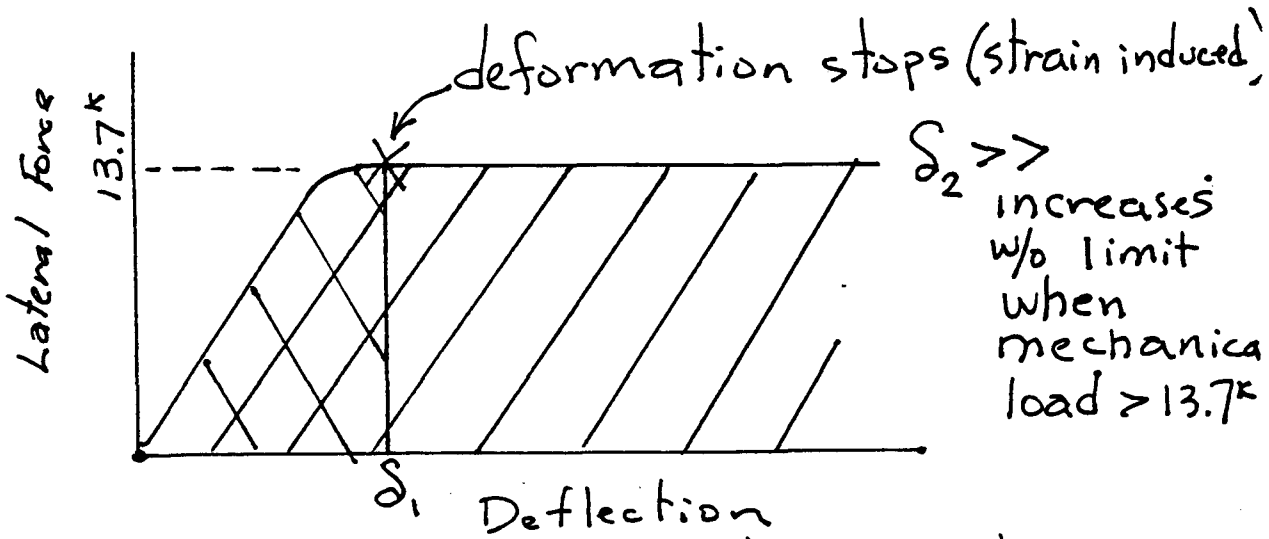
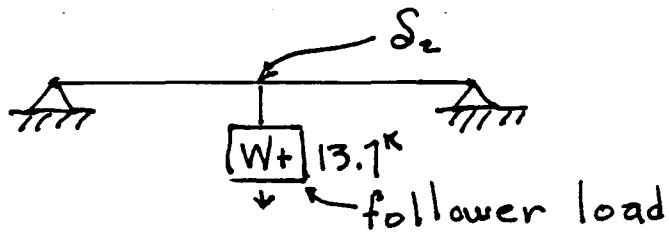
AXIAL FORCE (KIP)



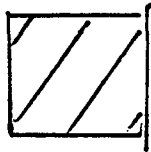
Strain Induced Load



Mechanically Induced Load



Available strain induced energy (limited)



Available mechanically induced energy is unlimited (δ_2 is not controlled)

Distribution (with enclosures)

Docket File
NRC PDR
Local PDR

Distribution (without Enclosures 2 - 5)

F. Miraglia	12-G-18
J. Partlow	12-G-18
S. Varga	14-E-4
G. Lainas	14-H-3
F. Hebdon	
M. Sanders	
P. Tam	
B. Wilson	RII
J. Weschelberger	17-G-21
G. Walton	RII
H. Livermore	RII
OGC	15-B-18
E. Jordan	MNBB-3701
David C. Jeng	7-H-15
S. B. Kim	7-H-15
G. Bagchi	7-H-15
J. Williams	14-B-21
ACRS (10)	
WBN Reading File	