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Dominion

FEB 2 6 2007

U. S. Nuclear Regulatory Commission
Attention: Document Control Desk
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Serial No.	07-0071
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Docket No.	50-336
License No.	DPR-65

DOMINION NUCLEAR CONNECTICUT, INC.
MILLSTONE POWER STATION UNIT 2
STARTUP TEST REPORT FOR CYCLE 18

Pursuant to Section 6.9.1.3 of the Millstone Unit 2 Technical Specifications, Dominion Nuclear Connecticut, Inc. hereby submits the enclosed Startup Test Report for Cycle 18.

Should you have any questions about the information provided or require additional information, please contact Mr. David W. Dodson at (860) 447-1791, extension 2346.

Very truly yours,

A. J. Jordan
Plant Manager - Nuclear

Enclosure: (1)

Commitments made in this letter: None.

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Millstone Power Station

Serial No. 07-0071
Docket No. 50-336

ENCLOSURE

STARTUP TEST REPORT FOR CYCLE 18

DOMINION NUCLEAR CONNECTICUT, INC.
MILLSTONE POWER STATION UNIT 2

Table of Contents

1. SUMMARY

The refueling outage preceding the Cycle 18 startup was approximately 44 days, starting on October 7, 2006 and ending on November 19, 2006.

The results of the Millstone 2, Cycle 18 low power physics testing and power ascension testing programs were in good agreement with the core design predictions. All measured parameters were within the review and acceptance criteria of the tests. All Technical Specification Limiting Conditions of Operation (LCOs) were met.

Millstone 2 performed a first time application of WCAP-16011-P-A, "Startup Test Activity Reduction Program." The results of the STAR Program implementation will be submitted in a summary report to the NRC. The report will (a) identify the core design method used, (b) compare the measured and calculated values and the differences between these values to the design method uncertainties and (c) show compliance with the STAR applicability requirements.

2. INTRODUCTION

The Millstone 2 Cycle 18 fuel loading was completed on November 6, 2006. The attached core map (Figure 6.1) shows the final core loading. The subsequent operation/testing milestones were completed as follows:

Initial Criticality	November 18, 2006
Low Power Physics Testing Complete	November 19, 2006
Turbine On-Line	November 19, 2006
30% Power Testing Complete	November 19, 2006
69% Power Testing Complete	November 20, 2006
100% Power Testing Complete	November 28, 2006

The Millstone 2 Cycle 18 core is comprised of 217 AREVA manufactured fuel assemblies.

3. LOW POWER PHYSICS TESTING RESULTS

Low Power Physics Testing was conducted at a power level of approximately 2×10^{-2} % power.

3.1 Unrodded Critical Boron Concentration

The Critical Boron Concentration (CBC) measured with CEA Group 7 at 148 steps withdrawn and an RCS temperature of 529.0°F was 1574 ppm.

Adjusted to the prediction conditions of Group 7 at 180 steps withdrawn and an RCS temperature of 532°F yields an adjusted, measured CBC of 1588 ppm.

Adjusted, measured unrodded CBC	=	1588 ppm
Predicted unrodded CBC	=	1615 ppm
Difference	=	-27 ppm (-219 pcm)

Review Criteria is ± 50 ppm of the predicted CBC.

Acceptance Criteria is ± 1000 pcm of the predicted CBC.

Review and Acceptance Criteria met? Yes.

3.2 Moderator Temperature Coefficient

The Isothermal Temperature Coefficient (ITC) measurements were performed at a boron concentration of 1574 ppm, an average RCS temperature of 528.9°F, and CEA Group 7 at 148 steps.

The measured ITC at these conditions was +1.40 pcm/°F.

Adjusted to the prediction conditions for an RCS boron concentration of 1602 ppm and an RCS temperature of 532°F yields an adjusted, measured ITC of +1.57 pcm/°F.

Adjusted, measured ITC	=	+1.57 pcm/°F
Predicted ITC	=	+1.09 pcm/°F
Difference	=	+0.48 pcm/°F

Review Criteria is ± 2 pcm/°F of the predicted ITC.

Review Criteria met? Yes.

The MTC was determined by subtracting the predicted Doppler Temperature Coefficient at the test conditions from the adjusted, measured ITC. The MTC at these conditions was $+0.303 \times 10^{-4}$ $\Delta\rho$/°F. The Millstone 2 Technical Specifications require the MTC be less positive than $+0.7 \times 10^{-4}$ $\Delta\rho$/°F for power levels less than 70% power.

Technical Specification limit met? Yes.

3.3 Control Element Assembly Rod Worth Parameters

Control Element Assembly (CEA) Rod Worth Parameters were not measured as allowed by WCAP-16011-P-A, "Startup Test Activity Reduction Program."

3.4 Rodded Critical Boron Concentration

The Critical Boron Concentration (CBC) measured with CEA Group A inserted was not performed during Cycle 18 startup testing due to application of the STAR Program.

3.5 Control Rod Drop Time Measurements

The Millstone 2 Technical Specifications require that all CEAs drop in less than or equal to 2.75 seconds to the 90% inserted position, with RCS conditions at greater than or equal to 515°F and full flow (all reactor coolant pumps operating).

Control rod drop time testing was done at an RCS temperature of 530°F with all 4 reactor coolant pumps operating. The average control rod drop time was 2.22 seconds to 90% insertion, with the fastest and slowest drop times being 2.13 seconds and 2.30 seconds, respectively.

Technical Specification limits met? Yes.

4. POWER ASCENSION TESTING RESULTS

4.1 Power Peaking, Linear Heat Rate and Incore Tilt Measurements

The following core power distribution parameters were measured during the power ascension to ensure compliance with the Technical Specifications:

- Total Unrodded Integrated Radial Peaking Factor (F_r^T) is the ratio of the peak fuel rod power to the average fuel rod power in an unrodded core. This value includes the effect of Azimuthal Power Tilt.
- Linear Heat Rate (LHR) is the amount of power being produced per linear length of fuel rod.
- Azimuthal Power Tilt is the maximum difference between the power generated in any core quadrant (upper or lower) and the average power of all quadrants in that half (upper or lower) of the core divided by the average power of all quadrants in that half (upper or lower) of the core.

The measurements of these parameters were:

Power Level	F_r^T	Peak Linear Heat Rate	Incore Tilt
69%	1.616	9.36 KW/ft	0.0059
100%	1.579	12.87 KW/ft	0.0069

The corresponding Technical Specification limits for all power levels for these parameters are:

- $F_r^T \leq 1.69$ (Note - larger values of F_r^T are permissible at less than 100% power)
- Peak Linear Heat Rate ≤ 15.1 KW/ft
- Azimuthal Power Tilt ≤ 0.02

Technical Specification limit for F_r^T met? Yes.

Technical Specification limit for LHR met? Yes.

Technical Specification limit for Tilt met? Yes.

4.2 Critical Boron Measurements

Critical Boron Concentration (CBC) measurement was performed at 100% power at equilibrium xenon conditions.

The CBC measured at 100% power with CEA Group 7 at 180 steps withdrawn and an RCS cold leg temperature of 545.1°F was 1118 ppm. The cycle average exposure at the time of this measurement was 222 MWD/MTU.

Adjusted to the prediction conditions of 100% power at an All Rods Out (ARO) condition and an RCS cold leg temperature of 545 °F yields an adjusted, measured CBC of 1118 ppm.

Adjusted, measured 100% power CBC	=	1118 ppm
Predicted 100% power CBC	=	1136 ppm
Difference	=	-18 ppm (-141 pcm)

Review Criteria is ± 50 ppm of the predicted CBC.

Acceptance Criteria is ± 1000 pcm of the predicted CBC.

Review and Acceptance Criteria met? Yes.

4.3 Hot Zero Power (HZP) to Hot Full Power (HFP) Critical Boron Concentration Difference

The difference in the adjusted measured Critical Boron Concentrations (CBC) performed at HZP and HFP was determined and compared to the design prediction.

Predicted change in CBC from HZP to HFP	=	479 ppm
Adjusted, measured change in CBC from HZP to HFP	=	470 ppm
Difference	=	9 ppm

Review Criteria is ± 50 ppm of the predicted CBC difference.

Review Criteria met? Yes.

4.4 Flux Symmetry Measurements

The core neutron flux symmetry was measured at approximately 30% power using the fixed incore detector monitoring system. The differences between measured and calculated signals in operable incore detector locations ranged from –0.037 to +0.058

Review Criteria is ± 0.10.

Review Criteria met? Yes.

The maximum azimuthal asymmetry in the neutron flux from measurements of the variation in incore detector signals from symmetric incore detectors was 5.34%

Review Criteria is ± 10%.

Review Criteria met? Yes.

4.5 Moderator Temperature Coefficient

The Isothermal Temperature Coefficient (ITC) measurements were performed at a power level of 98.5 %, an RCS boron concentration of 1113 ppm, and an average RCS temperature of 570°F, and CEA Group 7 at 180 steps.

The measured ITC at these conditions was –7.015 pcm/°F.

The predicted ITC was determined for a power level of 100%, an RCS boron concentration of 1144 ppm, an average RCS temperature of 570°F, and at an All Rods Out (ARO) condition.

The predicted ITC at these conditions was –7.27 pcm/°F.

The predicted ITC adjusted for 98.5% power, an actual RCS boron concentration of 1113 ppm and an RCS temperature of 569.4°F yields an adjusted, predicted ITC of –7.657 pcm/°F.

Adjusted, Predicted ITC	=	–7.657 pcm/°F
Measured ITC	=	–7.015 pcm/°F
Difference	=	-0.642 pcm/°F

Review Criteria is ± 2 pcm/°F of the predicted ITC.

Review Criteria met? Yes.

The MTC was determined by subtracting the predicted Doppler Temperature Coefficient at the test conditions from the adjusted, measured ITC. The MTC at these conditions was -0.578×10^{-4} Δρ/°F. The Millstone 2 Technical Specifications require the MTC be less than or equal to $+0.4 \times 10^{-4}$ Δρ/°F for power levels greater than 70% power.

Technical Specification limit met? Yes.

4.6 Reactor Coolant System Flow

The RCS flow rate was measured using the secondary calorimetric method, in which the RCS flow rate is inferred by performing a heat balance around the steam generators and RCS to determine reactor power, and measuring the differential temperature across the reactor core to determine the enthalpy rise.

The measured RCS flow rate at 100% power was 384,933 GPM.

When 13,000 GPM is subtracted from the measured flow rate to account for measurement uncertainties, the Minimum Guaranteed Safety Analysis RCS Flow Rate is 371,933 GPM. This value is used to satisfy the Technical Specification surveillance requirement.

The Millstone 2 Technical Specifications require the RCS flow rate to be greater than 360,000 GPM.

Technical Specification limit met? Yes.

4.7 Core Power Distributions

The core power distribution measurements were inferred from the signals obtained by the fixed incore detector monitoring system. These measurements were performed at 69% power and 100% to determine if the measured and predicted core power distributions are consistent.

The core power distribution map for 69% power, cycle average exposure of 16 MWD/MTU, *non*-equilibrium xenon conditions is shown in Figure 6.2.

This map shows that there is good agreement between the measured and predicted values.

The core power distribution map for 100%, cycle average exposure of 224 MWD/MTU, equilibrium xenon conditions is shown in Figure 6.3. This map also shows that there is good agreement between the measured and predicted values.

The Review Criteria for these measurements are:

1. The difference between the measured and predicted Relative Power Densities (RPDs) for core locations with an operable incore detector is less than 0.1.
2. The Root Mean Square (RMS) deviation for radial and axial power distributions between the measured and predicted values is less than 0.05.

Review Criteria met? Yes, for both 69% and 100% power.

4.8 Reactor Coolant System Radiochemistry

RCS radiochemistry analysis during the power ascension testing program and during subsequent power operation indicate activity levels with Iodine-131 values of about 7.2×10^{-4} μCi/ml. These RCS activity levels show that all failed fuel assemblies have been discharged from the core.

5. REFERENCES

5.1 EN 21004K, "Cycle 18, Low Power Physics Test"

5.2 EN 21004J, "Cycle 18, Power Ascension Testing"

5.3 "Millstone Unit 2, Cycle 18, Startup and Operations Report"

5.4 SP 21010, "CEA Drop Times,"

6. FIGURES

6.1 Cycle 18 Core Loading Map

6.2 69% Core Power Distribution Map

6.3 100% Core Power Distribution Map

						Y-8 T-49	Y-10 V-21	Y-12 V-20	Y-14 T-53							
			X-5 V-68	X-6 V-56	X-7 V-36	X-9 X-11 126	X-11 X-31	X-13 X-14 176	X-15 V-57	X-16 V-45	X-17 V-61					
		W-4 T-34	W-5 X-03 135	W-6 X-51	W-7 X-19 155	W-9 W-03	W-11 W-65 193	W-13 W-06	W-15 X-22 181	W-16 X-54	W-17 X-06 106	W-18 V-51				
	V-3 V-52	V-4 X-27 110	V-5 W-20	V-6 W-63 154	V-7 V-01	V-9 V-44 191	V-11 X-39	V-13 V-39 187	V-15 V-08	V-16 W-58 124	V-17 W-13	V-18 X-26 159	V-19 T-33			
T-2 V-62	T-3 X-07 103	T-4 W-14	T-5 W-22	T-6 X-63	T-7 W-55 105	T-9 X-43	T-11 V-27	T-13 X-46	T-15 W-50 165	T-16 X-66	T-17 W-21	T-18 W-19	T-19 X-02 113	T-20 V-67		
S-2 V-46	S-3 X-55	S-4 W-59 129	S-5 X-67	S-6 V-31 174	S-7 W-33	S-9 W-48	S-11 W-27	S-13 W-41	S-15 W-40	S-16 V-30 173	S-17 X-62	S-18 W-62 127	S-19 X-50	S-20 V-55		
R-2 V-58	R-3 X-23 158	R-4 V-05	R-5 W-51 119	R-6 W-37	R-7 X-59 183	R-9 V-11	R-11 X-35 122	R-13 V-14	R-15 X-58 166	R-16 W-36	R-17 W-54 161	R-18 V-04	R-19 X-18 170	R-20 V-35		
P-1 T-54	N-2 X-15 115	N-3 W-07	N-4 V-40 188	N-5 X-47	N-6 W-42	N-7 V-15	N-9 W-09 104	N-11 W-32	N-13 W-12 133	N-15 V-10	N-16 W-47	N-17 X-42	N-18 V-43 190	N-19 W-02	N-20 X-10 117	P-21 T-52
M-1 V-17	L-2 X-32	L-3 W-66 192	L-4 X-40	L-5 V-28	L-6 W-28	L-7 X-36 137	L-9 W-29	L-11 S-57 112	L-13 W-31	L-15 X-34 180	L-16 W-26	L-17 V-26	L-18 X-38	L-19 W-68 169	L-20 X-30	M-21 V-24
K-1 V-22	J-2 X-12 136	J-3 W-04	J-4 V-41 189	J-5 X-44	J-6 W-45	J-7 V-12	J-9 W-10 130	J-11 W-30	J-13 W-11 128	J-15 V-13	J-16 W-44	J-17 X-45	J-18 V-38 186	J-19 W-05	J-20 X-13 171	K-21 V-19
H-1 T-50	G-2 V-33	G-3 X-20 179	G-4 V-02	G-5 W-56 157	G-6 W-34	G-7 X-60 160	G-9 V-16	G-11 X-33 178	G-13 V-09	G-15 X-57 182	G-16 W-39	G-17 W-49 164	G-18 V-07	G-19 X-21 162	G-20 V-60	H-21 T-56
	F-2 V-53	F-3 X-52	F-4 W-64 163	F-5 X-64	F-6 V-32 175	F-7 W-38	F-9 W-43	F-11 W-25	F-13 W-46	F-15 W-35	F-16 V-29 172	F-17 X-65	F-18 W-57 116	F-19 X-53	F-20 V-48	
	E-2 V-65	E-3 X-04 132	E-4 W-17	E-5 W-23	E-6 X-68	E-7 W-52 109	E-9 X-48	E-11 V-25	E-13 X-41	E-15 W-53 108	E-16 X-61	E-17 W-24	E-18 W-16	E-19 X-05 123	E-20 V-64	
		D-3 T-38	D-4 X-28 111	D-5 W-15	D-6 W-60 134	D-7 V-06	D-9 V-37 184	D-11 X-37	D-13 V-42 185	D-15 V-03	D-16 W-61 125	D-17 W-18	D-18 X-25 156	D-19 V-50		
			C-4 V-49	C-5 X-08 121	C-6 X-56	C-7 X-24 177	C-9 W-08	C-11 W-67 168	C-13 W-01	C-15 X-17 167	C-16 X-49	C-17 X-01 120	C-18 T-36			
				B-5 V-63	B-6 V-47	B-7 V-59	B-9 X-16 118	B-11 X-29	B-13 X-09 114	B-15 V-34	B-16 V-54	B-17 V-66				
						A-8 T-55	A-10 V-18	A-12 V-23	A-14 T-51							

Key

B-9
X-16
118

Core Location
Fuel Assembly ID
Insert ID

Figure 6.1

Millstone Unit No. 2
Cycle 18 Core Map

								Y-8	Y-10	Y-12	Y-14 0.211 0.209 0.002											
				X-5	X-6	X-7 0.562 0.569 -0.007	X-9	X-11 1.210 1.199 0.011	X-13	X-15	X-16	X-17 0.293 0.295 -0.002									
			W-4 0.381 0.382 -0.001	W-5	W-6 1.247 1.233 0.014	W-7	W-9	W-11	W-13	W-15	W-16 INOP	W-17	W-18								
		V-3	V-4	V-5	V-6	V-7	V-9	V-11 1.344 1.337 0.007	V-13	V-15 1.072 1.053 0.019	V-16	V-17	V-18	V-19 0.379 0.382 -0.003								
	T-2 0.292 0.295 -0.003	T-3	T-4	T-5	T-6	T-7	T-9 1.313 1.351 -0.038	T-11	T-13	T-15	T-16 1.283 1.292 -0.009	T-17	T-18	T-19	T-20							
	S-2	S-3 1.237 1.241 -0.004	S-4	S-5	S-6	S-7	S-9	S-11 1.175 1.167 0.008	S-13	S-15	S-16	S-17	S-18	S-19	S-20 0.413 0.415 -0.002							
	R-2	R-3	R-4 1.070 1.054 0.016	R-5	R-6 1.152 1.157 -0.005	R-7	R-9	R-11	R-13	R-15	R-16	R-17	R-18	R-19	R-20							
P-1	N-2	N-3	N-4	N-5	N-6	N-7	N-9	N-11 1.041 1.069 -0.028	N-13	N-15 1.004 0.998 0.006	N-16	N-17 INOP	N-18	N-19	N-20	P-21						
M-1	L-2	L-3	L-4 1.333 1.337 -0.004	L-5	L-6 1.162 1.167 -0.005	L-7	L-9	L-11	L-13	L-15	L-16 1.166 1.166 0.000	L-17	L-18 1.353 1.337 0.016	L-19	L-20	M-21						
K-1	J-2	J-3	J-4	J-5	J-6	J-7 0.972 0.998 -0.026	J-9	J-11	J-13	J-15	J-16 1.168 1.170 -0.002	J-17	J-18	J-19	J-20	K-21						
H-1	G-2	G-3	G-4	G-5	G-6	G-7	G-9 0.983 0.998 -0.015	G-11	G-13	G-15	G-16	G-17	G-18 1.054 1.053 0.001	G-19	G-20	H-21						
	F-2	F-3 1.229 1.233 -0.004	F-4	F-5	F-6	F-7	F-9	F-11 1.167 1.166 0.001	F-13	F-15	F-16	F-17	F-18	F-19 1.248 1.241 0.007	F-20							
	E-2	E-3	E-4	E-5	E-6	E-7	E-9	E-11	E-13	E-15	E-16	E-17	E-18	E-19	E-20 0.285 0.295 -0.010							
		D-3 0.370 0.382 -0.012	D-4	D-5 1.254 1.258 -0.004	D-6	D-7 1.065 1.053 0.012	D-9	D-11 1.333 1.337 -0.004	D-13	D-15	D-16	D-17	D-18	D-19								
			C-4	C-5	C-6 1.253 1.241 0.012	C-7	C-9	C-11	C-13 1.297 1.243 0.054	C-15	C-16 1.248 1.233 0.015	C-17	C-18 0.376 0.382 -0.006									
				B-5 0.288 0.295 -0.007	B-6	B-7 0.565 0.566 -0.001	B-9	B-11	B-13	B-15 0.575 0.568 0.007	B-16	B-17										
								A-8	A-10 0.329 0.339 -0.010	A-12	A-14											

Key

B-15	Core Location
0.575	Measured RPD
0.568	Calculated RPD
0.007	Difference

Root Mean Square Deviation for all Core Locations = 0.009

Figure 6.2
69% Power Distribution Map
All Rods Out, Non-Equilibrium Xenon, 16 MWD/MTU

						Y-8	Y-10	Y-12	Y-14 0.214 0.214 0.000							
				X-5	X-6	X-7 0.560 0.570 -0.010	X-9	X-11 1.178 1.168 0.010	X-13	X-15	X-16	X-17 0.293 0.297 -0.004				
			W-4 0.379 0.381 -0.002	W-5	W-6 1.215 1.202 0.013	W-7	W-9	W-11	W-13	W-15	W-16 INOP	W-17	W-18			
		V-3	V-4	V-5	V-6	V-7	V-9	V-11 1.338 1.331 0.007	V-13	V-15 1.068 1.055 0.013	V-16	V-17	V-18	V-19 0.376 0.381 -0.005		
	T-2 0.292 0.297 -0.005	T-3	T-4	T-5	T-6	T-7	T-9 1.335 1.357 -0.022	T-11	T-13	T-15	T-16 1.281 1.285 -0.004	T-17	T-18	T-19	T-20	
	S-2	S-3 1.203 1.209 -0.006	S-4	S-5	S-6	S-7	S-9	S-11 1.201 1.194 0.007	S-13	S-15	S-16	S-17	S-18	S-19	S-20 0.414 0.418 -0.004	
	R-2	R-3	R-4 1.066 1.055 0.011	R-5	R-6 1.173 1.179 -0.006	R-7	R-9	R-11	R-13	R-15	R-16	R-17	R-18	R-19	R-20	
P-1																P-21
	N-2	N-3	N-4	N-5	N-6	N-7	N-9	N-11 1.103 1.116 -0.013	N-13	N-15 1.035 1.033 0.002	N-16	N-17 INOP	N-18	N-19	N-20	
M-1																M-21
	L-2	L-3	L-4 1.328 1.331 -0.003	L-5	L-6 1.187 1.194 -0.007	L-7	L-9	L-11	L-13	L-15	L-16 1.193 1.194 -0.001	L-17	L-18 1.350 1.330 0.020	L-19	L-20	
K-1																K-21
	J-2	J-3	J-4	J-5	J-6	J-7 1.003 1.033 -0.030	J-9	J-11	J-13	J-15	J-16 1.194 1.195 -0.001	J-17	J-18	J-19	J-20	
H-1																H-21
	G-2	G-3	G-4	G-5	G-6	G-7	G-9 1.014 1.033 -0.019	G-11	G-13	G-15	G-16	G-17	G-18 1.052 1.055 -0.003	G-19	G-20	
	F-2	F-3 1.200 1.202 -0.002	F-4	F-5	F-6	F-7	F-9	F-11 1.195 1.194 0.001	F-13	F-15	F-16	F-17	F-18	F-19 1.220 1.208 0.012	F-20	
	E-2	E-3	E-4	E-5	E-6	E-7	E-9	E-11	E-13	E-15	E-16	E-17	E-18	E-19	E-20 0.286 0.297 -0.011	
		D-3 0.369 0.381 -0.012	D-4	D-5 1.226 1.231 -0.005	D-6	D-7 1.061 1.055 0.006	D-9	D-11 1.330 1.330 0.000	D-13	D-15	D-16	D-17	D-18	D-19		
			C-4	C-5	C-6 1.223 1.209 0.014	C-7	C-9	C-11	C-13 1.280 1.226 0.054	C-15	C-16 1.221 1.202 0.019	C-17	C-18 0.375 0.381 -0.006			
				B-5 0.290 0.297 -0.007	B-6	B-7 0.564 0.567 -0.003	B-9	B-11	B-13	B-15 0.575 0.570 0.005	B-16	B-17				
						A-8	A-10 0.333 0.342 -0.009	A-12	A-14							

Radial
Root Mean Square Deviation
for all Core Locations = 0.009

Axial
Root Mean Square Core Average
Deviation = 0.017

Key

B-15 0.575 0.570 0.005	Core Location Measured RPD Calculated RPD Difference

Figure 6.3
100% Power Distribution Map
All Rods Out, Equilibrium Xenon, 224 MWD/MTU