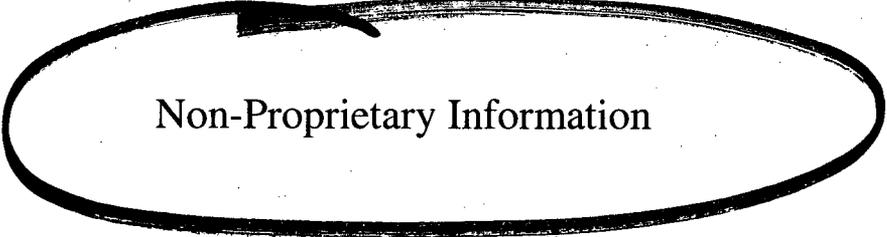


ENCLOSURE 2

FLN-2007-015

**GNF Technology Update Meeting, May 1-2, 2007, Draft
Presentations**



Non-Proprietary Information

IMPORTANT NOTICE

This is a non-proprietary version of Enclosure 1 to FLN-2007-015, which has the proprietary information removed. Portions of the document that have been removed are indicated by white space with an open and closed bracket as shown here [[]].

GNF Technology Update Meeting

LANCER/AETNA Status

Scott Palmtag

May 1-2, 2007

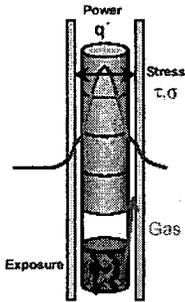


Global Nuclear Fuel

A Joint Venture of GE, Toshiba, & Hitachi

Preliminary Unverified Information

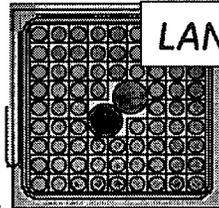
New Methods Code Suite



PRIME

Fuel rod thermal-mechanical
Mechanical behavior of fuel rod.

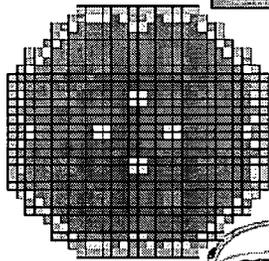
(Replaces GSTRM)



LANCER

2-D Lattice Physics
Nuclear Behavior of Fuel Rods Within Bundle.

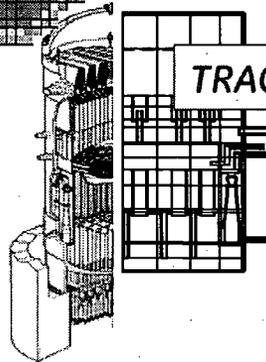
(Replaces TGBLA)



AETNA

3-D Core Simulation
Nuclear + Thermal-Hydraulic Behavior of Bundles in Core

(Replaces PANAC)



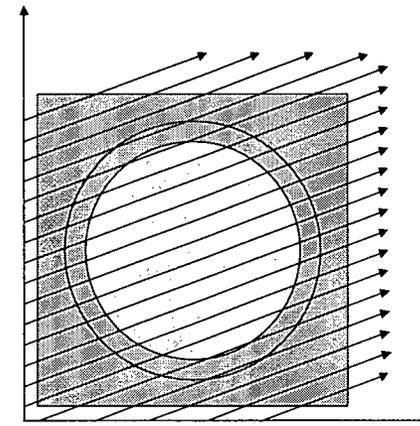
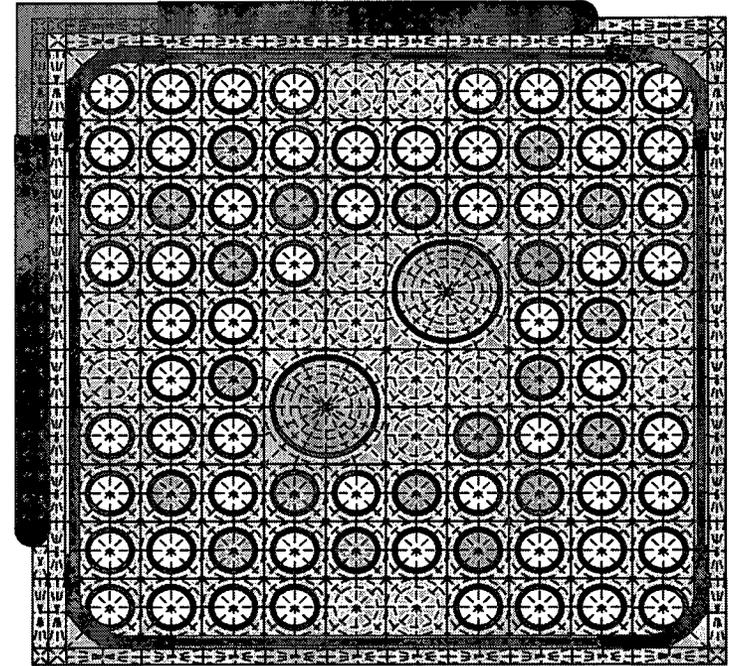
TRACG

Best Estimate Analysis of Operational Transients

(Replaces ODYN, TASC, SAFER, CORCL)

LANCER Highlights

- Model fuel rods (U+Gad) , water Rods, control blade within lattice
- Complex/exact geometry & material
- 2D fine-mesh spatial resolution (multiple angular + radial discretization)
- Method of Characteristics (MOC) transport solution – neutrons and gammas
- Detailed isotopic tracking
- Detailed neutron energy group structure
- Fine time-step temporal resolution (exposure dependence)
- Fundamental nuclear data from ENDF/B-VII



LANCER Status

[[

{3}]]

LANCER Benchmarks

Single assembly benchmarking against MCNP for a wide range of BWR applications

- High enrichment/Low enrichment
- High void/Low void
- High Gd/Low Gd
- Lumped Gd/Evenly distributed Gd
- Controlled/Uncontrolled
- Hot/Cold
- UOX/MOX
- Burnup (compare to MCNP/MOCUP)

Uncontrolled Δk (unverified)

[[

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Controlled Δk (unverified)

[[

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Uncontrolled Pin-wise %rms (unverified)

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Controlled Pin-wise %rms (unverified)

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0% Void Depletion (unverified)

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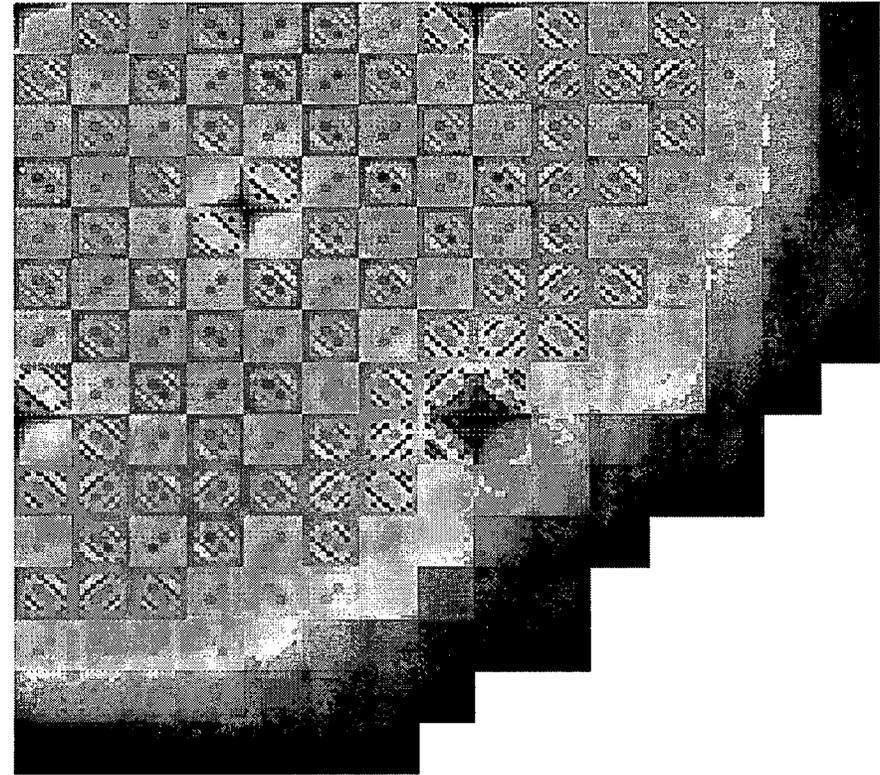
80% Void Depletion (unverified)

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AETNA Highlights

- Model all fuel bundles, control blades, and T/H within core
- Coupled neutronic-T/H feedback
- 3D coarse-mesh spatial resolution
- Few-group energy structure
- Diffusion theory physics (homogeneous solution)
- Pin power reconstruction (heterogeneous solution)
- Detailed nuclear data obtained from LANCER



*Improve Current and Future Applications
(e.g. EPU, ESBWR, MOX)*

AETNA Feature Detail

Built Upon PANAC11 Software Base

- Retain Functionality, User Interface and Automation Support

Cross Section Model

- Expanded Functional Matrix
 - **100% Void Branch / History**
 - Control Blade History
- Improved Spectral History Models (Void & Control Blade)

T/H Physics

- **All Channels modeled - T/H**
(5 Eqn. T/H)
- Multiple Bypass Regions
- Bypass Voiding
- ESBWR Modeling
 - 16 Bundle Chimney
 - Natural Circulation Heat Balance

Nodal Physics Models

- Semi-Analytic Nodal Method
- **3 Energy Groups** (Fast, Epithermal, Thermal)
- Improved Pin Power Reconstruction
- **Isotopic tracking** includes ^{241}Pu - ^{241}Am ,
 ^{135}I - ^{135}Xe , ^{149}Pm - ^{149}Sm , ^{140}Ba
- **Multi control blade modeling**
- Exposure Dependent Fuel Temperatures
- Channel Distortion
- Advanced Detector Models

Target Platform: Windows PC

AETNA Status

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Cycles 1-3 BWR/4 (unverified)

Forthcoming

Cycles 1-8 BWR/6 (unverified)

Forthcoming

Licensing Schedule

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Further Development

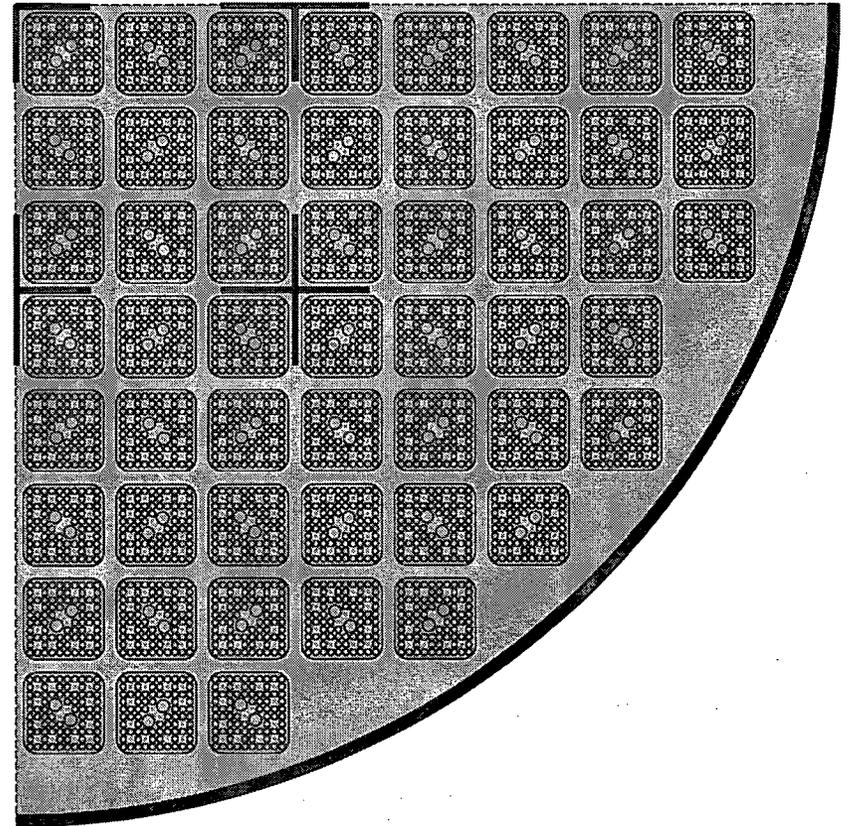
GNF is committed to developing and **maintaining** industry leading methods.

Advanced Methods Group created in 2005 to drive development of new methods.

Further Direction

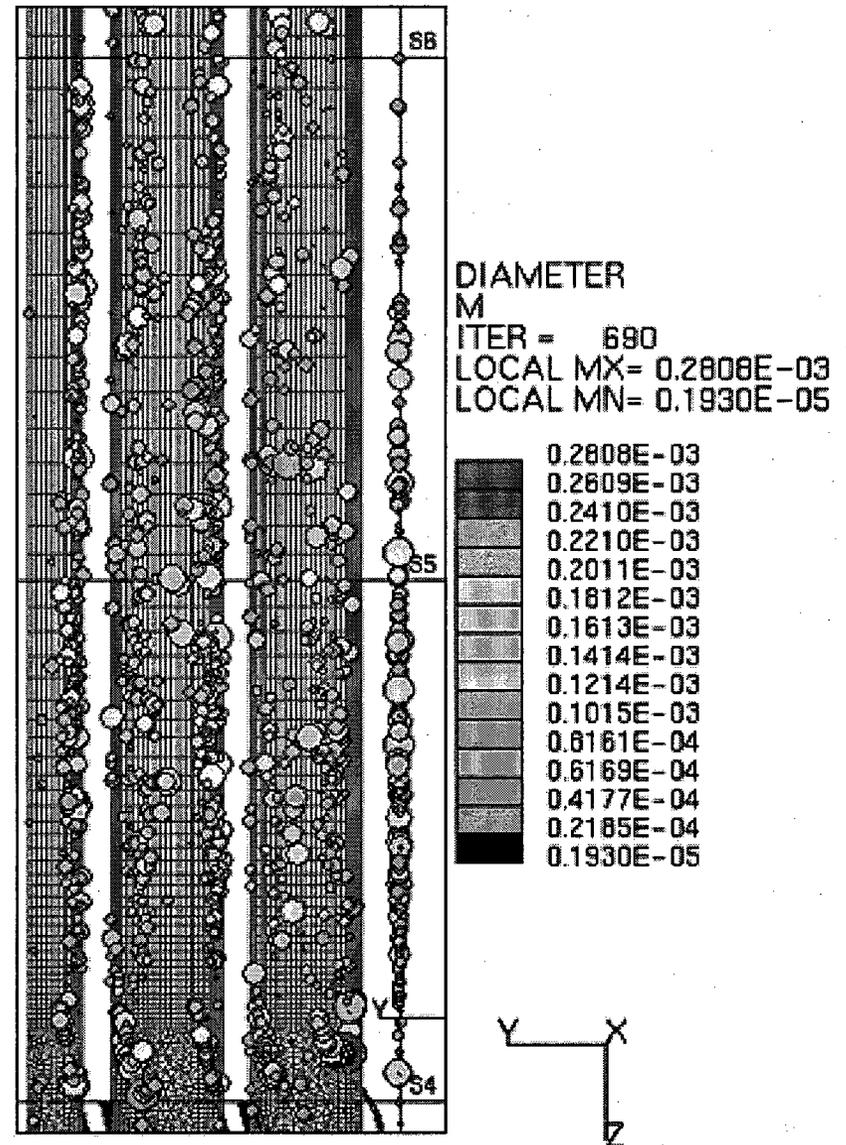
- Integration of AETNA02 models into TRACG06
- Full-core LANCER02 capability
- Advanced subchannel models
- Integration of COBRAG subchannel methods into AETNA02 and/or TRACG06
- 3-D LANCER

Large-scale parallel computation!



CFD Direction

- Single-phase CFD
- Turbulence Models
- Multi-phase CFD (adiabatic)
- Multi-phase CFD (steam/water)
- Experimental work to validate CFD models
- Working with GRC and Universities



GNF Technology Update Meeting

TRACG

Code and Application Status

May 1-2, 2007



Global Nuclear Fuel

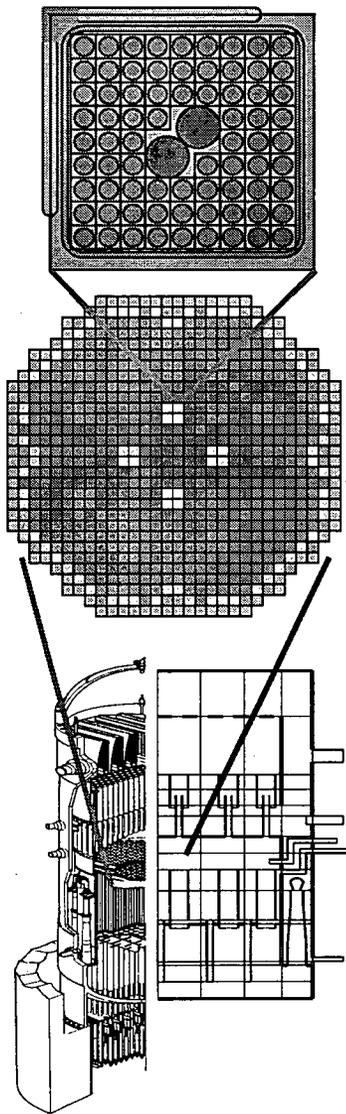
A Joint Venture of GE, Toshiba, & Hitachi

Preliminary Unverified Information

TRACG Benefits

- Improved fidelity:
 - Best Estimate models, 3D Effects, Mixed cores
- Transients:
 - 0.05 – 0.07 OLMCPR Improvement
- LOCA:
 - LHGR improvement for LOCA limited plants
- Stability:
 - Detect and suppress stability solutions
- ATWS:
 - Lower peak pressure and containment loads
- RIA/RDA:
 - Realistic assessment of margins
- ESBWR
 - Design and NRC certification

Relationship Between Codes



TGBLA06 -> LANCER02

2-D Lattice Physics

Nuclear Behavior of Fuel Rods Within Bundle

(LANCER replaces TGBLA)

PANAC11 -> AETNA02

3-D Core Simulation

Nuclear + Thermal-Hydraulic Behavior of Bundles in Core

(AETNA replaces PANAC)

TRACG04 -> TRACG06

Coupled Core and BOP Simulation

Best Estimate Analysis of Operational Transients

(Either TRACG can replace ODYN, TASC, SAFER, CORCL)

GSTRM -> PRIME

Fuel / Clad Thermal-Mechanical Analysis

Detailed fuel pellet, fission gas, and fuel-clad interactions

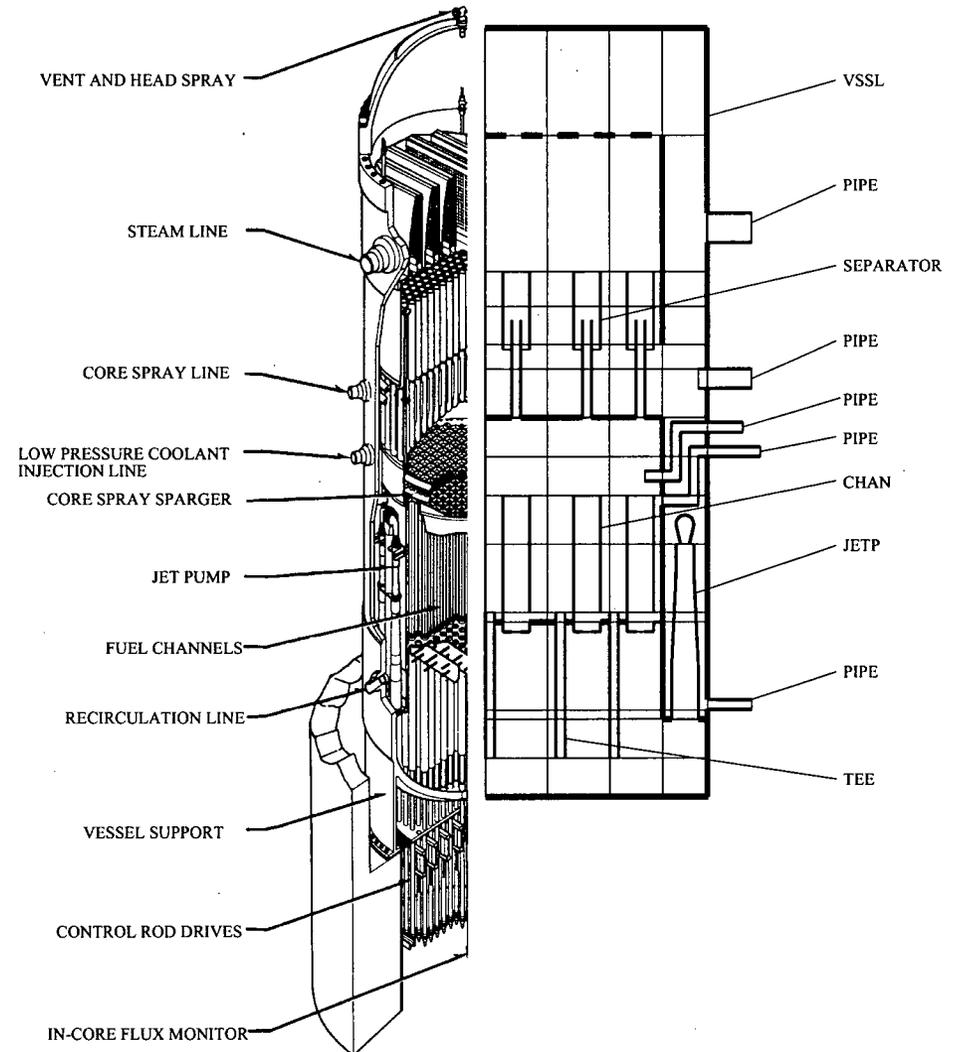
PRIME03 UO₂ thermal conductivity model is in TRACG04.

Model interfaces with TRACG via the fuel files.

TRACG

Realistic Code for BWR Transients

- Transients, LOCA, ATWS, Stability, RIA, RIPD
- Multi-dimensional thermal hydraulics
 - Two-fluid hydraulic model: Steam, liquid, boron and non-condensable gases
 - Best estimate basic models for shear and heat transfer
- Proven 3D nuclear kinetics consistent with GE core simulator PANACEA and AETNA
- Flexible modular structure with control system capability
 - Test facilities, BWR/2-6, ABWR and ESBWR
- BWR component models
 - Fuel elements, jet pumps, steam separators
- Extensive qualification
 - Simple separate effects tests
 - Scaled simulation
 - Full scale plant data



Extensive TRACG Qualification

Separate Effects Test

- Void Fraction: FRIGG OF64, Christensen, Wilson, Bartolomei, EBWR, Ontario Hydro, Toshiba, PSTF
- Heat Transfer: THTF, CSHT
- Counter Current Flow Limitation
- Critical flow: Marviken, PSTF, Edward
- Pressure drop: ATLAS
- Critical Power: ATLAS
- Natural circulation and T/H stability: FRIGG
- Kinetics: SPERT

Component Performance

- Jet pump: INEL 1/6 scale, Cooper, LaSalle
- Steam Separator: 2 and 3-stage full scale
- Upper plenum effects: SSTF
- Passive containment cooling: PANTHERS, PANDA, GIRAFFE

Included for ESBWR qualification

Integral System Effects test

- LOCA Simulation: TLTA, FIST, ROSA-IV, FIX, CSHT
- Multiple channel effects: SSTF
- ESBWR simulation: GIST, GIRAFFE, PANDA
- Containment: PSTF
- Loop oscillation tests: CRIEPI, SIRIUS
- Boron mixing: Vallecitos 1/6 scale tests

Plant Data

- Peach Bottom turbine trip test
- Hatch MSIV closure and pump trip tests
- Nine Mile Point pump upshift test
- Leibstadt loss of feedwater test
- Dodewaard
- LaSalle instability event
- Leibstadt stability test
- Forsmark stability test
- Cofrentes instability event
- Peach Bottom low decay ratio stability test
- Nine Mile Point Instability event
- Perry Instability event



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May 2007

Progression of TRACG Applications

TRACG02A (2000)

- PANAC10/TGBLA04 3D kinetics
- AOO, stability

TRACG04A,P (2006)

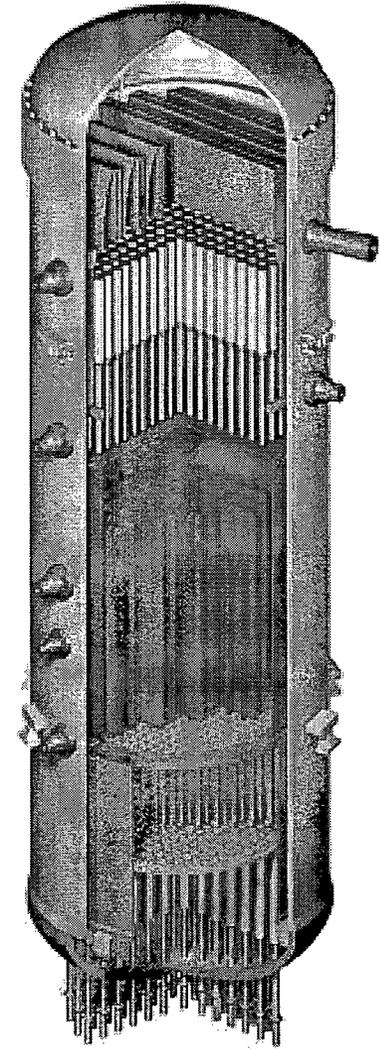
- PANAC11/TGBLA06 3D kinetics with improved boron model
- Integrate PRIME03 fuel thermal mechanical models
- BWR/2-6 and ABWR AOO, stability, LOCA and ATWS
- All ESBWR analyses

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TRACG04 Application to ESBWR

- All transient, stability, LOCA and ATWS calculations done with TRACG
 - Current design codes hardwired to the standard BWR geometry
- Additional models for ESBWR applications
 - ESBWR component simulation: Containment, Passive containment cooling system, Gravity driven ECC
- Additional qualification for ESBWR applications
 - Passive containment cooling systems: PANTHERS, PANDA, GIRAFFE
 - Gravity driven cooling systems: GIST, GIRAFFE, PANDA
 - Containment: GIST, GIRAFFE, PANDA, PSTF
 - CRIEPI startup oscillation tests
 - Dodewaard plant data



Planned Code Enhancements

- TRACG04A,P

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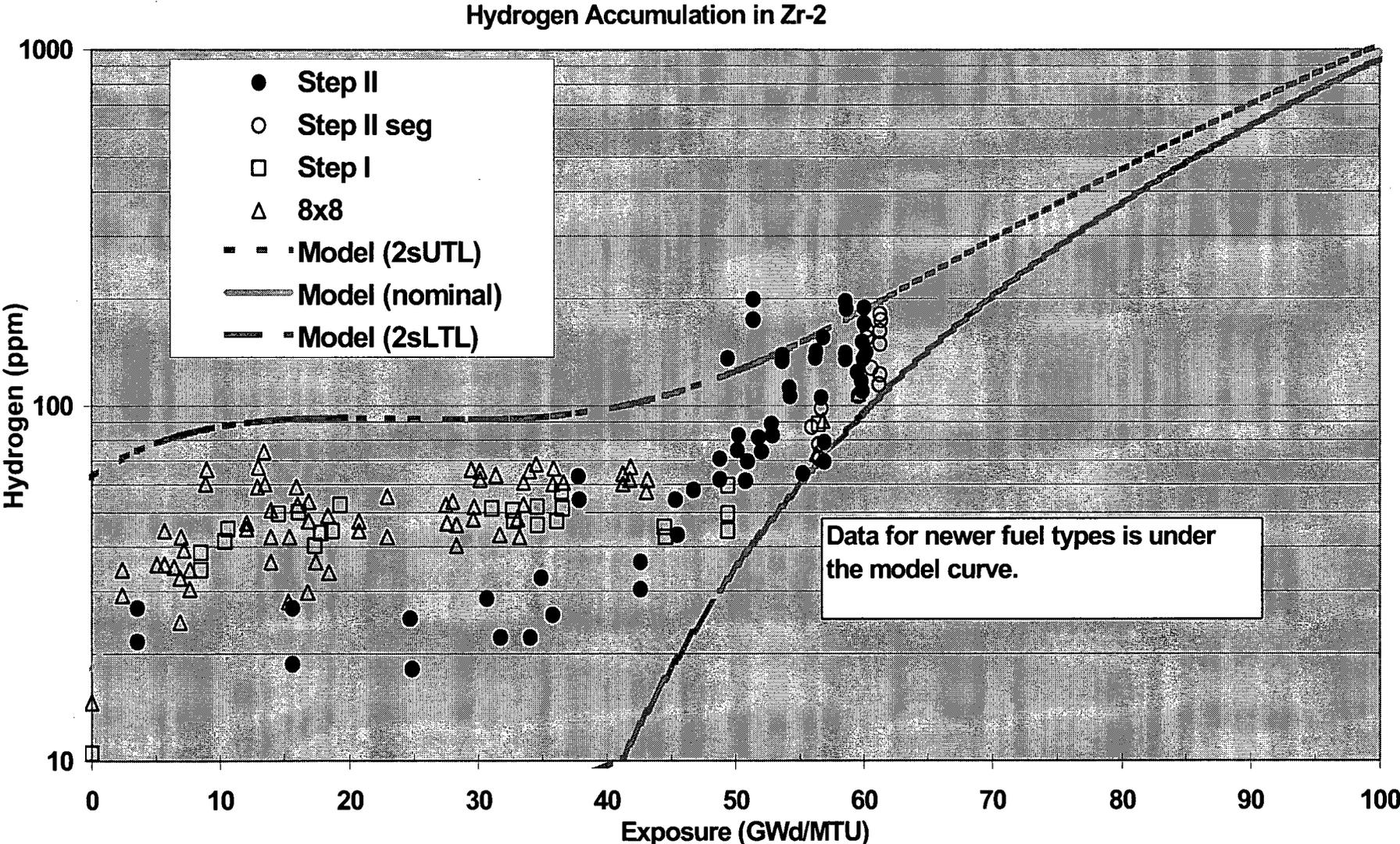
TRACG04 Application for RIA/RDA

- Additional models
 - Oxide and hydride correlations
 - Model for assumed fuel dispersal
 - Testing for pressure response from fuel dispersal
- Additional qualification
 - Additional SPERT cases for hot conditions
- Application elements

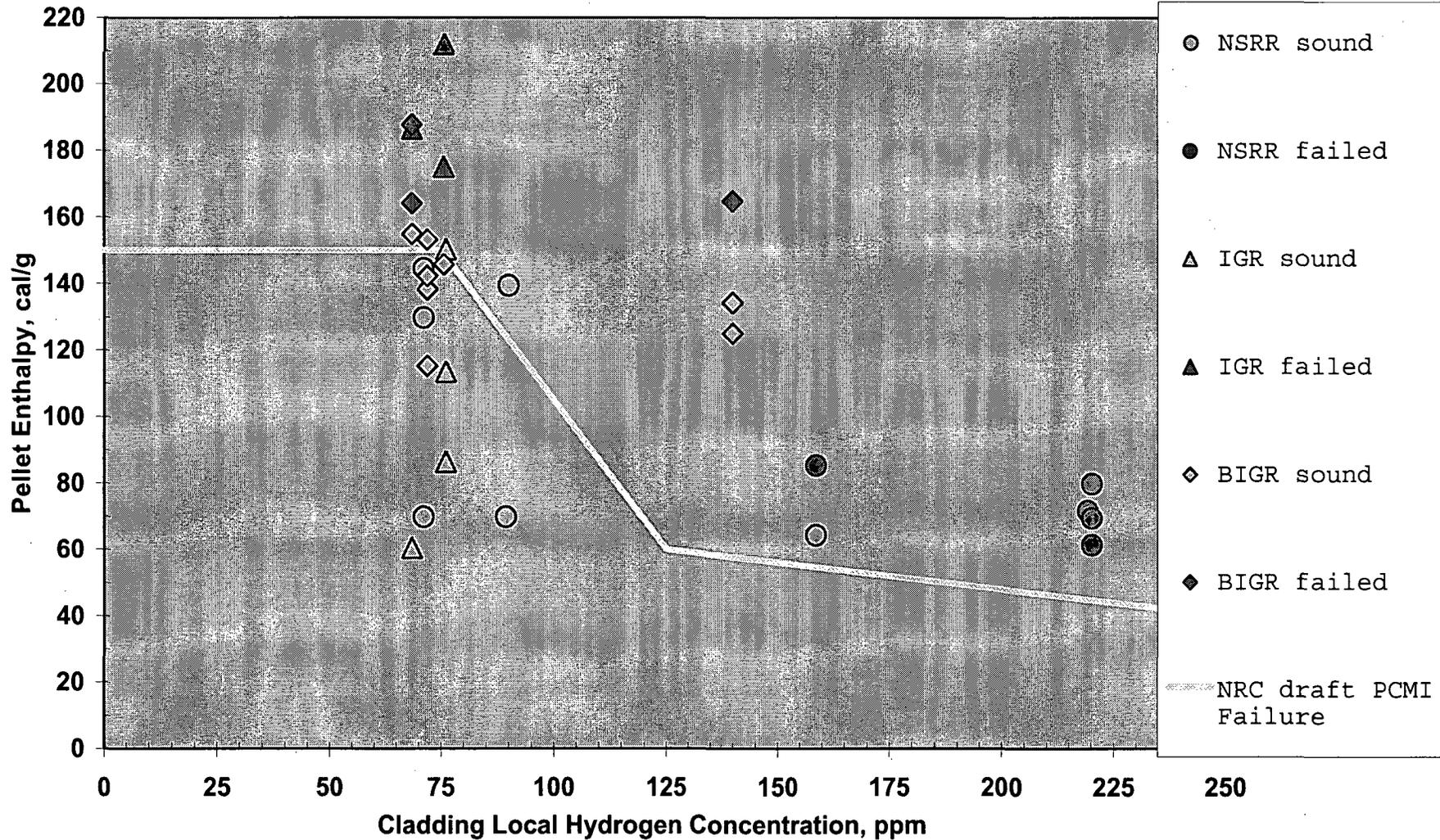
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Hydrogen Accumulation in BWR Zr-2 Cladding

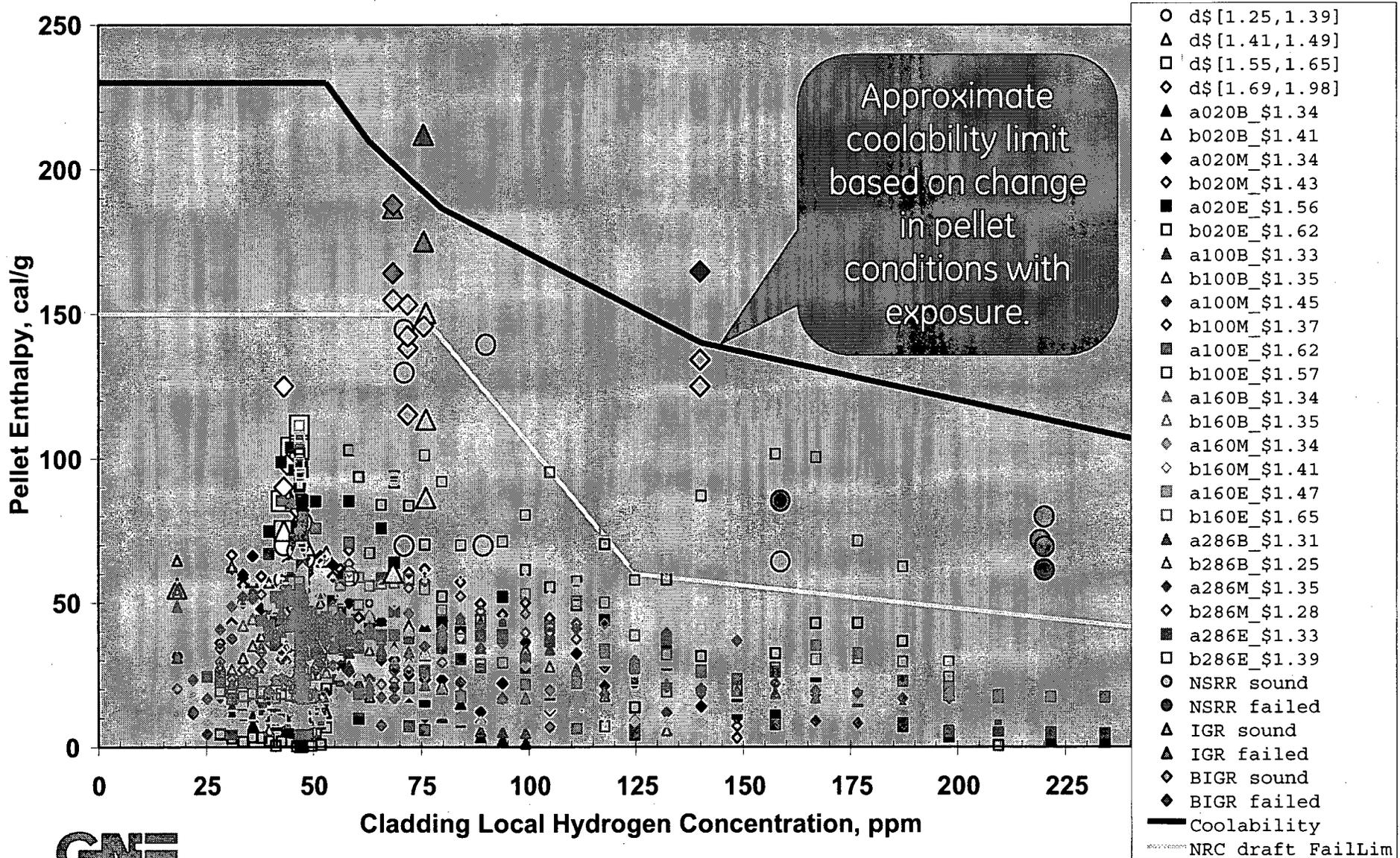


Failure Data Suggest Correlation to H2 Concentration



NRC draft PCMI Failure

BWR Best-Estimate Calculated CRDA Enthalpies & Interim USNRC Limits vs. Local H2 Concentration



Anticipated New Qualification

- Additional void fraction separate effects
 - Higher pressure range; high void fractions
- Brunswick scram on OPRM signal
- Leibstadt steam blowdown event
- Updated boron qualification cases for
 - Santa Barbara test
 - Vallecitos test
- Updated ABWR qualification cases

Anticipated TRACG LTRs

- TRACG Qualification LTR, Rev. 3, April 2007
- LOCA (June 2007)
- Generic Stability (April 2008)
- RIA/RDA (1Q 2008)
- ATWS (4Q 2008)

TRACG Benefits

- Improved fidelity:
 - Best Estimate models, 3D Effects, Mixed cores
- Transients:
 - 0.05 – 0.07 OLMCPR Improvement
- LOCA:
 - LHGR improvement for LOCA limited plants
- Stability:
 - Detect and suppress stability solutions
- ATWS:
 - Lower peak pressure and containment loads
- RIA/RDA:
 - Realistic assessment of margins
- ESBWR
 - Design and NRC certification

Stability Update

Presentation to NRC

Alan Chung



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Preliminary Unverified Information

Stability Update

- Brunswick 2 SLO OPRM Scram
- Plant-Specific DSS-CD Update
- Option I-D Plants for M+ Operation
- TRACG Stability LTR

Stability Update

Brunswick 2 SLO OPRM Scram

- Brunswick 2 had an OPRM SLO scram on Christmas last year
- The OPRM system tripped on the defense-in-depth Growth Rate Algorithm
- The GRA is designed for fast growing oscillations that have the characteristics of thermal-hydraulic instability
- The value of the OPRM cell relative signal (P/A) is compared at each hardware time step to a threshold setpoint, S_1 (1.10). If the relative signal exceeds S_1 , then the algorithm checks to determine if the relative signal decreases to a second setpoint, S_2 (0.92), within a time period typical of an instability oscillation
- After exceeding S_1 and decreasing below S_2 in the expected time window, a GRA trip is generated if a growth rate (1.30) is exceeded in the expected time window (T_2)

Stability Update

Brunswick 2 SLO OPRM Scram

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Stability Update

Brunswick 2 SLO OPRM Scram

- The OPRM system scrambled as designed
- The mode is core-wide in nature and does not appear to be driven by instability but rather by an external hydraulic excitation noise source.
- The ODYSY code predicted low core decay ratios, indicative of a non-THI condition
- The SLMCPR was protected during the power oscillation event
- The GRA is designed for fast growing oscillations that have the characteristics of thermal-hydraulic instability
- Additional detailed analysis using the TRACG model will be needed to study this power oscillation event

Stability Update

Plant-Specific DSS-CD Update for MELLLA+ Operation

- Generic DSS-CD LTR approved for EPU/MELLLA+
- Generic settings (10 counts and 1.03 amplitude setpoints) might not be adequate to prevent spurious scram during normal plant operation
- One simple change to fix the issue. Two-tiered power/flow-dependent setpoints proposed to fix the spurious scram concern
- The same generic methodology as approved in NEDC-33075 will be applied to setpoint generation for the two power/flow domains
- Browns Ferry Unit 1 will be the lead plant for this modification
- TRACG for DSS-CD LTR will be updated as part of this effort to include TRACG04

Stability Update

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Stability Update

Option I-D Plants for MELLLA+ Operation

- GE will submit Option I-D+ to MELLLA+ operation
- Will retain key elements of Option I-D such as flow-biased APRM flux scram line, dominance of core-wide mode
- APRM flow-biased flux scram line may carve out certain domain on the power/flow map (e.g., upper left corner) to ensure that the Option I-D solution elements are still applicable
- Same solution elements as the current Option I-D
 - Plant- and cycle-specific DIVOM
 - Digital Flow Control Trip Reference cards for multiple slope capability for the APRM flow-biased flux-scram lines
 - Exclusion and Buffer Regions
 - Stability online monitor
- GE putting together material for lead Option I-D plants (Vermont Yankee, DAEC)

Stability Update

Option I-D Plants for MELLLA+ Operation

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Stability Update

TRACG Stability LTR

- TRACG02 approved for the DIVOM application per NEDO-32465-A
- Approved SERs for separate ESBWR and DSS-CD applications
- New TRACG Stability LTR will provide the documentation to support the DIVOM application
- Will cover TRACG04 also
- Expected 1Q08

SLMCPR Methodology

MIP Criterion (MCPR Importance Parameter)

MIP Criterion Review Requirement

NRC Letter

Acceptance for referencing of licensing topical reports NEDC-32601P, Methodology and Uncertainties for Safety Limit MCPR Evaluations; NEDC-32694P, Power Distribution Uncertainties for Safety Limit MCPR Evaluation; ...

NRC SER ... actions should be taken as follows:

(3) In view of the importance of MIP criterion and its potential sensitivity to changes in fuel bundle designs, core loading and operating strategies, the MIP criterion should be reviewed periodically as part of the procedural review process to insure that the specified value recommended in NEDC-32601p is applicable to future designs and operating strategies.

Original MIP Criterion Basis

- Indirect technical argument based on CPR
 - Due to no direct measure of SLMCPR operating margin
 - Cores not on limits have inherent SLMCPR operating margin
 - Develop MIP criterion to determine SLMCPR conservatism
 - Result is an indirect method showing that the SLMCPR methodology is sufficiently conservative to SLMPCR operating margin

NEDC-32601P

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NEDC-32601P

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NEDC-32601P

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New MIP Criterion Basis

- Direct technical argument based on NRSBT
 - Due to new feature that allows for direct measure of SLMCPR operating margin
 - Using this new feature results in a direct method showing that the SLMCPR

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Typical SLMCPR Operating Margin (unverified)

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A00+.04 Operating Margin (unverified)

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What Next?

- LTR late 2007 / Approval late 2008

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Method Validation Programs

May 1, 2007

J.S. Bowman, *et. al.*



imagination at work

Preliminary Unverified Information

Agenda

Gamma scan campaigns

Void fraction comparisons



Gamma Scan Data

Gamma scans provide confirmation of power predictions

2002 Cofrentes gamma scan data

- GE12 10x10 fuel
- GE11 9x9 fuel
- In pool 4 bundle corner Ba140 at multiple axes & elevation
- Stretch power uprate with MELLLA

Cofrentes Cycle 13 (2002)

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Power & Flow History for Cofrentes

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May 1, 2007

A GE12 (10x10) Comparison

(Excerpt from Report)

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Summary Predicted vs. Measured

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Error Versus Bundle Power

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Error versus Axial Position

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Results

Measured vs. predicted power agreement

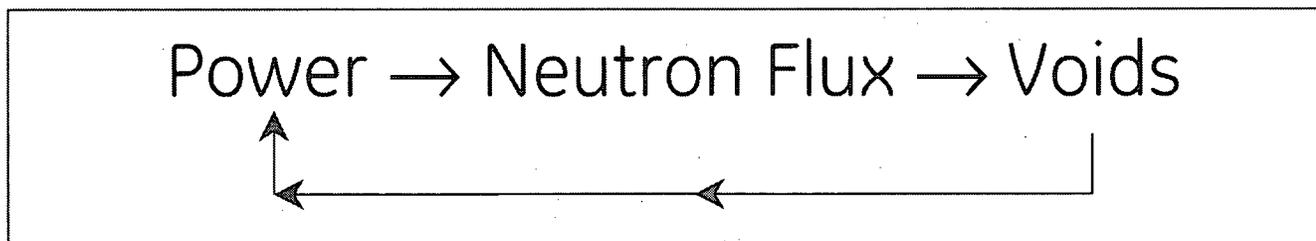
- 10x10 fuel – well predicted
- Power distribution uncertainties confirmed
- Nodal power agreement excellent
- Data does not indicate any trends with void fraction or bundle power level

Conclusions

Cofrentes Bundle Gamma Scan (2002)

Good comparison between measured and predicted power

- Approved uncertainty confirmed
- Indicates good void prediction
 - Validates Findlay-Dix correlation



System Deployed at Fitzpatrick

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imagination at work

Preliminary Unverified Information

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Rod Power Validation

NEDC-32601P-A, Section 3.1.4

Total rod power is measured

Compare total uncertainty to

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Confirms analytically derived σ is sufficient



Last Gamma Scan at Duane Arnold in 1984

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FitzPatrick Gamma Scan Statistics JLM420

Preliminary & Unverified

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FitzPatrick Gamma Scan Statistics JLM420

Preliminary & Unverified

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Rod Gamma Scan Preliminary Conclusions

Fitzpatrick Rod Gamma Scan (2006)

10x10 fuel, GE14 lead fuel → well predicted
Measurement statistics improved over DA'88
Prediction on modern methods/fuel better

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Post-processing and verification in 2007

Upcoming Gamma Scan Campaigns

More rod scans

Fission gas

Relative burnup

Void Fraction Comparisons

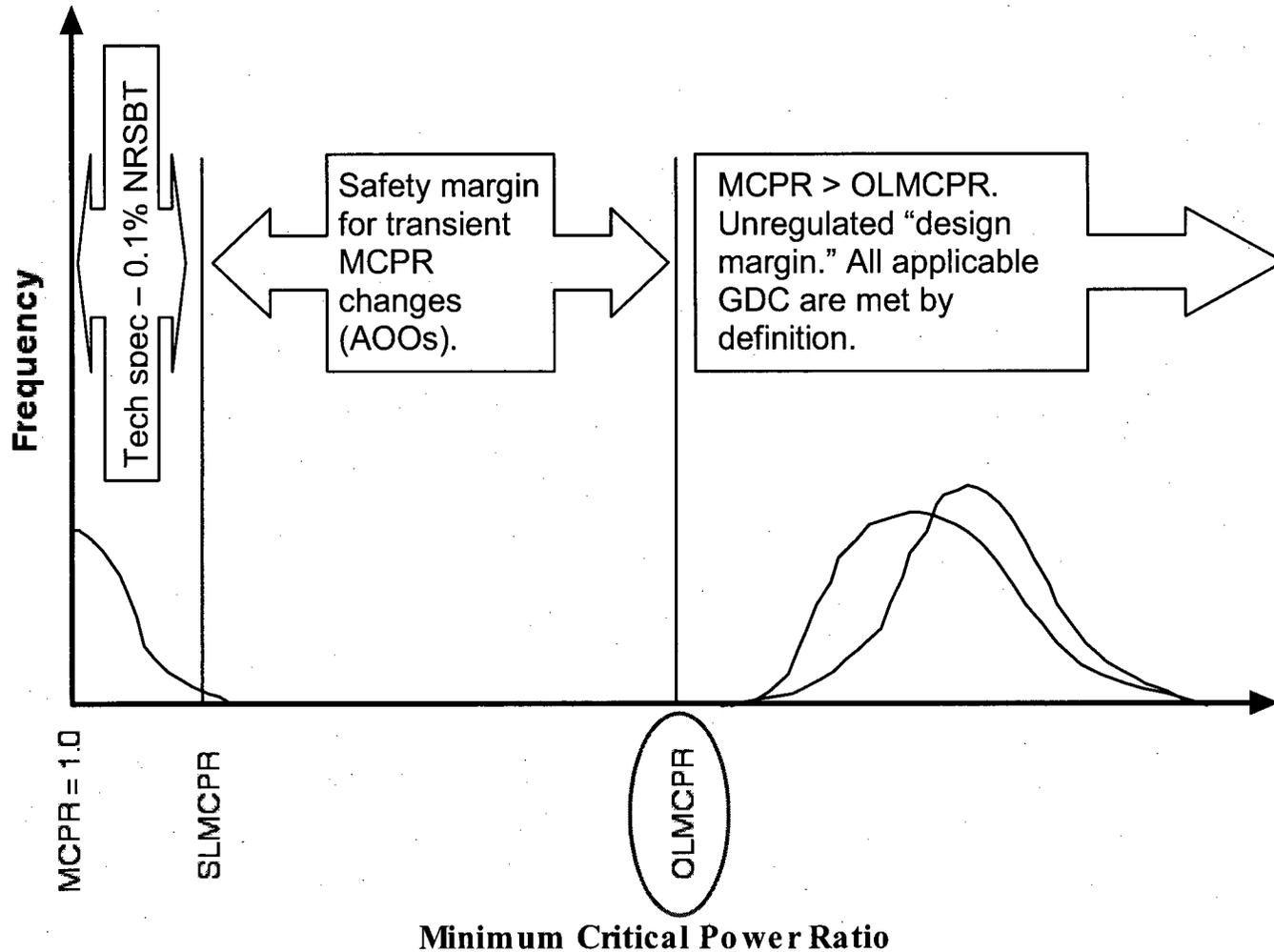
Establish the range of interest

10x10 ΔP Data

- Uncertainty analysis for α

How High Does the Void Fraction Get in the Reactor?

Margins Limit Void Fractions



Sample of BWR Fleet OLMCPRs Unverified

OLMCPR sets the max bundle power

Survey of 2005 data

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Maximum Expected Values

Full-Scale Tests [[

ATLAS and Stern Labs

- Critical power
- Pressure drop

GNF2 and GE14 tested

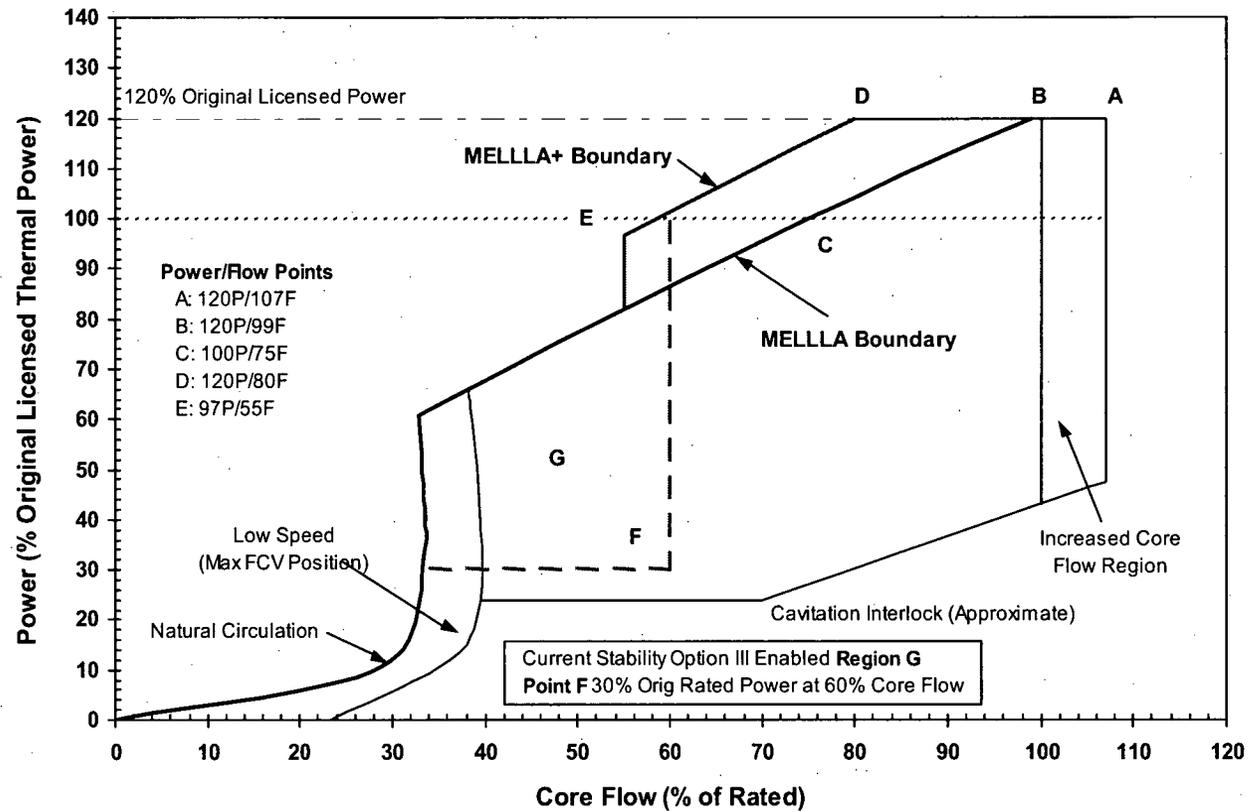
Range of Tests

Power range: 0 to 8 MWt

- Max approaches critical power

Flow range: 0.1 to 1.5 Mlbm/hr-ft²

- Natural circulation to ICF region



Broad test range to cover the BWR fleet

GE14 and GNF2

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GNF2

GE14

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Two geometries for 10x10



imagination at work

Preliminary Unverified Information

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10x10 ΔP Test Data Summary

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GE14 ΔP

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imagination at work

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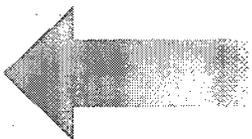
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GNF2 ΔP

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Method B Pressure Drop

ΔP friction

ΔP elevation  [[

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ΔP local losses

ΔP acceleration

+ ΔP expansion/contraction

ΔP total

Comparison to Findlay-Dix

Preliminary & Unverified

[[

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ΔP Residuals Correlate to Mass Flux

Preliminary & Unverified

[[

ΔP Residuals Do Not Correlate to α

Preliminary & Unverified

[[

Confirmatory Low Flow Data

Comparison to Findlay-Dix

Conclusions

- GE14 & GNF2 tests – geometry represents current fuel designs

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Next Steps

COBRAG Licensing Topical Report

- Critical power
- Subchannel voids

GEXL++

Improved GEXL Correlation
GNF Technology Update Meeting
May 1-2, 2007



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Preliminary Unverified Information

Background

- GEXL introduced with GETAB
 - GETAB, NEDO-10958A, 1977
 - $X_c = f(L_B, D_Q, G, P, R)$
 - GEXL01 for 7X7 and 8X8 fuel
- GEXL+ introduced with Amendment 15 to GESTAR II
 - Amendment 15 to GESTAR II, 1986
 - $X_c = f(L_B, D_Q, G, P, R, L_A)$
 - GEXL02 and GEXL05 for 8X8 fuel
 - GEXL07 and GEXL09 for 9X9 fuel
 - GEXL10, GEXL14 and GEXL17 for 10X10 fuel

GESTAR II Requirement GEXL form

$$X_C = \sum_{I=1}^{18} A(I) \cdot V(I)$$

1.1.7 Critical Power Correlation

- A. The currently approved critical power correlations will be confirmed or a new correlation will be established when there is a change in wetted parameters of the flow geometry; this specifically includes fuel and water rod diameter, channel sizing and spacer design. [[
- B. A new correlation may be established if significant new data exists for a fuel design(s).
- C. The criteria for establishing the new correlation are as follows.
- i. The new correlation shall be based on full-scale prototypical test assemblies.
 - ii. Tests shall be performed on assemblies with typical rod-to-rod peaking factors.
 - iii. The functional form of the currently approved correlations shall be maintained.
 - iv. Correlation fit to data shall be best fit.
 - v. One or more additional assemblies will be tested to verify correlation accuracy (i.e., test data not used to determine the new correlation coefficients).
 - vi. Coefficients in the correlation shall be determined as described in References 1-5 or 1-6.
 - vii. The uncertainty of the resulting correlation shall be determined by:

$$\sigma^2 = \frac{1}{N-1} \sum_{i=1}^N (\mu - ECPR_i)^2$$

where:

σ = standard deviation.

$$\mu = \frac{1}{N} \sum_{i=1}^N ECPR_i$$

N = Total number of data in both the data set used to determine the coefficients and the set used for verification.

$ECPR$ = Calculated bundle critical power divided by experimentally determined bundle critical power.

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Fuel and GEXL Development

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- **7X7 Fuel**
 - Egg Crate Spacers
- **8X8 Fuel**
 - Egg Crate Spacers
 - Water rods
- **8X8 Fuel**
 - Ferrule Spacers
 - Large central water rod
- **9X9 Fuel**
 - Ferrule Spacers
 - Large central water rods
 - Part length rods

[[- {3}]]

- **10X10 Fuel**
 - Ferrule and X-750 spacers with flow wings
 - Large central water rods
 - Part length rods

[[- {3}]]

{3}]]

GEXL++

[[

{3}]]

COBRAG Qualification

Existing qualification

[[

[[

{3}]]

{3}]]

COBRAG Qualification

Additional qualification (unverified)

[[

{3}]

Schedule - Tentative

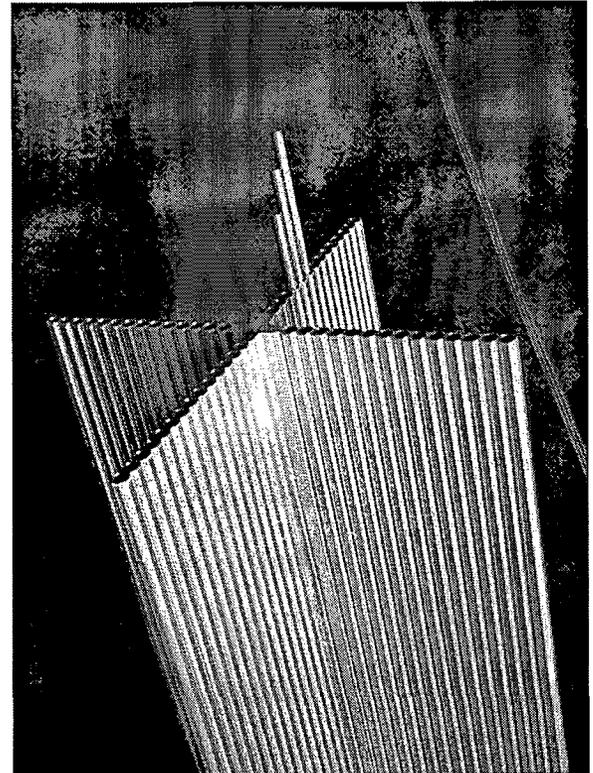
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{3}]]

Marathon-5S Control Rod Blade

GNF Technology Update Meeting

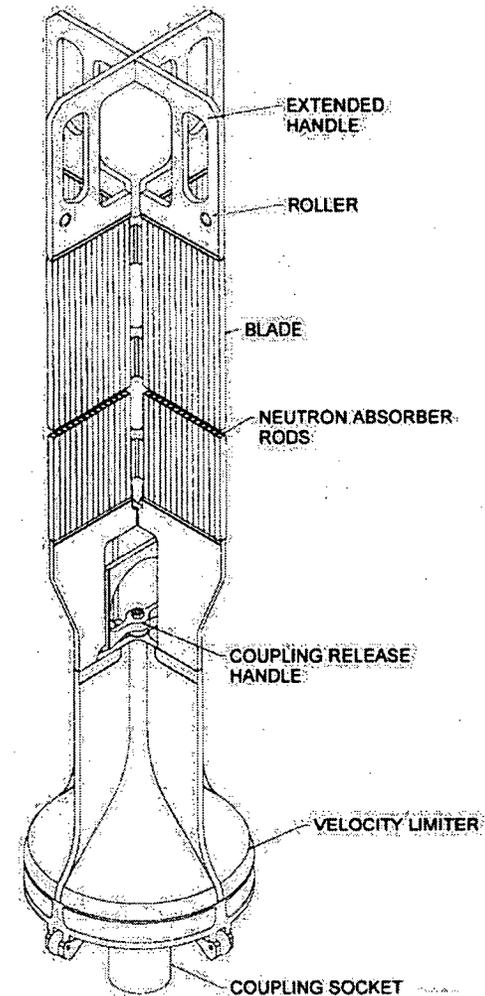
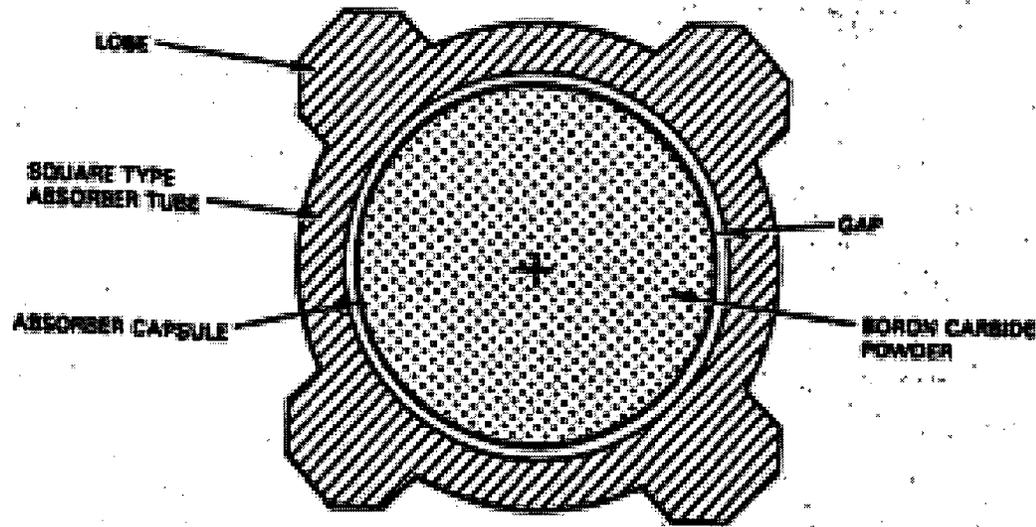
May 1-2, 2007



imagination at work

Marathon CRB Description

B4C powder capsule/hafnium rod within a 'square' absorber tube.



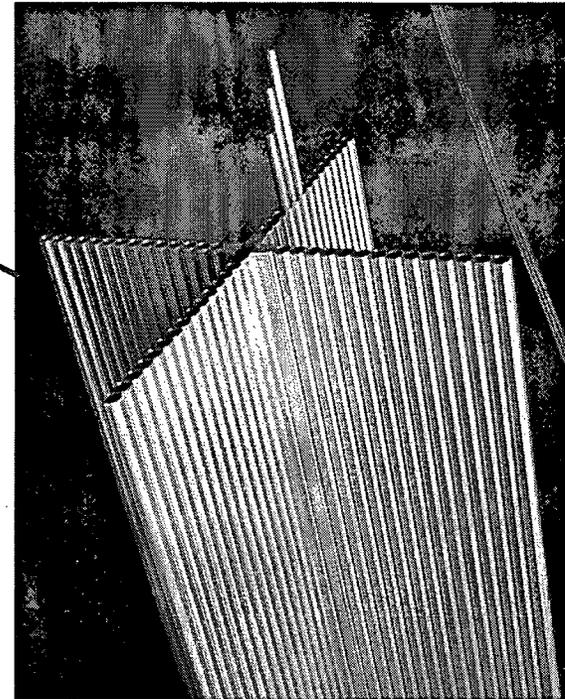
Marathon-5S CRB Description

- Simplified Absorber Tube Geometry
- All B₄C Capsule Design (no hafnium)
- Thicker Wall Capsule Body Tube
- Full-Length Tie Rod
- Roller-less Handle

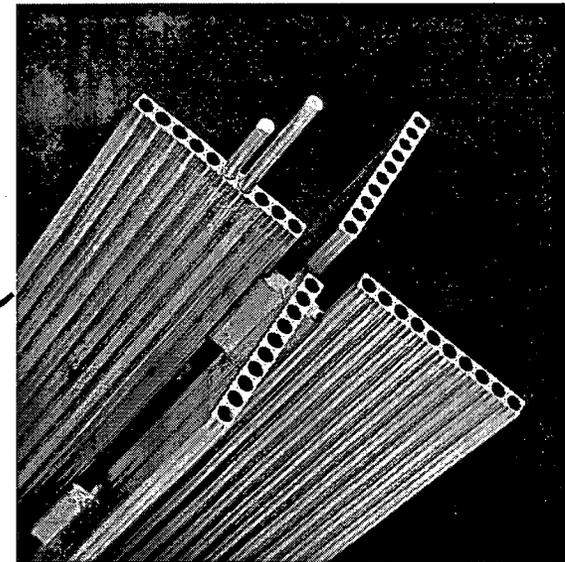
Marathon-5S

M-5S

- Comparison to Marathon-7S
- Same GE proprietary 304S crack-resistant stainless steel
- More conservative design criteria
 - [[



{3}]] M-7S



Marathon-5S Control Rod

- Licensing Topical Report, NEDE-33284P, currently being reviewed by NRC.
- A domestic BWR/6 plans to install 5 Marathon-5S control rods fall 2007.
- Seismic scram testing successfully completed at the end of 2006.

Marathon-5S Control Rod Nuclear Design Summary

- Matched worth design – initial cold and hot reactivity worths within $\pm 5\%$ of the original equipment.
- Nuclear end-of-life defined to be the $\frac{1}{4}$ segment depletion at which the cold reactivity worth is equivalent to a 10% reduction in the original equipment's cold reactivity worth.
- The nuclear lifetime is evaluated to be limiting over the mechanical lifetime for all cases.

Marathon-5S Control Rod Mechanical Design Summary

- The control rod is conservatively evaluated for worst case scram, stuck rod compression, handling loads, and loads due to absorber burn-up.
- Seismic and fuel channel bow induced bending, as well as fatigue are also analyzed.
- Maximum stresses and strains for the material, structure and welded connections are found to be acceptable.

Marathon-5S Control Rod – Capsule Swelling

- [[

{3}]]

Marathon Design	Licensing Topical Report(s)	Minimum Diametral Gap Between Capsule and Absorber Tube at Beginning-of-Life (inches)	Local Depletion at Capsule Contact with Absorber Tube Inside Diameter (Nominal)
Marathon - D/S Lattice	NEDE-31758P-A	[[{3}]]
Marathon - C Lattice	NEDE-31758P-A		
Marathon-5S - D/S Lattice	NEDE-33284P		
Marathon-5S - C Lattice	NEDE-33284P		

- [[

{3}]]



imagination at work

DRAFT

PRIME03 Status & PRIME Transient Models Development

Nayem Jahingir & Steve Liu

NRC/GNF Technology Update Meeting

May 1 – 2, 2007

GNF, Wilmington, NC



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Preliminary Unverified Information

PRIME03 Status

- A state-of-the-art computer program for fuel rod Thermal/Mechanical licensing and behavior analysis
- PRIME03 LTRs
 - PRIME Technical Bases (NEDC-33256P)
 - PRIME Qualification (NEDC-33257P)
 - PRIME Application (NEDC-33258P)
- LTRs Submitted to NRC on 02/07
- NRC acceptance review is complete
- SE anticipated ~ 08/08

PRIME03 Thermal/Mechanical Model

Model Summary

- > Developed to replace GESTR-Mechanical (and GESTR-LOCA)
- > To address high exposure mechanisms
 - Porous pellet rim
- > To reflect high exposure materials properties measurements
 - Pellet thermal conductivity (UO_2 / $(\text{U,Gd})\text{O}_2$ / Additive)
 - Pellet grain growth
 - Cladding irradiation creep and growth
- > To include revised performance models exposure dependencies
 - Pellet relocation
 - Pellet radial power distribution
 - FGR
 - Fuel-cladding axial slip

PRIME03 Thermal/Mechanical Model

Model Summary (cont)

Qualification based upon expanded high exposure data bases

- > Centerline temperature
- > Fission gas release and rod internal pressure
- > Cladding strain

Data bases include field data from GE11/13 and GE12 LUAs in commercial reactors

- > FGR field data to [[{3}]] Peak Pellet Exposure
- > Exposure dependent COINS measurements to [[{3}]]
 - Direct confirmation of cladding creep model
 - Indirect confirmation of integral PRIME prediction of pellet expansion (due to thermal expansion, densification, swelling and relocation)

PRIME FGR Model Qualification

[[

{3}]]

PRIME Transient Models Developments

- Current approach

- Separate codes for steady state and transient analysis
- Substantial effort to interpolate and transfer variables in between codes
- Additional code maintenance

- PRIME Transient

- Seamless data transfer from steady state to transient events
- Compatible numerical structures
- Qualified for fast transients like RIA

Transient Solution Approach

[[

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{3}]]

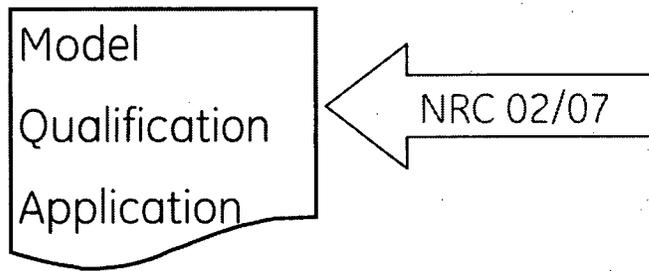
PRIME Transient Application

- Intended to replace current methods for licensing evaluations for transient events.
- PRIME transient Application
 - Licensing Calculation
 - No fuel melting
 - 1% plastic strain
 - RIA type of transient
 - Final RIA criteria development

PRIME Transient Licensing Approach

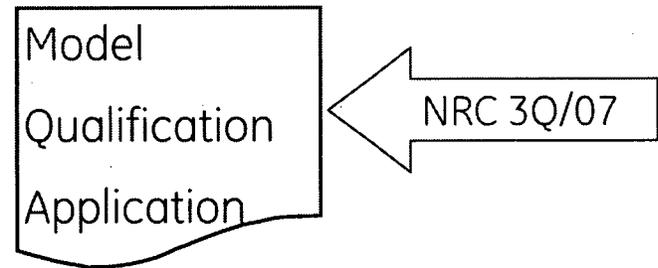


PRIME Steady State



SE expected ~ 08/08

PRIME Transient



SE expected ~ 1Q/09

PRIME SS & Tran Code

Summary

- PRIME03 Steady State Code
 - LTR Submitted 02/07
 - Support [[{3}]]
 - Replace GESTR-Mechanical and GESTR-LOCA
 - SE expected ~08/08
- PRIME transient Development
 - Level II DR is ongoing under GE/GNF QA procedure
 - No change in current steady state methods
 - LTR Submission ~ 3Q/07
- Maintain currently approved "GE/GNF Procedure for Fuel Property and Model Revision" (MFN-170-84)

Channel-Control Blade Interference Update

Presentation to NRC
May 1-2, 2007

Paul Cantonwine
Lead Engineer – Materials Technology & Fuel Reliability
Fuel Engineering



Global Nuclear Fuel

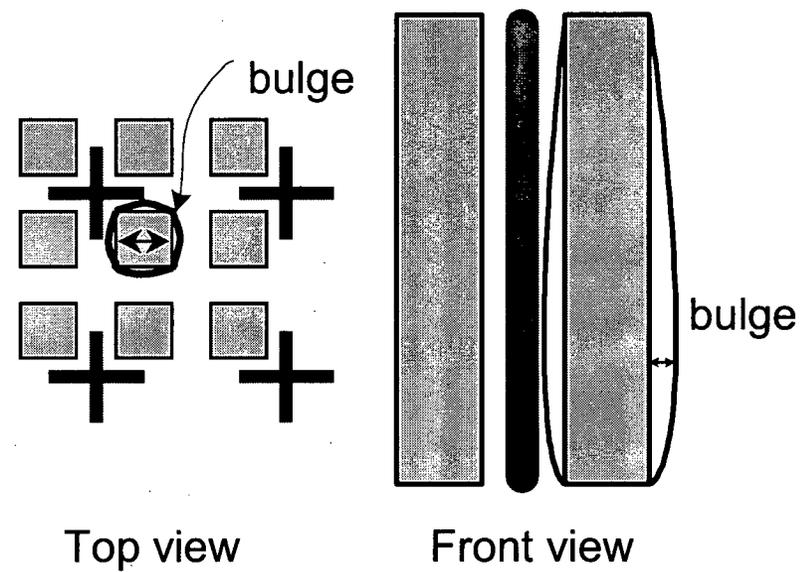
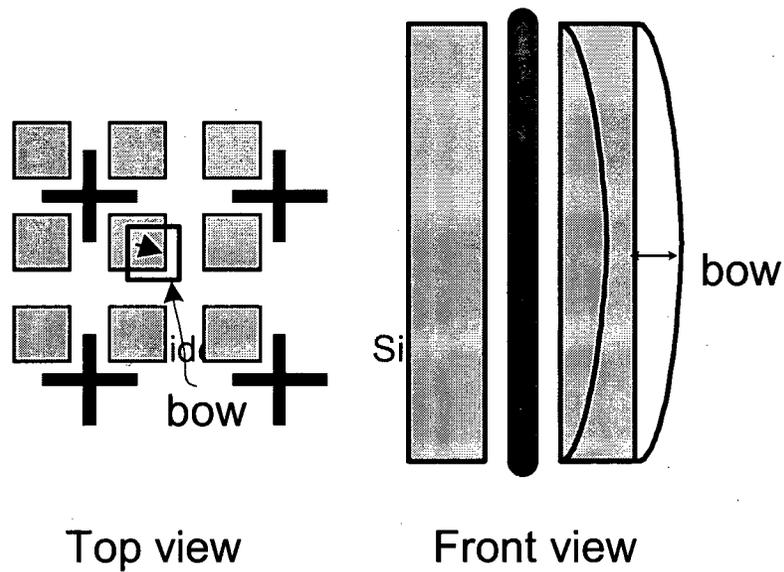
A Joint Venture of GE, Toshiba, & Hitachi

Preliminary Unverified Information

Outline

- Background
 - Channel bow and bulge
 - Observations of interference
 - GNF response to observations
- Mitigation Strategy
 - Cell Friction Methodology
 - Improve Channel Materials
 - Lead Use Channel Plans
- Summary

Deformations and Definition of Terms



Fluence Gradient Induced Bow

[[

{3}]]

Shadow Corrosion-Induced Channel Bow

[[

{3}]]

Impact of Channel-Control Blade Interference

- Slow Settle
 - $10 \text{ s} < \text{Settle Time} < 30 \text{ s}$
- No Settle
 - $\text{Settle Time} > 30 \text{ s}$
- Slow Scram Time
 - Scram time to 90% Insertion $< 7.0 \text{ sec}$
- Failure to Scram
 - Scram time to 90% Insertion $> 7.0 \text{ sec}$

Background - Observations

- BWR/6 S-Lattice Plants
 - Observed no-settle and slow-to-settle cells in 2000-2001
- BWR/4-5 C-lattice Plants
 - Observed no-settle and slow-to-settle cells in 2003
- BWR/2-4 D-Lattice Plants
 - One slow-settle observation in 2007

Background – GNF Response to Observations

Characterization program initiated

- Poolside channel bow, bulge, length measurements
 - Channel coupons retrieved for hotcell examination Safety Information
- 10 CFR Part 21 Communications
 - SC03-04: Notification of Interference Observations - March 3, 2003
 - New bow mechanism identified (shadow-corrosion induced bow)
 - SC03-08 Rev 1: Interim Surveillance Program – April 30, 2003
 - Introduced use of Effective Control Blade Exposure (ECBE; units inch-days) as a correlating parameter for shadow bow
 - SC05-06: Updated Surveillance Program – July 14, 2005
 - Introduced Cell Friction Methodology; a more quantitative tool that could be used to prevent interference in design
 - SC06-12: Updated Surveillance Program – September 26, 2006
 - Clarification of procedure for stall flow measurements and full stroke insertion testing
 - Updating Cell Friction Methodology to include shadow effect in D-Lattice Plants (2007)

Mitigation Strategy

[[

{3}]]

Near Term: Mitigate via Monitoring and Design

[[

{3}]]

Core Map of Cell Friction Metric Values

[[

{3}]]

Long Term: Mitigate via New Materials

[[

{3}]]

Status of In-core Demonstration Programs

[[

New Material LTA Program: Summary

[[

{3}]]

[[

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Shadow Corrosion Effect Assessment

[[

{3}]]

Summary

[[

{3}]]

GNF Technology Update Meeting

Defender Lower Tie Plate

[[

May 1-2, 2007



Global Nuclear Fuel

A Joint Venture of GE, Toshiba, & Hitachi

{3}]]

Preliminary Unverified Information

Agenda

- Defending Against Debris ... Customer Impact
- Debris Filter Evolution ... Three Generations !
- Defender Description
- Significant Testing
- Defender Development
- Defender Product Deployment

Customer Impact (Debris)

[[

{3}]]

Debris Filter Evolution ... Three Generations !

[[

Defender Description

- The Defender Bundle
- Capturing The Filter
- The Defender Filter

Defender Bundle – Assembly Description

[[

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Defender – Capturing the Filter

[[

{3}]

Defender Filter

[[

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Defender Testing

[[

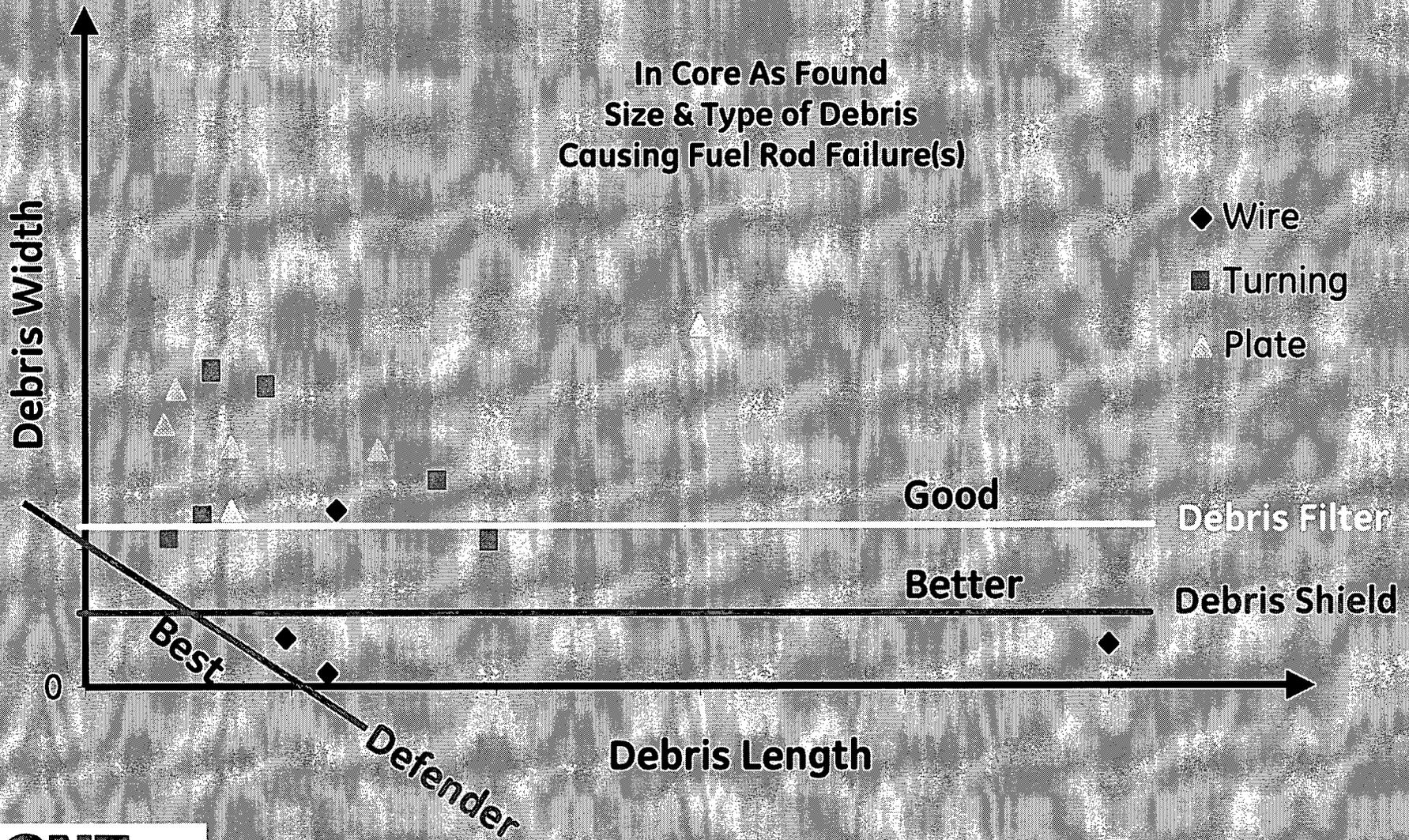
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Debris Testing – Selecting the Best Filter

[[

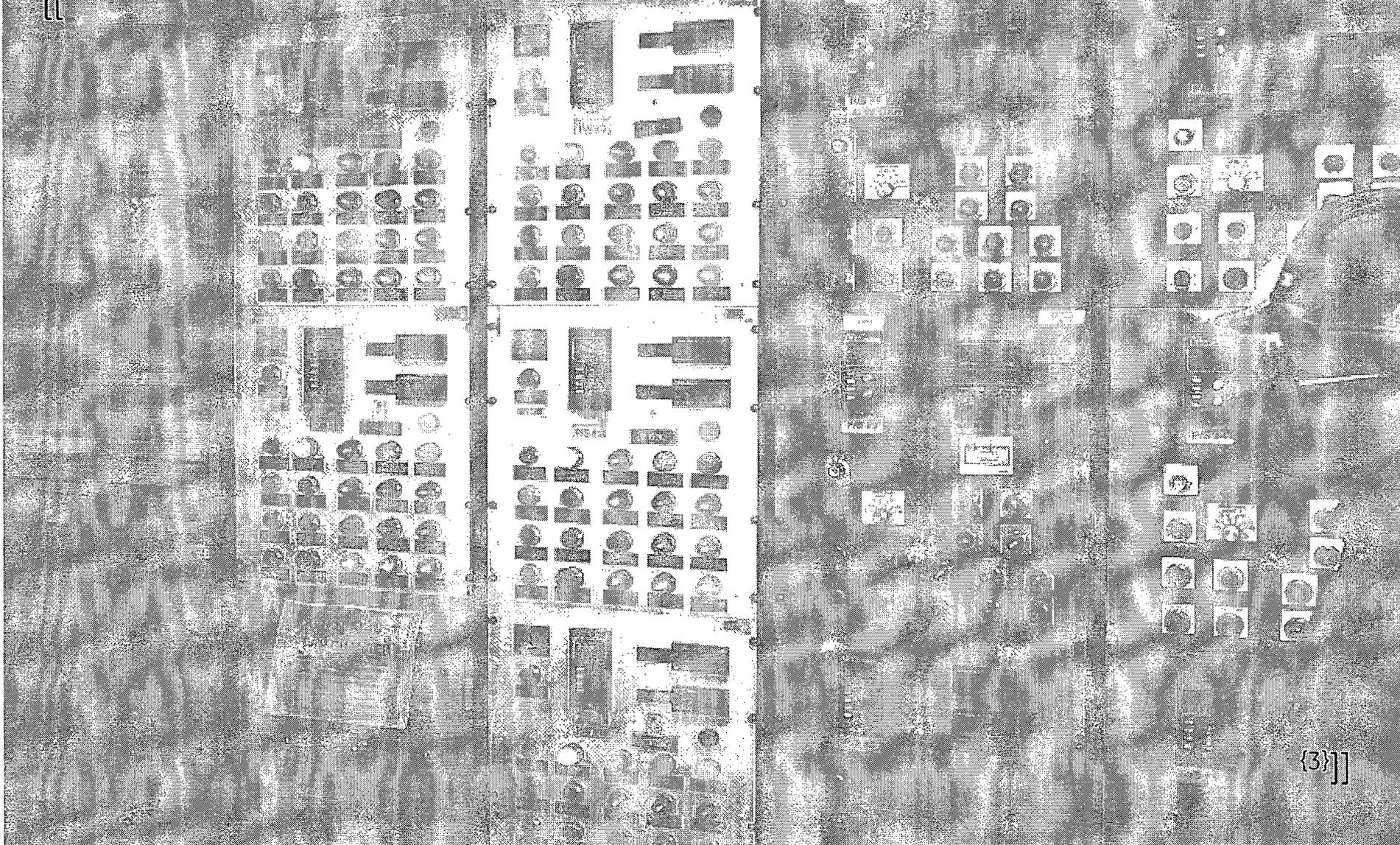
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Debris Testing – Selecting the Best Filter



Single Phase Testing – Tuning Defender

[[



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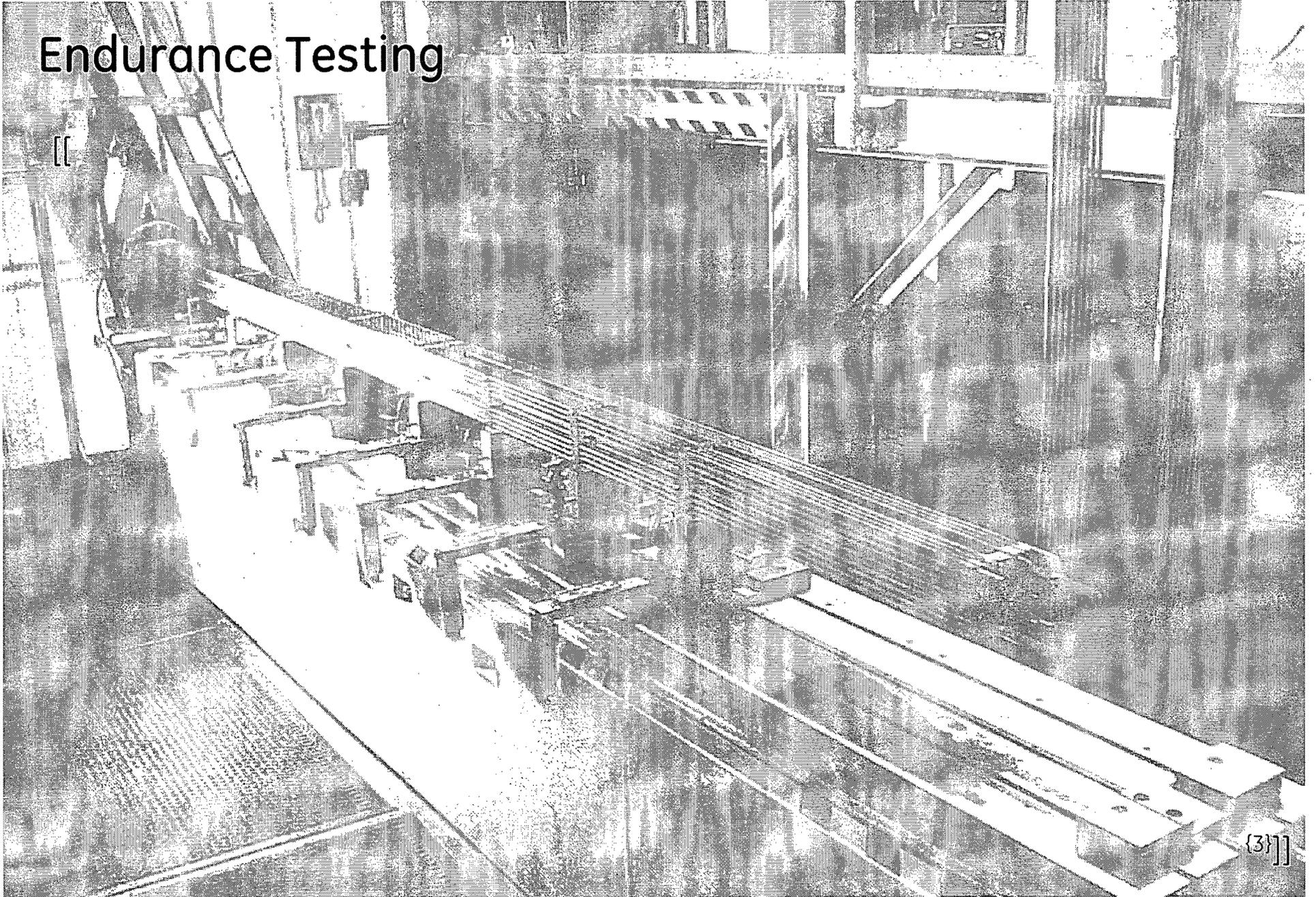
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Preliminary Unverified Information

12 /
GNF Title or job number /
4/5/2007

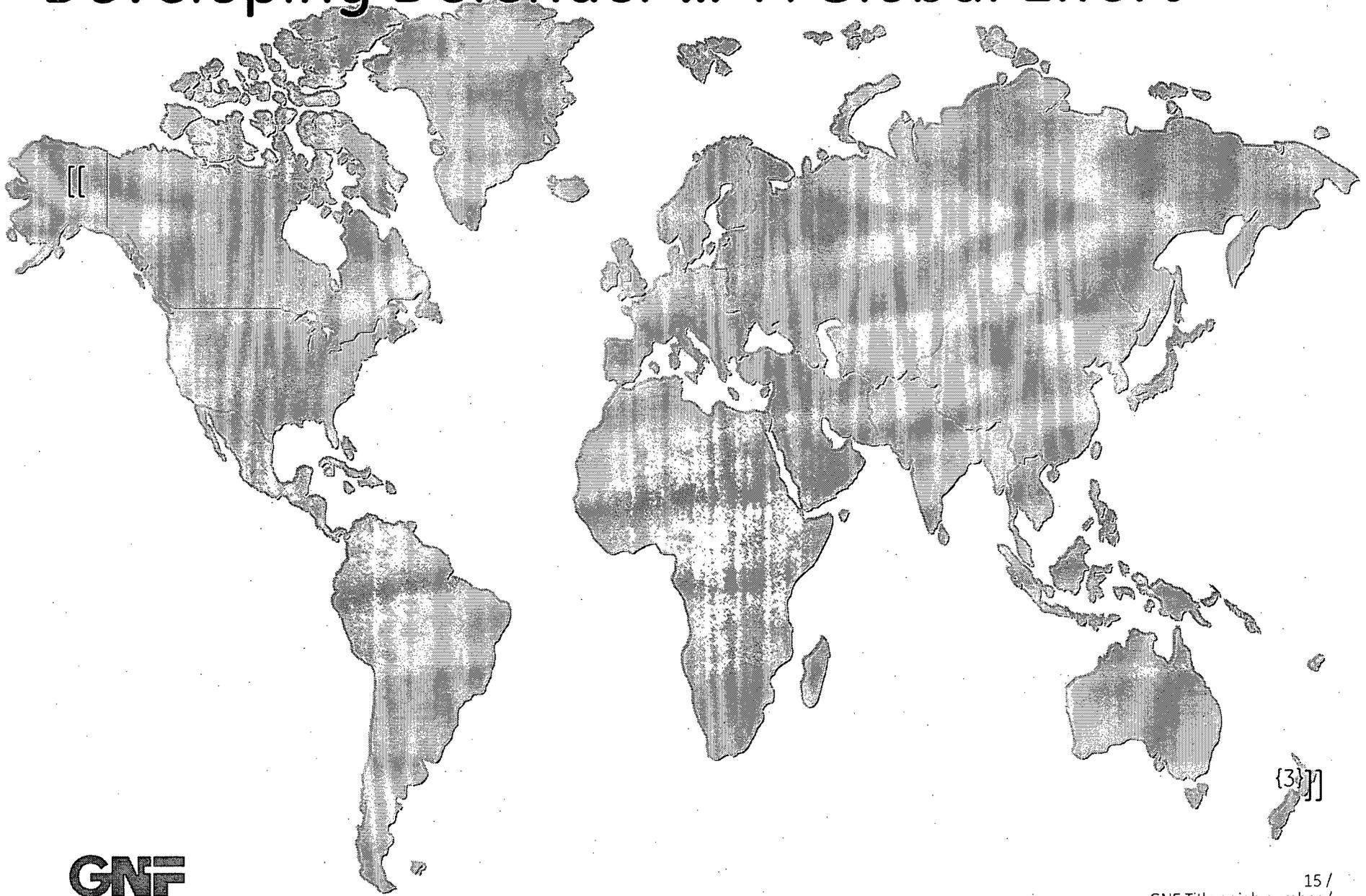
Endurance Testing



Defender Development

GNF & Suppliers **Key CTQ – Foreign Material Exclusion**

Developing Defender ... A Global Effort



{3}}

No Single Supplier Could Do It All !

[[

{3}]

Foreign Material Exclusion – Setting Expectations

[[

{3}]]

Defender Deployment

[[

{3}]]

GNF2 Advantage Description & Licensing

Russ Fawcett
Manager,
Core, Fuel & Advanced Design

Preliminary Unverified Information

GNF2 Design Description

[[

GNF2 Characteristics

[[

Margin Characteristics

[[

GNF2 Licensing Overview

[[

{3}]]

Generic New Fuel Licensing (A22)

[[

{3}]]

Generic New Fuel Licensing (A22)

- Thermal-Mechanical
- Nuclear

[[•

{3}]]

Generic New Fuel Licensing (A22)

[[

{3}]]

Generic New Fuel Licensing (A22)

- **GEXL**

- > GNF2 specific correlation is GEXL17

- GEXL form
- Documented in NEDC-33292P, Revision 0, "GEXL17 Correlation for GNF2 Fuel", November 2006.
- Provided to USNRC along with 33270P

Generic New Fuel Licensing (A22)

[[

{3}]]

GNF2 Plant Specific Analyses (NFI)

[[

{3}]]

GEXL17

Overview

[[

{3}]

Database

[[

{3}]

Correlation Performance

[[

{3}]]

Summary

[[

{3}]]

GNF Technology Update Meeting

GNF-Ziron Cladding

Yang-Pi Lin

May 1-2, 2007



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Preliminary Unverified Information

GNF-Ziron Cladding

Program Objective

Introduce [[

{3}]]

- Introduction/Background
- In-reactor Experience

[[

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{3}]]

Composition Comparison (wt%)

	Zircaloy-2	GNF-Ziron
Zirconium	> 97	[[
Tin	1.20 – 1.70	
Iron	0.07 – 0.20 (0.17 – 0.18 typical)	
Chromium	0.05 – 0.15	
Nickel	0.03 – 0.08	{3}]]

[[

{3}]]

GNF-Ziron Background

[[

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GNF-Ziron Experience

[[

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GNF-Ziron Performance

[[

{3}]]

Tensile Elongation

[[

{3}]

Creep Behavior

[[

{3}]]

GNF-Ziron – Lead Use Applications

[[

GNF-Ziron – Lead Use Applications

[[

Simulated LOCA Oxidation Results

[[

{3}]]

Simulated LOCA Test Results

[[

{3}]

Simulated LOCA Test – additional tests

[[

{3}]]

GNF-Ziron Licensing Strategy

[[

{3}]]

GNF Fuel Experience & Reliability

Presentation to NRC
May 2007

Rob Schneider



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Preliminary Unverified Information

Agenda

- Fuel Experience Summary
 - Total, current designs
- Reliability Trend
 - historical, recent trends
 - 2006 data
- Details
 - GE14 failures
- New Fuel Reload Surveillance Status
- LUA Surveillance Status
- Rod Gap Observations

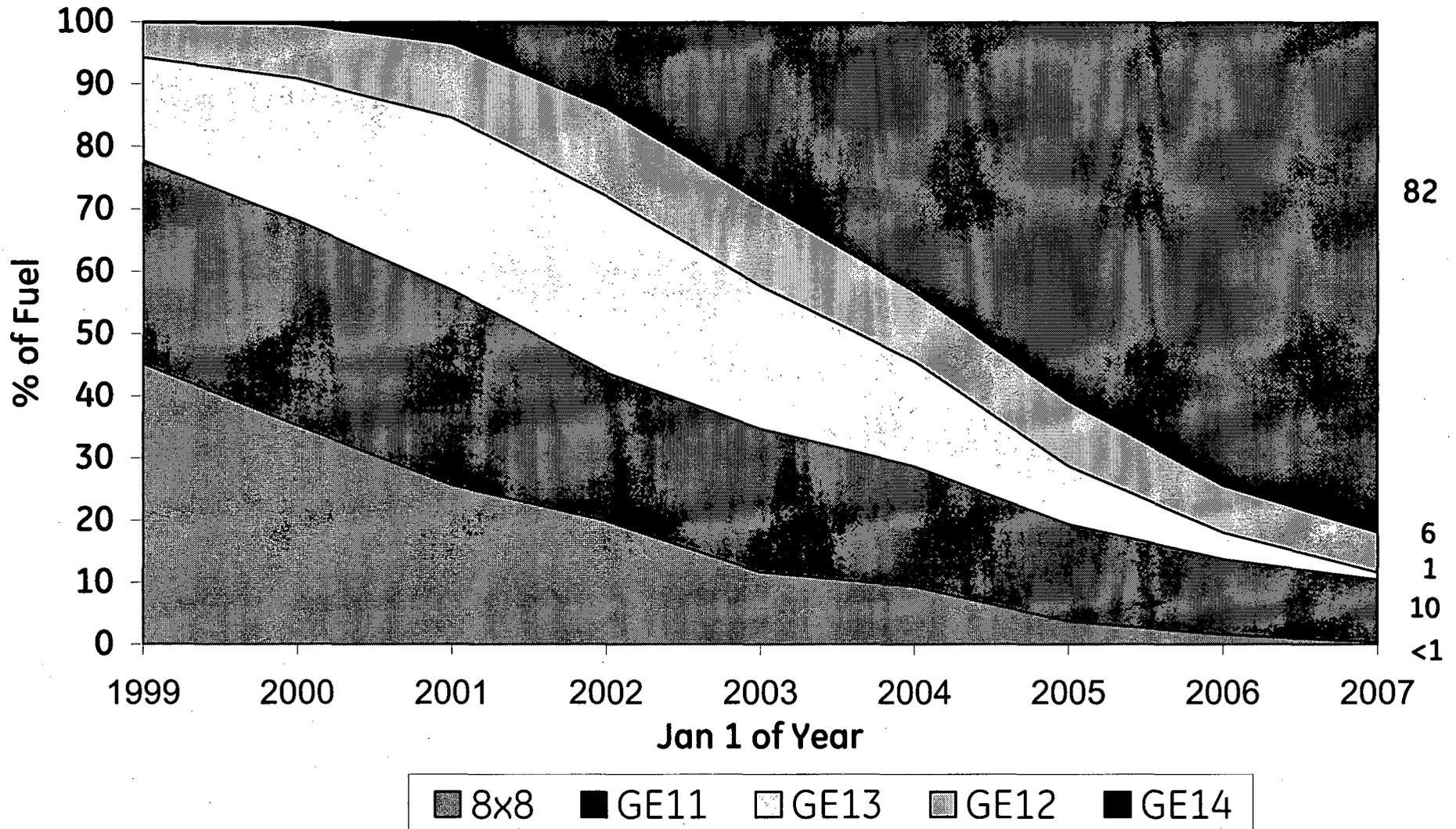
GNF Fuel Experience (May '74 to Dec '06)

[[

Fuel Experience Update (through 3/31/07)

[[

Fuel Experience Update



Historical Reliability Trends

[[

GNF Fuel Failures per Year – All designs

[[

2006 overview

[[

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New Fuel Reload Surveillances

- Completion reported to NRC for designs through GE11
- Inspections partially completed for GE13 and GE12
- GE14 - some reload bundles discharged after two cycles but not considered "end of life"

Fuel Design	1 st Year of Introduction	BOL Date Examined Bundles	Total Plants	Total Bundles Examined
GE8B	4/87-3/88	6/87-9/87	3	33
GE9B/GE10	11/89-5/91	6/90-6/91	4	30
GE11	7/92-6/93	7/92-8/93	3	28
GE12	12/96-1/97	12/96-5/98	3	5
	NOTE: also ~73 bundles with BOL 11/97, 5/99 inspected after two cycles at ~40 GWd/MT			
GE13	3/96-4/97	3/96-11/97	6	10
	NOTE: Numerous additional inspections at EOL of more recent bundles and channels			
GE14	2000-2001 in US			
	NOTE: over 70 inspections completed at various exposures (LUAs, failures, and routine surveillances associated w/ chemistry changes, etc.)			

Rod Gap Surveillance

[[



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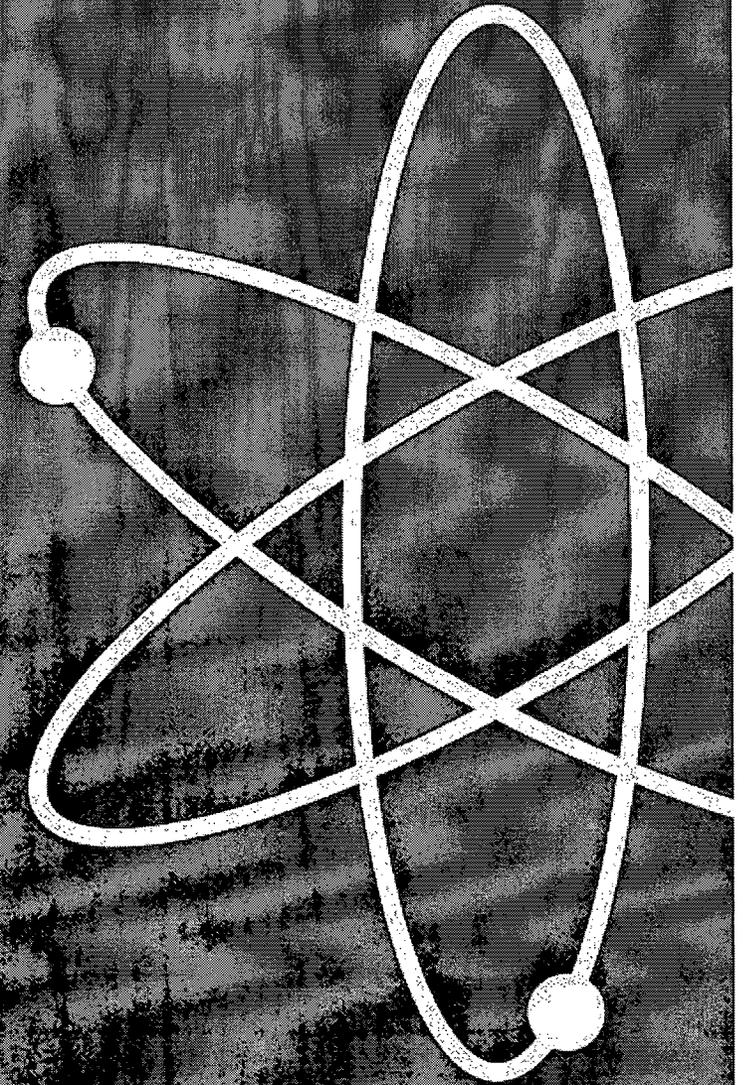
Preliminary Unverified Information

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10/
Schneider /
4/5/2007

GNF Fuel Reliability Program

John Schardt



Nuclear Innovations
creating a new dialogue



Fuel Experience ... Reliability

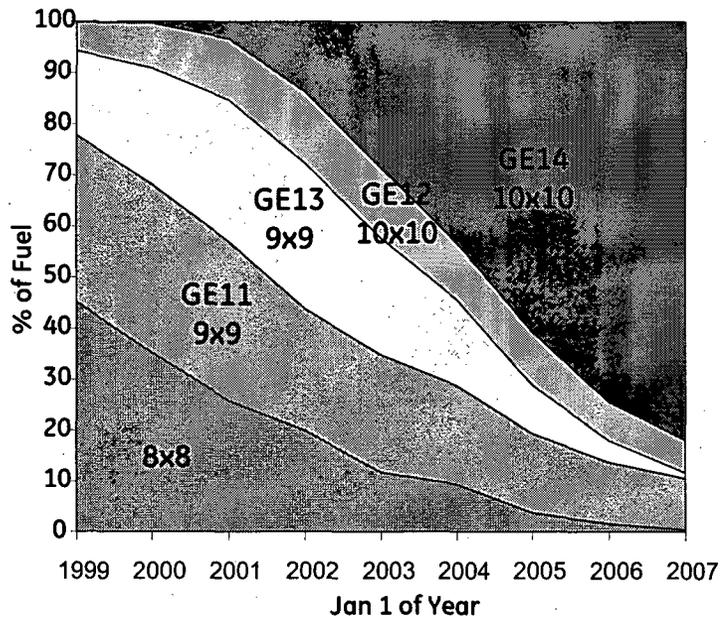
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Fuel Experience...the challenge

82% of operating fuel GE14

GE14 [[

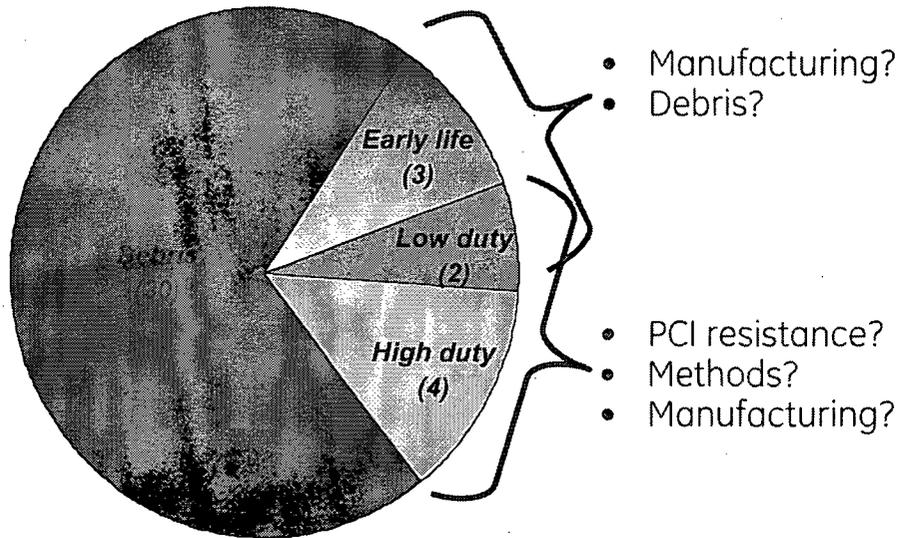


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Key to improved reliability is debris failures

Preliminary Unverified Information

GNF "Defense-in-Depth" Program



GE14 1999-2006

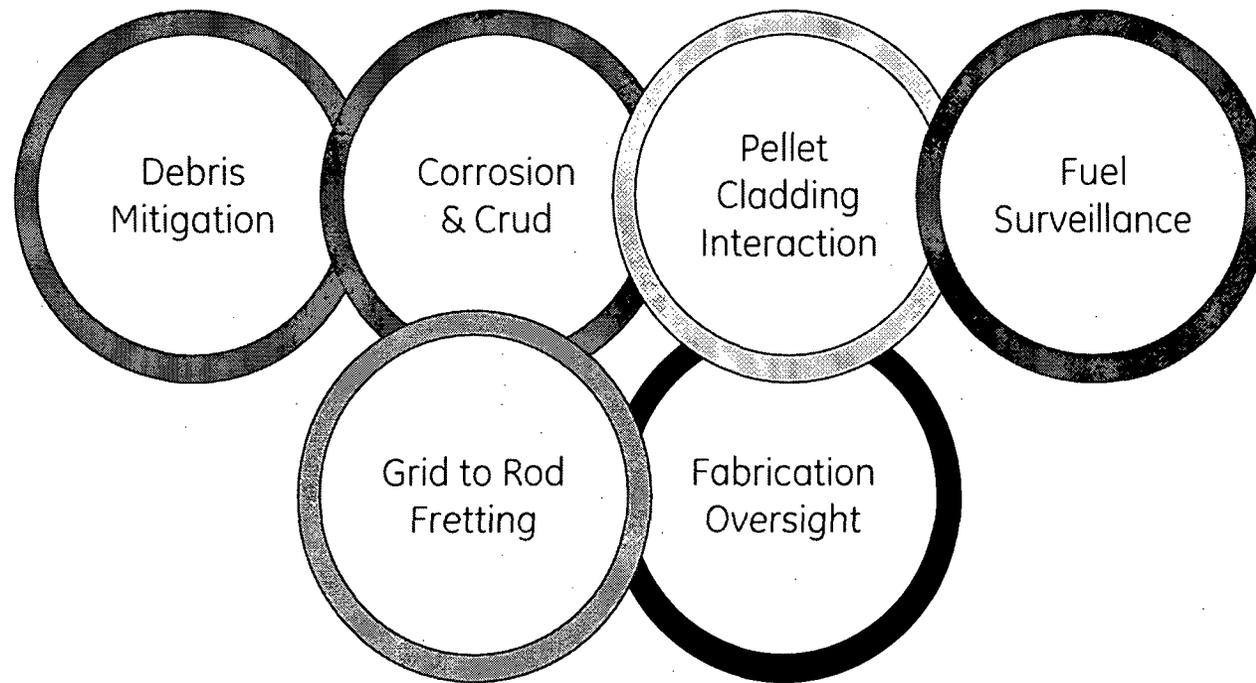
Program scope (target active mechanisms):

- Debris
- Duty
- Manufacturing
- Corrosion (BF2 9x9)

Validated by:

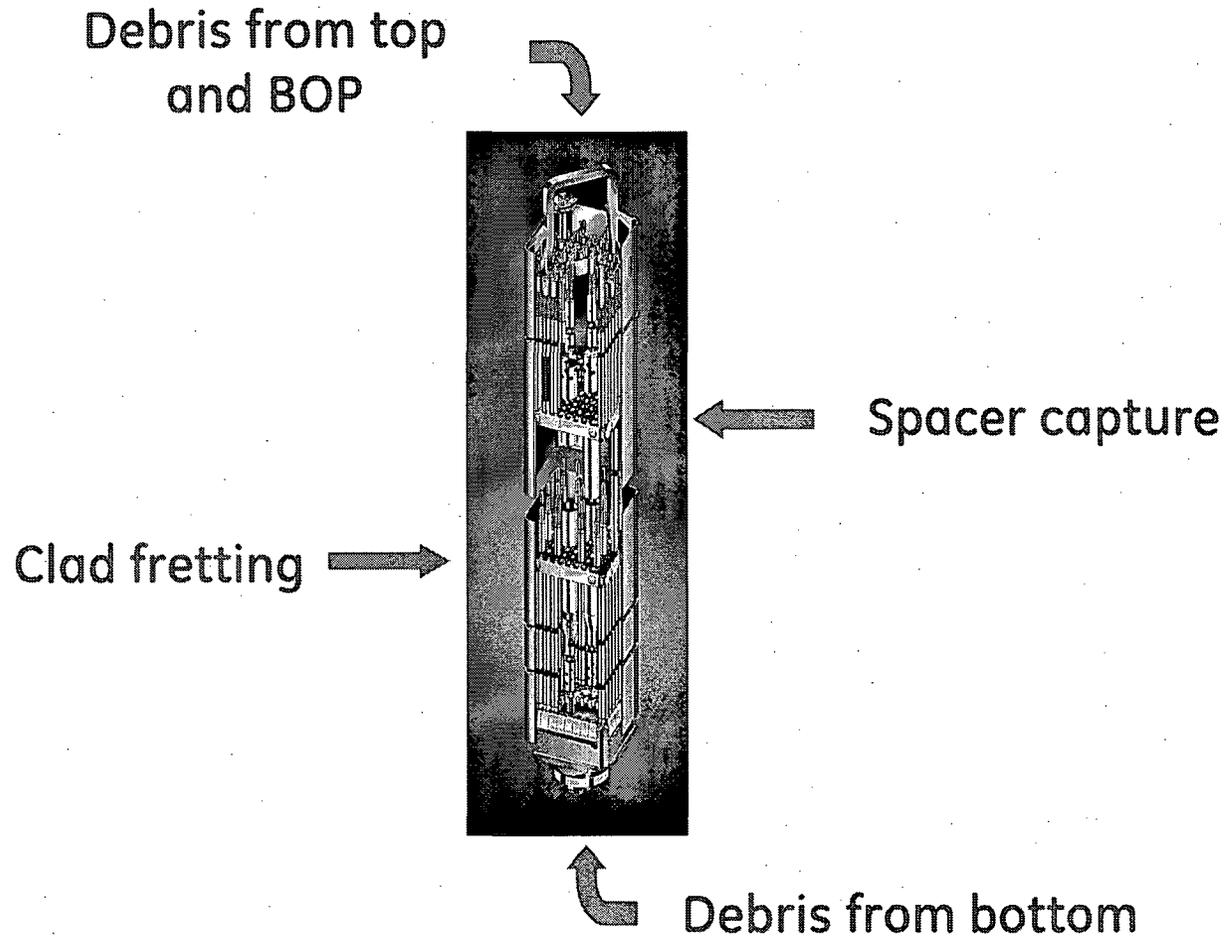
- EPRI Program Assessment
- Expert reviews
- Customer GE14 Reviews beginning 4/05

GNF Defense in Depth...consistent with INPO zero leaker initiative



***GNF team participating in all guideline area
except Grid-to-Rod fretting***

Defense-in-Depth ... Debris



Debris filter capability evolution

[[

{3}]]

Spacer 2Φ debris interaction study

[[

{3}]]

Fuel Rod Coatings...fretting tests at GRC

[[

{3}]]

Defender Debris Retention Testing

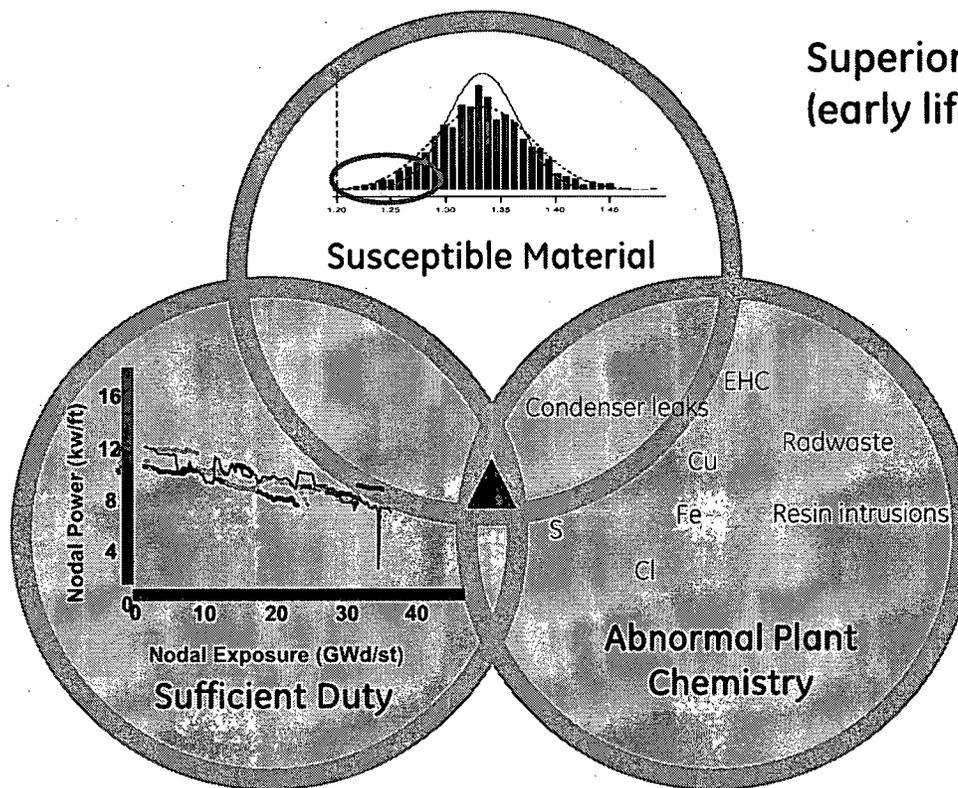
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Defense-in-Depth ... Corrosion Protection



Superior cladding nodular
(early life) corrosion resistance

Improved water
chemistry monitoring,
management

Prevention through collaboration ...cladding and chemistry

Defense-in-Depth ... P8 barrier cladding

[[

{3}]]

Defense in Depth....Ziron

[[

{3}]]

ZIRON.... experience to 68 GWd/MT

[[

{3}]]

Defense-in-Depth....Improved water chemistry monitoring, management

[[

{3}]]

Defense-in-Depth ... Duty (PCI) Protection

[[

{3}]]

Defense-in-Depth... Monitoring System Upgrade (3D Monicore)

[[

{3}]]

GNF Defense-in-Depth...Additive

[[

{3}]]

GNF Defense-in-Depth...state-of-the-art methods

[[

{3}]]

Defense in Depth....five duty initiatives

[[

{3}]]

GNF Defense-in-Depth....manufacturing

[[

{3}]]

Defense-in-Depth ... Research

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{3}]]

Defense-in-Depth Program

[[

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