

REACTOR CONTAINMENT BUILDING
INTEGRATED LEAK RATE TEST
WATTS BAR NUCLEAR PLANT UNIT 1

CONDUCTED JUNE 22-29, 1994

Docket No. 50-390

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Reactor Containment Building
Integrated Leak Rate Test
Watts Bar Nuclear Plant Unit 1

Conducted June 22-29, 1994

Test Report

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This report contains the summary technical analysis of the Reactor Containment Building Integrated Leak Rate Test (CILRT) conducted on Watts Bar Nuclear Plant (WBN) Unit 1 June 22-29. As prescribed in WBN Unit 1 Technical Specification 3.6.1.1, the leakage of air from the boundary forming the reactor primary Containment Building is limited to 0.25 percent by weight of the containment air mass per day at a pressure of 15.0 psig. This test was conducted in accordance with the requirements of Title 10, Code of Federal Regulations, Part 50, Appendix J, which is implemented by WBN Surveillance Instructions (SI) 1-SI-0-703. The American National Standard for Containment Testing, ANSI 45.4-1972, the proposed American Nuclear Society for Containment Testing, ANS 56.8, and the procedure outlined in Bechtel's Topical Report, "Testing Criteria for Integrated Leakage Rate Testing of Primary Containment Structure for Nuclear Power Plants" (BN-TOP-1, Revision 1), provided guidance for the procedure implemented by the SI.

WBN Unit 1 is a 3,425-megawatt thermal, pressurized-water reactor employing an ice condenser pressure suppression containment. The Final Safety Analysis Report defines the calculated peak accident pressure, Pa, to be 15.0 psig. The Reactor Building containment is divided into three major compartments for the CILRT analysis--the ice condenser compartment which houses the energy-absorbing ice beds and the support equipment for the ice condenser system, the lower compartment which contains the reactor and the main piping systems,

and the upper compartment which can accommodate the displaced air mass from the other compartments in the unlikely event of a loss-of-coolant accident (LOCA). These three compartments are connected by means of lower inlet doors (which open under a pressure differential) located between the lower compartment and bottom of the ice condenser compartment and blowout panels located between the upper compartment and top of the ice condenser compartment. In the event of a LOCA, steam flows from the lower compartment through the ice condenser compartment and into the upper compartment. The upper compartment is sealed from the lower compartment to ensure that any steam released in an accident will be forced through energy-absorbing ice beds. For the performance of the CILRT, the lower and upper compartments were not completely sealed from each other in order to provide access for test instrumentation cables and to promote the flow of air in containment.

This report outlines the objectives, principal events, special equipment used, and analysis of the test results for the CILRT completed on June 29, 1994, on WBN Unit 1. A summary of local leak rate tests (LLRTs) conducted prior to the CILRT are included in Appendix L.

2.0 SUMMARY

The WBN Unit 1 CILRT was conducted from June 22 to 29, 1994 in preparation for initial fuel load. The CILRT was successfully completed in 29 hours and 36 minutes and included 178 data samples.

Prior to performing the GILRT, the mass point leak rate (MLR) calculation technique was designated as the method that would be used for data analysis. The calculated MLR for the GILRT was 0.01379 percent per day (%/day). The associated reportable "as found" 95 percent upper confidence limit (UCL), which includes Type B and C leakages from testable penetrations in service at the time of the GILRT and water level changes not accounted for by the GILRT computer system, was 0.01669 %/day. The calculated total time leak rate (TTLR) was 0.01923 %/day. The associated reportable "as found" 95 percent upper confidence limit (UCL), which includes Type B and C leakages from testable penetrations in service at the time of the GILRT and water level changes not accounted for by the GILRT computer system, was 0.03766 %/day.

3.0

TEST PURPOSE AND RESULTS

3.1 Test Purpose

The objective of the preoperational GILRT was twofold. The primary objective of the GILRT was to demonstrate the leak tight integrity of the Unit 1 Reactor Building containment prior to power operation.

A problem unique to preoperational GILRT'S is that of possible incomplete construction. Therefore, the second objective was to verify that there were no unidentified openings in the containment vessel.

For Unit 1, the leak tight integrity is defined in Technical Specification 3.6.1.1 to be that the leakage of air from containment is not to exceed 0.1875 percent per day at peak accident pressure, P_a .

3.2 Test Results

Initial pressurization to 15.25 psig was completed at 0440 hours on June 24, 1994, and the pressurization header was isolated from the air compressors.

The criteria for temperature stabilization phase was met at 1115 hours on June 24, 1994. Although the pressurization rate had been limited to minimize destabilizing the containment parameters, the data was unstable beyond the initial four hours.

The pressurization rate had been controlled to achieve test pressure in about 10 hours. This was done to limit gross changes in containment vapor pressure and temperature. However, there was a temperature inversion with an increase in humidity in the 24 hours immediately preceding pressurization for the Unit 1 CILRT. This inversion was partially countered by limiting the pressurization rate; however, the stabilization phase had to be extended so that the total stabilization time was 6 hours and 35 minutes.

Additionally, completion of a preoperational test to verify the leak-tightness of containment pressure monitor sensing lines while the primary containment was at accident pressure necessitated

extending the stabilization time until 1223 hours for a total time of 7 hours and 13 minutes.

Although stabilization temperature criteria had been met, the ice condenser compartment temperature had been trending upward during the stabilization period. Operations personnel were working with glycol chillers and recirculation pumps to stabilize the compartment.

At 1910 hours, it had become evident that the ice condenser compartment temperature could not be stabilized. Evidence of a flow restriction in the glycol system inside the containment building was apparent. The decision was made to terminate the test, reduce pressure to below 14.3 psig to allow more convenient entries into containment, and resolve the system problems before proceeding.

An inspection of the air handling units (AHU's) inside the ice condenser found 35 of 60 units in tripped status. All units were reset. A second inspection was performed approximately three hours later, and again multiple AHU's were tripped. Electrical current measurements showed that the units were tripping on overcurrent at the elevated containment pressure.

AHU thermal overloads were examined and found to be adjustable. An engineering calculation was performed to ascertain the acceptability of increasing the overload setpoints from the existing 1.0 setting to a setting of 1.15. This increased setting did not significantly reduce the number of AHU's tripping.

The final adjustment made to the AHU's to prevent tripping during the test was to restrict the blower outlet damper opening on the units that were drawing more than their rated current. This adjustment was successful, and the test sequence was resumed.

Repressurization of containment commenced at 2245 hours on June 26. Pressurization to 15.255 psig was completed at 0313 hours on June 27, and the pressurization header was isolated from the air compressors. Stabilization temperature criteria was met after the required 4 hour period, and the 24 hour integrated leak rate test period began at 0722 hours.

The ice condenser temperature was controlled to within a narrow temperature band of approximately 2 degrees Fahrenheit during both the leak test period and the verification test period. However, due to the low leak rate measured, the relatively small temperature changes had a significant impact on testing. The rapidity of the changes (aggravated by the lack of the temperature-moderating ice mass) resulted in a magnification of their effect on the test parameters and caused the measured leak rate to appear lower or higher than actual, thereby increasing the time required to determine the true leak rate.

At approximately 11 hours and 20 minutes into the 24 hour leak rate test period, a glycol system chiller package tripped due to low flow. The sudden, unexpected trip caused a temporary surge in the glycol expansion tank level inside containment. This rapid level

change resulted in a pressure spike which was reflected throughout the containment. An apparent mass increase, corresponding to the pressure increase, ensued. This drove the measured leak rate into the negative range. Recovery from this perturbation, along with the temperature swings in the ice condenser, resulted in the duration of the test being extended to 29 hours and 36 minutes to obtain a stable and accurate leak rate.

The verification leak rate test was also extended from 4 hours to 9 hours and 7 minutes due to oscillations in the measured leak rate. Again, these oscillations were caused by the sudden temperature swings in the ice condenser compartment.

The following table presents the test results for the CILRT and verification tests. Additional specific data on these tests are included in the appendices.

Table of GILRT and Verification Test Results

Post Test ISG 0.032 percent of La (using repeatability)

| | MLR | TTLR |
|--|----------------------|----------------------|
| 1. Leakage for systems in service during test. | 0.00000 %/day | 0.00000 %/day |
| 2. Calculated 95% UCL during test. | 0.01106 %/day | 0.03203 %/day |
| 3. Leakage due to pressurizer level change | 0.00551 %/day | 0.00551 %/day |
| 4. Leakage due to sump level increase. | <u>0.00012 %/day</u> | <u>0.00012 %/day</u> |
| Total | 0.01669 %/day | 0.03766 %/day |

GILRT duration: 29 hours and 36 minutes
 Number of samples: 178

Verification Test

MLR agreement: -8.7 % La
 TTLR agreement: -6.0 % La

Verification duration: 9 hours and 7 minutes
 Number of samples: 109

Extended ANSI statistical analysis for GILRT (satisfaction of equations 1.1 or 1.2 and 2.1 is required)

| | | | | |
|----------|-----|---------|---|-----|
| Equation | 1.1 | 5.2392 | < | 1.0 |
| | 1.2 | 0.3890 | < | 1.0 |
| | 2.1 | 11.6742 | > | 1.0 |

4.0 CONDUCT OF TEST

The following is a summary of chronological events associated with the CILRT.

| <u>Dates and Time</u> | <u>Event</u> |
|-----------------------|--|
| 06/22/94 1800 | Completed 1-SI-88-4, "40 Month Visual Inspection of the Steel Containment Vessel". |
| 06/23/94 0141 | Completed final containment walkdown. |
| 06/23/94 0355 | Started compressors. |
| 06/23/94 0426 | Started pressurization. |
| 06/23/94 0430 | Compressors stopped. Apparent restriction in pressurization line. |
| 06/23/94 0700 | Found blind flange installed in temporary pressurization assembly. |
| 06/23/94 1630 | Issued Change notice to test instruction to place hold order on SSPS output breakers after discovering that previous software changes which bypassed channels for containment pressure signals could be inadvertently overridden and the channels reset to active status in the event of a short power interruption to the SSPS. |

06/23/94 1835 Blind flange removed from pressurization assembly;
received permission to pressurize containment.

06/23/94 1843 Started pressurization.

06/24/94 0440 Pressurization complete; stopped compressors.

06/24/94 0448 Pressurization header isolation valve shut.

06/24/94 0453 Containment pressure 15.25 psig; began stabilization.

06/24/94 0930 Pressurization header isolated and removed from
compressor.

06/24/94 1115 Met stabilization temperature criteria, but awaiting
post-modification inservice leak checks of containment
pressure monitor instrument lines to be completed.

06/24/94 1223 Started CILRT, but ice condenser compartment temperature
increasing significantly.

06/24/94 1910 Decision made by test director to terminate CILRT
because ice condenser compartment temperature has been
increasing more rapidly and Operations is unable to
stabilize. Temperature problem must be resolved prior to
resuming test.

06/24/94 2340 Began depressurization of containment to less than 14.3 psig to allow entries at less than one atmosphere for inspection/repair of ice condenser problems.

06/25/94 0030 Completed depressurization to 12.62 psig.

06/25/94 0900 Two entries made into containment found multiple ice condenser Air handling units (AHU) tripped.

06/25/94 1717 Permission received from Nuclear Engineering to reset AHU thermal overloads reset from 1.0 to 1.15. Thermal overloads reset.

06/25/94 Entry into containment found AHU's still tripping out almost immediately.

06/25/94 2330 Replacement of several AHU thermal overloads complete. AHU's still tripping. Measurements show current too high.

06/26/94 1050 Entered containment to throttle AHU discharge dampers to reduce current.

06/26/94 1804 Ice condenser temperature decreasing since throttling of AHU discharge dampers. Entered containment to verify operation.

06/26/94 2035 Finalizing preparations for repressurization of containment to test pressure.

06/26/94 2245 Started pressurization.

06/27/94 0313 Pressurization complete; stopped compressors.

06/27/94 0315 Containment pressure at 15.255 psig. Pressurization header isolation valve shut. Began stabilization.

06/27/94 0520 Pressurization header isolated and removed from compressor.

06/27/94 0722 Stabilization criteria met. Started CILRT at sample number 57.

06/27/94 2147 Very low measured leak rate went into negative range due to temperature cycling in the ice condenser and pressure surge in containment (Glycol chiller tripped).

06/28/94 0418 Leak rate went back into positive range. Still very low but increasing slowly.

06/28/94 1258 Terminated CILRT at sample number 234. Leak rate steady at .016472 percent per day; UCL at .019415 percent per day.

06/28/94 1330 Establish verification flow of 248.40 SCFH.

06/28/94 1428 Started verification with sample Number 243

06/28/94 2335 End verification with sample Number 351. Preliminary agreement -7.16 percent.

06/29/94 0113 Started depressurization.

06/29/94 0700 Containment pressure at 0.0 psig.

5.0 MEASUREMENTS AND CALCULATIONS

5.1 Test-Equipment

Appendix K lists the range, accuracy, and repeatability of the special test equipment used in the Unit 1 Preoperational GILRT.

5.2 Sensor Location

Appendix J lists the final volumetric weighing factor for each temperature and dewpoint sensor based on the 3-compartment model.

The associated figures indicate sensor locations. The pressure sensors were divided so that two sensors measured each of the three compartments through penetrations X-26A, X-96A, and X-96B.

Utilizing two pressure sensors per compartment allows the removal of any one malfunctioning pressure gauge during the test while

continuing to accurately monitor containment pressure. An additional pressure gauge measured barometric pressure at the test station.

5.3 Computer-Based Data Acquisition and Data Reduction

The test data measured by the special test instrumentation during the WBN Unit 1 CILRT was automatically scanned and collected by a PC computer system and then reduced. The computer produced immediate statistical and graphical results of the containment test parameters, including temperature, pressure, vapor pressure, mass, MLR, and TTLR plots.

These calculated results were reported automatically to the test director as the data was collected. Appendix I depicts the functional relationship between the special test instrumentation and the PC computer system.

All calculations performed by the computer system were in conformance with the procedure outlined in ANS 56.8, ANSI 45.4, and/or Bechtel Topical Report (BN-TOP-1), Revision 1.

Software used by the PC was purchased from Duke Engineering Company. Source listings for all computer programs are on file with the Plant Operating Systems group in Chattanooga, Tennessee. Additional software Commercial Dedication, Software Description, and User's manuals are located in the WBN Technical Support organization.

5.4 Reactor Building Containment Model

An ice condenser pressure suppression containment presents special problems not normally encountered in the leak testing of dry containment structures. The pressure suppression design feature requires the Reactor Building containment to be divided into distinct compartments, where vastly different temperatures and vapor pressures may exist. While each compartment is vented to the containment atmosphere during the performance of the CILRT, the direct circulation of air is limited.

Since an ice condenser containment typically exhibits a 40°F temperature differential between the ice compartments and others, it is necessary to compensate by compartmentalization so the leak rate is accurately measured. For the WBN Unit I CILRT, a 3-compartment containment model was used to measure the leak rate.

The free air mass was calculated individually for each compartment, and the containment leak rate was calculated from the sum of the compartmental masses.

Each sensor within the upper and lower containment compartments was volume weighted for the calculation of compartment average temperature, vapor pressure, and absolute pressure. Sensors for the calculation of the ice condenser compartment average temperature and pressure were volume weighted, but the relative humidity sensors were set to zero due to a question that arose prior to the test as

to the adequacy of the range required in the ice condenser. A conservative assumption of zero vapor pressure in this compartment was used for all calculations in this report. In retrospect, the measured relative humidity levels in the ice condenser compartment during the test were within the range of the instruments.

6.0 ANALYSIS OF TEST DATA

The previous sections of this report have discussed the general test conduct and test equipment. In this section, events and problems that influenced the test results are discussed and are used to formulate conclusions on the performance of the WBN Unit 1 Preoperational CILRT.

6.1 Instrument Check

The instrument complement for WBN Unit 1 was 50 temperature sensors (49 containment temperature sensors and 1 atmospheric temperature sensor), 13 relative humidity sensors (5 after deletion of the ice condenser compartment sensors and 1 upper compartment sensor found to be out of tolerance), 1 mass flow meter (for verification test flow), and 7 absolute pressure gauges (6 containment pressure gauges and one atmospheric pressure gauge).

Prior to the start of the test, several temperature and humidity sensors were removed from the data base. The mode of failure

appeared to be overranging. The primary cause was discovered to be an error in the timing setup in the software. All instrumentation that was initially removed from the data base was restored prior to the start of the CILRT, and no further sensor problems were experienced during the testing sequence. However, post-test calibration of the instrumentation showed one upper containment compartment relative humidity sensor to be out of tolerance. This sensor, RHE-1, was subsequently deleted from the calculations and the volume fractions of the remaining two upper compartment relative humidity sensors were adjusted to compensate for the sensor loss.

6.2 Discussions of Graphical and Tabular Results of the CILRT

Upon completion of initial pressurization and the subsequent repressurization from approximately 12.5 psig to test pressure, the relevant parameters began to achieve equilibrium conditions. The vapor pressure throughout containment was higher by a factor of approximately 1.75 over that which is normally expected when near equilibrium conditions exist. This condition was apparently caused by the temperature and humidity inversion which occurred prior to the test (i.e., the temperature dropped and it rained before and throughout both periods of pressurization). This highly humid condition resulted in prolonging the initial stabilization period (first test attempt) and caused less than ideal vapor pressure conditions to exist for the entire testing sequence. The vapor pressure dropped continuously throughout the test period.

The ice condenser compartment was a source of instability throughout the CILRT test and verification test phases. The initial problem of the tripping of the ice condenser air handling units coupled with the continuously inconsistent operation of the glycol cooling system caused temperature variations which resulted in swings in the leak rate data. These temperature variations were relatively large in magnitude and occurred rapidly due to the absence of ice (which would have served as a moderator) in the ice condenser. These variations ultimately resulted in prolonging both test phases.

In addition to the ice condenser temperature problems, the trip of a glycol chiller package approximately twelve hours into the CILRT test phase caused a surge in the glycol expansion tank level inside the upper containment compartment, which caused a pressure spike throughout containment. This resulted in the appearance of an increase in the containment mass and a corresponding negative leak rate for a period of approximately six hours. Although the leak rate returned to the positive range after the six hour period, recovery to a stable leak rate value required extending the test period from twenty four hours to twenty nine hours and thirty six minutes.

Following the containment pressure spike, an investigation of possible causes other than the glycol tank surge was conducted to ensure no other changes in conditions had occurred. A trace of the pressurizer level over the time period in question was obtained from the control room. This represented the only other level other than

the Reactor Building Floor and Equipment Drain Sump (RBFEDS) and the Auxiliary RBFEDS inside containment which could have been changed to cause a rapid increase in pressure. The trace showed that the pressurizer level remained essentially constant before, during, and after the event. The RBFEDS and ARBFEDS levels were checked after the test completion and the small increase in their respective levels was consistent with the level trends determined prior to the CILRT. It was concluded that these levels did not contribute to the containment pressure spike. No other anomalies were identified.

With the exceptions discussed above, the CILRT progressed satisfactorily to completion in accordance with the requirements of ANSI 45.4 and ANSI 56.8.

6.3 Discussion of Agreement (Verification Test)

Verification flow was allowed to stabilize for approximately one hour prior to the official start of the verification test.

A large and rapid temperature increase in the ice condenser compartment occurred approximately three hours and twenty minutes into the verification test period. This elevated temperature remained in the compartment for about two hours and resulted in the measured leak rate value falling below the acceptable range of agreement. After this event, the ice condenser temperature began a decline, which persisted for the remainder of the verification test period. The verification test was extended from the required four

hours to nine hours and seven minutes to allow the measured leak rate to return to an acceptable value and stabilize. No other significant trends or events occurred which affected test results.

7.0 CONCLUSIONS

The WBN Unit 1 preoperational CILRT was conducted with a total reportable leak rate of 0.01669 percent day (MLR) which is only 6.7 percent of the Technical Specification limit of 0.25 percent per day. The corresponding total (TTLR) leak rate was 0.03766 percent per day, which is only 15.1 percent of the limit allowed by Technical Specifications.

APPENDIX A

Stabilization Phase Graphs and Tabular Data

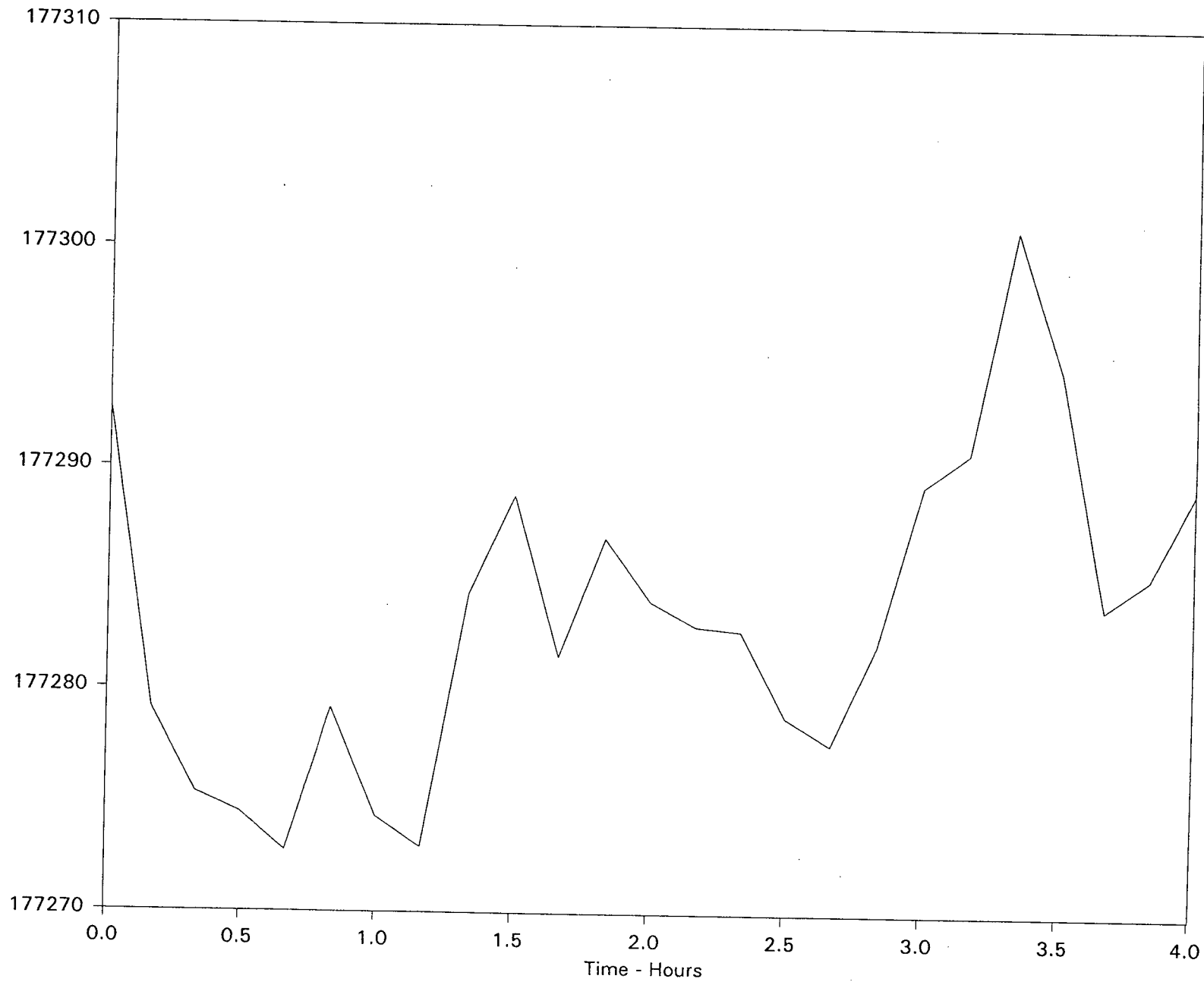
Contents: Temperature stabilization criteria - samples 32 to 56

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| Total Containment Mass | 23 |
| Upper Containment Compartment Mass | 24 |
| Lower Containment Compartment Mass | 25 |
| Ice Condenser Compartment Mass | 26 |
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Containment Mass

Watts Bar Nuclear Plant
Unit 1 - Startup

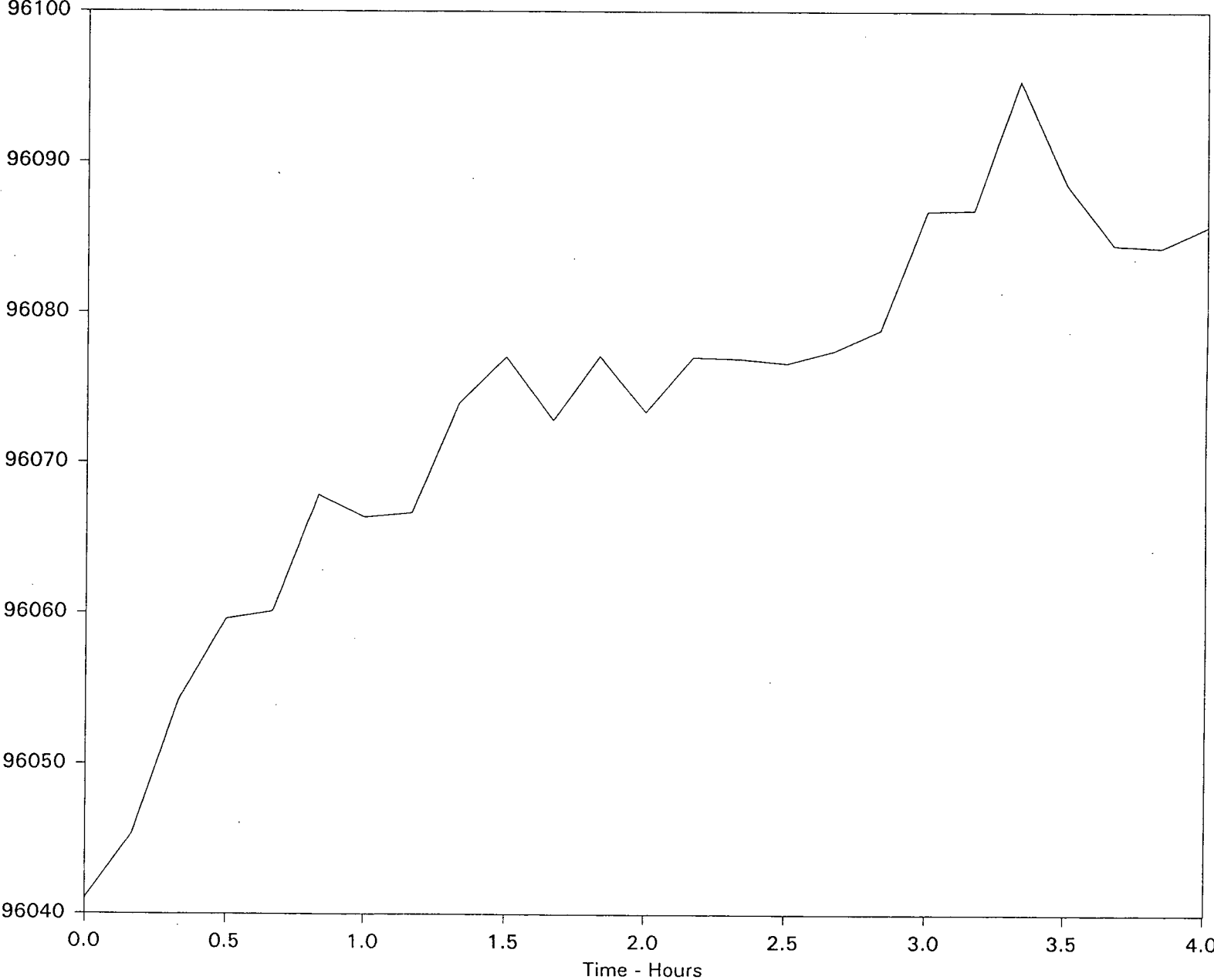
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Upper Containment Mass

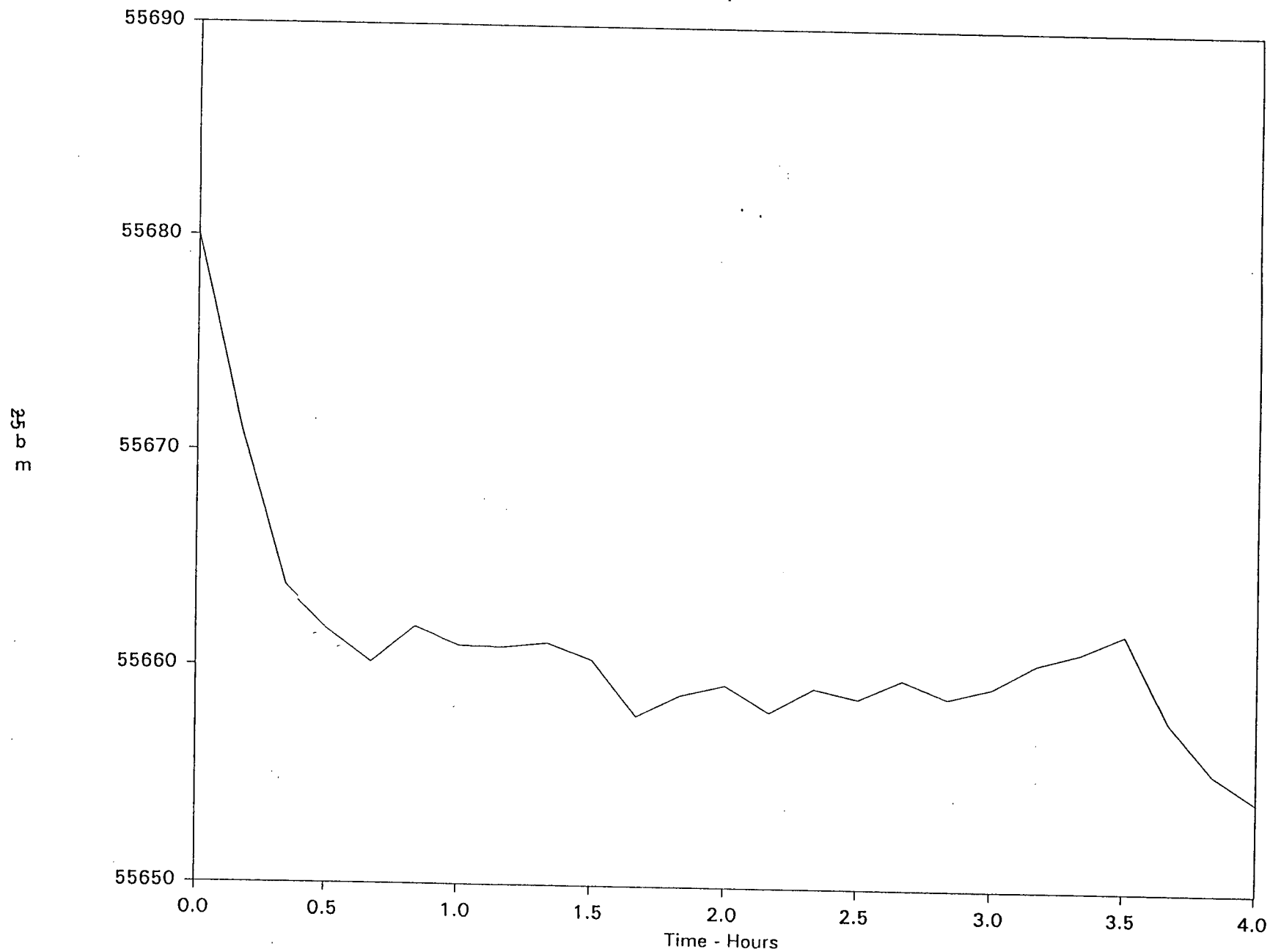
Watts Bar Nuclear Plant
Unit 1 - Startup

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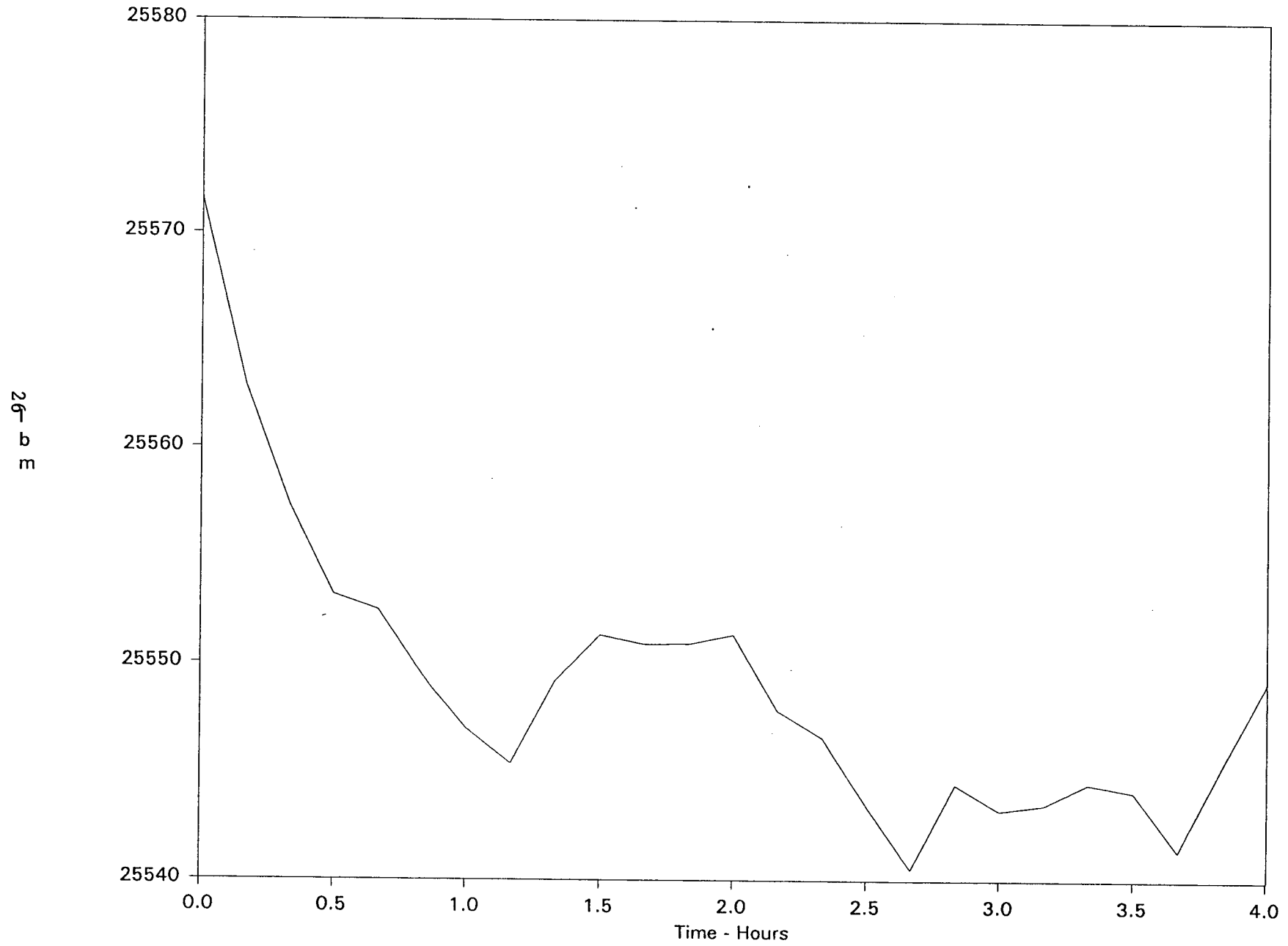
Lower Containment Mass

Watts Bar Nuclear Plant
Unit 1 - Startup



Ice Condenser Mass

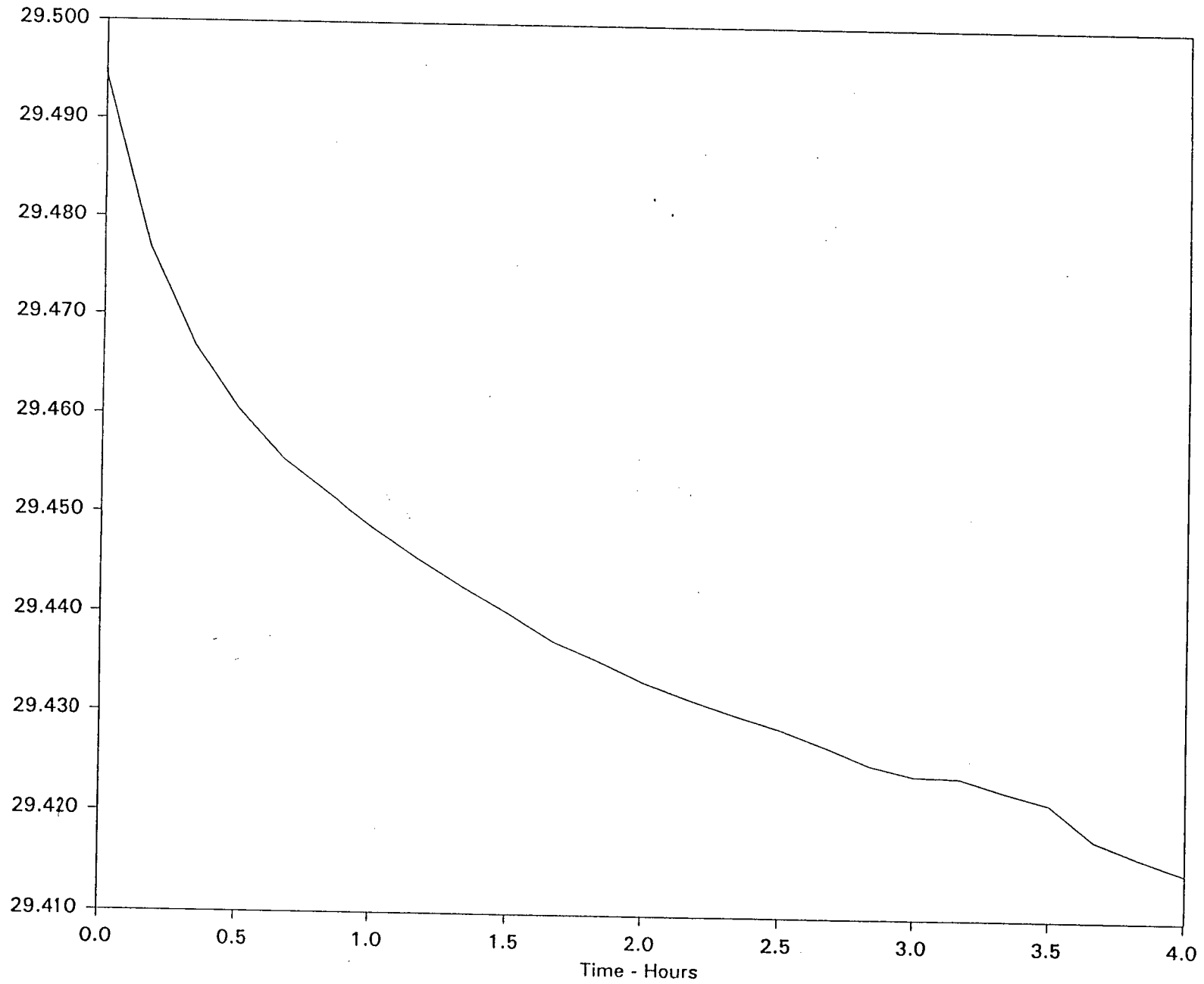
Watts Bar Nuclear Plant
Unit 1 - Startup



Upper Containment Average Pressure

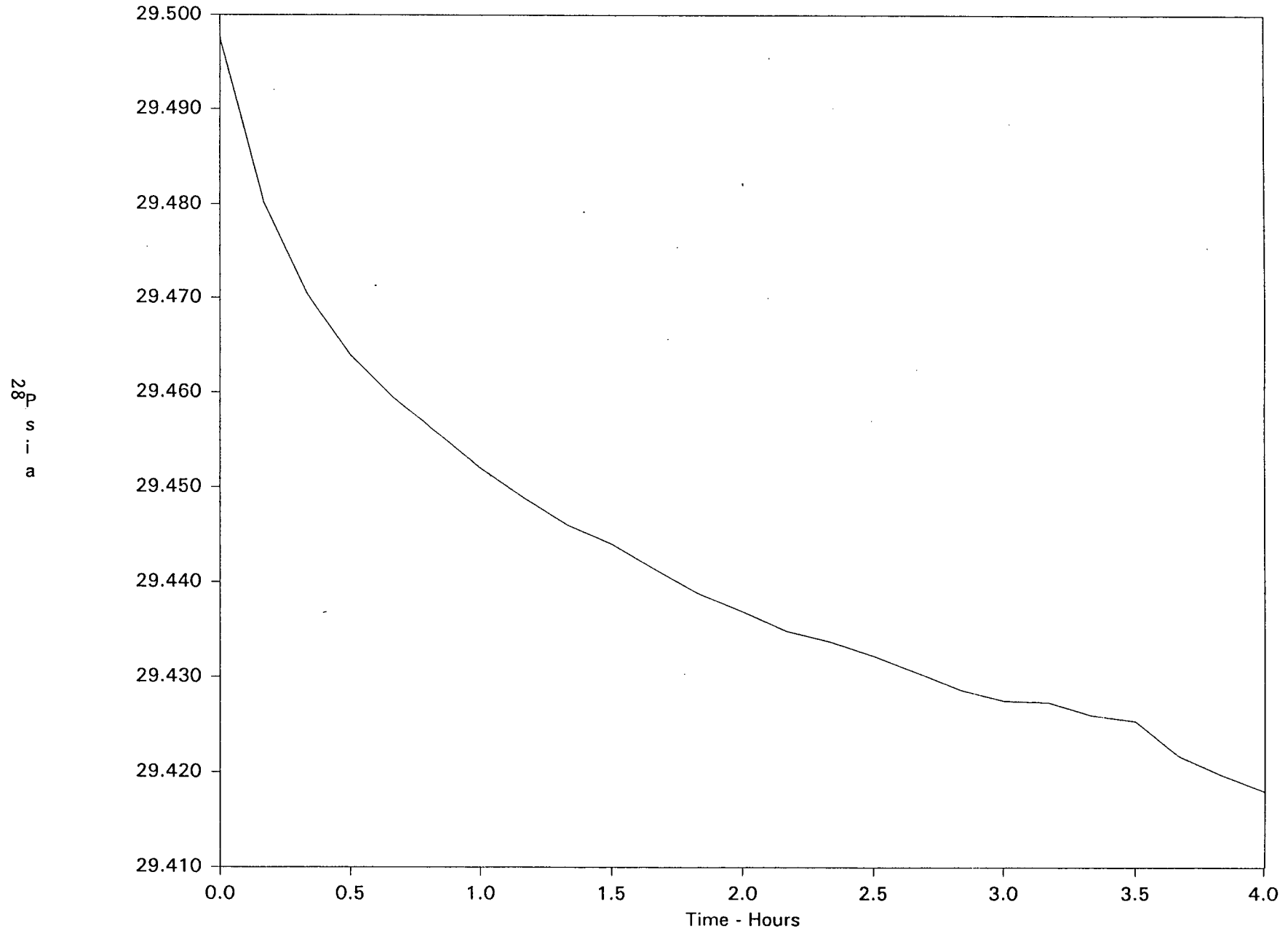
Watts Bar Nuclear Plant
Unit 1 - Startup

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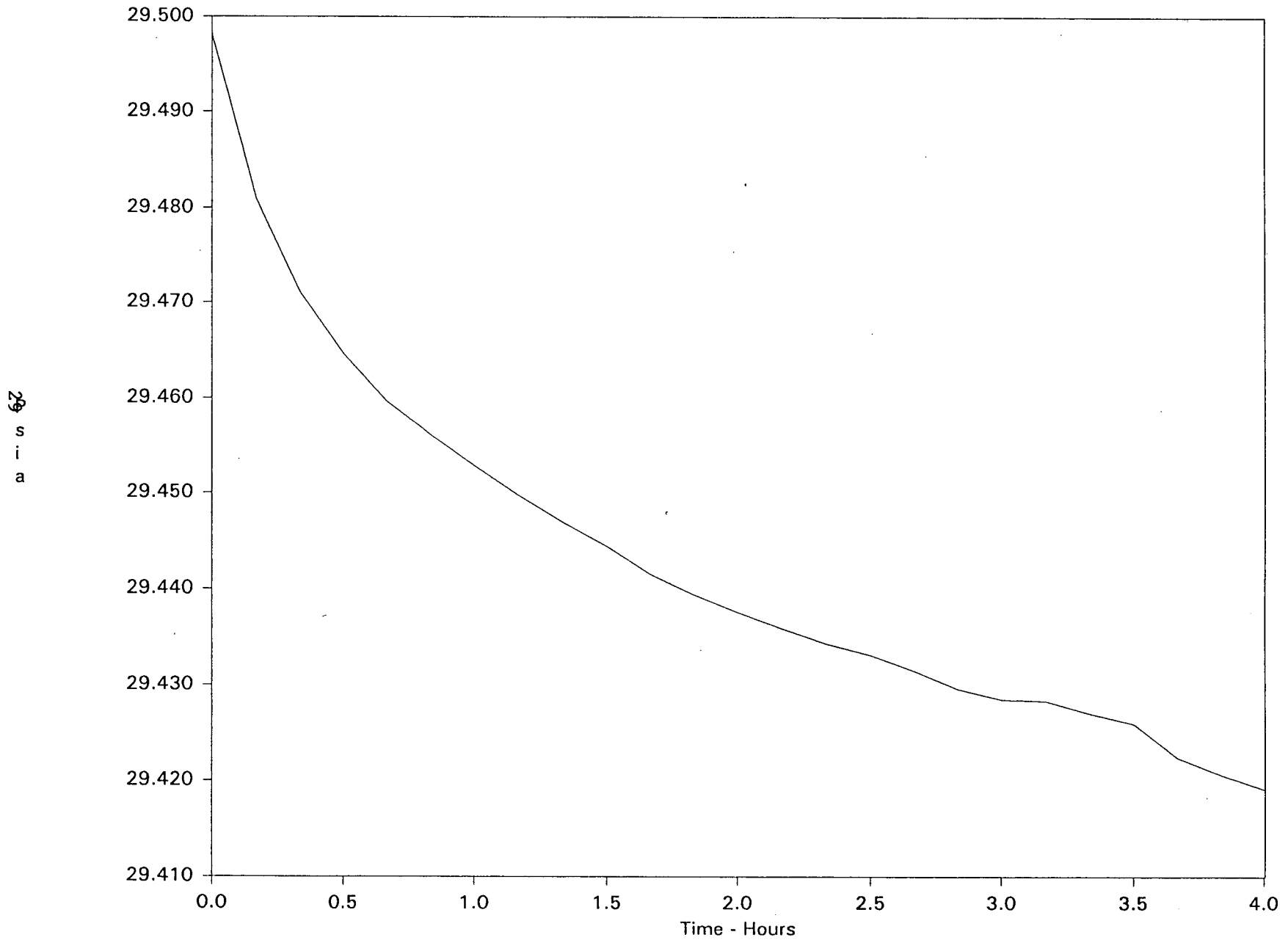
Lower Containment Average Pressure

Watts Bar Nuclear Plant
Unit 1 - Startup



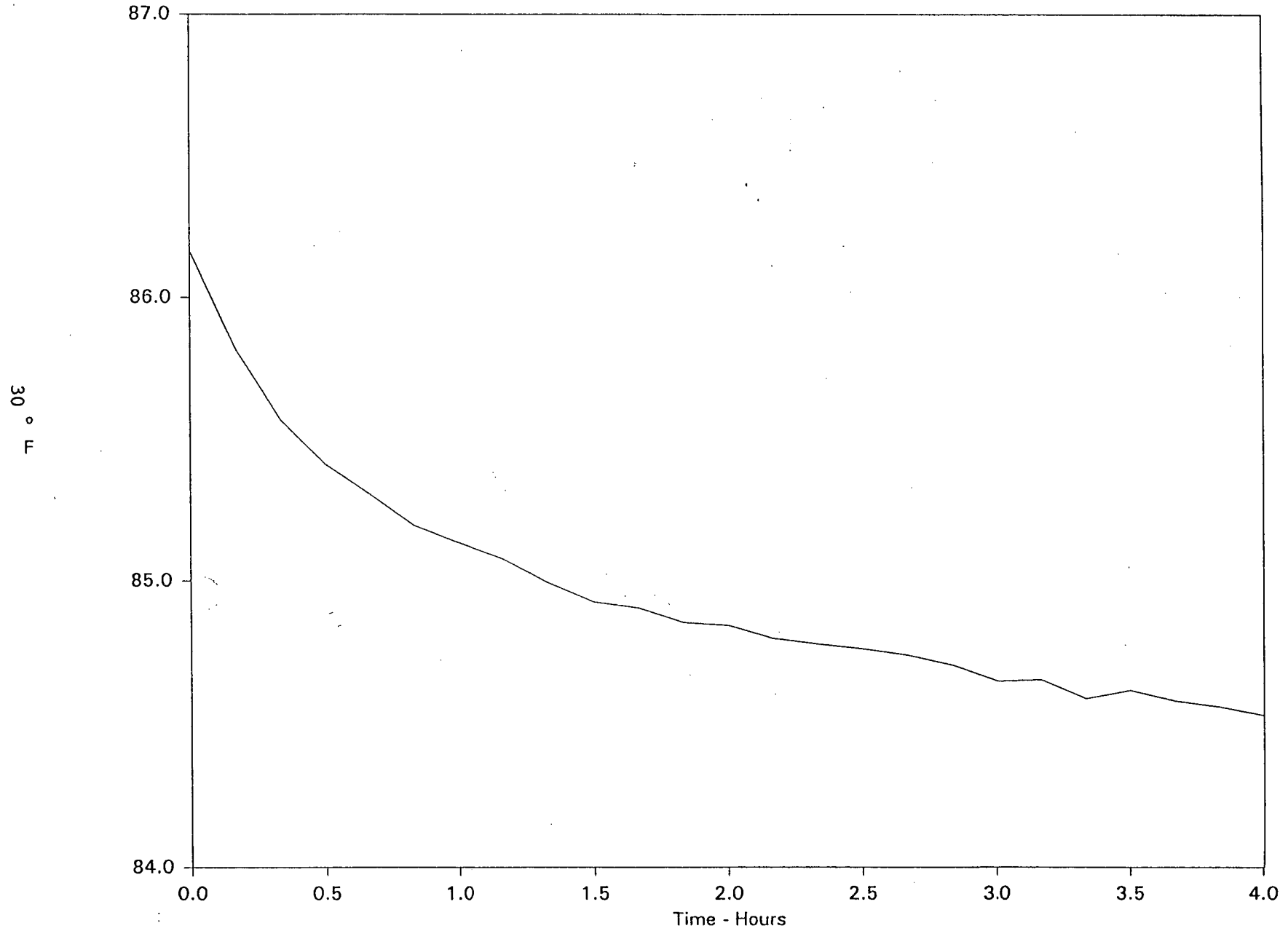
Ice Condenser Average Pressure

Watts Bar Nuclear Plant
Unit 1 - Startup



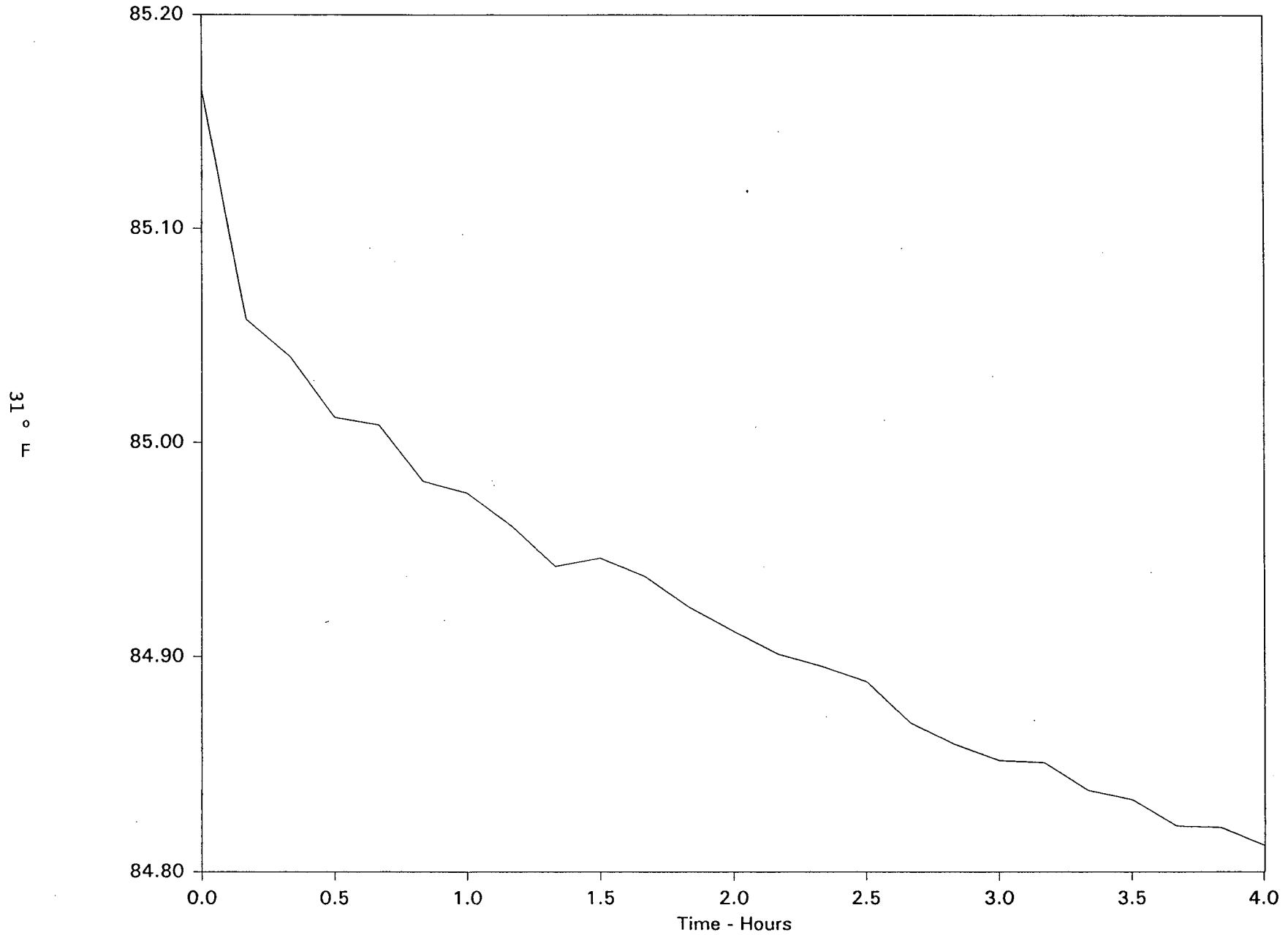
Upper Containment Average Temperature

Watts Bar Nuclear Plant
Unit 1 - Startup



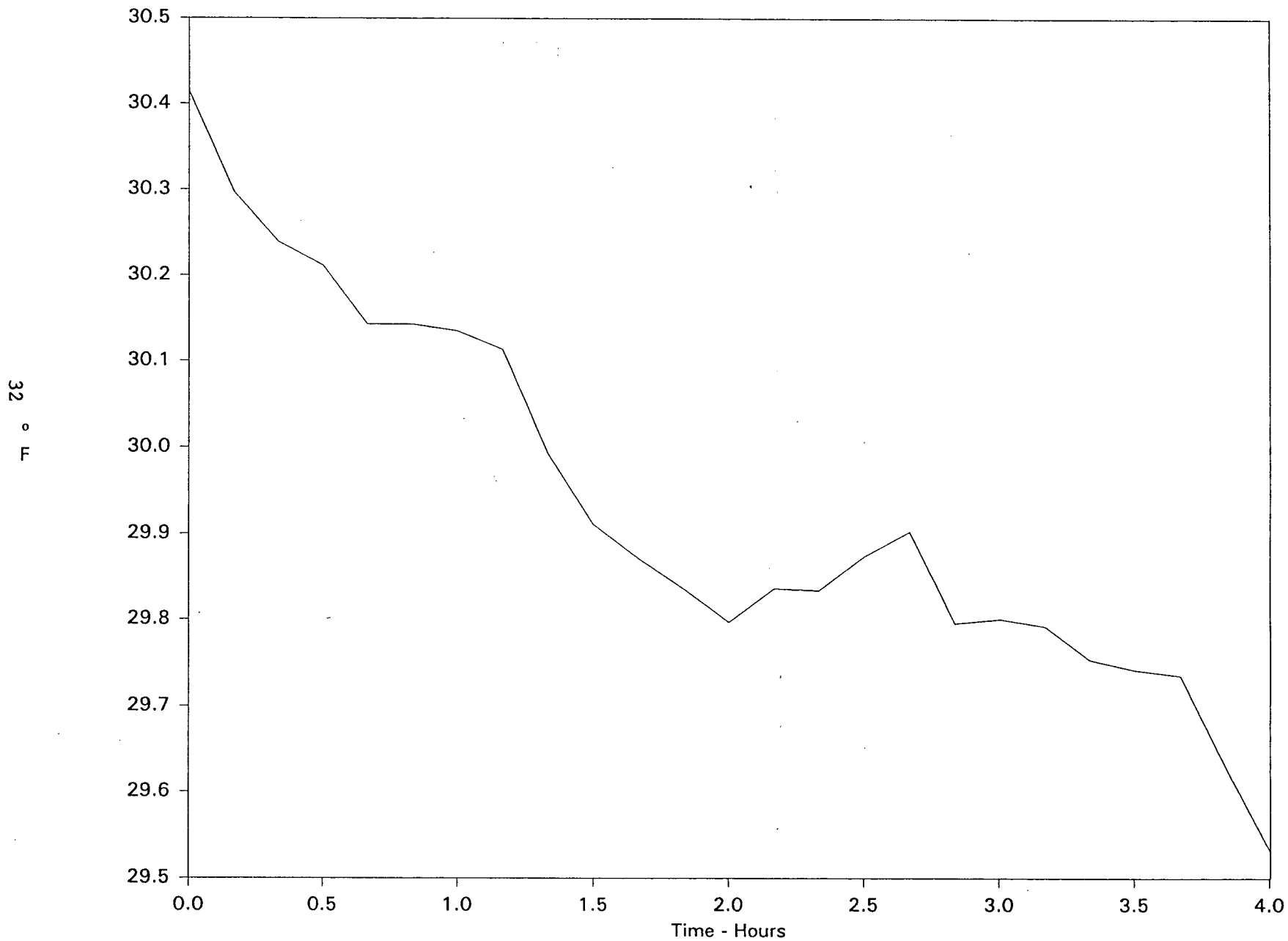
Lower Containment Average Temperature

Watts Bar Nuclear Plant
Unit 1 - Startup



Ice Condenser Average Temperature

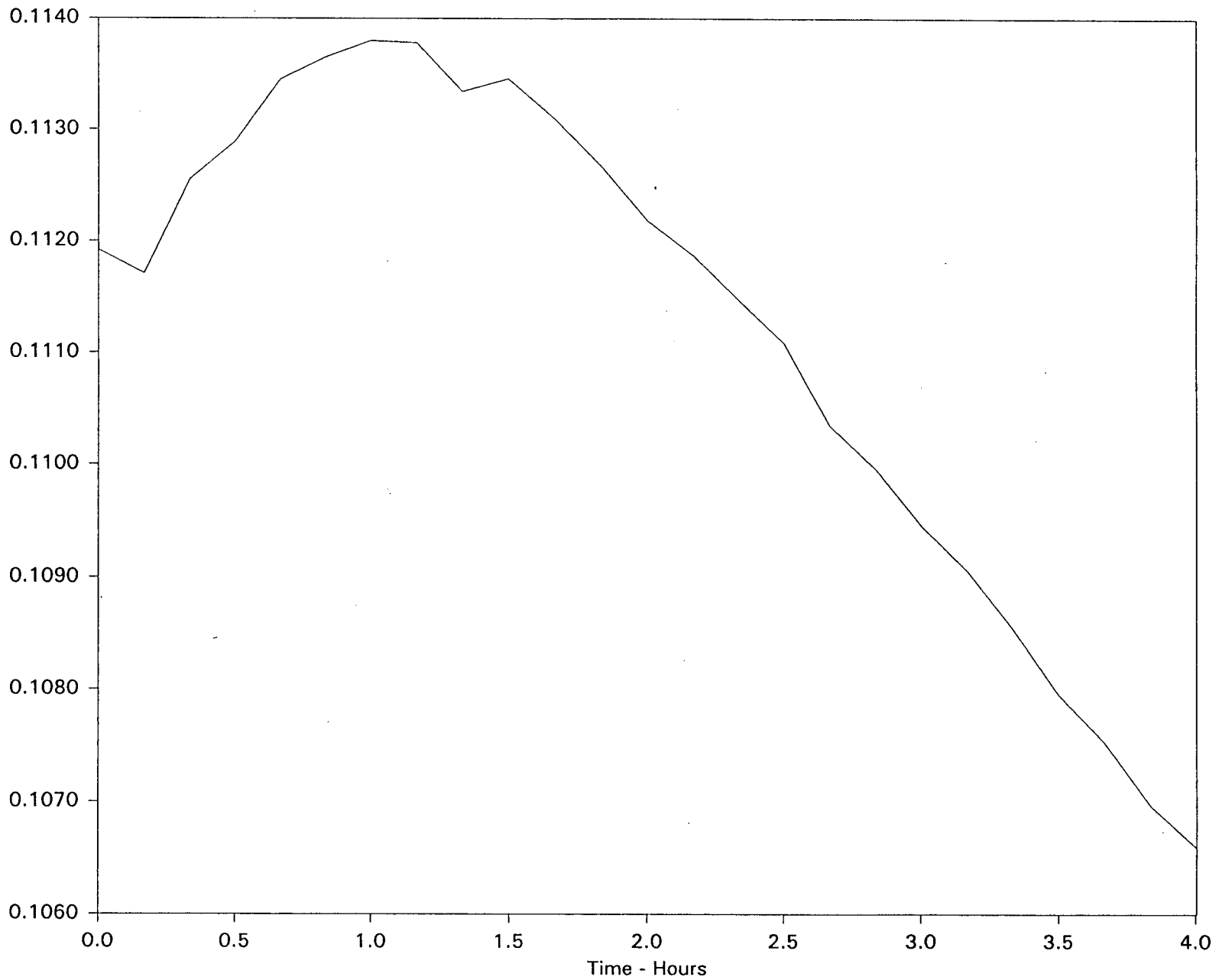
Watts Bar Nuclear Plant
Unit 1 - Startup



Upper Containment Average Vapor Pressure

Watts Bar Nuclear Plant
Unit 1 - Startup

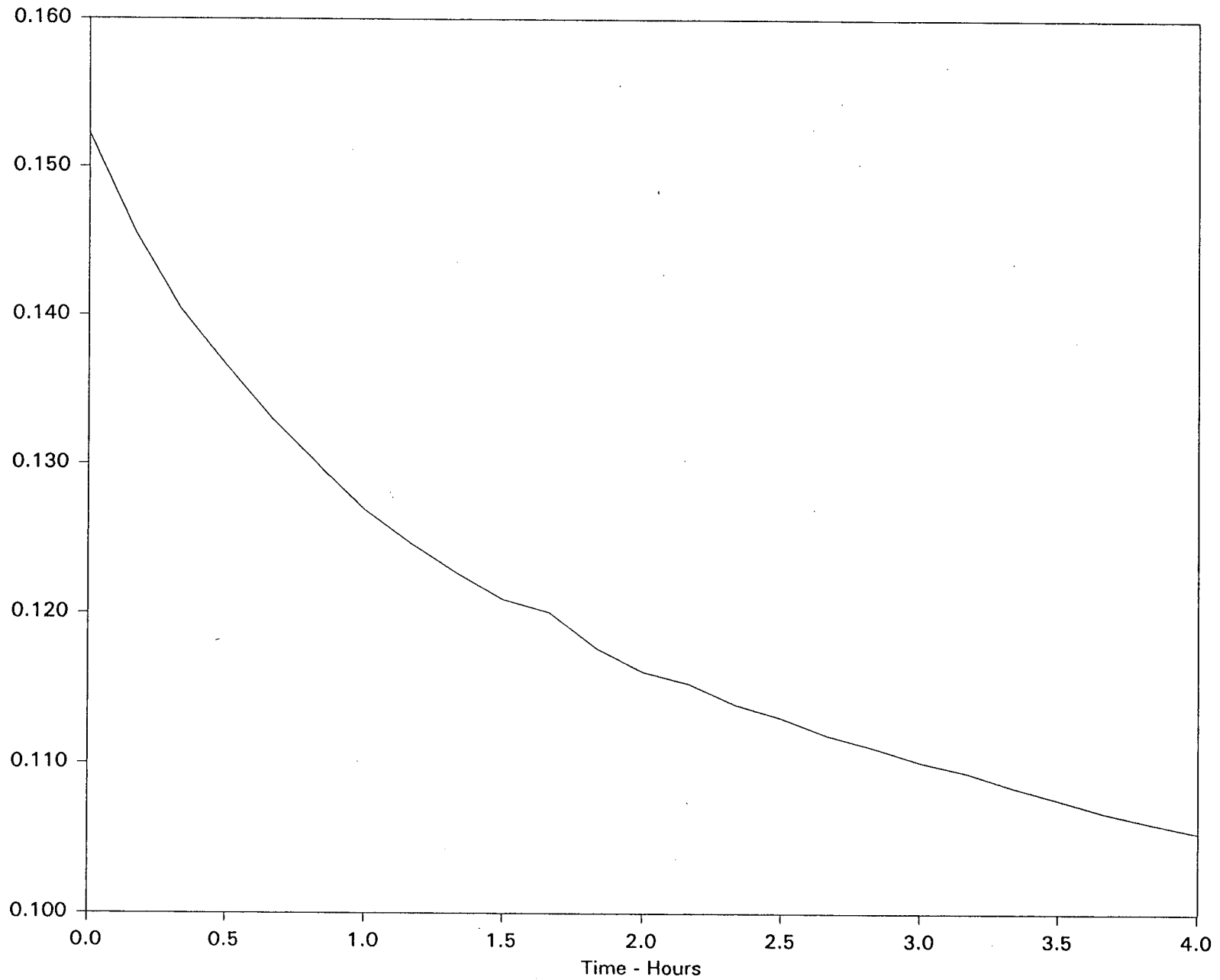
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Lower Containment Average Vapor Pressure

Watts Bar Nuclear Plant
Unit 1 - Startup

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Temperature Stabilization Criteria Review

| Time | Elapsed Time | Average Temperature | Rate of Change of Containment Temp. Last 4 Hrs.(DegF/Hr) | Rate of Change of Containment Temp. Last Hr. (DegF/Hr) |
|-------|--------------|---------------------|--|--|
| 03:12 | 00:00 | 78.537 | | |
| 03:22 | 00:10 | 78.297 | | |
| 03:32 | 00:20 | 78.146 | | |
| 03:42 | 00:30 | 78.048 | | |
| 03:52 | 00:40 | 77.979 | | |
| 04:02 | 00:50 | 77.911 | | |
| 04:12 | 00:60 | 77:875 | | |
| 04:22 | 01:10 | 77.836 | | |
| 04:32 | 01:20 | 77.767 | | |
| 04:42 | 01:30 | 77.720 | | |
| 04:52 | 01:40 | 77.700 | | |
| 05:02 | 01:50 | 77.662 | | |
| 05:12 | 02:00 | 77.649 | | |
| 05:22 | 02:10 | 77.626 | | |
| 05:32 | 02:20 | 77.613 | | |
| 05:42 | 02:30 | 77.606 | | |
| 05:52 | 02:40 | 77.592 | | |
| 06:02 | 02:50 | 77.555 | | |
| 06:12 | 03:00 | 77.523 | | |
| 06:22 | 03:10 | 77.525 | | |
| 06:32 | 03:20 | 77.480 | | |
| 06:42 | 03:30 | 77.493 | | |
| 06:52 | 03:40 | 77.468 | | |
| 07:02 | 03:50 | 77.443 | | |
| 07:12 | 04:00 | 77.411 | 0.281 | 0.112 |

The avg rate of temp change for the last 4 hours = 0.281 degF/hr.

The avg rate of temp change for the last hour = 0.112 degF/hr.

The temp stabilization check indicated a value of 0.169 degF/hr, which is only 33.8 % of the recommended 0.5 degF/hr.

Stability check indicates conditions are favorable to proceed with CILRT.

Containment Calculated Values Stabilization Phase

Watts Bar Nuclear Plant
Unit 1 - Startup

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|--------------------|-------------|-------------|--------------------|--------------|
| 32 | 03:12:15 | Upper Containment | 96041.06 | 86.163 | 0.1119 | 29.4943 |
| | | Lower Containment | 55680.05 | 85.165 | 0.1523 | 29.4975 |
| | | Ice Condenser | 25571.62 | 30.414 | 0.0185 | 29.4981 |
| | | TOTAL | 177292.73 | | | |
| 33 | 03:22:16 | Upper Containment | 96045.36 | 85.818 | 0.1117 | 29.4768 |
| | | Lower Containment | 55670.89 | 85.057 | 0.1456 | 29.4803 |
| | | Ice Condenser | 25562.9 | 30.297 | 0.0185 | 29.481 |
| | | TOTAL | 177279.15 | | | |
| 34 | 03:32:16 | Upper Containment | 96054.29 | 85.567 | 0.1126 | 29.4669 |
| | | Lower Containment | 55663.73 | 85.04 | 0.1404 | 29.4704 |
| | | Ice Condenser | 25557.33 | 30.239 | 0.0185 | 29.4711 |
| | | TOTAL | 177275.35 | | | |
| 35 | 03:42:16 | Upper Containment | 96059.59 | 85.411 | 0.1129 | 29.4605 |
| | | Lower Containment | 55661.7 | 85.012 | 0.1366 | 29.464 |
| | | Ice Condenser | 25553.18 | 30.211 | 0.0185 | 29.4646 |
| | | TOTAL | 177274.47 | | | |
| 36 | 03:52:17 | Upper Containment | 96060.11 | 85.305 | 0.1135 | 29.4555 |
| | | Lower Containment | 55660.19 | 85.008 | 0.133 | 29.4594 |
| | | Ice Condenser | 25552.46 | 30.143 | 0.0185 | 29.4597 |
| | | TOTAL | 177272.76 | | | |
| 37 | 04:02:17 | Upper Containment | 96067.85 | 85.195 | 0.1136 | 29.4521 |
| | | Lower Containment | 55661.84 | 84.982 | 0.1299 | 29.4558 |
| | | Ice Condenser | 25549.45 | 30.143 | 0.0185 | 29.4562 |
| | | TOTAL | 177279.14 | | | |
| 38 | 04:12:17 | Upper Containment | 96066.35 | 85.136 | 0.1138 | 29.4486 |
| | | Lower Containment | 55660.98 | 84.976 | 0.1269 | 29.452 |
| | | Ice Condenser | 25546.97 | 30.135 | 0.0185 | 29.4529 |
| | | TOTAL | 177274.29 | | | |
| 39 | 04:22:18 | Upper Containment | 96066.65 | 85.079 | 0.1138 | 29.4456 |
| | | Lower Containment | 55660.93 | 84.961 | 0.1246 | 29.4489 |
| | | Ice Condenser | 25545.35 | 30.114 | 0.0185 | 29.4497 |
| | | TOTAL | 177272.93 | | | |
| 40 | 04:32:18 | Upper Containment | 96073.97 | 84.992 | 0.1133 | 29.4428 |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|--------------------|-------------|-------------|--------------------|--------------|
| | | Lower Containment | 55661.16 | 84.942 | 0.1227 | 29.446 |
| | | Ice Condenser | 25549.18 | 29.993 | 0.0185 | 29.4469 |
| | | TOTAL | 177284.31 | | | |
| 41 | 04:42:18 | Upper Containment | 96077.04 | 84.925 | 0.1135 | 29.4402 |
| | | Lower Containment | 55660.41 | 84.946 | 0.1209 | 29.4441 |
| | | Ice Condenser | 25551.32 | 29.911 | 0.0185 | 29.4444 |
| | | TOTAL | 177288.77 | | | |
| 42 | 04:52:19 | Upper Containment | 96072.81 | 84.903 | 0.1131 | 29.4374 |
| | | Lower Containment | 55657.8 | 84.937 | 0.1201 | 29.4414 |
| | | Ice Condenser | 25550.9 | 29.871 | 0.0185 | 29.4415 |
| | | TOTAL | 177281.51 | | | |
| 43 | 05:02:19 | Upper Containment | 96077.12 | 84.851 | 0.1127 | 29.4355 |
| | | Lower Containment | 55658.8 | 84.923 | 0.1177 | 29.4388 |
| | | Ice Condenser | 25550.92 | 29.836 | 0.0185 | 29.4394 |
| | | TOTAL | 177286.84 | | | |
| 44 | 05:12:19 | Upper Containment | 96073.38 | 84.843 | 0.1122 | 29.4334 |
| | | Lower Containment | 55659.29 | 84.912 | 0.1162 | 29.4369 |
| | | Ice Condenser | 25551.34 | 29.797 | 0.0185 | 29.4376 |
| | | TOTAL | 177284.02 | | | |
| 45 | 05:22:20 | Upper Containment | 96077.05 | 84.797 | 0.1119 | 29.4317 |
| | | Lower Containment | 55658.05 | 84.901 | 0.1153 | 29.4348 |
| | | Ice Condenser | 25547.82 | 29.836 | 0.0185 | 29.4359 |
| | | TOTAL | 177282.92 | | | |
| 46 | 05:32:20 | Upper Containment | 96076.95 | 84.777 | 0.1115 | 29.4302 |
| | | Lower Containment | 55659.2 | 84.895 | 0.1139 | 29.4337 |
| | | Ice Condenser | 25546.57 | 29.834 | 0.0185 | 29.4343 |
| | | TOTAL | 177282.72 | | | |
| 47 | 05:42:20 | Upper Containment | 96076.65 | 84.76 | 0.1111 | 29.4298 |
| | | Lower Containment | 55658.74 | 84.888 | 0.1131 | 29.4322 |
| | | Ice Condenser | 25543.45 | 29.874 | 0.0185 | 29.4331 |
| | | TOTAL | 177278.84 | | | |
| 48 | 05:52:21 | Upper Containment | 96077.47 | 84.738 | 0.1103 | 29.4272 |
| | | Lower Containment | 55659.65 | 84.869 | 0.1119 | 29.4305 |
| | | Ice Condenser | 25540.52 | 29.902 | 0.0185 | 29.4315 |
| | | TOTAL | 177277.64 | | | |
| 49 | 06:02:21 | Upper Containment | 96078.87 | 84.703 | 0.11 | 29.4253 |
| | | Lower Containment | 55658.8 | 84.859 | 0.1111 | 29.4287 |
| | | Ice Condenser | 25544.43 | 29.796 | 0.0185 | 29.4296 |
| | | TOTAL | 177282.11 | | | |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|--------------------|-------------|-------------|--------------------|--------------|
| 50 | 06:12:21 | UppeContainment | 96086.77 8 | 4.649 0 | .1094 2 | 9.4243 |
| | | Lower Containment | 55659.32 | 84.851 | 0.1101 | 29.4276 |
| | | Ice Condenser | 25543.24 | 29.8 | 0.0185 | 29.4285 |
| | | TOTAL | 177289.33 | | | |
| 51 | 06:22:22 | Upper Containment | 96086.85 | 84.654 | 0.1091 | 29.4242 |
| | | Lower Containment | 55660.44 | 84.851 | 0.1094 | 29.4274 |
| | | Ice Condenser | 25543.52 | 29.793 | 0.0185 | 29.4283 |
| | | TOTAL | 177290.82 | | | |
| 52 | 06:32:22 | Upper Containment | 96095.43 | 84.589 | 0.1085 | 29.4228 |
| | | Lower Containment | 55660.99 | 84.838 | 0.1084 | 29.4261 |
| | | Ice Condenser | 25544.48 | 29.753 | 0.0185 | 29.4271 |
| | | TOTAL | 177300.9 | | | |
| 53 | 06:42:22 | Upper Containment | 96088.54 | 84.617 | 0.108 | 29.4216 |
| | | Lower Containment | 55661.89 | 84.833 | 0.1076 | 29.4255 |
| | | Ice Condenser | 25544.12 | 29.742 | 0.0185 | 29.426 |
| | | TOTAL | 177294.54 | | | |
| 54 | 06:52:23 | Upper Containment | 96084.56 | 84.582 | 0.1075 | 29.4181 |
| | | Lower Containment | 55657.85 | 84.821 | 0.1067 | 29.4218 |
| | | Ice Condenser | 25541.38 | 29.735 | 0.0185 | 29.4224 |
| | | TOTAL | 177283.79 | | | |
| 55 | 07:02:23 | Upper Containment | 96084.39 | 84.561 | 0.107 | 29.4164 |
| | | Lower Containment | 55655.46 | 84.821 | 0.106 | 29.4198 |
| | | Ice Condenser | 25545.36 | 29.629 | 0.0185 | 29.4206 |
| | | TOTAL | 177285.21 | | | |
| 56 | 07:12:24 | Upper Containment | 96085.8 | 84.532 | 0.1066 | 29.4148 |
| | | Lower Containment | 55654.17 | 84.812 | 0.1054 | 29.4181 |
| | | Ice Condenser | 25549.16 | 29.531 | 0.0185 | 29.4191 |
| | | TOTAL | 177289.13 | | | |

APPENDIX B

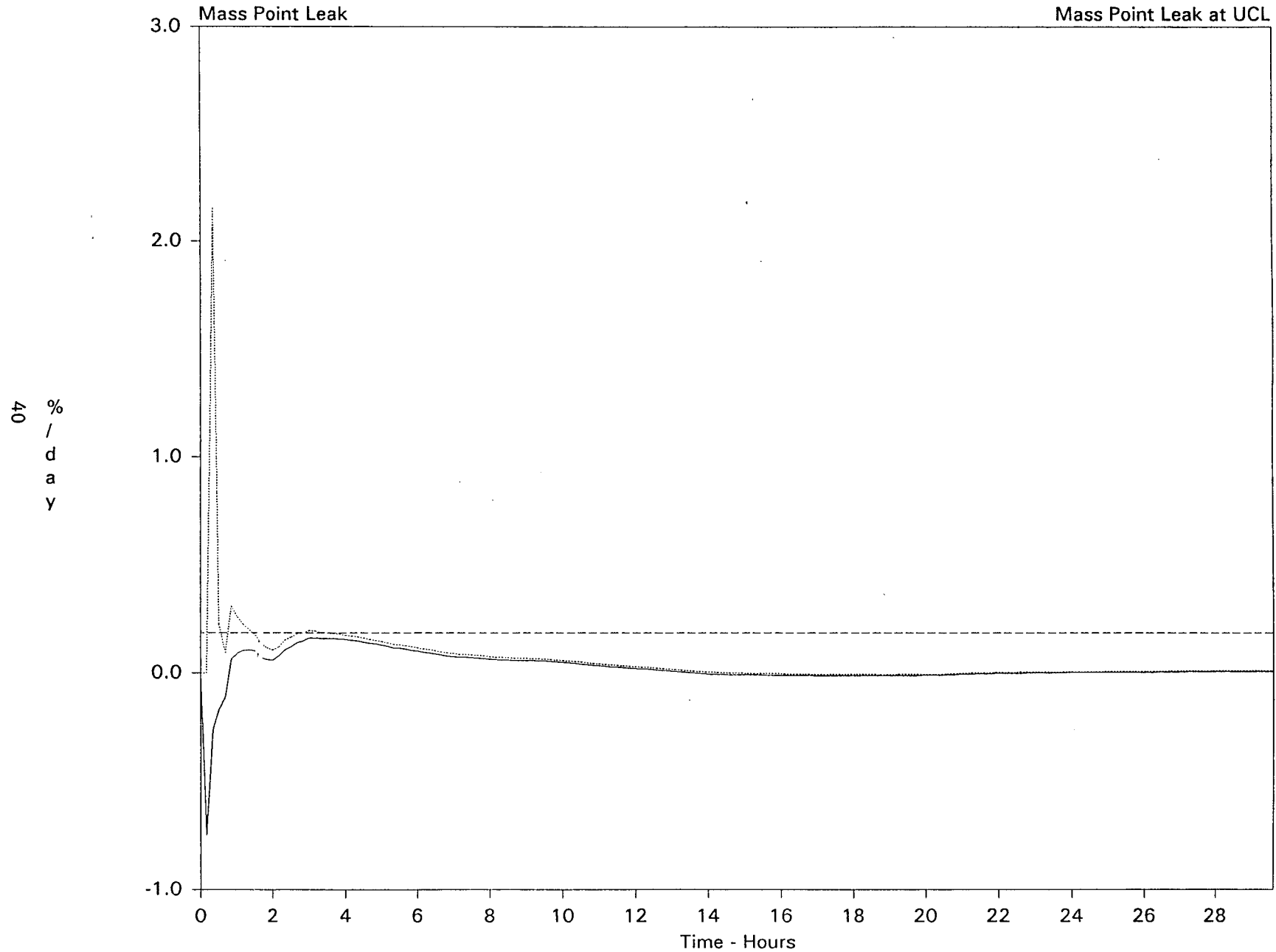
CILRT Test Phase Graphs

(samples 57 to 234)

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| Containment Mass Point Leak Rate & UCL | 40 |
| Containment Total Time Leak Rate & UCL | 41 |
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| Ice Condenser Compartment Temperature | 51 |
| Upper Containment Compartment Vapor Pressure | 52 |
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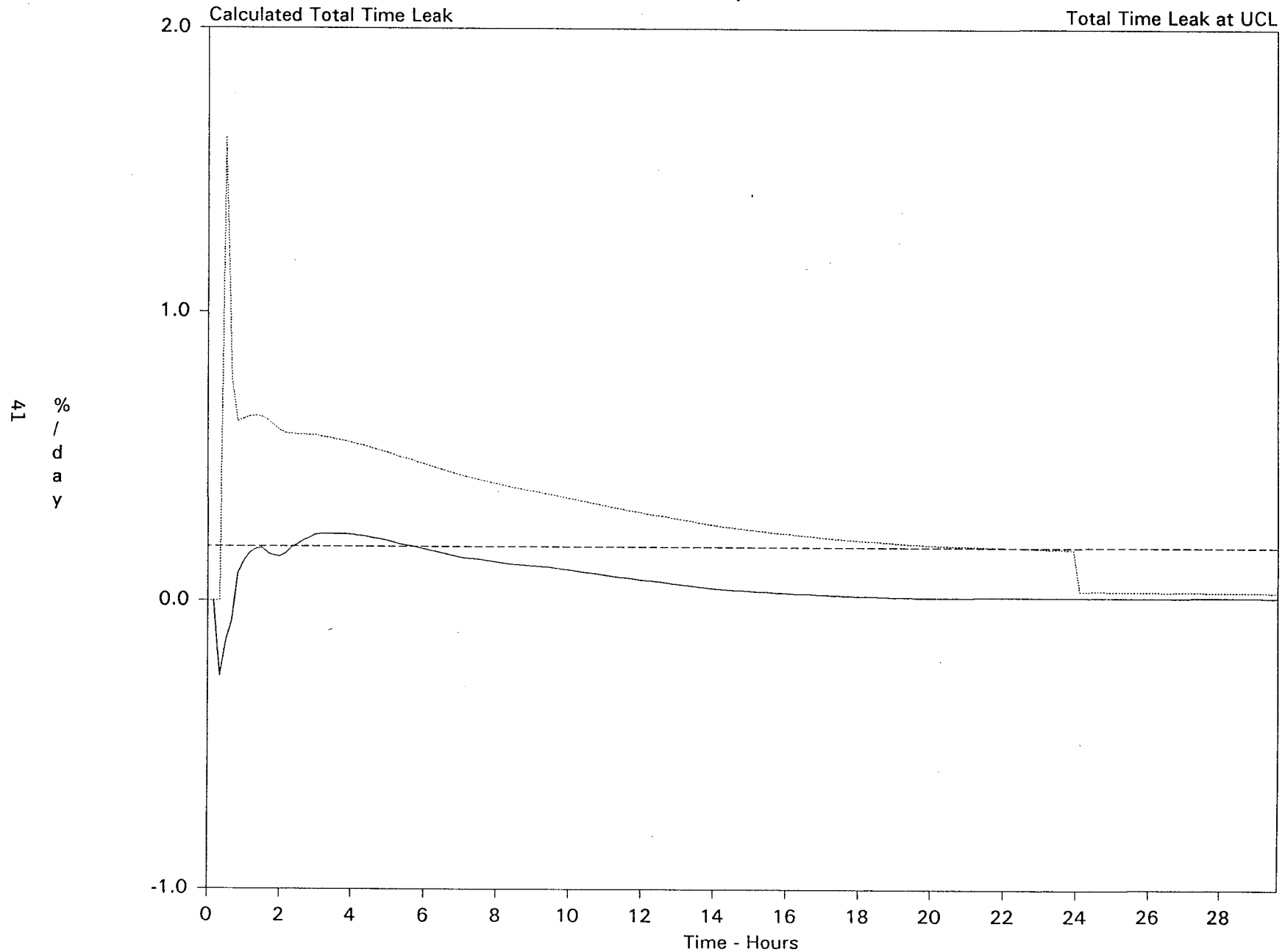
Mass Point Leak & Mass Point Leak at UCL

Watts Bar Nuclear Plant
Unit 1 - Startup



Calculated Total Time Leak & Total Time Leak at UCL

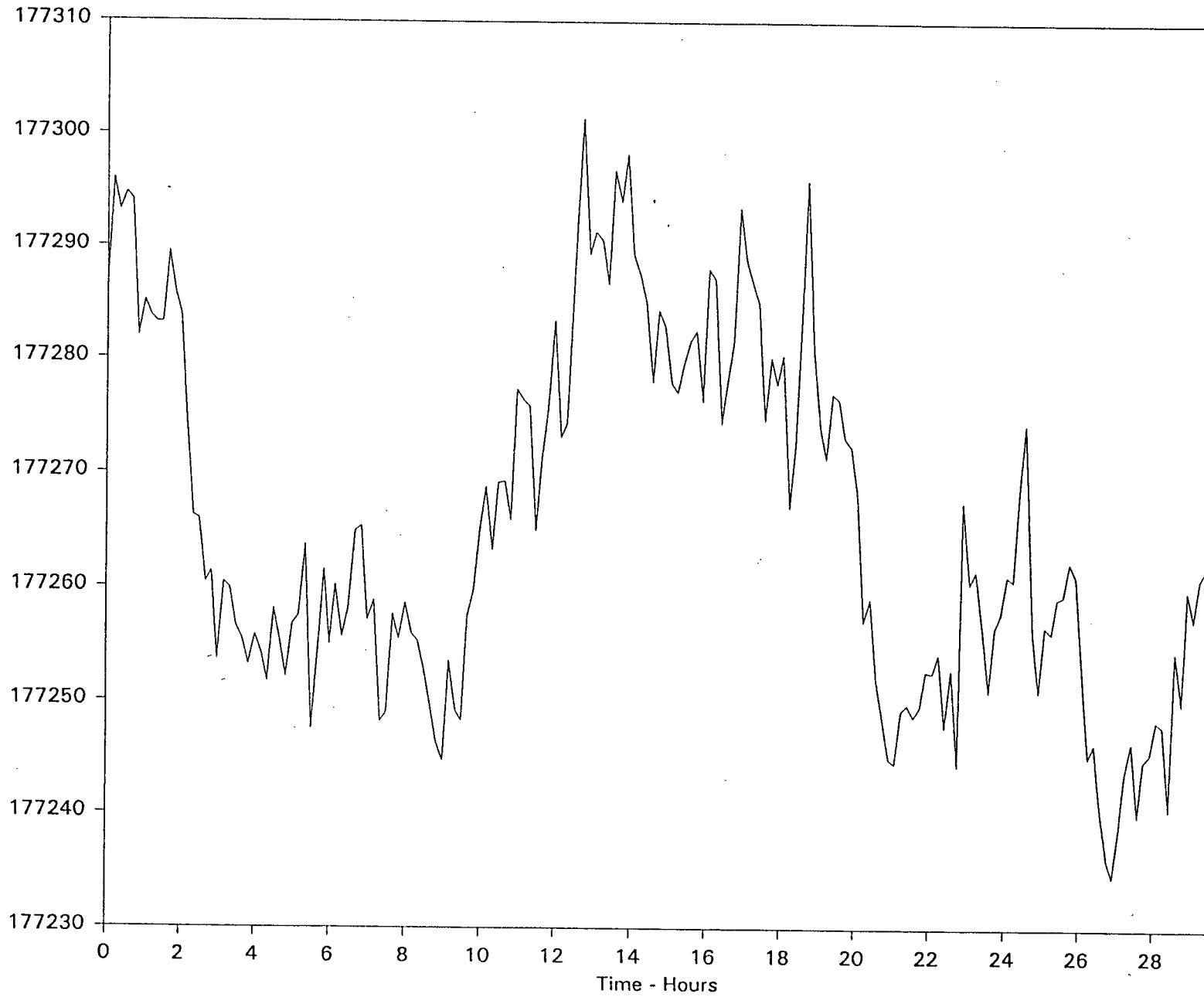
Watts Bar Nuclear Plant
Unit 1 - Startup



Containment Mass

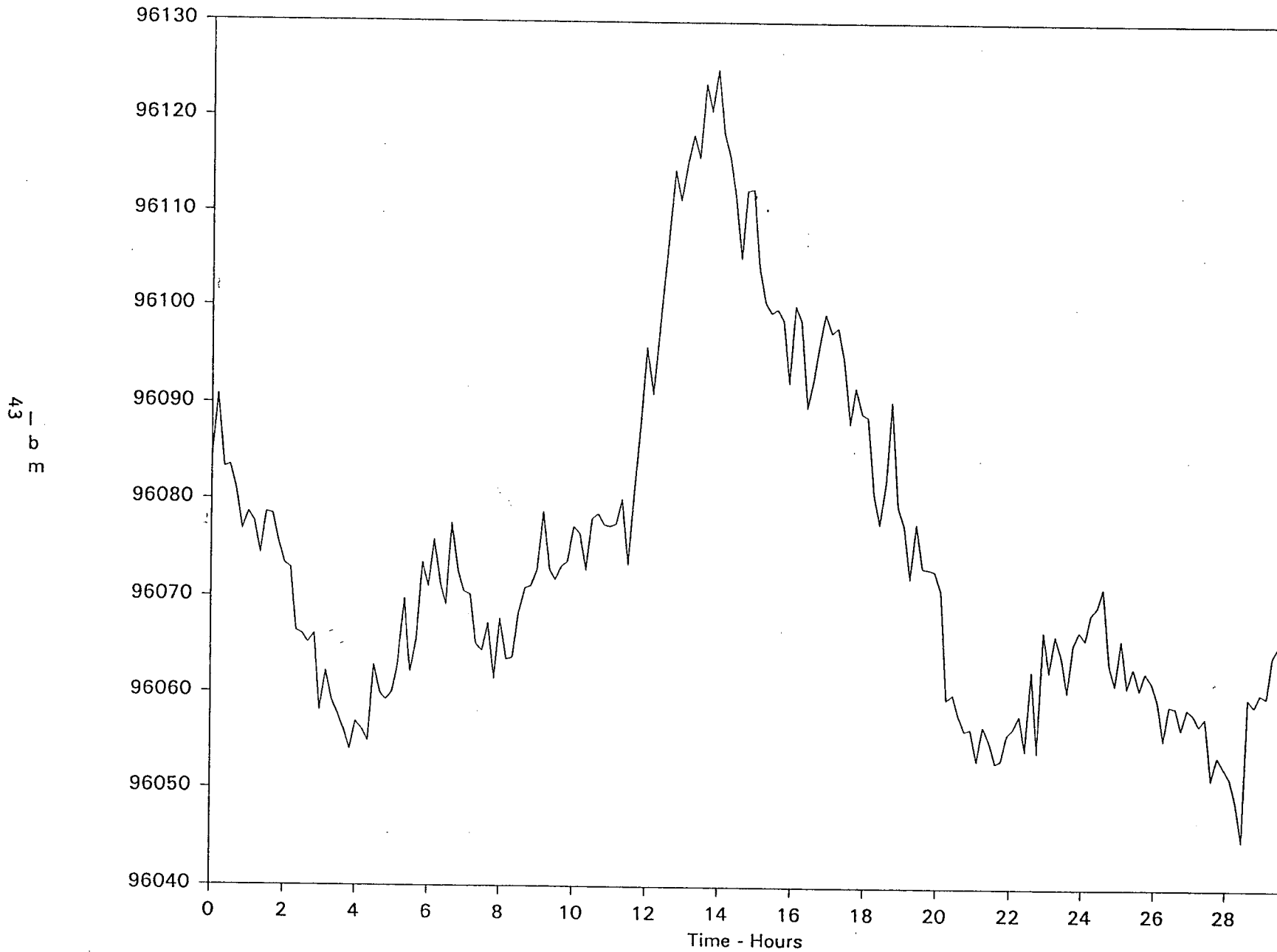
Watts Bar Nuclear Plant
Unit 1 - Startup

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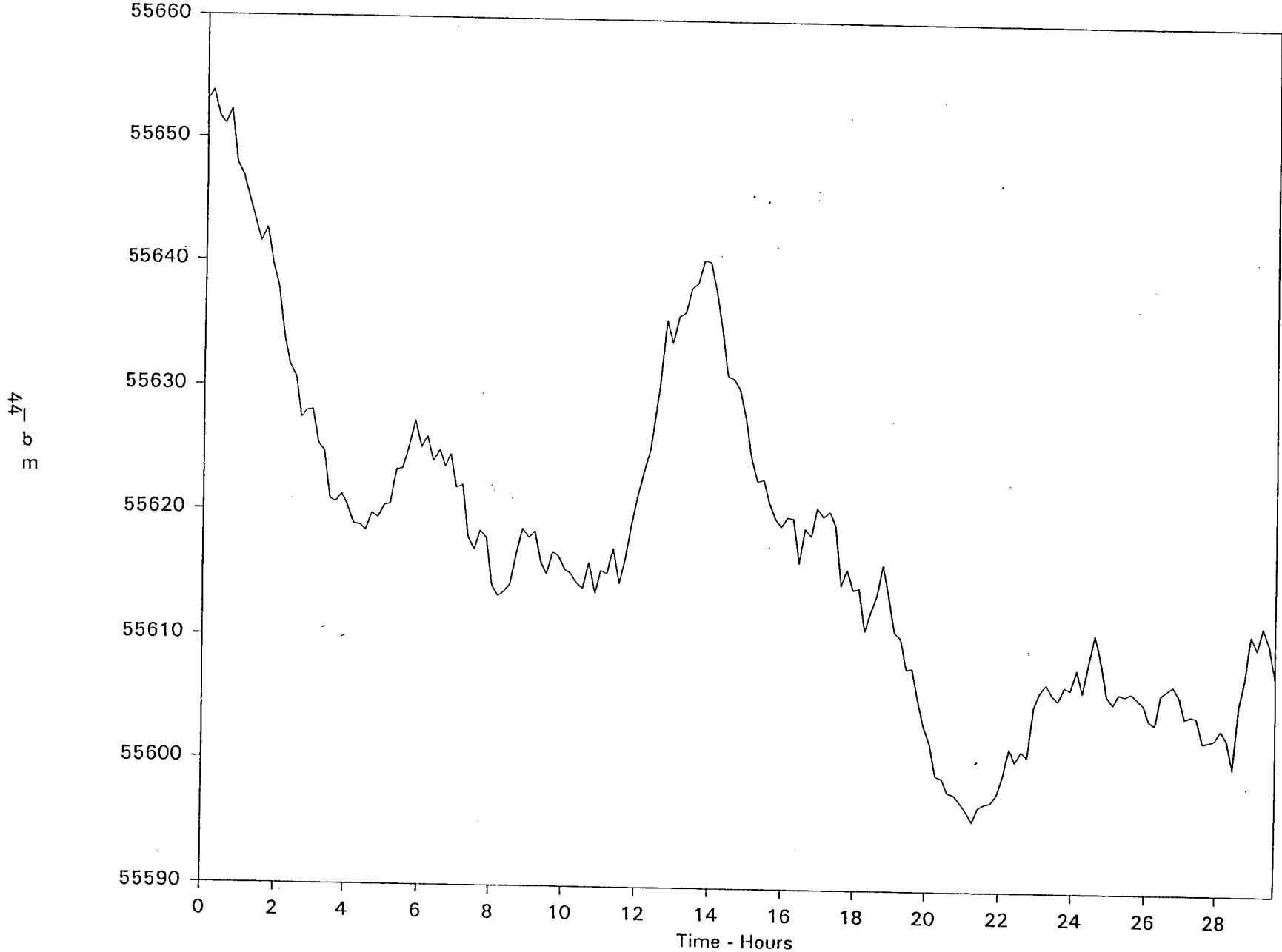
Upper Containment Mass

Watts Bar Nuclear Plant
Unit 1 - Startup



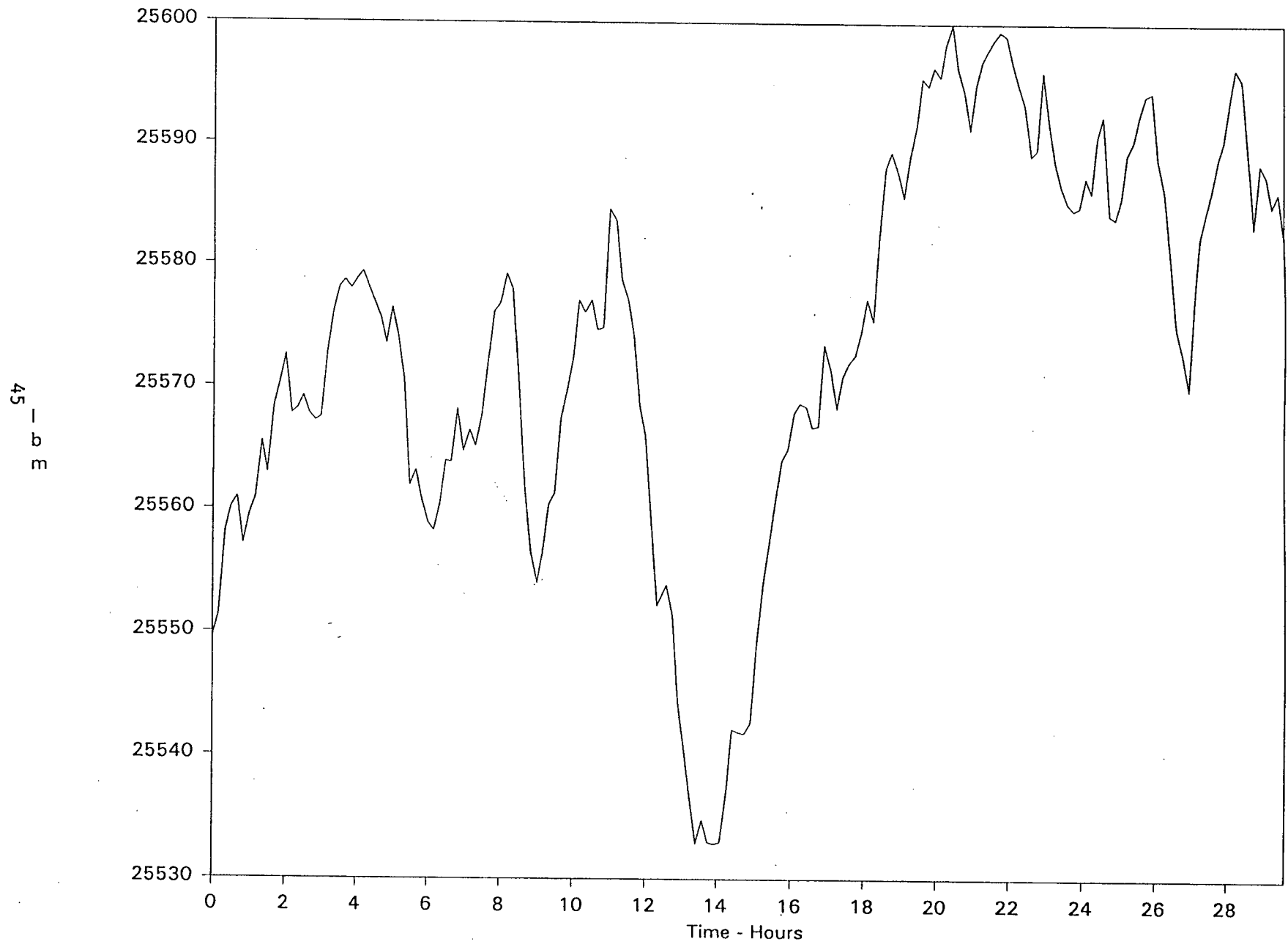
Lower Containment Mass

Watts Bar Nuclear Plant
Unit 1 - Startup



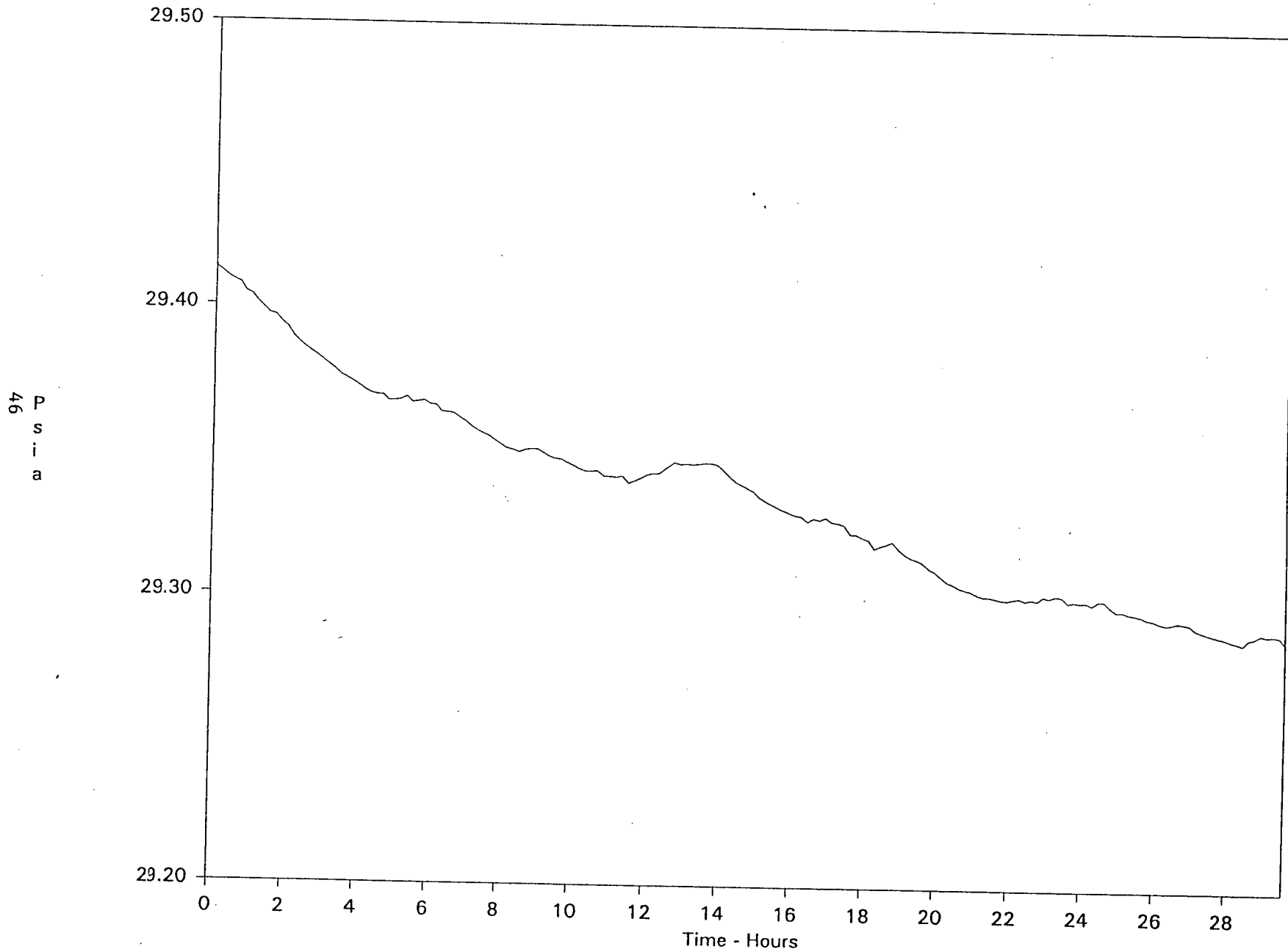
Ice Condenser Mass

Watts Bar Nuclear Plant
Unit 1 - Startup



Upper Containment Average Pressure

Watts Bar Nuclear Plant
Unit 1 - Startup

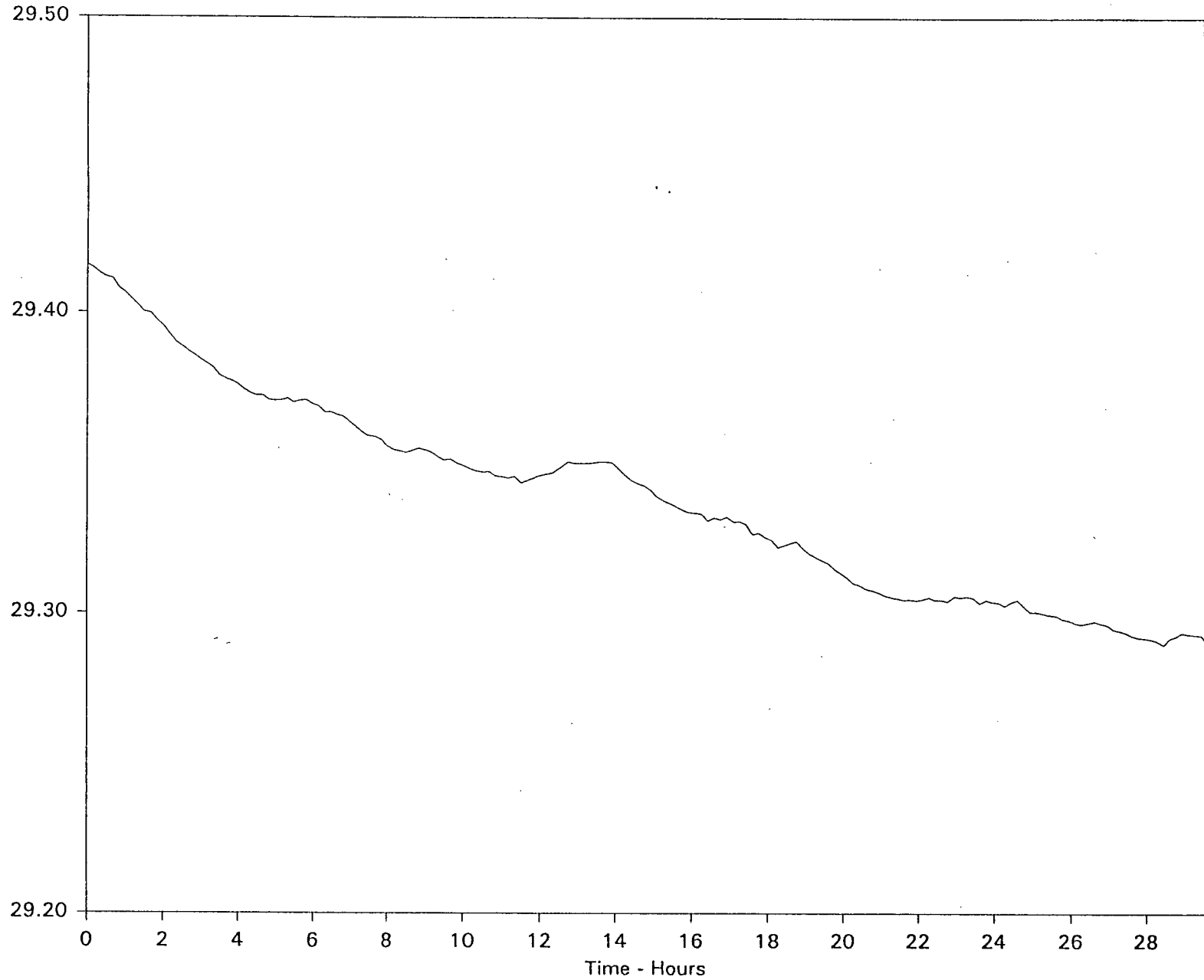


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Lower Containment Average Pressure

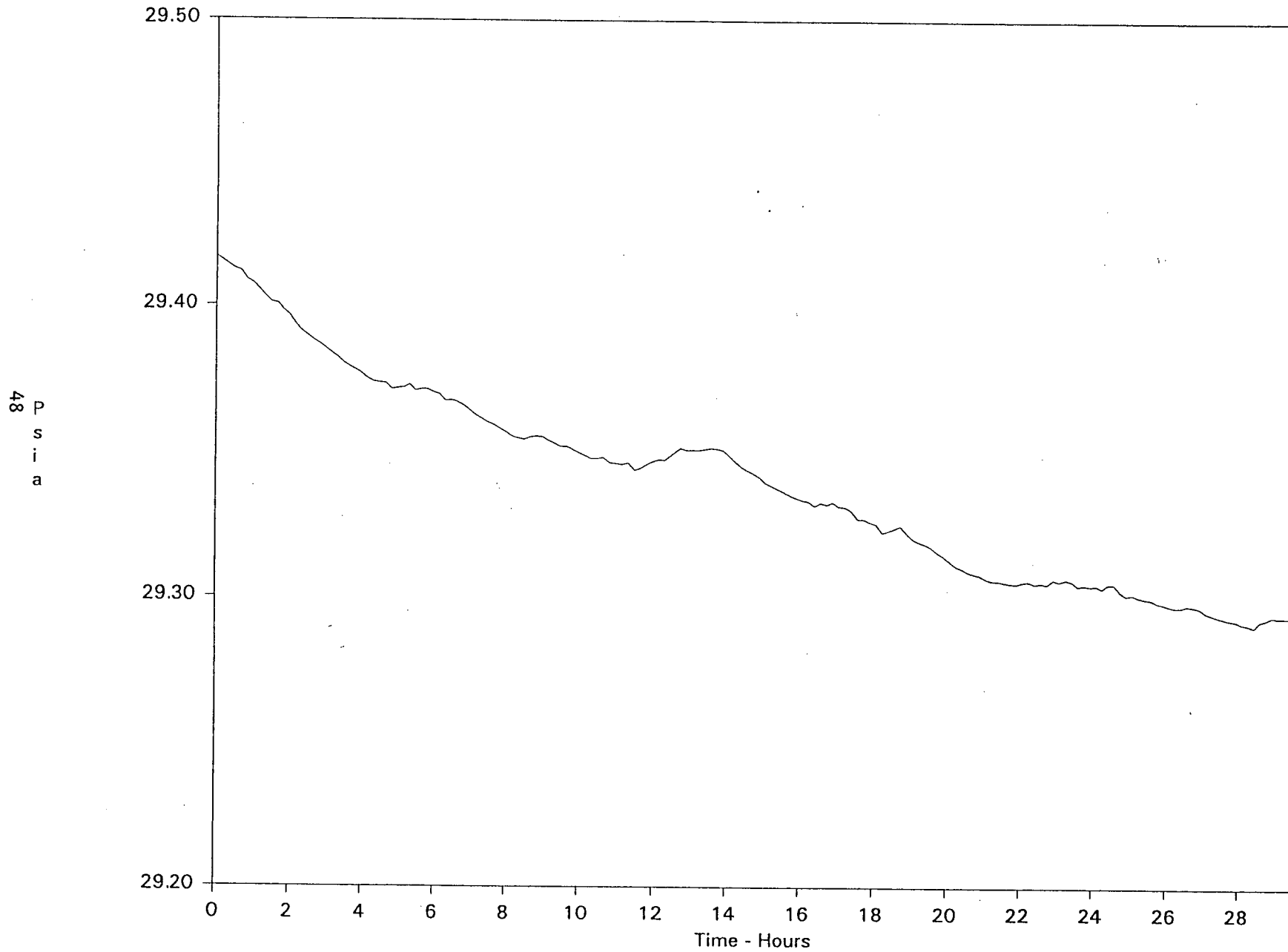
Watts Bar Nuclear Plant
Unit 1 - Startup

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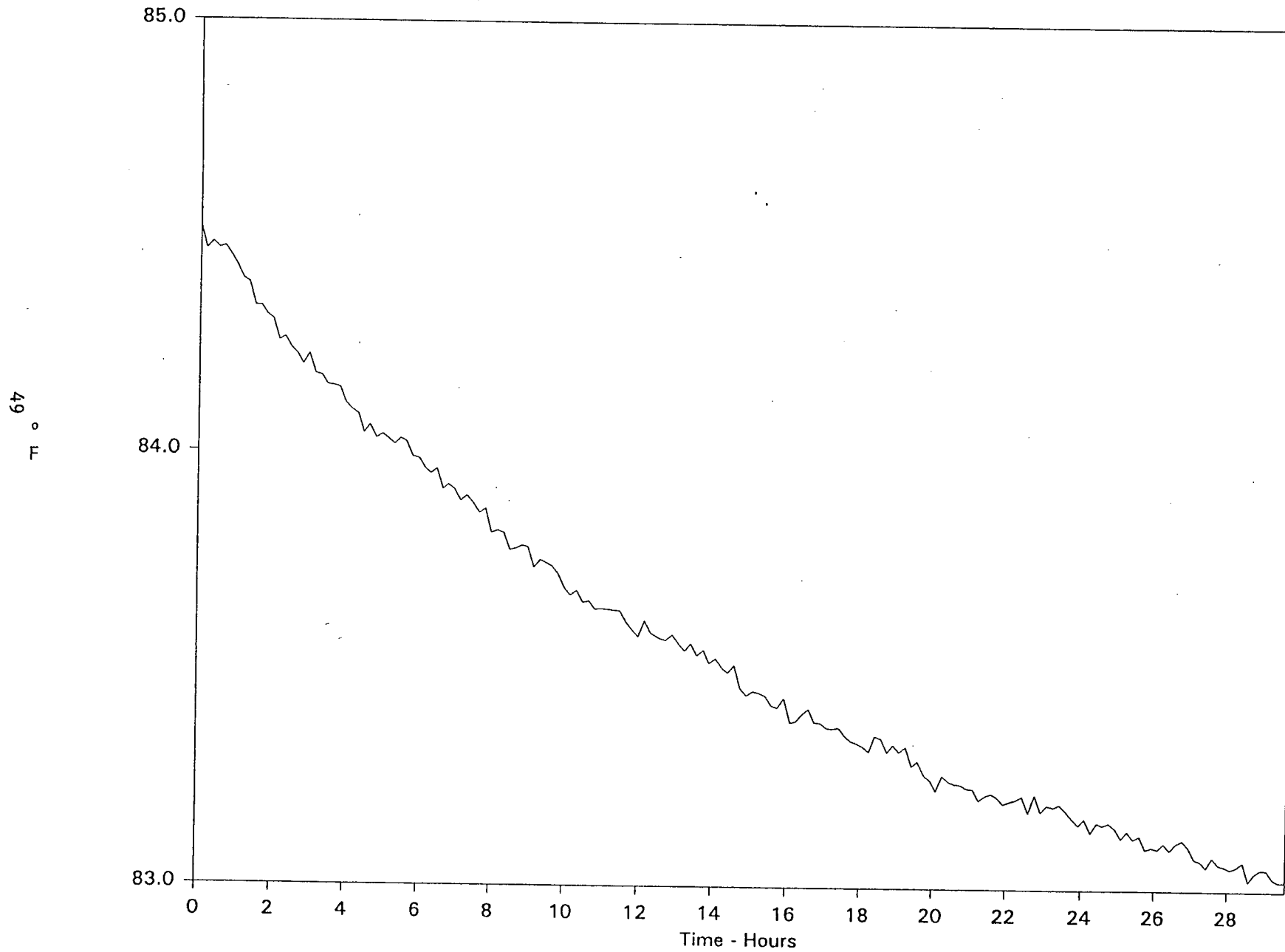
Ice Condenser Average Pressure

Watts Bar Nuclear Plant
Unit 1 - Startup



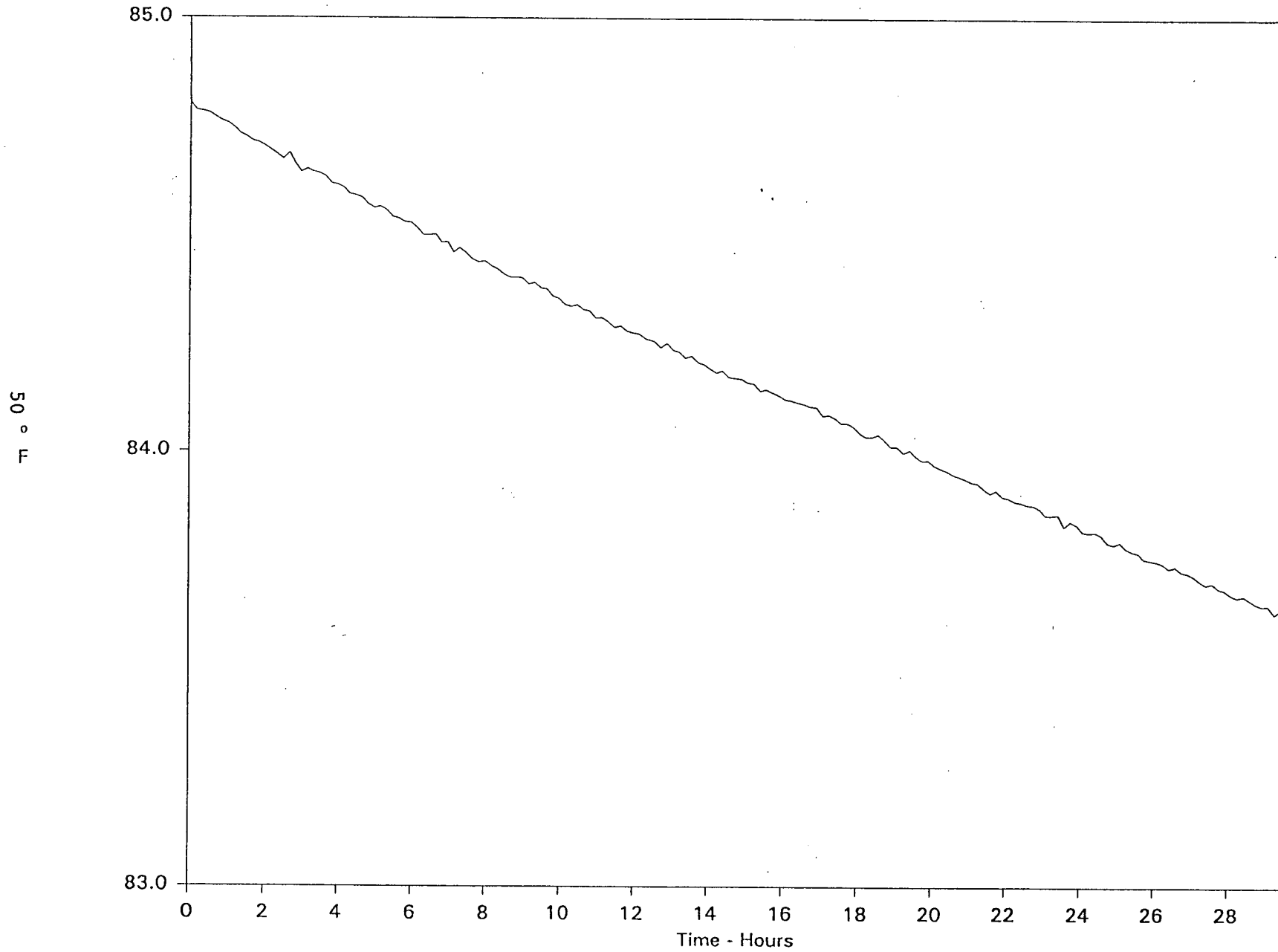
Upper Containment Average Temperature

Watts Bar Nuclear Plant
Unit 1 - Startup



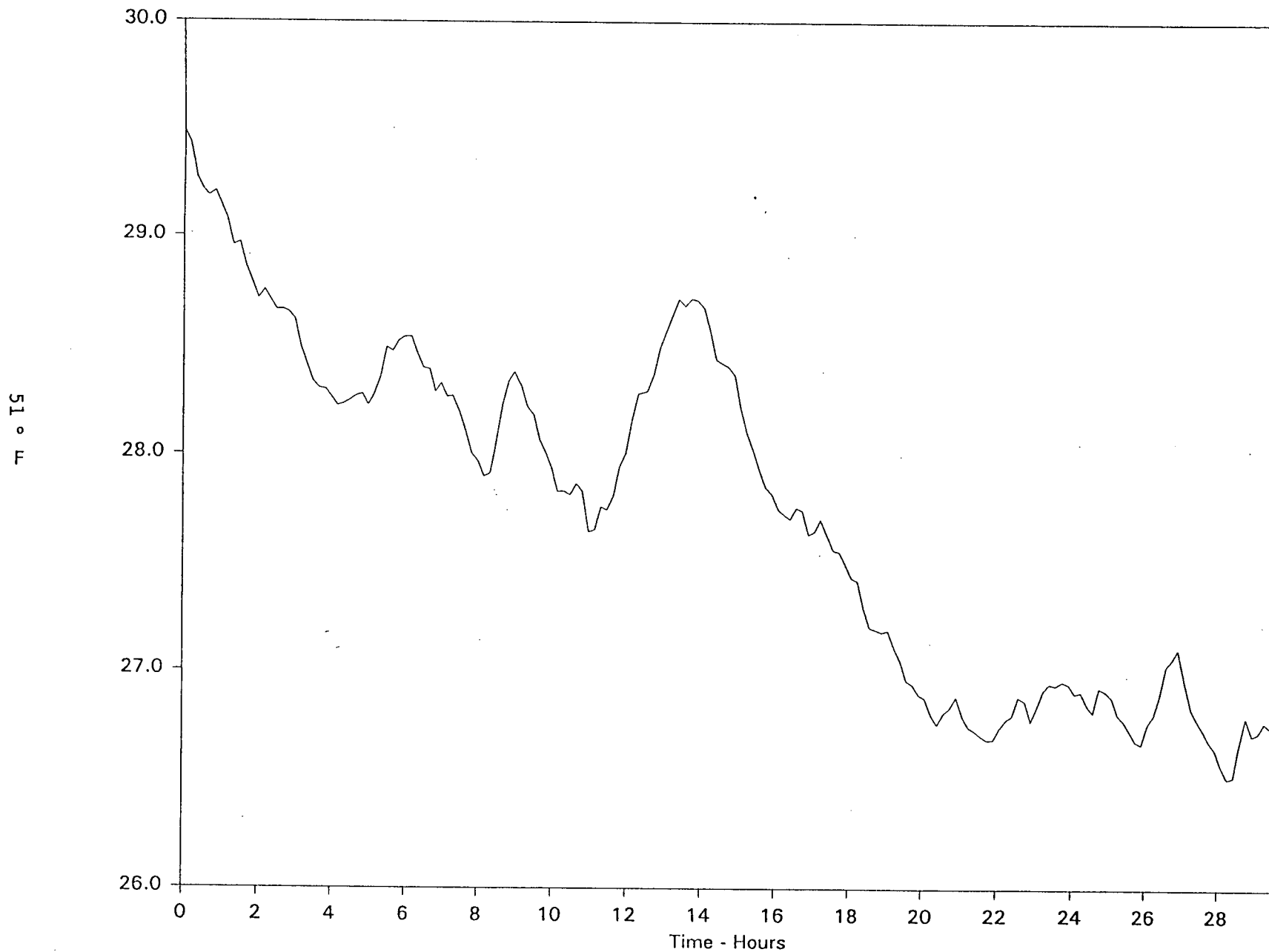
Lower Containment Average Temperature

Watts Bar Nuclear Plant
Unit 1 - Startup



Ice Condenser Average Temperature

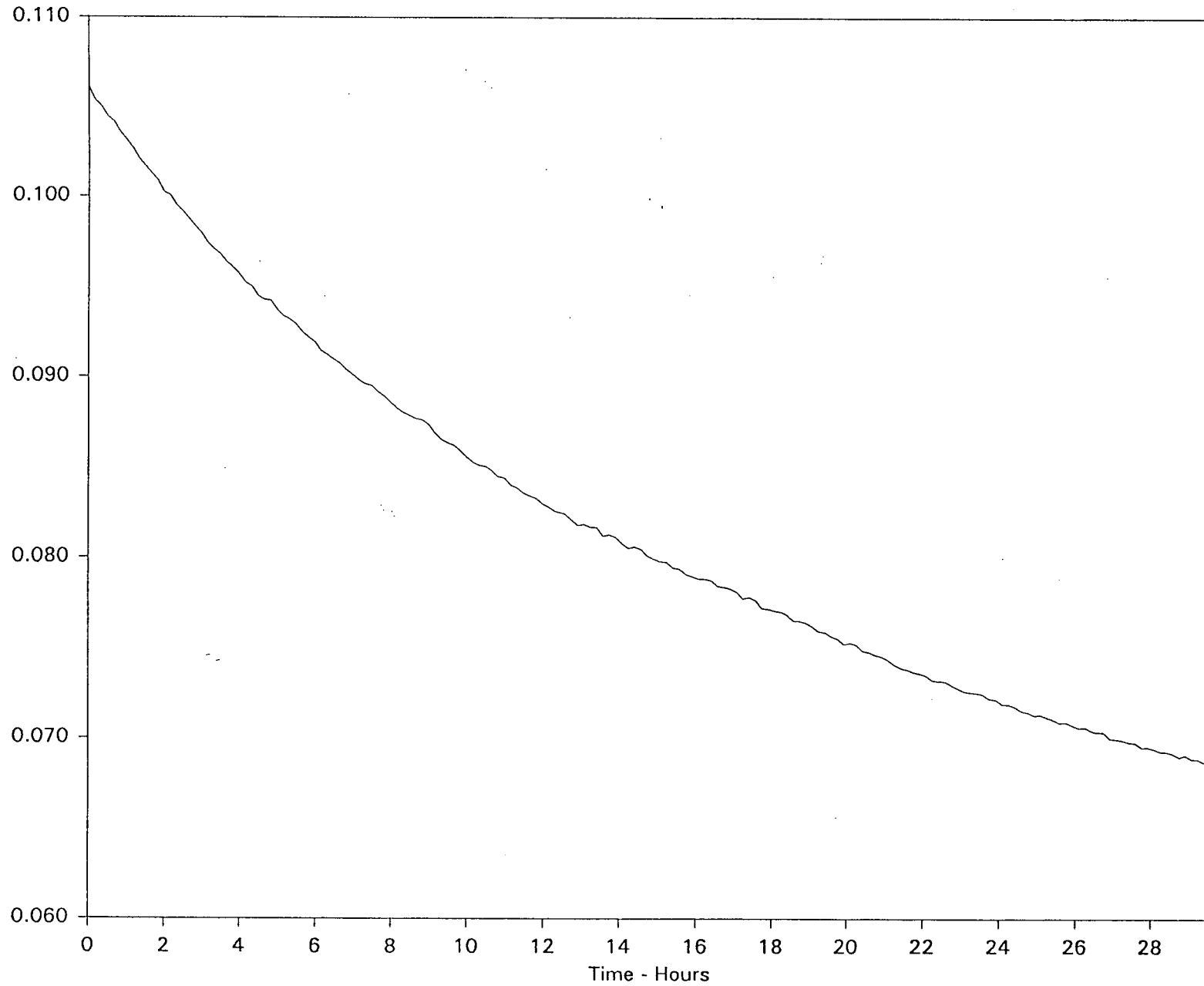
Watts Bar Nuclear Plant
Unit 1 - Startup



Upper Containment Average Vapor Pressure

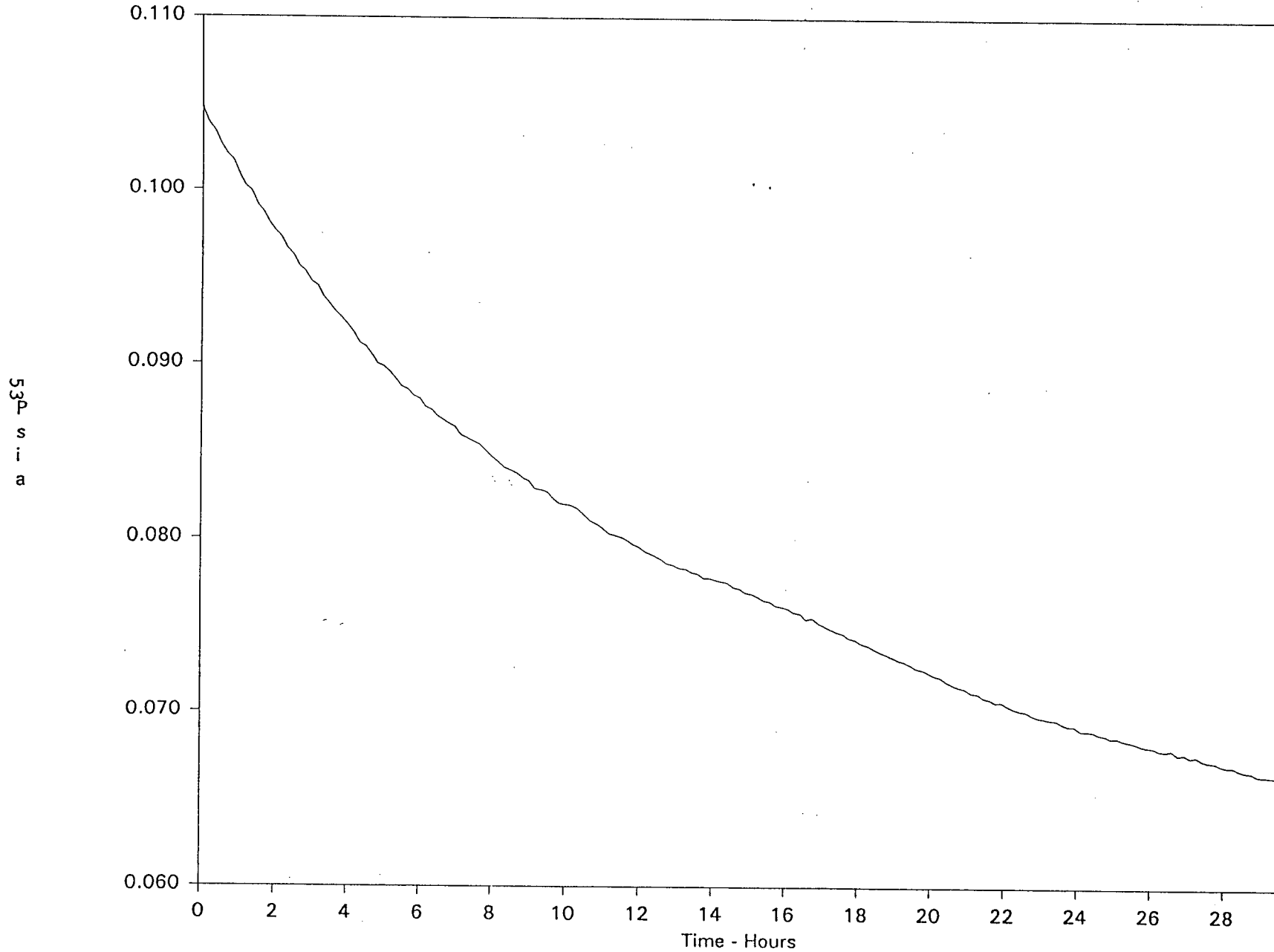
Watts Bar Nuclear Plant
Unit 1 - Startup

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Lower Containment Average Vapor Pressure

Watts Bar Nuclear Plant
Unit 1 - Startup



APPENDIX C

CILRT Test Phase Tabular Data
(samples 57 to 234)

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| CILRT Total Time Leak Rate Analysis | 64 |
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Mass Point Leak Rate Analysis

CILRT Phase

Watts Bar Nuclear Plant
Unit 1 - Startup

| <u>Rdg</u> | <u>Time</u> | <u>Norm Mass</u> | <u>MP Leak %/day</u> | <u>MP UCL %/day</u> |
|------------|-----------------|------------------|--------------------------|-------------------------|
| 57 | 27-Jun-94 07:22 | 1.000000 | 0.000000 | 0.000000 |
| 58 | 27-Jun-94 07:32 | 1.000052 | -0.751312 | 0.000000 |
| 59 | 27-Jun-94 07:42 | 1.000036 | -0.261998 | 2.152317 |
| 60 | 27-Jun-94 07:52 | 1.000045 | -0.173232 | 0.227590 |
| 61 | 27-Jun-94 08:02 | 1.000042 | -0.110591 | 0.093280 |
| 62 | 27-Jun-94 08:12 | 0.999973 | 0.064112 | 0.310703 |
| 63 | 27-Jun-94 08:22 | 0.999991 | 0.092363 | 0.260423 |
| 64 | 27-Jun-94 08:32 | 0.999984 | 0.105290 | 0.226965 |
| 65 | 27-Jun-94 08:42 | 0.999980 | 0.107442 | 0.199361 |
| 66 | 27-Jun-94 08:52 | 0.999980 | 0.102804 | 0.174947 |
| 67 | 27-Jun-94 09:02 | 1.000016 | 0.072283 | 0.138734 |
| 68 | 27-Jun-94 09:12 | 0.999995 | 0.063571 | 0.118992 |
| 69 | 27-Jun-94 09:22 | 0.999984 | 0.061435 | 0.107899 |
| 70 | 27-Jun-94 09:32 | 0.999932 | 0.079589 | 0.123274 |
| 71 | 27-Jun-94 09:42 | 0.999885 | 0.106399 | 0.152921 |
| 72 | 27-Jun-94 09:52 | 0.999883 | 0.122514 | 0.166168 |
| 73 | 27-Jun-94 10:02 | 0.999852 | 0.140025 | 0.182246 |
| 74 | 27-Jun-94 10:12 | 0.999857 | 0.148492 | 0.186815 |
| 75 | 27-Jun-94 10:22 | 0.999814 | 0.162080 | 0.198859 |
| 76 | 27-Jun-94 10:32 | 0.999852 | 0.161799 | 0.194786 |
| 77 | 27-Jun-94 10:42 | 0.999849 | 0.160025 | 0.189831 |
| 78 | 27-Jun-94 10:52 | 0.999831 | 0.159960 | 0.186982 |
| 79 | 27-Jun-94 11:02 | 0.999824 | 0.159249 | 0.183869 |
| 80 | 27-Jun-94 11:12 | 0.999811 | 0.158939 | 0.181459 |
| 81 | 27-Jun-94 11:22 | 0.999826 | 0.155213 | 0.176215 |
| 82 | 27-Jun-94 11:32 | 0.999817 | 0.152036 | 0.171639 |
| 83 | 27-Jun-94 11:42 | 0.999803 | 0.149966 | 0.168201 |
| 84 | 27-Jun-94 11:52 | 0.999839 | 0.143392 | 0.161494 |
| 85 | 27-Jun-94 12:02 | 0.999823 | 0.138674 | 0.156132 |
| 86 | 27-Jun-94 12:12 | 0.999805 | 0.135585 | 0.152137 |
| 87 | 27-Jun-94 12:22 | 0.999832 | 0.129929 | 0.146360 |
| 88 | 27-Jun-94 12:32 | 0.999835 | 0.124212 | 0.140586 |
| 89 | 27-Jun-94 12:42 | 0.999870 | 0.116137 | 0.133417 |
| 90 | 27-Jun-94 12:52 | 0.999779 | 0.115440 | 0.131700 |
| 91 | 27-Jun-94 13:02 | 0.999815 | 0.111855 | 0.127567 |
| 92 | 27-Jun-94 13:12 | 0.999858 | 0.105523 | 0.121587 |
| 93 | 27-Jun-94 13:22 | 0.999821 | 0.101978 | 0.117550 |
| 94 | 27-Jun-94 13:32 | 0.999850 | 0.096854 | 0.112417 |
| 95 | 27-Jun-94 13:42 | 0.999825 | 0.093491 | 0.108604 |
| 96 | 27-Jun-94 13:52 | 0.999839 | 0.089557 | 0.104407 |
| 97 | 27-Jun-94 14:02 | 0.999877 | 0.083927 | 0.099069 |

Mass Point Leak Rate Analysis

CILRT Phase

Watts Bar Nuclear Plant
Unit 1 - Startup

| <u>Rdg</u> | <u>Time</u> | <u>Norm Mass</u> | <u>MP Leak %/day</u> | <u>MP UCL %/day</u> |
|------------|-----------------|------------------|--------------------------|-------------------------|
| 98 | 27-Jun-94 14:12 | 0.999880 | 0.078665 | 0.093957 |
| 99 | 27-Jun-94 14:22 | 0.999834 | 0.075967 | 0.090773 |
| 100 | 27-Jun-94 14:32 | 0.999843 | 0.072974 | 0.087395 |
| 101 | 27-Jun-94 14:42 | 0.999783 | 0.072666 | 0.086442 |
| 102 | 27-Jun-94 14:52 | 0.999787 | 0.072013 | 0.085198 |
| 103 | 27-Jun-94 15:02 | 0.999836 | 0.069385 | 0.082258 |
| 104 | 27-Jun-94 15:12 | 0.999824 | 0.067338 | 0.079828 |
| 105 | 27-Jun-94 15:22 | 0.999842 | 0.064742 | 0.076977 |
| 106 | 27-Jun-94 15:32 | 0.999827 | 0.062796 | 0.074687 |
| 107 | 27-Jun-94 15:42 | 0.999823 | 0.061043 | 0.072589 |
| 108 | 27-Jun-94 15:52 | 0.999808 | 0.059821 | 0.070981 |
| 109 | 27-Jun-94 16:02 | 0.999790 | 0.059158 | 0.069912 |
| 110 | 27-Jun-94 16:12 | 0.999772 | 0.058971 | 0.069324 |
| 111 | 27-Jun-94 16:22 | 0.999763 | 0.058941 | 0.068914 |
| 112 | 27-Jun-94 16:32 | 0.999813 | 0.057450 | 0.067171 |
| 113 | 27-Jun-94 16:42 | 0.999788 | 0.056648 | 0.066056 |
| 114 | 27-Jun-94 16:52 | 0.999783 | 0.055961 | 0.065067 |
| 115 | 27-Jun-94 17:02 | 0.999835 | 0.053979 | 0.062979 |
| 116 | 27-Jun-94 17:12 | 0.999848 | 0.051792 | 0.060742 |
| 117 | 27-Jun-94 17:22 | 0.999878 | 0.049054 | 0.058103 |
| 118 | 27-Jun-94 17:32 | 0.999899 | 0.046028 | 0.055256 |
| 119 | 27-Jun-94 17:42 | 0.999868 | 0.043881 | 0.053050 |
| 120 | 27-Jun-94 17:52 | 0.999901 | 0.041170 | 0.050427 |
| 121 | 27-Jun-94 18:02 | 0.999902 | 0.038633 | 0.047930 |
| 122 | 27-Jun-94 18:12 | 0.999883 | 0.036642 | 0.045858 |
| 123 | 27-Jun-94 18:22 | 0.999948 | 0.033547 | 0.042970 |
| 124 | 27-Jun-94 18:32 | 0.999942 | 0.030775 | 0.040301 |
| 125 | 27-Jun-94 18:42 | 0.999939 | 0.028251 | 0.037813 |
| 126 | 27-Jun-94 18:52 | 0.999878 | 0.026975 | 0.036342 |
| 127 | 27-Jun-94 19:02 | 0.999914 | 0.025152 | 0.034421 |
| 128 | 27-Jun-94 19:12 | 0.999938 | 0.023056 | 0.032289 |
| 129 | 27-Jun-94 19:22 | 0.999981 | 0.020410 | 0.029742 |
| 130 | 27-Jun-94 19:32 | 0.999924 | 0.018848 | 0.028050 |
| 131 | 27-Jun-94 19:42 | 0.999931 | 0.017277 | 0.026358 |
| 132 | 27-Jun-94 19:57 | 1.000029 | 0.014327 | 0.023597 |
| 133 | 27-Jun-94 20:07 | 1.000083 | 0.010800 | 0.020425 |
| 134 | 27-Jun-94 20:17 | 1.000015 | 0.008493 | 0.018119 |
| 135 | 27-Jun-94 20:27 | 1.000026 | 0.006199 | 0.015826 |
| 136 | 27-Jun-94 20:37 | 1.000022 | 0.004125 | 0.013712 |
| 137 | 27-Jun-94 20:47 | 1.000000 | 0.002489 | 0.011963 |
| 138 | 27-Jun-94 20:57 | 1.000057 | 0.000246 | 0.009729 |

Mass Point Leak Rate Analysis

CILRT Phase

Watts Bar Nuclear Plant
Unit 1 - Startup

| <u>Rdg</u> | <u>Time</u> | <u>Norm Mass</u> | <u>MP Leak %/day</u> | <u>MP UCL %/day</u> |
|------------|-----------------|------------------|--------------------------|-------------------------|
| 139 | 27-Jun-94 21:07 | 1.000042 | -0.001645 | 0.007778 |
| 140 | 27-Jun-94 21:17 | 1.000065 | -0.003687 | 0.005712 |
| 141 | 27-Jun-94 21:27 | 1.000015 | -0.004988 | 0.004270 |
| 142 | 27-Jun-94 21:37 | 1.000005 | -0.006074 | 0.003025 |
| 143 | 27-Jun-94 21:47 | 0.999991 | -0.006925 | 0.001998 |
| 144 | 27-Jun-94 21:57 | 0.999951 | -0.007276 | 0.001448 |
| 145 | 27-Jun-94 22:07 | 0.999987 | -0.007980 | 0.000571 |
| 146 | 27-Jun-94 22:17 | 0.999979 | -0.008554 | -0.000176 |
| 147 | 27-Jun-94 22:27 | 0.999951 | -0.008790 | -0.000596 |
| 148 | 27-Jun-94 22:37 | 0.999946 | -0.008960 | -0.000945 |
| 149 | 27-Jun-94 22:48 | 0.999960 | -0.009250 | -0.001404 |
| 150 | 27-Jun-94 22:58 | 0.999972 | -0.009627 | -0.001941 |
| 151 | 27-Jun-94 23:08 | 0.999977 | -0.010022 | -0.002490 |
| 152 | 27-Jun-94 23:18 | 0.999942 | -0.010064 | -0.002690 |
| 153 | 27-Jun-94 23:28 | 1.000008 | -0.010693 | -0.003448 |
| 154 | 27-Jun-94 23:38 | 1.000003 | -0.011235 | -0.004120 |
| 155 | 27-Jun-94 23:48 | 0.999931 | -0.011114 | -0.004143 |
| 156 | 27-Jun-94 23:58 | 0.999952 | -0.011173 | -0.004343 |
| 157 | 28-Jun-94 00:08 | 0.999972 | -0.011383 | -0.004685 |
| 158 | 28-Jun-94 00:18 | 1.000039 | -0.012124 | -0.005521 |
| 159 | 28-Jun-94 00:28 | 1.000012 | -0.012604 | -0.006113 |
| 160 | 28-Jun-94 00:38 | 1.000000 | -0.012953 | -0.006579 |
| 161 | 28-Jun-94 00:48 | 0.999991 | -0.013204 | -0.006948 |
| 162 | 28-Jun-94 00:58 | 0.999932 | -0.012991 | -0.006850 |
| 163 | 28-Jun-94 01:08 | 0.999964 | -0.013016 | -0.006990 |
| 164 | 28-Jun-94 01:18 | 0.999950 | -0.012935 | -0.007021 |
| 165 | 28-Jun-94 01:28 | 0.999964 | -0.012954 | -0.007149 |
| 166 | 28-Jun-94 01:38 | 0.999889 | -0.012437 | -0.006717 |
| 167 | 28-Jun-94 01:48 | 0.999920 | -0.012154 | -0.006531 |
| 168 | 28-Jun-94 01:58 | 0.999984 | -0.012315 | -0.006791 |
| 169 | 28-Jun-94 02:08 | 1.000052 | -0.012916 | -0.007459 |
| 170 | 28-Jun-94 02:18 | 0.999967 | -0.012919 | -0.007559 |
| 171 | 28-Jun-94 02:28 | 0.999929 | -0.012674 | -0.007402 |
| 172 | 28-Jun-94 02:38 | 0.999914 | -0.012338 | -0.007148 |
| 173 | 28-Jun-94 02:48 | 0.999946 | -0.012214 | -0.007111 |
| 174 | 28-Jun-94 02:58 | 0.999943 | -0.012074 | -0.007056 |
| 175 | 28-Jun-94 03:08 | 0.999924 | -0.011821 | -0.006882 |
| 176 | 28-Jun-94 03:18 | 0.999920 | -0.011551 | -0.006687 |
| 177 | 28-Jun-94 03:28 | 0.999896 | -0.011152 | -0.006354 |
| 178 | 28-Jun-94 03:38 | 0.999833 | -0.010407 | -0.005634 |
| 179 | 28-Jun-94 03:48 | 0.999844 | -0.009758 | -0.005021 |

Mass Point Leak Rate Analysis

CILRT Phase

Watts Bar Nuclear Plant
Unit 1 - Startup

| <u>Rdg</u> | <u>Time</u> | <u>Norm Mass</u> | <u>MP Leak %/day</u> | <u>MP UCL %/day</u> |
|------------|-----------------|------------------|--------------------------|-------------------------|
| 180 | 28-Jun-94 03:58 | 0.999804 | -0.008915 | -0.004186 |
| 181 | 28-Jun-94 04:08 | 0.999784 | -0.007996 | -0.003261 |
| 182 | 28-Jun-94 04:18 | 0.999764 | -0.007014 | -0.002260 |
| 183 | 28-Jun-94 04:28 | 0.999762 | -0.006062 | -0.001294 |
| 184 | 28-Jun-94 04:38 | 0.999789 | -0.005291 | -0.000540 |
| 185 | 28-Jun-94 04:48 | 0.999792 | -0.004570 | 0.000158 |
| 186 | 28-Jun-94 04:58 | 0.999786 | -0.003848 | 0.000858 |
| 187 | 28-Jun-94 05:08 | 0.999791 | -0.003183 | 0.001494 |
| 188 | 28-Jun-94 05:18 | 0.999808 | -0.002632 | 0.002005 |
| 189 | 28-Jun-94 05:28 | 0.999808 | -0.002100 | 0.002494 |
| 190 | 28-Jun-94 05:38 | 0.999817 | -0.001637 | 0.002911 |
| 191 | 28-Jun-94 05:48 | 0.999780 | -0.001022 | 0.003497 |
| 192 | 28-Jun-94 05:58 | 0.999809 | -0.000566 | 0.003907 |
| 193 | 28-Jun-94 06:08 | 0.999761 | 0.000089 | 0.004541 |
| 194 | 28-Jun-94 06:18 | 0.999892 | 0.000130 | 0.004518 |
| 195 | 28-Jun-94 06:28 | 0.999852 | 0.000347 | 0.004677 |
| 196 | 28-Jun-94 06:38 | 0.999858 | 0.000528 | 0.004800 |
| 197 | 28-Jun-94 06:48 | 0.999829 | 0.000827 | 0.005047 |
| 198 | 28-Jun-94 06:58 | 0.999799 | 0.001240 | 0.005420 |
| 199 | 28-Jun-94 07:08 | 0.999830 | 0.001505 | 0.005633 |
| 200 | 28-Jun-94 07:18 | 0.999837 | 0.001728 | 0.005805 |
| 201 | 28-Jun-94 07:28 | 0.999856 | 0.001867 | 0.005890 |
| 202 | 28-Jun-94 07:38 | 0.999853 | 0.002010 | 0.005980 |
| 203 | 28-Jun-94 07:48 | 0.999898 | 0.001971 | 0.005887 |
| 204 | 28-Jun-94 07:58 | 0.999931 | 0.001805 | 0.005672 |
| 205 | 28-Jun-94 08:08 | 0.999827 | 0.002043 | 0.005865 |
| 206 | 28-Jun-94 08:18 | 0.999798 | 0.002380 | 0.006165 |
| 207 | 28-Jun-94 08:28 | 0.999831 | 0.002581 | 0.006321 |
| 208 | 28-Jun-94 08:38 | 0.999828 | 0.002786 | 0.006481 |
| 209 | 28-Jun-94 08:48 | 0.999845 | 0.002920 | 0.006569 |
| 210 | 28-Jun-94 08:58 | 0.999846 | 0.003044 | 0.006648 |
| 211 | 28-Jun-94 09:08 | 0.999863 | 0.003104 | 0.006661 |
| 212 | 28-Jun-94 09:18 | 0.999856 | 0.003185 | 0.006697 |
| 213 | 28-Jun-94 09:28 | 0.999806 | 0.003433 | 0.006910 |
| 214 | 28-Jun-94 09:38 | 0.999765 | 0.003811 | 0.007262 |
| 215 | 28-Jun-94 09:48 | 0.999772 | 0.004150 | 0.007573 |
| 216 | 28-Jun-94 09:58 | 0.999738 | 0.004591 | 0.007997 |
| 217 | 28-Jun-94 10:08 | 0.999715 | 0.005089 | 0.008487 |
| 218 | 28-Jun-94 10:18 | 0.999706 | 0.005597 | 0.008988 |
| 219 | 28-Jun-94 10:28 | 0.999731 | 0.006007 | 0.009379 |
| 220 | 28-Jun-94 10:38 | 0.999757 | 0.006315 | 0.009659 |

Mass Point Leak Rate Analysis

CILRT Phase

Watts Bar Nuclear Plant
Unit 1 - Startup

| <u>Rdg</u> | <u>Time</u> | <u>Norm Mass</u> | <u>MP Leak %/day</u> | <u>MP UCL %/day</u> |
|------------|-----------------|------------------|--------------------------|-------------------------|
| 221 | 28-Jun-94 10:48 | 0.999773 | 0.006562 | 0.009874 |
| 222 | 28-Jun-94 10:58 | 0.999736 | 0.006914 | 0.010203 |
| 223 | 28-Jun-94 11:08 | 0.999764 | 0.007166 | 0.010424 |
| 224 | 28-Jun-94 11:18 | 0.999767 | 0.007397 | 0.010624 |
| 225 | 28-Jun-94 11:28 | 0.999784 | 0.007568 | 0.010761 |
| 226 | 28-Jun-94 11:38 | 0.999782 | 0.007739 | 0.010899 |
| 227 | 28-Jun-94 11:48 | 0.999739 | 0.008027 | 0.011162 |
| 228 | 28-Jun-94 11:58 | 0.999818 | 0.008075 | 0.011174 |
| 229 | 28-Jun-94 12:08 | 0.999792 | 0.008193 | 0.011259 |
| 230 | 28-Jun-94 12:18 | 0.999848 | 0.008149 | 0.011179 |
| 231 | 28-Jun-94 12:28 | 0.999834 | 0.008144 | 0.011140 |
| 232 | 28-Jun-94 12:38 | 0.999854 | 0.008082 | 0.011045 |
| 233 | 28-Jun-94 12:48 | 0.999860 | 0.008006 | 0.010936 |
| 234 | 28-Jun-94 12:58 | 0.999774 | 0.008161 | 0.011062 |

Mass Point Termination Criteria

CILRT Phase

| Rdg | Date/Time | MP UCL %/ day | Watts Bar Nuclear Plant | | | Scatter 2.1 |
|-----|-----------------|------------------|-------------------------------|-------------|------------|-------------|
| | | | Unit 1 - Startup Curve 1.1 | Curve 1.1.1 | Curve 1.2 | |
| 57 | 27-Jun-94 07:22 | 0.000000 | 0.000000 | 0.000000 | 0.000000 | 0.000000 |
| 58 | 27-Jun-94 07:32 | 0.000000 | 0.000000 | 0.000000 | 0.000000 | 1.000000 |
| 59 | 27-Jun-94 07:42 | 2.152317 | 0.000000 | 0.000000 | 0.000000 | 0.489281 |
| 60 | 27-Jun-94 07:52 | 0.227590 | 0.006759 | -68.918621 | 211.622608 | 0.529025 |
| 61 | 27-Jun-94 08:02 | 0.093280 | 0.106099 | -39.528565 | 142.462168 | 0.535392 |
| 62 | 27-Jun-94 08:12 | 0.310703 | 1.271407 | -63.167392 | 441.617948 | 0.190699 |
| 63 | 27-Jun-94 08:22 | 0.260423 | 0.608353 | -35.037861 | 288.855659 | 0.363558 |
| 64 | 27-Jun-94 08:32 | 0.226965 | 0.425849 | -20.389812 | 183.110825 | 0.535412 |
| 65 | 27-Jun-94 08:42 | 0.199361 | 0.269254 | -11.549252 | 105.283258 | 0.683482 |
| 66 | 27-Jun-94 08:52 | 0.174947 | 0.129445 | -5.881902 | 51.929576 | 0.808983 |
| 67 | 27-Jun-94 09:02 | 0.138734 | 0.012720 | 1.579512 | 11.550062 | 0.764133 |
| 68 | 27-Jun-94 09:12 | 0.118992 | 0.052805 | 2.393627 | 16.685219 | 0.889198 |
| 69 | 27-Jun-94 09:22 | 0.107899 | 0.057623 | 1.911213 | 13.171576 | 1.048984 |
| 70 | 27-Jun-94 09:32 | 0.123274 | 0.029917 | -1.198838 | 9.142290 | 1.053880 |
| 71 | 27-Jun-94 09:42 | 0.152921 | 0.472999 | -4.339548 | 39.271915 | 0.950203 |
| 72 | 27-Jun-94 09:52 | 0.166168 | 0.982238 | -5.117215 | 52.163632 | 0.973474 |
| 73 | 27-Jun-94 10:02 | 0.182246 | 1.833605 | -5.812395 | 68.684750 | 0.974596 |
| 74 | 27-Jun-94 10:12 | 0.186815 | 2.161790 | -5.296640 | 67.810827 | 1.009299 |
| 75 | 27-Jun-94 10:22 | 0.198859 | 3.252227 | -5.468817 | 80.835819 | 1.011397 |
| 76 | 27-Jun-94 10:32 | 0.194786 | 2.185571 | -4.197935 | 61.852418 | 1.044889 |
| 77 | 27-Jun-94 10:42 | 0.189831 | 1.396436 | -3.114241 | 44.980512 | 1.074596 |
| 78 | 27-Jun-94 10:52 | 0.186982 | 1.090827 | -2.459482 | 35.497773 | 1.100345 |
| 79 | 27-Jun-94 11:02 | 0.183869 | 0.814461 | -1.904681 | 27.274724 | 1.123447 |
| 80 | 27-Jun-94 11:12 | 0.181459 | 0.645949 | -1.511887 | 21.576218 | 1.143485 |
| 81 | 27-Jun-94 11:22 | 0.176215 | 0.282907 | -0.926188 | 12.697961 | 1.162890 |
| 82 | 27-Jun-94 11:32 | 0.171639 | 0.103049 | -0.509508 | 6.758758 | 1.181917 |
| 83 | 27-Jun-94 11:42 | 0.168201 | 0.034045 | -0.263555 | 3.423789 | 1.200046 |
| 84 | 27-Jun-94 11:52 | 0.161494 | 0.037928 | 0.265816 | 3.240186 | 1.211851 |
| 85 | 27-Jun-94 12:02 | 0.156132 | 0.199814 | 0.560055 | 6.537512 | 1.229128 |
| 86 | 27-Jun-94 12:12 | 0.152137 | 0.366846 | 0.686380 | 7.795776 | 1.248614 |
| 87 | 27-Jun-94 12:22 | 0.146360 | 0.833011 | 0.962009 | 10.411637 | 1.263127 |
| 88 | 27-Jun-94 12:32 | 0.140586 | 1.487655 | 1.193045 | 12.325157 | 1.277808 |
| 89 | 27-Jun-94 12:42 | 0.133417 | 2.651154 | 1.533621 | 14.887875 | 1.276645 |
| 90 | 27-Jun-94 12:52 | 0.131700 | 2.441978 | 1.363541 | 13.168213 | 1.299819 |
| 91 | 27-Jun-94 13:02 | 0.127567 | 3.049864 | 1.393911 | 13.112189 | 1.323705 |
| 92 | 27-Jun-94 13:12 | 0.121587 | 4.426053 | 1.579578 | 14.207477 | 1.333348 |
| 93 | 27-Jun-94 13:22 | 0.117550 | 5.234740 | 1.578417 | 13.857022 | 1.360246 |
| 94 | 27-Jun-94 13:32 | 0.112417 | 6.762998 | 1.664925 | 14.127352 | 1.379257 |
| 95 | 27-Jun-94 13:42 | 0.108604 | 7.727377 | 1.643544 | 13.646280 | 1.409556 |
| 96 | 27-Jun-94 13:52 | 0.104407 | 9.158814 | 1.655343 | 13.407273 | 1.438025 |
| 97 | 27-Jun-94 14:02 | 0.099069 | 11.604439 | 1.752921 | 13.716208 | 1.450337 |
| 98 | 27-Jun-94 14:12 | 0.093957 | 14.266691 | 1.818610 | 13.793144 | 1.466872 |
| 99 | 27-Jun-94 14:22 | 0.090773 | 14.963502 | 1.749345 | 13.062151 | 1.507872 |
| 100 | 27-Jun-94 14:32 | 0.087395 | 16.181740 | 1.703330 | 12.503557 | 1.548815 |
| 101 | 27-Jun-94 14:42 | 0.086442 | 13.205261 | 1.536623 | 11.260270 | 1.588398 |
| 102 | 27-Jun-94 14:52 | 0.085198 | 11.641432 | 1.406680 | 10.270294 | 1.629804 |

Mass Point Termination Criteria

CILRT Phase

| <u>Rdg</u> | <u>Date/Time</u> | <u>MP UCL</u> <u>% / day</u> | Watts Bar Nuclear Plant | | | |
|------------|------------------|---------------------------------|---|--------------------|------------------|--------------------|
| | | | <u>Unit 1 - Startup</u> <u>Curve 1.1</u> | <u>Curve 1.1.1</u> | <u>Curve 1.2</u> | <u>Scatter 2.1</u> |
| 103 | 27-Jun-94 15:02 | 0.082258 | 12.777340 | 1.381944 | 9.942901 | 1.674031 |
| 104 | 27-Jun-94 15:12 | 0.079828 | 13.368690 | 1.334409 | 9.493327 | 1.722254 |
| 105 | 27-Jun-94 15:22 | 0.076977 | 14.728382 | 1.316351 | 9.233612 | 1.769771 |
| 106 | 27-Jun-94 15:32 | 0.074687 | 15.352346 | 1.272668 | 8.834428 | 1.822195 |
| 107 | 27-Jun-94 15:42 | 0.072589 | 15.781115 | 1.225864 | 8.430588 | 1.876836 |
| 108 | 27-Jun-94 15:52 | 0.070981 | 15.391073 | 1.162470 | 7.943275 | 1.931918 |
| 109 | 27-Jun-94 16:02 | 0.069912 | 14.114432 | 1.083501 | 7.377972 | 1.983125 |
| 110 | 27-Jun-94 16:12 | 0.069324 | 12.259567 | 0.994173 | 6.763077 | 2.026736 |
| 111 | 27-Jun-94 16:22 | 0.068914 | 10.569169 | 0.908129 | 6.176803 | 2.065861 |
| 112 | 27-Jun-94 16:32 | 0.067171 | 11.191670 | 0.886764 | 5.984806 | 2.123858 |
| 113 | 27-Jun-94 16:42 | 0.066056 | 10.952731 | 0.841747 | 5.657404 | 2.178200 |
| 114 | 27-Jun-94 16:52 | 0.065067 | 10.622927 | 0.796933 | 5.337281 | 2.231459 |
| 115 | 27-Jun-94 17:02 | 0.062979 | 11.981658 | 0.803613 | 5.327578 | 2.292291 |
| 116 | 27-Jun-94 17:12 | 0.060742 | 13.678616 | 0.816900 | 5.355929 | 2.353173 |
| 117 | 27-Jun-94 17:22 | 0.058103 | 16.028913 | 0.848340 | 5.486259 | 2.403227 |
| 118 | 27-Jun-94 17:32 | 0.055256 | 18.793166 | 0.886782 | 5.649781 | 2.441918 |
| 119 | 27-Jun-94 17:42 | 0.053050 | 20.940696 | 0.891747 | 5.622214 | 2.508527 |
| 120 | 27-Jun-94 17:52 | 0.050427 | 23.972206 | 0.915170 | 5.694973 | 2.556063 |
| 121 | 27-Jun-94 18:02 | 0.047930 | 27.086430 | 0.930748 | 5.722389 | 2.609035 |
| 122 | 27-Jun-94 18:12 | 0.045858 | 29.487041 | 0.927154 | 5.647100 | 2.682203 |
| 123 | 27-Jun-94 18:22 | 0.042970 | 33.554377 | 0.959291 | 5.759307 | 2.692126 |
| 124 | 27-Jun-94 18:32 | 0.040301 | 37.762863 | 0.978485 | 5.800249 | 2.718339 |
| 125 | 27-Jun-94 18:42 | 0.037813 | 41.966727 | 0.988316 | 5.791830 | 2.755820 |
| 126 | 27-Jun-94 18:52 | 0.036342 | 41.779994 | 0.958953 | 5.587599 | 2.850042 |
| 127 | 27-Jun-94 19:02 | 0.034421 | 44.375140 | 0.948562 | 5.482267 | 2.924294 |
| 128 | 27-Jun-94 19:12 | 0.032289 | 48.175045 | 0.947213 | 5.423895 | 2.977976 |
| 129 | 27-Jun-94 19:22 | 0.029742 | 53.504025 | 0.962211 | 5.446266 | 2.972647 |
| 130 | 27-Jun-94 19:32 | 0.028050 | 55.115532 | 0.944407 | 5.309396 | 3.052842 |
| 131 | 27-Jun-94 19:42 | 0.026358 | 56.988780 | 0.928285 | 5.183522 | 3.130223 |
| 132 | 27-Jun-94 19:57 | 0.023597 | 63.411679 | 0.950004 | 5.238399 | 3.088129 |
| 133 | 27-Jun-94 20:07 | 0.020425 | 69.142516 | 0.986393 | 5.358831 | 2.904090 |
| 134 | 27-Jun-94 20:17 | 0.018119 | 74.974712 | 0.985863 | 5.304796 | 2.892735 |
| 135 | 27-Jun-94 20:27 | 0.015826 | 81.156645 | 0.985270 | 5.251716 | 2.873050 |
| 136 | 27-Jun-94 20:37 | 0.013712 | 86.465008 | 0.978960 | 5.174075 | 2.869697 |
| 137 | 27-Jun-94 20:47 | 0.011963 | 88.199522 | 0.961674 | 5.049112 | 2.903082 |
| 138 | 27-Jun-94 20:57 | 0.009729 | 95.204757 | 0.961770 | 5.004285 | 2.860812 |
| 139 | 27-Jun-94 21:07 | 0.007778 | 100.071958 | 0.952939 | 4.921062 | 2.853502 |
| 140 | 27-Jun-94 21:17 | 0.005712 | 106.605078 | 0.948699 | 4.859745 | 2.820944 |
| 141 | 27-Jun-94 21:27 | 0.004270 | 104.050151 | 0.926214 | 4.720370 | 2.859287 |
| 142 | 27-Jun-94 21:37 | 0.003025 | 98.671256 | 0.900054 | 4.567612 | 2.910616 |
| 143 | 27-Jun-94 21:47 | 0.001998 | 90.571214 | 0.870021 | 4.400585 | 2.975760 |
| 144 | 27-Jun-94 21:57 | 0.001448 | 76.055790 | 0.829953 | 4.192207 | 3.065990 |
| 145 | 27-Jun-94 22:07 | 0.000571 | 70.452786 | 0.801125 | 4.035557 | 3.137580 |
| 146 | 27-Jun-94 22:17 | -0.000176 | 64.484766 | 0.771133 | 3.875881 | 3.216248 |
| 147 | 27-Jun-94 22:27 | -0.000596 | 56.068968 | 0.735243 | 3.692126 | 3.311544 |
| 148 | 27-Jun-94 22:37 | -0.000945 | 49.028737 | 0.700145 | 3.513589 | 3.410387 |

Mass Point Termination Criteria

CILRT Phase

| <u>Rdg</u> | <u>Date/Time</u> | <u>MP UCL</u> <u>% / day</u> | Watts Bar Nuclear Plant | | | |
|------------|------------------|---------------------------------|---|--------------------|------------------|--------------------|
| | | | <u>Unit 1 - Startup</u> <u>Curve 1.1</u> | <u>Curve 1.1.1</u> | <u>Curve 1.2</u> | <u>Scatter 2.1</u> |
| 149 | 27-Jun-94 22:48 | -0.001404 | 44.534993 | 0.670065 | 3.358886 | 3.505210 |
| 150 | 27-Jun-94 22:58 | -0.001941 | 41.483726 | 0.643882 | 3.222961 | 3.595137 |
| 151 | 27-Jun-94 23:08 | -0.002490 | 39.044363 | 0.619749 | 3.097459 | 3.683442 |
| 152 | 27-Jun-94 23:18 | -0.002690 | 34.809049 | 0.589225 | 2.944449 | 3.790751 |
| 153 | 27-Jun-94 23:28 | -0.003448 | 34.392496 | 0.573552 | 2.859210 | 3.855884 |
| 154 | 27-Jun-94 23:38 | -0.004120 | 33.667557 | 0.556903 | 2.770463 | 3.927653 |
| 155 | 27-Jun-94 23:48 | -0.004143 | 29.602696 | 0.526921 | 2.622534 | 4.041256 |
| 156 | 27-Jun-94 23:58 | -0.004343 | 27.156369 | 0.502550 | 2.500680 | 4.150675 |
| 157 | 28-Jun-94 00:08 | -0.004685 | 25.700550 | 0.482795 | 2.400462 | 4.251835 |
| 158 | 28-Jun-94 00:18 | -0.005521 | 26.303386 | 0.475373 | 2.356875 | 4.286476 |
| 159 | 28-Jun-94 00:28 | -0.006113 | 26.053699 | 0.462914 | 2.290918 | 4.355920 |
| 160 | 28-Jun-94 00:38 | -0.006579 | 25.375607 | 0.448476 | 2.216525 | 4.439015 |
| 161 | 28-Jun-94 00:48 | -0.006948 | 24.403039 | 0.432834 | 2.137182 | 4.531708 |
| 162 | 28-Jun-94 00:58 | -0.006850 | 21.641298 | 0.408644 | 2.019380 | 4.653165 |
| 163 | 28-Jun-94 01:08 | -0.006990 | 20.194936 | 0.390546 | 1.929772 | 4.766843 |
| 164 | 28-Jun-94 01:18 | -0.007021 | 18.547340 | 0.371337 | 1.835425 | 4.888188 |
| 165 | 28-Jun-94 01:28 | -0.007149 | 17.411791 | 0.355114 | 1.755121 | 5.005084 |
| 166 | 28-Jun-94 01:38 | -0.006717 | 14.678687 | 0.329259 | 1.630549 | 5.128012 |
| 167 | 28-Jun-94 01:48 | -0.006531 | 13.087930 | 0.309309 | 1.533413 | 5.260629 |
| 168 | 28-Jun-94 01:58 | -0.006791 | 12.748333 | 0.298965 | 1.481217 | 5.368795 |
| 169 | 28-Jun-94 02:08 | -0.007459 | 13.316690 | 0.297537 | 1.470782 | 5.390742 |
| 170 | 28-Jun-94 02:18 | -0.007559 | 12.617722 | 0.284878 | 1.408186 | 5.513591 |
| 171 | 28-Jun-94 02:28 | -0.007402 | 11.373782 | 0.268182 | 1.326900 | 5.650418 |
| 172 | 28-Jun-94 02:38 | -0.007148 | 10.059146 | 0.250653 | 1.241763 | 5.789035 |
| 173 | 28-Jun-94 02:48 | -0.007111 | 9.339585 | 0.237905 | 1.179167 | 5.927486 |
| 174 | 28-Jun-94 02:58 | -0.007056 | 8.646868 | 0.225481 | 1.118191 | 6.068850 |
| 175 | 28-Jun-94 03:08 | -0.006882 | 7.802128 | 0.211630 | 1.050519 | 6.215429 |
| 176 | 28-Jun-94 03:18 | -0.006687 | 7.006777 | 0.198131 | 0.984531 | 6.364217 |
| 177 | 28-Jun-94 03:28 | -0.006354 | 6.077180 | 0.183000 | 0.910731 | 6.509839 |
| 178 | 28-Jun-94 03:38 | -0.005634 | 4.729516 | 0.162429 | 0.810672 | 6.598907 |
| 179 | 28-Jun-94 03:48 | -0.005021 | 3.753414 | 0.144516 | 0.723077 | 6.705738 |
| 180 | 28-Jun-94 03:58 | -0.004186 | 2.734426 | 0.124070 | 0.622799 | 6.753140 |
| 181 | 28-Jun-94 04:08 | -0.003261 | 1.868962 | 0.103261 | 0.520193 | 6.763716 |
| 182 | 28-Jun-94 04:18 | -0.002260 | 1.171813 | 0.082325 | 0.416310 | 6.736953 |
| 183 | 28-Jun-94 04:28 | -0.001294 | 0.679894 | 0.062868 | 0.319103 | 6.712486 |
| 184 | 28-Jun-94 04:38 | -0.000540 | 0.391412 | 0.047376 | 0.241195 | 6.750114 |
| 185 | 28-Jun-94 04:48 | 0.000158 | 0.198663 | 0.033429 | 0.170673 | 6.797162 |
| 186 | 28-Jun-94 04:58 | 0.000858 | 0.073285 | 0.020094 | 0.102883 | 6.836272 |
| 187 | 28-Jun-94 05:08 | 0.001494 | 0.012839 | 0.008304 | 0.042627 | 6.888288 |
| 188 | 28-Jun-94 05:18 | 0.002005 | 0.000227 | -0.001086 | 0.005588 | 6.970415 |
| 189 | 28-Jun-94 05:28 | 0.002494 | 0.018854 | -0.009736 | 0.050196 | 7.053689 |
| 190 | 28-Jun-94 05:38 | 0.002911 | 0.059013 | -0.016911 | 0.087349 | 7.152192 |
| 191 | 28-Jun-94 05:48 | 0.003497 | 0.146094 | -0.026210 | 0.135708 | 7.196059 |
| 192 | 28-Jun-94 05:58 | 0.003907 | 0.234113 | -0.032564 | 0.168916 | 7.288183 |
| 193 | 28-Jun-94 06:08 | 0.004541 | 0.397208 | -0.041811 | 0.217452 | 7.301072 |
| 194 | 28-Jun-94 06:18 | 0.004518 | 0.398552 | -0.040977 | 0.213151 | 7.457968 |

Mass Point Termination Criteria

CILRT Phase

| <u>Rdg</u> | <u>Date/Time</u> | <u>MP UCL</u> <u>% / day</u> | Watts Bar Nuclear Plant | | | <u>Scatter 2.1</u> |
|------------|------------------|---------------------------------|---|--------------------|------------------|--------------------|
| | | | <u>Unit 1 - Startup</u> <u>Curve 1.1</u> | <u>Curve 1.1.1</u> | <u>Curve 1.2</u> | |
| 195 | 28-Jun-94 06:28 | 0.004677 | 0.456545 | -0.042930 | 0.223503 | 7.599510 |
| 196 | 28-Jun-94 06:38 | 0.004800 | 0.506177 | -0.044246 | 0.230520 | 7.747363 |
| 197 | 28-Jun-94 06:48 | 0.005047 | 0.603142 | -0.047321 | 0.246839 | 7.871582 |
| 198 | 28-Jun-94 06:58 | 0.005420 | 0.757063 | -0.052027 | 0.271835 | 7.957996 |
| 199 | 28-Jun-94 07:08 | 0.005633 | 0.858427 | -0.054273 | 0.283874 | 8.087261 |
| 200 | 28-Jun-94 07:18 | 0.005805 | 0.945824 | -0.055801 | 0.292129 | 8.225424 |
| 201 | 28-Jun-94 07:28 | 0.005890 | 0.993441 | -0.056009 | 0.293383 | 8.380159 |
| 202 | 28-Jun-94 07:38 | 0.005980 | 1.044608 | -0.056257 | 0.294851 | 8.535447 |
| 203 | 28-Jun-94 07:48 | 0.005887 | 0.993504 | -0.053791 | 0.281883 | 8.708163 |
| 204 | 28-Jun-94 07:58 | 0.005672 | 0.874135 | -0.049560 | 0.259537 | 8.873792 |
| 205 | 28-Jun-94 08:08 | 0.005865 | 0.978658 | -0.051412 | 0.269494 | 9.009223 |
| 206 | 28-Jun-94 08:18 | 0.006165 | 1.146893 | -0.054631 | 0.286756 | 9.105185 |
| 207 | 28-Jun-94 08:28 | 0.006321 | 1.243080 | -0.055760 | 0.292919 | 9.248217 |
| 208 | 28-Jun-94 08:38 | 0.006481 | 1.346122 | -0.056894 | 0.299126 | 9.389515 |
| 209 | 28-Jun-94 08:48 | 0.006569 | 1.404572 | -0.056979 | 0.299737 | 9.549761 |
| 210 | 28-Jun-94 08:58 | 0.006648 | 1.457552 | -0.056916 | 0.299554 | 9.712967 |
| 211 | 28-Jun-94 09:08 | 0.006661 | 1.463732 | -0.055945 | 0.294513 | 9.890306 |
| 212 | 28-Jun-94 09:18 | 0.006697 | 1.487273 | -0.055315 | 0.291293 | 10.065041 |
| 213 | 28-Jun-94 09:28 | 0.006910 | 1.641706 | -0.057041 | 0.300687 | 10.183965 |
| 214 | 28-Jun-94 09:38 | 0.007262 | 1.908661 | -0.060485 | 0.319332 | 10.224478 |
| 215 | 28-Jun-94 09:48 | 0.007573 | 2.162125 | -0.063268 | 0.334482 | 10.283978 |
| 216 | 28-Jun-94 09:58 | 0.007997 | 2.525720 | -0.067345 | 0.356680 | 10.261780 |
| 217 | 28-Jun-94 10:08 | 0.008487 | 2.971956 | -0.072052 | 0.382385 | 10.182276 |
| 218 | 28-Jun-94 10:18 | 0.008988 | 3.462629 | -0.076721 | 0.408009 | 10.086278 |
| 219 | 28-Jun-94 10:28 | 0.009379 | 3.878124 | -0.079893 | 0.425593 | 10.068271 |
| 220 | 28-Jun-94 10:38 | 0.009659 | 4.192080 | -0.081606 | 0.435269 | 10.116273 |
| 221 | 28-Jun-94 10:48 | 0.009874 | 4.436229 | -0.082440 | 0.440162 | 10.196643 |
| 222 | 28-Jun-94 10:58 | 0.010203 | 4.835643 | -0.084625 | 0.452482 | 10.203086 |
| 223 | 28-Jun-94 11:08 | 0.010424 | 5.107143 | -0.085423 | 0.457225 | 10.271865 |
| 224 | 28-Jun-94 11:18 | 0.010624 | 5.355880 | -0.085925 | 0.460351 | 10.348618 |
| 225 | 28-Jun-94 11:28 | 0.010761 | 5.512419 | -0.085629 | 0.459088 | 10.454960 |
| 226 | 28-Jun-94 11:38 | 0.010899 | 5.674895 | -0.085353 | 0.457932 | 10.558723 |
| 227 | 28-Jun-94 11:48 | 0.011162 | 6.042602 | -0.086573 | 0.465028 | 10.585310 |
| 228 | 28-Jun-94 11:58 | 0.011174 | 5.976162 | -0.084693 | 0.455023 | 10.737107 |
| 229 | 28-Jun-94 12:08 | 0.011259 | 6.052482 | -0.083780 | 0.450337 | 10.860700 |
| 230 | 28-Jun-94 12:18 | 0.011179 | 5.800163 | -0.080845 | 0.434479 | 11.036290 |
| 231 | 28-Jun-94 12:28 | 0.011140 | 5.639003 | -0.078503 | 0.421885 | 11.205400 |
| 232 | 28-Jun-94 12:38 | 0.011045 | 5.367250 | -0.075530 | 0.405802 | 11.387432 |
| 233 | 28-Jun-94 12:48 | 0.010936 | 5.078915 | -0.072484 | 0.389312 | 11.573021 |
| 234 | 28-Jun-94 12:58 | 0.011062 | 5.239246 | -0.072380 | 0.389005 | 11.674187 |

Total Time Leak Rate Analysis

CILRT Phase

Watts Bar Nuclear Plant
Unit 1 - Startup

| <u>Rdg</u> | <u>Date / Time</u> | <u>TT Meas</u> <u>% / day</u> | <u>TT Calc</u> <u>% / day</u> | <u>TT UCL</u> <u>% / day</u> |
|------------|--------------------|----------------------------------|----------------------------------|---------------------------------|
| 57 | 27-Jun-94 07:22 | 0.000000 | 0.000000 | 0.000000 |
| 58 | 27-Jun-94 07:32 | -0.751312 | 0.000000 | 0.000000 |
| 59 | 27-Jun-94 07:42 | -0.262136 | -0.262136 | 0.000000 |
| 60 | 27-Jun-94 07:52 | -0.217718 | -0.143604 | 1.613483 |
| 61 | 27-Jun-94 08:02 | -0.150487 | -0.068376 | 0.767111 |
| 62 | 27-Jun-94 08:12 | 0.076975 | 0.092808 | 0.622349 |
| 63 | 27-Jun-94 08:22 | 0.021757 | 0.139756 | 0.631553 |
| 64 | 27-Jun-94 08:32 | 0.033821 | 0.166319 | 0.639819 |
| 65 | 27-Jun-94 08:42 | 0.035486 | 0.178910 | 0.641882 |
| 66 | 27-Jun-94 08:52 | 0.031795 | 0.182070 | 0.637226 |
| 67 | 27-Jun-94 09:02 | -0.022698 | 0.162599 | 0.626720 |
| 68 | 27-Jun-94 09:12 | 0.006980 | 0.156013 | 0.608919 |
| 69 | 27-Jun-94 09:22 | 0.019604 | 0.153121 | 0.591635 |
| 70 | 27-Jun-94 09:32 | 0.075319 | 0.164868 | 0.582261 |
| 71 | 27-Jun-94 09:42 | 0.118503 | 0.183894 | 0.580465 |
| 72 | 27-Jun-94 09:52 | 0.112191 | 0.196202 | 0.577188 |
| 73 | 27-Jun-94 10:02 | 0.133408 | 0.209927 | 0.576615 |
| 74 | 27-Jun-94 10:12 | 0.120979 | 0.217551 | 0.574067 |
| 75 | 27-Jun-94 10:22 | 0.148997 | 0.228743 | 0.574462 |
| 76 | 27-Jun-94 10:32 | 0.112171 | 0.230168 | 0.570637 |
| 77 | 27-Jun-94 10:42 | 0.108629 | 0.230142 | 0.566326 |
| 78 | 27-Jun-94 10:52 | 0.116164 | 0.230898 | 0.562378 |
| 79 | 27-Jun-94 11:02 | 0.115385 | 0.230941 | 0.558229 |
| 80 | 27-Jun-94 11:12 | 0.118329 | 0.231067 | 0.554239 |
| 81 | 27-Jun-94 11:22 | 0.104286 | 0.228569 | 0.549104 |
| 82 | 27-Jun-94 11:32 | 0.105167 | 0.226200 | 0.543970 |
| 83 | 27-Jun-94 11:42 | 0.109164 | 0.224435 | 0.539127 |
| 84 | 27-Jun-94 11:52 | 0.086020 | 0.219343 | 0.532789 |
| 85 | 27-Jun-94 12:02 | 0.091108 | 0.215304 | 0.526757 |
| 86 | 27-Jun-94 12:12 | 0.096740 | 0.212265 | 0.521170 |
| 87 | 27-Jun-94 12:22 | 0.080798 | 0.207322 | 0.514677 |
| 88 | 27-Jun-94 12:32 | 0.076374 | 0.202188 | 0.508025 |
| 89 | 27-Jun-94 12:42 | 0.058381 | 0.195298 | 0.500547 |
| 90 | 27-Jun-94 12:52 | 0.096394 | 0.193351 | 0.495414 |
| 91 | 27-Jun-94 13:02 | 0.078421 | 0.189436 | 0.489292 |
| 92 | 27-Jun-94 13:12 | 0.058368 | 0.183592 | 0.482244 |
| 93 | 27-Jun-94 13:22 | 0.071485 | 0.179567 | 0.476059 |
| 94 | 27-Jun-94 13:32 | 0.058216 | 0.174430 | 0.469323 |
| 95 | 27-Jun-94 13:42 | 0.066166 | 0.170471 | 0.463220 |
| 96 | 27-Jun-94 13:52 | 0.059502 | 0.166101 | 0.456923 |
| 97 | 27-Jun-94 14:02 | 0.044142 | 0.160542 | 0.450026 |

Total Time Leak Rate Analysis

CILRT Phase

Watts Bar Nuclear Plant
Unit 1 - Startup

| <u>Rdg</u> | <u>Date / Time</u> | <u>TT Meas</u> <u>% / day</u> | <u>TT Calc</u> <u>% / day</u> | <u>TT UCL</u> <u>% / day</u> |
|------------|--------------------|----------------------------------|----------------------------------|---------------------------------|
| 98 | 27-Jun-94 14:12 | 0.042190 | 0.155197 | 0.443233 |
| 99 | 27-Jun-94 14:22 | 0.057047 | 0.151574 | 0.437405 |
| 100 | 27-Jun-94 14:32 | 0.052526 | 0.147771 | 0.431524 |
| 101 | 27-Jun-94 14:42 | 0.071049 | 0.145842 | 0.426895 |
| 102 | 27-Jun-94 14:52 | 0.068018 | 0.143738 | 0.422230 |
| 103 | 27-Jun-94 15:02 | 0.051306 | 0.140334 | 0.416805 |
| 104 | 27-Jun-94 15:12 | 0.053910 | 0.137354 | 0.411699 |
| 105 | 27-Jun-94 15:22 | 0.047467 | 0.134016 | 0.406419 |
| 106 | 27-Jun-94 15:32 | 0.050867 | 0.131142 | 0.401482 |
| 107 | 27-Jun-94 15:42 | 0.050862 | 0.128432 | 0.396711 |
| 108 | 27-Jun-94 15:52 | 0.054095 | 0.126112 | 0.392254 |
| 109 | 27-Jun-94 16:02 | 0.058109 | 0.124213 | 0.388149 |
| 110 | 27-Jun-94 16:12 | 0.061905 | 0.122690 | 0.384381 |
| 111 | 27-Jun-94 16:22 | 0.063163 | 0.121322 | 0.380787 |
| 112 | 27-Jun-94 16:32 | 0.048929 | 0.119006 | 0.376578 |
| 113 | 27-Jun-94 16:42 | 0.054356 | 0.117188 | 0.372770 |
| 114 | 27-Jun-94 16:52 | 0.054760 | 0.115481 | 0.369092 |
| 115 | 27-Jun-94 17:02 | 0.040904 | 0.112921 | 0.364867 |
| 116 | 27-Jun-94 17:12 | 0.037042 | 0.110238 | 0.360599 |
| 117 | 27-Jun-94 17:22 | 0.029299 | 0.107183 | 0.356119 |
| 118 | 27-Jun-94 17:32 | 0.023817 | 0.103931 | 0.351541 |
| 119 | 27-Jun-94 17:42 | 0.030668 | 0.101278 | 0.347381 |
| 120 | 27-Jun-94 17:52 | 0.022530 | 0.098246 | 0.343000 |
| 121 | 27-Jun-94 18:02 | 0.022053 | 0.095335 | 0.338724 |
| 122 | 27-Jun-94 18:12 | 0.025964 | 0.092802 | 0.334733 |
| 123 | 27-Jun-94 18:22 | 0.011441 | 0.089525 | 0.330275 |
| 124 | 27-Jun-94 18:32 | 0.012436 | 0.086464 | 0.325977 |
| 125 | 27-Jun-94 18:42 | 0.012870 | 0.083575 | 0.321816 |
| 126 | 27-Jun-94 18:52 | 0.025545 | 0.081537 | 0.318278 |
| 127 | 27-Jun-94 19:02 | 0.017647 | 0.079149 | 0.314518 |
| 128 | 27-Jun-94 19:12 | 0.012549 | 0.076589 | 0.310665 |
| 129 | 27-Jun-94 19:22 | 0.003723 | 0.073663 | 0.306585 |
| 130 | 27-Jun-94 19:32 | 0.015054 | 0.071475 | 0.303043 |
| 131 | 27-Jun-94 19:42 | 0.013410 | 0.069298 | 0.299536 |
| 132 | 27-Jun-94 19:57 | -0.005444 | 0.066555 | 0.295871 |
| 133 | 27-Jun-94 20:07 | -0.015600 | 0.063021 | 0.291464 |
| 134 | 27-Jun-94 20:17 | -0.002811 | 0.060291 | 0.287591 |
| 135 | 27-Jun-94 20:27 | -0.004833 | 0.057578 | 0.283752 |
| 136 | 27-Jun-94 20:37 | -0.004034 | 0.055027 | 0.280049 |
| 137 | 27-Jun-94 20:47 | -0.000058 | 0.052787 | 0.276595 |
| 138 | 27-Jun-94 20:57 | -0.010056 | 0.050151 | 0.272876 |

Total Time Leak Rate Analysis

CILRT Phase

Watts Bar Nuclear Plant
Unit 1 - Startup

| <u>Rdg</u> | <u>Date / Time</u> | <u>TT Meas</u> <u>% / day</u> | <u>TT Calc</u> <u>% / day</u> | <u>TT UCL</u> <u>% / day</u> |
|------------|--------------------|----------------------------------|----------------------------------|---------------------------------|
| 139 | 27-Jun-94 21:07 | -0.007283 | 0.047763 | 0.269355 |
| 140 | 27-Jun-94 21:17 | -0.011245 | 0.045287 | 0.265791 |
| 141 | 27-Jun-94 21:27 | -0.002576 | 0.043323 | 0.262631 |
| 142 | 27-Jun-94 21:37 | -0.000783 | 0.041524 | 0.259622 |
| 143 | 27-Jun-94 21:47 | 0.001512 | 0.039905 | 0.256779 |
| 144 | 27-Jun-94 21:57 | 0.008010 | 0.038646 | 0.254259 |
| 145 | 27-Jun-94 22:07 | 0.002158 | 0.037174 | 0.251582 |
| 146 | 27-Jun-94 22:17 | 0.003338 | 0.035813 | 0.249019 |
| 147 | 27-Jun-94 22:27 | 0.007817 | 0.034701 | 0.246690 |
| 148 | 27-Jun-94 22:37 | 0.008441 | 0.033659 | 0.244444 |
| 149 | 27-Jun-94 22:48 | 0.006187 | 0.032560 | 0.242169 |
| 150 | 27-Jun-94 22:58 | 0.004341 | 0.031423 | 0.239882 |
| 151 | 27-Jun-94 23:08 | 0.003525 | 0.030295 | 0.237621 |
| 152 | 27-Jun-94 23:18 | 0.008746 | 0.029425 | 0.235608 |
| 153 | 27-Jun-94 23:28 | -0.001177 | 0.028179 | 0.233285 |
| 154 | 27-Jun-94 23:38 | -0.000437 | 0.027008 | 0.231045 |
| 155 | 27-Jun-94 23:48 | 0.010032 | 0.026301 | 0.229233 |
| 156 | 27-Jun-94 23:58 | 0.006895 | 0.025495 | 0.227348 |
| 157 | 28-Jun-94 00:08 | 0.004075 | 0.024605 | 0.225407 |
| 158 | 28-Jun-94 00:18 | -0.005505 | 0.023372 | 0.223183 |
| 159 | 28-Jun-94 00:28 | -0.001726 | 0.022327 | 0.221138 |
| 160 | 28-Jun-94 00:38 | -0.000016 | 0.021385 | 0.219197 |
| 161 | 28-Jun-94 00:48 | 0.001260 | 0.020522 | 0.217343 |
| 162 | 28-Jun-94 00:58 | 0.009225 | 0.019989 | 0.215807 |
| 163 | 28-Jun-94 01:08 | 0.004919 | 0.019313 | 0.214153 |
| 164 | 28-Jun-94 01:18 | 0.006649 | 0.018724 | 0.212594 |
| 165 | 28-Jun-94 01:28 | 0.004718 | 0.018084 | 0.211003 |
| 166 | 28-Jun-94 01:38 | 0.014545 | 0.017821 | 0.209785 |
| 167 | 28-Jun-94 01:48 | 0.010405 | 0.017417 | 0.208445 |
| 168 | 28-Jun-94 01:58 | 0.002030 | 0.016730 | 0.206852 |
| 169 | 28-Jun-94 02:08 | -0.006681 | 0.015758 | 0.205016 |
| 170 | 28-Jun-94 02:18 | 0.004218 | 0.015197 | 0.203565 |
| 171 | 28-Jun-94 02:28 | 0.008929 | 0.014817 | 0.202300 |
| 172 | 28-Jun-94 02:38 | 0.010757 | 0.014511 | 0.201119 |
| 173 | 28-Jun-94 02:48 | 0.006696 | 0.014078 | 0.199826 |
| 174 | 28-Jun-94 02:58 | 0.006995 | 0.013668 | 0.198568 |
| 175 | 28-Jun-94 03:08 | 0.009237 | 0.013346 | 0.197407 |
| 176 | 28-Jun-94 03:18 | 0.009679 | 0.013049 | 0.196281 |
| 177 | 28-Jun-94 03:28 | 0.012397 | 0.012850 | 0.195264 |
| 178 | 28-Jun-94 03:38 | 0.019787 | 0.012899 | 0.194510 |
| 179 | 28-Jun-94 03:48 | 0.018298 | 0.012899 | 0.193715 |

Total Time Leak Rate Analysis

CILRT Phase

Watts Bar Nuclear Plant
Unit 1 - Startup

| <u>Rdg</u> | <u>Date / Time</u> | <u>TT Meas</u> <u>% / day</u> | <u>TT Calc</u> <u>% / day</u> | <u>TT UCL</u> <u>% / day</u> |
|------------|--------------------|----------------------------------|----------------------------------|---------------------------------|
| 180 | 28-Jun-94 03:58 | 0.022788 | 0.013044 | 0.193083 |
| 181 | 28-Jun-94 04:08 | 0.024989 | 0.013255 | 0.192530 |
| 182 | 28-Jun-94 04:18 | 0.027007 | 0.013525 | 0.192051 |
| 183 | 28-Jun-94 04:28 | 0.027074 | 0.013790 | 0.191576 |
| 184 | 28-Jun-94 04:38 | 0.023831 | 0.013948 | 0.190995 |
| 185 | 28-Jun-94 04:48 | 0.023284 | 0.014085 | 0.190401 |
| 186 | 28-Jun-94 04:58 | 0.023814 | 0.014235 | 0.189831 |
| 187 | 28-Jun-94 05:08 | 0.023055 | 0.014359 | 0.189241 |
| 188 | 28-Jun-94 05:18 | 0.020971 | 0.014417 | 0.188592 |
| 189 | 28-Jun-94 05:28 | 0.020896 | 0.014472 | 0.187948 |
| 190 | 28-Jun-94 05:38 | 0.019721 | 0.014491 | 0.187275 |
| 191 | 28-Jun-94 05:48 | 0.023486 | 0.014621 | 0.186726 |
| 192 | 28-Jun-94 05:58 | 0.020257 | 0.014654 | 0.186083 |
| 193 | 28-Jun-94 06:08 | 0.025188 | 0.014829 | 0.185598 |
| 194 | 28-Jun-94 06:18 | 0.011299 | 0.014600 | 0.184708 |
| 195 | 28-Jun-94 06:28 | 0.015397 | 0.014495 | 0.183947 |
| 196 | 28-Jun-94 06:38 | 0.014660 | 0.014372 | 0.183177 |
| 197 | 28-Jun-94 06:48 | 0.017547 | 0.014334 | 0.182499 |
| 198 | 28-Jun-94 06:58 | 0.020484 | 0.014379 | 0.181915 |
| 199 | 28-Jun-94 07:08 | 0.017161 | 0.014331 | 0.181243 |
| 200 | 28-Jun-94 07:18 | 0.016308 | 0.014262 | 0.180554 |
| 201 | 28-Jun-94 07:28 | 0.014375 | 0.014141 | 0.036812 |
| 202 | 28-Jun-94 07:38 | 0.014509 | 0.014028 | 0.036541 |
| 203 | 28-Jun-94 07:48 | 0.010029 | 0.013796 | 0.036154 |
| 204 | 28-Jun-94 07:58 | 0.006766 | 0.013483 | 0.035687 |
| 205 | 28-Jun-94 08:08 | 0.016761 | 0.013444 | 0.035497 |
| 206 | 28-Jun-94 08:18 | 0.019415 | 0.013476 | 0.035380 |
| 207 | 28-Jun-94 08:28 | 0.016164 | 0.013423 | 0.035180 |
| 208 | 28-Jun-94 08:38 | 0.016365 | 0.013377 | 0.034988 |
| 209 | 28-Jun-94 08:48 | 0.014656 | 0.013287 | 0.034756 |
| 210 | 28-Jun-94 08:58 | 0.014446 | 0.013195 | 0.034522 |
| 211 | 28-Jun-94 09:08 | 0.012801 | 0.013063 | 0.034250 |
| 212 | 28-Jun-94 09:18 | 0.013373 | 0.012949 | 0.033998 |
| 213 | 28-Jun-94 09:28 | 0.017844 | 0.012951 | 0.033864 |
| 214 | 28-Jun-94 09:38 | 0.021448 | 0.013044 | 0.033824 |
| 215 | 28-Jun-94 09:48 | 0.020670 | 0.013116 | 0.033764 |
| 216 | 28-Jun-94 09:58 | 0.023677 | 0.013262 | 0.033779 |
| 217 | 28-Jun-94 10:08 | 0.025562 | 0.013451 | 0.033841 |
| 218 | 28-Jun-94 10:18 | 0.026206 | 0.013652 | 0.033916 |
| 219 | 28-Jun-94 10:28 | 0.023859 | 0.013793 | 0.033932 |
| 220 | 28-Jun-94 10:38 | 0.021361 | 0.013869 | 0.033885 |

Total Time Leak Rate Analysis

CILRT Phase

Watts Bar Nuclear Plant
Unit 1 - Startup

| <u>Rdg</u> | <u>Date / Time</u> | <u>TT Meas</u> <u>% / day</u> | <u>TT Calc</u> <u>% / day</u> | <u>TT UCL</u> <u>% / day</u> |
|------------|--------------------|----------------------------------|----------------------------------|---------------------------------|
| 221 | 28-Jun-94 10:48 | 0.019856 | 0.013909 | 0.033801 |
| 222 | 28-Jun-94 10:58 | 0.022967 | 0.014022 | 0.033794 |
| 223 | 28-Jun-94 11:08 | 0.020399 | 0.014072 | 0.033725 |
| 224 | 28-Jun-94 11:18 | 0.019986 | 0.014112 | 0.033646 |
| 225 | 28-Jun-94 11:28 | 0.018419 | 0.014114 | 0.033531 |
| 226 | 28-Jun-94 11:38 | 0.018548 | 0.014119 | 0.033421 |
| 227 | 28-Jun-94 11:48 | 0.022015 | 0.014206 | 0.033394 |
| 228 | 28-Jun-94 11:58 | 0.015233 | 0.014134 | 0.033208 |
| 229 | 28-Jun-94 12:08 | 0.017325 | 0.014111 | 0.033075 |
| 230 | 28-Jun-94 12:18 | 0.012589 | 0.013981 | 0.032835 |
| 231 | 28-Jun-94 12:28 | 0.013688 | 0.013880 | 0.032624 |
| 232 | 28-Jun-94 12:38 | 0.011953 | 0.013741 | 0.032377 |
| 233 | 28-Jun-94 12:48 | 0.011451 | 0.013594 | 0.032123 |
| 234 | 28-Jun-94 12:58 | 0.018307 | 0.013603 | 0.032027 |

Containment Calculated Values CILRT Phase

Watts Bar Nuclear Plant
Unit 1 - Startup

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|--------------------|------------------|-------------|--------------------|--------------|
| 57 | 07:22:24 | Upper Containment | 96084.14 | 84.514 | 0.1061 | 29.4129 |
| | | Lower Containment | 55652.97 | 84.800 | 0.1047 | 29.4161 |
| | | Ice Condenser | 25549.56 | 29.489 | 0.0185 | 29.4170 |
| | | TOTAL | 177286.67 | | | |
| 58 | 07:32:24 | Upper Containment | 96090.76 | 84.464 | 0.1054 | 29.4115 |
| | | Lower Containment | 55653.76 | 84.783 | 0.1039 | 29.4148 |
| | | Ice Condenser | 25551.40 | 29.431 | 0.0185 | 29.4157 |
| | | TOTAL | 177295.92 | | | |
| 59 | 07:42:25 | Upper Containment | 96083.28 | 84.480 | 0.1050 | 29.4097 |
| | | Lower Containment | 55651.69 | 84.781 | 0.1034 | 29.4131 |
| | | Ice Condenser | 25558.17 | 29.274 | 0.0185 | 29.4140 |
| | | TOTAL | 177293.13 | | | |
| 60 | 07:52:25 | Upper Containment | 96083.51 | 84.466 | 0.1045 | 29.4085 |
| | | Lower Containment | 55651.08 | 84.777 | 0.1027 | 29.4118 |
| | | Ice Condenser | 25560.12 | 29.215 | 0.0185 | 29.4127 |
| | | TOTAL | 177294.71 | | | |
| 61 | 08:02:25 | Upper Containment | 96080.87 | 84.470 | 0.1042 | 29.4076 |
| | | Lower Containment | 55652.25 | 84.767 | 0.1021 | 29.4113 |
| | | Ice Condenser | 25560.96 | 29.186 | 0.0185 | 29.4119 |
| | | TOTAL | 177294.08 | | | |
| 62 | 08:12:26 | Upper Containment | 96076.83 | 84.447 | 0.1036 | 29.4045 |
| | | Lower Containment | 55647.98 | 84.759 | 0.1018 | 29.4083 |
| | | Ice Condenser | 25557.12 | 29.208 | 0.0185 | 29.4088 |
| | | TOTAL | 177281.93 | | | |
| 63 | 08:22:26 | Upper Containment | 96078.64 | 84.423 | 0.1031 | 29.4033 |
| | | Lower Containment | 55646.91 | 84.753 | 0.1009 | 29.4066 |
| | | Ice Condenser | 25559.51 | 29.140 | 0.0185 | 29.4075 |
| | | TOTAL | 177285.06 | | | |
| 64 | 08:32:26 | Upper Containment | 96077.67 | 84.396 | 0.1027 | 29.4011 |
| | | Lower Containment | 55645.18 | 84.743 | 0.1003 | 29.4045 |
| | | Ice Condenser | 25560.90 | 29.077 | 0.0185 | 29.4053 |
| | | TOTAL | 177283.75 | | | |
| 65 | 08:42:27 | Upper Containment | 96074.35 | 84.386 | 0.1021 | 29.3990 |
| | | Lower Containment | 55643.31 | 84.729 | 0.0999 | 29.4024 |
| | | Ice Condenser | 25565.50 | 28.953 | 0.0185 | 29.4031 |
| | | TOTAL | 177283.17 | | | |
| 66 | 08:52:27 | Upper Containment | 96078.62 | 84.332 | 0.1017 | 29.3970 |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|--------------------|-------------|-------------|--------------------|--------------|
| | | Lower Containment | 55641.58 | 84.721 | 0.0992 | 29.4003 |
| | | Ice Condenser | 25562.95 | 28.968 | 0.0185 | 29.4011 |
| | | TOTAL | 177283.14 | | | |
| 67 | 09:02:27 | Upper Containment | 96078.44 | 84.333 | 0.1013 | 29.3966 |
| | | Lower Containment | 55642.69 | 84.711 | 0.0987 | 29.3999 |
| | | Ice Condenser | 25568.34 | 28.859 | 0.0185 | 29.4007 |
| | | TOTAL | 177289.46 | | | |
| 68 | 09:12:28 | Upper Containment | 96075.74 | 84.312 | 0.1009 | 29.3943 |
| | | Lower Containment | 55639.84 | 84.708 | 0.0981 | 29.3976 |
| | | Ice Condenser | 25570.15 | 28.786 | 0.0185 | 29.3984 |
| | | TOTAL | 177285.72 | | | |
| 69 | 09:22:28 | Upper Containment | 96073.40 | 84.302 | 0.1003 | 29.3923 |
| | | Lower Containment | 55637.83 | 84.700 | 0.0976 | 29.3956 |
| | | Ice Condenser | 25572.54 | 28.709 | 0.0185 | 29.3966 |
| | | TOTAL | 177283.77 | | | |
| 70 | 09:32:28 | Upper Containment | 96072.89 | 84.253 | 0.1001 | 29.3893 |
| | | Lower Containment | 55633.94 | 84.690 | 0.0973 | 29.3927 |
| | | Ice Condenser | 25567.78 | 28.749 | 0.0185 | 29.3935 |
| | | TOTAL | 177274.61 | | | |
| 71 | 09:42:29 | Upper Containment | 96066.41 | 84.260 | 0.0995 | 29.3872 |
| | | Lower Containment | 55631.64 | 84.681 | 0.0966 | 29.3903 |
| | | Ice Condenser | 25568.18 | 28.705 | 0.0185 | 29.3913 |
| | | TOTAL | 177266.23 | | | |
| 72 | 09:52:29 | Upper Containment | 96066.11 | 84.236 | 0.0992 | 29.3855 |
| | | Lower Containment | 55630.65 | 84.670 | 0.0962 | 29.3888 |
| | | Ice Condenser | 25569.18 | 28.658 | 0.0185 | 29.3896 |
| | | TOTAL | 177265.94 | | | |
| 73 | 10:02:29 | Upper Containment | 96065.13 | 84.222 | 0.0988 | 29.3840 |
| | | Lower Containment | 55627.44 | 84.684 | 0.0956 | 29.3873 |
| | | Ice Condenser | 25567.80 | 28.659 | 0.0185 | 29.3881 |
| | | TOTAL | 177260.38 | | | |
| 74 | 10:12:30 | Upper Containment | 96066.12 | 84.198 | 0.0984 | 29.3826 |
| | | Lower Containment | 55628.00 | 84.660 | 0.0952 | 29.3859 |
| | | Ice Condenser | 25567.22 | 28.647 | 0.0185 | 29.3867 |
| | | TOTAL | 177261.33 | | | |
| 75 | 10:22:30 | Upper Containment | 96058.00 | 84.223 | 0.0980 | 29.3811 |
| | | Lower Containment | 55628.10 | 84.640 | 0.0947 | 29.3844 |
| | | Ice Condenser | 25567.53 | 28.616 | 0.0185 | 29.3852 |
| | | TOTAL | 177253.63 | | | |
| 76 | 10:32:30 | Upper Containment | 96062.23 | 84.177 | 0.0974 | 29.3794 |
| | | Lower Containment | 55625.36 | 84.649 | 0.0944 | 29.3831 |
| | | Ice Condenser | 25572.82 | 28.487 | 0.0185 | 29.3835 |
| | | TOTAL | 177260.42 | | | |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|--------------------|-------------|-------------|--------------------|--------------|
| 77 | 10:42:31 | Upper Containment | 96059.22 | 84.174 | 0.0971 | 29.3780 |
| | | Lower Containment | 55624.75 | 84.640 | 0.0938 | 29.3817 |
| | | Ice Condenser | 25575.94 | 28.406 | 0.0185 | 29.3822 |
| | | TOTAL | 177259.91 | | | |
| 78 | 10:52:31 | Upper Containment | 96057.67 | 84.153 | 0.0968 | 29.3760 |
| | | Lower Containment | 55620.88 | 84.639 | 0.0934 | 29.3792 |
| | | Ice Condenser | 25578.06 | 28.332 | 0.0185 | 29.3802 |
| | | TOTAL | 177256.62 | | | |
| 79 | 11:02:31 | Upper Containment | 96056.10 | 84.151 | 0.0964 | 29.3750 |
| | | Lower Containment | 55620.64 | 84.630 | 0.0930 | 29.3782 |
| | | Ice Condenser | 25578.67 | 28.302 | 0.0185 | 29.3791 |
| | | TOTAL | 177255.40 | | | |
| 80 | 11:12:32 | Upper Containment | 96053.95 | 84.148 | 0.0960 | 29.3739 |
| | | Lower Containment | 55621.26 | 84.614 | 0.0926 | 29.3773 |
| | | Ice Condenser | 25577.94 | 28.297 | 0.0185 | 29.3780 |
| | | TOTAL | 177253.14 | | | |
| 81 | 11:22:32 | Upper Containment | 96056.86 | 84.112 | 0.0957 | 29.3725 |
| | | Lower Containment | 55620.29 | 84.612 | 0.0922 | 29.3763 |
| | | Ice Condenser | 25578.69 | 28.262 | 0.0185 | 29.3767 |
| | | TOTAL | 177255.84 | | | |
| 82 | 11:32:32 | Upper Containment | 96056.08 | 84.097 | 0.0952 | 29.3709 |
| | | Lower Containment | 55618.87 | 84.605 | 0.0918 | 29.3747 |
| | | Ice Condenser | 25579.33 | 28.221 | 0.0185 | 29.3750 |
| | | TOTAL | 177254.28 | | | |
| 83 | 11:42:33 | Upper Containment | 96054.85 | 84.086 | 0.0950 | 29.3698 |
| | | Lower Containment | 55618.82 | 84.590 | 0.0912 | 29.3732 |
| | | Ice Condenser | 25578.04 | 28.230 | 0.0185 | 29.3740 |
| | | TOTAL | 177251.71 | | | |
| 84 | 11:52:33 | Upper Containment | 96062.86 | 84.042 | 0.0944 | 29.3693 |
| | | Lower Containment | 55618.35 | 84.587 | 0.0910 | 29.3727 |
| | | Ice Condenser | 25576.85 | 28.245 | 0.0185 | 29.3736 |
| | | TOTAL | 177258.06 | | | |
| 85 | 12:02:33 | Upper Containment | 96059.90 | 84.061 | 0.0942 | 29.3692 |
| | | Lower Containment | 55619.75 | 84.581 | 0.0905 | 29.3726 |
| | | Ice Condenser | 25575.60 | 28.267 | 0.0185 | 29.3735 |
| | | TOTAL | 177255.24 | | | |
| 86 | 12:12:34 | Upper Containment | 96059.21 | 84.031 | 0.0942 | 29.3674 |
| | | Lower Containment | 55619.40 | 84.567 | 0.0900 | 29.3711 |
| | | Ice Condenser | 25573.50 | 28.274 | 0.0185 | 29.3715 |
| | | TOTAL | 177252.11 | | | |
| 87 | 12:22:34 | Upper Containment | 96060.01 | 84.039 | 0.0937 | 29.3675 |
| | | Lower Containment | 55620.44 | 84.557 | 0.0899 | 29.3710 |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|--------------------|-------------|-------------|--------------------|--------------|
| | | Ice Condenser | 25576.36 | 28.223 | 0.0185 | 29.3717 |
| | | TOTAL | 177256.81 | | | |
| 88 | 12:32:34 | Upper Containment | 96062.96 | 84.030 | 0.0933 | 29.3676 |
| | | Lower Containment | 55620.49 | 84.561 | 0.0895 | 29.3709 |
| | | Ice Condenser | 25574.05 | 28.271 | 0.0185 | 29.3720 |
| | | TOTAL | 177257.50 | | | |
| 89 | 12:42:35 | Upper Containment | 96069.79 | 84.016 | 0.0931 | 29.3687 |
| | | Lower Containment | 55623.32 | 84.553 | 0.0891 | 29.3716 |
| | | Ice Condenser | 25570.54 | 28.354 | 0.0185 | 29.3729 |
| | | TOTAL | 177263.66 | | | |
| 90 | 12:52:35 | Upper Containment | 96062.16 | 84.030 | 0.0929 | 29.3669 |
| | | Lower Containment | 55623.39 | 84.536 | 0.0887 | 29.3703 |
| | | Ice Condenser | 25561.93 | 28.487 | 0.0185 | 29.3710 |
| | | TOTAL | 177247.48 | | | |
| 91 | 13:02:35 | Upper Containment | 96065.44 | 84.024 | 0.0924 | 29.3671 |
| | | Lower Containment | 55625.15 | 84.533 | 0.0885 | 29.3709 |
| | | Ice Condenser | 25563.23 | 28.471 | 0.0185 | 29.3715 |
| | | TOTAL | 177253.82 | | | |
| 92 | 13:12:36 | Upper Containment | 96073.47 | 83.989 | 0.0922 | 29.3674 |
| | | Lower Containment | 55627.31 | 84.524 | 0.0882 | 29.3712 |
| | | Ice Condenser | 25560.72 | 28.518 | 0.0185 | 29.3715 |
| | | TOTAL | 177261.50 | | | |
| 93 | 13:22:36 | Upper Containment | 96070.98 | 83.986 | 0.0919 | 29.3662 |
| | | Lower Containment | 55625.08 | 84.523 | 0.0880 | 29.3698 |
| | | Ice Condenser | 25558.91 | 28.536 | 0.0185 | 29.3705 |
| | | TOTAL | 177254.97 | | | |
| 94 | 13:32:36 | Upper Containment | 96075.83 | 83.962 | 0.0914 | 29.3660 |
| | | Lower Containment | 55626.04 | 84.510 | 0.0876 | 29.3691 |
| | | Ice Condenser | 25558.27 | 28.536 | 0.0185 | 29.3698 |
| | | TOTAL | 177260.14 | | | |
| 95 | 13:42:37 | Upper Containment | 96071.22 | 83.950 | 0.0912 | 29.3637 |
| | | Lower Containment | 55623.97 | 84.494 | 0.0874 | 29.3670 |
| | | Ice Condenser | 25560.50 | 28.459 | 0.0185 | 29.3677 |
| | | TOTAL | 177255.70 | | | |
| 96 | 13:52:37 | Upper Containment | 96069.15 | 83.962 | 0.0910 | 29.3634 |
| | | Lower Containment | 55624.93 | 84.495 | 0.0870 | 29.3672 |
| | | Ice Condenser | 25564.00 | 28.393 | 0.0185 | 29.3678 |
| | | TOTAL | 177258.08 | | | |
| 97 | 14:02:37 | Upper Containment | 96077.52 | 83.914 | 0.0907 | 29.3632 |
| | | Lower Containment | 55623.54 | 84.495 | 0.0868 | 29.3663 |
| | | Ice Condenser | 25563.86 | 28.389 | 0.0185 | 29.3674 |
| | | TOTAL | 177264.92 | | | |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|---------------------|-------------|-------------|--------------------|--------------|
| 98 | 14:12:38 | Upper Containment | 96072.59 | 83.925 | 0.0904 | 29.3619 |
| | | Lower Containment | 55624.60 | 84.476 | 0.0866 | 29.3656 |
| | | Ice Condenser | 25568.17 | 28.286 | 0.0185 | 29.3661 |
| | | TOTAL | 177265.36 | | | |
| 99 | 14:22:38 | Upper Containment | 96070.54 | 83.914 | 0.0901 | 29.3604 |
| | | Lower Containment | 55621.90 | 84.478 | 0.0864 | 29.3641 |
| | | Ice Condenser | 25564.72 | 28.327 | 0.0185 | 29.3646 |
| | | TOTAL | 177257.15 | | | |
| 100 | 14:32:38 | 0 Upper Containment | 96070.24 | 83.887 | 0.0898 | 29.3586 |
| | | Lower Containment | 55622.13 | 84.453 | 0.0859 | 29.3624 |
| | | Ice Condenser | 25566.48 | 28.263 | 0.0185 | 29.3628 |
| | | TOTAL | 177258.85 | | | |
| 101 | 14:42:39 | 1 Upper Containment | 96065.09 | 83.899 | 0.0896 | 29.3575 |
| | | Lower Containment | 55617.91 | 84.464 | 0.0858 | 29.3606 |
| | | Ice Condenser | 25565.16 | 28.269 | 0.0185 | 29.3616 |
| | | TOTAL | 177248.16 | | | |
| 102 | 14:52:39 | 2 Upper Containment | 96064.39 | 83.882 | 0.0895 | 29.3563 |
| | | Lower Containment | 55616.92 | 84.452 | 0.0856 | 29.3592 |
| | | Ice Condenser | 25567.65 | 28.201 | 0.0185 | 29.3604 |
| | | TOTAL | 177248.96 | | | |
| 103 | 15:02:39 | 3 Upper Containment | 96067.22 | 83.859 | 0.0892 | 29.3555 |
| | | Lower Containment | 55618.48 | 84.437 | 0.0854 | 29.3591 |
| | | Ice Condenser | 25571.90 | 28.106 | 0.0185 | 29.3595 |
| | | TOTAL | 177257.60 | | | |
| 104 | 15:12:40 | 4 Upper Containment | 96061.45 | 83.869 | 0.0889 | 29.3541 |
| | | Lower Containment | 55617.88 | 84.431 | 0.0850 | 29.3581 |
| | | Ice Condenser | 25576.13 | 28.003 | 0.0185 | 29.3582 |
| | | TOTAL | 177255.46 | | | |
| 105 | 15:22:40 | 5 Upper Containment | 96067.70 | 83.814 | 0.0886 | 29.3527 |
| | | Lower Containment | 55614.15 | 84.433 | 0.0847 | 29.3559 |
| | | Ice Condenser | 25576.76 | 27.970 | 0.0185 | 29.3570 |
| | | TOTAL | 177258.60 | | | |
| 106 | 15:32:40 | 6 Upper Containment | 96063.49 | 83.819 | 0.0883 | 29.3513 |
| | | Lower Containment | 55613.28 | 84.422 | 0.0844 | 29.3545 |
| | | Ice Condenser | 25579.20 | 27.899 | 0.0185 | 29.3555 |
| | | TOTAL | 177255.97 | | | |
| 107 | 15:42:41 | 7 Upper Containment | 96063.69 | 83.814 | 0.0880 | 29.3509 |
| | | Lower Containment | 55613.71 | 84.415 | 0.0841 | 29.3540 |
| | | Ice Condenser | 25577.93 | 27.914 | 0.0185 | 29.3549 |
| | | TOTAL | 177255.34 | | | |
| 108 | 15:52:41 | 8 Upper Containment | 96068.36 | 83.775 | 0.0879 | 29.3500 |
| | | Lower Containment | 55614.25 | 84.404 | 0.0839 | 29.3536 |
| | | Ice Condenser | 25570.07 | 28.054 | 0.0185 | 29.3543 |
| | | | | | | |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|----------------------------|-------------|-------------|--------------------|--------------|
| | | TOTAL | 177252.68 | | | |
| 109 | 16:02:41 | 9 Upper Containment | 96070.92 | 83.778 | 0.0877 | 29.3508 |
| | | Lower Containment | 55616.74 | 84.395 | 0.0838 | 29.3543 |
| | | Ice Condenser | 25561.78 | 28.225 | 0.0185 | 29.3551 |
| | | TOTAL | 177249.45 | | | |
| 110 | 16:12:42 | 0 Upper Containment | 96071.12 | 83.785 | 0.0876 | 29.3512 |
| | | Lower Containment | 55618.70 | 84.395 | 0.0835 | 29.3550 |
| | | Ice Condenser | 25556.43 | 28.334 | 0.0185 | 29.3555 |
| | | TOTAL | 177246.25 | | | |
| 111 | 16:22:42 | 1 Upper Containment | 96072.76 | 83.782 | 0.0873 | 29.3512 |
| | | Lower Containment | 55617.92 | 84.395 | 0.0833 | 29.3544 |
| | | Ice Condenser | 25553.97 | 28.377 | 0.0185 | 29.3553 |
| | | TOTAL | 177244.65 | | | |
| 112 | 16:32:42 | 2 Upper Containment | 96078.75 | 83.735 | 0.0869 | 29.3501 |
| | | Lower Containment | 55618.49 | 84.380 | 0.0829 | 29.3535 |
| | | Ice Condenser | 25556.28 | 28.314 | 0.0185 | 29.3541 |
| | | TOTAL | 177253.52 | | | |
| 113 | 16:42:43 | 3 Upper Containment | 96072.85 | 83.752 | 0.0866 | 29.3489 |
| | | Lower Containment | 55615.95 | 84.383 | 0.0828 | 29.3522 |
| | | Ice Condenser | 25560.38 | 28.220 | 0.0185 | 29.3532 |
| | | TOTAL | 177249.17 | | | |
| 114 | 16:52:43 | 4 Upper Containment | 96071.78 | 83.745 | 0.0864 | 29.3480 |
| | | Lower Containment | 55615.07 | 84.371 | 0.0827 | 29.3510 |
| | | Ice Condenser | 25561.37 | 28.182 | 0.0185 | 29.3520 |
| | | TOTAL | 177248.22 | | | |
| 115 | 17:02:43 | 5 Upper Containment | 96073.18 | 83.738 | 0.0862 | 29.3479 |
| | | Lower Containment | 55616.85 | 84.369 | 0.0823 | 29.3514 |
| | | Ice Condenser | 25567.41 | 28.067 | 0.0185 | 29.3521 |
| | | TOTAL | 177257.44 | | | |
| 116 | 17:12:44 | 6 Upper Containment | 96073.61 | 83.720 | 0.0859 | 29.3468 |
| | | Lower Containment | 55616.52 | 84.352 | 0.0820 | 29.3501 |
| | | Ice Condenser | 25569.62 | 28.009 | 0.0185 | 29.3511 |
| | | TOTAL | 177259.75 | | | |
| 117 | 17:22:44 | 7 Upper Containment | 96077.25 | 83.688 | 0.0856 | 29.3458 |
| | | Lower Containment | 55615.46 | 84.347 | 0.0819 | 29.3492 |
| | | Ice Condenser | 25572.30 | 27.937 | 0.0185 | 29.3498 |
| | | TOTAL | 177265.01 | | | |
| 118 | 17:32:44 | 8 Upper Containment | 96076.60 | 83.673 | 0.0853 | 29.3445 |
| | | Lower Containment | 55615.17 | 84.334 | 0.0819 | 29.3483 |
| | | Ice Condenser | 25577.00 | 27.830 | 0.0185 | 29.3488 |
| | | TOTAL | 177268.77 | | | |
| 119 | 17:42:45 | 9 Upper Containment | 96072.78 | 83.683 | 0.0851 | 29.3437 |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|----------------------------|------------------|-------------|--------------------|--------------|
| | | Lower Containment | 55614.40 | 84.329 | 0.0817 | 29.3474 |
| | | Ice Condenser | 25576.07 | 27.832 | 0.0185 | 29.3479 |
| | | TOTAL | 177263.25 | | | |
| 120 | 17:52:45 | 0 Upper Containment | 96078.12 | 83.656 | 0.0851 | 29.3438 |
| | | Lower Containment | 55613.99 | 84.333 | 0.0814 | 29.3471 |
| | | Ice Condenser | 25577.08 | 27.814 | 0.0185 | 29.3479 |
| | | TOTAL | 177269.18 | | | |
| 121 | 18:02:45 | 1 Upper Containment | 96078.60 | 83.658 | 0.0848 | 29.3438 |
| | | Lower Containment | 55616.03 | 84.322 | 0.0810 | 29.3472 |
| | | Ice Condenser | 25574.66 | 27.864 | 0.0185 | 29.3482 |
| | | TOTAL | 177269.28 | | | |
| 122 | 18:12:46 | 2 Upper Containment | 96077.46 | 83.640 | 0.0845 | 29.3421 |
| | | Lower Containment | 55613.62 | 84.319 | 0.0809 | 29.3456 |
| | | Ice Condenser | 25574.81 | 27.832 | 0.0185 | 29.3464 |
| | | TOTAL | 177265.88 | | | |
| 123 | 18:22:46 | 3 Upper Containment | 96077.34 | 83.640 | 0.0844 | 29.3421 |
| | | Lower Containment | 55615.43 | 84.302 | 0.0807 | 29.3455 |
| | | Ice Condenser | 25584.59 | 27.643 | 0.0185 | 29.3463 |
| | | TOTAL | 177277.37 | | | |
| 124 | 18:32:46 | 4 Upper Containment | 96077.55 | 83.640 | 0.0840 | 29.3417 |
| | | Lower Containment | 55615.18 | 84.303 | 0.0803 | 29.3451 |
| | | Ice Condenser | 25583.67 | 27.654 | 0.0185 | 29.3459 |
| | | TOTAL | 177276.40 | | | |
| 125 | 18:42:47 | 5 Upper Containment | 96080.04 | 83.638 | 0.0839 | 29.3422 |
| | | Lower Containment | 55617.16 | 84.294 | 0.0802 | 29.3455 |
| | | Ice Condenser | 25578.69 | 27.758 | 0.0185 | 29.3464 |
| | | TOTAL | 177275.89 | | | |
| 126 | 18:52:47 | 6 Upper Containment | 96073.38 | 83.636 | 0.0836 | 29.3398 |
| | | Lower Containment | 55614.43 | 84.282 | 0.0801 | 29.3433 |
| | | Ice Condenser | 25577.15 | 27.746 | 0.0185 | 29.3439 |
| | | TOTAL | 177264.96 | | | |
| 127 | 19:02:47 | 7 Upper Containment | 96080.87 | 83.610 | 0.0834 | 29.3405 |
| | | Lower Containment | 55616.23 | 84.284 | 0.0800 | 29.3442 |
| | | Ice Condenser | 25574.36 | 27.810 | 0.0185 | 29.3446 |
| | | TOTAL | 177271.45 | | | |
| 128 | 19:12:48 | 8 Upper Containment | 96088.02 | 83.593 | 0.0833 | 29.3416 |
| | | Lower Containment | 55619.17 | 84.274 | 0.0797 | 29.3450 |
| | | Ice Condenser | 25568.50 | 27.943 | 0.0185 | 29.3458 |
| | | TOTAL | 177275.69 | | | |
| 129 | 19:22:48 | 9 Upper Containment | 96095.83 | 83.576 | 0.0830 | 29.3428 |
| | | Lower Containment | 55621.49 | 84.270 | 0.0796 | 29.3458 |
| | | Ice Condenser | 25566.05 | 28.008 | 0.0185 | 29.3469 |
| | | TOTAL | 177283.37 | | | |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|---------------------|-------------|-------------|--------------------|--------------|
| 130 | 19:32:48 | 0 Upper Containment | 96091.10 | 83.613 | 0.0828 | 29.3432 |
| | | Lower Containment | 55623.45 | 84.267 | 0.0793 | 29.3464 |
| | | Ice Condenser | 25558.59 | 28.160 | 0.0185 | 29.3475 |
| | | TOTAL | 177273.13 | | | |
| 131 | 19:42:49 | 1 Upper Containment | 96097.04 | 83.585 | 0.0826 | 29.3432 |
| | | Lower Containment | 55625.19 | 84.256 | 0.0792 | 29.3466 |
| | | Ice Condenser | 25552.21 | 28.280 | 0.0185 | 29.3474 |
| | | TOTAL | 177274.44 | | | |
| 132 | 19:57:36 | 2 Upper Containment | 96107.32 | 83.572 | 0.0824 | 29.3455 |
| | | Lower Containment | 55630.55 | 84.250 | 0.0789 | 29.3489 |
| | | Ice Condenser | 25553.86 | 28.289 | 0.0185 | 29.3499 |
| | | TOTAL | 177291.73 | | | |
| 133 | 20:07:54 | 3 Upper Containment | 96114.43 | 83.568 | 0.0821 | 29.3472 |
| | | Lower Containment | 55635.55 | 84.236 | 0.0786 | 29.3505 |
| | | Ice Condenser | 25551.38 | 28.363 | 0.0185 | 29.3515 |
| | | TOTAL | 177301.37 | | | |
| 134 | 20:17:55 | 4 Upper Containment | 96111.26 | 83.581 | 0.0818 | 29.3466 |
| | | Lower Containment | 55633.77 | 84.246 | 0.0786 | 29.3500 |
| | | Ice Condenser | 25544.32 | 28.489 | 0.0185 | 29.3509 |
| | | TOTAL | 177289.35 | | | |
| 135 | 20:27:55 | 5 Upper Containment | 96115.16 | 83.560 | 0.0818 | 29.3467 |
| | | Lower Containment | 55635.88 | 84.230 | 0.0784 | 29.3501 |
| | | Ice Condenser | 25540.30 | 28.564 | 0.0185 | 29.3508 |
| | | TOTAL | 177291.34 | | | |
| 136 | 20:37:55 | 6 Upper Containment | 96118.12 | 83.543 | 0.0817 | 29.3465 |
| | | Lower Containment | 55636.21 | 84.226 | 0.0784 | 29.3500 |
| | | Ice Condenser | 25536.30 | 28.641 | 0.0185 | 29.3508 |
| | | TOTAL | 177290.62 | | | |
| 137 | 20:47:56 | 7 Upper Containment | 96115.70 | 83.560 | 0.0817 | 29.3467 |
| | | Lower Containment | 55638.18 | 84.213 | 0.0782 | 29.3501 |
| | | Ice Condenser | 25532.85 | 28.712 | 0.0185 | 29.3511 |
| | | TOTAL | 177286.73 | | | |
| 138 | 20:57:56 | 6 Upper Containment | 96123.42 | 83.533 | 0.0812 | 29.3471 |
| | | Lower Containment | 55638.59 | 84.217 | 0.0781 | 29.3505 |
| | | Ice Condenser | 25534.75 | 28.681 | 0.0185 | 29.3515 |
| | | TOTAL | 177296.77 | | | |
| 139 | 21:07:56 | 9 Upper Containment | 96120.62 | 83.545 | 0.0813 | 29.3470 |
| | | Lower Containment | 55640.48 | 84.203 | 0.0778 | 29.3505 |
| | | Ice Condenser | 25532.97 | 28.714 | 0.0185 | 29.3514 |
| | | TOTAL | 177294.07 | | | |
| 140 | 21:17:57 | 0 Upper Containment | 96125.00 | 83.515 | 0.0811 | 29.3465 |
| | | Lower Containment | 55640.39 | 84.198 | 0.0778 | 29.3502 |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|----------------------------|-------------|-------------|--------------------|--------------|
| | | Ice Condenser | 25532.84 | 28.708 | 0.0185 | 29.3509 |
| | | TOTAL | 177298.24 | | | |
| 141 | 21:27:57 | 1 Upper Containment | 96118.35 | 83.526 | 0.0808 | 29.3448 |
| | | Lower Containment | 55638.05 | 84.188 | 0.0777 | 29.3483 |
| | | Ice Condenser | 25532.96 | 28.674 | 0.0185 | 29.3490 |
| | | TOTAL | 177289.35 | | | |
| 142 | 21:37:57 | 2 Upper Containment | 96115.82 | 83.505 | 0.0805 | 29.3426 |
| | | Lower Containment | 55634.84 | 84.180 | 0.0776 | 29.3461 |
| | | Ice Condenser | 25536.84 | 28.566 | 0.0185 | 29.3469 |
| | | TOTAL | 177287.49 | | | |
| 143 | 21:47:58 | 3 Upper Containment | 96111.75 | 83.493 | 0.0806 | 29.3408 |
| | | Lower Containment | 55631.21 | 84.184 | 0.0776 | 29.3443 |
| | | Ice Condenser | 25542.09 | 28.436 | 0.0185 | 29.3452 |
| | | TOTAL | 177285.06 | | | |
| 144 | 21:57:58 | 4 Upper Containment | 96105.17 | 83.510 | 0.0804 | 29.3396 |
| | | Lower Containment | 55631.00 | 84.169 | 0.0773 | 29.3432 |
| | | Ice Condenser | 25541.86 | 28.420 | 0.0185 | 29.3439 |
| | | TOTAL | 177278.03 | | | |
| 145 | 22:07:58 | 5 Upper Containment | 96112.368 | 83.4560 | 0.08012 | 29.3385 |
| | | Lower Containment | 55630.21 | 84.167 | 0.0773 | 29.3426 |
| | | Ice Condenser | 25541.74 | 28.404 | 0.0185 | 29.3429 |
| | | TOTAL | 177284.32 | | | |
| 146 | 22:17:59 | 6 Upper Containment | 96112.47 | 83.440 | 0.0799 | 29.3375 |
| | | Lower Containment | 55627.90 | 84.166 | 0.0770 | 29.3410 |
| | | Ice Condenser | 25542.62 | 28.366 | 0.0185 | 29.3416 |
| | | TOTAL | 177282.99 | | | |
| 147 | 22:27:59 | 7 Upper Containment | 96104.24 | 83.449 | 0.0798 | 29.3353 |
| | | Lower Containment | 55624.73 | 84.157 | 0.0769 | 29.3388 |
| | | Ice Condenser | 25548.99 | 28.211 | 0.0185 | 29.3396 |
| | | TOTAL | 177277.95 | | | |
| 148 | 22:37:59 | 8 Upper Containment | 96100.57 | 83.446 | 0.0798 | 29.3340 |
| | | Lower Containment | 55622.76 | 84.155 | 0.0768 | 29.3375 |
| | | Ice Condenser | 25553.82 | 28.100 | 0.0185 | 29.3385 |
| | | TOTAL | 177277.15 | | | |
| 149 | 22:48:00 | 9 Upper Containment | 96099.44 | 83.439 | 0.0794 | 29.3330 |
| | | Lower Containment | 55622.89 | 84.139 | 0.0766 | 29.3365 |
| | | Ice Condenser | 25557.29 | 28.017 | 0.0185 | 29.3374 |
| | | TOTAL | 177279.62 | | | |
| 150 | 22:58:00 | 0 Upper Containment | 96099.87 | 83.417 | 0.0794 | 29.3319 |
| | | Lower Containment | 55621.04 | 84.141 | 0.0765 | 29.3356 |
| | | Ice Condenser | 25560.76 | 27.933 | 0.0185 | 29.3364 |
| | | TOTAL | 177281.67 | | | |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|---------------------|-------------|-------------|--------------------|--------------|
| 151 | 23:08:00 | 1 Upper Containment | 96098.72 | 83.411 | 0.0791 | 29.3309 |
| | | Lower Containment | 55619.73 | 84.135 | 0.0762 | 29.3343 |
| | | Ice Condenser | 25564.11 | 27.851 | 0.0185 | 29.3353 |
| | | TOTAL | 177282.56 | | | |
| 152 | 23:18:01 | 2 Upper Containment | 96092.30 | 83.434 | 0.0790 | 29.3301 |
| | | Lower Containment | 55619.09 | 84.129 | 0.0762 | 29.3336 |
| | | Ice Condenser | 25564.99 | 27.820 | 0.0185 | 29.3344 |
| | | TOTAL | 177276.38 | | | |
| 153 | 23:28:01 | 3 Upper Containment | 96100.22 | 83.378 | 0.0789 | 29.3293 |
| | | Lower Containment | 55619.87 | 84.120 | 0.0761 | 29.3334 |
| | | Ice Condenser | 25567.98 | 27.750 | 0.0185 | 29.3336 |
| | | TOTAL | 177288.07 | | | |
| 154 | 23:38:01 | 4 Upper Containment | 96098.66 | 83.380 | 0.0789 | 29.3290 |
| | | Lower Containment | 55619.81 | 84.117 | 0.0758 | 29.3330 |
| | | Ice Condenser | 25568.72 | 27.728 | 0.0185 | 29.3332 |
| | | TOTAL | 177287.19 | | | |
| 155 | 23:48:02 | 5 Upper Containment | 96089.78 | 83.398 | 0.0788 | 29.3271 |
| | | Lower Containment | 55616.21 | 84.113 | 0.0758 | 29.3308 |
| | | Ice Condenser | 25568.50 | 27.706 | 0.0185 | 29.3316 |
| | | TOTAL | 177274.50 | | | |
| 156 | 23:58:02 | 6 Upper Containment | 96092.46 | 83.409 | 0.0784 | 29.3283 |
| | | Lower Containment | 55618.99 | 84.110 | 0.0754 | 29.3318 |
| | | Ice Condenser | 25566.77 | 27.757 | 0.0185 | 29.3327 |
| | | TOTAL | 177278.22 | | | |
| 157 | 00:08:02 | 7 Upper Containment | 96096.34 | 83.378 | 0.0784 | 29.3277 |
| | | Lower Containment | 55618.38 | 84.104 | 0.0755 | 29.3312 |
| | | Ice Condenser | 25566.91 | 27.745 | 0.0185 | 29.3321 |
| | | TOTAL | 177281.62 | | | |
| 158 | 00:18:03 | 8 Upper Containment | 96099.38 | 83.378 | 0.0783 | 29.3285 |
| | | Lower Containment | 55620.70 | 84.103 | 0.0753 | 29.3321 |
| | | Ice Condenser | 25573.47 | 27.634 | 0.0185 | 29.3330 |
| | | TOTAL | 177293.55 | | | |
| 159 | 00:28:03 | 9 Upper Containment | 96097.40 | 83.365 | 0.0782 | 29.3271 |
| | | Lower Containment | 55619.97 | 84.083 | 0.0751 | 29.3305 |
| | | Ice Condenser | 25571.48 | 27.647 | 0.0185 | 29.3315 |
| | | TOTAL | 177288.85 | | | |
| 160 | 00:38:03 | 0 Upper Containment | 96097.98 | 83.364 | 0.0778 | 29.3268 |
| | | Lower Containment | 55620.39 | 84.085 | 0.0749 | 29.3306 |
| | | Ice Condenser | 25568.32 | 27.703 | 0.0185 | 29.3312 |
| | | TOTAL | 177286.69 | | | |
| 161 | 00:48:04 | 1 Upper Containment | 96094.84 | 83.366 | 0.0779 | 29.3261 |
| | | Lower Containment | 55619.28 | 84.079 | 0.0747 | 29.3295 |
| | | Ice Condenser | 25570.93 | 27.633 | 0.0185 | 29.3300 |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|----------------------------|-------------|-------------|--------------------|--------------|
| | | TOTAL | 177285.05 | | | |
| 162 | 00:58:04 | 2 Upper Containment | 96088.14 | 83.348 | 0.0777 | 29.3229 |
| | | Lower Containment | 55614.49 | 84.067 | 0.0746 | 29.3263 |
| | | Ice Condenser | 25572.05 | 27.562 | 0.0185 | 29.3270 |
| | | TOTAL | 177274.68 | | | |
| 163 | 01:08:04 | 3 Upper Containment | 96091.81 | 83.335 | 0.0772 | 29.3229 |
| | | Lower Containment | 55615.81 | 84.067 | 0.0744 | 29.3267 |
| | | Ice Condenser | 25572.59 | 27.554 | 0.0185 | 29.3271 |
| | | TOTAL | 177280.22 | | | |
| 164 | 01:18:05 | 4 Upper Containment | 96089.21 | 83.331 | 0.0772 | 29.3218 |
| | | Lower Containment | 55614.13 | 84.059 | 0.0743 | 29.3253 |
| | | Ice Condenser | 25574.53 | 27.499 | 0.0185 | 29.3260 |
| | | TOTAL | 177277.86 | | | |
| 165 | 01:28:05 | 5 Upper Containment | 96088.82 | 83.323 | 0.0771 | 29.3211 |
| | | Lower Containment | 55614.35 | 84.044 | 0.0741 | 29.3244 |
| | | Ice Condenser | 25577.20 | 27.437 | 0.0185 | 29.3254 |
| | | TOTAL | 177280.36 | | | |
| 166 | 01:38:05 | 6 Upper Containment | 96080.78 | 83.311 | 0.0770 | 29.3180 |
| | | Lower Containment | 55610.84 | 84.035 | 0.0739 | 29.3220 |
| | | Ice Condenser | 25575.43 | 27.422 | 0.0185 | 29.3225 |
| | | TOTAL | 177267.05 | | | |
| 167 | 01:48:06 | 7 Upper Containment | 96077.68 | 83.347 | 0.0769 | 29.3189 |
| | | Lower Containment | 55612.40 | 84.036 | 0.0738 | 29.3227 |
| | | Ice Condenser | 25582.42 | 27.299 | 0.0185 | 29.3231 |
| | | TOTAL | 177272.50 | | | |
| 168 | 01:58:06 | 8 Upper Containment | 96082.07 | 83.342 | 0.0766 | 29.3196 |
| | | Lower Containment | 55613.78 | 84.041 | 0.0736 | 29.3235 |
| | | Ice Condenser | 25588.03 | 27.206 | 0.0185 | 29.3239 |
| | | TOTAL | 177283.88 | | | |
| 169 | 02:08:06 | 9 Upper Containment | 96090.38 | 83.310 | 0.0766 | 29.3204 |
| | | Lower Containment | 55616.20 | 84.028 | 0.0734 | 29.3239 |
| | | Ice Condenser | 25589.35 | 27.196 | 0.0185 | 29.3248 |
| | | TOTAL | 177295.93 | | | |
| 170 | 02:18:07 | 0 Upper Containment | 96079.50 | 83.328 | 0.0765 | 29.3179 |
| | | Lower Containment | 55613.54 | 84.013 | 0.0733 | 29.3216 |
| | | Ice Condenser | 25587.73 | 27.185 | 0.0185 | 29.3223 |
| | | TOTAL | 177280.77 | | | |
| 171 | 02:28:07 | 1 Upper Containment | 96077.64 | 83.310 | 0.0762 | 29.3162 |
| | | Lower Containment | 55610.81 | 84.013 | 0.0731 | 29.3200 |
| | | Ice Condenser | 25585.63 | 27.192 | 0.0185 | 29.3203 |
| | | TOTAL | 177274.07 | | | |
| 172 | 02:38:07 | 2 Upper Containment | 96072.01 | 83.323 | 0.0760 | 29.3149 |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|----------------------------|-------------|-------------|--------------------|--------------|
| | | Lower Containment | 55610.35 | 83.999 | 0.0730 | 29.3188 |
| | | Ice Condenser | 25589.00 | 27.111 | 0.0185 | 29.3193 |
| | | TOTAL | 177271.36 | | | |
| 173 | 02:48:08 | 3 Upper Containment | 96077.70 | 83.279 | 0.0759 | 29.3142 |
| | | Lower Containment | 55607.77 | 84.005 | 0.0729 | 29.3177 |
| | | Ice Condenser | 25591.58 | 27.047 | 0.0185 | 29.3184 |
| | | TOTAL | 177277.06 | | | |
| 174 | 02:58:08 | 4 Upper Containment | 96073.17 | 83.290 | 0.0757 | 29.3132 |
| | | Lower Containment | 55607.89 | 83.991 | 0.0726 | 29.3167 |
| | | Ice Condenser | 25595.48 | 26.959 | 0.0185 | 29.3175 |
| | | TOTAL | 177276.54 | | | |
| 175 | 03:08:09 | 5 Upper Containment | 96073.10 | 83.259 | 0.0755 | 29.3114 |
| | | Lower Containment | 55605.23 | 83.981 | 0.0725 | 29.3147 |
| | | Ice Condenser | 25594.85 | 26.939 | 0.0185 | 29.3156 |
| | | TOTAL | 177273.18 | | | |
| 176 | 03:18:09 | 6 Upper Containment | 96072.90 | 83.247 | 0.0753 | 29.3104 |
| | | Lower Containment | 55603.16 | 83.982 | 0.0724 | 29.3135 |
| | | Ice Condenser | 25596.36 | 26.892 | 0.0185 | 29.3145 |
| | | TOTAL | 177272.42 | | | |
| 177 | 03:28:09 | 7 Upper Containment | 96070.87 | 83.223 | 0.0753 | 29.3085 |
| | | Lower Containment | 55601.80 | 83.970 | 0.0722 | 29.3119 |
| | | Ice Condenser | 25595.61 | 26.876 | 0.0185 | 29.3127 |
| | | TOTAL | 177268.27 | | | |
| 178 | 03:38:10 | 8 Upper Containment | 96059.53 | 83.258 | 0.0752 | 29.3069 |
| | | Lower Containment | 55599.21 | 83.963 | 0.0721 | 29.3101 |
| | | Ice Condenser | 25598.31 | 26.798 | 0.0185 | 29.3111 |
| | | TOTAL | 177257.05 | | | |
| 179 | 03:48:10 | 9 Upper Containment | 96060.11 | 83.245 | 0.0749 | 29.3060 |
| | | Lower Containment | 55599.04 | 83.958 | 0.0718 | 29.3095 |
| | | Ice Condenser | 25599.91 | 26.753 | 0.0185 | 29.3102 |
| | | TOTAL | 177259.06 | | | |
| 180 | 03:58:10 | 0 Upper Containment | 96057.88 | 83.238 | 0.0748 | 29.3049 |
| | | Lower Containment | 55597.90 | 83.949 | 0.0717 | 29.3083 |
| | | Ice Condenser | 25596.22 | 26.806 | 0.0185 | 29.3092 |
| | | TOTAL | 177252.00 | | | |
| 181 | 04:08:11 | 1 Upper Containment | 96056.24 | 83.237 | 0.0746 | 29.3042 |
| | | Lower Containment | 55597.73 | 83.945 | 0.0715 | 29.3078 |
| | | Ice Condenser | 25594.37 | 26.830 | 0.0185 | 29.3085 |
| | | TOTAL | 177248.34 | | | |
| 182 | 04:18:11 | 2 Upper Containment | 96056.45 | 83.228 | 0.0746 | 29.3037 |
| | | Lower Containment | 55597.20 | 83.939 | 0.0714 | 29.3071 |
| | | Ice Condenser | 25591.27 | 26.881 | 0.0185 | 29.3080 |
| | | TOTAL | 177244.91 | | | |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|----------------------------|-------------|-------------|--------------------|--------------|
| 183 | 04:28:11 | 3 Upper Containment | 96053.02 | 83.228 | 0.0744 | 29.3024 |
| | | Lower Containment | 55596.45 | 83.931 | 0.0712 | 29.3061 |
| | | Ice Condenser | 25595.01 | 26.789 | 0.0185 | 29.3068 |
| | | TOTAL | 177244.48 | | | |
| 184 | 04:38:12 | 4 Upper Containment | 96056.68 | 83.202 | 0.0741 | 29.3019 |
| | | Lower Containment | 55595.60 | 83.929 | 0.0711 | 29.3055 |
| | | Ice Condenser | 25596.96 | 26.742 | 0.0185 | 29.3062 |
| | | TOTAL | 177249.24 | | | |
| 185 | 04:48:12 | 5 Upper Containment | 96055.25 | 83.212 | 0.0739 | 29.3018 |
| | | Lower Containment | 55596.71 | 83.916 | 0.0709 | 29.3051 |
| | | Ice Condenser | 25597.85 | 26.724 | 0.0185 | 29.3061 |
| | | TOTAL | 177249.81 | | | |
| 186 | 04:58:12 | 6 Upper Containment | 96052.90 | 83.217 | 0.0738 | 29.3013 |
| | | Lower Containment | 55597.04 | 83.906 | 0.0708 | 29.3046 |
| | | Ice Condenser | 25598.74 | 26.699 | 0.0185 | 29.3056 |
| | | TOTAL | 177248.68 | | | |
| 187 | 05:08:13 | 7 Upper Containment | 96053.12 | 83.210 | 0.0737 | 29.3008 |
| | | Lower Containment | 55597.11 | 83.912 | 0.0706 | 29.3048 |
| | | Ice Condenser | 25599.37 | 26.681 | 0.0185 | 29.3053 |
| | | TOTAL | 177249.60 | | | |
| 188 | 05:18:13 | 8 Upper Containment | 96055.90 | 83.194 | 0.0736 | 29.3007 |
| | | Lower Containment | 55597.76 | 83.898 | 0.0707 | 29.3044 |
| | | Ice Condenser | 25599.03 | 26.684 | 0.0185 | 29.3051 |
| | | TOTAL | 177252.70 | | | |
| 189 | 05:28:13 | 9 Upper Containment | 96056.50 | 83.200 | 0.0735 | 29.3011 |
| | | Lower Containment | 55599.22 | 83.895 | 0.0704 | 29.3048 |
| | | Ice Condenser | 25596.84 | 26.738 | 0.0185 | 29.3058 |
| | | TOTAL | 177252.56 | | | |
| 190 | 05:38:14 | 0 Upper Containment | 96057.88 | 83.204 | 0.0732 | 29.3015 |
| | | Lower Containment | 55601.46 | 83.887 | 0.0703 | 29.3054 |
| | | Ice Condenser | 25594.90 | 26.777 | 0.0185 | 29.3059 |
| | | TOTAL | 177254.23 | | | |
| 191 | 05:48:14 | 1 Upper Containment | 96054.14 | 83.212 | 0.0732 | 29.3007 |
| | | Lower Containment | 55600.32 | 83.885 | 0.0701 | 29.3046 |
| | | Ice Condenser | 25593.29 | 26.794 | 0.0185 | 29.3051 |
| | | TOTAL | 177247.75 | | | |
| 192 | 05:58:14 | 2 Upper Containment | 96062.54 | 83.174 | 0.0732 | 29.3012 |
| | | Lower Containment | 55601.25 | 83.880 | 0.0701 | 29.3047 |
| | | Ice Condenser | 25589.07 | 26.881 | 0.0185 | 29.3055 |
| | | TOTAL | 177252.85 | | | |
| 193 | 06:08:15 | 3 Upper Containment | 96053.95 | 83.215 | 0.0730 | 29.3006 |
| | | Lower Containment | 55600.74 | 83.878 | 0.0699 | 29.3042 |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|----------------------------|-------------|-------------|--------------------|--------------|
| | | Ice Condenser | 25589.62 | 26.862 | 0.0185 | 29.3050 |
| | | TOTAL | 177244.31 | | | |
| 194 | 06:18:15 | 4 Upper Containment | 96066.67 | 83.177 | 0.0728 | 29.3022 |
| | | Lower Containment | 55604.82 | 83.870 | 0.0698 | 29.3058 |
| | | Ice Condenser | 25596.03 | 26.767 | 0.0185 | 29.3066 |
| | | TOTAL | 177267.53 | | | |
| 195 | 06:28:15 | 5 Upper Containment | 96062.48 | 83.192 | 0.0726 | 29.3016 |
| | | Lower Containment | 55606.07 | 83.855 | 0.0697 | 29.3055 |
| | | Ice Condenser | 25591.84 | 26.835 | 0.0185 | 29.3059 |
| | | TOTAL | 177260.40 | | | |
| 196 | 06:38:16 | 6 Upper Containment | 96066.31 | 83.187 | 0.0726 | 29.3025 |
| | | Lower Containment | 55606.75 | 83.855 | 0.0696 | 29.3058 |
| | | Ice Condenser | 25588.41 | 26.914 | 0.0185 | 29.3067 |
| | | TOTAL | 177261.48 | | | |
| 197 | 06:48:16 | 7 Upper Containment | 96063.99 | 83.194 | 0.0725 | 29.3021 |
| | | Lower Containment | 55605.85 | 83.856 | 0.0696 | 29.3054 |
| | | Ice Condenser | 25586.46 | 26.942 | 0.0185 | 29.3062 |
| | | TOTAL | 177256.30 | | | |
| 198 | 06:58:16 | 8 Upper Containment | 96060.39 | 83.180 | 0.0725 | 29.3002 |
| | | Lower Containment | 55605.37 | 83.828 | 0.0694 | 29.3034 |
| | | Ice Condenser | 25585.20 | 26.937 | 0.0185 | 29.3044 |
| | | TOTAL | 177250.96 | | | |
| 199 | 07:08:17 | 9 Upper Containment | 96065.35 | 83.163 | 0.0722 | 29.3005 |
| | | Lower Containment | 55606.56 | 83.841 | 0.0693 | 29.3046 |
| | | Ice Condenser | 25584.64 | 26.953 | 0.0185 | 29.3048 |
| | | TOTAL | 177256.54 | | | |
| 200 | 07:18:17 | 0 Upper Containment | 96066.73 | 83.148 | 0.0722 | 29.3001 |
| | | Lower Containment | 55606.26 | 83.833 | 0.0693 | 29.3040 |
| | | Ice Condenser | 25584.85 | 26.943 | 0.0185 | 29.3044 |
| | | TOTAL | 177257.84 | | | |
| 201 | 07:28:17 | 1 Upper Containment | 96065.85 | 83.163 | 0.0719 | 29.3003 |
| | | Lower Containment | 55607.92 | 83.817 | 0.0690 | 29.3038 |
| | | Ice Condenser | 25587.31 | 26.900 | 0.0185 | 29.3046 |
| | | TOTAL | 177261.08 | | | |
| 202 | 07:38:18 | 2 Upper Containment | 96068.56 | 83.130 | 0.0719 | 29.2994 |
| | | Lower Containment | 55606.02 | 83.815 | 0.0690 | 29.3027 |
| | | Ice Condenser | 25586.08 | 26.906 | 0.0185 | 29.3036 |
| | | TOTAL | 177260.66 | | | |
| 203 | 07:48:18 | 3 Upper Containment | 96069.28 | 83.154 | 0.0718 | 29.3008 |
| | | Lower Containment | 55608.57 | 83.816 | 0.0690 | 29.3040 |
| | | Ice Condenser | 25590.71 | 26.843 | 0.0185 | 29.3051 |
| | | TOTAL | 177268.57 | | | |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|---------------------|-------------|-------------|--------------------|--------------|
| 204 | 07:58:18 | 4 Upper Containment | 96071.18 | 83.148 | 0.0715 | 29.3008 |
| | | Lower Containment | 55610.81 | 83.809 | 0.0688 | 29.3047 |
| | | Ice Condenser | 25592.38 | 26.811 | 0.0185 | 29.3051 |
| | | TOTAL | 177274.37 | | | |
| 205 | 08:08:19 | 5 Upper Containment | 96063.25 | 83.154 | 0.0715 | 29.2986 |
| | | Lower Containment | 55608.54 | 83.792 | 0.0687 | 29.3025 |
| | | Ice Condenser | 25584.22 | 26.926 | 0.0185 | 29.3027 |
| | | TOTAL | 177256.01 | | | |
| 206 | 08:18:19 | 6 Upper Containment | 96061.16 | 83.142 | 0.0713 | 29.2972 |
| | | Lower Containment | 55605.84 | 83.787 | 0.0686 | 29.3006 |
| | | Ice Condenser | 25583.92 | 26.909 | 0.0185 | 29.3013 |
| | | TOTAL | 177250.91 | | | |
| 207 | 08:28:19 | 7 Upper Containment | 96065.87 | 83.118 | 0.0713 | 29.2973 |
| | | Lower Containment | 55605.16 | 83.793 | 0.0686 | 29.3006 |
| | | Ice Condenser | 25585.67 | 26.881 | 0.0185 | 29.3016 |
| | | TOTAL | 177256.70 | | | |
| 208 | 08:38:20 | 8 Upper Containment | 96060.85 | 83.135 | 0.0712 | 29.2966 |
| | | Lower Containment | 55606.04 | 83.780 | 0.0685 | 29.3002 |
| | | Ice Condenser | 25589.24 | 26.801 | 0.0185 | 29.3009 |
| | | TOTAL | 177256.13 | | | |
| 209 | 08:48:20 | 9 Upper Containment | 96062.98 | 83.117 | 0.0710 | 29.2961 |
| | | Lower Containment | 55605.84 | 83.772 | 0.0684 | 29.2996 |
| | | Ice Condenser | 25590.32 | 26.772 | 0.0185 | 29.3004 |
| | | TOTAL | 177259.14 | | | |
| 210 | 08:58:20 | 0 Upper Containment | 96060.66 | 83.124 | 0.0709 | 29.2957 |
| | | Lower Containment | 55606.11 | 83.768 | 0.0683 | 29.2995 |
| | | Ice Condenser | 25592.58 | 26.723 | 0.0185 | 29.3000 |
| | | TOTAL | 177259.35 | | | |
| 211 | 09:08:21 | 1 Upper Containment | 96062.52 | 83.094 | 0.0709 | 29.2946 |
| | | Lower Containment | 55605.65 | 83.754 | 0.0682 | 29.2983 |
| | | Ice Condenser | 25594.13 | 26.676 | 0.0185 | 29.2990 |
| | | TOTAL | 177262.30 | | | |
| 212 | 09:18:21 | 2 Upper Containment | 96061.53 | 83.099 | 0.0707 | 29.2944 |
| | | Lower Containment | 55605.17 | 83.751 | 0.0681 | 29.2979 |
| | | Ice Condenser | 25594.35 | 26.664 | 0.0185 | 29.2985 |
| | | TOTAL | 177261.05 | | | |
| 213 | 09:28:21 | 3 Upper Containment | 96059.64 | 83.095 | 0.0706 | 29.2935 |
| | | Lower Containment | 55603.87 | 83.749 | 0.0680 | 29.2970 |
| | | Ice Condenser | 25588.76 | 26.758 | 0.0185 | 29.2978 |
| | | TOTAL | 177252.27 | | | |
| 214 | 09:38:22 | 4 Upper Containment | 96055.31 | 83.108 | 0.0706 | 29.2929 |
| | | Lower Containment | 55603.52 | 83.744 | 0.0679 | 29.2964 |
| | | Ice Condenser | 25586.22 | 26.799 | 0.0185 | 29.2973 |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|----------------------------|-------------|-------------|--------------------|--------------|
| | | TOTAL | 177245.05 | | | |
| 215 | 09:48:22 | 5 Upper Containment | 96059.01 | 83.093 | 0.0704 | 29.2930 |
| | | Lower Containment | 55605.99 | 83.733 | 0.0678 | 29.2971 |
| | | Ice Condenser | 25581.31 | 26.892 | 0.0185 | 29.2973 |
| | | TOTAL | 177246.31 | | | |
| 216 | 09:58:22 | 6 Upper Containment | 96058.88 | 83.108 | 0.0703 | 29.2937 |
| | | Lower Containment | 55606.39 | 83.737 | 0.0679 | 29.2976 |
| | | Ice Condenser | 25574.88 | 27.027 | 0.0185 | 29.2981 |
| | | TOTAL | 177240.15 | | | |
| 217 | 10:08:23 | 7 Upper Containment | 96056.50 | 83.115 | 0.0703 | 29.2934 |
| | | Lower Containment | 55606.75 | 83.726 | 0.0676 | 29.2969 |
| | | Ice Condenser | 25572.88 | 27.059 | 0.0185 | 29.2977 |
| | | TOTAL | 177236.13 | | | |
| 218 | 10:18:23 | 8 Upper Containment | 96058.73 | 83.102 | 0.0700 | 29.2930 |
| | | Lower Containment | 55605.87 | 83.723 | 0.0677 | 29.2963 |
| | | Ice Condenser | 25569.93 | 27.107 | 0.0185 | 29.2972 |
| | | TOTAL | 177234.53 | | | |
| 219 | 10:28:23 | 9 Upper Containment | 96058.18 | 83.074 | 0.0700 | 29.2913 |
| | | Lower Containment | 55604.09 | 83.715 | 0.0675 | 29.2948 |
| | | Ice Condenser | 25576.64 | 26.954 | 0.0185 | 29.2957 |
| | | TOTAL | 177238.91 | | | |
| 220 | 10:38:24 | 0 Upper Containment | 96056.92 | 83.068 | 0.0699 | 29.2905 |
| | | Lower Containment | 55604.30 | 83.705 | 0.0676 | 29.2944 |
| | | Ice Condenser | 25582.42 | 26.829 | 0.0185 | 29.2948 |
| | | TOTAL | 177243.64 | | | |
| 221 | 10:48:24 | 1 Upper Containment | 96057.79 | 83.053 | 0.0698 | 29.2899 |
| | | Lower Containment | 55604.17 | 83.697 | 0.0674 | 29.2937 |
| | | Ice Condenser | 25584.48 | 26.779 | 0.0185 | 29.2941 |
| | | TOTAL | 177246.43 | | | |
| 222 | 10:58:24 | 2 Upper Containment | 96051.25 | 83.077 | 0.0698 | 29.2891 |
| | | Lower Containment | 55602.10 | 83.700 | 0.0673 | 29.2927 |
| | | Ice Condenser | 25586.50 | 26.730 | 0.0185 | 29.2935 |
| | | TOTAL | 177239.84 | | | |
| 223 | 11:08:25 | 3 Upper Containment | 96053.70 | 83.060 | 0.0695 | 29.2887 |
| | | Lower Containment | 55602.23 | 83.687 | 0.0672 | 29.2920 |
| | | Ice Condenser | 25588.90 | 26.677 | 0.0185 | 29.2931 |
| | | TOTAL | 177244.83 | | | |
| 224 | 11:18:25 | 4 Upper Containment | 96052.59 | 83.057 | 0.0695 | 29.2882 |
| | | Lower Containment | 55602.40 | 83.684 | 0.0671 | 29.2918 |
| | | Ice Condenser | 25590.44 | 26.642 | 0.0185 | 29.2927 |
| | | TOTAL | 177245.43 | | | |
| 225 | 11:28:25 | 5 Upper Containment | 96051.50 | 83.050 | 0.0694 | 29.2874 |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|----------------------------|------------------|-------------|--------------------|--------------|
| | | Lower Containment | 55603.18 | 83.673 | 0.0670 | 29.2915 |
| | | Ice Condenser | 25593.76 | 26.563 | 0.0185 | 29.2917 |
| | | TOTAL | 177248.43 | | | |
| 226 | 11:38:26 | 6 Upper Containment | 96049.13 | 83.056 | 0.0693 | 29.2869 |
| | | Lower Containment | 55602.42 | 83.668 | 0.0670 | 29.2908 |
| | | Ice Condenser | 25596.39 | 26.505 | 0.0185 | 29.2913 |
| | | TOTAL | 177247.94 | | | |
| 227 | 11:48:26 | 7 Upper Containment | 96044.97 | 83.067 | 0.0693 | 29.2862 |
| | | Lower Containment | 55600.03 | 83.671 | 0.0668 | 29.2896 |
| | | Ice Condenser | 25595.43 | 26.512 | 0.0185 | 29.2906 |
| | | TOTAL | 177240.43 | | | |
| 228 | 11:58:26 | 8 Upper Containment | 96059.88 | 83.023 | 0.0691 | 29.2882 |
| | | Lower Containment | 55605.20 | 83.662 | 0.0667 | 29.2917 |
| | | Ice Condenser | 25589.41 | 26.661 | 0.0185 | 29.2927 |
| | | TOTAL | 177254.49 | | | |
| 229 | 12:08:27 | 9 Upper Containment | 96059.01 | 83.041 | 0.0690 | 29.2888 |
| | | Lower Containment | 55607.61 | 83.654 | 0.0667 | 29.2925 |
| | | Ice Condenser | 25583.23 | 26.787 | 0.0185 | 29.2932 |
| | | TOTAL | 177249.85 | | | |
| 230 | 12:18:27 | 0 Upper Containment | 96060.37 | 83.051 | 0.0691 | 29.2898 |
| | | Lower Containment | 55610.91 | 83.648 | 0.0665 | 29.2937 |
| | | Ice Condenser | 25588.48 | 26.704 | 0.0185 | 29.2942 |
| | | TOTAL | 177259.76 | | | |
| 231 | 12:28:27 | 1 Upper Containment | 96059.98 | 83.049 | 0.0689 | 29.2894 |
| | | Lower Containment | 55609.77 | 83.649 | 0.0664 | 29.2931 |
| | | Ice Condenser | 25587.50 | 26.716 | 0.0185 | 29.2938 |
| | | TOTAL | 177257.24 | | | |
| 232 | 12:38:28 | 2 Upper Containment | 96064.22 | 83.029 | 0.0688 | 29.2896 |
| | | Lower Containment | 55611.62 | 83.629 | 0.0664 | 29.2930 |
| | | Ice Condenser | 25584.99 | 26.766 | 0.0185 | 29.2939 |
| | | TOTAL | 177260.83 | | | |
| 233 | 12:48:28 | 3 Upper Containment | 96065.42 | 83.022 | 0.0687 | 29.2894 |
| | | Lower Containment | 55610.19 | 83.639 | 0.0664 | 29.2928 |
| | | Ice Condenser | 25586.15 | 26.741 | 0.0185 | 29.2938 |
| | | TOTAL | 177261.77 | | | |
| 234 | 12:58:28 | 4 Upper Containment | 96057.01 | 83.022 | 0.0686 | 29.2868 |
| | | Lower Containment | 55607.35 | 83.623 | 0.0662 | 29.2902 |
| | | Ice Condenser | 25582.28 | 26.772 | 0.0185 | 29.2912 |
| | | TOTAL | 177246.64 | | | |
| 235 | 13:08:29 | 5 Upper Containment | 96054.96 | 83.039 | 0.0686 | 29.2870 |
| | | Lower Containment | 55609.58 | 83.615 | 0.0662 | 29.2910 |
| | | Ice Condenser | 25582.66 | 26.765 | 0.0185 | 29.2912 |
| | | TOTAL | 177247.20 | | | |

APPENDIX D

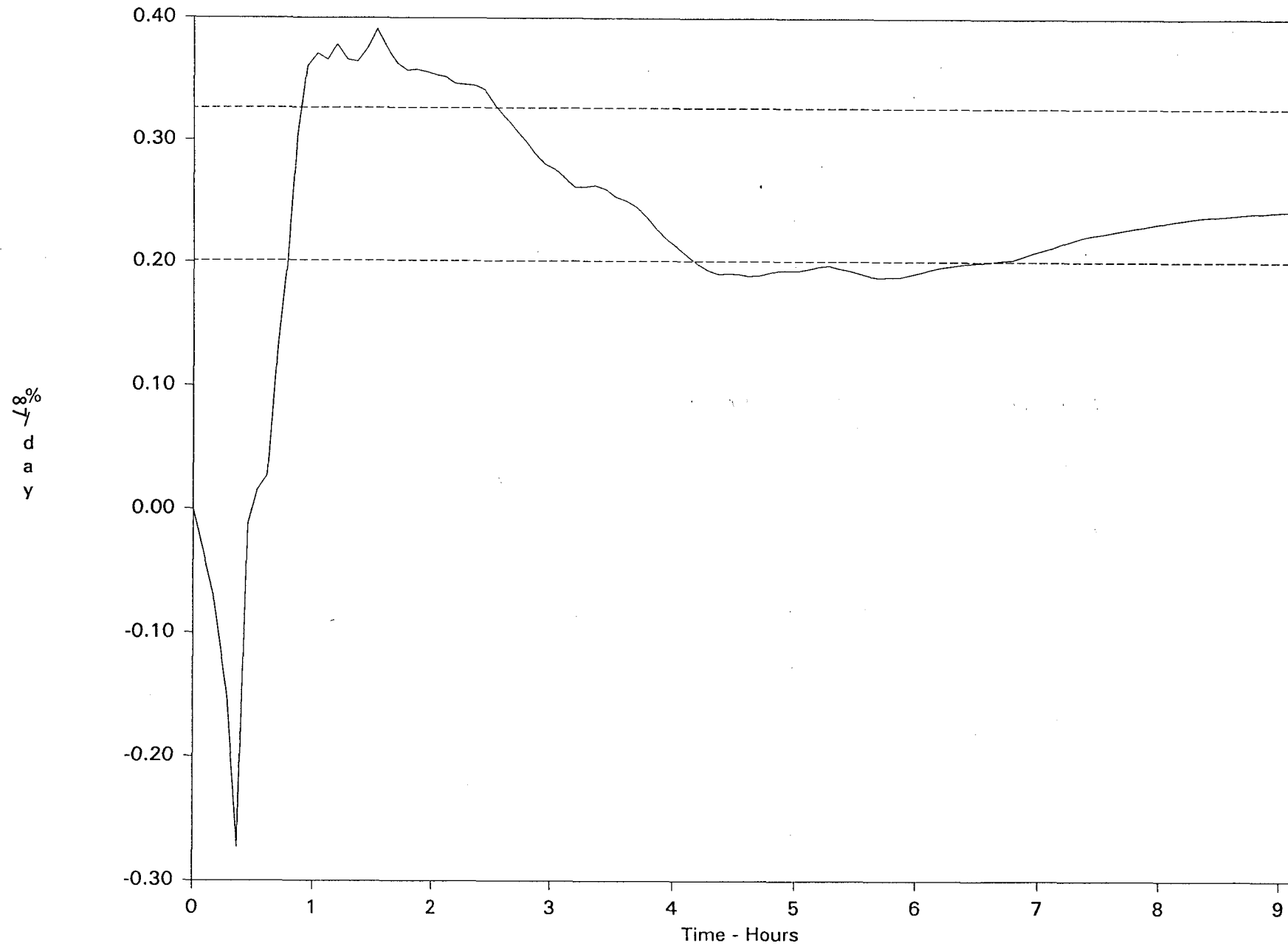
Verification Test Phase Graphs

(samples 243 to 351)

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| Ice Condenser Compartment Temperature | 98 |
| Upper Containment Compartment Vapor Pressure | 99 |
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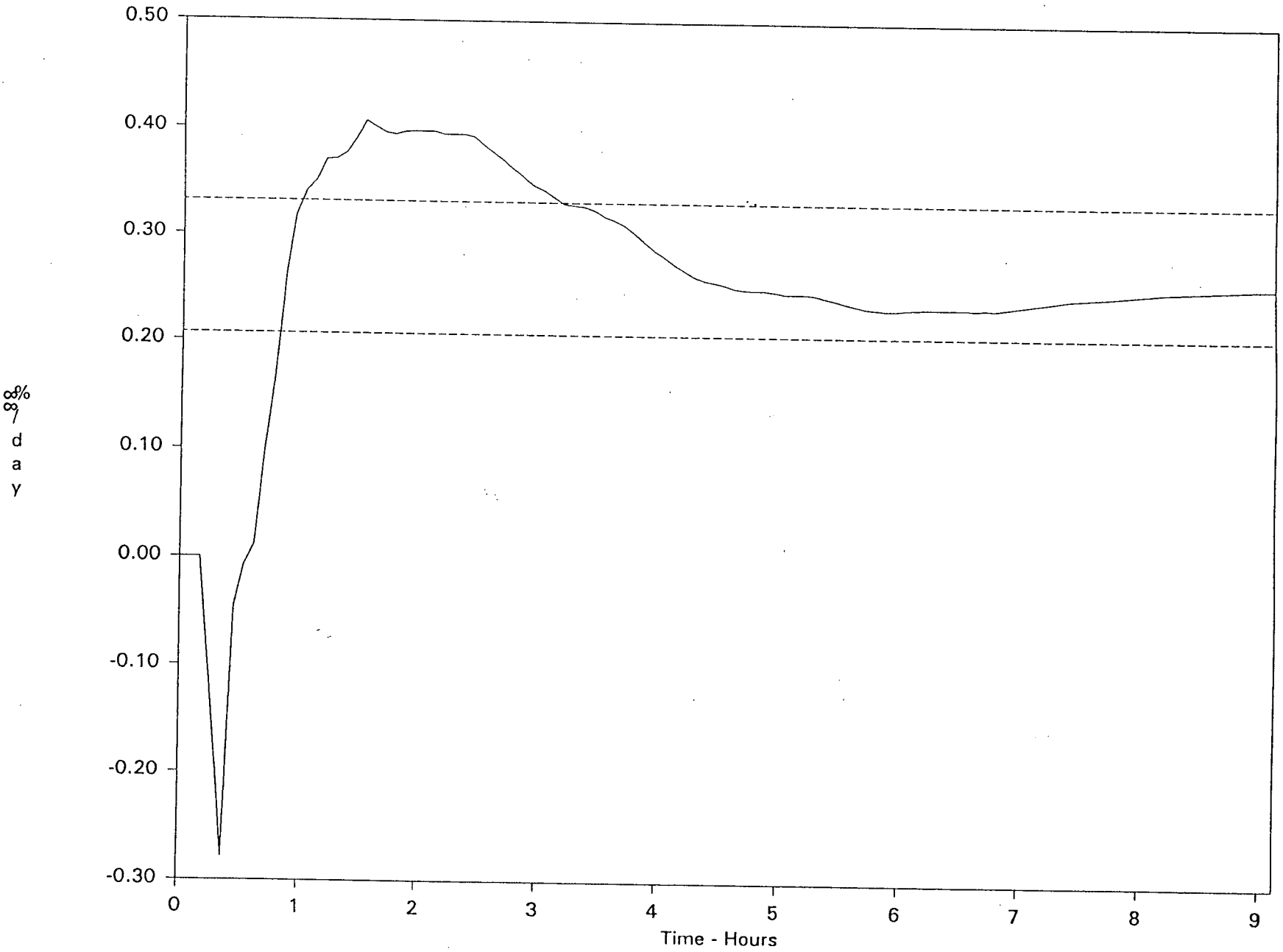
Mass Point Leak

Watts Bar Nuclear Plant
Unit 1 - Startup



Calculated Total Time Leak

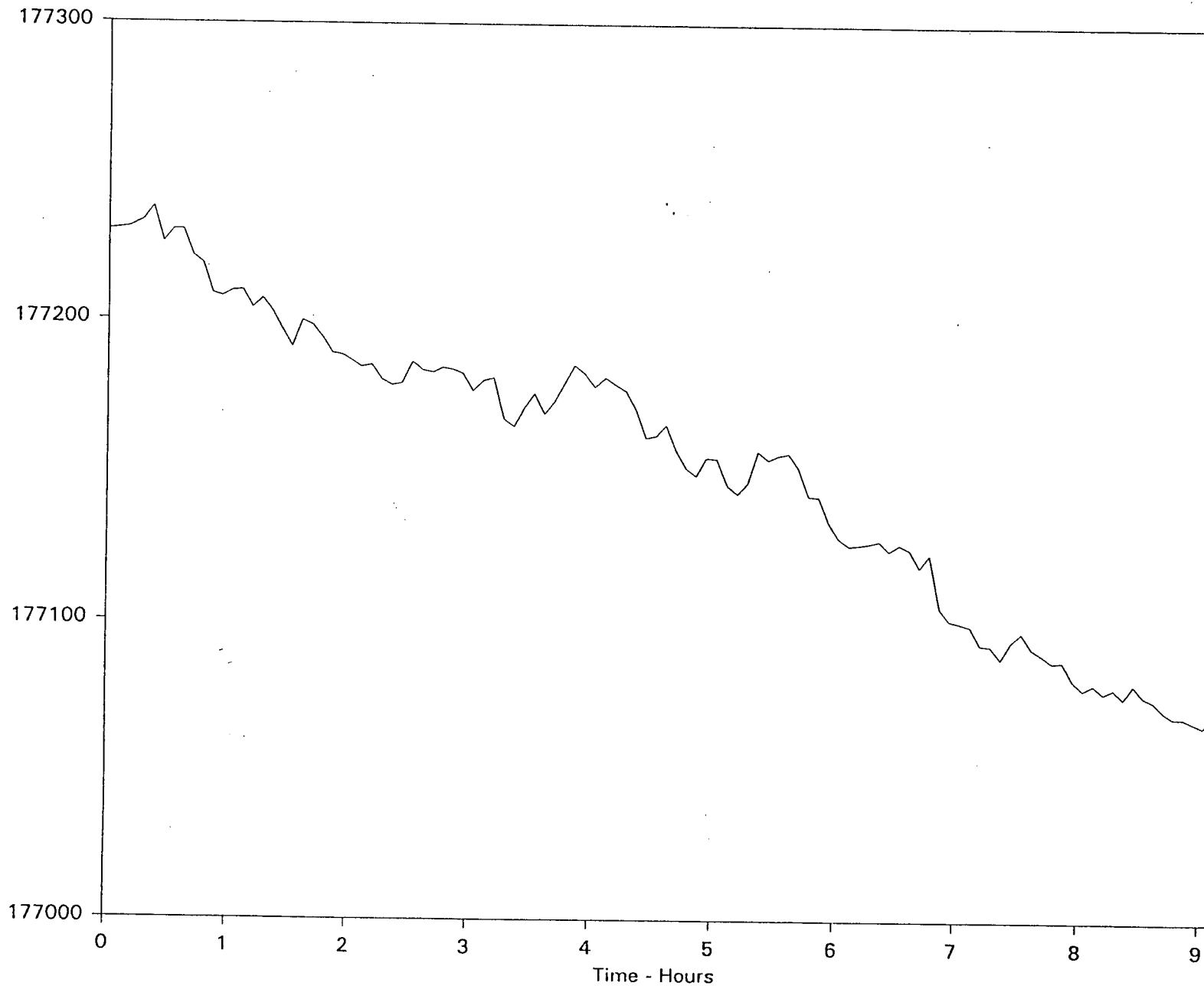
Watts Bar Nuclear Plant
Unit 1 - Startup



Containment Mass

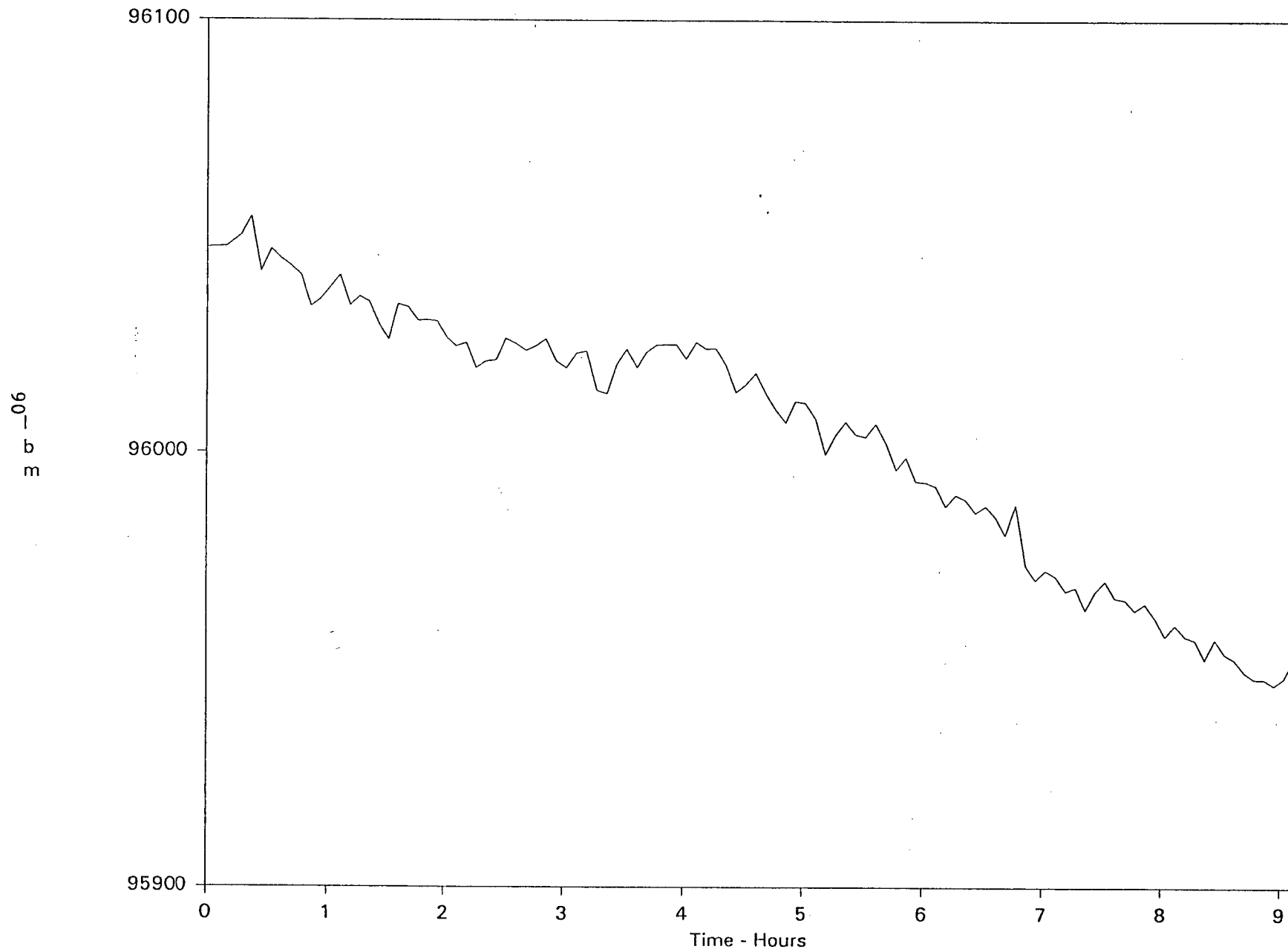
Watts Bar Nuclear Plant
Unit 1 - Startup

89-5 E



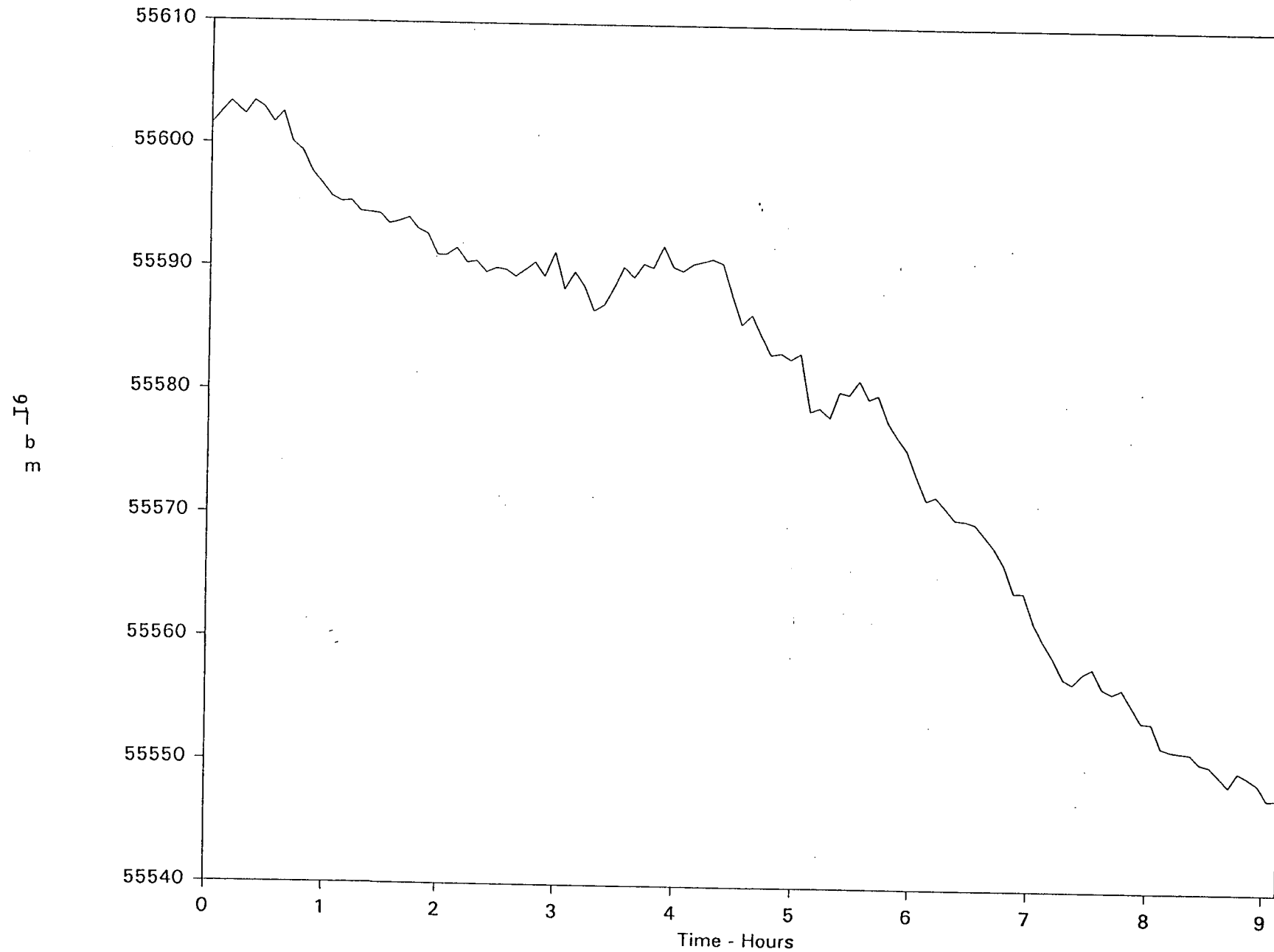
Upper Containment Mass

Watts Bar Nuclear Plant
Unit 1 - Startup



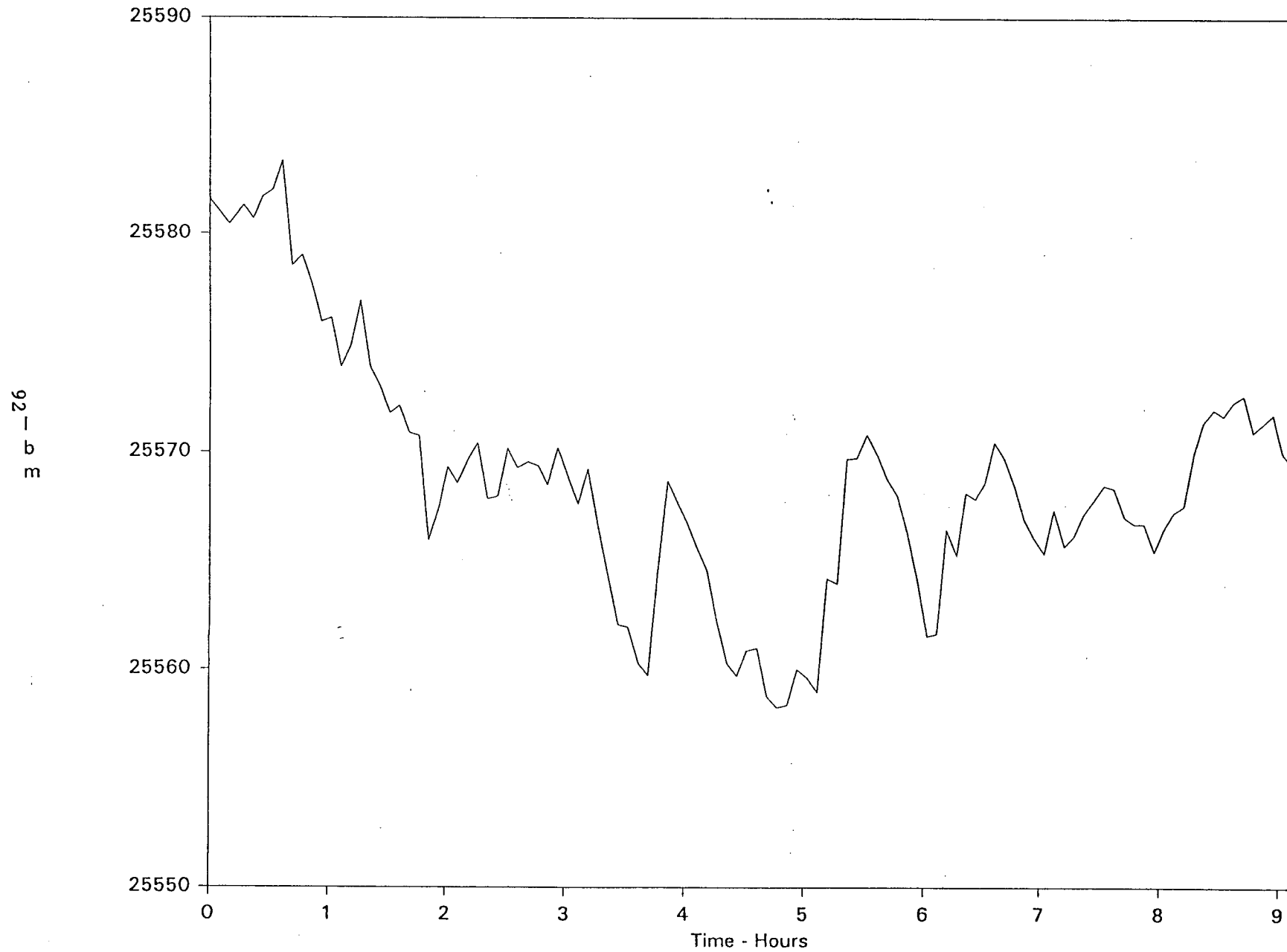
Lower Containment Mass

Watts Bar Nuclear Plant
Unit 1 - Startup



Ice Condenser Mass

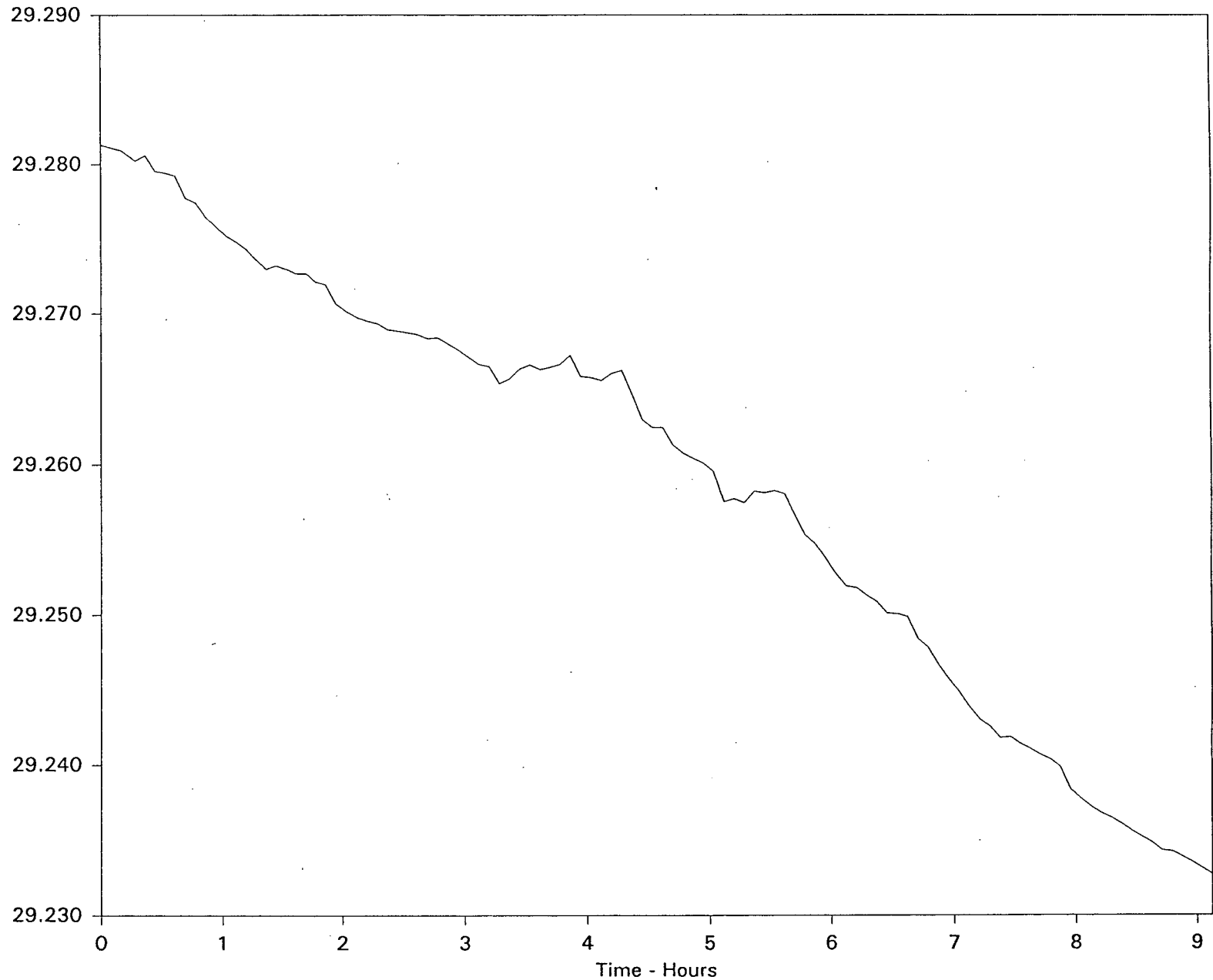
Watts Bar Nuclear Plant
Unit 1 - Startup



Upper Containment Average Pressure

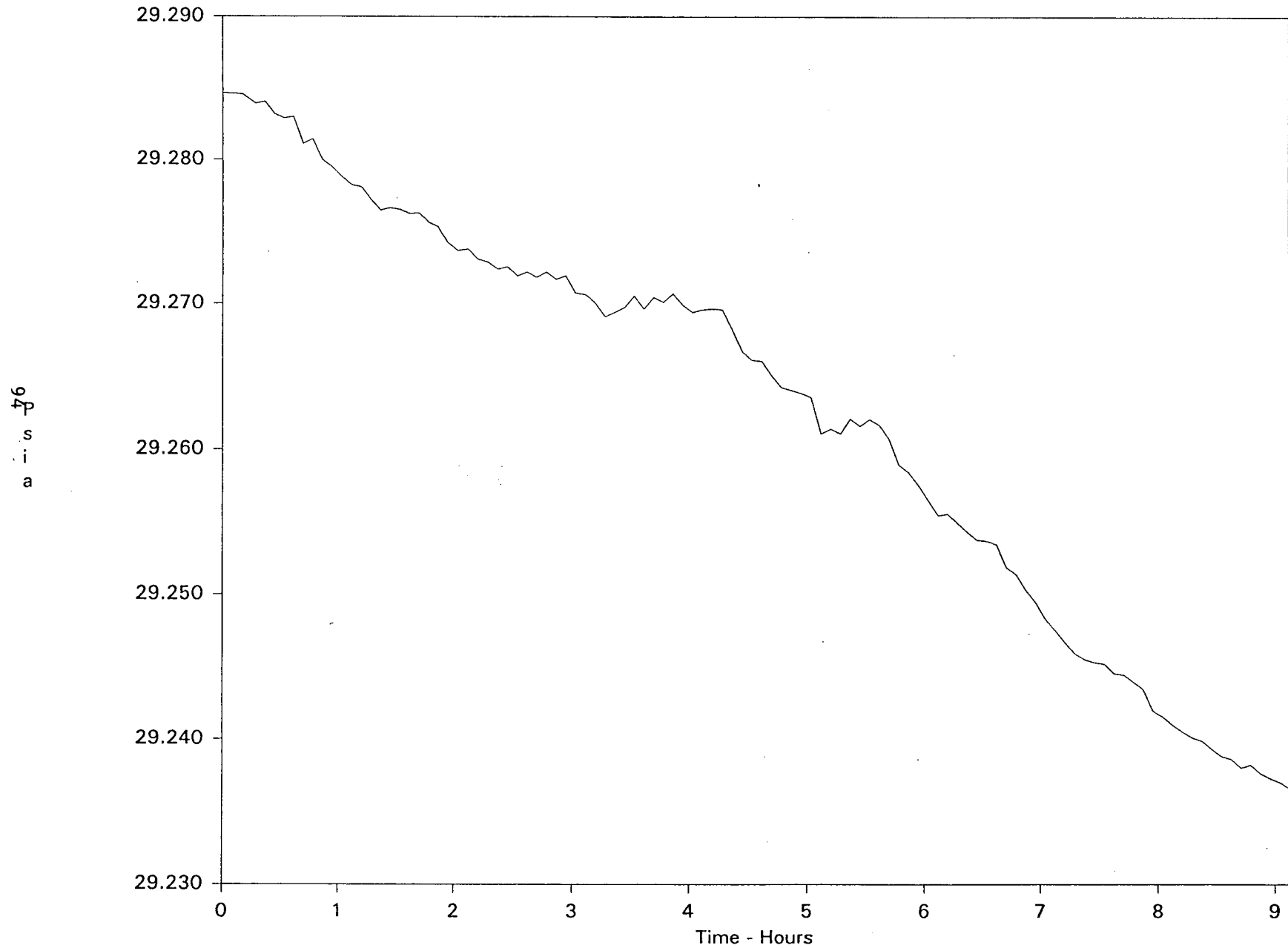
Watts Bar Nuclear Plant
Unit 1 - Startup

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Lower Containment Average Pressure

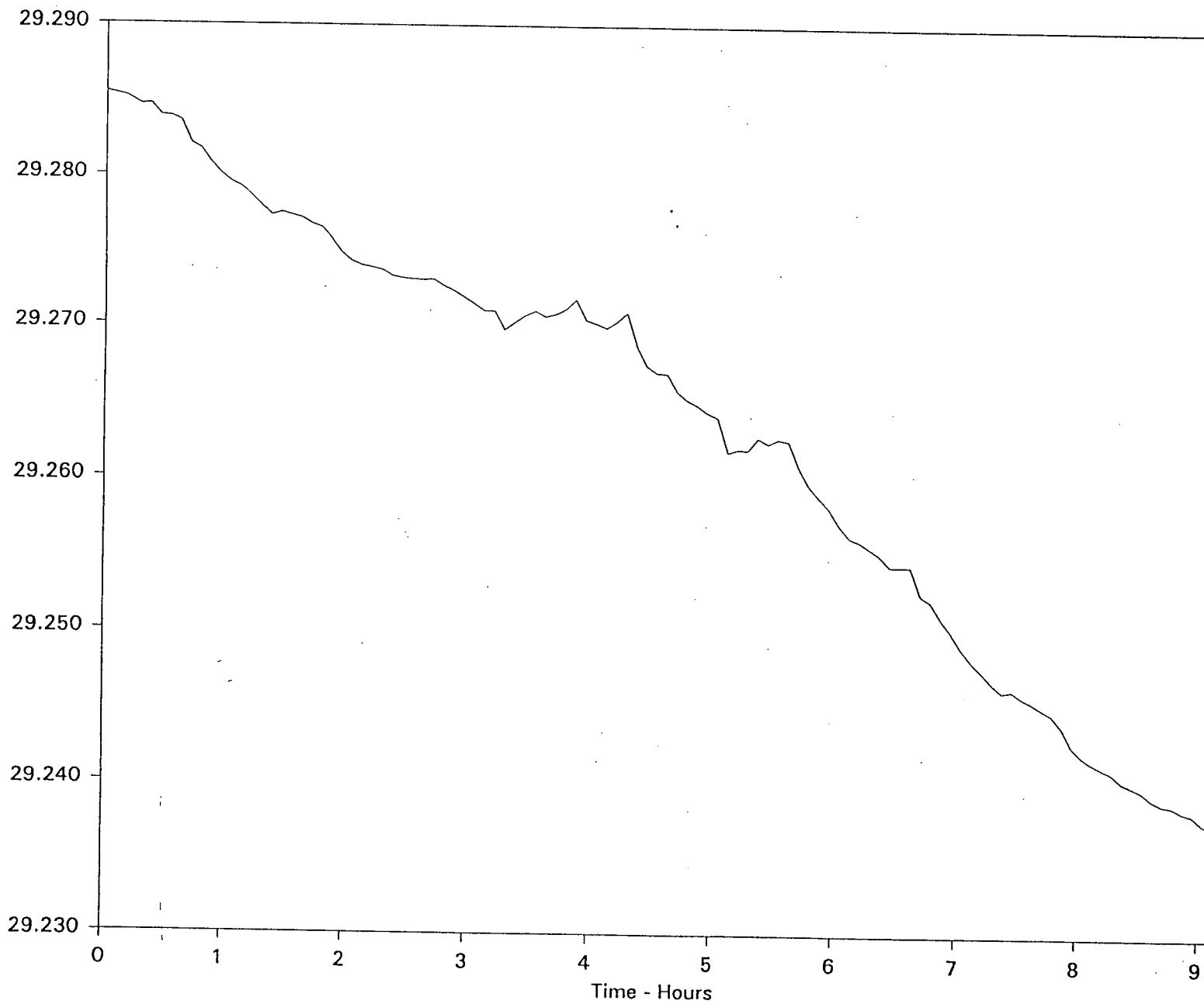
Watts Bar Nuclear Plant
Unit 1 - Startup



Ice Condenser Average Pressure

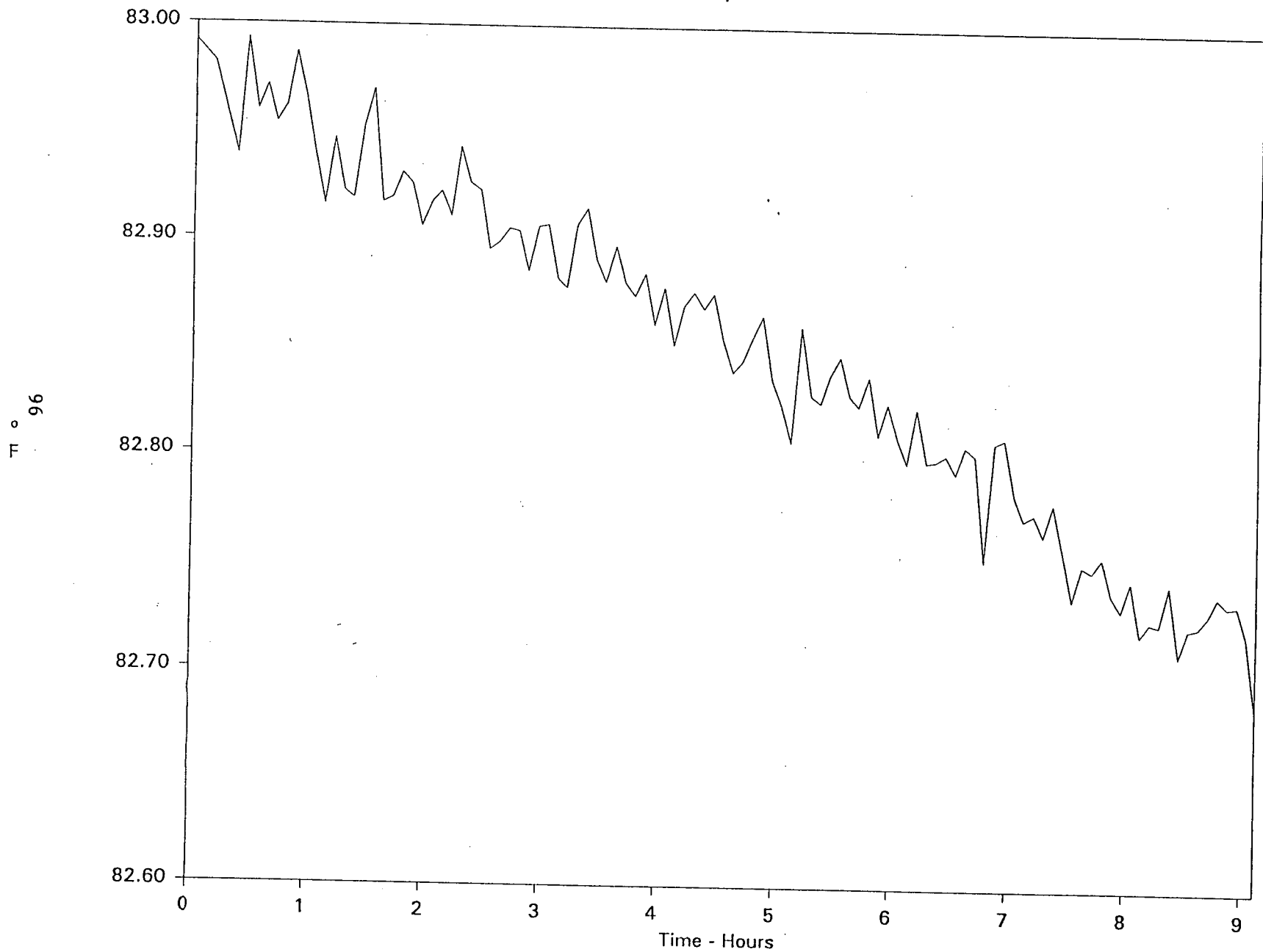
Watts Bar Nuclear Plant
Unit 1 - Startup

95000



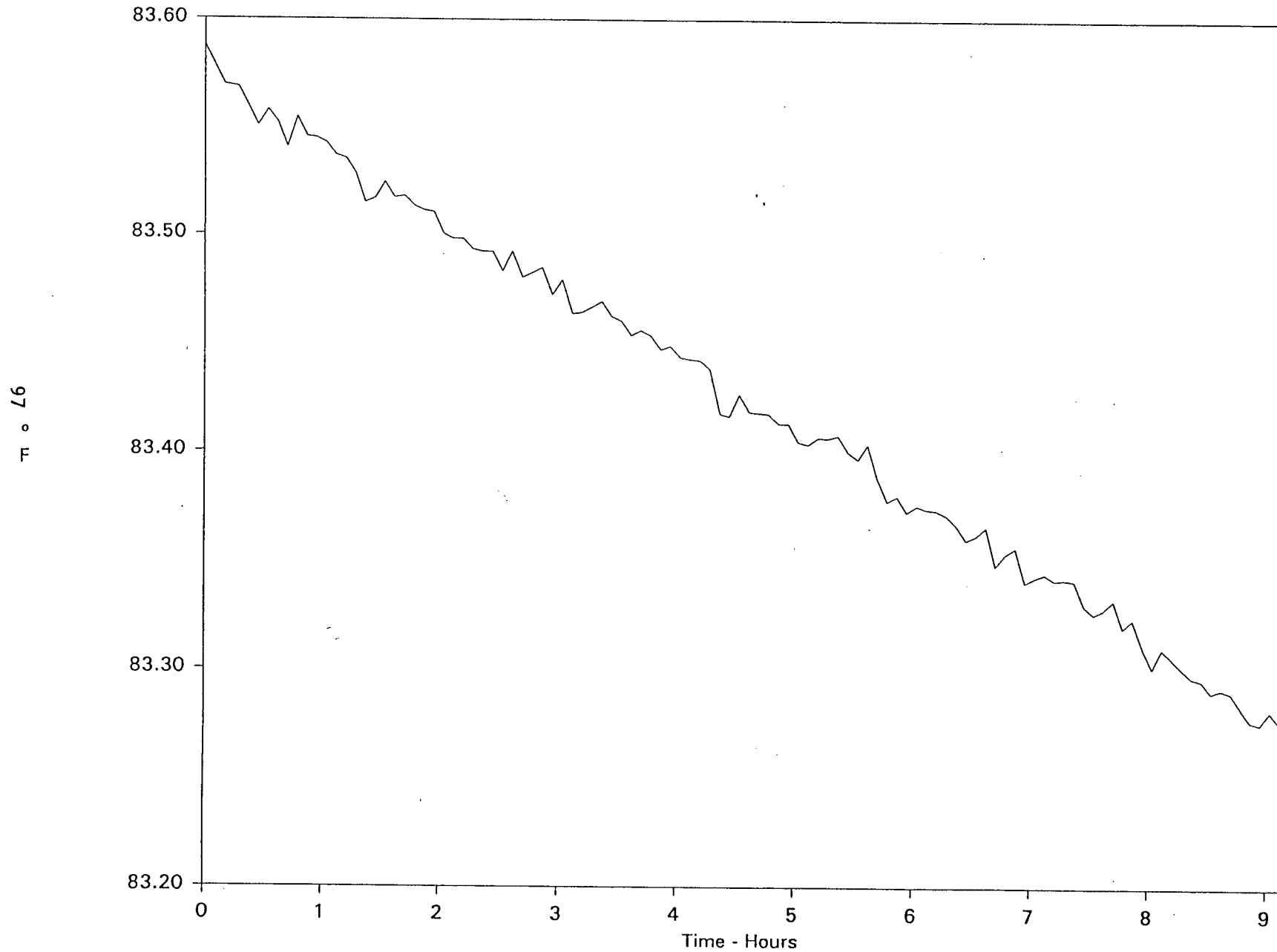
Upper Containment Average Temperature

Watts Bar Nuclear Plant
Unit 1 - Startup



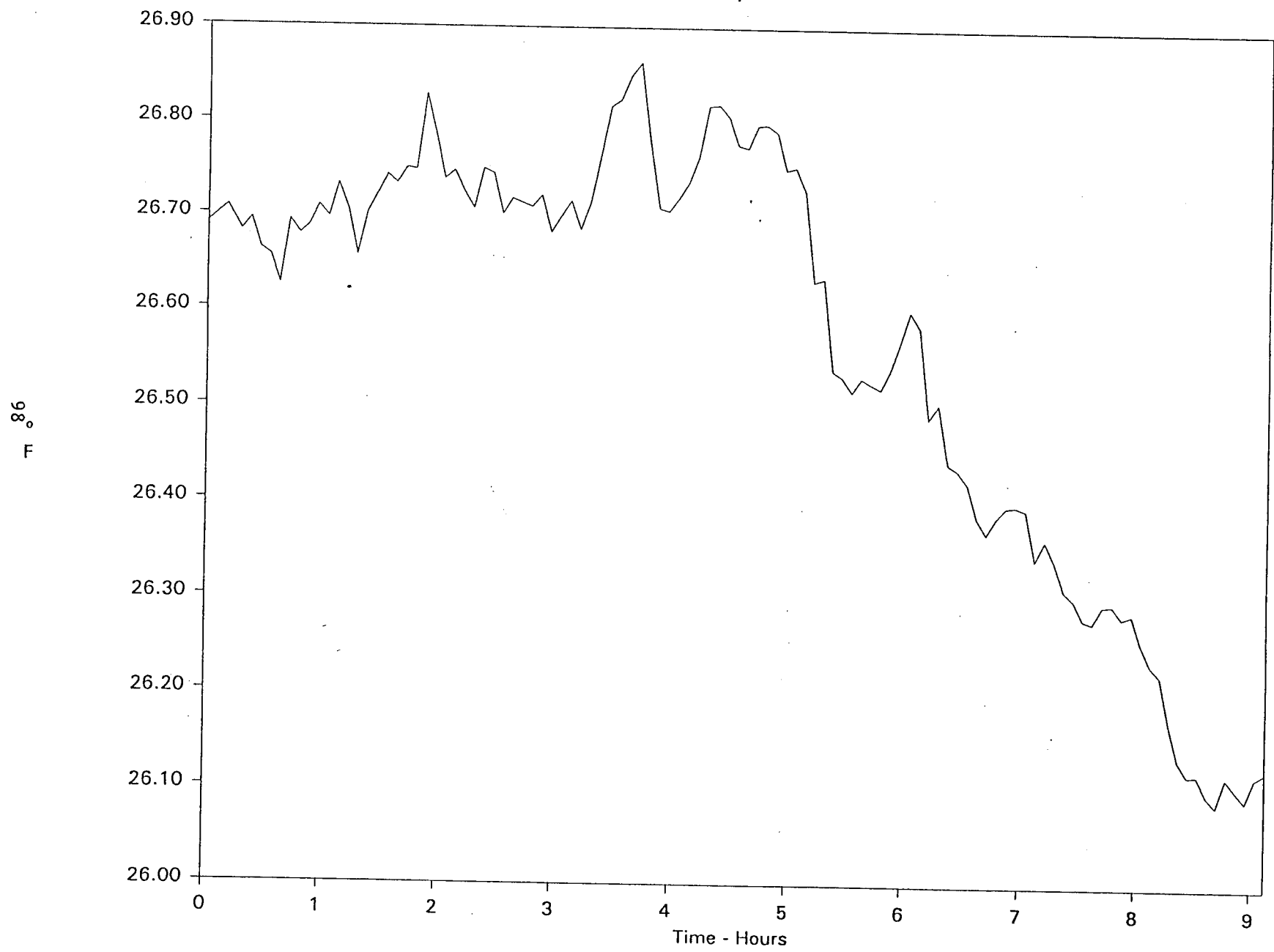
Lower Containment Average Temperature

Watts Bar Nuclear Plant
Unit 1 - Startup



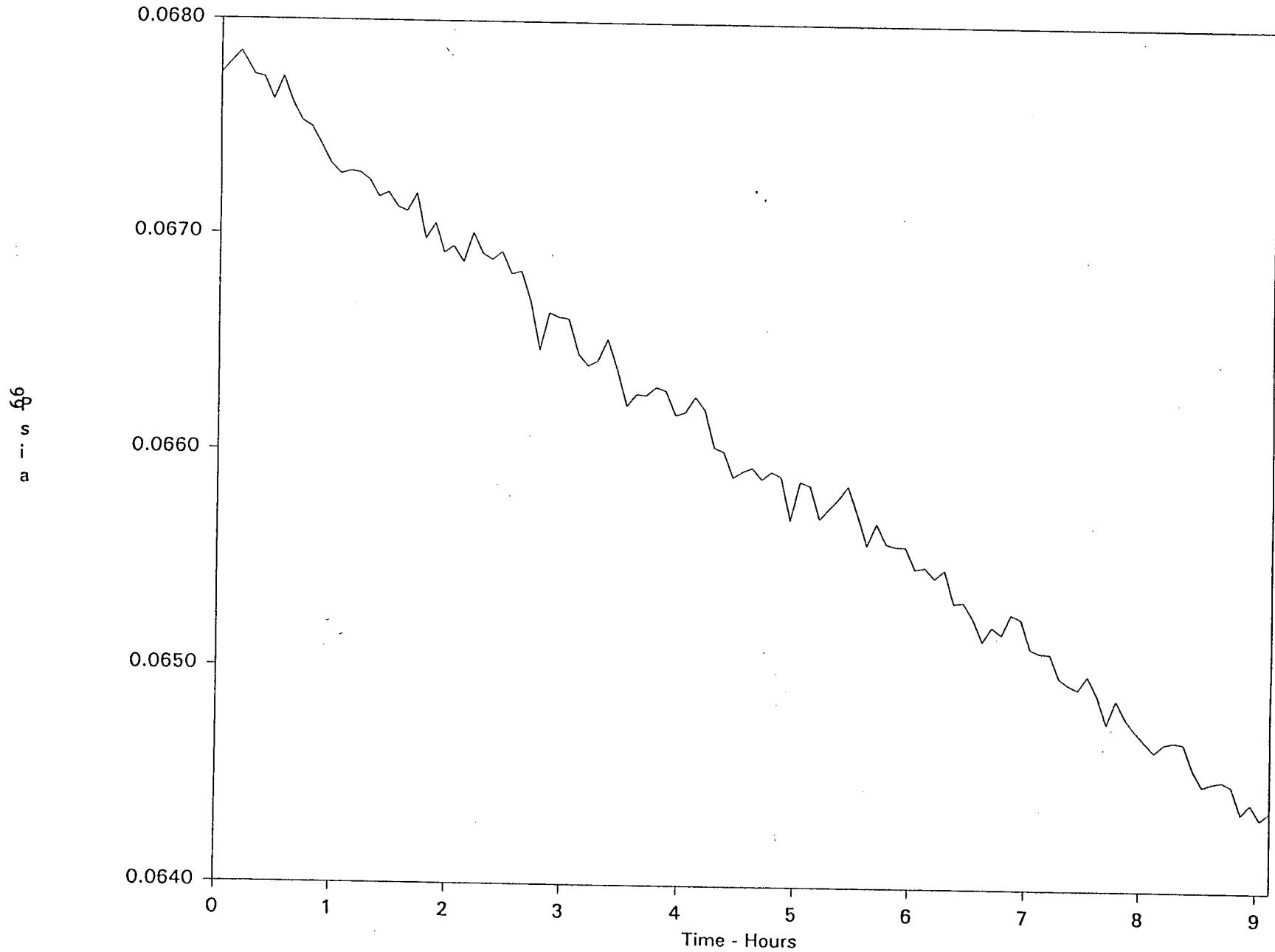
Ice Condenser Average Temperature

Watts Bar Nuclear Plant
Unit 1 - Startup



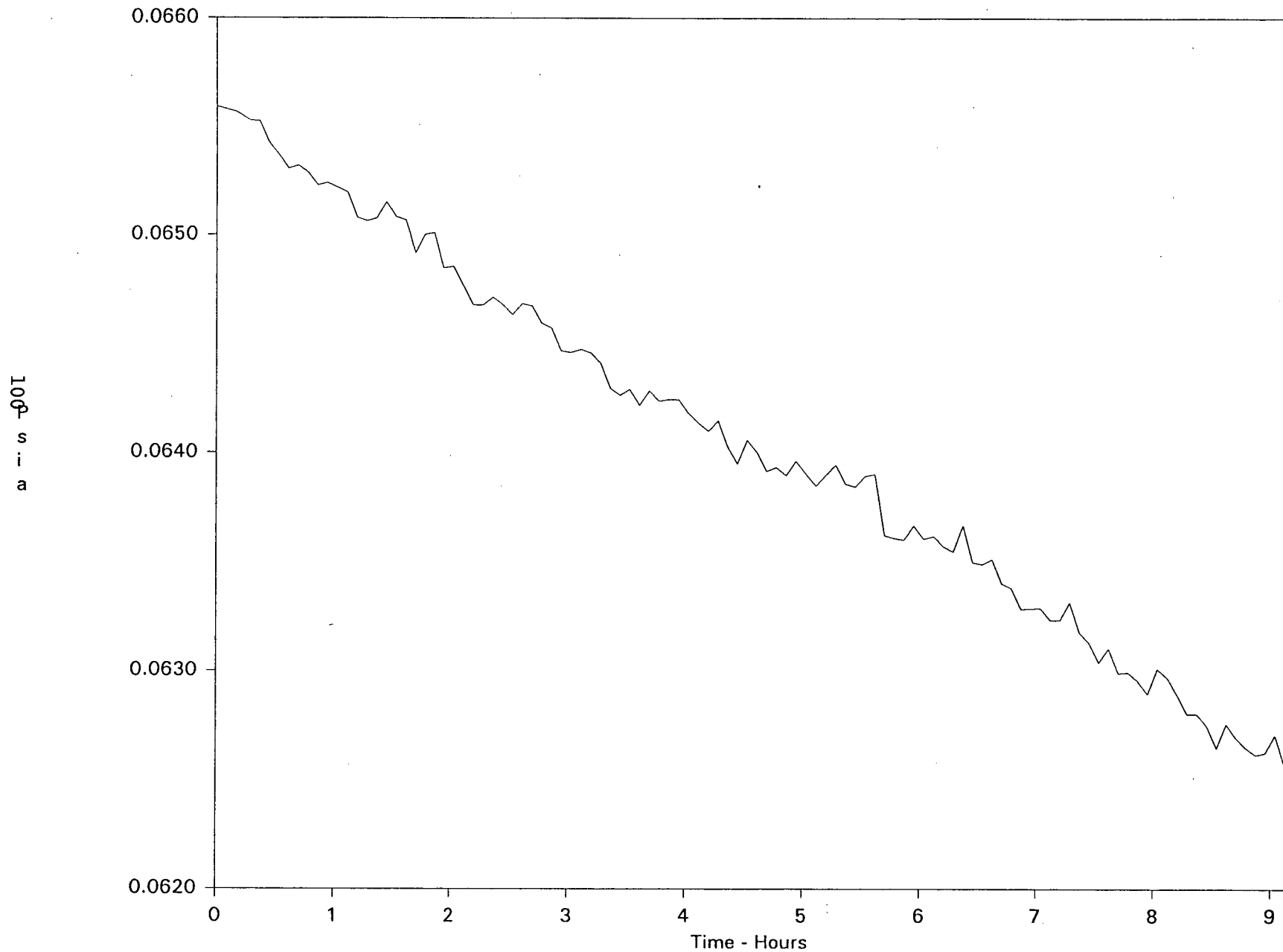
Upper Containment Average Vapor Pressure

Watts Bar Nuclear Plant
Unit 1 - Startup



Lower Containment Average Vapor Pressure

Watts Bar Nuclear Plant
Unit 1 - Startup



APPENDIX E

CILRT Verification Tabular Data

(samples 243 to 351)

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Mass Point Leak Rate Analysis

Verification Phase

Watts Bar Nuclear Plant
Unit 1 - Startup

| <u>Rdg</u> | <u>Time</u> | <u>Norm Mass</u> | <u>MP Leak %/day</u> | <u>MP UCL %/day</u> |
|------------|-----------------|------------------|--------------------------|-------------------------|
| 243 | 28-Jun-94 14:28 | 1.000000 | 0.000000 | 0.000000 |
| 244 | 28-Jun-94 14:38 | 1.000005 | -0.069530 | 0.000000 |
| 245 | 28-Jun-94 14:45 | 1.000019 | -0.152029 | 0.357867 |
| 246 | 28-Jun-94 14:50 | 1.000045 | -0.273551 | 0.012715 |
| 247 | 28-Jun-94 14:55 | 0.999977 | -0.012716 | 0.454796 |
| 248 | 28-Jun-94 15:00 | 1.000001 | 0.015580 | 0.315224 |
| 249 | 28-Jun-94 15:05 | 1.000001 | 0.027035 | 0.237659 |
| 250 | 28-Jun-94 15:10 | 0.999950 | 0.128716 | 0.330763 |
| 251 | 28-Jun-94 15:15 | 0.999936 | 0.197210 | 0.373945 |
| 252 | 28-Jun-94 15:20 | 0.999878 | 0.304038 | 0.491613 |
| 253 | 28-Jun-94 15:25 | 0.999872 | 0.360178 | 0.525972 |
| 254 | 28-Jun-94 15:30 | 0.999883 | 0.370810 | 0.509316 |
| 255 | 28-Jun-94 15:35 | 0.999884 | 0.365667 | 0.482872 |
| 256 | 28-Jun-94 15:40 | 0.999850 | 0.378251 | 0.479514 |
| 257 | 28-Jun-94 15:45 | 0.999868 | 0.365776 | 0.454445 |
| 258 | 28-Jun-94 15:50 | 0.999844 | 0.364076 | 0.441614 |
| 259 | 28-Jun-94 15:55 | 0.999810 | 0.374541 | 0.443759 |
| 260 | 28-Jun-94 16:00 | 0.999778 | 0.391042 | 0.454836 |
| 261 | 28-Jun-94 16:05 | 0.999828 | 0.375559 | 0.434761 |
| 262 | 28-Jun-94 16:10 | 0.999819 | 0.362544 | 0.417415 |
| 263 | 28-Jun-94 16:15 | 0.999795 | 0.356753 | 0.406707 |
| 264 | 28-Jun-94 16:20 | 0.999767 | 0.357687 | 0.403076 |
| 265 | 28-Jun-94 16:25 | 0.999763 | 0.355570 | 0.397038 |
| 266 | 28-Jun-94 16:30 | 0.999753 | 0.353386 | 0.391437 |
| 267 | 28-Jun-94 16:35 | 0.999741 | 0.351539 | 0.386570 |
| 268 | 28-Jun-94 16:40 | 0.999745 | 0.346299 | 0.379036 |
| 269 | 28-Jun-94 16:45 | 0.999717 | 0.345617 | 0.375919 |
| 270 | 28-Jun-94 16:50 | 0.999707 | 0.344724 | 0.372859 |
| 271 | 28-Jun-94 16:55 | 0.999711 | 0.340961 | 0.367406 |
| 272 | 28-Jun-94 17:00 | 0.999750 | 0.328526 | 0.356100 |
| 273 | 28-Jun-94 17:05 | 0.999735 | 0.318879 | 0.346369 |
| 274 | 28-Jun-94 17:10 | 0.999732 | 0.309723 | 0.337021 |
| 275 | 28-Jun-94 17:15 | 0.999740 | 0.299186 | 0.326842 |
| 276 | 28-Jun-94 17:20 | 0.999737 | 0.289345 | 0.317108 |
| 277 | 28-Jun-94 17:25 | 0.999729 | 0.280776 | 0.308265 |
| 278 | 28-Jun-94 17:30 | 0.999696 | 0.276512 | 0.302798 |
| 279 | 28-Jun-94 17:35 | 0.999716 | 0.269338 | 0.295170 |
| 280 | 28-Jun-94 17:40 | 0.999721 | 0.261557 | 0.287181 |
| 281 | 28-Jun-94 17:45 | 0.999645 | 0.262289 | 0.286600 |
| 282 | 28-Jun-94 17:50 | 0.999631 | 0.263431 | 0.286545 |
| 283 | 28-Jun-94 17:55 | 0.999665 | 0.260139 | 0.282352 |

Mass Point Leak Rate Analysis

Verification Phase

Watts Bar Nuclear Plant
Unit 1 - Startup

| <u>Rdg</u> | <u>Time</u> | <u>Norm Mass</u> | <u>MP Leak %/day</u> | <u>MP UCL %/day</u> |
|------------|-----------------|------------------|--------------------------|-------------------------|
| 284 | 28-Jun-94 18:00 | 0.999692 | 0.253867 | 0.275884 |
| 285 | 28-Jun-94 18:05 | 0.999654 | 0.251043 | 0.272209 |
| 286 | 28-Jun-94 18:10 | 0.999677 | 0.245831 | 0.266658 |
| 287 | 28-Jun-94 18:15 | 0.999711 | 0.237763 | 0.259155 |
| 288 | 28-Jun-94 18:20 | 0.999746 | 0.227285 | 0.250144 |
| 289 | 28-Jun-94 18:25 | 0.999731 | 0.218622 | 0.242069 |
| 290 | 28-Jun-94 18:30 | 0.999705 | 0.212316 | 0.235602 |
| 291 | 28-Jun-94 18:35 | 0.999724 | 0.204943 | 0.228395 |
| 292 | 28-Jun-94 18:40 | 0.999710 | 0.198852 | 0.222124 |
| 293 | 28-Jun-94 18:45 | 0.999699 | 0.193733 | 0.216633 |
| 294 | 28-Jun-94 18:50 | 0.999664 | 0.190910 | 0.213094 |
| 295 | 28-Jun-94 18:55 | 0.999611 | 0.191186 | 0.212529 |
| 296 | 28-Jun-94 19:00 | 0.999615 | 0.190831 | 0.211381 |
| 297 | 28-Jun-94 19:05 | 0.999635 | 0.189036 | 0.208911 |
| 298 | 28-Jun-94 19:10 | 0.999587 | 0.189628 | 0.208798 |
| 299 | 28-Jun-94 19:15 | 0.999554 | 0.191531 | 0.210116 |
| 300 | 28-Jun-94 19:20 | 0.999539 | 0.193672 | 0.211732 |
| 301 | 28-Jun-94 19:25 | 0.999573 | 0.193631 | 0.211075 |
| 302 | 28-Jun-94 19:30 | 0.999572 | 0.193327 | 0.210189 |
| 303 | 28-Jun-94 19:35 | 0.999521 | 0.195046 | 0.211436 |
| 304 | 28-Jun-94 19:40 | 0.999506 | 0.196991 | 0.212961 |
| 305 | 28-Jun-94 19:45 | 0.999526 | 0.197591 | 0.213062 |
| 306 | 28-Jun-94 19:50 | 0.999587 | 0.195355 | 0.210494 |
| 307 | 28-Jun-94 19:55 | 0.999570 | 0.193714 | 0.208471 |
| 308 | 28-Jun-94 20:00 | 0.999579 | 0.191602 | 0.206054 |
| 309 | 28-Jun-94 20:05 | 0.999582 | 0.189290 | 0.203485 |
| 310 | 28-Jun-94 20:10 | 0.999554 | 0.187975 | 0.201809 |
| 311 | 28-Jun-94 20:15 | 0.999501 | 0.188412 | 0.201849 |
| 312 | 28-Jun-94 20:20 | 0.999501 | 0.188597 | 0.201649 |
| 313 | 28-Jun-94 20:25 | 0.999452 | 0.190213 | 0.202991 |
| 314 | 28-Jun-94 20:30 | 0.999423 | 0.192426 | 0.205030 |
| 315 | 28-Jun-94 20:35 | 0.999409 | 0.194704 | 0.207155 |
| 316 | 28-Jun-94 20:40 | 0.999411 | 0.196522 | 0.208761 |
| 317 | 28-Jun-94 20:45 | 0.999414 | 0.197906 | 0.209892 |
| 318 | 28-Jun-94 20:50 | 0.999419 | 0.198838 | 0.210541 |
| 319 | 28-Jun-94 20:55 | 0.999400 | 0.200036 | 0.211492 |
| 320 | 28-Jun-94 21:00 | 0.999411 | 0.200631 | 0.211806 |
| 321 | 28-Jun-94 21:05 | 0.999403 | 0.201229 | 0.212136 |
| 322 | 28-Jun-94 21:10 | 0.999369 | 0.202499 | 0.213201 |
| 323 | 28-Jun-94 21:15 | 0.999393 | 0.202864 | 0.213307 |
| 324 | 28-Jun-94 21:20 | 0.999294 | 0.205531 | 0.216036 |

Mass Point Leak Rate Analysis

Verification Phase

Watts Bar Nuclear Plant
Unit 1 - Startup

| <u>Rdg</u> | <u>Time</u> | <u>Norm Mass</u> | <u>MP Leak %/day</u> | <u>MP UCL %/day</u> |
|------------|-----------------|------------------|--------------------------|-------------------------|
| 325 | 28-Jun-94 21:25 | 0.999270 | 0.208425 | 0.219047 |
| 326 | 28-Jun-94 21:30 | 0.999265 | 0.211055 | 0.221727 |
| 327 | 28-Jun-94 21:35 | 0.999260 | 0.213461 | 0.224135 |
| 328 | 28-Jun-94 21:40 | 0.999225 | 0.216346 | 0.227133 |
| 329 | 28-Jun-94 21:45 | 0.999222 | 0.218926 | 0.229751 |
| 330 | 28-Jun-94 21:50 | 0.999197 | 0.221712 | 0.232625 |
| 331 | 28-Jun-94 21:55 | 0.999229 | 0.223457 | 0.234254 |
| 332 | 28-Jun-94 22:00 | 0.999248 | 0.224534 | 0.235141 |
| 333 | 28-Jun-94 22:05 | 0.999217 | 0.226013 | 0.236483 |
| 334 | 28-Jun-94 22:10 | 0.999205 | 0.227484 | 0.237822 |
| 335 | 28-Jun-94 22:15 | 0.999191 | 0.228978 | 0.239194 |
| 336 | 28-Jun-94 22:20 | 0.999193 | 0.230194 | 0.240259 |
| 337 | 28-Jun-94 22:25 | 0.999159 | 0.231828 | 0.241805 |
| 338 | 28-Jun-94 22:30 | 0.999141 | 0.233544 | 0.243450 |
| 339 | 28-Jun-94 22:35 | 0.999150 | 0.234852 | 0.244635 |
| 340 | 28-Jun-94 22:40 | 0.999135 | 0.236207 | 0.245876 |
| 341 | 28-Jun-94 22:45 | 0.999143 | 0.237194 | 0.246715 |
| 342 | 28-Jun-94 22:50 | 0.999125 | 0.238285 | 0.247673 |
| 343 | 28-Jun-94 22:55 | 0.999150 | 0.238753 | 0.247965 |
| 344 | 28-Jun-94 23:00 | 0.999129 | 0.239407 | 0.248460 |
| 345 | 28-Jun-94 23:05 | 0.999120 | 0.240027 | 0.248923 |
| 346 | 28-Jun-94 23:10 | 0.999101 | 0.240783 | 0.249538 |
| 347 | 28-Jun-94 23:15 | 0.999089 | 0.241551 | 0.250170 |
| 348 | 28-Jun-94 23:20 | 0.999089 | 0.242151 | 0.250626 |
| 349 | 28-Jun-94 23:25 | 0.999081 | 0.242722 | 0.251056 |
| 350 | 28-Jun-94 23:30 | 0.999072 | 0.243262 | 0.251457 |
| 351 | 28-Jun-94 23:35 | 0.999094 | 0.243336 | 0.251381 |

Total Time Leak Rate Analysis

Verification Phase

Watts Bar Nuclear Plant
Unit 1 - Startup

| <u>Rdg</u> | <u>Date / Time</u> | <u>TT Meas</u> <u>% / day</u> | <u>TT Calc</u> <u>% / day</u> | <u>TT UCL</u> <u>% / day</u> |
|------------|--------------------|----------------------------------|----------------------------------|---------------------------------|
| 243 | 6/28/94 14:28 | 0.000000 | 0.000000 | 0.000000 |
| 244 | 6/28/94 14:38 | -0.069530 | 0.000000 | 0.000000 |
| 245 | 6/28/94 14:45 | -0.158129 | -0.158129 | 0.000000 |
| 246 | 6/28/94 14:50 | -0.295658 | -0.278970 | 0.056578 |
| 247 | 6/28/94 14:55 | 0.124906 | -0.046220 | 0.982128 |
| 248 | 6/28/94 15:00 | -0.004333 | -0.008008 | 0.642487 |
| 249 | 6/28/94 15:05 | -0.003141 | 0.011842 | 0.504196 |
| 250 | 6/28/94 15:10 | 0.171032 | 0.100371 | 0.524554 |
| 251 | 6/28/94 15:15 | 0.196537 | 0.165385 | 0.532830 |
| 252 | 6/28/94 15:20 | 0.338065 | 0.259373 | 0.600505 |
| 253 | 6/28/94 15:25 | 0.322319 | 0.317642 | 0.625749 |
| 254 | 6/28/94 15:30 | 0.270748 | 0.341596 | 0.633454 |
| 255 | 6/28/94 15:35 | 0.248830 | 0.351381 | 0.638904 |
| 256 | 6/28/94 15:40 | 0.298957 | 0.370855 | 0.646968 |
| 257 | 6/28/94 15:45 | 0.245823 | 0.371160 | 0.650513 |
| 258 | 6/28/94 15:50 | 0.273250 | 0.376906 | 0.653078 |
| 259 | 6/28/94 15:55 | 0.314656 | 0.389944 | 0.658300 |
| 260 | 6/28/94 16:00 | 0.347440 | 0.406714 | 0.666301 |
| 261 | 6/28/94 16:05 | 0.255826 | 0.401167 | 0.667450 |
| 262 | 6/28/94 16:10 | 0.255907 | 0.395859 | 0.666338 |
| 263 | 6/28/94 16:15 | 0.275589 | 0.394500 | 0.664768 |
| 264 | 6/28/94 16:20 | 0.299953 | 0.397169 | 0.664242 |
| 265 | 6/28/94 16:25 | 0.290917 | 0.397473 | 0.662724 |
| 266 | 6/28/94 16:30 | 0.291269 | 0.397397 | 0.660897 |
| 267 | 6/28/94 16:35 | 0.293116 | 0.397314 | 0.658974 |
| 268 | 6/28/94 16:40 | 0.278139 | 0.394619 | 0.655864 |
| 269 | 6/28/94 16:45 | 0.297087 | 0.394727 | 0.653694 |
| 270 | 6/28/94 16:50 | 0.297111 | 0.394566 | 0.651399 |
| 271 | 6/28/94 16:55 | 0.283421 | 0.392337 | 0.648167 |
| 272 | 6/28/94 17:00 | 0.236610 | 0.384033 | 0.642805 |
| 273 | 6/28/94 17:05 | 0.242561 | 0.377247 | 0.637305 |
| 274 | 6/28/94 17:10 | 0.238346 | 0.370468 | 0.631417 |
| 275 | 6/28/94 17:15 | 0.223810 | 0.362517 | 0.624851 |
| 276 | 6/28/94 17:20 | 0.219922 | 0.354789 | 0.618027 |
| 277 | 6/28/94 17:25 | 0.220042 | 0.347716 | 0.611181 |
| 278 | 6/28/94 17:30 | 0.240054 | 0.343402 | 0.605383 |
| 279 | 6/28/94 17:35 | 0.218448 | 0.337113 | 0.598671 |
| 280 | 6/28/94 17:40 | 0.208885 | 0.330293 | 0.591617 |
| 281 | 6/28/94 17:45 | 0.259520 | 0.329116 | 0.587540 |
| 282 | 6/28/94 17:50 | 0.263105 | 0.328319 | 0.583828 |
| 283 | 6/28/94 17:55 | 0.233152 | 0.324639 | 0.578434 |

Total Time Leak Rate Analysis

Verification Phase

Watts Bar Nuclear Plant
Unit 1 - Startup

| <u>Rdg</u> | <u>Date / Time</u> | <u>TT Meas</u> <u>% / day</u> | <u>TT Calc</u> <u>% / day</u> | <u>TT UCL</u> <u>% / day</u> |
|------------|--------------------|----------------------------------|----------------------------------|---------------------------------|
| 284 | 6/28/94 18:00 | 0.209224 | 0.318950 | 0.572033 |
| 285 | 6/28/94 18:05 | 0.229468 | 0.315534 | 0.566807 |
| 286 | 6/28/94 18:10 | 0.209296 | 0.310508 | 0.560725 |
| 287 | 6/28/94 18:15 | 0.183143 | 0.303526 | 0.553716 |
| 288 | 6/28/94 18:20 | 0.157594 | 0.294833 | 0.545962 |
| 289 | 6/28/94 18:25 | 0.163388 | 0.287232 | 0.538479 |
| 290 | 6/28/94 18:30 | 0.175335 | 0.281131 | 0.531604 |
| 291 | 6/28/94 18:35 | 0.161073 | 0.274290 | 0.524356 |
| 292 | 6/28/94 18:40 | 0.165636 | 0.268249 | 0.517457 |
| 293 | 6/28/94 18:45 | 0.168767 | 0.262840 | 0.510889 |
| 294 | 6/28/94 18:50 | 0.184512 | 0.258970 | 0.505260 |
| 295 | 6/28/94 18:55 | 0.209735 | 0.257219 | 0.501183 |
| 296 | 6/28/94 19:00 | 0.203877 | 0.255133 | 0.496921 |
| 297 | 6/28/94 19:05 | 0.189887 | 0.252161 | 0.492079 |
| 298 | 6/28/94 19:10 | 0.210755 | 0.250830 | 0.488521 |
| 299 | 6/28/94 19:15 | 0.223625 | 0.250460 | 0.485834 |
| 300 | 6/28/94 19:20 | 0.227272 | 0.250349 | 0.483443 |
| 301 | 6/28/94 19:25 | 0.207010 | 0.248870 | 0.479968 |
| 302 | 6/28/94 19:30 | 0.204079 | 0.247272 | 0.476454 |
| 303 | 6/28/94 19:35 | 0.224473 | 0.247084 | 0.474171 |
| 304 | 6/28/94 19:40 | 0.228062 | 0.247121 | 0.472147 |
| 305 | 6/28/94 19:45 | 0.215154 | 0.246334 | 0.469458 |
| 306 | 6/28/94 19:50 | 0.184788 | 0.243698 | 0.465391 |
| 307 | 6/28/94 19:55 | 0.189306 | 0.241471 | 0.461650 |
| 308 | 6/28/94 20:00 | 0.182511 | 0.238945 | 0.457727 |
| 309 | 6/28/94 20:05 | 0.178309 | 0.236296 | 0.453750 |
| 310 | 6/28/94 20:10 | 0.187647 | 0.234319 | 0.450289 |
| 311 | 6/28/94 20:15 | 0.206763 | 0.233535 | 0.447830 |
| 312 | 6/28/94 20:20 | 0.203954 | 0.232626 | 0.445303 |
| 313 | 6/28/94 20:25 | 0.221062 | 0.232712 | 0.443704 |
| 314 | 6/28/94 20:30 | 0.229472 | 0.233253 | 0.442581 |
| 315 | 6/28/94 20:35 | 0.231932 | 0.233898 | 0.441601 |
| 316 | 6/28/94 20:40 | 0.227928 | 0.234296 | 0.440416 |
| 317 | 6/28/94 20:45 | 0.223820 | 0.234444 | 0.439024 |
| 318 | 6/28/94 20:50 | 0.219051 | 0.234336 | 0.437431 |
| 319 | 6/28/94 20:55 | 0.223157 | 0.234440 | 0.436066 |
| 320 | 6/28/94 21:00 | 0.216114 | 0.234176 | 0.434394 |
| 321 | 6/28/94 21:05 | 0.216554 | 0.233944 | 0.432781 |
| 322 | 6/28/94 21:10 | 0.225986 | 0.234184 | 0.431636 |
| 323 | 6/28/94 21:15 | 0.214626 | 0.233853 | 0.429990 |
| 324 | 6/28/94 21:20 | 0.246608 | 0.235081 | 0.429898 |

Total Time Leak Rate Analysis

Verification Phase

Watts Bar Nuclear Plant
Unit 1 - Startup

| <u>Rdg</u> | <u>Date / Time</u> | <u>TT Meas</u> <u>% / day</u> | <u>TT Calc</u> <u>% / day</u> | <u>TT UCL</u> <u>% / day</u> |
|------------|--------------------|----------------------------------|----------------------------------|---------------------------------|
| 325 | 6/28/94 21:25 | 0.251915 | 0.236509 | 0.430047 |
| 326 | 6/28/94 21:30 | 0.250518 | 0.237807 | 0.430080 |
| 327 | 6/28/94 21:35 | 0.249442 | 0.239000 | 0.430027 |
| 328 | 6/28/94 21:40 | 0.258320 | 0.240549 | 0.430382 |
| 329 | 6/28/94 21:45 | 0.256211 | 0.241935 | 0.430582 |
| 330 | 6/28/94 21:50 | 0.261398 | 0.243497 | 0.430996 |
| 331 | 6/28/94 21:55 | 0.248107 | 0.244400 | 0.430731 |
| 332 | 6/28/94 22:00 | 0.239442 | 0.244881 | 0.430068 |
| 333 | 6/28/94 22:05 | 0.246494 | 0.245650 | 0.429710 |
| 334 | 6/28/94 22:10 | 0.247598 | 0.246432 | 0.429385 |
| 335 | 6/28/94 22:15 | 0.249195 | 0.247249 | 0.429115 |
| 336 | 6/28/94 22:20 | 0.246067 | 0.247899 | 0.428697 |
| 337 | 6/28/94 22:25 | 0.253778 | 0.248844 | 0.428596 |
| 338 | 6/28/94 22:30 | 0.256478 | 0.249866 | 0.428592 |
| 339 | 6/28/94 22:35 | 0.251294 | 0.250632 | 0.428343 |
| 340 | 6/28/94 22:40 | 0.253171 | 0.251443 | 0.428158 |
| 341 | 6/28/94 22:45 | 0.248242 | 0.252024 | 0.427760 |
| 342 | 6/28/94 22:50 | 0.250833 | 0.252685 | 0.427456 |
| 343 | 6/28/94 22:55 | 0.241223 | 0.252940 | 0.426779 |
| 344 | 6/28/94 23:00 | 0.244841 | 0.253340 | 0.426256 |
| 345 | 6/28/94 23:05 | 0.244847 | 0.253694 | 0.425698 |
| 346 | 6/28/94 23:10 | 0.247808 | 0.254159 | 0.425264 |
| 347 | 6/28/94 23:15 | 0.248685 | 0.254639 | 0.424857 |
| 348 | 6/28/94 23:20 | 0.246375 | 0.255013 | 0.424363 |
| 349 | 6/28/94 23:25 | 0.246424 | 0.255374 | 0.423870 |
| 350 | 6/28/94 23:30 | 0.246382 | 0.255720 | 0.423376 |
| 351 | 6/28/94 23:35 | 0.238371 | 0.255757 | 0.422611 |

Containment Calculated Values Verification Phase

Watts Bar Nuclear Plant
Unit 1 - Startup

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|--------------------|-------------|-------------|--------------------|--------------|
| 243 | 14:28:31 | Upper Containment | 96047.29 | 82.992 | 0.0677 | 29.2813 |
| | | Lower Containment | 55601.58 | 83.587 | 0.0656 | 29.2847 |
| | | Ice Condenser | 25581.62 | 26.69 | 0.0185 | 29.2855 |
| | | TOTAL | 177230.49 | | | |
| 244 | 14:38:32 | Upper Containment | 96047.55 | 82.982 | 0.0678 | 29.281 |
| | | Lower Containment | 55603.37 | 83.569 | 0.0656 | 29.2846 |
| | | Ice Condenser | 25580.43 | 26.708 | 0.0185 | 29.2852 |
| | | TOTAL | 177231.35 | | | |
| 245 | 14:45:32 | Upper Containment | 96050.14 | 82.956 | 0.0677 | 29.2803 |
| | | Lower Containment | 55602.34 | 83.568 | 0.0655 | 29.284 |
| | | Ice Condenser | 25581.32 | 26.682 | 0.0185 | 29.2847 |
| | | TOTAL | 177233.8 | | | |
| 246 | 14:50:32 | Upper Containment | 96054.38 | 82.939 | 0.0677 | 29.2806 |
| | | Lower Containment | 55603.43 | 83.559 | 0.0655 | 29.2841 |
| | | Ice Condenser | 25580.69 | 26.695 | 0.0185 | 29.2847 |
| | | TOTAL | 177238.5 | | | |
| 247 | 14:55:32 | Upper Containment | 96041.71 | 82.993 | 0.0676 | 29.2796 |
| | | Lower Containment | 55602.91 | 83.551 | 0.0654 | 29.2832 |
| | | Ice Condenser | 25581.72 | 26.663 | 0.0185 | 29.284 |
| | | TOTAL | 177226.34 | | | |
| 248 | 15:00:32 | Upper Containment | 96046.9 | 82.96 | 0.0677 | 29.2795 |
| | | Lower Containment | 55601.7 | 83.558 | 0.0654 | 29.2829 |
| | | Ice Condenser | 25582.05 | 26.656 | 0.0185 | 29.2839 |
| | | TOTAL | 177230.66 | | | |
| 249 | 15:05:33 | Upper Containment | 96044.65 | 82.971 | 0.0676 | 29.2793 |
| | | Lower Containment | 55602.59 | 83.552 | 0.0653 | 29.283 |
| | | Ice Condenser | 25583.4 | 26.625 | 0.0185 | 29.2836 |
| | | TOTAL | 177230.63 | | | |
| 250 | 15:10:33 | Upper Containment | 96043.01 | 82.954 | 0.0675 | 29.2778 |
| | | Lower Containment | 55600.14 | 83.541 | 0.0653 | 29.2811 |
| | | Ice Condenser | 25578.5 | 26.693 | 0.0185 | 29.2821 |
| | | TOTAL | 177221.64 | | | |
| 251 | 15:15:33 | Upper Containment | 96040.72 | 82.962 | 0.0675 | 29.2775 |
| | | Lower Containment | 55599.42 | 83.555 | 0.0653 | 29.2815 |
| | | Ice Condenser | 25578.97 | 26.679 | 0.0185 | 29.2818 |
| | | TOTAL | 177219.11 | | | |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|--------------------|-------------|-------------|--------------------|--------------|
| 252 | 15:20:33 | Upper Containment | 96033.48 | 82.987 | 0.0674 | 29.2765 |
| | | Lower Containment | 55597.72 | 83.545 | 0.0652 | 29.28 |
| | | Ice Condenser | 25577.64 | 26.688 | 0.0185 | 29.2808 |
| | | TOTAL | 177208.84 | | | |
| 253 | 15:25:33 | Upper Containment | 96035.17 | 82.967 | 0.0673 | 29.2759 |
| | | Lower Containment | 55596.79 | 83.545 | 0.0652 | 29.2795 |
| | | Ice Condenser | 25575.91 | 26.709 | 0.0185 | 29.2801 |
| | | TOTAL | 177207.87 | | | |
| 254 | 15:30:33 | Upper Containment | 96037.98 | 82.94 | 0.0673 | 29.2752 |
| | | Lower Containment | 55595.75 | 83.543 | 0.0652 | 29.2788 |
| | | Ice Condenser | 25576.09 | 26.697 | 0.0185 | 29.2796 |
| | | TOTAL | 177209.82 | | | |
| 255 | 15:35:34 | Upper Containment | 96040.76 | 82.916 | 0.0673 | 29.2748 |
| | | Lower Containment | 55595.32 | 83.537 | 0.0652 | 29.2783 |
| | | Ice Condenser | 25573.88 | 26.733 | 0.0185 | 29.2792 |
| | | TOTAL | 177209.96 | | | |
| 256 | 15:40:34 | Upper Containment | 96033.71 | 82.947 | 0.0673 | 29.2743 |
| | | Lower Containment | 55595.42 | 83.535 | 0.0651 | 29.2781 |
| | | Ice Condenser | 25574.85 | 26.704 | 0.0185 | 29.2786 |
| | | TOTAL | 177203.98 | | | |
| 257 | 15:45:34 | Upper Containment | 96035.8 | 82.923 | 0.0673 | 29.2736 |
| | | Lower Containment | 55594.53 | 83.529 | 0.0651 | 29.2773 |
| | | Ice Condenser | 25576.85 | 26.656 | 0.0185 | 29.278 |
| | | TOTAL | 177207.18 | | | |
| 258 | 15:50:34 | Upper Containment | 96034.56 | 82.919 | 0.0672 | 29.273 |
| | | Lower Containment | 55594.47 | 83.515 | 0.0651 | 29.2765 |
| | | Ice Condenser | 25573.87 | 26.702 | 0.0185 | 29.2774 |
| | | TOTAL | 177202.9 | | | |
| 259 | 15:55:34 | Upper Containment | 96029.39 | 82.952 | 0.0672 | 29.2732 |
| | | Lower Containment | 55594.4 | 83.517 | 0.0652 | 29.2767 |
| | | Ice Condenser | 25572.99 | 26.722 | 0.0185 | 29.2776 |
| | | TOTAL | 177196.78 | | | |
| 260 | 16:00:34 | Upper Containment | 96025.78 | 82.969 | 0.0671 | 29.273 |
| | | Lower Containment | 55593.56 | 83.525 | 0.0651 | 29.2766 |
| | | Ice Condenser | 25571.79 | 26.742 | 0.0185 | 29.2774 |
| | | TOTAL | 177191.13 | | | |
| 261 | 16:05:35 | Upper Containment | 96034.04 | 82.918 | 0.0671 | 29.2727 |
| | | Lower Containment | 55593.76 | 83.517 | 0.0651 | 29.2763 |
| | | Ice Condenser | 25572.13 | 26.733 | 0.0185 | 29.2772 |
| | | TOTAL | 177199.93 | | | |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|--------------------|-------------|-------------|--------------------|--------------|
| 262 | 16:10:35 | Upper Containment | 96033.39 | 82.92 | 0.0672 | 29.2727 |
| | | Lower Containment | 55594.06 | 83.518 | 0.0649 | 29.2763 |
| | | Ice Condenser | 25570.9 | 26.75 | 0.0185 | 29.2768 |
| | | TOTAL | 177198.34 | | | |
| 263 | 16:15:35 | Upper Containment | 96030.26 | 82.931 | 0.067 | 29.2721 |
| | | Lower Containment | 55593.15 | 83.513 | 0.065 | 29.2757 |
| | | Ice Condenser | 25570.76 | 26.748 | 0.0185 | 29.2766 |
| | | TOTAL | 177194.18 | | | |
| 264 | 16:20:35 | Upper Containment | 96030.41 | 82.926 | 0.0671 | 29.272 |
| | | Lower Containment | 55592.77 | 83.511 | 0.065 | 29.2754 |
| | | Ice Condenser | 25565.94 | 26.828 | 0.0185 | 29.2758 |
| | | TOTAL | 177189.12 | | | |
| 265 | 16:25:35 | Upper Containment | 96030.12 | 82.906 | 0.0669 | 29.2707 |
| | | Lower Containment | 55591.07 | 83.511 | 0.0648 | 29.2743 |
| | | Ice Condenser | 25567.38 | 26.785 | 0.0185 | 29.2749 |
| | | TOTAL | 177188.57 | | | |
| 266 | 16:30:35 | Upper Containment | 96026.37 | 82.917 | 0.0669 | 29.2702 |
| | | Lower Containment | 55591.04 | 83.501 | 0.0649 | 29.2737 |
| | | Ice Condenser | 25569.32 | 26.738 | 0.0185 | 29.2743 |
| | | TOTAL | 177186.73 | | | |
| 267 | 16:35:36 | Upper Containment | 96024.42 | 82.922 | 0.0669 | 29.2698 |
| | | Lower Containment | 55591.64 | 83.498 | 0.0648 | 29.2738 |
| | | Ice Condenser | 25568.58 | 26.747 | 0.0185 | 29.274 |
| | | TOTAL | 177184.64 | | | |
| 268 | 16:40:36 | Upper Containment | 96025.16 | 82.911 | 0.067 | 29.2695 |
| | | Lower Containment | 55590.48 | 83.498 | 0.0647 | 29.2731 |
| | | Ice Condenser | 25569.64 | 26.725 | 0.0185 | 29.2739 |
| | | TOTAL | 177185.28 | | | |
| 269 | 16:45:36 | Upper Containment | 96019.35 | 82.943 | 0.0669 | 29.2694 |
| | | Lower Containment | 55590.59 | 83.493 | 0.0647 | 29.2729 |
| | | Ice Condenser | 25570.43 | 26.707 | 0.0185 | 29.2737 |
| | | TOTAL | 177180.37 | | | |
| 270 | 16:50:36 | Upper Containment | 96020.99 | 82.927 | 0.0669 | 29.269 |
| | | Lower Containment | 55589.69 | 83.492 | 0.0647 | 29.2724 |
| | | Ice Condenser | 25567.85 | 26.75 | 0.0185 | 29.2733 |
| | | TOTAL | 177178.53 | | | |
| 271 | 16:55:36 | Upper Containment | 96021.18 | 82.923 | 0.0669 | 29.2689 |
| | | Lower Containment | 55590.04 | 83.492 | 0.0647 | 29.2726 |
| | | Ice Condenser | 25567.97 | 26.745 | 0.0185 | 29.2732 |
| | | TOTAL | 177179.18 | | | |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|--------------------|-------------|-------------|--------------------|--------------|
| 272 | 17:00:36 | Upper Containment | 96026.1 | 82.895 | 0.0668 | 29.2688 |
| | | Lower Containment | 55589.93 | 83.483 | 0.0646 | 29.272 |
| | | Ice Condenser | 25570.18 | 26.702 | 0.0185 | 29.2731 |
| | | TOTAL | 177186.2 | | | |
| 273 | 17:05:37 | Upper Containment | 96024.94 | 82.899 | 0.0668 | 29.2686 |
| | | Lower Containment | 55589.36 | 83.492 | 0.0647 | 29.2722 |
| | | Ice Condenser | 25569.28 | 26.718 | 0.0185 | 29.2731 |
| | | TOTAL | 177183.59 | | | |
| 274 | 17:10:37 | Upper Containment | 96023.43 | 82.905 | 0.0667 | 29.2684 |
| | | Lower Containment | 55589.95 | 83.48 | 0.0647 | 29.2719 |
| | | Ice Condenser | 25569.55 | 26.714 | 0.0185 | 29.2731 |
| | | TOTAL | 177182.94 | | | |
| 275 | 17:15:37 | Upper Containment | 96024.52 | 82.904 | 0.0665 | 29.2684 |
| | | Lower Containment | 55590.57 | 83.482 | 0.0646 | 29.2722 |
| | | Ice Condenser | 25569.38 | 26.71 | 0.0185 | 29.2727 |
| | | TOTAL | 177184.46 | | | |
| 276 | 17:20:37 | Upper Containment | 96026.01 | 82.885 | 0.0666 | 29.268 |
| | | Lower Containment | 55589.4 | 83.485 | 0.0646 | 29.2717 |
| | | Ice Condenser | 25568.49 | 26.722 | 0.0185 | 29.2724 |
| | | TOTAL | 177183.91 | | | |
| 277 | 17:25:37 | Upper Containment | 96020.99 | 82.907 | 0.0666 | 29.2676 |
| | | Lower Containment | 55591.35 | 83.472 | 0.0645 | 29.272 |
| | | Ice Condenser | 25570.19 | 26.683 | 0.0185 | 29.272 |
| | | TOTAL | 177182.53 | | | |
| 278 | 17:30:37 | Upper Containment | 96019.4 | 82.907 | 0.0666 | 29.2672 |
| | | Lower Containment | 55588.38 | 83.479 | 0.0645 | 29.2708 |
| | | Ice Condenser | 25568.91 | 26.699 | 0.0185 | 29.2715 |
| | | TOTAL | 177176.69 | | | |
| 279 | 17:35:38 | Upper Containment | 96022.8 | 82.882 | 0.0664 | 29.2667 |
| | | Lower Containment | 55589.77 | 83.463 | 0.0645 | 29.2707 |
| | | Ice Condenser | 25567.61 | 26.716 | 0.0185 | 29.271 |
| | | TOTAL | 177180.18 | | | |
| 280 | 17:40:38 | Upper Containment | 96023.27 | 82.877 | 0.0664 | 29.2665 |
| | | Lower Containment | 55588.61 | 83.464 | 0.0645 | 29.2701 |
| | | Ice Condenser | 25569.22 | 26.685 | 0.0185 | 29.271 |
| | | TOTAL | 177181.1 | | | |
| 281 | 17:45:38 | Upper Containment | 96014.27 | 82.907 | 0.0664 | 29.2654 |
| | | Lower Containment | 55586.64 | 83.466 | 0.0644 | 29.2691 |
| | | Ice Condenser | 25566.62 | 26.714 | 0.0185 | 29.2698 |
| | | TOTAL | 177167.53 | | | |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|--------------------|-------------|-------------|--------------------|--------------|
| 282 | 17:50:38 | Upper Containment | 96013.56 | 82.915 | 0.0665 | 29.2657 |
| | | Lower Containment | 55587.15 | 83.469 | 0.0643 | 29.2694 |
| | | Ice Condenser | 25564.33 | 26.766 | 0.0185 | 29.2703 |
| | | TOTAL | 177165.04 | | | |
| 283 | 17:55:38 | Upper Containment | 96020.42 | 82.891 | 0.0664 | 29.2664 |
| | | Lower Containment | 55588.57 | 83.462 | 0.0643 | 29.2698 |
| | | Ice Condenser | 25562.07 | 26.816 | 0.0185 | 29.2707 |
| | | TOTAL | 177171.06 | | | |
| 284 | 18:00:38 | Upper Containment | 96023.66 | 82.88 | 0.0662 | 29.2666 |
| | | Lower Containment | 55590.25 | 83.46 | 0.0643 | 29.2706 |
| | | Ice Condenser | 25561.96 | 26.823 | 0.0185 | 29.271 |
| | | TOTAL | 177175.87 | | | |
| 285 | 18:05:39 | Upper Containment | 96019.5 | 82.897 | 0.0663 | 29.2663 |
| | | Lower Containment | 55589.37 | 83.453 | 0.0642 | 29.2697 |
| | | Ice Condenser | 25560.3 | 26.849 | 0.0185 | 29.2707 |
| | | TOTAL | 177169.17 | | | |
| 286 | 18:10:39 | Upper Containment | 96023.03 | 82.88 | 0.0663 | 29.2665 |
| | | Lower Containment | 55590.52 | 83.456 | 0.0643 | 29.2705 |
| | | Ice Condenser | 25559.72 | 26.863 | 0.0185 | 29.2708 |
| | | TOTAL | 177173.27 | | | |
| 287 | 18:15:39 | Upper Containment | 96024.69 | 82.874 | 0.0663 | 29.2667 |
| | | Lower Containment | 55590.18 | 83.453 | 0.0642 | 29.2701 |
| | | Ice Condenser | 25564.42 | 26.779 | 0.0185 | 29.2712 |
| | | TOTAL | 177179.29 | | | |
| 288 | 18:20:39 | Upper Containment | 96024.82 | 82.885 | 0.0663 | 29.2673 |
| | | Lower Containment | 55591.97 | 83.447 | 0.0642 | 29.2707 |
| | | Ice Condenser | 25568.67 | 26.709 | 0.0185 | 29.2718 |
| | | TOTAL | 177185.47 | | | |
| 289 | 18:25:39 | Upper Containment | 96024.86 | 82.86 | 0.0662 | 29.2659 |
| | | Lower Containment | 55590.28 | 83.449 | 0.0642 | 29.2699 |
| | | Ice Condenser | 25567.66 | 26.706 | 0.0185 | 29.2705 |
| | | TOTAL | 177182.81 | | | |
| 290 | 18:30:39 | Upper Containment | 96021.54 | 82.878 | 0.0662 | 29.2658 |
| | | Lower Containment | 55589.98 | 83.443 | 0.0642 | 29.2694 |
| | | Ice Condenser | 25566.72 | 26.72 | 0.0185 | 29.2702 |
| | | TOTAL | 177178.24 | | | |
| 291 | 18:35:40 | Upper Containment | 96025.4 | 82.851 | 0.0663 | 29.2656 |
| | | Lower Containment | 55590.54 | 83.443 | 0.0641 | 29.2696 |
| | | Ice Condenser | 25565.56 | 26.737 | 0.0185 | 29.2699 |
| | | TOTAL | 177181.49 | | | |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|--------------------|-------------|-------------|--------------------|--------------|
| 292 | 18:40:40 | Upper Containment | 96023.81 | 82.87 | 0.0662 | 29.2661 |
| | | Lower Containment | 55590.74 | 83.442 | 0.0641 | 29.2697 |
| | | Ice Condenser | 25564.55 | 26.763 | 0.0185 | 29.2704 |
| | | TOTAL | 177179.09 | | | |
| 293 | 18:45:40 | Upper Containment | 96023.9 | 82.876 | 0.066 | 29.2663 |
| | | Lower Containment | 55590.96 | 83.438 | 0.0641 | 29.2696 |
| | | Ice Condenser | 25562.22 | 26.818 | 0.0185 | 29.271 |
| | | TOTAL | 177177.08 | | | |
| 294 | 18:50:40 | Upper Containment | 96020.08 | 82.868 | 0.066 | 29.2647 |
| | | Lower Containment | 55590.62 | 83.418 | 0.064 | 29.2682 |
| | | Ice Condenser | 25560.26 | 26.818 | 0.0185 | 29.2688 |
| | | TOTAL | 177170.96 | | | |
| 295 | 18:55:40 | Upper Containment | 96013.8 | 82.875 | 0.0659 | 29.263 |
| | | Lower Containment | 55588.03 | 83.417 | 0.0639 | 29.2667 |
| | | Ice Condenser | 25559.69 | 26.807 | 0.0185 | 29.2674 |
| | | TOTAL | 177161.53 | | | |
| 296 | 19:00:40 | Upper Containment | 96015.67 | 82.854 | 0.0659 | 29.2625 |
| | | Lower Containment | 55585.66 | 83.427 | 0.0641 | 29.2661 |
| | | Ice Condenser | 25560.87 | 26.777 | 0.0185 | 29.267 |
| | | TOTAL | 177162.2 | | | |
| 297 | 19:05:41 | Upper Containment | 96018.24 | 82.839 | 0.0659 | 29.2625 |
| | | Lower Containment | 55586.49 | 83.419 | 0.064 | 29.2661 |
| | | Ice Condenser | 25560.98 | 26.774 | 0.0185 | 29.2669 |
| | | TOTAL | 177165.72 | | | |
| 298 | 19:10:41 | Upper Containment | 96013.77 | 82.844 | 0.0659 | 29.2613 |
| | | Lower Containment | 55584.79 | 83.418 | 0.0639 | 29.2651 |
| | | Ice Condenser | 25558.74 | 26.797 | 0.0185 | 29.2658 |
| | | TOTAL | 177157.3 | | | |
| 299 | 19:15:41 | Upper Containment | 96009.95 | 82.855 | 0.0659 | 29.2608 |
| | | Lower Containment | 55583.27 | 83.418 | 0.0639 | 29.2643 |
| | | Ice Condenser | 25558.23 | 26.798 | 0.0185 | 29.2652 |
| | | TOTAL | 177151.45 | | | |
| 300 | 19:20:41 | Upper Containment | 96007.01 | 82.865 | 0.0659 | 29.2604 |
| | | Lower Containment | 55583.42 | 83.413 | 0.0639 | 29.2641 |
| | | Ice Condenser | 25558.33 | 26.79 | 0.0185 | 29.2649 |
| | | TOTAL | 177148.77 | | | |
| 301 | 19:25:41 | Upper Containment | 96011.86 | 82.836 | 0.0657 | 29.2601 |
| | | Lower Containment | 55582.91 | 83.413 | 0.064 | 29.2639 |
| | | Ice Condenser | 25560.01 | 26.751 | 0.0185 | 29.2644 |
| | | TOTAL | 177154.78 | | | |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|--------------------|-------------|-------------|--------------------|--------------|
| 302 | 19:30:41 | Upper Containment | 96011.56 | 82.824 | 0.0659 | 29.2596 |
| | | Lower Containment | 55583.4 | 83.405 | 0.0639 | 29.2636 |
| | | Ice Condenser | 25559.63 | 26.753 | 0.0185 | 29.2641 |
| | | TOTAL | 177154.59 | | | |
| 303 | 19:35:42 | Upper Containment | 96007.91 | 82.807 | 0.0659 | 29.2575 |
| | | Lower Containment | 55578.77 | 83.404 | 0.0638 | 29.2611 |
| | | Ice Condenser | 25558.94 | 26.728 | 0.0185 | 29.2618 |
| | | TOTAL | 177145.62 | | | |
| 304 | 19:40:42 | Upper Containment | 95999.66 | 82.86 | 0.0657 | 29.2577 |
| | | Lower Containment | 55579.02 | 83.407 | 0.0639 | 29.2614 |
| | | Ice Condenser | 25564.19 | 26.631 | 0.0185 | 29.262 |
| | | TOTAL | 177142.86 | | | |
| 305 | 19:45:42 | Upper Containment | 96004.22 | 82.829 | 0.0658 | 29.2575 |
| | | Lower Containment | 55578.31 | 83.407 | 0.0639 | 29.2611 |
| | | Ice Condenser | 25563.98 | 26.635 | 0.0185 | 29.262 |
| | | TOTAL | 177146.5 | | | |
| 306 | 19:50:42 | Upper Containment | 96007.16 | 82.825 | 0.0658 | 29.2582 |
| | | Lower Containment | 55580.35 | 83.408 | 0.0639 | 29.2621 |
| | | Ice Condenser | 25569.7 | 26.539 | 0.0185 | 29.2628 |
| | | TOTAL | 177157.22 | | | |
| 307 | 19:55:42 | Upper Containment | 96004.36 | 82.838 | 0.0659 | 29.2581 |
| | | Lower Containment | 55580.16 | 83.401 | 0.0638 | 29.2616 |
| | | Ice Condenser | 25569.74 | 26.532 | 0.0185 | 29.2624 |
| | | TOTAL | 177154.26 | | | |
| 308 | 20:00:42 | Upper Containment | 96003.76 | 82.847 | 0.0657 | 29.2583 |
| | | Lower Containment | 55581.29 | 83.397 | 0.0639 | 29.2621 |
| | | Ice Condenser | 25570.82 | 26.517 | 0.0185 | 29.2627 |
| | | TOTAL | 177155.87 | | | |
| 309 | 20:05:43 | Upper Containment | 96006.74 | 82.829 | 0.0656 | 29.2581 |
| | | Lower Containment | 55579.81 | 83.404 | 0.0639 | 29.2617 |
| | | Ice Condenser | 25569.94 | 26.531 | 0.0185 | 29.2626 |
| | | TOTAL | 177156.49 | | | |
| 310 | 20:10:43 | Upper Containment | 96002.51 | 82.824 | 0.0657 | 29.2566 |
| | | Lower Containment | 55580.14 | 83.388 | 0.0636 | 29.2607 |
| | | Ice Condenser | 25568.81 | 26.525 | 0.0185 | 29.2609 |
| | | TOTAL | 177151.46 | | | |
| 311 | 20:15:43 | Upper Containment | 95996.17 | 82.837 | 0.0656 | 29.2553 |
| | | Lower Containment | 55577.94 | 83.377 | 0.0636 | 29.259 |
| | | Ice Condenser | 25568.02 | 26.52 | 0.0185 | 29.2597 |
| | | TOTAL | 177142.14 | | | |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|--------------------|-------------|-------------|--------------------|--------------|
| 312 | 20:20:43 | Upper Containment | 95999.01 | 82.81 | 0.0656 | 29.2547 |
| | | Lower Containment | 55576.75 | 83.38 | 0.0636 | 29.2585 |
| | | Ice Condenser | 25566.32 | 26.54 | 0.0185 | 29.259 |
| | | TOTAL | 177142.08 | | | |
| 313 | 20:25:43 | Upper Containment | 95993.41 | 82.825 | 0.0656 | 29.2538 |
| | | Lower Containment | 55575.65 | 83.373 | 0.0637 | 29.2576 |
| | | Ice Condenser | 25564.24 | 26.568 | 0.0185 | 29.2583 |
| | | TOTAL | 177133.31 | | | |
| 314 | 20:30:43 | Upper Containment | 95993.19 | 82.809 | 0.0655 | 29.2528 |
| | | Lower Containment | 55573.48 | 83.375 | 0.0636 | 29.2565 |
| | | Ice Condenser | 25561.53 | 26.601 | 0.0185 | 29.2572 |
| | | TOTAL | 177128.2 | | | |
| 315 | 20:35:44 | Upper Containment | 95992.39 | 82.798 | 0.0655 | 29.2519 |
| | | Lower Containment | 55571.62 | 83.374 | 0.0636 | 29.2555 |
| | | Ice Condenser | 25561.65 | 26.585 | 0.0185 | 29.2563 |
| | | TOTAL | 177125.67 | | | |
| 316 | 20:40:46 | Upper Containment | 95987.7 | 82.823 | 0.0654 | 29.2518 |
| | | Lower Containment | 55571.94 | 83.373 | 0.0636 | 29.2556 |
| | | Ice Condenser | 25566.42 | 26.49 | 0.0185 | 29.2561 |
| | | TOTAL | 177126.06 | | | |
| 317 | 20:45:44 | Upper Containment | 95990.33 | 82.798 | 0.0655 | 29.2513 |
| | | Lower Containment | 55571 | 83.371 | 0.0635 | 29.2549 |
| | | Ice Condenser | 25565.25 | 26.505 | 0.0185 | 29.2556 |
| | | TOTAL | 177126.58 | | | |
| 318 | 20:50:44 | Upper Containment | 95989.24 | 82.799 | 0.0653 | 29.2509 |
| | | Lower Containment | 55570.08 | 83.367 | 0.0637 | 29.2543 |
| | | Ice Condenser | 25568.13 | 26.443 | 0.0185 | 29.2552 |
| | | TOTAL | 177127.44 | | | |
| 319 | 20:55:44 | Upper Containment | 95986.24 | 82.802 | 0.0653 | 29.2501 |
| | | Lower Containment | 55570.05 | 83.36 | 0.0635 | 29.2538 |
| | | Ice Condenser | 25567.85 | 26.436 | 0.0185 | 29.2545 |
| | | TOTAL | 177124.14 | | | |
| 320 | 21:00:44 | Upper Containment | 95987.82 | 82.793 | 0.0653 | 29.2501 |
| | | Lower Containment | 55569.76 | 83.362 | 0.0635 | 29.2537 |
| | | Ice Condenser | 25568.58 | 26.422 | 0.0185 | 29.2545 |
| | | TOTAL | 177126.17 | | | |
| 321 | 21:05:45 | Upper Containment | 95985.31 | 82.806 | 0.0651 | 29.2499 |
| | | Lower Containment | 55568.84 | 83.366 | 0.0635 | 29.2535 |
| | | Ice Condenser | 25570.47 | 26.386 | 0.0185 | 29.2545 |
| | | TOTAL | 177124.62 | | | |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|--------------------|-------------|-------------|--------------------|--------------|
| 322 | 21:10:45 | Upper Containment | 95981.02 | 82.802 | 0.0652 | 29.2484 |
| | | Lower Containment | 55567.85 | 83.348 | 0.0634 | 29.2519 |
| | | Ice Condenser | 25569.74 | 26.369 | 0.0185 | 29.2526 |
| | | TOTAL | 177118.62 | | | |
| 323 | 21:15:45 | Upper Containment | 95988.02 | 82.753 | 0.0652 | 29.2479 |
| | | Lower Containment | 55566.45 | 83.353 | 0.0634 | 29.2514 |
| | | Ice Condenser | 25568.44 | 26.387 | 0.0185 | 29.2522 |
| | | TOTAL | 177122.92 | | | |
| 324 | 21:20:45 | Upper Containment | 95974.21 | 82.808 | 0.0653 | 29.2467 |
| | | Lower Containment | 55564.26 | 83.356 | 0.0633 | 29.2503 |
| | | Ice Condenser | 25566.9 | 26.398 | 0.0185 | 29.2511 |
| | | TOTAL | 177105.37 | | | |
| 325 | 21:25:45 | Upper Containment | 95970.8 | 82.81 | 0.0653 | 29.2458 |
| | | Lower Containment | 55564.27 | 83.34 | 0.0633 | 29.2495 |
| | | Ice Condenser | 25566.05 | 26.399 | 0.0185 | 29.2502 |
| | | TOTAL | 177101.13 | | | |
| 326 | 21:30:45 | Upper Containment | 95973.12 | 82.783 | 0.0651 | 29.2449 |
| | | Lower Containment | 55561.83 | 83.343 | 0.0633 | 29.2483 |
| | | Ice Condenser | 25565.35 | 26.395 | 0.0185 | 29.2491 |
| | | TOTAL | 177100.3 | | | |
| 327 | 21:35:46 | Upper Containment | 95971.74 | 82.772 | 0.0651 | 29.2439 |
| | | Lower Containment | 55560.25 | 83.344 | 0.0632 | 29.2475 |
| | | Ice Condenser | 25567.33 | 26.342 | 0.0185 | 29.2482 |
| | | TOTAL | 177099.32 | | | |
| 328 | 21:40:46 | Upper Containment | 95968.48 | 82.775 | 0.0651 | 29.243 |
| | | Lower Containment | 55558.92 | 83.341 | 0.0632 | 29.2467 |
| | | Ice Condenser | 25565.67 | 26.363 | 0.0185 | 29.2476 |
| | | TOTAL | 177093.06 | | | |
| 329 | 21:45:46 | Upper Containment | 95969.15 | 82.764 | 0.065 | 29.2426 |
| | | Lower Containment | 55557.3 | 83.342 | 0.0633 | 29.2459 |
| | | Ice Condenser | 25566.16 | 26.341 | 0.0185 | 29.2468 |
| | | TOTAL | 177092.61 | | | |
| 330 | 21:50:46 | Upper Containment | 95964.14 | 82.779 | 0.0649 | 29.2418 |
| | | Lower Containment | 55556.88 | 83.341 | 0.0632 | 29.2455 |
| | | Ice Condenser | 25567.19 | 26.312 | 0.0185 | 29.2462 |
| | | TOTAL | 177088.21 | | | |
| 331 | 21:55:46 | Upper Containment | 95968.36 | 82.757 | 0.0649 | 29.2419 |
| | | Lower Containment | 55557.73 | 83.33 | 0.0631 | 29.2453 |
| | | Ice Condenser | 25567.83 | 26.301 | 0.0185 | 29.2463 |
| | | TOTAL | 177093.92 | | | |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|--------------------|-------------|-------------|--------------------|--------------|
| 332 | 22:00:46 | Upper Containment | 95970.58 | 82.735 | 0.065 | 29.2414 |
| | | Lower Containment | 55558.13 | 83.326 | 0.063 | 29.2452 |
| | | Ice Condenser | 25568.5 | 26.281 | 0.0185 | 29.2459 |
| | | TOTAL | 177097.21 | | | |
| 333 | 22:05:47 | Upper Containment | 95966.84 | 82.751 | 0.0649 | 29.2411 |
| | | Lower Containment | 55556.56 | 83.328 | 0.0631 | 29.2446 |
| | | Ice Condenser | 25568.36 | 26.278 | 0.0185 | 29.2455 |
| | | TOTAL | 177091.77 | | | |
| 334 | 22:10:47 | Upper Containment | 95966.45 | 82.748 | 0.0648 | 29.2407 |
| | | Lower Containment | 55556.13 | 83.332 | 0.063 | 29.2445 |
| | | Ice Condenser | 25567.04 | 26.296 | 0.0185 | 29.2451 |
| | | TOTAL | 177089.62 | | | |
| 335 | 22:15:47 | Upper Containment | 95963.97 | 82.755 | 0.0649 | 29.2404 |
| | | Lower Containment | 55556.49 | 83.319 | 0.063 | 29.244 |
| | | Ice Condenser | 25566.72 | 26.296 | 0.0185 | 29.2448 |
| | | TOTAL | 177087.18 | | | |
| 336 | 22:20:47 | Upper Containment | 95965.55 | 82.738 | 0.0648 | 29.2399 |
| | | Lower Containment | 55555.2 | 83.323 | 0.063 | 29.2435 |
| | | Ice Condenser | 25566.72 | 26.283 | 0.0185 | 29.244 |
| | | TOTAL | 177087.46 | | | |
| 337 | 22:25:47 | Upper Containment | 95962.17 | 82.73 | 0.0647 | 29.2384 |
| | | Lower Containment | 55553.81 | 83.31 | 0.0629 | 29.242 |
| | | Ice Condenser | 25565.45 | 26.286 | 0.0185 | 29.2427 |
| | | TOTAL | 177081.42 | | | |
| 338 | 22:30:48 | Upper Containment | 95957.97 | 82.744 | 0.0647 | 29.2378 |
| | | Lower Containment | 55553.77 | 83.301 | 0.063 | 29.2416 |
| | | Ice Condenser | 25566.51 | 26.255 | 0.0185 | 29.2421 |
| | | TOTAL | 177078.25 | | | |
| 339 | 22:35:48 | Upper Containment | 95960.71 | 82.719 | 0.0646 | 29.2372 |
| | | Lower Containment | 55551.81 | 83.31 | 0.063 | 29.241 |
| | | Ice Condenser | 25567.26 | 26.234 | 0.0185 | 29.2416 |
| | | TOTAL | 177079.78 | | | |
| 340 | 22:40:48 | Upper Containment | 95957.99 | 82.725 | 0.0647 | 29.2368 |
| | | Lower Containment | 55551.55 | 83.305 | 0.0629 | 29.2405 |
| | | Ice Condenser | 25567.56 | 26.222 | 0.0185 | 29.2413 |
| | | TOTAL | 177077.1 | | | |
| 341 | 22:45:48 | Upper Containment | 95957.22 | 82.724 | 0.0647 | 29.2365 |
| | | Lower Containment | 55551.4 | 83.301 | 0.0628 | 29.2401 |
| | | Ice Condenser | 25569.93 | 26.172 | 0.0185 | 29.241 |
| | | TOTAL | 177078.56 | | | |

| <u>Rd</u> | <u>Time</u> | <u>Compartment</u> | <u>Mass</u> | <u>Temp</u> | <u>Vapor Press</u> | <u>Press</u> |
|-----------|-------------|--------------------|-------------|-------------|--------------------|--------------|
| 342 | 22:50:48 | Upper Containment | 95952.68 | 82.742 | 0.0647 | 29.2361 |
| | | Lower Containment | 55551.34 | 83.297 | 0.0628 | 29.2399 |
| | | Ice Condenser | 25571.42 | 26.134 | 0.0185 | 29.2404 |
| | | TOTAL | 177075.43 | | | |
| 343 | 22:55:48 | Upper Containment | 95957.38 | 82.71 | 0.0646 | 29.2356 |
| | | Lower Containment | 55550.51 | 83.296 | 0.0628 | 29.2393 |
| | | Ice Condenser | 25571.99 | 26.118 | 0.0185 | 29.2401 |
| | | TOTAL | 177079.88 | | | |
| 344 | 23:00:55 | Upper Containment | 95954.04 | 82.722 | 0.0645 | 29.2352 |
| | | Lower Containment | 55550.33 | 83.29 | 0.0626 | 29.2388 |
| | | Ice Condenser | 25571.71 | 26.118 | 0.0185 | 29.2398 |
| | | TOTAL | 177076.08 | | | |
| 345 | 23:05:49 | Upper Containment | 95952.69 | 82.723 | 0.0645 | 29.2349 |
| | | Lower Containment | 55549.58 | 83.292 | 0.0628 | 29.2386 |
| | | Ice Condenser | 25572.33 | 26.097 | 0.0185 | 29.2392 |
| | | TOTAL | 177074.6 | | | |
| 346 | 23:10:49 | Upper Containment | 95949.86 | 82.729 | 0.0645 | 29.2343 |
| | | Lower Containment | 55548.72 | 83.29 | 0.0627 | 29.238 |
| | | Ice Condenser | 25572.61 | 26.086 | 0.0185 | 29.2389 |
| | | TOTAL | 177071.19 | | | |
| 347 | 23:15:49 | Upper Containment | 95948.26 | 82.737 | 0.0645 | 29.2343 |
| | | Lower Containment | 55549.88 | 83.283 | 0.0626 | 29.2382 |
| | | Ice Condenser | 25570.95 | 26.116 | 0.0185 | 29.2388 |
| | | TOTAL | 177069.1 | | | |
| 348 | 23:20:49 | Upper Containment | 95948.3 | 82.733 | 0.0644 | 29.2339 |
| | | Lower Containment | 55549.46 | 83.277 | 0.0626 | 29.2376 |
| | | Ice Condenser | 25571.33 | 26.103 | 0.0185 | 29.2384 |
| | | TOTAL | 177069.08 | | | |
| 349 | 23:25:49 | Upper Containment | 95946.86 | 82.734 | 0.0644 | 29.2336 |
| | | Lower Containment | 55548.9 | 83.276 | 0.0626 | 29.2373 |
| | | Ice Condenser | 25571.78 | 26.091 | 0.0185 | 29.2382 |
| | | TOTAL | 177067.53 | | | |
| 350 | 23:30:50 | Upper Containment | 95948.42 | 82.719 | 0.0643 | 29.2332 |
| | | Lower Containment | 55547.65 | 83.282 | 0.0627 | 29.237 |
| | | Ice Condenser | 25569.97 | 26.116 | 0.0185 | 29.2376 |
| | | TOTAL | 177066.04 | | | |
| 351 | 23:35:50 | Upper Containment | 95952.84 | 82.685 | 0.0644 | 29.2327 |
| | | Lower Containment | 55547.68 | 83.276 | 0.0626 | 29.2366 |
| | | Ice Condenser | 25569.39 | 26.122 | 0.0185 | 29.2373 |
| | | TOTAL | 177069.92 | | | |

APPENDIX F

Verification Analysis Summary

| | |
|---|---------|
| MLR reported during Verification Test (%/day): | 0.24346 |
| TTLR reported during Verification Test (%/day): | 0.25588 |
| MLR reported during GILRT (%/day): | 0.01379 |
| TTLR reported during GILRT (%/day): | 0.01923 |
| Imposed Leak (%/day): | 0.25154 |
| Maximum Allowable Leak Rate (%/day): | 0.25000 |
| MLR Agreement: | -8.7 % |
| TTLR Agreement: | -6.0 % |

APPENDIX G

Penetrations In Service During The CILRT

| <u>Penetration</u> | <u>Description</u> | <u>Justification</u> | <u>Leakage Rate Added to 95% UCL</u> |
|--------------------|--|--|--|
| X-26A | Integrated Leak Rate System Pressure containment pressure. | Isolation valves required to be open to monitor | 0.0000 SCFH |
| X-47A | Ice Condenser System | Glycol cooling supply to air handling units in ice condenser required to maintain temperature. | 0.0000 SCFH |
| X-47B | Ice Condenser System | Same as X-47A. | 0.0000 SCFH |
| X-54 | Thimble Renewal | Used as pressurization point for air compressors | 0.0000 SCFH |
| X-96A | Integrated Leak Rate | Same as X-26A. | 0.0000 SCFH |
| X-96B | Integrated Leak Rate | Same as X-26A. | 0.0000 SCFH |
| X-114 | Ice Condenser System | Glycol return from air handling units required to maintain ice condenser temperature. | 0.0000 SCFH |
| X-115 | Ice Condenser System | Same as X-114. | 0.0000 SCFH |
| X-118 | Layup Water Treatment | Used as source for verification flow and post-test depressurization. | 0.0000 SCFH |

APPENDIX H

Calculation of change in CILRT leak rate
due to level changes inside containment

P_a conditions are: P = 29.696 psia V = 1,201,500 ft³ T = 70°F

The amount of mass at P_a is

$$M = \frac{29.696 \text{ psia} (1,201,500 \text{ ft}^3) (144 \text{ W}^2/\text{ft}^2)}{(53.35) \frac{\text{lb ft}}{\text{lbm}^\circ\text{R}} (529.67 \text{ R})}$$

$$= 181,821.1593 \text{ lbm}$$

The combined increase in the ARBFEDS AND RBFEDS sump levels was 0.4558 gallons/hour or 1.462 ft³ over 24 hours.

The increase in the pressurizer level was 2.8264 ft³/hour or 67.834 ft³ over 24 hours.

The total increase in level was 69.296 ft³ over 24 hours.

CILRT average temperature was 76.61607°F

CILRT average pressure was 29.35155 psia

CILRT Containment Volume was 1,201,500 ft³

$$\frac{(69.296 \text{ ft}^3) 29.35155 \text{ psia} (144 \text{ in}^2/\text{ft}^2)}{(53.35) \frac{\text{lb ft}}{\text{lbm}^\circ\text{R}} (536.28607^\circ\text{R})} = 10.2370 \text{ lbm/day}$$

The increase in leak rate is $\frac{10.2370 \text{ lbm/day} \times 100}{181,821.1593} = 0.00563 \text{ \%/day}$

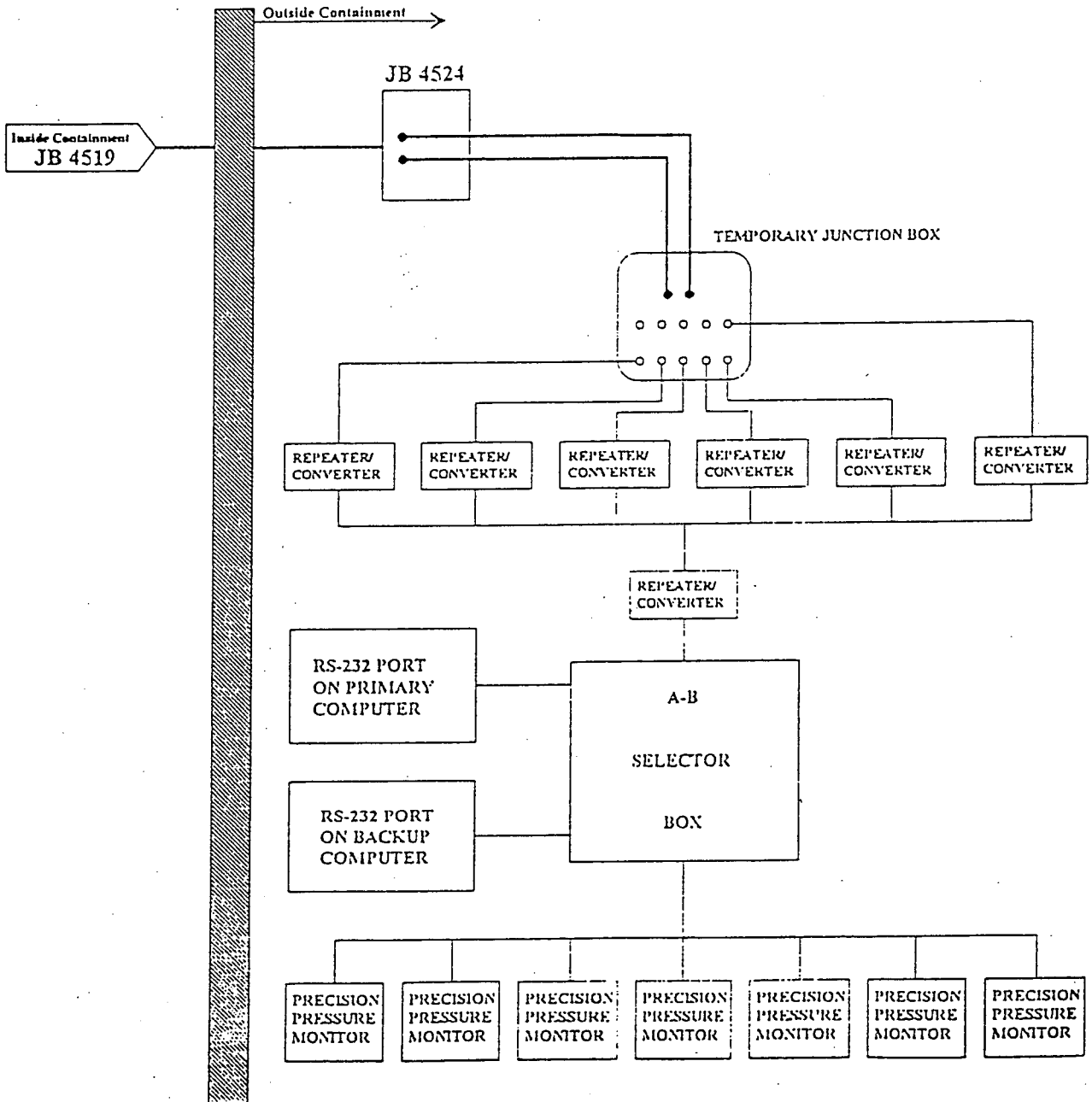
ARBFEDS = Auxiliary Reactor Building Floor and Equipment Drain Sump

RBFEDS = Reactor Building Floor and Equipment Drain Sump

APPENDIX I

Computer System Block Diagram

TEMPORARY TEST INSTRUMENTATION



APPENDIX J

Compartment Parameters and Instrument Location

Compartment Parameters

| <u>Temperature</u> | <u>Number of Transducers</u> | <u>Segment Volume</u> | <u>Volumetric Weight Per Sensor by Compartment (%)</u> |
|-----------------------|----------------------------------|---------------------------|--|
| I. Upper compartment | 14 | 661,000 | 7.142857 |
| II. Lower compartment | 25 | 383,720 | 4.000000 |
| III. Ice compartment | | (157,500) | |
| Ice-upper | 6 | 47,000 | 4.973545 |
| Ice-lower | <u>4</u> | 110,500 | 17.539683 |
| Total | 49 | | |

| <u>Relative Humidity</u> | | | |
|--------------------------|----------|-----------|-----------|
| I. Upper compartment | 2 | 661,000 | 50.000000 |
| II. Lower compartment | 3 | 383,720 | 33.333333 |
| III. Ice compartment | | (157,500) | |
| Ice-upper | 0 | 47,000 | 0.000000 |
| Ice-lower | <u>0</u> | 110,500 | 0.000000 |
| Total | 5 | | |

| <u>Pressure Sensor</u> | | | |
|------------------------|----------|---------|-----------|
| I. Upper compartment | 2 | 661,000 | 50.000000 |
| II. Lower compartment | 2 | 383,720 | 50.000000 |
| III. Ice compartment | <u>2</u> | 157,500 | 50.000000 |
| Total | 6 | | |

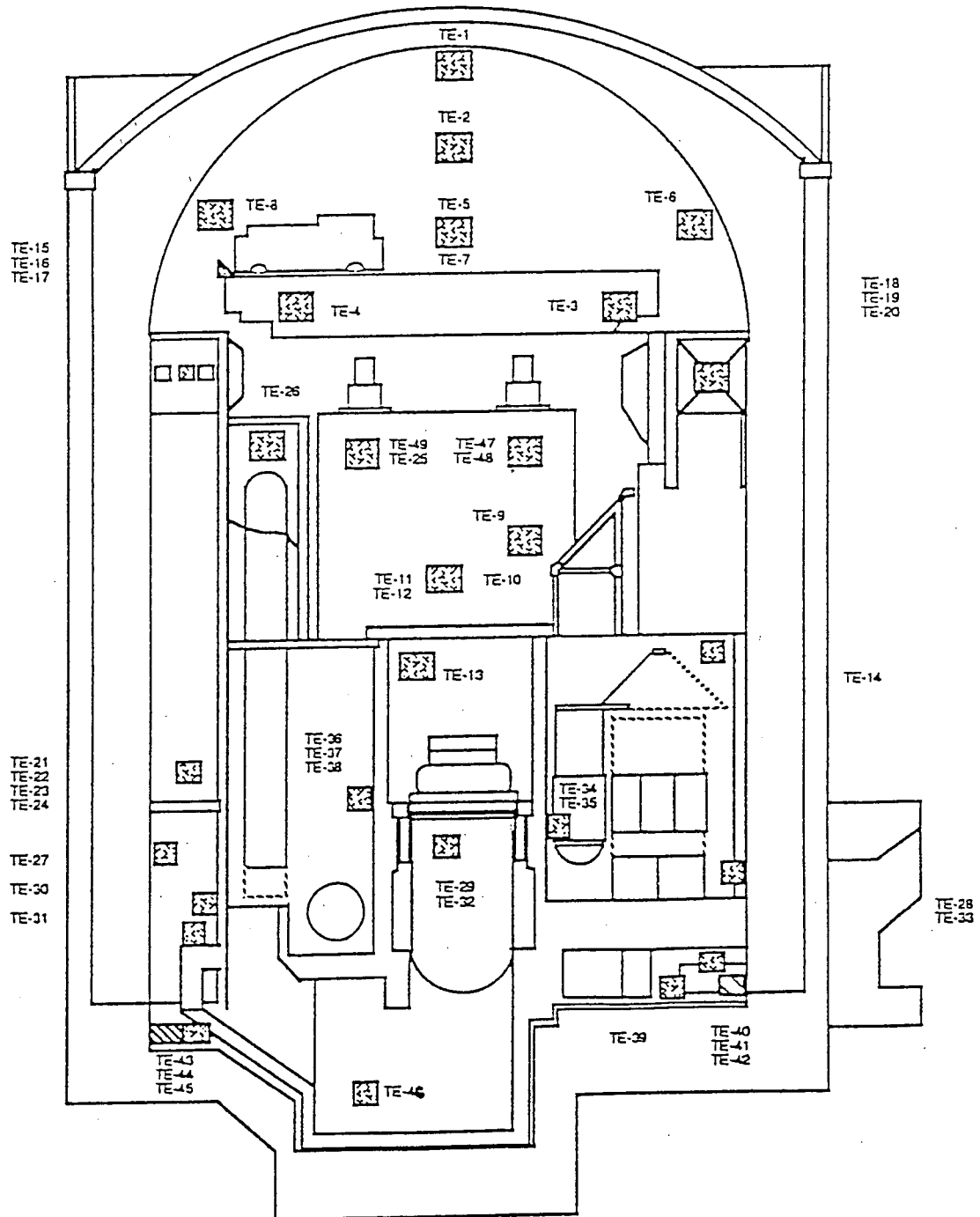
Compartment Volume Weights

| <u>Containment Compartment</u> | <u>Segment Volume (ft³)</u> | <u>Volumetric Weight (%)</u> |
|------------------------------------|--|----------------------------------|
| I. Upper compartment | 661,000 | 55.014565 |
| II. Lower compartment | 383,000 | 31.876821 |
| III. Ice compartment | 157,500 | 13.108614 |
| Total Containment | 1,201,500 | 100.000000 |

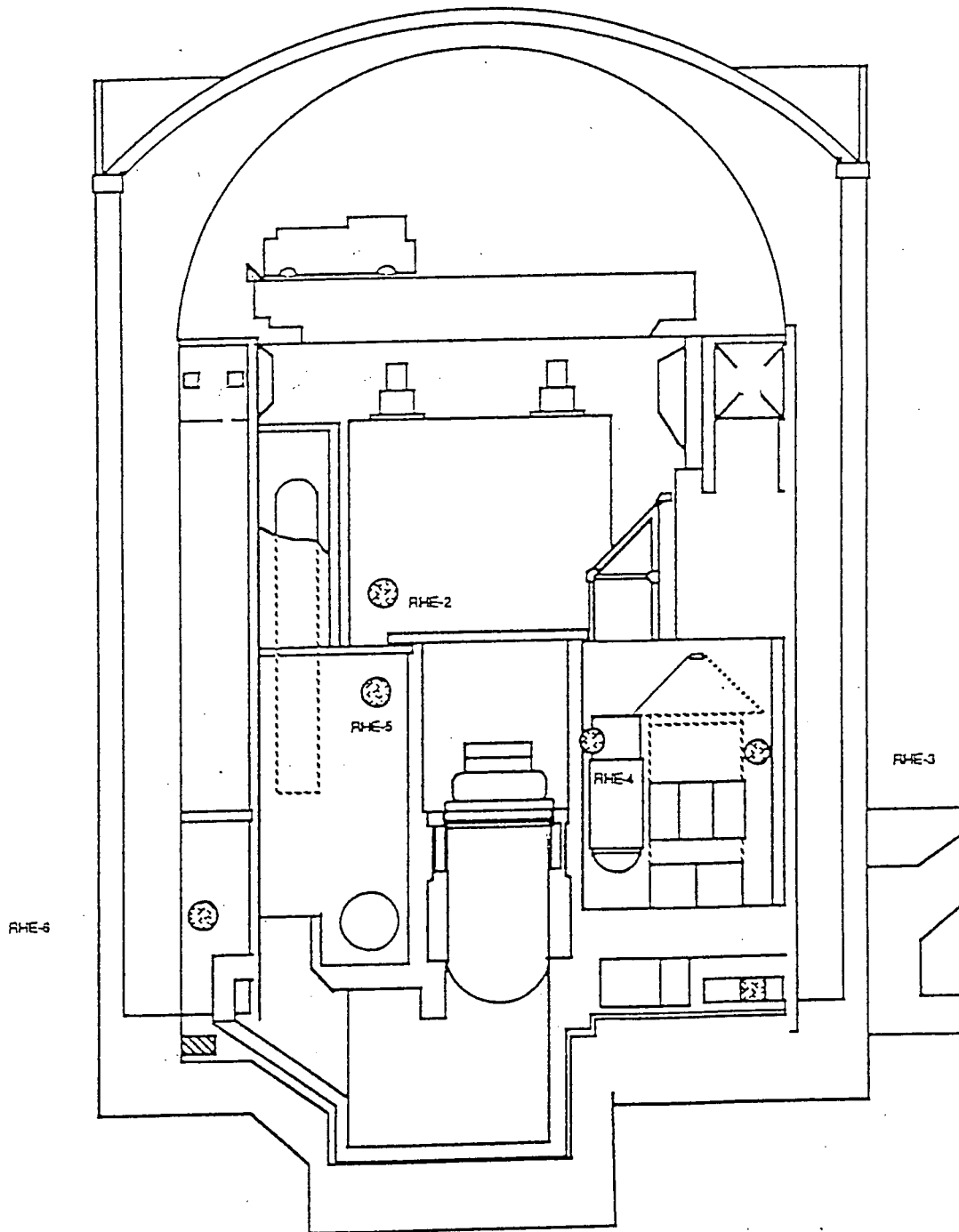
RHE/TE ASSOCIATIONS

| <u>RHE Sensor</u> | <u>TE</u> |
|-------------------|-----------|
| RHE-2 | TE-12 |
| RHE-3 | TE-10 |
| RHE-4 | TE-34 |
| RHE-5 | TE-37 |
| RHE-6 | TE-31 |

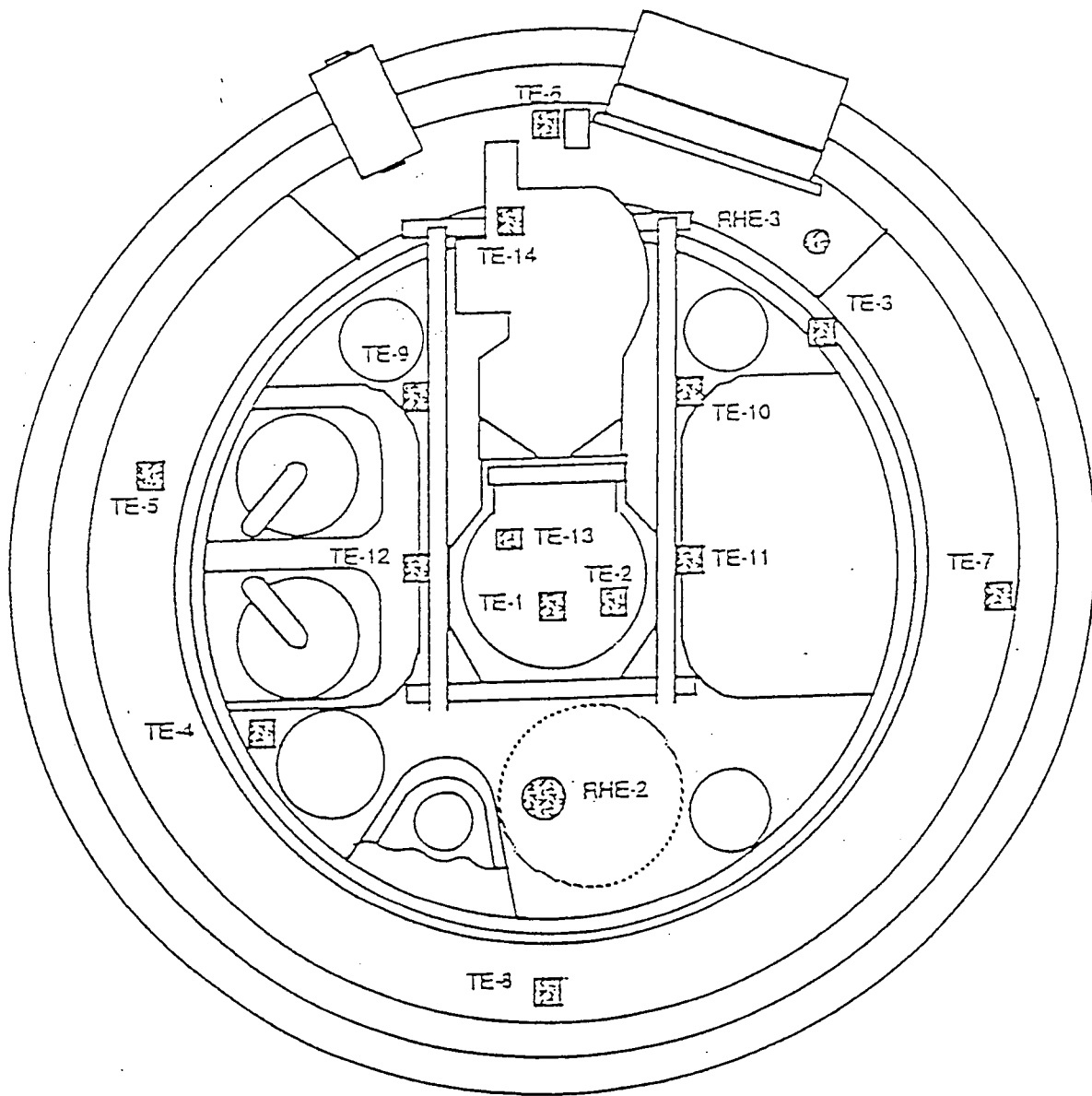
TEMPERATURE SENSOR LOCATIONS (Elevation View)



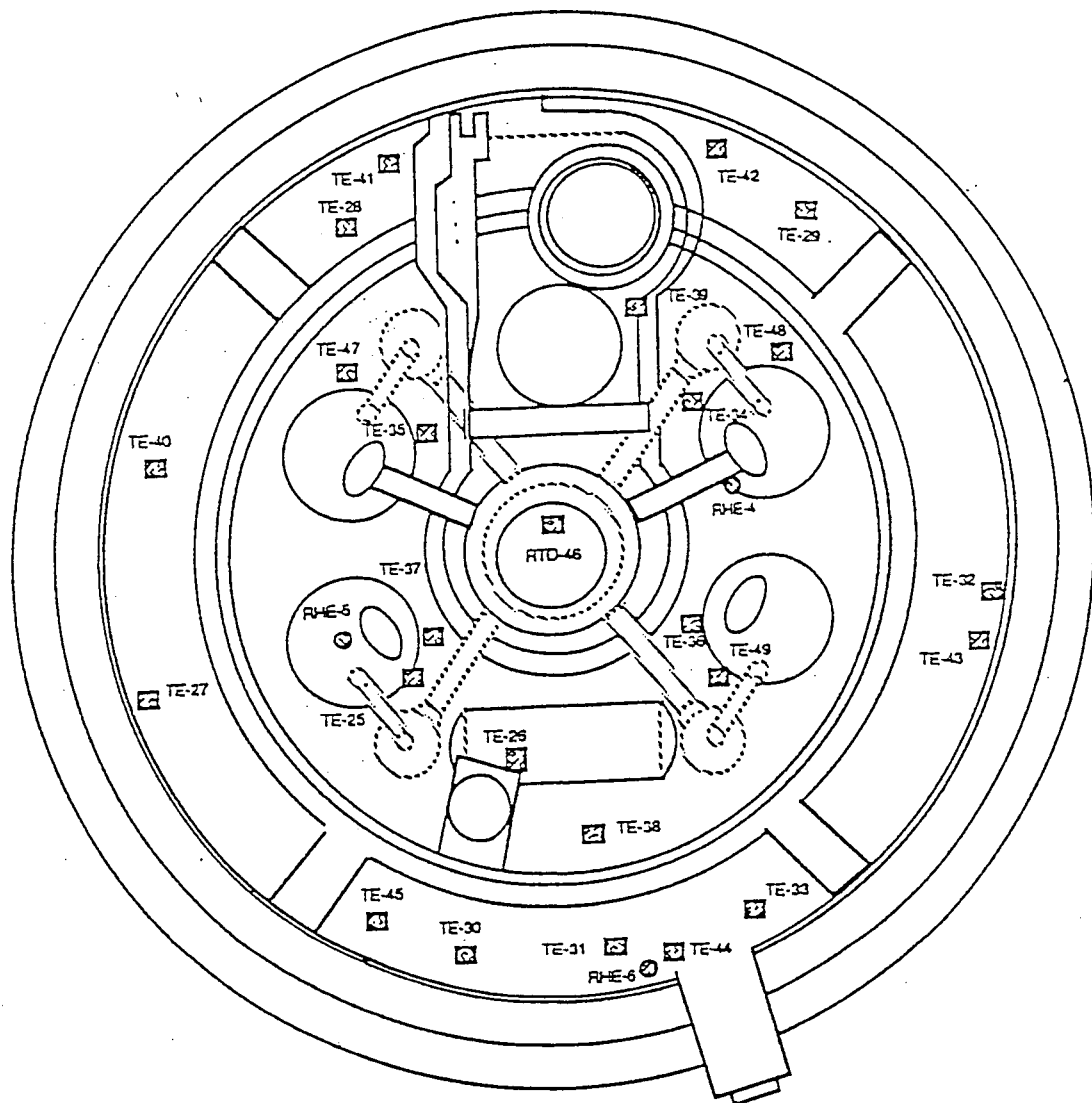
RELATIVE HUMIDITY SENSOR LOCATIONS (Elevation View)



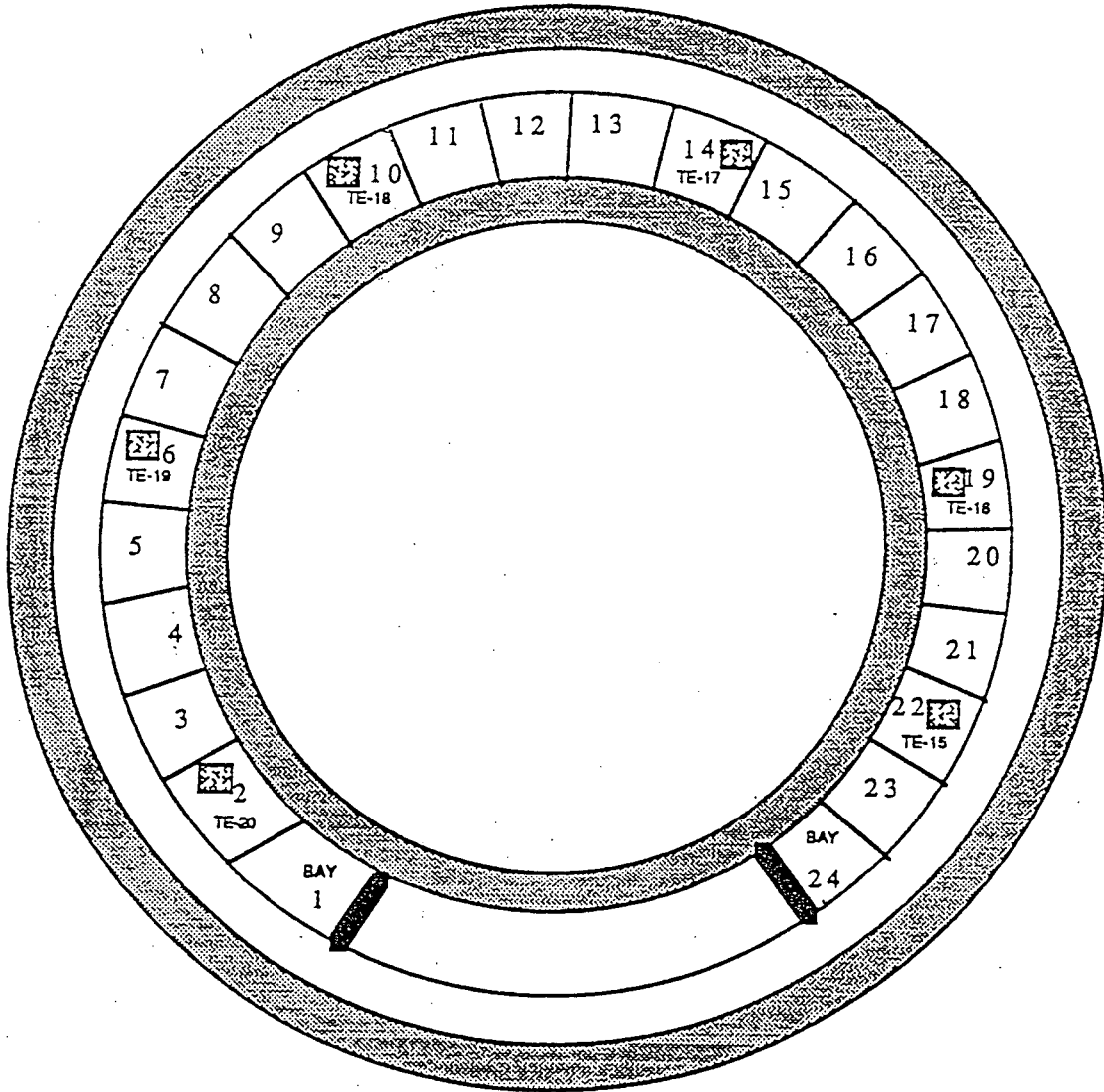
UPPER COMPARTMENT SENSOR LOCATIONS



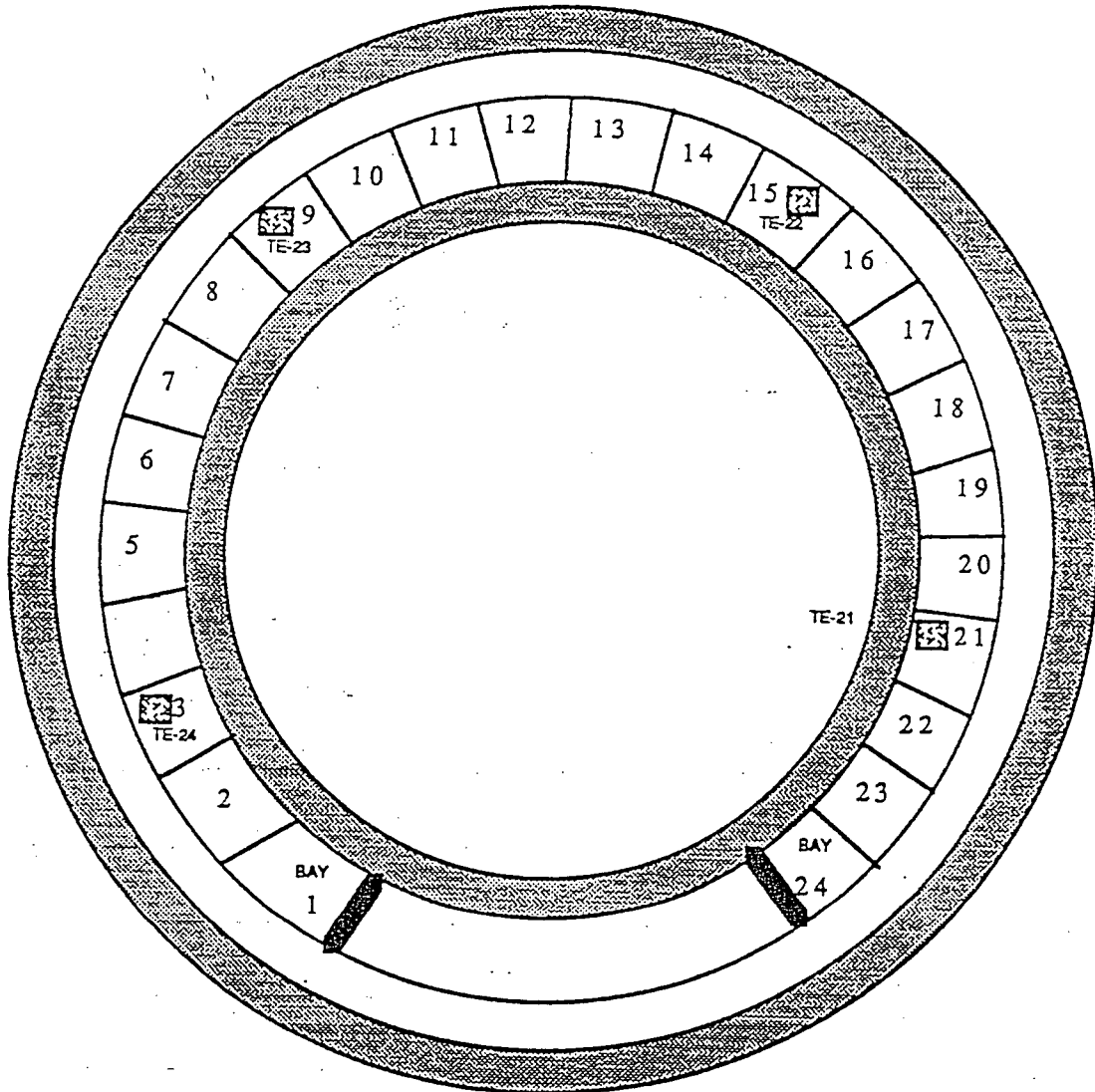
LOWER COMPARTMENT SENSOR LOCATIONS



UPPER ICE SENSOR LOCATIONS



LOWER ICE SENSOR LOCATIONS



APPENDIX K

Instrumentation Specifications

APPENDIX K

| <u>Measured Parameter Specification</u> | <u>Manufacturer and Model No.</u> | <u>Number Used</u> | <u>Instrument</u> | |
|---|--|------------------------|---------------------------------------|--|
| Containment Temperature | Graftel Model No. 9202 LT | 49 | Range: Accuracy: Repeatability: | 0-114°F ±0.24°F 0.01°F |
| Containment Pressure | Paroscientific Model No. 760-100A | 6 | Range: Accuracy: Repeatability: | 0-100 psia ±0.015% F.S. ±0.005% F.S. |
| Containment Relative Humidity | Graftel | 5 | Range: Accuracy: Repeatability: | 17-100% RH ±2°F dewpoint ±0.1°F |
| Verification Flow | Teledyne-Hastings Mass Flow Meter Model AHL 25 with H-3M Transducer | 1 | Range: Accuracy: Repeatability: | 0-5 SCFM ±2% range ±1/2% range |
| Atmospheric Pressure | Paroscientific Model No. 760-100A | 1 | Range: Accuracy: | 0-100 psia ±0.015% range |

APPENDIX L

Summary of Local Leak Rate Tests Conducted Prior to the CILRT

The local leak rate test program was completed prior to the performance of the CILRT with the exception of the water inventory tests required for the Containment Spray and RHR Spray isolation valves (penetrations X-48A, X-48B, X-49A, and X-49B), and the Hydrogen Analyzer System loop test outside the H₂ Analyzer System isolation valves (penetrations X-92A, X-92B, X-99, and X-100).

The water inventory tests will be performed and any necessary repairs completed by September 30, 1994 to ensure that inventory limits are not exceeded and that penetrations X-48A, X-48B, X-49A, and X-49B do not contribute to the overall containment air leakage. The H₂ Analyzer System loop checks will also be performed and any necessary repairs completed prior to September 30, 1994 to ensure no detectable leakage exists.

A supplemental report containing the final results of these local leak rate tests will be submitted within 30 days of work completion.

Note: All leak rates are given in standard cubic feet per hour

1. IB = Inboard
2. OB = Outboard
3. ISV = Hand Control Valve
4. FCV = Flow Control Valve
5. FSV = Flow Solenoid Valve
6. CKV = Check Valve
7. BYV = Bypass Valve

Bellows

| Penetration No. | Name | As Left | Date |
|--------------------|------------------|---------|----------|
| X-8A (IB&OB) | Feedwater Bypass | 0.0000 | 02/02/94 |
| X-8B (IB&OB) | Feedwater Bypass | 0.0000 | 02/08/94 |
| X-8C (IB&OB) | Feedwater Bypass | 0.0000 | 02/08/94 |
| X-8D (IB&OB) | Feedwater Bypass | 0.0000 | 02/10/94 |
| X-12A (IB&OB) | Main Feedwater | 0.0000 | 02/21/94 |
| X-12B (IB&OB) | Main Feedwater | 0.0000 | 02/08/94 |
| X-12C (IB&OB) | Main Feedwater | 0.0000 | 02/08/94 |
| X-12D (IB&OB) | Main Feedwater | 0.0000 | 02/10/94 |
| X-13A (IB&OB) | Main Steam | 0.0000 | 02/21/94 |
| X-13B (IB&OB) | Main Steam | 0.0000 | 02/22/94 |
| X-13C (IB&OB) | Main Steam | 0.0000 | 02/22/94 |
| X-13D (IB&OB) | Main Steam | 0.0000 | 02/21/94 |
| X-14A | S/G Blowdown | 0.0000 | 02/02/94 |
| X-14B | S/G Blowdown | 0.0000 | 02/10/94 |
| X-14C | S/G Blowdown | 0.0000 | 02/02/94 |
| X-14D | S/G Blowdown | 0.0000 | 02/10/94 |

Bellows (cont.)

| Penetration No. | Name | As Left | Date |
|--------------------|--------------------------------|---------|----------|
| X-15 | CVCS | 0.0000 | 02/09/94 |
| X-17 | RHR Pump Return | 0.0000 | 02/0994 |
| X-20A | Low Head S.I. | 0.0000 | 02/21/94 |
| X-20B | Low Head S.I. | 0.0000 | 02/21/94 |
| X-21 | Hot Leg S.I. | 0.0000 | 02/09/94 |
| X-22 | BIT Chg. Pump Dischg. | 0.0000 | 02/09/94 |
| X-24 | SIS Relief Vlv Dischg. | 0.0000 | 02/09/94 |
| X-30 | Accum. to Holdup Tank | 0.0000 | 02/11/94 |
| X-32 | High Head SIS | 0.0000 | 02/11/94 |
| X-33 | High Head SIS | 0.0000 | 02/11/94 |
| X-45 | RCDT and PRT to Vent Header | 0.0000 | 02/11/94 |
| X-46 | RCDT Pump Dischg." | 0.0000 | 02/11/94 |
| X-47A | Glycol Return | 0.0000 | 02/22/94 |
| X-47B | Glycol Supply | 0.0000 | 02/22/94 |
| X-81 | RCDT to Gas Analyzer | 0.0000 | 02/11/94 |
| X-107 | RHR Supply | 0.0000 | 02/11/94 |
| X-108 | Maintenance Port | 0.0000 | 02/12/94 |
| X-109 | Maintenance Port | 0.0000 | 02/12/94 |

Resilient Seals

| Penetration No. | Name | As Left | Date |
|--------------------|----------------------------|---------|----------|
| X-1 | Equipment Hatch | 0.0000 | 06/19/94 |
| X-3 | Fuel Transfer Tube | 0.0000 | 02/14/94 |
| X-36 | Steam Generator Cleanup | 0.0000 | 02/23/94 |
| X-37 | Maintenance Port | 0.0000 | 04/19/94 |
| X-40D | Hydrogen Purge | 0.0000 | 02/25/94 |
| X-54 | Thimble Renewal | 0.0000 | 06/16/94 |
| X-79A | Ice Blowing | 0.0000 | 02/22/94 |
| X-79B | Negative Return | 0.0000 | 02/22/94 |
| X-108 | Maintenance Port | 0.0000 | 06/16/94 |
| X-109 | Maintenance Port | 0.0000 | 06/22/94 |
| X-117 | Maintenance Port | 0.0000 | 02/25/94 |
| X-118 | Maintenance Port | 0.0000 | 02/24/94 |

Electrical Penetrations

| Penetration No. | Name | As Left | Date |
|--------------------|-------------------------|---------|----------|
| X-121E | RCP 1 | 0.0000 | 02/12/94 |
| X-122E | RCP 2 | 0.0000 | 02/12/94 |
| X-123E | RCP 3 | 0.0000 | 02/12/94 |
| X-124E | RCP 4 | 0.0000 | 02/23/94 |
| X-125E | 480V Power Non-Div | 0.0000 | 02/23/94 |
| X-126E | 480V Power A | 0.0000 | 02/03/94 |
| X-127E | 480V Power B | 0.0000 | 02/07/94 |
| X-128E | 480V Power A | 0.0000 | 02/14/94 |
| X-129E | 480V Power B | 0.0000 | 02/17/94 |
| X-130E | Control Non-Div | 0.0000 | 02/23/94 |
| X-131E | 480V Power Non-Div | 0.0000 | 02/23/94 |
| X-132E | Control Rod Drive Power | 0.0000 | 02/14/94 |
| X-133E | Control Rod Drive Power | 0.0000 | 02/14/94 |
| X-134E | 480V Power A | 0.0000 | 02/04/94 |
| X-135E | 480V Power A | 0.0000 | 02/05/94 |
| X-136E | 480V Power B | 0.0000 | 02/05/94 |
| X-137E | 480V Power B | 0.0000 | 02/05/94 |
| X-138E | Low Level Non-Div | 0.0000 | 02/03/94 |
| X-139E | Process Instrumentation | 0.0000 | 02/03/94 |
| X-140E | Incore Instrumentation | 0.0000 | 02/24/94 |
| X-141E | 480V Power A | 0.0000 | 02/15/94 |
| X-142E | Incore Instrumentation | 0.0000 | 02/04/94 |

Electrical Penetrations (cont.)

| Penetration No. | Name | As Left | Date |
|--------------------|------------------------------------|---------|----------|
| X-143E | NIS Channel III | 0.0000 | 03/18/94 |
| X-144E | 480V Power Non-Div | 0.0000 | 02/15/94 |
| X-145E | Control Rod Position Indication | 0.0000 | 02/23/94 |
| X-146E | Control Rod Drive Power | 0.0000 | 02/23/94 |
| X-147E | Control A | 0.0000 | 02/03/94 |
| X-148E | Process Inst Control | 0.0000 | 02/04/94 |
| X-149E | Miscellaneous Control | 0.0000 | 02/04/94 |
| X-150E | Miscellaneous Control | 0.0000 | 02/03/94 |
| X-151E | NIS Channel IV | 0.0000 | 02/04/94 |
| X-152E | 480V Power Non-Div | 0.0000 | 02/04/94 |
| X-153E | Low Level Non-Div | 0.0000 | 02/07/94 |
| X-154E | Process Inst Control | 0.0000 | 02/05/94 |
| X-155E | 480V Power Non-Div | 0.0000 | 02/05/94 |
| X-156E | Control B | 0.0000 | 03/24/94 |
| X-157E | Annunciation | 0.0000 | 02/05/94 |
| X-158E | Process Inst Protection | 0.0000 | 02/07/94 |
| X-159E | Process Inst Control | 0.0000 | 02/14/94 |
| X-160E | Communication | 0.0000 | 02/14/94 |
| X-161E | 480V Power Non-Div | 0.0000 | 02/14/94 |
| X-163E | NIS Channel I | 0.0000 | 02/14/94 |
| X-164E | Control A | 0.0000 | 02/14/94 |

Electrical Penetrations (cont.)

| Penetration No. | Name | As Left | Date |
|--------------------|-------------------------|---------|----------|
| X-165E | Process Inst Protection | 0.0000 | 02/14/94 |
| X-166E | Control Non-Div | 0.0000 | 02/05/94 |
| X-167E | 480V Power Non-Div | 0.0000 | 02/17/94 |
| X-168E | Control Non-Div | 0.0000 | 02/17/94 |
| X-169E | Process Inst Protection | 0.0000 | 04/12/94 |
| X-170E | Process Inst Control | 0.0000 | 02/17/94 |
| X-171E | Control Non-Div | 0.0000 | 02/04/94 |
| X-172E | Control B | 0.0000 | 02/17/94 |
| X-173E | Control Non-Div | 0.0000 | 02/15/94 |
| X-174E | NIS Channel II | 0.0000 | 02/24/94 |

Containment Isolation Valves

| Penetration No. | Name | As Left | Date |
|--------------------|----------------|----------|----------|
| X-4 | 1-FCV-30-56/57 | 0.36834 | 06/16/94 |
| X-5 | 1-FCV-30-58/59 | 0.32110 | 05/25/94 |
| X-6 | 1-FCV-30-50/51 | 0.00000 | 06/15/94 |
| X-7 | 1-FCV-30-52/53 | 0.35977 | 05/27/94 |
| X-9A | 1-FCV-30-7/8 | 0.00000 | 06/13/94 |
| X-9B | 1-FCV-30-9/10 | 0.082844 | 06/18/94 |
| X-10A | 1-FCV-30-14/15 | 0.95130 | 05/25/94 |
| X-10B | 1-FCV-30-16/17 | 0.07663 | 05/25/94 |
| X-11 | 1-FCV-30-19/20 | 0.00000 | 06/11/94 |
| X-15 | 1-FCV-62-72 | 0.00000 | 06/12/94 |
| | 1-FCV-62-73 | 0.00000 | 06/12/94 |
| | 1-FCV-62-74 | 0.00000 | 06/12/94 |
| | 1-FCV-62-76 | 0.00000 | 06/12/94 |
| | 1-FCV-62-77 | 0.00000 | 06/12/94 |
| | 1-RFV-62-662 | 0.00000 | 06/12/94 |
| X-23 | 1-FSV-43-318 | 0.00000 | 05/16/94 |
| | 1-FSV-43-319 | 0.00000 | 05/16/94 |
| X-25A | 1-FCV-43-11 | 0.00000 | 04/19/94 |
| | 1-FCV-43-12 | 0.00000 | 04/19/94 |
| X-25D | 1-FCV-43-2 | 0.00000 | 06/17/94 |
| | 1-FCV-43-3 | 0.00000 | 06/17/94 |
| X-26A | 1-ISV-52-504 | 0.00000 | 02/16/94 |
| | 1-ISV-52-500 | 0.00000 | 02/16/94 |
| X-26B | 1-ISV-52-501 | 0.00000 | 02/16/94 |
| | 1-ISV-52-505 | 0.00000 | 02/16/94 |
| X-28 | 1-FSV-43-341 | 0.00000 | 04/14/94 |
| | 1-CKV-43-834 | 0.00000 | 04/14/94 |

Containment Isolation Valves (cont.)

| Penetration No. | Name | As Left | Date |
|--------------------|---------------|---------|----------|
| X-29 | 1-FCV-70-89 | 0.00000 | 06/10/94 |
| | 1-FCV-70-92 | 0.00000 | 06/10/94 |
| | 1-CKV-70-698 | 0.00000 | 06/10/94 |
| X-30 | 1-FCV-63-71 | 0.00000 | 06/12/94 |
| | 1-FCV-63-84 | 0.00000 | 06/23/94 |
| | 1-CKV-63-23 | 0.00000 | 06/23/94 |
| X-31 | 1-FCV-26-243 | 0.00000 | 06/17/94 |
| | 1-CKV-26-1296 | 0.44960 | 06/17/94 |
| X-34 | 1-FCV-32-110 | 0.00000 | 06/15/94 |
| | 1-BYV-32-288 | 0.00000 | 06/15/94 |
| | 1-CKV-32-293 | 0.00000 | 06/15/94 |
| X-35 | 1-FCV-70-85 | 0.00000 | 06/11/94 |
| | 1-RFV-70-703 | 0.00000 | 06/11/94 |
| X-39A | 1-FCV-63-64 | 0.00000 | 06/09/94 |
| | 1-CKV-77-868 | 0.00000 | 06/09/94 |
| X-39B | 1-FCV-68-305 | 0.00000 | 06/17/94 |
| | 1-CKV-77-849 | 0.00000 | 06/17/94 |
| X-41 | 1-FCV-77-127 | 0.00000 | 06/17/94 |
| | 1-FCV-77-128 | 0.00000 | 06/17/94 |
| X-42 | 1-FCV-81-12 | 0.00000 | 02/26/94 |
| | 1-CKV-81-502 | 0.00000 | 02/26/94 |
| X-44 | 1-FCV-62-61 | 0.00000 | 03/15/94 |
| | 1-FCV-62-63 | 0.00000 | 03/15/94 |
| | 1-CKV-62-639 | 0.00000 | 03/15/94 |
| X-45 | 1-FCV-77-18 | 0.00000 | 06/21/94 |
| | 1-FCV-77-19 | 0.00000 | 06/21/94 |
| | 1-FCV-77-20 | 0.00000 | 06/21/94 |
| X-46 | 1-FCV-77-9 | 0.00000 | 06/20/94 |
| | 1-FCV-77-10 | 0.00000 | 06/20/94 |
| | 1-ISV-84-530 | 0.00000 | 06/20/94 |

Containment Isolation Valves (cont.)

| Penetration No. | Name | As Left | Date |
|--------------------|----------------|---------|----------|
| X-47A | 1-FCV-61-191 | 0.00000 | 05/07/94 |
| | 1-FCV-61-192 | 0.00000 | 05/07/94 |
| | 1-CKV-61-533 | 0.00000 | 05/07/94 |
| X-47B | 1-FCV-61-193 | 0.00000 | 05/07/94 |
| | 1-FCV-61-194 | 0.00000 | 05/07/94 |
| | 1-CKV-61-680 | 0.00000 | 05/07/94 |
| X-50A | 1-FCV-70-87 | 0.00000 | 06/10/94 |
| | 1-FCV-70-90 | 0.00000 | 06/10/94 |
| | 1-CKV-70-687 | 0.00000 | 06/10/94 |
| X-50B | 1-CKV-70-679 | 0.00000 | 06/10/94 |
| | 1-FCV-70-134 | 0.00000 | 06/17/94 |
| X-52 | 1-FCV-70-140 | 0.00000 | 06/10/94 |
| | 1-FCV-70-100 | 0.00000 | 06/10/94 |
| | 1-CKV-70-790 | 0.00000 | 06/10/94 |
| X-53 | 1-FCV-70-143 | 0.00000 | 06/10/94 |
| X-56A | 1-FCV-67-107 | 0.00000 | 03/04/94 |
| | 1-FCV-67-113 | 0.00000 | 03/04/94 |
| | 1-CKV-67-1054D | 0.00000 | 03/04/94 |
| X-57A | 1-FCV-67-111 | 0.14820 | 03/04/94 |
| | 1-FCV-67-112 | 0.00000 | 03/04/94 |
| | 1-CKV-67-575D | 0.00000 | 03/04/94 |
| X-58A | 1-FCV-67-83 | 0.00000 | 03/03/94 |
| | 1-FCV-67-89 | 0.00000 | 03/03/94 |
| | 1-CKV-67-1054A | 0.00000 | 03/03/94 |
| X-59A | 1-FCV-67-87 | 0.00000 | 03/03/94 |
| | 1-FCV-67-88 | 0.00000 | 03/03/94 |
| | 1-CKV-67-575A | 0.00000 | 03/03/94 |
| X-60A | 1-FCV-67-99 | 0.00000 | 03/04/94 |
| | 1-FCV-67-105 | 0.00000 | 03/04/94 |
| | 1-CKV-67-1054B | 0.00000 | 03/04/94 |

Containment Isolation Valves (cont.)

| Penetration No. | Name | As Left | Date |
|--------------------|----------------|---------|----------|
| X-61A | 1-FCV-67-103 | 0.00000 | 03/05/94 |
| | 1-FCV-67-104 | 0.00000 | 03/05/94 |
| | 1-CKV-67-575B | 0.00000 | 03/05/94 |
| X-62A | 1-FCV-67-91 | 0.00000 | 03/05/94 |
| | 1-FCV-67-97 | 0.00000 | 03/05/94 |
| | 1-CKV-67-1054C | 0.00000 | 03/05/94 |
| X-63A | 1-FCV-67-95 | 0.00000 | 06/19/94 |
| | 1-FCV-67-96 | 0.00000 | 06/19/94 |
| | 1-CKV-67-575C | 0.00000 | 06/19/94 |
| X-64 | 1-FCV-31-305 | 0.00000 | 03/26/94 |
| | 1-FCV-31-306 | 0.00000 | 03/26/94 |
| | 1-CKV-31-3421 | 0.00000 | 03/26/94 |
| X-65 | 1-FCV-31-308 | 0.00000 | 03/27/94 |
| | 1-FCV-31-309 | 0.00000 | 03/27/94 |
| | 1-CKV-31-3407 | 0.00000 | 03/27/94 |
| X-66 | 1-FCV-31-326 | 0.00000 | 04/25/94 |
| | 1-FCV-31-327 | 0.00000 | 04/25/94 |
| | 1-CKV-31-3392 | 0.00000 | 04/25/94 |
| X-67 | 1-FCV-31-329 | 0.00000 | 04/25/94 |
| | 1-FCV-31-330 | 0.00000 | 04/25/94 |
| | 1-CKV-31-3378 | 0.00000 | 04/25/94 |
| X-68 | 1-FCV-67-141 | 0.00000 | 03/06/94 |
| | 1-CKV-67-580D | 0.00000 | 03/06/94 |
| X-69 | 1-FCV-67-130 | 0.00000 | 03/10/94 |
| | 1-CKV-67-580A | 0.00000 | 03/10/94 |
| X-70 | 1-FCV-67-139 | 0.00000 | 03/06/94 |
| | 1-FCV-67-297 | 0.00000 | 03/06/94 |
| | 1-CKV-67-585B | 0.00000 | 03/06/94 |
| X-71 | 1-FCV-67-134 | 0.00000 | 03/08/94 |
| | 1-FCV-67-296 | 0.00000 | 03/08/94 |
| | 1-CKV-67-585C | 0.00000 | 03/08/94 |

Containment Isolation Valves (cont.)

| Penetration No. | Name | As Left | Date |
|--------------------|----------------|---------|----------|
| X-72 | 1-FCV-67-142 | 0.00000 | 03/06/94 |
| | 1-FCV-67-298 | 0.00000 | 03/06/94 |
| | 1-CKV-67-585D | 0.00000 | 03/06/94 |
| X-73 | 1-FCV-67-131 | 0.00000 | 03/10/94 |
| | 1-FCV-67-295 | 0.00000 | 03/10/94 |
| | 1-CKV-67-585A | 0.00000 | 03/10/94 |
| X-74 | 1-FCV-67-138 | 0.00000 | 03/06/94 |
| | 1-CKV-67-580B | 0.00000 | 03/06/94 |
| X-75 | 1-FCV-67-133 | 0.00000 | 03/08/94 |
| | 1-CKV-67-580C | 0.00000 | 03/08/94 |
| X-76 | 1-ISV-33-713 | 0.00000 | 05/06/94 |
| | 1-ISV-33-714 | 0.00000 | 05/06/94 |
| X-77 | 1-ISV-59-522 | 0.00000 | 03/24/94 |
| | 1-ISV-59-698 | 0.00000 | 03/24/94 |
| X-78 | 1-FCV-26-240 | 0.00000 | 06/15/94 |
| | 1-CKV-26-1260 | 0.00000 | 06/15/94 |
| X-80 | 1-FCV-30-37/40 | 0.12899 | 05/18/94 |
| X-81 | 1-FCV-77-16 | 0.00000 | 06/16/94 |
| | 1-FCV-77-17 | 0.00000 | 06/16/94 |
| X-82 | 1-ISV-78-560 | 0.00000 | 03/01/94 |
| | 1-ISV-78-561 | 0.00000 | 03/01/94 |
| X-83 | 1-ISV-78-557 | 0.00000 | 03/09/94 |
| | 1-ISV-78-558 | 0.00000 | 03/09/94 |
| X-84A | 1-FCV-68-307 | 0.04818 | 06/15/94 |
| | 1-FCV-68-308 | 0.00000 | 06/15/94 |
| X-85A | 1-FCV-43-75 | 0.00000 | 04/14/94 |
| | 1-FCV-43-77 | 0.00000 | 04/14/94 |
| X-85B | 1-FCV-43-22 | 0.00000 | 06/17/94 |
| | 1-FCV-43-23 | 0.00000 | 06/17/94 |

Containment Isolation Valves (cont.)

| Penetration No. | Name | As Left | Date |
|--------------------|--------------|---------|----------|
| X-86A | 1-FSV-43-287 | 0.00000 | 06/20/94 |
| | 1-FSV-43-288 | 0.00000 | 05/12/94 |
| X-86B | 1-CKV-43-883 | 0.00000 | 05/03/94 |
| | 1-FSV-43-307 | 0.00000 | 05/03/94 |
| X-86C | 1-CKV-43-841 | 0.13568 | 06/10/94 |
| | 1-FSV-43-342 | 0.00000 | 06/10/94 |
| X-90 | 1-FCV-32-102 | 0.00000 | 06/14/94 |
| | 1-BYV-32-308 | 0.00000 | 06/14/94 |
| | 1-CKV-32-313 | 0.00000 | 06/14/94 |
| X-91 | 1-FCV-32-80 | 0.00000 | 06/14/94 |
| | 1-BYV-32-298 | 0.00000 | 06/14/94 |
| | 1-CKV-32-303 | 0.00000 | 06/18/94 |
| X-92A | 1-FCV-43-207 | 0.00000 | 06/08/94 |
| | 1-FCV-43-435 | 0.00000 | 06/08/94 |
| X-92B | 1-FCV-43-208 | 0.03725 | 06/20/94 |
| | 1-FCV-43-436 | 0.00000 | 06/08/94 |
| X-92C | 1-FSV-43-250 | 0.00000 | 04/15/94 |
| | 1-FSV-43-251 | 0.00000 | 06/11/94 |
| X-93 | 1-FCV-43-34 | 0.00000 | 04/19/94 |
| | 1-FCV-43-35 | 0.00000 | 04/19/94 |
| X-94B | 1-FCV-90-110 | 0.00000 | 06/22/94 |
| | 1-FCV-90-111 | 0.00000 | 06/22/94 |
| X-94C | 1-FCV-90-107 | 0.00000 | 05/15/94 |
| | 1-FCV-90-108 | 0.00000 | 05/15/94 |
| | 1-FCV-90-109 | 0.00000 | 05/15/94 |
| X-95B | 1-FCV-90-116 | 0.00000 | 05/15/94 |
| | 1-FCV-90-117 | 0.00000 | 05/15/94 |
| X-95C | 1-FCV-90-113 | 0.00000 | 05/18/94 |
| | 1-FCV-90-114 | 0.00000 | 05/18/94 |
| | 1-FCV-90-115 | 0.00000 | 05/18/94 |

Containment Isolation Valves (cont.)

| Penetration No. | Name | As Left | Date |
|--------------------|--------------|---------|----------|
| X-96A | 1-ISV-52-506 | 0.00000 | 02/16/94 |
| | 1-ISV-52-502 | 0.00000 | 02/16/94 |
| X-96B | 1-ISV-52-507 | 0.00000 | 02/16/94 |
| | 1-ISV-52-503 | 0.00000 | 02/16/94 |
| X-97 | 1-FSV-30-134 | 0.00000 | 05/28/94 |
| | 1-FSV-30-135 | 0.00000 | 05/28/94 |
| X-99 | 1-FCV-43-202 | 0.00000 | 06/08/94 |
| | 1-FCV-43-434 | 0.06322 | 06/08/94 |
| X-100 | 1-FCV-43-201 | 0.00000 | 06/08/94 |
| | 1-FCV-43-433 | 0.00000 | 06/08/94 |
| X-105 | 1-FSV-43-325 | 0.00000 | 06/09/94 |
| | 1-CKV-43-884 | 0.00000 | 06/09/94 |
| X-106 | 1-FSV-43-310 | 0.00000 | 06/20/94 |
| | 1-FSV-43-309 | 0.00000 | 06/20/94 |
| X-114 | 1-FCV-61-110 | 0.00000 | 05/04/94 |
| | 1-FCV-61-122 | 0.00000 | 05/04/94 |
| | 1-CKV-61-745 | 0.00000 | 05/04/94 |
| X-115 | 1-FCV-61-96 | 0.00000 | 05/04/94 |
| | 1-FCV-61-97 | 0.00000 | 05/04/94 |
| | 1-CKV-61-692 | 0.00000 | 05/04/94 |

Personnel Air Locks

| Penetration No. | Name | As Left | Date |
|--------------------|----------------|---------|----------|
| X-2A | Lower Air Lock | 7.00000 | 06/18/94 |
| X-2B | Upper Air Lock | 7.00000 | 06/18/94 |

Closed Systems Outside Containment

| Penetration No. | Name | As Left | Date |
|--------------------|------------------------------------|---------|------|
| X-99/100 | A Train H ₂ Analyzer | Later | |
| X-92A/92B | B Train H ₂ Analyzer | Later | |

Water Inventory Tests

| Penetration No. | Name | As Left | Date |
|--------------------|-------------|---------|------|
| X-48A | 1-FCV-72-39 | Later | |
| X-48B | 1-FCV-72-2 | Later | |
| X-49A | 1-FCV-72-40 | Later | |
| X-49B | 1-FCV-72-41 | Later | |

ENCLOSURE 2

LIST OF COMMITMENTS

1. TVA will perform leak rate testing (water inventory tests) required for the containment spray and residual heat removal (RHR) spray isolation valves, and leak rate testing for the hydrogen analyzer system loop test outside the hydrogen analyzer isolation valves. TVA anticipates these tests will be performed and any necessary repairs completed by September 30, 1994, to ensure leakage is within acceptable limits.
2. A supplemental report containing the final results of these local leak rate tests will be submitted to NRC within 30 days of work completion.

ENCLOSURE 1

WATTS BAR NUCLEAR PLANT UNITS 1 AND 2
SEVERE ACCIDENT MITIGATION DESIGN ALTERNATIVE
RESPONSE TO NRC'S REQUEST FOR ADDITIONAL INFORMATION

OCTOBER 7, 1994