

May 5, 1997

Mr. Oliver D. Kingsley, Jr.
President, TVA Nuclear and
Chief Nuclear Officer
Tennessee Valley Authority
6A Lookout Place
1101 Market Street
Chattanooga, Tennessee 37402-2801

SUBJECT: REQUEST FOR ADDITIONAL INFORMATION REGARDING SPENT FUEL POOL RERACK
FOR THE WATTS BAR NUCLEAR PLANT, UNIT 1 (TAC NO. M96930)

Dear Mr. Kingsley:

The NRC staff is continuing its review of the Tennessee Valley Authority's (TVA) application of October 23, 1996 for amendment of the Technical Specifications (TS) for Watts Bar Nuclear Plant, Unit 1 regarding the reracking of the spent fuel pool. Additional information, as identified in the enclosure, is requested to enable us to continue the review.

Sincerely,

Original signed

Robert E. Martin, Senior Project Manager
Project Directorate II-3
Division of Reactor Projects I/II
Office of Nuclear Reactor Regulation

Docket Nos. 50-390 and 50-391

Enclosure: Request for Additional Information

cc w/enclosure: See next page

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Mr. Michael H. Mobley, Director
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3rd Floor, L and C Annex
401 Church Street
Nashville, TN 37243-1532

**SECOND REQUEST FOR ADDITIONAL INFORMATION ON THE SPENT
FUEL POOL STORAGE RACK MODIFICATION AT WATTS BAR NUCLEAR PLANT UNIT 1**

1. The result of the maximum horizontal pedestal load is not given in Table 2.1 of the response to our request for additional information (RAI) question number 2. Provide it.
2. During the telephone conference on April 24, 1997, you indicated that the results of the safe shutdown earthquake (SSE) analysis in Table 2.1 are for the rack with the dimensions 8 ft X 9 ft. Confirm that this is in fact the rack dimension.
3. You indicated that the results of the SSE analysis in Table 2.1 for the rack (15 ft X 15 ft) are for the consolidated fuel load. The consolidated fuel is not related to the licensing amendment submitted. Submit appropriate analysis results with the intake fuel load for our review.
4. Provide a complete deformation shape of the rack from the bottom to the top for the single rack SSE analysis when the maximum displacement at the rack top corner equals 0.704 inch.
5. The result of the maximum displacement at the baseplate is not given in Table 2.2 of the response to our RAI question number 2. Provide it.
6. Provide a complete deformation shape of the rack for the multi-rack SSE analysis when the maximum displacement at the rack top corner equals 1.394 inches.
7. Indicate whether the rack dimension of 8 ft X 9 ft and the assumption of consolidated fuel are used for the multi-rack analysis.
8. You indicated in Table 4.1 that the elastic modulus of $2.76E+06$ psi was used for a stainless steel material in the rack analysis and design. It is a very small modulus for a stainless steel. Confirm that this is in fact the actual material property of the steel.
9. You stated in the January 14, 1997 meeting at NRC that the WBN Unit 1 does not have plug welds on the spent fuel pool liner and that all liner plates were welded to the embedded channels in the concrete. However, you corrected this in the response to our first RAI by stating that WBN used plug welds on the wall liner plates. Provide analysis results that demonstrate that there is no local buckling on the liner plate or a liner plate separation from the weld plug under the maximum temperature loading condition during an accident.

ENCLOSURE

10. In the response to our first RAI, you did not clearly describe how the floor liner plates were attached to the concrete base slab. Your response seems to indicate that the liner plates are not welded to the channels embedded in the concrete slab except the plates near to the concrete walls. If that is the case, you are requested to provide analysis results that demonstrate there is no buckling problem for the floor liner plates under the maximum temperature loading condition during an accident.