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U. S. Nuclear Regulatory Commission
ATTN: Document Control Desk
Washington, D. C. 20555-0001

Joseph M. Farley Nuclear Plant – Unit 2
Cycle 19 Core Operating Limits Report

Ladies and Gentlemen:

In accordance with Technical Specification 5.6.5.d, Southern Nuclear Operating Company submits the enclosed Core Operating Limits Report (COLR) for Farley Nuclear Plant Unit 2 Cycle 19, Rev. 0.

This letter contains no NRC commitments. If there are any questions, please advise.

Sincerely,

A handwritten signature in black ink, appearing to read "B. J. George". The signature is written in a cursive style with a long horizontal stroke at the end.

B. J. George
Manager, Nuclear Licensing

BJG/CHM/daj

Enclosure: FNP Core Operating Limits Report Unit 2– Cycle 19, Rev. 0

cc: Southern Nuclear Operating Company
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**Joseph M. Farley Nuclear Plant – Unit 2
Cycle 19 Core Operating Limits Report**

Enclosure

FNP Core Operating Limits Report Unit 2– Cycle 19, Rev. 0



Joseph M. Farley Nuclear Plant

Core Operating Limits Report

Unit 2 - Cycle 19

Revision 0

1.0 CORE OPERATING LIMITS REPORT

This Core Operating Limits Report (COLR) for FNP UNIT 2 CYCLE 18 has been prepared in accordance with the requirements of Technical Specification 5.6.5.

The Technical Requirement affected by this report is listed below:

13.1.1 SHUTDOWN MARGIN - MODES 1 and 2 (with $k_{\text{eff}} \geq 1$)

The Technical Specifications affected by this report are listed below:

2.1.1 Reactor Core Safety Limits for THERMAL POWER

3.1.1 SHUTDOWN MARGIN - MODES 2 (with $k_{\text{eff}} < 1$), 3, 4 and 5

3.1.3 Moderator Temperature Coefficient

3.1.5 Shutdown Bank Insertion Limits

3.1.6 Control Bank Insertion Limits

3.2.1 Heat Flux Hot Channel Factor - $F_Q(Z)$

3.2.2 Nuclear Enthalpy Rise Hot Channel Factor - $F_{\Delta H}^N$

3.2.3 Axial Flux Difference

3.3.1 Reactor Trip System Instrumentation Overtemperature ΔT (OT ΔT) and Overpower ΔT (OP ΔT) Setpoint Parameter Values for Table 3.3.1-1

3.4.1 RCS DNB Parameters for Pressurizer Pressure, RCS Average Temperature, and RCS Total Flow Rate

3.9.1 Boron Concentration

2.0 OPERATING LIMITS

The cycle-specific parameter limits for the specifications listed in Section 1.0 are presented in the following subsections. These limits have been developed using NRC-approved methodologies, including those specified in Technical Specification 5.6.5.

2.1 SHUTDOWN MARGIN - MODES 1 AND 2 (with $k_{\text{eff}} \geq 1.0$) (Technical Requirement 13.1.1)

2.1.1 The SHUTDOWN MARGIN shall be greater than or equal to 1.77 percent $\Delta k/k$.

2.2 SHUTDOWN MARGIN - MODES 2 (with $k_{\text{eff}} < 1.0$), 3, 4 and 5 (Specification 3.1.1)

2.2.1 Modes 2 ($k_{\text{eff}} < 1.0$), 3 and 4 - The SHUTDOWN MARGIN shall be greater than or equal to 1.77 percent $\Delta k/k$.

2.2.2 Mode 5 - The SHUTDOWN MARGIN shall be greater than or equal to 1.0 percent $\Delta k/k$.

2.3 Moderator Temperature Coefficient (Specification 3.1.3)

2.3.1 The Moderator Temperature Coefficient (MTC) limits are:

The BOL/ARO/HZP-MTC shall be less than or equal to $+0.7 \times 10^{-4} \Delta k/k/^\circ\text{F}$ for power levels up to 70 percent RTP with a linear ramp to 0 $\Delta k/k/^\circ\text{F}$ at 100 percent RTP.

The EOL/ARO/RTP-MTC shall be less negative than $-4.3 \times 10^{-4} \Delta k/k/^\circ\text{F}$.

2.3.2 The MTC Surveillance limits are:

The 300 ppm/ARO/RTP-MTC should be less negative than or equal to $-3.65 \times 10^{-4} \Delta k/k/^\circ\text{F}$.

The 100 ppm/ARO/RTP-MTC should be less negative than $-4.0 \times 10^{-4} \Delta k/k/^\circ\text{F}$.

where: BOL stands for Beginning of Cycle Life
ARO stands for All Rods Out
HZP stands for Hot Zero THERMAL POWER
EOL stands for End of Cycle Life
RTP stands for RATED THERMAL POWER

2.4 Shutdown Bank Insertion Limits (Specification 3.1.5)

2.4.1 The shutdown banks shall be withdrawn to a position greater than or equal to 225 steps.

2.5 Control Bank Insertion Limits (Specification 3.1.6)

2.5.1 The control rod banks shall be limited in physical insertion as shown in Figure 1.

2.6 Heat Flux Hot Channel Factor - $F_Q(Z)$ (Specification 3.2.1)

$$2.6.1 \quad F_Q(Z) \leq \frac{F_Q^{RTP}}{P} * K(Z) \quad \text{for } P > 0.5$$

$$F_Q(Z) \leq \frac{F_Q^{RTP}}{0.5} * K(Z) \quad \text{for } P \leq 0.5$$

$$\text{where: } P = \frac{\text{THERMALPOWER}}{\text{RATEDTHERMALPOWER}}$$

$$2.6.2 \quad F_Q^{RTP} = 2.50$$

2.6.3 $K(Z)$ is provided in Figure 2.

$$2.6.4 \quad F_Q(Z) \leq \frac{F_Q^{RTP} * K(Z)}{P * W(Z)} \quad \text{for } P > 0.5$$

$$F_Q(Z) \leq \frac{F_Q^{RTP} * K(Z)}{0.5 * W(Z)} \quad \text{for } P \leq 0.5$$

2.6.5 $W(Z)$ values are provided in Table 4.

2.6.6 The $F_Q(Z)$ penalty factors are provided in Table 1.

2.7 Nuclear Enthalpy Rise Hot Channel Factor - $F_{\Delta H}^N$ (Specification 3.2.2)

$$2.7.1 \quad F_{\Delta H}^N \leq F_{\Delta H}^{RTP} * (1 + PF_{\Delta H} * (1 - P))$$

$$\text{where: } P = \frac{\text{THERMAL POWER}}{\text{RATED THERMAL POWER}}$$

$$2.7.2 \quad F_{\Delta H}^{RTP} = 1.70$$

$$2.7.3 \quad PF_{\Delta H} = 0.3$$

2.8 Axial Flux Difference (Specification 3.2.3)

2.8.1 The Axial Flux Difference (AFD) acceptable operation limits are provided in Figure 3.

2.9 Boron Concentration (Specification 3.9.1)

2.9.1 The boron concentration shall be greater than or equal to 2000 ppm.¹

2.10 Reactor Core Safety Limits for THERMAL POWER (Specification 2.1.1)

2.10.1 In MODES 1 and 2, the combination of THERMAL POWER, Reactor Coolant System (RCS) highest loop average temperature, and pressurizer pressure shall not exceed the safety limits specified in Figure 4.

2.11 Reactor Trip System Instrumentation Overtemperature ΔT (OT ΔT) and Overpower ΔT (OP ΔT) Setpoint Parameter Values for Table 3.3.1-1 (Specification 3.3.1)

2.11.1 The Reactor Trip System Instrumentation Overtemperature ΔT (OT ΔT) and Overpower ΔT (OP ΔT) setpoint parameter values for TS Table 3.3.1-1 are listed in COLR Tables 2 and 3.

¹ This concentration bounds the condition of $k_{\text{eff}} \leq 0.95$ (all rods in less the most reactive rod) and subcriticality (all rods out) over the entire cycle. This concentration includes additional boron to address uncertainties and B¹⁰ depletion.

2.12 RCS DNB Parameters for Pressurizer Pressure, RCS Average Temperature, and RCS Total Flow Rate (Specification 3.4.1)

2.12.1 RCS DNB parameters for pressurizer pressure, RCS average temperature, and RCS total flow rate shall be within the limits specified below:

- a. Pressurizer pressure ≥ 2209 psig;
- b. RCS average temperature $\leq 580.3^{\circ}\text{F}$; and
- c. The minimum RCS total flow rate shall be $\geq 263,400$ GPM when using the precision heat balance method and $\geq 264,200$ GPM when using the elbow tap method.

Table 1

$F_Q(Z)$ Penalty Factor

Cycle Burnup (MWD/MTU)	$F_Q(Z)$ Penalty Factor
354	1.020
559	1.024
763	1.036
1376	1.036
1580	1.026
1784	1.020
5052	1.020
5256	1.029
6278	1.034
6891	1.029
7095	1.021
7299	1.020

Notes:

1. The Penalty Factor, to be applied to $F_Q(Z)$ in accordance with SR 3.2.1.2, is the maximum factor by which $F_Q(Z)$ is expected to increase over a 39 EFPD interval (surveillance interval of 31 EFPD plus the maximum allowable extension not to exceed 25% of the surveillance interval per SR 3.0.2) starting from the burnup at which the $F_Q(Z)$ was determined.
2. Linear interpolation is adequate for intermediate cycle burnups.
3. For all cycle burnups outside the range of the table, a penalty factor of 1.020 shall be used.

Table 2

**Reactor Trip System Instrumentation - Overtemperature ΔT (OT ΔT)
Setpoint Parameter Values**

$T' \leq 577.2^\circ\text{F}$	$P' = 2235 \text{ psig}$	
$K_1 = 1.17$	$K_2 = 0.017/^\circ\text{F}$	$K_3 = 0.000825/\text{psi}$
$\tau_1 \geq 30 \text{ sec}$	$\tau_2 \leq 4 \text{ sec}$	
$\tau_4 = 0 \text{ sec}$	$\tau_5 \leq 6 \text{ sec}$	$\tau_6 \leq 6 \text{ sec}$
$f_1(\Delta I) =$	$-2.48 \{23 + (q_t - q_b)\}$ 0% of RTP $2.05 \{(q_t - q_b) - 15\}$	when $(q_t - q_b) \leq -23\% \text{ RTP}$ when $-23\% \text{ RTP} < (q_t - q_b) \leq 15\% \text{ RTP}$ when $(q_t - q_b) > 15\% \text{ RTP}$

Table 3

**Reactor Trip System Instrumentation - Overpower ΔT (OP ΔT)
Setpoint Parameter Values**

$$T'' \leq 577.2^{\circ}\text{F}$$

$$K_4 = 1.10$$

$$K_5 = 0.02/^{\circ}\text{F} \text{ for increasing } T_{\text{avg}}$$
$$K_5 = 0/^{\circ}\text{F} \text{ for decreasing } T_{\text{avg}}$$

$$K_6 = 0.00109/^{\circ}\text{F} \text{ when } T > T''$$
$$K_6 = 0/^{\circ}\text{F} \text{ when } T \leq T''$$

$$\tau_3 \geq 10 \text{ sec}$$

$$\tau_4 = 0 \text{ sec}$$

$$\tau_5 \leq 6 \text{ sec}$$

$$\tau_6 \leq 6 \text{ sec}$$

$$f_2(\Delta I) = 0\% \text{ RTP for all } \Delta I$$

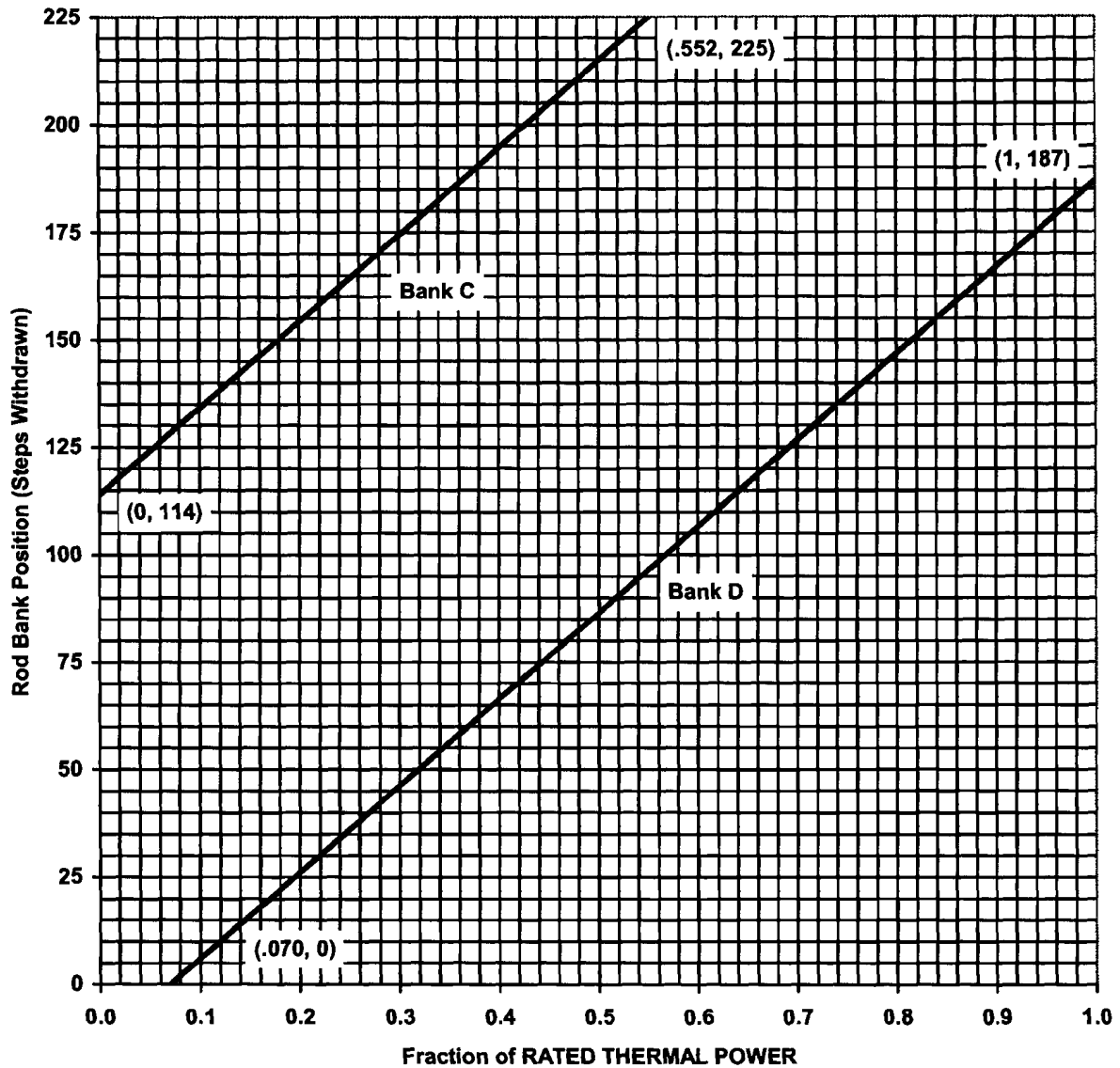
Table 4
RAOC W(Z)

	Axial Point	Elevation (feet)	150 MWD/MTU	4000 MWD/MTU	10000 MWD/MTU	18000 MWD/MTU
*	1	12.00	1.0000	1.0000	1.0000	1.0000
*	2	11.80	1.0000	1.0000	1.0000	1.0000
*	3	11.60	1.0000	1.0000	1.0000	1.0000
*	4	11.40	1.0000	1.0000	1.0000	1.0000
*	5	11.20	1.0000	1.0000	1.0000	1.0000
	6	11.00	1.1352	1.2433	1.2611	1.2476
	7	10.80	1.1303	1.2405	1.2566	1.2410
	8	10.60	1.1246	1.2362	1.2508	1.2354
	9	10.40	1.1227	1.2303	1.2443	1.2287
	10	10.20	1.1307	1.2242	1.2370	1.2216
	11	10.00	1.1380	1.2164	1.2280	1.2142
	12	9.80	1.1419	1.2067	1.2305	1.2104
	13	9.60	1.1441	1.1980	1.2325	1.2182
	14	9.40	1.1451	1.1912	1.2355	1.2223
	15	9.20	1.1431	1.1825	1.2356	1.2246
	16	9.00	1.1403	1.1713	1.2385	1.2332
	17	8.80	1.1432	1.1695	1.2492	1.2480
	18	8.60	1.1543	1.1738	1.2610	1.2657
	19	8.40	1.1656	1.1841	1.2726	1.2854
	20	8.20	1.1743	1.1910	1.2819	1.3064
	21	8.00	1.1808	1.1956	1.2880	1.3236
	22	7.80	1.1852	1.1982	1.2910	1.3370
	23	7.60	1.1874	1.1985	1.2910	1.3466
	24	7.40	1.1879	1.1970	1.2881	1.3525
	25	7.20	1.1878	1.1948	1.2825	1.3549
	26	7.00	1.1861	1.1910	1.2743	1.3538
	27	6.80	1.1827	1.1857	1.2639	1.3496
	28	6.60	1.1781	1.1789	1.2514	1.3424
	29	6.40	1.1721	1.1709	1.2371	1.3324
	30	6.20	1.1651	1.1619	1.2212	1.3198
	31	6.00	1.1575	1.1520	1.2034	1.3046
	32	5.80	1.1475	1.1405	1.1870	1.2878
	33	5.60	1.1514	1.1329	1.1737	1.2669
	34	5.40	1.1632	1.1333	1.1647	1.2466
	35	5.20	1.1737	1.1406	1.1622	1.2425
	36	5.00	1.1834	1.1477	1.1604	1.2400
	37	4.80	1.1924	1.1536	1.1583	1.2348
	38	4.60	1.2004	1.1589	1.1560	1.2279
	39	4.40	1.2074	1.1634	1.1524	1.2189
	40	4.20	1.2133	1.1669	1.1477	1.2079
	41	4.00	1.2180	1.1694	1.1420	1.1950
	42	3.80	1.2216	1.1711	1.1353	1.1805
	43	3.60	1.2238	1.1716	1.1302	1.1665
	44	3.40	1.2270	1.1719	1.1282	1.1536
	45	3.20	1.2383	1.1752	1.1256	1.1395
	46	3.00	1.2535	1.1836	1.1243	1.1376
	47	2.80	1.2708	1.1977	1.1315	1.1485
	48	2.60	1.2910	1.2148	1.1375	1.1637
	49	2.40	1.3133	1.2349	1.1438	1.1779
	50	2.20	1.3352	1.2568	1.1501	1.1919
	51	2.00	1.3566	1.2785	1.1590	1.2060
	52	1.80	1.3774	1.2995	1.1679	1.2201
	53	1.60	1.3974	1.3198	1.1768	1.2342
	54	1.40	1.4164	1.3389	1.1858	1.2483
	55	1.20	1.4342	1.3567	1.1945	1.2623
	56	1.00	1.4501	1.3727	1.2027	1.2759
*	57	0.80	1.0000	1.0000	1.0000	1.0000
*	58	0.60	1.0000	1.0000	1.0000	1.0000
*	59	0.40	1.0000	1.0000	1.0000	1.0000
*	60	0.20	1.0000	1.0000	1.0000	1.0000
*	61	0.00	1.0000	1.0000	1.0000	1.0000

* Top and bottom 5 axial points excluded per Technical Specification B 3.2.1.

Figure 1
Rod Bank Insertion Limits versus Rated Thermal Power

Fully Withdrawn – 225 to 231 steps, inclusive



Fully Withdrawn shall be the condition where control rods are at a position within the interval ≥ 225 and ≤ 231 steps withdrawn.

Note: The Rod Bank Insertion Limits are based on the control bank withdrawal sequence A, B, C, D and a control bank tip-to-tip distance of 128 steps.

Figure 2
K(Z) – Normalized $F_Q(Z)$ as a Function of Core Height

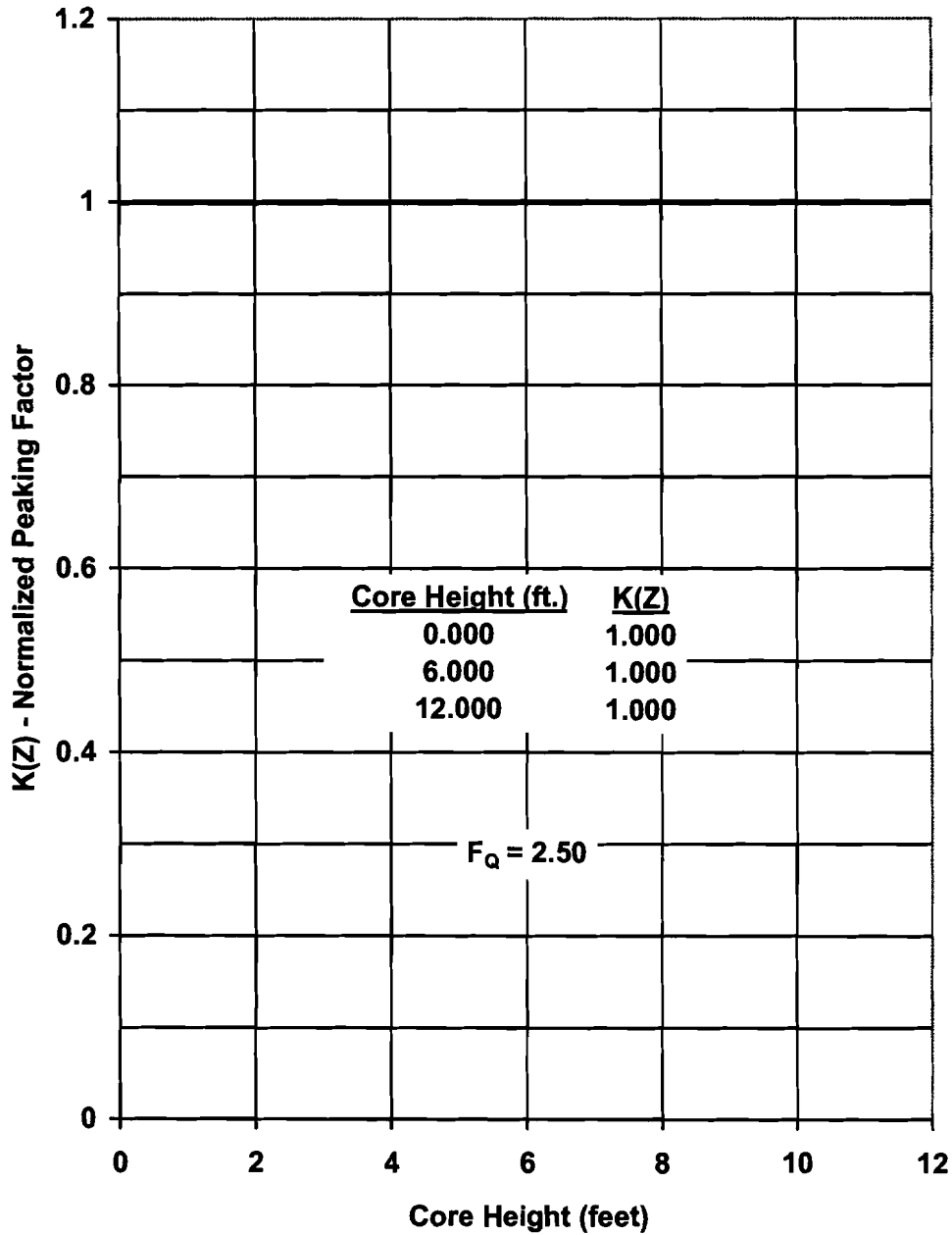


Figure 3
Axial Flux Difference Limits as a Function of
Rated Thermal Power for RAOC

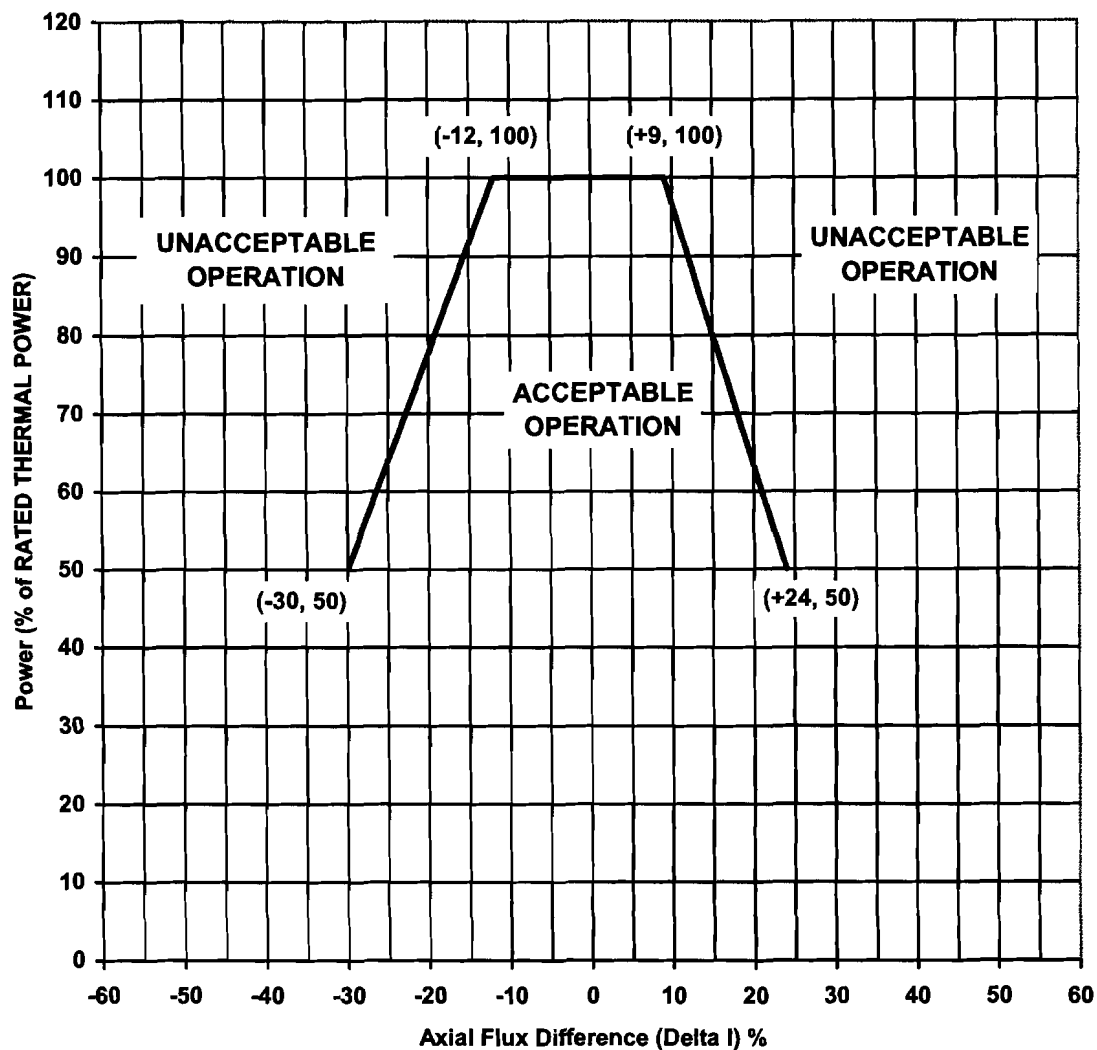


Figure 4
Reactor Core Safety Limits

