









EPRI/NRC-RES FIRE PRA METHODOLOGY

Module 2: Fire PRA Circuit Analysis Overview

D. Funk - Edan Engineering Corp. F. Wyant - Sandia National Laboratories Joint RES/EPRI Fire PRA Workshop July and August 2007 Palo Alto, CA

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CIRCUIT ANALYSIS Presentation Road Map

- Circuit Analysis "Big Picture" Overview
- Circuit Analysis Strategy & Implementation
- Introduction to Key Considerations & Factors
- Review and Discussion of Tasks
- Relationship to Appendix R & NFPA 805
- Examples

CIRCUIT ANALYSIS Circuit Analysis Tasks

- Task 3 Fire PRA Cable Selection
- Task 9 Detailed Circuit Analysis
- Task 10 Circuit Failure Mode Likelihood Analysis
- Support Task B Fire PRA Database

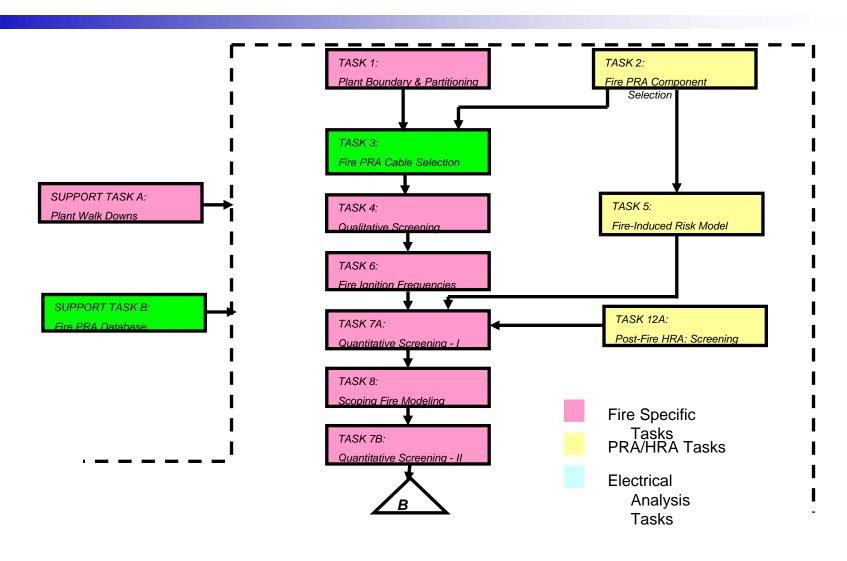
CIRCUIT ANALYSIS Circuit Analysis Overview

- Substantial Technical and Process-Related Advances
- Collective Awareness of Circuit Failure Implications Greatly Improved
- Knowledge Base Improvements
 - Fire Tests: EPRI, CAROLFIRE, Duke: Better but not perfect understanding of fire-Induced circuit failures
 - Working knowledge in applying test results
 - Practical experience from NFPA 805 transition projects

CIRCUIT ANALYSIS Circuit Analysis Overview

- Circuit Analysis is Now an Integral and Formal Part of the Fire PRA Process
 - Rigorous and formal process for correlating cables-to-equipmentto-affected locations
 - Definitive data and criteria has replaced estimations and judgment
 - Emerging trend to Integrate with Appendix R circuit analysis
- Further Refinements to "State-of-the-Art" Techniques Realistic
 - Practical aspects of dealing with an integrated data set
 - Practical approach for dealing with MSOs

CIRCUIT ANALYSIS PRA Task Flow Chart

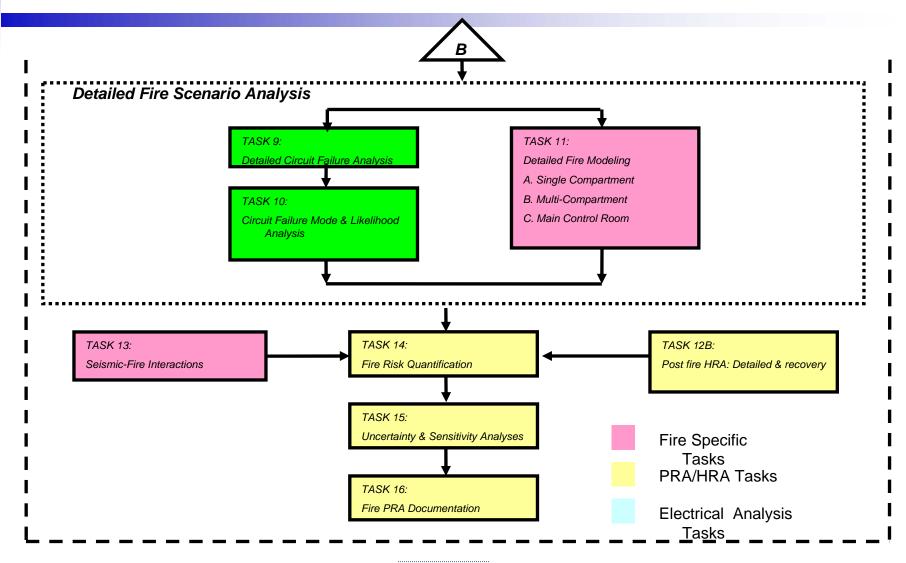


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CIRCUIT ANALYSIS PRA Task Flow Chart



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CIRCUIT ANALYSIS Overall Strategy & Implementation

- Each Electrical Analysis Task Represents a Refined Level of Detail, i.e., Graded Approach
- Level-of-Effort for the Electrical Work is a Key Driver for Project Scope, Schedule, and Resources
 - High Programmatic Risk if Not Carefully Controlled
 - Analysis and Routing of all Cables can be a Large Resource Sink with Minimal Overall Benefit
 - Concerns Validated by Numerous Projects
- Detailed Analysis Driven by Quantitative Screening Results
 - Intelligence-Based Circuit Analysis
 - Iterative Process
 - Conservative First Pass with Realism Incorporated Where it Matters

CIRCUIT ANALYSIS Overall Strategy & Implementation

- Recommended Methods are Consistent with Industry Best Practices
- Use Risk Perspectives to Streamline and Focus Analysis
- Remains a Technically and Logistically Challenging Area
- Limitations to the State-of-the-Art:
 - Number of Multiple Hot Shorts/Spurious Actuations
 - Spurious Actuation Probabilities
 - Timing Considerations

CIRCUIT ANALYSIS Overall Strategy & Implementation

- Circuit Analysis (including cable tracing) Can Consume 40%-70% of Overall Budget
- Circuit Analysis Scope MUST be a Primary Consideration During Project Scoping
- Qualified and Experienced Electrical Analysts Must be Integral Member of PRA Team
- Coordination and Integration with Appendix R Must Occur Early and Must be Rigorous
- Coordination with Task 2 (Component Section) is Essential – MUST Understand the EXACT Functionality Credited for Each Component

CIRCUIT ANALYSIS Key Considerations

- Relationship with Appendix R/NFPA 805 Analysis
- Long-Term Strategy for Data Configuration Control Especially if Shared Data with Appendix R
- Availability, Quality, and Format of Cable Data
- Usability of Appendix R Circuit Analysis Data
 - Recent Re-Analysis
 - Automated Tools
 - Many plants are finding that circuit analysis rebasline is necessary to support upgraded Fire PRA and Appendix R Associated Circuits (RIS 2004-003)
- User-Friendliness of Electrical Drawings
- Off-Site Power Analysis
- Availability of Electrical Engineering Support

CIRCUIT ANALYSIS Summary

- Do Not Underestimate Scope
- Ensure Proper Resources are Committed to Project
- Very Doable But MUST Work Smart
- Do Not "Broad Brush" Interface with Appendix R Have a Detailed Plan Before Starting
- Constant Interaction with Systems Analysts Critical
- Develop Project Procedures But Don't Get Carried Away
- Compilation and Management of Large Volume of Data
 - Automated Tools Imperative for Efficient Process
 - Be Mindful of Long-Term Configuration Management











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Module 2: Task 3 - Fire PRA Cable Selection

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FIRE PRA CABLE SELECTION Purpose & Scope

- Identify Circuits/Cables Associated with Fire PRA Components
- Determine Routing/Location of the Identified Cables
- Use Component-to-Cable-to-Location Relationships to Determine What Components Could be Affected for Postulated Fire Scenarios

Note: Scenario can be Fire Area, Room, Raceway, or Other Specific Location

Identify Fire PRA Power Supplies

FIRE PRA CABLE SELECTION

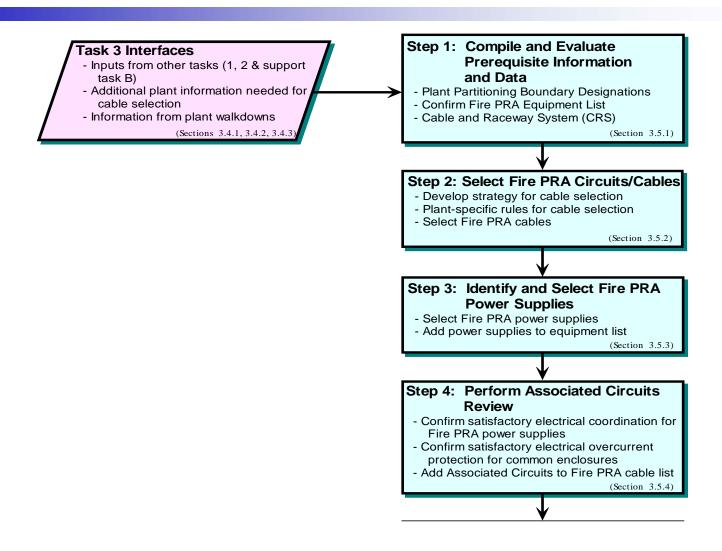
Introduction

Conducted for all Fire PRA Components

Note: Exceptions do exist

- Deterministic Process
- Cables Associated to Components Irrespective of Failure Mode
 - Some circuit analysis incorporated to prevent overwhelming the PRA model with inconsequential cable failures
 - Final product is a listing of components that could be impacted by a fire for a given location (Fire Area, Fire Compartment, Fire Scenario)
- Procedure subdivided into six (6) distinct steps

FIRE PRA CABLE SELECTION Flowchart



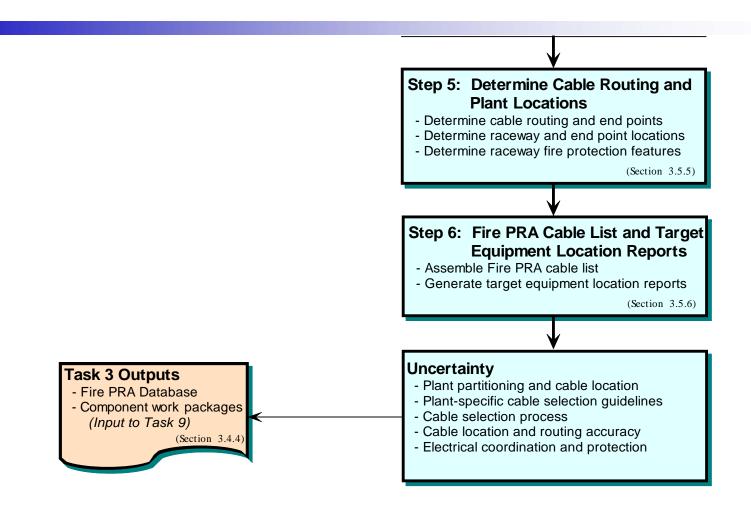
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Module 2: Task 3 - Fire PRA Cable Selection

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FIRE PRA CABLE SELECTION Flowchart



FIRE PRA CABLE SELECTION Task Interfaces - Input

- Plant Boundary Partitions (Task 1)
- Fire PRA Component List (Task 2)
- Fire PRA Database (Support Task B)
- Appendix R Circuit Analysis
- Plant Cable & Raceway Database
- Plant Drawings

FIRE PRA CABLE SELECTION Task Interfaces - Output

- Fire PRA Cable List
- Fire PRA Power Supply List
- Associated Circuits review
- Component Analysis Packages
- Target Equipment Location Reports (Potential Equipment Losses Broken Down by Location or Scenario)

FIRE PRA CABLE SELECTION Step 1 – Prerequisite Information

- Confirm Plant Partitioning is Compatible
 - Do partitions align with cable location data?
- Confirm PRA Equipment List is Final
 - Input into a formal and controlled database
- Evaluate Database Requirements
 - What currently exists?
 - What is needed to support work?
 - How is data to be managed and controlled?
 - This is a "Biggy"

FIRE PRA CABLE SELECTION Step 2 – Select Fire PRA Cables

Analysis Cases

- Appendix R Component with Same Functional Requirements
- Appendix R Component with Different Functional Requirements
- Non-Appendix R Component with Cable Location Data
- Non-Appendix R Component without Cable Location Data

Analysis Sub-Steps

- Step 2.1 Analysis Strategy
- Step 2.2 Plant Specific Rules
- Step 2.3 Select Cables

FIRE PRA CABLE SELECTION Step 2.1 – Analysis Strategy

- Coordinate with Systems Analysts to Establish Functional Requirements and General Rules
 - Equipment functional states, basic events, initiators
 - Initial conditions and equipment lines (i.e., normal state)
 - Consistent conventions for equipment functions/state/position
 - Multiple function components
- Evaluate Appendix R Component & Circuit Data
 - Ensure equipment list comparison conducted during Task 2
 - Review in detail the comparison list ask questions
 - Essential that comparison includes detailed review/comparison of "desired functional state(s)"

FIRE PRA CABLE SELECTION Step 2.1 – Analysis Strategy

- Goal Efficient and Accurate Process to Obtain Required Information
- Revisit Past Assumptions, Conventions, Approach
- Potential Trouble Areas
 - How is off-site power going to be handled?
 - Instrument circuits understand exactly what is credited
 - ESAFA, Load-Shed, EDG Sequencer
 - Medium-voltage switchgear control power
- Extent of Detailed Analysis to be Conducted Concurrently
- Determine How Analysis Will be Documented

FIRE PRA CABLE SELECTION Step 2.2 – Plant Specific Cable Selection Rules

- Objective is Consistency
- Approach for Groups of Components
- Approach for Spurious Actuation Equipment
- Auxiliary Contacts
- System-Wide Actuation Signals
- Bus or Breaker?
- Subcomponents
- Identification of Permanent Damage Scenarios
- Procedure Develop Circuit Analysis Procedure/Guidelines

FIRE PRA CABLE SELECTION Step 2.2 – Ready to Start?

- Develop Written Project Procedure/Guidelines
 - Consistency, Consistency
 - Checking Process?
 - Problem Resolution
- Training for Analysts

FIRE PRA CABLE SELECTION Step 2.3 – Select Cables

- Case 1: Incorporate Existing Appendix R Analysis
 - Confirm adequacy of existing analyses IAW plan
- Cases 2 & 3: New Functional State/Component: w/ Cable Routing Data
 - Collect drawings and/or past analysis information
 - Identify/select cables IAW plant specific procedure/guidelines
 - Conduct detailed analysis to the extent decided upon
 - Formally document cable selection IAW established procedures/guidelines

FIRE PRA CABLE SELECTION Step 2.3 – Select Cables

- Case 3: New Component: w/o Cable Routing Data Available
 - Same as Case 2 & 3, plus...
 - Determine cable routing and associate with plant locations
- Analysis Work Packages
 - Retrieve from Past Appendix R Analysis
 - Highly Recommended for New Components
 - Major time saver for future work

FIRE PRA CABLE SELECTION Step 3 – Select Fire PRA Power Supplies

- Identify Power Supplies as Integral Part of Cable Selection
 - Make sure to differentiate between "Required" and "Not Required" power supplies
 - Switchgear and Instrument power supplies can be tricky
- Add Power Supplies to Fire PRA Component List
- Make sure Fire PRA model, equipment list, and electrical analysis are consistent
- Does Fire PRA model consider spurious circuit breaker operations?

FIRE PRA CABLE SELECTION Step 4 – Associated Circuits Review

- Objective is to Confirm Existing Studies Adequate
- View the Process as a "Gap Analysis"
- Common Power Supply Circuits Assess Plant Coordination Studies
- Common Enclosure Circuits Assess Plant Electrical Protection
- Roll Up Results to Circuit Analysis or Model as Appropriate

Note: Ensure Switchgear Internal Fusing Supports Analysis Assumptions

FIRE PRA CABLE SELECTION Step 5 – Determine Cable Routing and Locations

- Correlate Cables-to-Raceways-to-Locations
- Conceptually Straightforward
- Logistically Challenging
 - Labor intensive
 - Manual review of layout drawings
 - Plant walkdowns often required
- Determine Cable Protective Features
 - Fire wraps
 - Embedded conduit

FIRE PRA CABLE SELECTION Step 6 – Target Equipment Loss Reports

- Data Entered into Fire PRA Database
- Sorts and Queries to Generate Target Equipment Location Reports

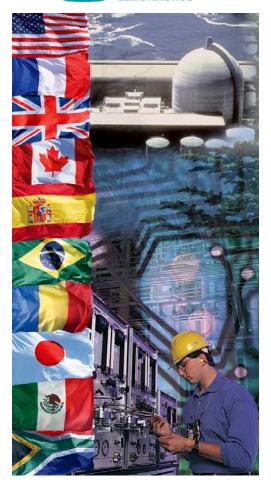
Perspective....Cable selection process should be viewed as providing "Design Input" to the Fire PRA. It does not, however, provide any risk-based results. In its simplest form it provides a list of equipment that could be affected by a fire at a specified location or for a specific scenario.











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Module 2: Task 9 - Detailed Circuit Failure Analysis

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July and August 2007
Palo Alto, CA

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DETAILED CIRCUIT FAILURE ANALYSIS Purpose & Scope

The Detailed Circuit Failure Analysis Task is intended to:

- Identify the potential response of circuits and components to specific cable failure modes associated with fireinduced cable damage
- Screen out cables that do not impact the ability of a component to complete its credited function

DETAILED CIRCUIT FAILURE ANALYSIS *Introduction (1)*

- Fundamentally a deterministic analysis
- Conduct coincident with cable selection (Task 3) to the extent feasible and cost effective
- Difficult cases generally reserved for situations in which Quantitative Screening indicates a clear need and advantage for further analysis
- Detailed Failure Modes Analysis
 - Requires knowledge about desired functionality and component failure modes
 - Conductor-by-conductor evaluation (Hot Probe method recommended)
- Objective is to screen out all cables that CANNOT impact the ability of a component to fulfill the specific function of interest

DETAILED CIRCUIT FAILURE ANALYSIS Introduction (2)

- Failure Modes Considered
 - Single Shorts-to-Ground (Reference Ground)
 - Grounded System
 - Ungrounded System
 - Resistance Grounded System
 - Single Hot Shorts
 - Compatible Polarity Multiple Hot Shorts for Ungrounded AC and DC Circuits
 - Coincident Independent Hot Shorts On Separate Cables
 - Multiple Intra-cable Hot Shorts
 - Cables Associated Through Common Power Supply

DETAILED CIRCUIT FAILURE ANALYSIS Introduction (3)

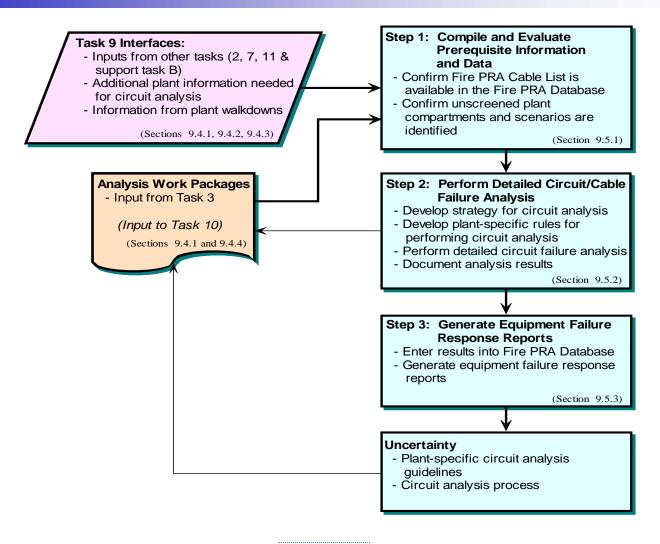
- Failure Modes NOT Considered
 - 3-phase proper sequence hot shorts (except high consequence equipment and thermoplastic insulated conductor)
 - Inter-cable hot shorts for armored cable and cable in dedicated conduit
 - Open circuit conductor failures
 - Multiple high-impedance faults

DETAILED CIRCUIT FAILURE ANALYSIS Assumptions

The Following Assumptions Form the Basis for Task 9:

- An Appendix R analysis for the plant has been completed and is available for identifying equipment failure responses to specific cable failure modes
- Component Work Packages have been assembled as part of the Task 3 activities or previous Appendix R analyses
- Equipment is assumed to be in its normal position or operating condition at the onset of the fire – the equipment state might be variable
- Users of this procedure are knowledgeable on and have experience with circuit design and analysis methods

DETAILED CIRCUIT FAILURE ANALYSIS Flowchart



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Module 2: Task 9 - Detailed Circuit Failure Analysis

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DETAILED CIRCUIT FAILURE ANALYSIS Task Interfaces - Inputs

- Fire PRA Components List (Task 2)
- Fire PRA Cable List (Task 3)
- Fire PRA Database (Support Task B)
- Results of Quantitative Screenings (Task 7)
- Results of Detailed Fire Modeling (Task 11)
- Appendix R Circuit Analysis
- Plant Drawings
- CRS Database

DETAILED CIRCUIT FAILURE ANALYSIS Task Interfaces - Outputs

- Equipment Failure Response Reports
- Component Analysis Packages (Updated)
- Revised Cable List
- Fire PRA Database & Model Updates

DETAILED CIRCUIT FAILURE ANALYSIS Step 1 - Compile Prerequisite Information

- Ensure that prerequisite information and data is available and usable before beginning the analyses (ideally the necessary drawings are already in the Work Packages).
- Step 1.1: Confirm Fire PRA Cable List is Available in the Fire PRA Database
 - Component ⇒ Cable ⇒ Raceway ⇒ Compartment
- Step 1.2: Confirm Unscreened Plant Compartments and Scenarios are Identified
 - Target Equipment Location Reports
 - Equipment ID, Normal Status, Functional Requirements, etc.

DETAILED CIRCUIT FAILURE ANALYSIS Step 2 - Perform Circuit Failure Analysis

- Perform a Deterministic-Based detailed circuit analysis for the Fire PRA cables of interest that are located in the unscreened plant locations.
- Step 2.1: Develop Strategy/Plan for Circuit Analysis
- Step 2.2: Develop Plant-Specific Rules for Performing the Detailed Circuit Analysis
- Step 2.3: Perform Detailed Circuit Failure Analysis
- Document Analysis Results ⇒ Component Work Packages

DETAILED CIRCUIT FAILURE ANALYSIS Step 3 - Generate Equipment Failure Response Reports

- Enter Results into Fire PRA Database
- Generate Equipment Failure Response Reports
 - A Listing by location (room, zone, area) of equipment and associated cables affected by fire
 - Provides specific equipment responses that are possible as a result of fire damage to the cables
 - May only need to track equipment responses of concern to the PRA Model

DETAILED CIRCUIT FAILURE ANALYSIS Caveats & Recommendations

- This Detailed Circuit Failure Analysis Methodology is a Static Analysis (No Timing Issues are Considered)
- Be Aware of Possible Cable Logic Relationships
- Work Packages (Highly Recommended!)
- "Hot Probe" (Conductor-to-Conductor) Analysis Must be Rolled-Up to Cable/Component Level
- Outputs Need to Be Compatible with Fire PRA Database Format and Field Structure
- Coordinate with the Fire PRA Modelers/Analysts Early-On to Define the Fire PRA Component Failure Modes of Concern











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Module 2: Task 10 - Circuit Failure Mode Likelihood Analysis

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CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS Purpose & Scope

The Circuit Failure Mode Likelihood Analysis Task is Intended to:

 Establish First-Order Probability Estimates for the Circuit Failure Modes of Interest

AND

Correlate Those Failure Mode Probabilities to Specific Components

CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS Introduction (1)

- Probabilistic Based Analysis
- Two Methods Presented
 - Expert Panel Results (Look-Up Tables)
 - Computation-Based Analysis (Formulas)
- Requires Knowledge About Circuit Design, Cable Type and Construction, Installed Configuration, and Component Attributes
- Generally Reserved for Only Those Cases that Cannot be Resolved Through Other Means

CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS Introduction (2)

Caveats:

- Our Knowledge is Greatly Improved but <u>Uncertainties are Still High</u>
 - Very limited data for many issues
- For This Reason, Implementing Guidance is Conservative
- Practical Implementation is Challenging
- Further Analysis of Existing Test Data and Follow-On Tests Would be Beneficial:
 - Reduce Uncertainties, including conservatisms as appropriate
 - Solidify Key Influence Factors
 - Incorporate Time as a Factor
 - Incorporate "End-Device" Functional Attributes and States (e.g., latching circuits vs. drop-out design)
- Computation-based method (formula) is an extrapolation of existing data; validation remains to be done. Conservatism has not been established.
- Probabilities of sufficient quality to move ahead

CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS Introduction (3)

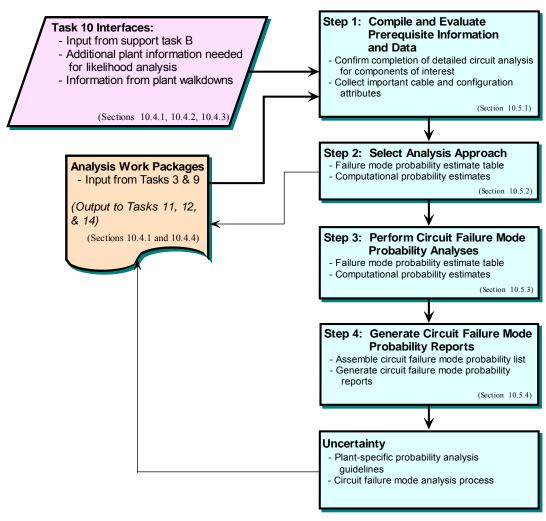
- Public and Peer Review Comments
 - Several Questions Involving Interpretation of the EPRI Test Data Lead to Extensive Discussions Regarding the Most Appropriate Way to Tally Spurious Actuation Probabilities (Many Subtleties for Implementation)
 - Team's Consensus is that Expert Panel Values are, in General, somewhat Conservative
 - Additional Independent Review of the Computational Method was Solicited as a Result of Peer and Public Comments
 - Review was Favorable, However the Team Acknowledges the Inevitable Limitations With a "Version 1.0" Release

CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS Assumptions

The Following Assumptions Form the Basis for Task 10:

- Specific Cable/Circuit Configuration Attributes are Available or Can Be Determined
- The Equipment is in Its Normal Position or Operating Condition at the Onset of the Fire
- Users of This Procedure are Knowledgeable and Have Experience with Circuit Design and Analysis Methods and Probability Estimating Techniques
- This Analysis Method is Applied to Cables with No More than 15 Conductors

CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS Flowchart



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Module 2: Task 10 - Circuit Failure Mode Likelihood Analysis

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CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS Task Interfaces - Inputs

- Fire PRA Cable List (Task 3)
- Fire PRA Database (Support Task B)
- Results of Detailed Circuit Failure Analysis (Task 9)
- Specific Scenarios Identifying Affected Cables (Tasks 11 & 14)
- Cable & Circuit Configuration Attributes
- Plant Drawings

CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS Task Interfaces - Outputs

- Quantification of Fire Risk (Task 14)
- Post-Fire HRA (Task 12)
- Detailed Fire Scenario Quantification (Task 11)
- Circuit Failure Mode Probability Reports
- Component Work Packages (Finalized)
- Fire PRA Database & Model

CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS Step 1 - Compile Prerequisite Information

Ensure that Prerequisite Information and Data is Available and Usable before Beginning the Analyses.

- Confirm Completion of Detailed Circuit Analysis for Components of Interest
- Collect Important Cable and Configuration Attributes
 - Insulation
 - Number of Conductors
 - Raceway Types
 - Power Source(s)
 - Number of Source & Target Conductors (for Option #2 Only)

CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS Step 2 - Select Analysis Approach

Decide Which Analysis Option is Best Suited for Conducting the Evaluation.

1. Failure Mode Probability Estimate Tables

- Grounded Circuit Design
- Non-Complex Control Circuit
- Single Component Service
- Cable Configuration Matches Table Categories
- Principal Failure Mode of Concern is Spurious Actuation

2. Computational Probability Estimate Formulas

- Ungrounded or Resistance-Grounded Circuit Design
- Complex Circuit or Component
- Failure Potentially Affects Multiple Components
- Cable Configuration Not Easily Categorized in Tables

CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS Step 3 - Estimate Circuit Failure Mode Probabilities

Estimate Circuit Failure Mode Probabilities Employing the Selected Method

Option #1: Failure Mode Probability Estimate Tables

- •Table 10-1, Thermoset Cables with CPTs
- Table 10-2, Thermoset Cables without CPTs
- •Table 10-3, Thermoplastic Cables with CPTs
- Table 10-4, Thermoplastic Cables without CPTs
- •Table 10-5, Armored or Shielded Cables

Option #2: Computational Probability Estimate Formulas

$$P_{CC} = (C_{Tot} - C_G) / [(C_{Tot} - C_G) + (2 \times C_G) + n]$$

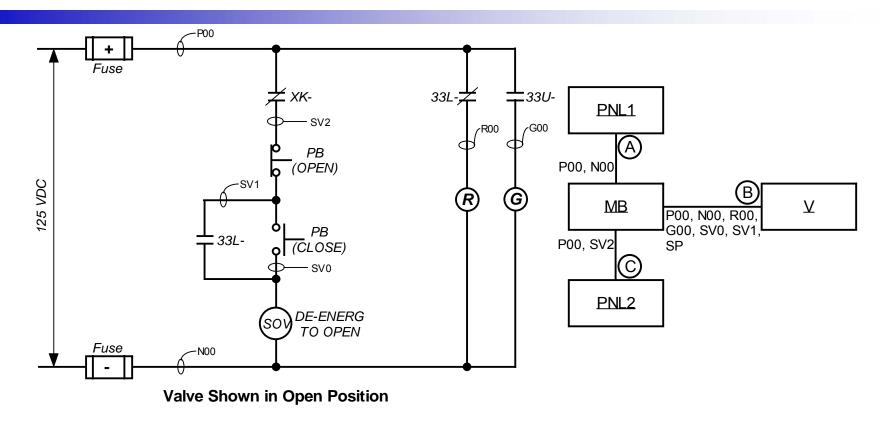
$$CF = \{C_T \times [C_S + (0.5 / C_{Tot})]\} / C_{Tot}$$

$$P_{FM} = CF \times P_{CC}$$

CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS Step 4 - Generate Failure Mode Probability Reports

- Enter Results into Fire PRA Database
- Generate Circuit Failure Mode Probability Reports
 - Listing the Probability Estimates for the Circuit Failure Modes of Concern for Each Component of Interest by Plant Area (Compartment, Fire Area, Fire Zone, etc.)

CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS Example - SOV Control Circuit



QUESTION: What is the <u>probability</u> that damage to Cable B will result in spurious closure of the SOV?

See next slide >

CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS Example – Step 1: Prerequisite Information

Detailed circuit analysis completed & documented? Yes

Cable	+125 VDC Hot Probe	-125 VDC Hot Probe	
А	LOC	LOC	
В	LOC, EI, SO - Close	LOC	
С	NC	LOC	

Collect important cable and configuration data:

– Cable insulation? Thermoset

Number of conductors? Seven

– Raceway type? Tray

– Power source? Ungrounded DC bus (no CPT)

Number of source & target conductors? 3 sources, 1 target

See next slide >

CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS Example – Step 2: Select Analysis Approach

Option #1: Failure Mode Probability Tables

– Grounded circuit design?	No
----------------------------	----

– Control circuit cable? Yes

– Single component circuit? Yes

– Known cable configuration? Yes

Spurious operation concern? Yes

Option #2: Computational Probability Estimate

– Ungrounded circuit? Yes

– Complex circuit/component? No

– Multiple component circuit? No

Cable configuration not categorized? No

For this example, we'll show both methods

See next slide >

CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS Example – Step 3: Perform Analysis (1)

- Option #1:
 - Which Table to Use? Table 10-2, Thermoset Cable without CPT

Raceway Type	Description of Hot Short	Best Estimate	High Confidence Range
Tray	M/C Intra-cable 1/C Inter-cable M/C → 1/C Inter-cable M/C → M/C Inter-cable	0.60 0.40 0.20 0.02 – 0.1	0.20 - 1.0 0.1 - 0.60 0.1 - 0.40
Conduit	M/C Intra-cable 1/C Inter-cable M/C → 1/C Inter-cable M/C → M/C Inter-cable	0.15 0.1 0.05 0.01 – 0.02	0.05 - 0.25 0.025 - 0.15 0.025 - 0.1

- Probability Estimate, P = 0.62 (0.60 + 0.06 - 0.60*0.06)

See next slide →

CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS Example – Step 3: Perform Analysis (2)

• Option #2:

Calculate probability of a conductor-to-conductor short:

$$P_{CC} = (C_{Tot} - C_G) / [(C_{Tot} - C_G) + (2 * C_G)]$$

$$P_{CC} = (7 - 1) / [(7 - 1) + (2 * 1)]$$

$$P_{CC} = 6 / [6 + 2]$$

$$P_{CC} = 0.75$$

– Determine cable configuration factor:

$$CF_{SO} = \{C_T * [C_S + (0.5 / C_{Tot})]\} / C_{Tot}$$

$$CF_{SO} = \{1 * [3 + (0.5 / 7)]\} / 7$$

$$CF_{SO} = 3.071 / 7$$

$$CF_{SO} = 0.44$$

- Probability of spurious operation, $P_{SO} = 0.75 * 0.44 = 0.33$

CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS Example – Step 4: Failure Mode Probability Report

Failure Code	Estimated Probability (Calculated)	Estimated Probability (From Table 10-2)
SO (Closed)	0.33	0.62

Task 10: Circuit Failure Mode Likelihood Analysis Methodology

This document summarizes the process for determining the probability, or likelihood, of a particular circuit failure mode occurrence. It includes the five Failure Mode Probability Estimate Tables employed under the Option #1 analysis approach, and the Option #2 Computational Probability Estimate formulas. **Important!** Please refer to the complete discussion of this methodology provided in NUREG/CR-6850, EPRI 1011989, "EPRI/NRC-RES Fire PRA Methodology for Nuclear Power Facilities; Volume 2: Detailed Methodology," Final Report, September 2005.

Selecting the Analysis Approach

1. Option #1: Failure Mode Probability Estimate Tables

Tables of probability estimates would appropriately be used for cables that meet the following criteria:

- The circuit is of a grounded design (including impedance grounded systems with ground fault trip capability),
- The cable is part of the control circuit for a typical component (e.g., non-complex MOVs, SOVs, pumps),
- The cable is associated with a single component,
- The cable configuration is known and can be readily associated with one of the defined configurations in Tables 1 through 5, and
- The principal hot short failure mode of concern is a spurious operation of the component.
- 2. Option #2: Computational Probability Estimates

Use of the probability estimate formulas are recommended for cases where:

- The circuit is ungrounded or is impedance grounded without ground fault trip capability,
- The cable is part of a relatively complex circuit or component,
- The cable is associated with or can influence the behavior of multiple components (e.g., safeguards actuation signal, bus shed scheme, etc.),
- The cable configuration is not easily categorized into one of the defined configurations contained in Tables 1 through 5.

Performing the Circuit Failure Mode Probability Analyses

Option #1: Failure Mode Probability Estimate Tables

1. Categorize the circuit of interest based on its configuration attributes.

- 2. From the appropriate table (Tables 1 to 5), select the probability estimates for the failure modes of concern.
- 3. If the cable failure mode can occur due to different cable interactions, the probability estimate is taken as the simple sum of both estimates. For example, if a particular thermoset cable failure mode can be induced either by an intra-cable shorting event (P = 0.30) or by an inter-cable shorting event (P = 0.03; mid-range of 0.01-0.05), the overall probability of that failure mode is estimated to be 0.33.

Table-1
Failure Mode Probability Estimates Given Cable Damage
Thermoset Cable with Control Power Transformer (CPT)

Raceway Type	Description of Hot Short	Best Estimate	High Confidence Range
Tray	M/C Intra-cable 1/C Inter-cable M/C → 1/C Inter-cable M/C → M/C Inter-cable	0.30 0.20 0.10 0.01 – 0.05	0.10 - 0.50 0.05 - 0.30 0.05 - 0.20
Conduit	M/C Intra-cable 1/C Inter-cable M/C → 1/C Inter-cable M/C → M/C Inter-cable	0.075 0.05 0.025 0.005 – 0.01	0.025 - 0.125 0.0125 - 0.075 0.0125 - 0.05

M/C: Multi-conductor cable 1/C: Single conductor cable

Intra-cable: An internally generated hot short. The source conductor is part of the cable of interest Inter-cable: An externally generated hot short. The source conductor is from a separate cable

Table-2
Failure Mode Probability Estimates Given Cable Damage
Thermoset Cable without CPT

Raceway Type	Description of Hot Short	Best Estimate	High Confidence Range
Tray	M/C Intra-cable 1/C Inter-cable M/C → 1/C Inter-cable M/C → M/C Inter-cable	0.60 0.40 0.20 0.02 – 0.1	0.20 - 1.0 0.1 - 0.60 0.1 - 0.40
Conduit	M/C Intra-cable 1/C Inter-cable M/C → 1/C Inter-cable M/C → M/C Inter-cable	0.15 0.1 0.05 0.01 – 0.02	0.05 - 0.25 0.025 - 0.15 0.025 - 0.1

Table-3
Failure Mode Probability Estimates Given Cable Damage
Thermoplastic Cable with CPT

Raceway Type	Description of Hot Short	Best Estimate	High Confidence Range
Tray	M/C Intra-cable 1/C Inter-cable M/C → 1/C Inter-cable M/C → M/C Inter-cable	0.30 0.20 0.10 0.01 – 0.05	0.10 - 0.50 0.05 - 0.30 0.05 - 0.20
Conduit	M/C Intra-cable 1/C Inter-cable M/C → 1/C Inter-cable M/C → M/C Inter-cable	0.075 0.05 0.025 0.005 – 0.01	0.025 - 0.125 0.0125 - 0.075 0.0125 - 0.05

Table-4
Failure Mode Probability Estimates Given Cable Damage
Thermoplastic Cable without CPT

Raceway Type	Description of Hot Short	Best Estimate	High Confidence Range
Tray	M/C Intra-cable 1/C Inter-cable M/C → 1/C Inter-cable M/C → M/C Inter-cable	0.60 0.40 0.20 0.02 – 0.1	0.20 - 1.0 0.1 - 0.60 0.1 - 0.40
Conduit	M/C Intra-cable 1/C Inter-cable M/C → 1/C Inter-cable M/C → M/C Inter-cable	0.15 0.1 0.05 0.01 – 0.02	0.05 - 0.25 0.025 - 0.15 0.025 - 0.1

Table-5
Failure Mode Probability Estimates Given Cable Damage
Armored or Shielded Cable

Raceway Type	Description of Hot Short	Best Estimate	High Confidence Range
With CPT	M/C Intra-cable	0.075	0.02 – 0.15
Without CPT	M/C Intra-cable	0.15	0.04 – 0.30

3. When more than one cable can cause the component failure mode of concern, and those cables are within the boundary of influence for the scenario under investigation, the

probability estimates associated with all affected cables should be considered when deriving a failure estimate for the component. In general, the probabilities should be combined as follows:

$$P_{Component failure} = (P_{Failure Cable A}) + (P_{Failure Cable B}) - (P_{Failure Cable A})(P_{Failure Cable B})$$

Option #2: Computational Probability Estimates

Application of this calculational method is more complex and is only recommended for cases where Option #1 cannot reasonably be applied. The intent is to give the analyst a means of refining the estimated circuit failure mode probabilities based on the most important characteristics of the cable/circuit under study.

This computational method involves applying circuit failure mode probability estimation formulas. The following discussions provide only the minimum definition of the failure mode likelihood estimation formulas and their terms. For a complete discussion of the technical basis, detailed explanations, and examples of usage, please refer to Appendices J and K in Volume 2 of EPRI 1011989, NUREG/CR-6850.

The probability of occurrence for a specific hot short failure mode (P_{FM}) is estimated by the formula:

$$P_{FM} = CF \times P_{CC}$$

Where:

 P_{FM} = The probability that a specific hot short failure mode of interest will occur in a specific circuit given a fire of sufficient intensity to cause cable damage,

 P_{CC} = The probability that a conductor-to-conductor short will occur prior to a short-to-ground or short to a grounded conductor, and

CF = A configuration factor applied to P_{CC} to account for the relative number of source conductors and target conductors. Target conductors are those conductors of a circuit that, if contacted by an electrical source of proper magnitude and voltage, will result in abnormal energization of the circuit, component or device of concern. Source conductors represent energized conductors that are a potential source of electrical energy.

1. Calculate P_{CC} as follows:

Cables in trays: $P_{CC} = (C_{Tot} - C_G) / [(C_{Tot} - C_G) + (2 \times C_G) + 1]$

Cables in conduit¹: $P_{CC} = (C_{Tot} - C_G) / [(C_{Tot} - C_G) + (2 \times C_G) + 3]$

Ungrounded systems: $P_{CC} = (C_{Tot} - C_G) / [(C_{Tot} - C_G) + (2 \times C_G)]$

¹ Armored and shielded cable should use the equation for conduit.

Where:

 $C_{Tot} = The total number of conductors in the cable of interest (including spares), and$

C_G = The number of grounded (or common) conductors in the cable of interest. The analyst should determine the number of grounded/common conductors based on the circuit configuration (contact positions, etc.) that represent the normal operating state of the component. If this information is unavailable or indeterminate, the worst-case conditions should be assumed.

Note: For ungrounded AC and DC systems, C_G represents the number of return conductors to the power source associated with the circuit of interest (e.g., the negative polarity conductors for an ungrounded 125 VDC circuit)

2. Calculate CF as follows.

Non-armored cables: $CF = \{C_T \times [C_S + (0.5 / C_{Tot})]\} / C_{Tot}$

Armored cables: $CF = (C_T \times C_S) / C_{Tot}$

Where:

 C_S = The total number of source conductors in the cable under evaluation,

 C_T = The total number of target conductors in the cable², and

 C_{Tot} = The total number of conductors in the cable, as before.

Note: CF should be ≤ 1.0 . If the calculated value of CF is greater than 1, then set CF = 1. In practical applications it is highly unlikely that the calculated value of CF will ever exceed 1. For this to occur, virtually all conductors in the cable would need to be either a source conductor or target conductor.

Note: The analyst should determine the number of target and source conductors based on the circuit configuration (contact positions, etc.) that represents the normal operating state of the component. If this information is unavailable or indeterminate, the worst-case conditions should be assumed.

3. Calculate P_{FM} as follows:

$$P_{FM} = CF \times P_{CC}$$

where CF and P_{CC} are determined using the formulas discussed above.

4. When more than one cable can cause the component failure mode of concern, and those cables are within the boundary of influence for the scenario under investigation, the

² Target conductors are only those cable conductors capable of forcing the component or circuit into the undesired state or condition of interest. For example, the target conductors associated with causing a spurious operation of the component will likely differ from target conductors associated with causing a loss of control condition.

probability estimates associated with all affected cables should be considered in deriving a failure estimate for the component. In general, the probabilities should be combined as follows:

 $P_{\text{Component failure}} = (P_{\text{Failure Cable A}}) + (P_{\text{Failure Cable B}}) - (P_{\text{Failure Cable A}})(P_{\text{Failure Cable B}})$











EPRI/NRC-RES FIRE PRA METHODOLOGY

Module 2: Support Task B - Fire PRA Database

D. Funk - Edan Engineering Corp. F. Wyant - Sandia National Laboratories Joint RES/EPRI Fire PRA Course July and August 2007 Palo Alto, CA

A Collaboration of U.S. NRC Office of Nuclear Regulatory Research (RES) & Electric Power Research Institute (EPRI)

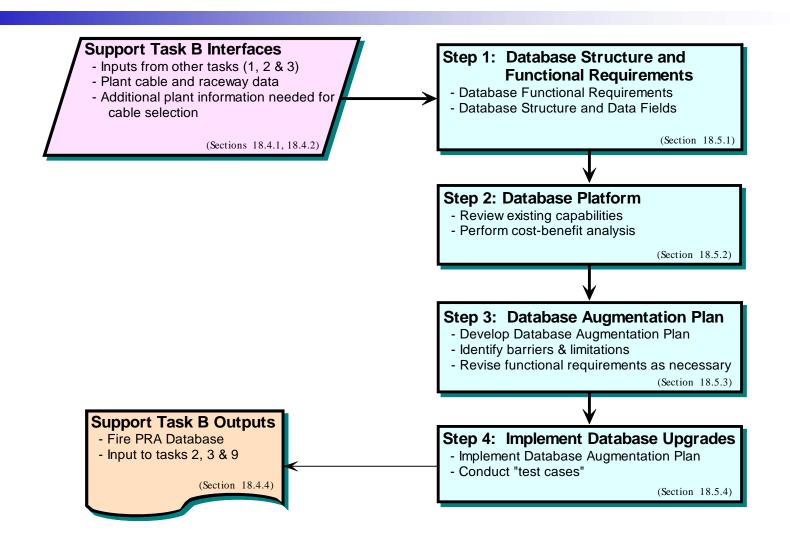
FIRE PRA DATABASE Purpose & Scope

- Identify Required Database Functionality
- Assess Capability of Existing Systems
- Implement Structured Process to Obtain the Required Database Capability
- New Software and Data Management Tools are Finding Their Way Into the Market

FIRE PRA DATABASE Introduction

- Task is Distinctly Different from Other Tasks
- Essential Element of PRA
 - Proposed Methods Require Manipulation and Correlation of Large Amounts of Data
 - Must be Efficient and User Friendly for Effective Implementation
 - Manual Analysis Not Practical

FIRE PRA DATABASE Flowchart



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Module 2: Support Task B - Fire PRA Database

Slide 4

FIRE PRA DATABASE Step 1.1 - Database Functional Criteria

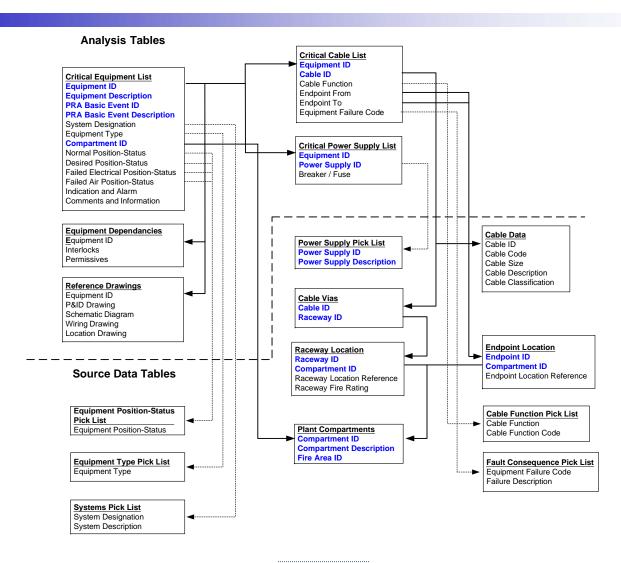
Data Input Criteria

- In what shape and format is existing data?
- How and who will entered and control data?
- Will data be shared by separate groups? If so, who can change data?

Data Output Criteria

- Define Required Output Reports
- Define Sort and Query Options

FIRE PRA DATABASE Step 1.2 - Database Structure (Example A)



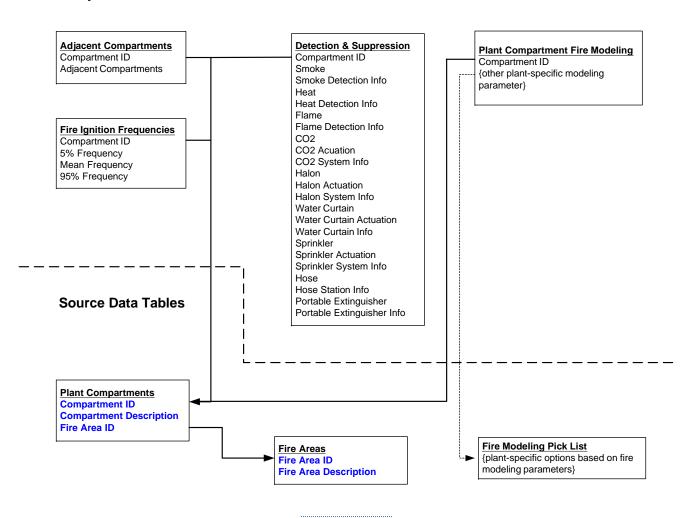
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FIRE PRA DATABASE Step 1.2 - Database Structure (Example A)

Analysis Tables

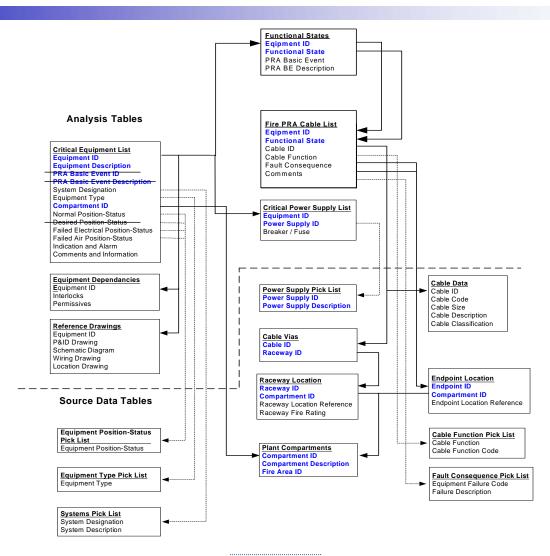


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Module 2: Support Task B - Fire PRA Database

Slide 7

FIRE PRA DATABASE Step 1.2 - Database Structure (Example B)



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Module 2: Support Task B - Fire PRA Database

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FIRE PRA DATABASE Step 2 - Database Platform

- Decide on Platform for Database
 - Existing System
 - New Stand Alone System
 - Upgrade Existing System
 - Combination of Existing and New
- Vendors are Responding to the Call for New and Improved Software Functionality
 - Highly Integrated Solutions are Emerging as the Standard for NFPA 805 Plants
 - Seamless Link to Fire PRA Software is in the Works But Not Yet Available as Production Software

FIRE PRA DATABASE Step 3 - Database Augmentation Plan

- Augmentation Plan is Based on the Results of Step 2
- Formalize Process for Upgrades/Changes
- Determine Necessary Resources
 - This Effort Can Innocently Affect Many Plant Organizations
 - The Cost, Resources, Schedule, Training, Procedural Changes and Overall Impact of Major Software Changes ALWAYS Seems to be Underestimated
- Involve IS/IT Department from the Beginning

FIRE PRA DATABASE Step 4 – Implement Database Upgrades

- Have a Clear Plan BEFORE Beginning any Significant Work
- Consider Long-Term Maintainability
- Plan for De-bugging and Test Runs
- Do Not Overlook Data Integrity and Configuration Control Features
- Determine All Affected Users and Involve Then Early
- The Days of "Rouge" PRA Databases are Gone!













EPRI/NRC-RES FIRE PRA METHODOLOGY

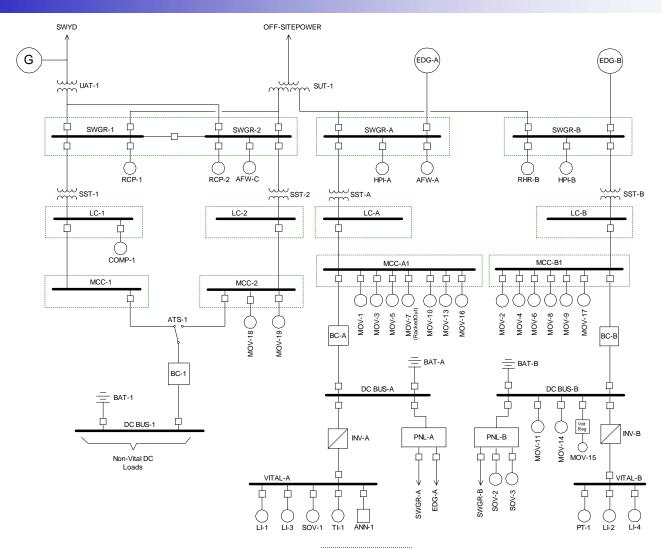
Module 2: Electrical Examples

D. Funk - Edan Engineering Corp. F. Wyant - Sandia National Laboratories Joint RES/EPRI Fire PRA Course July and August 2007 Palo Alto, CA

OVERVIEW OF EXAMPLES

- Provide Hands-On Practical Experience
- Cover Many (But Not All) Typical Cases
- Exposure to Typical Problems and Decisions
- Appreciation for Challenges and Trade-Offs
- A Worn Out Expression, Yes...But for Circuit Analysis the "Devil is in the Detail"

SNPP ONE-LINE DIAGRAM



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Slide 3

EXAMPLE PROBLEMS

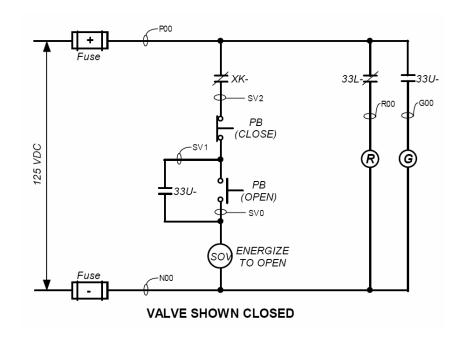
Example No.	Component	Description of Analysis	NUREG/CR-6850	Comments
1	AOV-1 (SOV-1)	Std AC Solenoid Control Circuit	No	Multi-function component - analyzed for open and close
2	AOV-3 (SOV-3)	Std DC Solenoid Control Circuit	Yes - Figure I-2	Spurious only analysis
3	MOV-9	Typ MOV Control Circuit	Yes - Figure I-4	Functional anlysis - change of position required
4	MOV-15	Double Pole DC Motor Control Circuit	Yes - Figure I-6	Functional anlysis - change of position required
5	MOV-13	Ungnd AC, Inverted MOV Control Circuit	Yes - Figure I-8	Functional analysis - change of position required
6	MOV-10	Ungnd AC MOV Control Circuit	Yes - Figure I-10	Functional anlysis - change of position required
7	MOV-8	MOV Control Circuit w/ Dual Controls	Yes - Figure I-12	Spurious only, classified as high consequence component
8	MOV-11	Typ DC MOV Control Circuit	No	Functional analysis - change of position required
9	MOV-16	Typ MOV Control Circuit	Yes - Figure I-4	Spurious Only
10	PI-1	Instrument Circuit	No	Indication only
11	ANN-1	Annunciator Circuit	No	No false indication
12	HPI-B	4.16 kV Motor	No	Functional analysis
13	COMP-1	480 V Motor	No	Functional analysis
14	SWGR-B	4.16 kV Bus	No	Multiple source options
15	LC-B	480V LC	No	Functional analysis
16	MCC-1B	480V MCC	No	Functional analysis

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HANDS ON WORK

		CIRCUIT	ANALYSIS WORK	SHEET
Component	D:		Component Typ	e:
Component	Description:			
BE Code:				
Required Po Functional S				
Normal Posi	tion:			
Failed Electr	ical Position:			
Failed Air Po	sition:			
High Consec	juence Comp	onent Y	∕es □ No []
Power Supp	ies.		E	reaker.
т ожет одрр				reaker.
Cable Analy:	sis:			
Cable ID	Required?	Function	Fault Consequence	Commments
	1			
Comments:				
Comments:				



Fire PRA Workshop, 2007, Palo Alto, CA **Module 2: Electrical Examples**

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Circuit Analysis Example Summary

Example No.	Component	Description of Analysis	NUREG/CR-6850	Comments
1	AOV-1 (SOV-1)	Std AC Solenoid Control Circuit	No	Multi-function component - analyzed for open and close
2	AOV-3 (SOV-3)	Std DC Solenoid Control Circuit	Yes - Figure I-2	Spurious only analysis
3	MOV-9	Typ MOV Control Circuit	Yes - Figure I-4	Functional anlysis - change of position required
4	MOV-15	Double Pole DC Motor Control Circuit	Yes - Figure I-6	Functional anlysis - change of position required
5	MOV-13	Ungnd AC, Inverted MOV Control Circuit	Yes - Figure I-8	Functional analysis - change of position required
6	MOV-10	Ungnd AC MOV Control Circuit	Yes - Figure I-10	Functional anlysis - change of position required
7	MOV-8	MOV Control Circuit w/ Dual Controls	Yes - Figure I-12	Spurious only, classified as high consequence component
8	MOV-11	Typ DC MOV Control Circuit	No	Functional analysis - change of position required
9	MOV-16	Typ MOV Control Circuit	Yes - Figure I-4	Spurious Only
10	PI-1	Instrument Circuit	No	Indication only
11	ANN-1	Annunciator Circuit	No	No false indication
12	HPI-B	4.16 kV Motor	No	Functional analysis
13	COMP-1	480 V Motor	No	Functional analysis
14	SWGR-B	4.16 kV Bus	No	Multiple source options
15	LC-B	480V LC	No	Functional analysis
16	MCC-1B	480V MCC	No	Functional analysis

Component ID): <u> </u>		Component Typ	e:	_
Component De	escription:				
BE Code:					_
Required Posi Functional Sta					
Normal Position	on:				
Failed Electric	al Position:				
Failed Air Posi	ition:				
High Consequ	ence Compo	onent Y	es □ No [
Power Supplie	es:			Breaker: Breaker:	_
Cable Analysis	3:				
Cable ID	Required?	Function	Fault Consequence	Commments	
	l				
Comments:					_
-					_

Component ID: Continuation Sheet (of)											
Cable Analysis:											
Cable ID	Required?	Function	Fault Consequence	Comments							
	1										

Equipment Loss Report

Equipment ID	Equipment Description	Equipment Type	Location	Desired Position/ Status	Potential Loss Areas
HPI-A	High pressure safety injection	Pump	Aux Bldg. El. 0 Ft	On	1, 2, 3, 10
ПРІ-А	pump A	Pump	Aux Biag. El. 0 Ft	On	1, 2, 3, 10
LIDI D	High pressure safety injection	Dum	Aux Dida El O Et	On	1, 2, 3, 11
HPI-B	pump B	Pump	Aux Bldg. El. 0 Ft	On	1, 2, 3, 11
RHR-B	Residual heat removal pump B	Pump	Aux Bldg. El20 Ft	Off	1, 2, 3, 4A, 9, 11
AFW-A	Motor driven AFW pump A	Pump	Aux Bldg. EL. 0 Ft	On	1, 3, 4B, 9, 10
AFW-B	Steam driven AFW pump B	Pump	Aux Bldg. EL. 0 Ft	On	1, 3, 4B, 9, 11
AFW-C	Motor driven AFW pump C	Pump	Turbine Bldg. El. 0 Ft	On	1, 3, 12
RCP-1	Reactor coolant pump 1	Pump	Containment	Off	1, 2, 3, 7, 12
RCP-2	Reactor coolant pump 2	Pump	Containment	Off	1, 2, 3, 7, 12
COMP-1	Instrument air compressor	Compressor	Turbine Bldg. El. 0 Ft	Cycle	12
AOV-1	December 1 and 1 a	101/	O. stalenast	Closed	1, 3, 7, 9
(SOV-1)	Power operated relief valve	AOV	Containment	Open	1, 3, 7, 9, 10
AOV-2 (SOV-2)	Letdown isolation valve	AOV	Aux Bldg. El. 0 Ft	Closed	1, 2, 3, 9
AOV-3 (SOV-3)	Charging pump injection valve	AOV	Aux Bldg. El. 0 Ft	Closed	1, 2, 3, 9
MOV-1	HPI discharge valve	MOV	Aux Bldg. El. 0 Ft	Open	1, 2, 3, 9, 10
MOV-2	VCT isolation valve	MOV	Aux Bldg. El. 0 Ft	Closed	1, 2, 3, 9, 11
MOV-3	Cont. sump recirc valve	MOV	Aux Bldg. El20 Ft	Open/ Closed ²	1, 2, 3, 4A, 9, 10
MOV-4	Cont. sump recirc valve	MOV	Aux Bldg. El20 Ft	Open/ Closed	1, 2, 3, 4A, 9, 11
MOV-5	RWST isolation valve	MOV	Aux Bldg. El. 0 Ft	Open	1, 2, 3, 12
MOV-6	RWST isolation valve	MOV	Aux Bldg. El. 0 Ft	Open	1, 2, 3, 12
MOV-7	RHR inboard suction valve	MOV	Containment	Closed	4A,7,9,12
MOV-8	RHR outboard suction valve	MOV	Aux Bldg. El20 Ft	Closed	4A,9,12
MOV-9	HPI discharge valve	MOV	Aux Bldg. El. 0 Ft	Open	1,2,3,,9
MOV-10	AFW pump A discharge valve	MOV	Aux Bldg. EL. 0 Ft	Open	1,3,4B,9,12
MOV-11	AFW pump B discharge valve	MOV	Aux Bldg. EL. 0 Ft	Open	1,3,4B,9,11,12
MOV-13	PORV block valve	MOV	Containment	Open/ Closed ¹	1, 3, 7, 9
MOV-14	AFW pump B turbine steam line isolation valve	MOV	Turbine Bldg. El. 0 Ft	Open	1, 3, 4B, 12

Equipment ID	Equipment Description	Equipment Type	Location	Desired Position/ Status	Potential Loss Areas
MOV-15	AFW pump B steam inlet throttle valve	MOV	Turbine Bldg. El. 0 Ft	Throttled	1, 3, 4B, 12
MOV-18	AFW pump C discharge valve	MOV	Turbine Bldg. El. 0 Ft	Open	1, 3, 12
V-12	CST isolation valve	MOV	Turbine Bldg. El. 0 Ft	Open	12
LI-1	RWST level	Instrument	Yard	Available	1, 3, 12, 13
LI-2	RWST level	Instrument	Yard	Available	1, 3, 12, 13
LI-3	Cont. sump level	Instrument	Containment	Available	1, 3, 7, 12
LI-4	Cont. sump level	Instrument	Containment	Available	1, 3, 7, 12
TI-1	Letdown heat exchanger outlet temperature	Instrument	Aux Bldg El. 0 Ft	Available	1, 2, 3, 9
PI-1	RCS pressure	Instrument	Containment	Available	1, 3, 7
ANN-1	AFW motor high temperature	Annunciator	SWG Access Room	Non spurious	1, 2, 3, 9, 4B
014/05 4	T : A 4400 V :: I	0 11	0 % 1	Energized from SUT-1	1, 3, 10, 12, 13
SWGR-A	Train A 4160 V switchgear	Switchgear	Switchgear Room A	Energized from EDG-A	1, 3, 8A, 10, 12
				Energized from SUT-1	1, 3, 9, 11, 12, 13
SWGR-B	Train B 4160 V switchgear	Switchgear	Switchgear Room B	Energized from EDG-A	1, 3, 8B, 9, 11, 12
SWGR-1	Non-safety 4160 V switchgear	Switchgear	Turbine Bldg. El. 0ft	Energized	1, 3, 12, 13
SWGR-2	Non-safety 4160 V switchgear	Switchgear	Turbine Bldg. El. 0ft	Energized	1, 3, 12, 13
SUT-1	Startup transformer	Transformer	Yard	Energized	1, 3, 12, 13
EDG-A	Train A emergency diesel generator	Diesel Generator	DG Bldg.	On	1, 3, 8A, 10, 12
EDG-B	Train B emergency diesel generator	Diesel Generator	DG Bldg.	On	1, 3, 8B, 10, 12
LC-1	Non-safety 480 V load center	Load Center	Turbine Bldg. El. 0 ft	Energized	1, 3, 12
LC-2	Non-safety 480 V load center	Load Center	Turbine Bldg. El. 0 ft	Energized	1, 3, 12
LC-A	Train A 480 V load center	Load Center	Switchgear Room A	Energized	1, 3,10
LC-B	Train B 480 V load center	Load Center	Switchgear Room B	Energized	1, 3, 11
SST-1	Non-safety station service transformer	Transformer	Turbine Bldg. El. 0 F	Energized	12
SST-2	Non-safety station service transformer	Transformer	Turbine Bldg. El. 0 F	Energized	12
SST-A	Train A station service transformer	Transformer	Switchgear Room A	Energized	10
SST-B	Train B station service transformer	Transformer	Switchgear Room B	Energized	11
MCC-1	Non-safety 480 V motor control center	Motor Control Center	Turbine Bldg El. 0 Ft	Energized	12
MCC-2	Non-safety 480 V motor control center	Motor Control Center	Turbine Bldg El. 0 Ft	Energized	12

Equipment ID	Equipment Description	Equipment Type	Location	Desired Position/ Status	Potential Loss Areas
MCC-A1	Train A 480 V motor control center	Motor Control Center	SWG Access Room	Energized	9, 10
MCC-B1	Train B 480 V motor control center	Motor Control Center	SWG Access Room	Energized	9, 11
ATS-1	Automatic transfer switch	ATS	SWG Access Room	Energized from MCC-1	12
BC-1	Non-safety swing battery charger	Battery Charger	Turbine Bldg El. 0 Ft	Energized	12
BC-A	Train A battery charger	Battery Charger	Switchgear Room A	Energized	9, 10
BC-B	Train B battery charger	Battery Charger	Switchgear Room B	Energized	9, 11
BAT-1	Non-safety battery	Battery	Turbine Bldg El. 0 Ft	Available	12, 15
BAT-A	Train A battery	Battery	Battery Room A	Available	5, 10
BAT-B	Train B battery	Battery	Battery Room B	Available	6, 11
DC BUS-1	Non-safety 250 VDC bus	DC Bus	Turbine Bldg El. 0 Ft	Energized	12
DC BUS-A	Train A 125 VDC bus	DC Bus	Switchgear Room A	Energized	10
DC BUS-B	Train B 125 VDC bus	DC Bus	Switchgear Room B	Energized	11
PNL-A	Train A 125 VDC panel	Panelboard	Switchgear Room A	Energized	10
PNL-B	Train B 125 VDC panel	Panelboard	Switchgear Room B	Energized	11
INV-A	Train A inverter	Inverter	Switchgear Room A	Energized	3, 9, 10
INV-B	Train B inverter	Inverter	Switchgear Room B	Energized	3, 9, 11
VITAL-A	Train A 120 VAC vital bus	120VAC Bus	SWG Access Room	Energized	9, 10
VITAL-B	Train B 120 VAC vital bus	120VAC Bus	SWG Access Room	Energized	9, 11

Component ID	: AOV	/-1 (SOV-1)		Component	Type:	AOV	
Component De	escription:	Power O	perated	Relief Valve			
BE Code:		AOV-	·1_TO	(PORV AOV	/-1 TRANS	FERS OPEN)	
Required Posi Functional Sta		CLO	SED				
Normal Position	n:	CLO	SED				
Failed Electric	al Position:	CLO	SED				
Failed Air Posi	tion:	CLO	SED				
High Consequ	ence Compo	onent Yes	□ No	\triangleright			
Power Supplie	s:			<u>Brea</u>	ker:		
				<u>Brea</u>	ker:		_
Cable Analysis	S:						
Cable ID	Required?	Function	Fault C	onsequence	Comment	S	
			1		1		
Comments:							

Component ID	: AO\	/-1 (SOV-1)		Component	Туре:	AOV	
Component De	escription:	Power O	perated	Relief Valve			
BE Code:		AOV-	-1_FTO	(PORV AOV	-1 FAILS TO	OPEN)	
Required Posi Functional Sta		OPE	N				
Normal Position	n:	CLOS	SED				
Failed Electric	al Position:	CLOS	SED				
Failed Air Posi	ition:	CLO	SED				
High Consequ	ence Compo	onent Yes	☐ No				
Power Supplie	es:			<u>Breal</u>	ker:		
				<u>Breal</u>	ker:		
Cable Analysis	S:						
Cable ID	Required?	Function	Fault Co	onsequence	Comments		
	•		•		•		
Comments:							

Component ID	: AOV	/-3 (SOV-3)		Component	Type:	AOV	
Component De	escription:	Chargin	g Pump	Injection Val	ve		
BE Code:		AOV-	3_FTC	(AOV-3 FAI	LS TO CLC	SE)	
Required Posit Functional Sta		CLO	SED				
Normal Positio	n:	OPEI	N				
Failed Electrica	al Position:	CLO	SED				
Failed Air Posi	tion:	CLO	SED				
High Consequ	ence Compo	onent Yes	☐ No				
Power Supplie	s:			<u>Brea</u>	ker:		
				Brea	ker:		_
Cable Analysis	S:						
Cable ID	Required?	Function	Fault Co	onsequence	Comments	3	
	,		1				
Comments:							

Component ID	: MO \	/-9	Co	mponent ⁻	Туре:	MOV		
Component De	escription:	High Pre	essure Injec	tion Valve	•			
BE Code: MOV-9_FTO (MOV-9 FAILS TO OPEN)								
Required Posit Functional Stat		OPE	N					
Normal Positio	n:	CLO	SED					
Failed Electrica	al Position:	AS-IS	8					
Failed Air Posi	tion:	N/A						
High Conseque	ence Compo	onent Yes	☐ No ⊠					
Power Supplie	s:			<u>Breal</u>	ker:	<u>-</u>		
				<u>Breal</u>	ker:			
Cable Analysis	i:							
Cable ID	Required?	Function	Fault Conse	equence	Comments			
Comments:								

Component ID	: MO \	/ -15	Co	omponent ⁻	Туре:	MOV	
Component De	escription:	AFW Ste	am Inlet Th	rottle Val	ve		
BE Code:		MOV	-10_FTO	(MOV-10	FAILS TO	OPEN)	
Required Posit Functional Sta		THRO	OTTLED				
Normal Positio	n:	CLOS	SED				
Failed Electrical Position: AS-IS							
Failed Air Position: N/A							
High Conseque	ence Compo	onent Yes	☐ No ⊠]			
Power Supplies: Breaker:							
				<u>Breal</u>	ker:		
Cable Analysis	::						
Cable ID	Required?	Function	Fault Conse	equence	Comments		
Comments:							

Component ID	MOV	/-13	Co	mponent	Туре:	MOV		
Component De	escription:	PORV B	lock Valve					
BE Code:		MOV	-13_FTC	(MOV-13	FAILS TO	CLOSE)		
Required Posit Functional Stat		OPE	N / CLOSED)				
Normal Positio	n:	OPE	N					
Failed Electrica	al Position:	AS-I	S					
Failed Air Position: N/A								
High Consequence Component Yes ☐ No ☐								
Power Supplies: Breaker:								
				<u>Brea</u>	ker:			
Cable Analysis	:							
Cable ID	Required?	Function	Fault Conse	equence	Comments	3		
			1		1			
Comments:								

Component ID	: MO \	/-10		Compon	ent Type:	MOV	
Component De	escription:	AFW Dis	charge Iso	lation Val	ve		
BE Code:		MOV	-10_FTO	(MOV-10	FAILS TO O	PEN)	
Required Positi Functional Sta		OPE	N				
Normal Position	n:	CLO	SED				
Failed Electrical Position: AS-IS							
Failed Air Position: N/A							
High Consequ	ence Compo	onent Yes	☐ No ⊠]			
Power Supplie	s:		<u>Brea</u>	ker:			
				<u>Brea</u>	ker:		
Cable Analysis	S:						
Cable ID	Required?	Function	Fault Cons	equence Comments			
Comments:							

Component ID: MOV-8			(Component	Туре:	MOV	
Component De	scription:	RHR Ou	tboard Su	ction Valve			
BE Code:		MOV	-8_TO	(MOV-8	TRANSFER	S OPEN)	
Required Positi Functional Stat		CLO	SED				
Normal Position	n:	CLO	SED				
Failed Electrica	I Position:	AS-IS	S				
Failed Air Position: N/A							
High Consequence Component Yes No							
Power Supplies: <u>Breaker:</u>							
				<u>Breal</u>	ker:		
Cable Analysis	:						
Cable ID	Required?	Function	Fault Con	sequence	Comments		
Comments:							

Component ID	: MO \	/-11		Compon	ent Type:	MOV	
Component De	escription:	AFW Dis	scharge Iso	lation Val	ve		
BE Code:		MOV	-11_FTO	(MOV-11	FAILS TO O	PEN)	
Required Posit Functional Sta		OPE	N				
Normal Positio	n:	CLO	SED				
Failed Electrica	al Position:	AS-I	S				
Failed Air Position: N/A							
High Consequ	ence Compo	onent Yes	☐ No ⊠				
Power Supplie	s:		<u>Brea</u> l	ker:			
				<u>Breal</u>	ker:		
Cable Analysis	S:						
Cable ID	Required?	Function	Fault Conse	equence Comments			
	I		I		I		
Comments:							

Component ID	: MO \	/-16		Compone	ent Type:	MOV	
Component De	escription:	AFW Tes	st Line Isola	ntion Valv	e		
BE Code:		MOV	-16_TO	(MOV-16	TRANSFERS	OPEN)	
Required Posit Functional Sta		CLOS	CLOSED				
Normal Positio	n:	CLOS	SED				
Failed Electrica	al Position:	AS-IS	5				
Failed Air Position: N/A							
High Conseque	ence Compo	onent Yes	☐ No ⊠				
Power Supplies: <u>Breaker:</u>							
				<u>Break</u>	cer:		
Cable Analysis	i:						
Cable ID	Required?	Function	Fault Conse	equence	Comments		
					I		
Comments:							

Component ID	: PI-1			Compon	ent Type:	Instrument	
Component De	escription:	RCS Pre	ssure				
BE Code:		PI-1_	FL (RCS Press	ure Indicatio	n Fails High)	
Required Posit Functional Sta		AVAI	LABLE				
Normal Positio	n:	AVAI	LABLE				
Failed Electrical Position: LOW							
Failed Air Position: N/A							
High Consequ	ence Compo	onent Yes	☐ No [\boxtimes			
Power Supplies:				Breaker:			
				Brea	ker:		
Cable Analysis	S:						
Cable ID	Required?	Function	Fault Con	sequence Comments			
			ı		1		
Comments:							

Component ID	: ANN	I-1		Compon	ent Type:	Annunciator
Component De	escription:	AFW Mo	tor High	Temperatur	е	
BE Code:		ANN-	1_FH	(AFW Pumր	o Motor Spuri	ous High Ann)
Required Positi Functional Sta		NON-	SPURIO	US		
Normal Position	n:	AVAI	LABLE			
Failed Electric	al Position:	UNA	VAILABL	.E		
Failed Air Posi	tion:	N/A				
High Consequ	ence Compo	onent Yes	☐ No	\boxtimes		
Power Supplies: Breaker:						
				Brea	ker:	
Cable Analysis	S:					
Cable ID	Required?	Function	Fault Co	nsequence	Comments	
Comments:						

Component ID	: HPI-	В		C	Compone	ent Type:	Pump
Component De	escription:	Higl	h Pressur	e Injectio	on Pum _l	рВ	
BE Code:			HPIA_FTS HPIA_FTF			to Start) to Run)	
Required Posit Functional Stat		(ON				
Normal Positio	n:	;	STANDBY / ON				
Failed Electrica	al Position:	(Off				
Failed Air Posi	tion:	İ	N/A				
High Conseque	ence Compo	onent '	Yes 🗌	No 🛚			
Power Supplies: Breaker:							
					Break	ker:	
Cable Analysis	::						
Cable ID	Required?	Function	on Fau	lt Consequ	ience	Comments	
Comments:							

Component ID	: CON	/IP-1		Com	ponent Type:	Compressor
Component De	escription:	Instrume	ent Air Com	pressor		
BE Code:		COM	P-1_FTR	(COMP-	1 Fails to Run)	
Required Positi Functional Sta		CYC	LE			
Normal Position	n:	CYC	LE			
Failed Electric	al Position:	Off				
Failed Air Posi	tion:	N/A				
High Consequ	ence Compo	onent Yes	☐ No ⊠]		
Power Supplies:Br					ıker:	_
				<u>Brea</u>	ıker:	
Cable Analysis	S:					
Cable ID	Required?	Function	Fault Conse	equence Comments		
			I			
Comments:						

Component ID	: SW	GR-B		Comp	onent Type:	Switchgear
Component De	escription:	Train B 4	4160V Switchgea	ar		
BE Code:		PNL-	B EPS-4VBUSB	F-1	(4KV BUS B F	FAULT)
Required Posi Functional Sta		ENE	RGIZED FROM S	UT-1		
Normal Position	n:	ENE	RGIZED FROM S	UT-1		
Failed Electric	al Position:	Off				
Failed Air Posi	tion:	N/A				
High Consequ	ence Compo	onent Yes	☐ No ⊠			
Power Supplies:				Breaker:		
				Break	er:	
Cable Analysis	S:					
Cable ID	Required?	Function	Fault Consequen	се	Comments	
Comments:						

Component ID	: SWC	GR-B		Comp	onent Type:	Switchgear
Component De	escription:	Train B	4160V Switchge	ear		
BE Code:		PNL-	B EPS-4VBUSE	3F-2	(4KV BUS B F	AULT)
Required Positi Functional Sta	tion: te	ENE	RGIZED FROM	EDG-B	3	
Normal Position	n:	ENE	RGIZED FROM	SUT-1		
Failed Electric	al Position:	Off				
Failed Air Posi	tion:	N/A				
High Consequ	ence Compo	onent Yes	☐ No ⊠			
Power Supplie	s:			Break	er:	
				Break	er:	
Cable Analysis	S:					
Cable ID	Required?	Function	Fault Conseque	nce	Comments	
Comments:						

Component ID	: LC-I	3		Compone	ent Type:	Load Center				
Component Description: Train B 480 V Load Center										
BE Code:		EPS-	EPS-480VLCBF		(480V LOAD CENTER B FAULT)					
Required Position: Functional State		ENEF	ENERGIZED							
Normal Position:		ENEF	ENERGIZED							
Failed Electrica	al Position:	Off								
Failed Air Position: N/A										
High Consequence Component Yes ☐ No ☒										
Power Supplies: Breaker:										
				Breaker:						
Cable Analysis	S:									
Cable ID Required? Functi		Function	on Fault Consequence		Comments					
	l									
Comments:										

Component ID	: MCC	C-1B		Comp	oonent Type:	MCC					
Component Description: Train B 480 V Motor Control Center											
BE Code:		EPS-	EPS-480MCCB1F		/ MCC B1 FAULT)						
Required Posit Functional Sta		ENEF	ENERGIZED								
Normal Positio	n:	ENEF	ENERGIZED								
Failed Electrical Position: Off											
Failed Air Position: N/A											
High Consequence Component Yes ☐ No ☒											
Power Supplie	s:		Break	ker:							
				<u>Break</u>	ker:						
Cable Analysis): :										
Cable ID	Required?	Function	Fault Conseque	ence	Comments						
Comments:											
						_					