

TECHNICAL REPORT TITLE PAGE

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**Instrument Efficiency Determination for Use in Minimum Detectable Concentration Calculations in Support of the Final Status Survey at Yankee Rowe**

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Title

YA-REPT-00-015-04  
REV. 0

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Technical Report Number

**Approvals**

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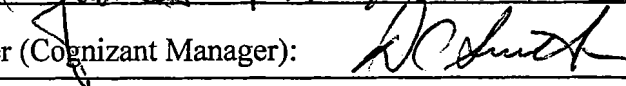
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## 1.0 Executive Summary:

The minimum detectable concentration (MDC) of the field survey instrumentation is an important factor affecting the quality of the final status survey (FSS). The efficiency of an instrument inversely impacts the MDC value. The objective of this report is to determine the instrument and source efficiency values used to calculate MDC. Several factors were considered when determining these efficiencies and are discussed in the body of this report. Instrument efficiencies ( $\epsilon_i$ ), and source efficiencies ( $\epsilon_s$ ), for alpha beta detection equipment under various field conditions, and instrument conversion factors ( $E_i$ ), for gamma scanning detectors were determined and the results are provided herein.

## 2.0 Introduction:

Before performing Final Status Surveys of building surfaces and land areas, the minimum detectable concentration (MDC) must be calculated to establish the instrument sensitivity. Table 5.4 of the License Termination Plan (LTP) [8.6] lists the available instrumentation and nominal detection sensitivities; however for the purposes of this basis document, efficiencies for the 100cm<sup>2</sup> gas proportional and the 2"x2" NaI (TI) detectors will be determined. Efficiencies for the other instrumentation listed in the LTP shall be determined on an as needed basis. The 100 cm<sup>2</sup> gas proportional probe will be used to perform surveys (i.e. fixed point measurements). A 2" x2" NaI (TI) detector will be used to perform gamma surveys (i.e., surface scans) of portions of land areas and possibly supplemental structural scans at the Yankee Rowe site. Although surface scans and fixed point measurements can be performed using the same instrumentation, the calculated MDCs will be quite different. MDC is dependent on many factors and may include but is not limited to:

- instrument efficiency
- background
- integration time
- surface type
- source to detector geometry
- source efficiency

A significant factor in determining an instrument MDC is the total efficiency, which is dependent on the instrument efficiency, the source efficiency and the type and energy of the radiation. MDC values are inversely affected by efficiency, as efficiencies increase, MDC values will decrease. Accounting for both the instrument and source components of the total efficiency provides for a more accurate assessment of surface activity.

## 3.0 Calibration Sources:

For accurate measurement of surface activity it is desirable that the field instrumentation be calibrated with source standards similar to the type and energy of the anticipated contamination. The nuclides listed in Table 3.1 illustrate the nuclides found in soil and building surface area DCGL results that are listed in the LTP.

Instrument response varies with incident radiations and energies; therefore, instrumentation selection for field surveys must be modeled on the expected surface activity. For the purposes of this report, isotopes with max beta energies less than that of C-14 (0.158 MeV) will be considered difficult to detect (reference table 3.1). The detectability of radionuclides with max beta energies less than 0.158 MeV, utilizing gas proportional detectors, will be negligible at typical source to detector distances of approximately 0.5

inches. The source to detector distance of 1.27 cm (0.5 inches) is the distance to the detector with the attached standoff (DP-8534 "Operation and Source Checks of Proportional Friskers") [8.5]. Table 3.1 provides a summary of the LTP radionuclides and their detectability using Radiological Health Handbook [8.4] data.

Table 3.1  
Nuclides and Major Radiations: Approximate Energies (Reference 8.4)

| Nuclide | $\alpha$ Energy (MeV)                                | $E_{\beta_{max}}$ (MeV) | Average $E_{\beta}$ (MeV) | Photon Energy (MeV)   | $\alpha$ Detectable w/ Gas Proportional | $\beta$ Detectable w/ Gas Proportional | $\gamma$ Detectable w/ NaI 2x2" |
|---------|--|-------------------------|---------------------------|---|---|--|---------------------------------|
| H-3     |  | 0.018                   | 0.005                     |   |   |  |                                 |
| C-14    |  | 0.158                   | 0.049                     |   |   |  |                                 |
| Fe-55   |  |                         |                           | 0.23 (0.004%)<br>bremsstrahlung   |   |  |                                 |
| Co-60   |  | 0.314                   | 0.094                     | 1.173 (100%), 1.332 (100%)  |   | √                                      | √                               |
| Ni-63   |  | 0.066                   | 0.017                     |   |   |  |                                 |
| Sr-90   |  | 0.544<br>2.245 (Y-90)   | 0.200<br>0.931            |   |   | √                                      |                                 |
| Nb-94   |  | 0.50                    | 0.156                     | 0.702 (100%), 0.871 (100%)  |   | √                                      | √                               |
| Tc-99   |  | 0.295                   | 0.085                     |   |   | √                                      |                                 |
| Ag-108m |  | 1.65 (Ag-108)           | 0.624 (Ag-108)            | 0.434 (0.45%), 0.511 (0.56%)<br>0.615 (0.18%), 0.632 (1.7%)   |   |  | √                               |
| Sb-125  |  | 0.612                   | 0.084                     | 0.6, 0.25, 0.41, 0.46, 0.68, 0.77, 0.92, 1.10, 1.34   |   | √                                      | √                               |
| Cs-134  |  | 1.453                   | 0.152                     | 0.57 (23%), 0.605 (98%)<br>0.796 (99%), 1.038 (1.0%)<br>1.168 (1.9%), 1.365 (3.4%)                          |   | √                                      | √                               |
| Cs-137  |  | 1.167                   | 0.195                     | 0.662 (85%) Ba-137m X-rays  |   | √                                      | √                               |
| Eu-152  |  | 1.840                   | 0.288                     | 0.122 (37%), 0.245 (8%)<br>0.344 (27%), 0.779 (14%)<br>0.965 (15%), 1.087 (12%)<br>1.113 (14%), 1.408 (22%) |   | √                                      | √                               |
| Eu-154  |  | 1.850 (10%)             | 0.228                     |   |   |  |                                 |
| Eu-155  |  | 0.247                   | 0.044                     | 0.087 (32%), 0.105 (20%)  |   | √                                      |                                 |
| Pu-238  | 5.50 (72%)<br>5.46 (28%)                             |                         |                           | 0.099 (8E-3%)<br>0.150 (1E-3%)<br>0.77 (5E-5%)  | √                                       |  |                                 |
| Pu-239  | 5.16 (88%)<br>5.11 (11%)                             |                         |                           | 0.039 (0.007%), 0.052 (0.20%), 0.129 (0.005%)...  | √                                       |  |                                 |
| Pu-241  | 4.90 (0.0019%)<br>4.85 (0.0003%)                     | 0.021                   | 0.005                     | 0.145 (1.6E-4%)   |   |  |                                 |
| Am-241  | 5.49 (85%)<br>5.44 (13%)                             |                         |                           | 0.060 (36%), 0.101 (0.04%)...   | √                                       |  |                                 |
| Cm-243  | 6.06 (6%)<br>5.99 (6%)<br>5.79 (73%)<br>5.74 (11.5%) |                         |                           | 0.209 (4%), 0.228 (12%), 0.278 (14%)  | √                                       |  |                                 |

NUREG-1507 and ISO 7503-1 provide guidance for selecting calibration sources and their use in determining total efficiency. It is common practice to calibrate instrument efficiency for a single beta energy; however the energy of this reference source should not be significantly greater than the beta energy of the lowest energy to be measured.

Tc-99 (0.295 MeV max) and Th-230 (4.68 MeV at 76% and 4.62 MeV at 24%) have been selected as the beta and alpha calibration standards respectively, because their energies conservatively approximate the beta and alpha energies of the plant specific radionuclides.

#### 4.0 Efficiency Determination:

Typically, using the instrument  $4\pi$  efficiency exclusively provides a good approximation of surface activity. Using these means for calculating the efficiency often results in an under estimate of activity levels in the field. Applying both the instrument  $2\pi$  efficiency and the surface efficiency components to determine the total efficiency allows for a more accurate measurement due to consideration of the actual characteristics of the source surfaces. ISO 7503-1 [8.2] recommends that the total surface activity be calculated using:

$$A_s = \frac{R_{S+B} - R_B}{(\epsilon_i)(W)(\epsilon_s)}$$

where:

$A_s$  is the total surface activity in dpm/cm<sup>2</sup>,

$R_{S+B}$  is the gross count rate of the measurement in cpm,

$R_B$  is the background count rate in cpm,

$\epsilon_i$  is the instrument or detector  $2\pi$  efficiency

$\epsilon_s$  is the efficiency of the source

$W$  is the area of the detector window (cm<sup>2</sup>)

#### 4.1 Alpha and Beta Instrument Efficiency ( $\epsilon_i$ ):

Instrument efficiency ( $\epsilon_i$ ) reflects instrument characteristics and counting geometry, such as source construction, activity distribution, source area, particles incident on the detector per unit time and therefore source to detector geometry. Theoretically the maximum value of  $\epsilon_i$  is 1.0, assuming all the emissions from the source are  $2\pi$  and that all emissions from the source are detected. The ISO 7503-1 methodology for determining the instrument efficiency is similar to the historical  $4\pi$  approach; however the detector response, in cpm, is divided by the  $2\pi$  surface emission rate of the calibration source. The instrument efficiency is calculated by dividing the net count rate by the  $2\pi$  surface emission rate ( $q_{2\pi}$ ) (includes absorption in detector window, source detector geometry). The instrument efficiency is expressed in ISO 7503-1 by:

$$\epsilon_i = \frac{R_{S+B} - R_B}{q_{2\pi}}$$

where:

$R_{S+B}$  is the gross count rate of the measurement in cpm,

$R_B$  is the background count rate in cpm,

$q_{2\pi}$  is the  $2\pi$  surface emission rate in reciprocal seconds

Note that both the  $2\pi$  surface emission rate and the source activity are usually stated on the certification sheet provided by the calibration source manufacturer and certified as National Institute of Standards and Technology (NIST) traceable. Table 4.1 depicts instrument efficiencies that have been determined during calibration using the  $2\pi$  surface emission rate of the source.

Table 4.1  
Instrument Efficiencies ( $\epsilon_i$ )

| Source | Emission | Active Area of Source (cm <sup>2</sup> ) | Effective Area of Detector | 100 cm <sup>2</sup> Gas Proportional HP-100 Instrument Efficiency ( $\epsilon_i$ ) (Contact) |
|--------|----------|--|----------------------------|--|
| Tc-99  | $\beta$  | 15.2                                     | 100 cm <sup>2</sup>        | 0.4148   |
| Th-230 | $\alpha$ | 15.2                                     | 100 cm <sup>2</sup>        | 0.5545   |

#### 4.2 Source to Detector Distance Considerations:

A major factor affecting instrument efficiency is source to detector distance. Consideration must be given to this distance when selecting accurate instrument efficiency. The distance from the source to the detector shall to be as close as practicable to geometric conditions that exist in the field. A range of source to detector distances has been chosen, taking into account site specific survey conditions. In an effort to minimize the error associated with geometry, instrument efficiencies have been determined for source to detector distances representative of those survey distances expected in the field. The results shown in Table 4.2 illustrate the imposing reduction in detector response with increased distance from the source. Typically this source to detector distance will be 0.5 inches for fixed point measurements and 0.5 inches for scan surveys on flat surfaces, however they may differ for other surfaces. Table 4.2 makes provisions for the selection of source to detector distances for field survey conditions of up to 2 inches. If surface conditions dictate the placement of the detector at distances greater than 2 inches instrument efficiencies will be determined on an as needed basis.

##### 4.2.1 Methodology:

The practical application of choosing the proper instrument efficiency may be determined by averaging the surface variation (peaks and valleys narrower than the length of the detector) and adding 0.5 inches, the spacing that should be maintained between the detector and the highest peaks of the surface. Select the source to detector distance from Table 4.2 that best reflects this pre-determined geometry.

Table 4.2  
Source to Detector Distance Effects on Instrument Efficiencies for  $\alpha$ -  $\beta$  Emitters

| Source to Detector Distance (cm) | Instrument Efficiency ( $\epsilon_i$ ) |                    |
|----------------------------------|--|--------------------|
|                                  | Tc-99 Distributed                      | Th-230 Distributed |
| Contact                          | 0.4148                                 | 0.5545             |
| 1.27 (0.5 in)                    | 0.2413                                 | 0.1764             |
| 2.54 (1 in)                      | 0.1490                                 | 0.0265             |
| 5.08 (2 in)                      | 0.0784                                 | 0.0002             |

**4.3 Source (or Surface) Efficiency ( $\epsilon_s$ ) Determination:**

Source efficiency ( $\epsilon_s$ ), reflects the physical characteristics of the surface and any surface coatings. The source efficiency is the ratio between the number of particles emerging from surface and the total number of particles released within the source. The source efficiency accounts for attenuation and backscatter.  $\epsilon_s$  is nominally 0.5 (no self-absorption/attenuation, no backscatter)—backscatter increases the value, self-absorption decreases the value. Source efficiencies may either be derived experimentally or simply selected from the guidance contained in ISO 7503-1. ISO 7503-1 takes a conservative approach by recommending the use of factors to correct for alpha and beta self-absorption/attenuation when determining surface activity. However, this approach may prove to be too conservative for radionuclides with max beta energies that are marginally lower than 0.400 MeV, such as Co-60 with a  $\beta_{max}$  of 0.314 MeV. In this situation, it may be more appropriate to determine the source efficiency by considering the energies of other beta emitting radionuclides. Using this approach it is possible to determine weighted average source efficiency. For example, a source efficiency of 0.375 may be calculated based on a 50/50 mix of Co-60 and Cs-137. The source efficiencies for Co-60 and Cs-137 are 0.25 and 0.5 respectively, since the radionuclide fraction for Co-60 and Cs-137 is 50% for each, the weighted average source efficiency for the mix may be calculated in the following manner:

$$(0.25)(0.5) + (0.5)(0.5) = 0.375$$

Table 4.3 lists guidance on source efficiencies from ISO 7503-1.

Table 4.3  
Source Efficiencies as listed in ISO 7503-1

|                | $> 0.400 \text{ MeV}_{max}$ | $\leq 0.400 \text{ MeV}_{max}$ |
|----------------|-----------------------------|--------------------------------|
| Beta emitters  | $\epsilon_s = 0.5$          | $\epsilon_s = 0.25$            |
| Alpha emitters | $\epsilon_s = 0.25$         | $\epsilon_s = 0.25$            |

It should be noted that source efficiency is not typically addressed for gamma detectors as the value is effectively unity.



### 5.0 Instrument Conversion Factor ( $E_i$ ) (Instrument Efficiency for Scanning):

Separate modeling analysis (Microshield™) was conducted using the common gamma emitters with a concentration of 1 pCi/g of uniformly distributed contamination throughout the volume. MicroShield is a comprehensive photon/gamma ray shielding and dose assessment program, which is widely used throughout the radiological safety community. An activity concentration of 1 pCi/g for the nuclides was entered as the source term. The radial dimension of the cylindrical source was 28 cm, the depth was 15 cm, and the dose point above the surface was 10 cm with a soil density of 1.6 g/cm<sup>3</sup>. The instrument efficiency when scanning,  $E_i$ , is the product of the modeled exposure rate (MicroShield™) in mRhr<sup>-1</sup>/pCi/g for and the energy response factor in cpm/mR/hr as derived from the energy response curve provided by Eberline Instruments (Appendix O). Table 5.1 demonstrates the derived efficiencies for the major gamma emitting isotopes listed in Table 3.1.

TABLE 5.1  
Energy Response and Efficiency for Photon Emitting Isotopes

| Isotope | Calculations for $E_i$   | $E_i$<br>(cpm/pCi/g) |
|---------|--------------------------|----------------------|
|         | See appendix A through L |                      |
| Co-60   | See Appendix A and B     | 379                  |
| Nb-94   | See Appendix C and D     | 416                  |
| Ag-108m | See Appendix E and F     | 637                  |
| Sb-125  | See Appendix G and H     | 210                  |
| Cs-134  | See Appendix I and J     | 506                  |
| Cs-137  | See Appendix K and L     | 188                  |
| Eu-152  | See Appendix M and N     | 344                  |

When performing gamma scan measurements on soil surfaces the effective source to detector geometry is as close as is reasonably possible (less than 3 inches).

### 6.0 Applying Efficiency Corrections Based on the Effects of Field Conditions for Total Efficiency:

The total efficiency for any given condition can now be calculated from the product of the instrument efficiency  $\epsilon_i$  and the source efficiency  $\epsilon_s$ .

$$\epsilon_{tot} = \epsilon_i \times \epsilon_s$$

The following example illustrates the process of determining total efficiency. For this example we will assume the following:

- Surface activity readings need to be made in the Primary Auxiliary Building (PAB) on the concrete wall surfaces using the E-600 and C-100 gas proportional detector.
- Data obtained from characterization results from the PAB indicate the presence of beta emitters with energies greater than 0.400 Mev.
- The source (activity on wall) to detector distance is 1.27 cm (0.5 in detector stand off). To calculate the total efficiency,  $\epsilon_{tot}$ , refer to Table 4.2 "Source to Detector Distance Effects on Instrument Efficiencies for  $\alpha$ -  $\beta$  Emitters" to obtain the appropriate  $\epsilon_s$  value.
- Contamination on all surfaces is distributed relative to the effective detector area.

- When performing fixed point measurements with gas proportional instrumentation the effective source to detector geometry is representative of the calibrated geometries listed in Table 4.2 “Source to Detector Distance Effects on Instrument Efficiencies for  $\alpha$ -  $\beta$  Emitters”.
- Corrections for temperature and pressure are not substantial.

In this example, the value for  $\epsilon_i$  is 0.2413 as depicted in Table 4.2 “Source to Detector Distance Effects on Instrument Efficiencies for  $\alpha$ -  $\beta$  Emitters”. The  $\epsilon_s$  value of 0.5 is chosen refer to Table 4.3 “Source Efficiencies as listed in ISO 7503-1”. Therefore the total efficiency for this condition becomes  $\epsilon_{tot} = \epsilon_i \times \epsilon_s = 0.2413 \times 0.5 = 0.121$  or 12.1%.

### 7.0 Conclusion:

Field conditions may significantly influence the usefulness of a survey instrument. When applying the instrument and source efficiencies in MDC calculations, field conditions must be considered. Tables have been constructed to assist in the selection of appropriate instrument and source efficiencies. Table 4.2 “Source to Detector Distance Effects on Instrument Efficiencies for  $\alpha$ - $\beta$  Emitters” lists instrument efficiencies ( $\epsilon_i$ ) at various source to detector distances for alpha and beta emitters. The appropriate  $\epsilon_i$  value should be applied, accounting for the field condition, i.e. the relation between the detector and the surface to be measured.

Source efficiencies shall be selected from Table 4.3 “Source Efficiencies as listed in ISO 7503-1”. This table lists conservative  $\epsilon_s$  values that correct for self-absorption and attenuation of surface activity.

Table 5.1 “Energy Response and Efficiency for Photon Emitting Isotopes” lists  $E_i$  values that apply to scanning MDC calculations. The Microshield™ model code was used to determine instrument efficiency assuming contamination conditions and detector geometry cited in section 5.6.2.4.4 “MDCs for Gamma Scans of Land Areas” of the License Termination Plan [8.6].

Detector and source conditions equivalent to those modeled herein may directly apply to the results of this report.

## 8.0 References

- 8.1 NUREG-1507, "Minimum Detectable Concentrations with Typical Radiation Survey Instruments for Various Contaminants and Field Conditions," 1998
- 8.2 ISO 7503-1, "Evaluation of Surface Contamination – Part I: Beta Emitters and Alpha Emitters," 1988-08-01.
- 8.3 ISO 8769, "Reference Sources for the Calibration of Surface Contamination Monitors- Beta-emitters (maximum beta energy greater 0.15MeV) and Alpha-emitters," 1988-06-15.
- 8.4 "Radiological Health Handbook," Revised Edition 1970.
- 8.5 DP-8534, "Operation and source Checks of Portable Friskers".
- 8.6 Yankee Nuclear Plant Site License Termination Plan, Rev.0, November 2003.

# APPENDIX A

## MicroShield v6.02 (6.02-00253)

**Page** : 1  
**DOS File** : SPA3-EFF-Co-60.ms6  
**Run Date** : September 10, 2004  
**Run Time** : 8:56:50 AM  
**Duration** : 00:00:00

**File Ref** :  
**Date** :  
**By** :  
**Checked** :

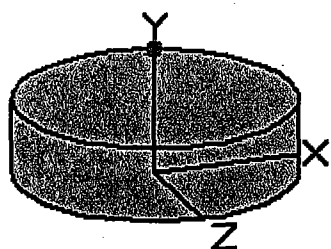
**Case Title:** SPA3-EFF-Co-60  
**Description:** SPA-3 Soil scan - 28 cm radius 1pCi/cm<sup>3</sup> Co-60  
**Geometry:** 8 - Cylinder Volume - End Shields

**Source Dimensions:**

|               |         |           |
|---------------|---------|-----------|
| <b>Height</b> | 15.0 cm | (5.9 in)  |
| <b>Radius</b> | 28.0 cm | (11.0 in) |

**Dose Points**

|     | A    | X      | Y     | Z      |
|-----|------|--------|-------|--------|
| # 1 | 0 cm | 0.0 in | 25 cm | 9.8 in |
|     |      |        | 0 cm  | 0.0 in |



**Shields**

| Shield N | Dimension                | Material | Density |
|----------|--------------------------|----------|---------|
| Source   | 3.69e+04 cm <sup>3</sup> | Concrete | 1.6     |
| Air Gap  |                          | Air      | 0.00122 |

| Nuclide | Source Input : Grouping Method - Actual Photon Energies |             |                     |                    |
|---------|---|-------------|---------------------|--------------------|
|         | curies  | becquerels  | μCi/cm <sup>3</sup> | Bq/cm <sup>3</sup> |
| Co-60   | 3.6945e-008   | 1.3670e+003 | 1.0000e-006         | 3.7000e-002        |

**Buildup : The material reference is - Source Integration Parameters**

|                     |    |
|---------------------|----|
| Radial              | 20 |
| Circumferential     | 10 |
| Y Direction (axial) | 10 |

| Energy MeV    | Activity Photons/sec | Fluence Rate MeV/cm <sup>2</sup> /sec |                  | Exposure Rate mR/hr |                  |
|---------------|----------------------|---------------------------------------|------------------|---------------------|------------------|
|               |                      | No Buildup                            | With Buildup     | No Buildup          | With Buildup     |
| 0.6938        | 2.230e-01            | 9.055e-06                             | 1.590e-05        | 1.748e-08           | 3.070e-08        |
| 1.1732        | 1.367e+03            | 1.098e-01                             | 1.669e-01        | 1.962e-04           | 2.982e-04        |
| 1.3325        | 1.367e+03            | 1.293e-01                             | 1.904e-01        | 2.244e-04           | 3.303e-04        |
| <b>Totals</b> | <b>2.734e+03</b>     | <b>2.391e-01</b>                      | <b>3.573e-01</b> | <b>4.205e-04</b>    | <b>6.286e-04</b> |

## APPENDIX B

| <b>Co-60</b>   |            |            |                              |                             |                            |
|--|------------|------------|------------------------------|-----------------------------|----------------------------|
| <b>Microsoft Excel E<sub>i</sub> Calculation Sheet</b> |            |            |                              |                             |                            |
|  | Energy MeV | Energy keV | Exposure Rate (mR/hr-µpCi/g) | Energy Response (cpm/mR/hr) | E <sub>i</sub> (cpm/µCi/g) |
| 694  | 0.6938     | 694        | 3.07E-03                     | 1112.630                    | 0                          |
| 1173   | 1.1732     | 1173       | 2.98E-04                     | 660.557                     | 197                        |
| 1333   | 1.3325     | 1333       | 3.30E-04                     | 552.233                     | 182                        |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| 0  |            | 0          |                              |                             | 0                          |
| <b>(E<sub>i</sub>) Total:</b>                          |            |            |                              |                             | <b>379</b>                 |

# APPENDIX C

## MicroShield v6.02 (6.02-00253)

**Page** : 1  
**DOS File** : SPA3-EFF-Nb-94.ms6  
**Run Date** : September 16, 2004  
**Run Time** : 3:22:38 PM  
**Duration** : 00:00:00

**File Ref** :  
**Date** :  
**By** :  
**Checked** :

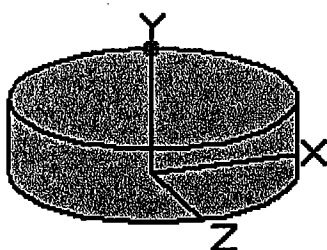
**Case Title:** SPA3-EFF-Nb-94  
**Description:** SPA-3 Soil scan - 28 cm radius 1pCi/cm3 Nb-94  
**Geometry:** 8 - Cylinder Volume - End Shields

**Source Dimensions:**

|               |         |           |
|---------------|---------|-----------|
| <b>Height</b> | 15.0 cm | (5.9 in)  |
| <b>Radius</b> | 28.0 cm | (11.0 in) |

**Dose Points**

|     | A      | X      | Y      | Z      |
|-----|--------|--------|--------|--------|
| # 1 | 0 cm   | 25 cm  | 0 cm   | 0 cm   |
|     | 0.0 in | 9.8 in | 0.0 in | 0.0 in |



**Shields**

| Shield N | Dimension                | Material | Density |
|----------|--------------------------|----------|---------|
| Source   | 3.69e+04 cm <sup>3</sup> | Concrete | 1.6     |
| Air Gap  |                          | Air      | 0.00122 |

**Source Input : Grouping Method - Actual Photon Energies**

| Nuclide | curies      | becquerels  | μCi/cm <sup>3</sup> | Bq/cm <sup>3</sup> |
|---------|-------------|-------------|---------------------|--------------------|
| Nb-94   | 3.6945e-008 | 1.3670e+003 | 1.0000e-006         | 3.7000e-002        |

**Buildup : The material reference is - Source Integration Parameters**

|                     |    |
|---------------------|----|
| Radial              | 20 |
| Circumferential     | 10 |
| Y Direction (axial) | 10 |

**Results**

| Energy MeV    | Activity Photons/sec | Fluence Rate MeV/cm <sup>2</sup> /sec |                  | Exposure Rate mR/hr |                  |
|---------------|----------------------|---------------------------------------|------------------|---------------------|------------------|
|               |                      | No Buildup                            | With Buildup     | No Buildup          | With Buildup     |
| 0.0023        | 9.067e-02            | 1.391e-10                             | 1.430e-10        | 1.861e-10           | 1.913e-10        |
| 0.0174        | 4.834e-01            | 8.762e-09                             | 9.129e-09        | 4.729e-10           | 4.927e-10        |
| 0.0175        | 9.260e-01            | 1.719e-08                             | 1.792e-08        | 9.104e-10           | 9.491e-10        |
| 0.0196        | 2.720e-01            | 7.924e-09                             | 8.356e-09        | 2.925e-10           | 3.085e-10        |
| 0.7026        | 1.367e+03            | 5.643e-02                             | 9.872e-02        | 1.088e-04           | 1.904e-04        |
| 0.8711        | 1.367e+03            | 7.464e-02                             | 1.228e-01        | 1.405e-04           | 2.312e-04        |
| <b>Totals</b> | <b>2.736e+03</b>     | <b>1.311e-01</b>                      | <b>2.216e-01</b> | <b>2.493e-04</b>    | <b>4.216e-04</b> |





# APPENDIX E

## MicroShield v6.02 (6.02-00253)

**Page** :1  
**DOS File** :SPA3-EFF-Ag-108m.ms6  
**Run Date** : September 16, 2004  
**Run Time** : 3:30:40 PM  
**Duration** : 00:00:00

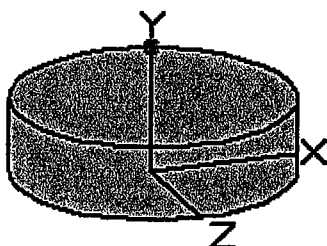
**File Ref** :  
**Date** :  
**By** :  
**Checked** :

**Case Title:** SPA3-EFF-Ag-108m  
**Description:** SPA-3 Soil scan - 28 cm radius 1pCi/cm3 Ag-108m  
**Geometry:** 8 - Cylinder Volume - End Shields

**Source Dimensions:**  
 Height 15.0 cm (5.9 in)  
 Radius 28.0 cm (11.0 in)

**Dose Points**  

| A   | X              | Y               | Z              |
|-----|----------------|-----------------|----------------|
| # 1 | 0 cm<br>0.0 in | 25 cm<br>9.8 in | 0 cm<br>0.0 in |



**Shields**  

| Shield N | Dimension                | Material | Density |
|----------|--------------------------|----------|---------|
| Source   | 3.69e+04 cm <sup>3</sup> | Concrete | 1.6     |
| Air Gap  |                          | Air      | 0.00122 |

**Source Input : Grouping Method - Actual Photon Energies**

| Nuclide | curies      | becquerels  | μCi/cm <sup>3</sup> | Bq/cm <sup>3</sup> |
|---------|-------------|-------------|---------------------|--------------------|
| Ag-108m | 3.6945e-008 | 1.3670e+003 | 1.0000e-006         | 3.7000e-002        |

**Buildup : The material reference is - Source Integration Parameters**

|                     |    |
|---------------------|----|
| Radial              | 20 |
| Circumferential     | 10 |
| Y Direction (axial) | 10 |

| Energy MeV    | Activity Photons/sec | Fluence Rate                        |                                       | Exposure Rate    |                    |
|---------------|----------------------|-------------------------------------|---------------------------------------|------------------|--------------------|
|               |                      | MeV/cm <sup>2</sup> /sec No Buildup | MeV/cm <sup>2</sup> /sec With Buildup | mR/hr No Buildup | mR/hr With Buildup |
| 0.0028        | 6.580e+01            | 1.252e-07                           | 1.287e-07                             | 1.351e-07        | 1.388e-07          |
| 0.003         | 7.853e+00            | 1.568e-08                           | 1.612e-08                             | 1.612e-08        | 1.657e-08          |
| 0.021         | 2.491e+02            | 9.534e-06                           | 1.015e-05                             | 2.824e-07        | 3.007e-07          |
| 0.0212        | 4.727e+02            | 1.862e-05                           | 1.985e-05                             | 5.389e-07        | 5.744e-07          |
| 0.022         | 7.024e+00            | 3.202e-07                           | 3.434e-07                             | 8.233e-09        | 8.831e-09          |
| 0.0222        | 1.330e+01            | 6.251e-07                           | 6.714e-07                             | 1.568e-08        | 1.685e-08          |
| 0.0238        | 1.501e+02            | 9.273e-06                           | 1.010e-05                             | 1.863e-07        | 2.029e-07          |
| 0.0249        | 4.289e+00            | 3.145e-07                           | 3.464e-07                             | 5.492e-09        | 6.050e-09          |
| 0.0304        | 2.902e-04            | 4.431e-11                           | 5.248e-11                             | 4.230e-13        | 5.010e-13          |
| 0.0792        | 9.687e+01            | 2.008e-04                           | 4.802e-04                             | 3.190e-07        | 7.629e-07          |
| 0.4339        | 1.229e+03            | 2.705e-02                           | 5.514e-02                             | 5.294e-05        | 1.079e-04          |
| 0.6144        | 1.236e+03            | 4.282e-02                           | 7.808e-02                             | 8.347e-05        | 1.522e-04          |
| 0.7229        | 1.237e+03            | 5.300e-02                           | 9.194e-02                             | 1.019e-04        | 1.768e-04          |
| <b>Totals</b> | <b>4.768e+03</b>     | <b>1.231e-01</b>                    | <b>2.257e-01</b>                      | <b>2.398e-04</b> | <b>4.389e-04</b>   |





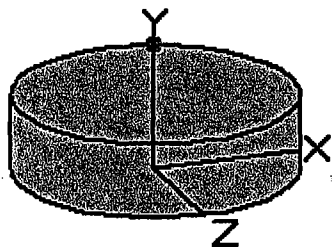
# APPENDIX G

MicroShield v6.02 (6.02-00253)

Page : 1  
 DOS File : SPA3-EFF-Sb-125.ms6  
 Run Date : September 16, 2004  
 Run Time : 3:34:07 PM  
 Duration : 00:00:00

File Ref :  
 Date :  
 By :  
 Checked :

**Case Title: SPA3-EFF-Sb-125**  
**Description: SPA-3 Soil scan - 28 cm radius 1pCi/cm3 Sb-125**  
**Geometry: 8 - Cylinder Volume - End Shields**



**Source Dimensions:**  
 Height 15.0 cm (5.9 in)  
 Radius 28.0 cm (11.0 in)

**Dose Points**

| A   | X              | Y               | Z              |
|-----|----------------|-----------------|----------------|
| # 1 | 0 cm<br>0.0 in | 25 cm<br>9.8 in | 0 cm<br>0.0 in |

**Shields**

| Shield N | Dimension                | Material | Density |
|----------|--------------------------|----------|---------|
| Source   | 3.69e+04 cm <sup>3</sup> | Concrete | 1.6     |
| Air Gap  |                          | Air      | 0.00122 |

Source Input : Grouping Method - Actual Photon Energies

| Nuclide | curies      | Becquerels  | μCi/cm <sup>3</sup> | Bq/cm <sup>3</sup> |
|---------|-------------|-------------|---------------------|--------------------|
| Sb-125  | 3.6945e-008 | 1.3670e+003 | 1.0000e-006         | 3.7000e-002        |

Buildup : The material reference is - Source  
 Integration Parameters

|                     |    |
|---------------------|----|
| Radial              | 20 |
| Circumferential     | 10 |
| Y Direction (axial) | 10 |

### Results

| Energy MeV    | Activity Photons/sec | Fluence Rate MeV/cm <sup>2</sup> /sec No Buildup | Fluence Rate MeV/cm <sup>2</sup> /sec |                  | Exposure Rate mR/hr |              |
|---------------|----------------------|--|---------------------------------------|------------------|---------------------|--------------|
|               |                      |  | With Buildup                          | No Buildup       | No Buildup          | With Buildup |
| 0.0038        | 6.762e+01            | 1.708e-07  | 1.756e-07                             | 1.388e-07        | 1.427e-07           |              |
| 0.0272        | 1.748e+02            | 1.785e-05  | 2.020e-05                             | 2.376e-07        | 2.689e-07           |              |
| 0.0275        | 3.262e+02            | 3.453e-05  | 3.922e-05                             | 4.461e-07        | 5.067e-07           |              |
| 0.031         | 1.132e+02            | 1.857e-05  | 2.221e-05                             | 1.670e-07        | 1.997e-07           |              |
| 0.0355        | 5.693e+01            | 1.492e-05  | 1.918e-05                             | 9.090e-08        | 1.169e-07           |              |
| 0.117         | 3.568e+00            | 1.380e-05  | 3.715e-05                             | 2.146e-08        | 5.778e-08           |              |
| 0.159         | 9.531e-01            | 5.634e-06  | 1.499e-05                             | 9.416e-09        | 2.505e-08           |              |
| 0.1726        | 2.478e+00            | 1.634e-05  | 4.295e-05                             | 2.787e-08        | 7.326e-08           |              |
| 0.1763        | 9.422e+01            | 6.392e-04  | 1.674e-03                             | 1.096e-06        | 2.870e-06           |              |
| 0.2041        | 4.410e+00            | 3.630e-05  | 9.230e-05                             | 6.435e-08        | 1.636e-07           |              |
| 0.2081        | 3.324e+00            | 2.805e-05  | 7.103e-05                             | 4.994e-08        | 1.264e-07           |              |
| 0.2279        | 1.796e+00            | 1.708e-05  | 4.229e-05                             | 3.098e-08        | 7.670e-08           |              |
| 0.321         | 5.701e+00            | 8.474e-05  | 1.899e-04                             | 1.620e-07        | 3.632e-07           |              |
| 0.3804        | 2.045e+01            | 3.792e-04  | 8.052e-04                             | 7.364e-07        | 1.564e-06           |              |
| 0.408         | 2.486e+00            | 5.051e-05  | 1.049e-04                             | 9.853e-08        | 2.047e-07           |              |
| 0.4279        | 4.009e+02            | 8.668e-03  | 1.774e-02                             | 1.695e-05        | 3.470e-05           |              |
| 0.4435        | 4.130e+00            | 9.356e-05  | 1.894e-04                             | 1.832e-07        | 3.709e-07           |              |
| 0.4634        | 1.415e+02            | 3.395e-03  | 6.781e-03                             | 6.658e-06        | 1.330e-05           |              |
| 0.6006        | 2.430e+02            | 8.174e-03  | 1.501e-02                             | 1.595e-05        | 2.930e-05           |              |
| 0.6066        | 6.864e+01            | 2.340e-03  | 4.283e-03                             | 4.564e-06        | 8.355e-06           |              |
| 0.6359        | 1.548e+02            | 5.609e-03  | 1.012e-02                             | 1.091e-05        | 1.967e-05           |              |
| 0.6714        | 2.478e+01            | 9.640e-04  | 1.710e-03                             | 1.867e-06        | 3.311e-06           |              |
| <b>Totals</b> | <b>1.916e+03</b>     | <b>3.060e-02</b>                                 | <b>5.901e-02</b>                      | <b>6.046e-05</b> | <b>1.158e-04</b>    |              |

# APPENDIX H

## Sb-125

| Energy MeV | Energy keV | Exposure Rate<br>(mR/hr) / (µCi/g) | Energy Response<br>(cpm/mR/h) | Et (cpm/µCi/g) |
|------------|------------|------------------------------------|-------------------------------|----------------|
| 4          | 0.0038     | 1.43E-07                           | 6.618312                      | 0              |
| 27         | 0.0272     | 2.69E-07                           | 510.290                       | 0              |
| 28         | 0.0275     | 5.07E-07                           | 554.334                       | 0              |
| 31         | 0.031      | 2.00E-07                           | 1.219.281                     | 0              |
| 36         | 0.0355     | 1.17E-07                           | 2.418.948                     | 0              |
| 117        | 0.117      | 5.78E-08                           | 9.167.000                     | 1              |
| 159        | 0.159      | 2.51E-08                           | 8917.000                      | 0              |
| 173        | 0.1726     | 7.33E-08                           | 6859.000                      | 1              |
| 176        | 0.1763     | 2.87E-06                           | 61926.00                      | 18             |
| 204        | 0.2041     | 1.64E-07                           | 6011.300                      | 1              |
| 208        | 0.2081     | 1.26E-07                           | 4073.050                      | 1              |
| 228        | 0.2279     | 7.67E-08                           | 3110.500                      | 0              |
| 321        | 0.321      | 3.63E-07                           | 3000.500                      | 1              |
| 380        | 0.3804     | 0.000001564                        | 2348.000                      | 4              |
| 408        | 0.408      | 2.047E-07                          | 2155.800                      | 0              |
| 428        | 0.4279     | 0.0000647                          | 2083.165                      | 72             |
| 444        | 0.4435     | 3.709E-07                          | 2026.225                      | 1              |
| 463        | 0.4634     | 0.0000133                          | 1953.590                      | 26             |
| 601        | 0.6006     | 0.0000293                          | 1452.810                      | 43             |
| 607        | 0.6066     | 0.000008355                        | 1430.910                      | 12             |
| 636        | 0.6359     | 0.00001967                         | 1323.965                      | 26             |
| 671        | 0.6714     | 0.000003311                        | 1194.390                      | 4              |
| 0          | 0          |                                    |                               | 0              |
| 0          | 0          |                                    |                               | 0              |
| 0          | 0          |                                    |                               | 0              |
| 0          | 0          |                                    |                               | 0              |
| 0          | 0          |                                    |                               | 0              |
| 0          | 0          |                                    |                               | 0              |
| 0          | 0          |                                    |                               | 0              |
| 0          | 0          |                                    |                               | 0              |

**(E) Total: 210**

# APPENDIX I

## MicroShield v6.02 (6.02-00253)

Page :1  
 DOS File :SPA3-EFF-Cs-134.ms6  
 Run Date : September 16, 2004  
 Run Time : 3:39:09 PM  
 Duration : 00:00:00

File Ref :  
 Date :  
 By :  
 Checked :

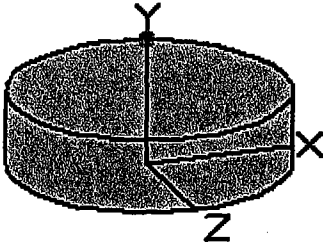
**Case Title: SPA3-EFF-Cs-134**  
**Description: SPA-3 Soil scan - 28 cm radius 1pCi/cm<sup>3</sup> Cs-134**  
**Geometry: 8 - Cylinder Volume - End Shields**

**Source Dimensions:**

Height 15.0 cm (5.9 in)  
 Radius 28.0 cm (11.0 in)

**Dose Points**

| A   | X              | Y               | Z              |
|-----|----------------|-----------------|----------------|
| # 1 | 0 cm<br>0.0 in | 25 cm<br>9.8 in | 0 cm<br>0.0 in |



**Shields**

| Shield N | Dimension                | Material | Density |
|----------|--------------------------|----------|---------|
| Source   | 3.69e+04 cm <sup>3</sup> | Concrete | 1.6     |
| Air Gap  |                          | Air      | 0.00122 |

**Source Input : Grouping Method - Actual Photon Energies**

| Nuclide | curies      | becquerels  | μCi/cm <sup>3</sup> | Bq/cm <sup>3</sup> |
|---------|-------------|-------------|---------------------|--------------------|
| Cs-134  | 3.6945e-008 | 1.3670e+003 | 1.0000e-006         | 3.7000e-002        |

**Buildup : The material reference is - Source Integration Parameters**

|                     |    |
|---------------------|----|
| Radial              | 20 |
| Circumferential     | 10 |
| Y Direction (axial) | 10 |

**Results**

| Energy MeV    | Activity Photons/sec | Fluence Rate                           | Fluence Rate                             | Exposure Rate       | Exposure Rate         |
|---------------|----------------------|--|--|---------------------|-----------------------|
|               |                      | MeV/cm <sup>2</sup> /sec<br>No Buildup | MeV/cm <sup>2</sup> /sec<br>With Buildup | mR/hr<br>No Buildup | mR/hr<br>With Buildup |
| 0.0045        | 1.222e+00            | 3.658e-09                              | 3.760e-09                                | 2.507e-09           | 2.577e-09             |
| 0.0318        | 2.931e+00            | 5.271e-07                              | 6.386e-07                                | 4.391e-09           | 5.320e-09             |
| 0.0322        | 5.407e+00            | 1.014e-06                              | 1.236e-06                                | 8.157e-09           | 9.943e-09             |
| 0.0364        | 1.968e+00            | 5.611e-07                              | 7.321e-07                                | 3.188e-09           | 4.160e-09             |
| 0.2769        | 4.839e-01            | 5.931e-06                              | 1.391e-05                                | 1.113e-08           | 2.610e-08             |
| 0.4753        | 1.996e+01            | 4.950e-04                              | 9.808e-04                                | 9.712e-07           | 1.924e-06             |
| 0.5632        | 1.146e+02            | 3.545e-03                              | 6.648e-03                                | 6.940e-06           | 1.302e-05             |
| 0.5693        | 2.109e+02            | 6.619e-03                              | 1.237e-02                                | 1.295e-05           | 2.421e-05             |
| 0.6047        | 1.334e+03            | 4.529e-02                              | 8.300e-02                                | 8.836e-05           | 1.619e-04             |
| 0.7958        | 1.167e+03            | 5.668e-02                              | 9.564e-02                                | 1.079e-04           | 1.820e-04             |
| 0.8019        | 1.193e+02            | 5.852e-03                              | 9.853e-03                                | 1.113e-05           | 1.874e-05             |
| 1.0386        | 1.367e+01            | 9.377e-04                              | 1.472e-03                                | 1.717e-06           | 2.696e-06             |
| 1.1679        | 2.461e+01            | 1.964e-03                              | 2.990e-03                                | 3.514e-06           | 5.349e-06             |
| 1.3652        | 4.156e+01            | 4.055e-03                              | 5.936e-03                                | 6.993e-06           | 1.024e-05             |
| <b>Totals</b> | <b>3.058e+03</b>     | <b>1.254e-01</b>                       | <b>2.189e-01</b>                         | <b>2.405e-04</b>    | <b>4.202e-04</b>      |





# APPENDIX K

## MicroShield v6.02 (6.02-00253)

**Page** :1  
**DOS File** :SPA3-EFF-Cs-137.ms6  
**Run Date** : September 10, 2004  
**Run Time** : 8:52:18 AM  
**Duration** : 00:00:00

**File Ref** :  
**Date** :  
**By** :  
**Checked** :

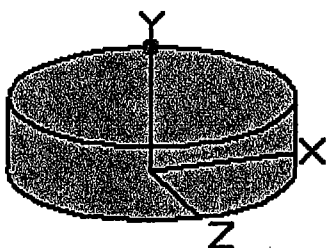
**Case Title:** SPA3-EFF-Cs-137  
**Description:** SPA-3 Soil scan - 28 cm radius 1pCi/cm<sup>3</sup> Cs-137 and Daughters  
**Geometry:** 8 - Cylinder Volume - End Shields

### Source Dimensions:

|               |         |           |
|---------------|---------|-----------|
| <b>Height</b> | 15.0 cm | (5.9 in)  |
| <b>Radius</b> | 28.0 cm | (11.0 in) |

### Dose Points

| A   | X              | Y               | Z              |
|-----|----------------|-----------------|----------------|
| # 1 | 0 cm<br>0.0 in | 25 cm<br>9.8 in | 0 cm<br>0.0 in |



### Shields

| Shield N | Dimension                | Material | Density |
|----------|--------------------------|----------|---------|
| Source   | 3.69e+04 cm <sup>3</sup> | Concrete | 1.6     |
| Air Gap  |                          | Air      | 0.00122 |

### Source Input : Grouping Method - Actual Photon Energies

| Nuclide | curies      | becquerels  | μCi/cm <sup>3</sup> | Bq/cm <sup>3</sup> |
|---------|-------------|-------------|---------------------|--------------------|
| Ba-137m | 3.4950e-008 | 1.2932e+003 | 9.4600e-007         | 3.5002e-002        |
| Cs-137  | 3.6945e-008 | 1.3670e+003 | 1.0000e-006         | 3.7000e-002        |

### Buildup : The material reference is - Source Integration Parameters

|                     |    |
|---------------------|----|
| Radial              | 20 |
| Circumferential     | 10 |
| Y Direction (axial) | 10 |

### Results

| Energy MeV    | Activity Photons/sec | Fluence Rate MeV/cm <sup>2</sup> /sec No Buildup | Fluence Rate MeV/cm <sup>2</sup> /sec With Buildup | Exposure Rate mR/hr No Buildup | Exposure Rate mR/hr With Buildup |
|---------------|----------------------|--|--|--------------------------------|----------------------------------|
| 0.0045        | 1.342e+01            | 4.020e-08  | 4.133e-08  | 2.755e-08                      | 2.833e-08                        |
| 0.0318        | 2.677e+01            | 4.815e-06  | 5.834e-06  | 4.011e-08                      | 4.860e-08                        |
| 0.0322        | 4.939e+01            | 9.260e-06  | 1.129e-05  | 7.452e-08                      | 9.084e-08                        |
| 0.0364        | 1.797e+01            | 5.126e-06  | 6.688e-06  | 2.912e-08                      | 3.800e-08                        |
| 0.6616        | 1.164e+03            | 4.442e-02  | 7.913e-02  | 8.611e-05                      | 1.534e-04                        |
| <b>Totals</b> | <b>1.271e+03</b>     | <b>4.444e-02</b>                                 | <b>7.915e-02</b>                                   | <b>8.628e-05</b>               | <b>1.536e-04</b>                 |

# APPENDIX L

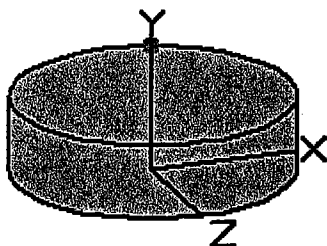
| Cs-137                              |            |            |                                    |                               |               |
|-------------------------------------|------------|------------|------------------------------------|-------------------------------|---------------|
| Microsoft Excel E Calculation Sheet |            |            |                                    |                               |               |
|                                     | Energy MeV | Energy keV | Exposure Rate<br>(mR/hr<br>1pCi/g) | Energy Response<br>(cpm/mR/h) | E (cpm/pCi/g) |
| 5                                   | 0.0045     | 5          | 2.83E-08                           |                               | 0             |
| 32                                  | 0.0318     | 32         | 4.86E-08                           | 1,406.947                     | 0             |
| 32                                  | 0.0322     | 32         | 9.08E-08                           | 1,505.273                     | 0             |
| 36                                  | 0.0364     | 36         | 3.80E-08                           | 2,696.122                     | 0             |
| 662                                 | 0.6616     | 662        | 1.53E-04                           | 1,228.700                     | 188           |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| 0                                   | 0          | 0          |                                    |                               | 0             |
| <b>(E<sub>i</sub>) Total:</b>       |            |            |                                    |                               | <b>188</b>    |

# APPENDIX M

MicroShield v6.02 (6.02-00253)

|          |                      |          |   |
|----------|----------------------|----------|---|
| Page     | :1                   | File Ref | : |
| DOS File | :SPA3-EFF-Eu-152.ms6 | Date     | : |
| Run Date | : October 7, 2004    | By       | : |
| Run Time | : 11:25:11 AM        | Checked  | : |
| Duration | : 00:00:00           |          |   |

Case Title: SPA-3-EFF-Eu-152  
 Description: SPA-3 Soil scan - 28cm radius 1 pCi/cm<sup>3</sup> Eu-152  
 Geometry: 8 - Cylinder Volume - End Shields



**Source Dimensions:**

|        |         |           |
|--------|---------|-----------|
| Height | 15.0 cm | (5.9 in)  |
| Radius | 28.0 cm | (11.0 in) |

**Dose Points**

| A   | X              | Y               | Z              |
|-----|----------------|-----------------|----------------|
| # 1 | 0 cm<br>0.0 in | 25 cm<br>9.8 in | 0 cm<br>0.0 in |

**Shields**

| Shield N | Dimension                | Material | Density |
|----------|--------------------------|----------|---------|
| Source   | 3.69e+04 cm <sup>3</sup> | Concrete | 1.6     |
| Air Gap  |                          | Air      | 0.00122 |

Source Input : Grouping Method - Standard Indices  
 Number of Groups : 25  
 Lower Energy Cutoff : 0.015  
 Photons < 0.015 : Included  
 Library : Grove

| Nuclide | curies      | becquerels  | µCi/cm <sup>3</sup> | Bq/cm <sup>3</sup> |
|---------|-------------|-------------|---------------------|--------------------|
| Eu-152  | 3.6945e-008 | 1.3670e+003 | 1.0000e-006         | 3.7000e-002        |

Buildup : The material reference is - Source  
 Integration Parameters

|                     |    |
|---------------------|----|
| Radial              | 20 |
| Circumferential     | 10 |
| Y Direction (axial) | 10 |

**Results**

| Energy MeV    | Activity Photons/sec | Fluence Rate MeV/cm <sup>2</sup> /sec No Buildup | Fluence Rate MeV/cm <sup>2</sup> /sec With Buildup | Exposure Rate mR/hr No Buildup | Exposure Rate mR/hr With Buildup |
|---------------|----------------------|--|--|--------------------------------|----------------------------------|
| 0.015         | 2.077e+02            | 2.087e-06  | 2.146e-06  | 1.790e-07                      | 1.841e-07                        |
| 0.04          | 8.088e+02            | 3.131e-04  | 4.331e-04  | 1.385e-06                      | 1.916e-06                        |
| 0.05          | 2.022e+02            | 1.507e-04  | 2.467e-04  | 4.014e-07                      | 6.572e-07                        |
| 0.1           | 3.887e+02            | 1.189e-03  | 3.118e-03  | 1.819e-06                      | 4.770e-06                        |
| 0.2           | 1.024e+02            | 8.207e-04  | 2.097e-03  | 1.448e-06                      | 3.700e-06                        |
| 0.3           | 3.696e+02            | 5.029e-03  | 1.151e-02  | 9.540e-06                      | 2.184e-05                        |
| 0.4           | 8.590e+01            | 1.701e-03  | 3.555e-03  | 3.314e-06                      | 6.926e-06                        |
| 0.5           | 7.711e+00            | 2.043e-04  | 3.984e-04  | 4.010e-07                      | 7.819e-07                        |
| 0.6           | 5.797e+01            | 1.948e-03  | 3.579e-03  | 3.802e-06                      | 6.985e-06                        |
| 0.8           | 2.434e+02            | 1.190e-02  | 2.005e-02  | 2.263e-05                      | 3.813e-05                        |
| 1.0           | 5.849e+02            | 3.820e-02  | 6.058e-02  | 7.042e-05                      | 1.117e-04                        |
| 1.5           | 3.171e+02            | 3.490e-02  | 4.999e-02  | 5.871e-05                      | 8.411e-05                        |
| <b>Totals</b> | <b>3.376e+03</b>     | <b>9.635e-02</b>                                 | <b>1.556e-01</b>                                   | <b>1.740e-04</b>               | <b>2.817e-04</b>                 |





APPENDIX O

Calculated Energy Response  
(Eberline Instruments)

CPM/mR/h

