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MFN 06-159 Supplement 1

Docket No. 52-010

September 12, 2007

U.S. Nuclear Regulatory Commission
Document Control Desk
Washington, D.C. 20555-0001

Subject: **Response to Portion of NRC Request for Additional Information
Letter No. 18 - Related to ESBWR Design Certification Application -
Containment Subcompartment Loads - RAI Numbers 6.2-15 S01,
6.2-18 S01, and 6.2-23 S01**

Enclosure 1 contains the GE-Hitachi Nuclear Energy Americas LLC (GEH) response to the subject NRC RAIs originally transmitted via the Reference 1 letter and supplemented by NRC requests for clarification.

If you have any questions or require additional information, please contact me.

Sincerely,



James C. Kinsey
Project Manager, ESBWR Licensing

DC68
HRO

Reference:

1. MFN 06-113, Letter from U.S. Nuclear Regulatory Commission to David Hinds, *Request for Additional Information Letter No. 18 Related to ESBWR Design Certification Application*, April 24, 2006

Enclosure:

1. MFN 06-159 Supplement 1 - Response to Portion of NRC Request for Additional Information Letter No. 18 - Related to ESBWR Design Certification Application - Containment Subcompartment Loads - RAI Numbers 6.2-15 S01, 6.2-18 S01, and 6.2-23 S01

cc: AE Cabbage USNRC (with enclosures)
GB Stramback GEH/San Jose (with enclosures)
RE Brown GEH/Wilmington (with enclosures)
eDRF 0000-0071-5294

Enclosure 1

MFN 06-159 Supplement 1

Response to Portion of NRC Request for

Additional Information Letter No. 18

Related to ESBWR Design Certification Application

Containment Subcompartment Loads

RAI Numbers 6.2-15 S01, 6.2-18 S01, and 6.2-23 S01

NRC RAI 6.2-15 S01:

GE's response to RAI 6.2-15, MFN 06-159, and DCD, Tier 2, Rev. 3, Section 6.2.1.2.1, states that "[a]t least 15% margin above the analytically determined pressure is applied for structural analysis." DCD, Tier 2, Rev. 3, Section 6.2.1.2, notes that a factor of 1.4 is applied to the peak differential pressure calculated for the subcompartment, structure, and the enclosed components. Please explain this apparent discrepancy.

GEH Response:

See response to RAI 6.2-18 S01, Part A.

DCD Impact:

No DCD changes will be made in response to this RAI.

NRC RAI 6.2-18 S01:

GE's response to RAI 6.2-18, and DCD, Tier 2, Rev. 3, Section 6.2.1.2.3 states that "[t]he mass release rates are determined with Moody's Frictionless Critical Flow Model and Analyzed with TRACG, the peak subcompartment pressure responses were found to be below the design pressure for all postulated pipe break accidents."

- A. Please explain how the statement subcompartment pressure responses were found to be below the design pressure relates to the factor of 1.4" margin stated in Section 6.2.1.2 and the "at least 15% margin" in Section 6.2.1.2.1.*
- B. In GE's response to RAI 6.2-18, GE stated that it did not use computer codes to calculate mass and energy release for containment subcompartment analysis. Please confirm this statement and include it in DCD, Tier 2.*
- C. Please provide the design pressure in DCD, Tier 2.*

GEH Response:

- A. A multiplier of 1.2 was applied to the peak pressures calculated for annulus pressurization before being applied to structural analyses. This 1.2 multiplier ensures at least 15% margin above the analytically determined pressures. The last paragraph of DCD Tier 2, Revision 3, Subsection 6.2.1.2 will be rephrased with "a factor of 1.2".
- B. No computer program was used to calculate mass and energy releases. A copy of the calculation used is included in the response to RAI 6.2-23 S01, Part C. The mass release rates are based on F. J. Moody, "Maximum Discharge Rate of Liquid Vapor Mixtures from Vessels," Proceedings of the ASME Symposium on Non-Equilibrium Two-Phase Flows, p. 27-36, 1975.
- C. The structural integrity of subcompartments is evaluated based on load combination described in DCD Tier 2, Revision 3, Subsection 3.G.1.5.2, instead of a single design pressure. The integrity of the reactor shield wall is discussed in DCD Tier 2, Revision 3, Subsection 3G.1.5.4.2.3.

DCD Impact:

- A. In the last paragraph of DCD Tier 2, Subsection 6.2.1.2, "a factor of 1.4" will be replaced with "a factor of 1.2".
- B. DCD Tier 2, Subsection 6.2.1.2.3, will be amended to state the following:

"The mass release rates are determined with Moody's Critical Flow Model for Homogenous Equilibrium Mixture (Reference 6.2-7). The manually determined flows are 9.389×10^4 kg/(sec-m²) and 4.868×10^4 kg/(sec-m²) for FWL and RWCU breaks, respectively."

The added Reference 6.2-7 is:

F. J. Moody, "Maximum Discharge Rate of Liquid Vapor Mixtures from Vessels," Proceedings of the ASME Symposium on Non-Equilibrium Two-Phase Flows, p. 27-36, 1975.

C. The last sentence of DCD Tier 2, Subsection 6.2.1.2.3 will be amended to state the following:

"The subcompartment pressure responses were analyzed with TRACG. The integrity of the reactor shield wall is discussed in Subsection 3G.1.5.4.2.3."

The last paragraph of DCD Tier 2, Subsection 6.2.1.2 will be further amended to state the following:

"During the construction permit stage, a factor of 1.2 is applied to the peak differential pressure calculated for the subcompartment, structure and the enclosed components, for use in the design of the structure and the component supports. At the operating license (OL) stage, the peak calculated differential pressure can be used in structural evaluations. It is expected that the post-OL peak calculated differential pressure would not be substantially different from that of the construction permit stage. However, improvements in the analytical models or changes in the as-built subcompartment may affect the available margin."

NRC RAI 6.2-23 S01:

In RAI 6.2-23 the staff requested for subcompartment nodalization information in accordance with the formats of Regulatory Guide 1.70, "Standard Format and Content of Safety Analysis Reports for Nuclear Power Plants (LWR Edition) Rev. 3, Section 6.2.1.2. In GE's response, MFN 06-159, GE provided nodal data but stated without specifics that it calculated large pipe and vessel support structure volumes and hydraulic diameters and accounted for the additional obstructions by applying a 10% reduction factor in the annulus volume for cells where a specific obstruction is not modeled.

Please provide the following information needed to perform a confirmatory subcompartment analysis of the vessel/shield wall annular volume:

- A. The TRACG input for the reactor shield wall subcompartment analysis.*
- B. The results of a sensitivity analysis on the number and size of the control volumes used in the shield wall subcompartment analysis. This information is needed to verify the appropriateness of the control volume nodalization used in the final reported analysis.*
- C. A copy of the calculation used to obtain the break mass and energy releases. This information is needed to confirm the appropriateness of the assumptions used in this calculation.*
- D. Detailed information and/or drawings describing the space between the reactor vessel and shield wall to include the following:*
 - 1. The outer diameter of the reactor vessel.*
 - 2. A description of the upper and lower heads of the reactor vessel.*
 - 3. A description of the shield wall including inner diameter and the volumes surrounding the upper and lower vessel heads.*
 - 4. The type and thickness of the reactor vessel insulation, and information on how the insulation is treated in the subcompartment analysis (i.e., whether the insulation is assumed to stay in place or blown away and its affect on the calculated volume and nodalization of the annular volume).*
 - 5. A description of the flow obstructions in the reactor vessel/shield wall annular volume: flow area, flow resistance, and flow obstructions providing boundaries for the control volume nodalization.*
 - 6. A description of the flow connections (i.e., flow area and flow resistance) between the reactor vessel/shield wall annulus and the upper part of the drywell.*

GEH Response:

- A. Two TRACG input decks are included as Attachments 1 and 2 of this enclosure:

FW_r2.bdk	for feedwater line (FWL) break
RWCU_r2.bdk	for reactor water clean-up (RWCU) line break

- B. The GEH experience with annulus pressurization of previous BWRs has indicated that smaller node sizes around the break location resulted in higher pressures. Based on this, smaller node sizes are applied near the break location. The nodalization of ESBWR annulus pressurization was supplied with the original response to RAI 6.2-23 (MFN 06-159, dated June 5, 2006). The nodes around the postulated breaks, (i.e., Levels 7 through 14) have a dimension of 0.34 m, the smallest size without encroaching the inside diameter of a feedwater line or RWCU line.

A sensitivity study was performed to show the impact of the annulus volume. Annulus volumes where no specific obstructions are present were increased by 10%, and the cell volume where the peak pressure occurs was not changed due to presence of obstruction. For a RWCU line break, the peak pressure of the sensitivity cases is reduced to 1.228 MPa, compared to 1.267 MPa of the base case.

- C. Pages showing calculations of mass and energy releases are included as Attachment 3 in this enclosure.

- D. Following are item-by-item responses:

1. The outer diameter of the reactor vessel is 7.476 meters.
2. Descriptions of the reactor vessel, including upper and lower reactor pressure vessel (RPV) heads, are provided in DCD Tier 2, Revision 3, Subsection 5.3.3.2.1.
3. The geometry of the reactor shield wall (RSW) is shown in the attached Figure (Upper Drywell). The inner diameter of the RSW is 9.292 meters. The thickness is 0.016 meter.
4. A description of RPV insulation is provided in DCD Tier 2, Revision 3, Subsection 5.3.3.2.2, under the heading "Reactor Vessel Insulation." The insulation is designed to remain in place and resist damage during a safe shutdown earthquake. The reactor insulation is not modeled in the annulus pressurization analysis.

The effect of blown-away insulation is addressed in a sensitivity study of reduced vent area between the annulus and drywell. A decrease in the RSW to drywell vent flow area (50% reduction) results in practically no change in the peak annulus pressure.

Decreasing drywell venting does show a moderate increase in the annulus pressures as the transient progresses, however, since the peak pressure occurs so soon (3 ms) into the transient, the drywell venting does not affect the peak annulus pressures.

5. The annulus contains various piping and support structures that presents a reduction in volume from the ideal cylinder. Large piping and vessel support structure volumes and hydraulic diameters are calculated to model the obstruction in the annulus nodal volumes. Volumes are minimized for conservatism and simplicity where necessary. For this analysis, the main steam line, feedwater, DPV, and RWCU piping is specifically incorporated. Also, the RPV stabilizer and vessel support structure are incorporated. All other smaller geometries are assumed to be distributed about the annulus. These additional obstructions are accounted for by applying a 10% reduction in the annulus volume for cells where a specific obstruction is not modeled.

6. The geometry of upper drywell head is shown in DCD Tier 2, Revision 3, Figure 3G.1-51. The flow paths between the drywell head and RSW are shown in the attached Figure. The upper drywell head volume is not credited in the annulus pressurization calculation to maximize the annulus pressure.

DCD Impact:

No DCD changes will be made in response to this RAI.

=ESBWR Annulus Model FW

* This file models the annulus between the RPV and RSW

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*          IEOS   NTRACE   IST   NEXTR
OPTIONS    0       0      -1     0
*          DSTEP   TIMET    STDYST  TRANSI  NCOMP  NJUN  IPAK
MAIN00     0     0.0000E+00   0       1       3     2     1
*          EPSO     EPSI     EPSS    IMPCON  OITMAX  IITMAX
MAIN01     1.0000E-04  1.0000E-04  1.0000E-04  1       10     0
*          SITMAX  NTRX    NDMPTR  ICTR   IBORC   IOPTCD  CMULT
MAIN02     10      0       0       0       0       2     1.0000E+02
*          IAIR   ICONTA  NROT    MIXING
MAIN03     1       0       0       1
  
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***** COMPONENT LIST CARDS

COMPLIST00 99 01 02

*

***** TIME STEP DATA CARDS

*

*23456789012345678901234567890123456789*123456789012345678901234567890123456789E

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*          DTMIN   DTMAX    TEND  RTWFP  EDINFP  GFINT   DMPINT   SEDINT
TIMESTEP010  1.0E-08  1.0E-04  0.004  1.0   5.0E-04  5.0E-04  8.0E+03  1.00E+06
TIMESTEP020  1.0E-08  1.0E-03  0.018  1.0   2.0E-03  2.0E-03  8.0E+03  1.00E+06
TIMESTEP030  1.0E-08  2.5E-03  0.200  1.0   5.0E-03  5.0E-03  8.0E+03  1.00E+06
  
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***** VSSL HEADER CARD

VSSL9900000 99 "3D Annulus"

*

VSSL SIMPLE PARAMETER CARD

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*          NASX     NRSX     NTSX     NCSR
VSSL9900010    18       2       9       1
*          IDCU   IDCL   IDCR   ICRU   ICRL   ICRR
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*          ROHS     CPHS     CHS     EMHS
VSSL9900012  2.35000E+03  8.82000E+02  1.62780E+00  7.00000E-01
*          ISDU     ISDL     ISDR
VSSL9900013     0     0     0
*          CZSDL     CRSDV
VSSL9900014  1.00000E+26  1.00000E+26
*          NODESD     DHOUTL     DHOUTV     DTOUTL     DTOUTV
VSSL9900015     0     0.0     0.0     0.0     0.0
  
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Z
VSSL9900110  2.362     5.377     7.637     9.897
VSSL9900111  12.157    14.417    14.757    15.097
VSSL9900112  15.437    15.777    16.117    16.457
VSSL9900113  16.797    17.137    19.005    20.874
VSSL9900114  21.892    31.892    E
  
```

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RAD
VSSL9900120  3.738     4.646     E
*****
TH
VSSL9900130  0.0698    0.1396    0.2094    0.3491
VSSL9900131  0.7854    1.5708    2.3562    3.1416
VSSL9900132  6.2832    E
  
```

* This set of source cards is commented out, because it is overlaid below:

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*          ISRL   ISRC   ISRF     JUNS     ZJN
VSSL9900140    13    10    -3       2       0.5
*VSSL9900140     8     1    -3       2       0.5
  
```

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VSSL9901DSAZ0 F 0.0 E
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MFN 06-159 Supplement 1
Enclosure 1
Attachment 1

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VSSL9909FRICP-Z0	F	0.0	E
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VSSL9907FRICP-Z0	F	0.0	E
VSSL9906FRICP-Z0	F	0.0	E
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VSSL9918PA0	F	1.0133E+05	E
VSSL9917PA0	F	1.0133E+05	E
VSSL9916PA0	F	1.0133E+05	E
VSSL9915PA0	F	1.0133E+05	E
VSSL9914PA0	F	1.0133E+05	E
VSSL9913PA0	F	1.0133E+05	E
VSSL9912PA0	F	1.0133E+05	E
VSSL9911PA0	F	1.0133E+05	E
VSSL9910PA0	F	1.0133E+05	E
VSSL9909PA0	F	1.0133E+05	E
VSSL9908PA0	F	1.0133E+05	E
VSSL9907PA0	F	1.0133E+05	E
VSSL9906PA0	F	1.0133E+05	E
VSSL9905PA0	F	1.0133E+05	E
VSSL9904PA0	F	1.0133E+05	E
VSSL9903PA0	F	1.0133E+05	E
VSSL9902PA0	F	1.0133E+05	E
VSSL9901PA0	F	1.0133E+05	E
VSSL9918PNO	F	1.0133E+05	E
VSSL9917PNO	F	1.0133E+05	E
VSSL9916PNO	F	1.0133E+05	E
VSSL9915PNO	F	1.0133E+05	E
VSSL9914PNO	F	1.0133E+05	E
VSSL9913PNO	F	1.0133E+05	E
VSSL9912PNO	F	1.0133E+05	E
VSSL9911PNO	F	1.0133E+05	E
VSSL9910PNO	F	1.0133E+05	E
VSSL9909PNO	F	1.0133E+05	E
VSSL9908PNO	F	1.0133E+05	E
VSSL9907PNO	F	1.0133E+05	E
VSSL9906PNO	F	1.0133E+05	E
VSSL9905PNO	F	1.0133E+05	E
VSSL9904PNO	F	1.0133E+05	E
VSSL9903PNO	F	1.0133E+05	E
VSSL9902PNO	F	1.0133E+05	E
VSSL9901PNO	F	1.0133E+05	E
VSSL9918TLNO	F	280.1	E
VSSL9917TLNO	F	280.1	E
VSSL9916TLNO	F	280.1	E
VSSL9915TLNO	F	280.1	E
VSSL9914TLNO	F	280.1	E
VSSL9913TLNO	F	280.1	E
VSSL9912TLNO	F	280.1	E
VSSL9911TLNO	F	280.1	E
VSSL9910TLNO	F	280.1	E
VSSL9909TLNO	F	280.1	E
VSSL9908TLNO	F	280.1	E
VSSL9907TLNO	F	280.1	E
VSSL9906TLNO	F	280.1	E
VSSL9905TLNO	F	280.1	E
VSSL9904TLNO	F	280.1	E
VSSL9903TLNO	F	280.1	E
VSSL9902TLNO	F	280.1	E
VSSL9901TLNO	F	280.1	E

MFN 06-159 Supplement 1
Enclosure 1
Attachment 1

VSSL9918TVNO	F	373.1	E
VSSL9917TVNO	F	373.1	E
VSSL9916TVNO	F	373.1	E
VSSL9915TVNO	F	373.1	E
VSSL9914TVNO	F	373.1	E
VSSL9913TVNO	F	373.1	E
VSSL9912TVNO	F	373.1	E
VSSL9911TVNO	F	373.1	E
VSSL9910TVNO	F	373.1	E
VSSL9909TVNO	F	373.1	E
VSSL9908TVNO	F	373.1	E
VSSL9907TVNO	F	373.1	E
VSSL9906TVNO	F	373.1	E
VSSL9905TVNO	F	373.1	E
VSSL9904TVNO	F	373.1	E
VSSL9903TVNO	F	373.1	E
VSSL9902TVNO	F	373.1	E
VSSL9901TVNO	F	373.1	E
VSSL9918VLN-R0	F 0.0		E
VSSL9917VLN-R0	F 0.0		E
VSSL9916VLN-R0	F 0.0		E
VSSL9915VLN-R0	F 0.0		E
VSSL9914VLN-R0	F 0.0		E
VSSL9913VLN-R0	F 0.0		E
VSSL9912VLN-R0	F 0.0		E
VSSL9911VLN-R0	F 0.0		E
VSSL9910VLN-R0	F 0.0		E
VSSL9909VLN-R0	F 0.0		E
VSSL9908VLN-R0	F 0.0		E
VSSL9907VLN-R0	F 0.0		E
VSSL9906VLN-R0	F 0.0		E
VSSL9905VLN-R0	F 0.0		E
VSSL9904VLN-R0	F 0.0		E
VSSL9903VLN-R0	F 0.0		E
VSSL9902VLN-R0	F 0.0		E
VSSL9901VLN-R0	F 0.0		E
VSSL9918VLN-T0	F 0.0		E
VSSL9917VLN-T0	F 0.0		E
VSSL9916VLN-T0	F 0.0		E
VSSL9915VLN-T0	F 0.0		E
VSSL9914VLN-T0	F 0.0		E
VSSL9913VLN-T0	F 0.0		E
VSSL9912VLN-T0	F 0.0		E
VSSL9911VLN-T0	F 0.0		E
VSSL9910VLN-T0	F 0.0		E
VSSL9909VLN-T0	F 0.0		E
VSSL9908VLN-T0	F 0.0		E
VSSL9907VLN-T0	F 0.0		E
VSSL9906VLN-T0	F 0.0		E
VSSL9905VLN-T0	F 0.0		E
VSSL9904VLN-T0	F 0.0		E
VSSL9903VLN-T0	F 0.0		E
VSSL9902VLN-T0	F 0.0		E
VSSL9901VLN-T0	F 0.0		E
VSSL9918VLN-Z0	F 0.0		E

VSSL9917VFN-T0	F 0.0	E
VSSL9916VFN-T0	F 0.0	E
VSSL9915VFN-T0	F 0.0	E
VSSL9914VFN-T0	F 0.0	E
VSSL9913VFN-T0	F 0.0	E
VSSL9912VFN-T0	F 0.0	E
VSSL9911VFN-T0	F 0.0	E
VSSL9910VFN-T0	F 0.0	E
VSSL9909VFN-T0	F 0.0	E
VSSL9908VFN-T0	F 0.0	E
VSSL9907VFN-T0	F 0.0	E
VSSL9906VFN-T0	F 0.0	E
VSSL9905VFN-T0	F 0.0	E
VSSL9904VFN-T0	F 0.0	E
VSSL9903VFN-T0	F 0.0	E
VSSL9902VFN-T0	F 0.0	E
VSSL9901VFN-T0	F 0.0	E
VSSL9918VFN-Z0	F 0.0	E
VSSL9917VFN-Z0	F 0.0	E
VSSL9916VFN-Z0	F 0.0	E
VSSL9915VFN-Z0	F 0.0	E
VSSL9914VFN-Z0	F 0.0	E
VSSL9913VFN-Z0	F 0.0	E
VSSL9912VFN-Z0	F 0.0	E
VSSL9911VFN-Z0	F 0.0	E
VSSL9910VFN-Z0	F 0.0	E
VSSL9909VFN-Z0	F 0.0	E
VSSL9908VFN-Z0	F 0.0	E
VSSL9907VFN-Z0	F 0.0	E
VSSL9906VFN-Z0	F 0.0	E
VSSL9905VFN-Z0	F 0.0	E
VSSL9904VFN-Z0	F 0.0	E
VSSL9903VFN-Z0	F 0.0	E
VSSL9902VFN-Z0	F 0.0	E
VSSL9901VFN-Z0	F 0.0	E

*

***** PIPE

*

PIPE02000	2	"FW BREAK AND VESSEL"			
*	NCELLS	NODES	JUN1	JUN2	MAT
PIPE02010	1	0	1	2	0
PIPE02DX0		0.355		E	
PIPE02VOL0		0.0166		E	
PIPE02TL0		488.75		E	
PIPE02TV0		488.75		E	
PIPE02P0		7.305E+06		E	
PIPE02PA0		0.0		E	
PIPE02ALP		0.0		E	
PIPE02FRICN0	0.0	1.0		E	
PIPE02FRICP0	0.0	0.0		E	
PIPE02FA0	0.0468	0.0468		E	
PIPE02VL0	0.0	0.0		E	
PIPE02VV0	0.0	0.0		E	
PIPE02ICHOKE0	0	0		E	

*

```
*****          FILL
*
FILL01000      1  "FW PIPE VELOCITY BOUNDARY"
*              JUN1   IFTY   IFTR   NFTX
FILL01010      1      0      0      4
*              DXIN   VOLIN   ALPIN  VIN   TIN   PIN   BRCIN
FILL01011      0.355  0.0166  0.0   55.2  488.75 7.305E+06 0
*
.END OF INPUTS
```

=ESBWR Annulus Model RWCU

* This file models the annulus between the RPV and RSW

```

*          IEOS   NTRACE   IST   NEXTR
OPTIONS    0       0      -1     0
*          DSTEP   TIMET    STDYST  TRANSI  NCOMP  NJUN  IPAK
MAIN00     0     0.0000E+00   0       1       3     2     1
*          EPSO     EPSI     EPSS   IMPCON  OITMAX  IITMAX
MAIN01     1.0000E-04  1.0000E-04  1.0000E-04   1       10     0
*          SITMAX  NTRX    NDMPTR  ICTR   IBORC  IOPTCD  CMULT
MAIN02     10      0       0       0       0       2     1.0000E+02
*          IAIR   ICONTA  NROT   MIXING
MAIN03     1       0       0       1
  
```

***** COMPONENT LIST CARDS

COMPLIST00 99 01 02

*

***** TIME STEP DATA CARDS

*

*23456789012345678901234567890123456789*123456789012345678901234567890123456789E

```

*          DTMIN   DTMAX    TEND  RTWFP  EDINFP  GFINT   DMPINT   SEDINT
TIMESTEP010  1.0E-08  1.0E-04  0.004  1.0   5.0E-04  5.0E-04  8.0E+03  1.00E+06
TIMESTEP020  1.0E-08  1.0E-03  0.018  1.0   2.0E-03  2.0E-03  8.0E+03  1.00E+06
TIMESTEP030  1.0E-08  2.5E-03  0.200  1.0   5.0E-03  5.0E-03  8.0E+03  1.00E+06
  
```

***** VSSL HEADER CARD

VSSL9900000 99 "3D Annulus"

*

VSSL SIMPLE PARAMETER CARD

```

*          NASX     NRSX     NTSX     NCSR
VSSL9900010    18       2       9       1
*          IDCU   IDCL   IDCR   ICRU   ICRL   ICRR
VSSL9900011     0     0     0     0     0     0
*          ROHS     CPHS     CHS     EMHS
VSSL9900012  2.35000E+03  8.82000E+02  1.62780E+00  7.00000E-01
*          ISDU     ISDL     ISDR
VSSL9900013     0     0     0
*          CZSDL     CRSDV
VSSL9900014  1.00000E+26  1.00000E+26
*          NODESD     DHOUTL     DHOUTV     DTOUTL     DTOUTV
VSSL9900015     0     0.0     0.0     0.0     0.0
  
```

```

VSSL9900110  2.362  Z      5.377      7.637      9.897
VSSL9900111 12.157      14.417     14.757     15.097
VSSL9900112 15.437      15.777     16.117     16.457
VSSL9900113 16.797      17.137     19.005     20.874
VSSL9900114 21.892      31.892  E
  
```

```

VSSL9900120  3.738  RAD      4.646  E
*****
VSSL9900130  0.0698  TH      0.1396     0.2094     0.3491
VSSL9900131  0.7854     1.5708     2.3562     3.1416
VSSL9900132  6.2832  E
  
```

* This set of source cards is commented out, because it is overlaid below:

```

*          ISRL   ISRC   ISRF     JUNS     ZJN
*SSL9900140    13    10    -3       2       0.5
VSSL9900140     8    10    -3       2       0.5
  
```



```
***** Level VSSL99LVNNNN0 Data
VSSL9918ALPNO R09 0.0 R09 1.0 E
VSSL9917ALPNO R09 0.0 R09 1.0 E
VSSL9916ALPNO R09 0.0 R09 1.0 E
VSSL9915ALPNO R09 0.0 R09 1.0 E
VSSL9914ALPNO R09 0.0 R09 1.0 E
VSSL9913ALPNO R09 0.0 R09 1.0 E
VSSL9912ALPNO R09 0.0 R09 1.0 E
VSSL9911ALPNO R09 0.0 R09 1.0 E
VSSL9910ALPNO R09 0.0 R09 1.0 E
VSSL9909ALPNO R09 0.0 R09 1.0 E
VSSL9908ALPNO R09 0.0 R09 1.0 E
VSSL9907ALPNO R09 0.0 R09 1.0 E
VSSL9906ALPNO R09 0.0 R09 1.0 E
VSSL9905ALPNO R09 0.0 R09 1.0 E
VSSL9904ALPNO R09 0.0 R09 1.0 E
VSSL9903ALPNO R09 0.0 R09 1.0 E
VSSL9902ALPNO R09 0.0 R09 1.0 E
VSSL9901ALPNO R09 0.0 R09 1.0 E
VSSL9918DSA0 F 0.0 E
VSSL9917DSA0 F 0.0 E
VSSL9916DSA0 F 0.0 E
VSSL9915DSA0 F 0.0 E
VSSL9914DSA0 F 0.0 E
VSSL9913DSA0 F 0.0 E
VSSL9912DSA0 F 0.0 E
VSSL9911DSA0 F 0.0 E
VSSL9910DSA0 F 0.0 E
VSSL9909DSA0 F 0.0 E
VSSL9908DSA0 F 0.0 E
VSSL9907DSA0 F 0.0 E
VSSL9906DSA0 F 0.0 E
VSSL9905DSA0 F 0.0 E
VSSL9904DSA0 F 0.0 E
VSSL9903DSA0 F 0.0 E
VSSL9902DSA0 F 0.0 E
VSSL9901DSA0 F 0.0 E
VSSL9918DSAZ0 F 0.0 E
VSSL9917DSAZ0 F 0.0 E
VSSL9916DSAZ0 F 0.0 E
VSSL9915DSAZ0 F 0.0 E
VSSL9914DSAZ0 F 0.0 E
VSSL9913DSAZ0 F 0.0 E
VSSL9912DSAZ0 F 0.0 E
VSSL9911DSAZ0 F 0.0 E
VSSL9910DSAZ0 F 0.0 E
VSSL9909DSAZ0 F 0.0 E
VSSL9908DSAZ0 F 0.0 E
VSSL9907DSAZ0 F 0.0 E
VSSL9906DSAZ0 F 0.0 E
VSSL9905DSAZ0 F 0.0 E
VSSL9904DSAZ0 F 0.0 E
VSSL9903DSAZ0 F 0.0 E
VSSL9902DSAZ0 F 0.0 E
VSSL9901DSAZ0 F 0.0 E
```

VSSL9900DSAZO	F 0.0	E
VSSL9918DSSLX0	F 400.0	E
VSSL9917DSSLX0	F 400.0	E
VSSL9916DSSLX0	F 400.0	E
VSSL9915DSSLX0	F 400.0	E
VSSL9914DSSLX0	F 400.0	E
VSSL9913DSSLX0	F 400.0	E
VSSL9912DSSLX0	F 400.0	E
VSSL9911DSSLX0	F 400.0	E
VSSL9910DSSLX0	F 400.0	E
VSSL9909DSSLX0	F 400.0	E
VSSL9908DSSLX0	F 400.0	E
VSSL9907DSSLX0	F 400.0	E
VSSL9906DSSLX0	F 400.0	E
VSSL9905DSSLX0	F 400.0	E
VSSL9904DSSLX0	F 400.0	E
VSSL9903DSSLX0	F 400.0	E
VSSL9902DSSLX0	F 400.0	E
VSSL9901DSSLX0	F 400.0	E
VSSL9918DSHVX0	F 400.0	E
VSSL9917DSHVX0	F 400.0	E
VSSL9916DSHVX0	F 400.0	E
VSSL9915DSHVX0	F 400.0	E
VSSL9914DSHVX0	F 400.0	E
VSSL9913DSHVX0	F 400.0	E
VSSL9912DSHVX0	F 400.0	E
VSSL9911DSHVX0	F 400.0	E
VSSL9910DSHVX0	F 400.0	E
VSSL9909DSHVX0	F 400.0	E
VSSL9908DSHVX0	F 400.0	E
VSSL9907DSHVX0	F 400.0	E
VSSL9906DSHVX0	F 400.0	E
VSSL9905DSHVX0	F 400.0	E
VSSL9904DSHVX0	F 400.0	E
VSSL9903DSHVX0	F 400.0	E
VSSL9902DSHVX0	F 400.0	E
VSSL9901DSHVX0	F 400.0	E
VSSL9918DSTH0	F 0.0	E
VSSL9917DSTH0	F 0.0	E
VSSL9916DSTH0	F 0.0	E
VSSL9915DSTH0	F 0.0	E
VSSL9914DSTH0	F 0.0	E
VSSL9913DSTH0	F 0.0	E
VSSL9912DSTH0	F 0.0	E
VSSL9911DSTH0	F 0.0	E
VSSL9910DSTH0	F 0.0	E
VSSL9909DSTH0	F 0.0	E
VSSL9908DSTH0	F 0.0	E
VSSL9907DSTH0	F 0.0	E
VSSL9906DSTH0	F 0.0	E
VSSL9905DSTH0	F 0.0	E
VSSL9904DSTH0	F 0.0	E
VSSL9903DSTH0	F 0.0	E
VSSL9902DSTH0	F 0.0	E
VSSL9901DSTH0	F 0.0	E

VSSL9918DSTHZ0	F 0.0	E
VSSL9917DSTHZ0	F 0.0	E
VSSL9916DSTHZ0	F 0.0	E
VSSL9915DSTHZ0	F 0.0	E
VSSL9914DSTHZ0	F 0.0	E
VSSL9913DSTHZ0	F 0.0	E
VSSL9912DSTHZ0	F 0.0	E
VSSL9911DSTHZ0	F 0.0	E
VSSL9910DSTHZ0	F 0.0	E
VSSL9909DSTHZ0	F 0.0	E
VSSL9908DSTHZ0	F 0.0	E
VSSL9907DSTHZ0	F 0.0	E
VSSL9906DSTHZ0	F 0.0	E
VSSL9905DSTHZ0	F 0.0	E
VSSL9904DSTHZ0	F 0.0	E
VSSL9903DSTHZ0	F 0.0	E
VSSL9902DSTHZ0	F 0.0	E
VSSL9901DSTHZ0	F 0.0	E
VSSL9900DSTHZ0	F 400.0	E
VSSL9918DSTLX0	F 400.0	E
VSSL9917DSTLX0	F 400.0	E
VSSL9916DSTLX0	F 400.0	E
VSSL9915DSTLX0	F 400.0	E
VSSL9914DSTLX0	F 400.0	E
VSSL9913DSTLX0	F 400.0	E
VSSL9912DSTLX0	F 400.0	E
VSSL9911DSTLX0	F 400.0	E
VSSL9910DSTLX0	F 400.0	E
VSSL9909DSTLX0	F 400.0	E
VSSL9908DSTLX0	F 400.0	E
VSSL9907DSTLX0	F 400.0	E
VSSL9906DSTLX0	F 400.0	E
VSSL9905DSTLX0	F 400.0	E
VSSL9904DSTLX0	F 400.0	E
VSSL9903DSTLX0	F 400.0	E
VSSL9902DSTLX0	F 400.0	E
VSSL9901DSTLX0	F 400.0	E
VSSL9918DSTVX0	F 400.0	E
VSSL9917DSTVX0	F 400.0	E
VSSL9916DSTVX0	F 400.0	E
VSSL9915DSTVX0	F 400.0	E
VSSL9914DSTVX0	F 400.0	E
VSSL9913DSTVX0	F 400.0	E
VSSL9912DSTVX0	F 400.0	E
VSSL9911DSTVX0	F 400.0	E
VSSL9910DSTVX0	F 400.0	E
VSSL9909DSTVX0	F 400.0	E
VSSL9908DSTVX0	F 400.0	E
VSSL9907DSTVX0	F 400.0	E
VSSL9906DSTVX0	F 400.0	E
VSSL9905DSTVX0	F 400.0	E
VSSL9904DSTVX0	F 400.0	E
VSSL9903DSTVX0	F 400.0	E
VSSL9902DSTVX0	F 400.0	E
VSSL9901DSTVX0	F 400.0	E

VSSL9903FRICN-Z0	F	0.0	E
VSSL9902FRICN-Z0	F	0.0	E
VSSL9901FRICN-Z0	F	0.0	E
VSSL9918FRICP-R0	F	0.0	E
VSSL9917FRICP-R0	F	0.0	E
VSSL9916FRICP-R0	F	0.0	E
VSSL9915FRICP-R0	F	0.0	E
VSSL9914FRICP-R0	F	0.0	E
VSSL9913FRICP-R0	F	0.0	E
VSSL9912FRICP-R0	F	0.0	E
VSSL9911FRICP-R0	F	0.0	E
VSSL9910FRICP-R0	F	0.0	E
VSSL9909FRICP-R0	F	0.0	E
VSSL9908FRICP-R0	F	0.0	E
VSSL9907FRICP-R0	F	0.0	E
VSSL9906FRICP-R0	F	0.0	E
VSSL9905FRICP-R0	F	0.0	E
VSSL9904FRICP-R0	F	0.0	E
VSSL9903FRICP-R0	F	0.0	E
VSSL9902FRICP-R0	F	0.0	E
VSSL9901FRICP-R0	F	0.0	E
VSSL9918FRICP-T0	F	0.0	E
VSSL9917FRICP-T0	F	0.0	E
VSSL9916FRICP-T0	F	0.0	E
VSSL9915FRICP-T0	F	0.0	E
VSSL9914FRICP-T0	F	0.0	E
VSSL9913FRICP-T0	F	0.0	E
VSSL9912FRICP-T0	F	0.0	E
VSSL9911FRICP-T0	F	0.0	E
VSSL9910FRICP-T0	F	0.0	E
VSSL9909FRICP-T0	F	0.0	E
VSSL9908FRICP-T0	F	0.0	E
VSSL9907FRICP-T0	F	0.0	E
VSSL9906FRICP-T0	F	0.0	E
VSSL9905FRICP-T0	F	0.0	E
VSSL9904FRICP-T0	F	0.0	E
VSSL9903FRICP-T0	F	0.0	E
VSSL9902FRICP-T0	F	0.0	E
VSSL9901FRICP-T0	F	0.0	E
VSSL9918FRICP-Z0	F	0.0	E
VSSL9917FRICP-Z0	F	0.0	E
VSSL9916FRICP-Z0	F	0.0	E
VSSL9915FRICP-Z0	F	0.0	E
VSSL9914FRICP-Z0	F	0.0	E
VSSL9913FRICP-Z0	F	0.0	E
VSSL9912FRICP-Z0	F	0.0	E
VSSL9911FRICP-Z0	F	0.0	E
VSSL9910FRICP-Z0	F	0.0	E
VSSL9909FRICP-Z0	F	0.0	E
VSSL9908FRICP-Z0	F	0.0	E
VSSL9907FRICP-Z0	F	0.0	E
VSSL9906FRICP-Z0	F	0.0	E
VSSL9905FRICP-Z0	F	0.0	E
VSSL9904FRICP-Z0	F	0.0	E
VSSL9903FRICP-Z0	F	0.0	E

VSSL9901520000	F	400.0	E
VSSL9918PA0	F	1.0133E+05	E
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VSSL9909PA0	F	1.0133E+05	E
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VSSL9907PA0	F	1.0133E+05	E
VSSL9906PA0	F	1.0133E+05	E
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Enclosure 1
Attachment 2

VSSL9918TVNO	F	373.1	E
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*

***** PIPE

*

PIPE02000	2	"FW BREAK AND VESSEL"			
*	NCELLS	NODES	JUN1	JUN2	MAT
PIPE02010	1	0	1	2	0
PIPE02DX0		0.355		E	
PIPE02VOL0		0.0233		E	
PIPE02TLO		545.5		E	
PIPE02TVO		545.5		E	
PIPE02P0		7.235E+06		E	
PIPE02PA0		0.0		E	
PIPE02ALP		0.0		E	
PIPE02FRICN0	0.0	1.0		E	
PIPE02FRICP0	0.0	0.0		E	
PIPE02FA0	0.0656	0.0656		E	
PIPE02VLO	0.0	0.0		E	
PIPE02VVO	0.0	0.0		E	
PIPE02ICHOKE0	0	0		E	

*

```
*****          FILL
*
FILL01000      1  "FW PIPE VELOCITY BOUNDARY"
*              JUN1      IFTY      IFTR      NFTX
FILL01010      1          0          0          4
*              DXIN      VOLIN      ALPIN      VIN      TIN      PIN      BORCIN
FILL01011      0.355    0.0233    0.0      31.8    545.5  7.235E+06  0
*
.END OF INPUTS
```

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Attachment 3 - Break Boundary Conditions

Feedwater Line Break

The FW line break flow is from both sides of the break. From ref. 2, attachment 2, the RPV side break area is limited by the sum of nozzle areas attached to the feedwater sparger. The flow feeding the feedwater line sees a limiting flow area at the break between the RPV and RSW.

The feedwater line thermal hydraulic conditions are obtained from the reactor heatbalance of reference 3. The pressure at the feedwater line break is based on the steady state TRACG calculation in reference 3 for nominal conditions, (from reference 4 the feedwater component is tee 0061, cell 10 connects to the vessel and represents the safe end break location).

$A_1 = 0.0280\text{m}^2$	$A_1 = 0.301\text{ft}^2$	RPV side - 18 sparger nozzle areas (ref. 2)
$A_2 = 0.0656\text{m}^2$	$A_2 = 0.706\text{ft}^2$	RSW side - FW pipe flow area (ref. 2)
$A = \frac{(A_1 + A_2)}{2}$		Combined flow area is 1/2 actual flow area since we are modeling only 1/2 the annulus.
$A = 0.0468\text{m}^2$	$A = 0.504\text{ft}^2$	
$P = 7.305 \cdot 10^6 \text{Pa}$	$P = 1060 \text{psi}$	FW line pressure, from ref. 3, TRACG component TEE0061, cell 9.
$h = 0.925 \cdot 10^6 \frac{\text{joule}}{\text{kg}}$	$h = 397.7 \frac{\text{BTU}}{\text{lb}}$	FW enthalpy (ref. 3)
$T = 488.75\text{K}$		FW temperature (ref. 3)
$v_f = 1.176 \cdot 10^{-3} \frac{\text{m}^3}{\text{kg}}$	$v_f = 0.0188 \frac{\text{ft}^3}{\text{lb}}$	specific volume from steam tables (ref. 6)
$P_{\text{annulus}} = 0.101325 \cdot 10^6 \text{Pa}$	$P_{\text{annulus}} = 14.7 \text{psi}$	

The critical mass flux may be used to find the mass flow rate through the break.

$$G_c = 9.389 \times 10^4 \frac{\text{kg}}{\text{s} \cdot \text{m}^2} \quad G_c = 19230 \frac{\text{lb}}{\text{s} \cdot \text{ft}^2} \quad \text{From reference 7 using above input}$$

Note: in the ref. 1 analysis, the critical mass flow rate has been adjusted by correcting for the over-prediction of the critical mass flux during inventory depletion. This was done by applying a critical flow inventory multiplier, *f* (see reference 5). For conservatism, the reduction multiplier is not applied for the ESBWR analysis (value set to 1.0). If the multiplier had been included, the break flow would be significantly reduced, thus lowering the peak AP load.

$$f_1 = 1.0 \quad \text{subscript 1 is the RPV side}$$

$$f_2 = 1.0 \quad \text{subscript 2 is the FW supply side}$$

$$m_1 = f_1 \cdot G_c \cdot A_1$$

$$m_2 = f_2 \cdot G_c \cdot A_2$$

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$$m_1 = 2629 \frac{\text{kg}}{\text{s}}$$

$$m_2 = 6159 \frac{\text{kg}}{\text{s}}$$

The total mass flow rate is found by combining the flow from the two sources. Since we are modeling only 1/2 the annulus, the total mass flow rate entering the model is 1/2 the total flow rate.

$$m_{\text{tot}} = \frac{1}{2}(m_1 + m_2)$$

$$m_{\text{tot}} = 4394 \frac{\text{kg}}{\text{s}}$$

$$V = \frac{m_{\text{tot}} \cdot \gamma_f}{(A_1 + A_2)}$$

velocity at break

$$V = 55.207 \frac{\text{m}}{\text{s}}$$

value applied to TRACG boundary condition
 (component FILL01)

RWCU/SDC Line Break

The RWCU/SDC line break flow is from both sides of the break. The flow area is based on the piping ID from ref. 2, attachment 2

The RWCU line thermal hydraulic conditions are obtained from the reactor heatbalance of reference 3. The pressure at the feedwater line break is based on the conditions in the downcomer at the elevation of the RWCU/SDC line. This is obtained from the steady state TRACG calculation in reference 3 for nominal conditions, (VSSL level 15, theta node 10).

$A_1 = 0.0656 \text{m}^2$	$A_1 = 0.706 \text{ft}^2$	RPV side - 18 sparger nozzle areas (ref. 2)
$A_2 = 0.0656 \text{m}^2$	$A_2 = 0.706 \text{ft}^2$	RSW side - FW pipe flow area (ref. 2)
$A = \frac{(A_1 + A_2)}{2}$		Combined flow area is 1/2 actual flow area since we are modeling only 1/2 the annulus.
$A = 0.0656 \text{m}^2$	$A = 0.706 \text{ft}^2$	
$P = 7.235 \cdot 10^6 \text{Pa}$	$P = 1049 \text{psi}$	Downcomer pressure at RWCU elevation (ref 3)
$h = 1.1967 \cdot 10^6 \frac{\text{joule}}{\text{kg}}$	$h = 514.5 \frac{\text{BTU}}{\text{lb}}$	Downcomer enthalpy at RWCU elev. (ref. 3)
$T = 545.5 \text{K}$		FW temperature (ref. 3)
$v_f = 1.305 \cdot 10^{-3} \frac{\text{m}^3}{\text{kg}}$	$v_f = 0.0209 \frac{\text{ft}^3}{\text{lb}}$	specific volume from steam tables (ref. 6)
$P_{\text{annulus}} = 0.101325 \cdot 10^6 \text{Pa}$	$P_{\text{annulus}} = 14.7 \text{psi}$	

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ESBWR Annulus Pressurization

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The critical mass flux may be used to find the mass flow rate through the break.

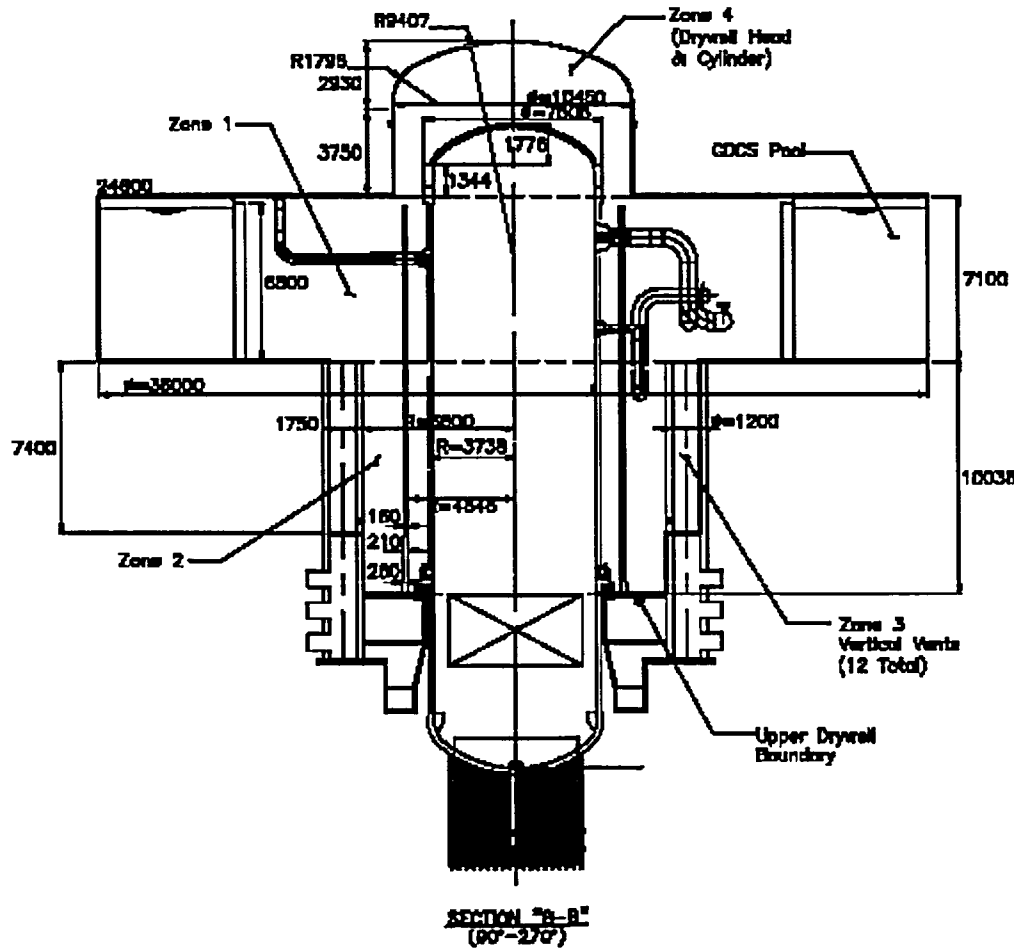
$$G_c = 4.868 \cdot 10^4 \frac{\text{kg}}{\text{m}^2 \text{s}} \quad G_c = 9970 \frac{\text{lb}}{\text{s} \cdot \text{ft}^2} \quad \text{From reference 7 using above input.}$$

Note: in the ref. 1 analysis, the critical mass flow rate has been adjusted by correcting for the over-prediction of the critical mass flux during inventory depletion. This was done by applying a critical flow inventory multiplier, f (see reference 5). For conservatism, the reduction multiplier is not applied for the ESBWR analysis (value set to 1.0). If the multiplier had been included, the break flow would be reduced, thus lowering the peak AP load.

$$\begin{aligned} f_1 &= 1.0 && \text{subscript 1 is the RPV side} \\ f_2 &= 1.0 && \text{subscript 2 is the FW supply side} \\ m_1 &= f_1 \cdot G_c \cdot A_1 \\ m_2 &= f_2 \cdot G_c \cdot A_2 \\ m_1 &= 3193 \frac{\text{kg}}{\text{s}} \\ m_2 &= 3193 \frac{\text{kg}}{\text{s}} \end{aligned}$$

The total mass flow rate is found by combining the flow from the two sources. Since we are modeling only 1/2 the annulus, the total mass flow rate entering the model is 1/2 the total flow rate.

$$\begin{aligned} m_{\text{tot}} &= \frac{1}{2} (m_1 + m_2) \\ m_{\text{tot}} &= 3193 \frac{\text{kg}}{\text{s}} \\ V &= \frac{m_{\text{tot}} \cdot V_f}{(A_1 + A_2)} && \text{velocity at break} \\ V &= 31.764 \frac{\text{m}}{\text{s}} && \text{value applied to TRACG boundary condition} \\ &&& \text{(component FILL01)} \end{aligned}$$



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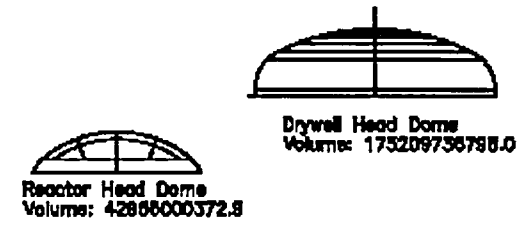


Figure 2. Upper Drywell