



FPL Energy.

Duane Arnold Energy Center

November 3, 2006

FPL Energy Duane Arnold, LLC
3277 DAEC Road
Palo, Iowa 52324

NG-06-0733
10 CFR 50.55a

U.S. Nuclear Regulatory Commission
ATTN: Document Control Desk
Washington, DC 20555-0001

Duane Arnold Energy Center
Docket No: 50-331
Op. License No: DPR-49

Response To Request For Additional Information Related To Request For Relief
Concerning Flow Measurement For the Standby Liquid Control Pumps

References: 1) Letter dated September 28, 2006, "Request For Additional Information
Related To The Request For Relief Concerning Flow Measurement
For The Standby Liquid Control Pumps," (TAC NO. MD1844)
2) Letter to NRC from G. Van Middlesworth, "Fourth Ten-Year Interval
Inservice Testing Program Relief Requests," dated May 8, 2006

By letter dated September 28, 2006 (Reference 1), the NRC issued a request for additional information (RAI) related to the May 8, 2006 (Reference 2) request for relief concerning flow measurement for the Standby Liquid Control Pumps (Relief Request PR-03). Per discussions with the Staff on August 10, 2006, a response to this RAI is due within 30 days of receipt of the RAI. The RAI was received on October 5, 2006 (via e-mail). The requested additional information is contained in the Enclosure to this letter. Should you have any questions regarding this matter, please contact Steve Catron, Duane Arnold Energy Center Licensing Manager, at (319) 851-7234. This letter contains no new commitments or revisions to existing commitments.

Gary Van Middlesworth
Site Vice President, Duane Arnold Energy Center
FPL Energy Duane Arnold, LLC

Enclosure

cc: Administrator, Region III, USNRC
Project Manager, DAEC, USNRC
Resident Inspector, DAEC, USNRC

A001

ENCLOSURE

Response To Request For Additional Information Related To Request For Relief Concerning Flow Measurement For The Standby Liquid Control Pumps

NRC Question 1

Please provide isometric diagram of the Standby Liquid Control (SBLC) System including details such as the length of piping and system components.

FPL Energy Duane Arnold Response to Question 1

The following diagrams of the Standby Liquid Control System are included in Attachment 1 to this Enclosure:

ISO-HCB-002-01 Rev. 8
FSK-03959 Rev. 9
FSK-3960 Rev. 8
FSK-3963 Rev. 1
FSK-3989 Rev. 2
FSK-3990 Rev. 2
FSK-3991 Rev. 2
FSK-3992 Rev. 4
FSK-3993 Rev. 5
FSK-3734 Rev. 16

NRC Question 2

The licensee stated that portable ultrasonic flow meters were installed on the common SBLC pump discharge piping to determine the practicality of using later technology ultrasonic flow meters to measure flow. The flow meter transducers were installed at three different locations on the discharge piping. However, each location resulted in significantly different measured flow rates compared to the other locations and the test tank level method. Please provide the data on the measured flow rates at different locations using the ultrasonic flow meters and compare them to those using the test tank level method.

FPL Energy Duane Arnold Response to Question 2

In March 2006, during the performance of Surveillance Test Procedure (STP) "SBLC Pump Operability Test," portable ultrasonic flow meters were installed on the SBLC pump discharge piping to determine the practicality of using ultrasonic flow meters to measure flow per the ASME OM Code. The flowmeter transducers were installed at three different locations on the discharge piping (as identified on the Attachment 1 drawings FSK-03959, FSK-3963, and FSK-3960). A vendor representative was on-site to facilitate proper installation and setup of the

transducers and flow meters. The pump flow rate calculated using the change in tank level method of the STP was 28.7 gpm for the "A" SBLC pump. The reference value for the "A" pump is 28.8 gpm. The flow rate from each subsequent test is compared to this value. Because of the simplicity of this test method, 28.7 gpm is considered the correct baseline value. Following are the results of flow measurement at each of the locations using the portable ultrasonic flow meters.

Location 1:

The transducers at location 1 were originally set up in direct measurement mode. (In direct measurement mode the transducers are placed on opposite sides of the pipe and a signal is passed through the pipe and fluid from one transducer to the other in both directions.) This mode, which was recommended by the manufacturer, did not provide adequate signal strength. The flow meter was then reprogrammed and the transducers were reconfigured for reflective mode. (In reflective mode both transducers are installed on the same side of the pipe and the signal from each transducer is reflected off the opposite side of the pipe and into the other transducer.) This mode indicated adequate signal strength. Initial flow rate in this configuration was steady at 28.2 to 28.5 gpm. After several minutes running in this configuration the vendor representative added additional UT couplant to the transducer that had been moved earlier. Flow rate increased to 30 gpm following addition of couplant. The vendor representative then programmed into the flow meter the "T" in the flow path just upstream of the transducer. Resulting flow rate was about 31.2 gpm. No more changes were made to this flow meter.

Location 2:

The transducers for the flow meter mounted at location 2 were mounted and programmed for direct measurement. Following pump start, this flow meter read erratically between 20 and 26 gpm and occasionally indicated a faulted condition. It was judged that due to the location (only a few feet from where flow enters the test tank and on the same elevation and down stream of the throttle valve) there may be air in the pipe which caused the erratic flow rates and faults. The transducers were then moved to Location 3.

Location 3:

At location 3, the transducers were mounted for measurement in the reflective mode. Flow measured in this configuration was 27.5 gpm. In the judgement of the vendor representative, the lower flow rate was the result of the elbow just downstream of the transducers.

As can be seen from the flow variances between the location and the tank level method, the measured flow variance is much higher than would be desirable or acceptable. The flow variance is caused by the tight piping routing and minimal straight runs of piping.

NRC Question 3

Paragraph ISTB-3510(a) of the American Society of Mechanical Engineers Operation and Maintenance Code specifies that the flow rate determination shall be

accurate to within ± 2 percent actual. Please provide the flow rate determination methodology that meets this Code requirement. Also, include the correlation curve conversion from test tank level to water volume.

FPL Energy Duane Arnold Response to Question 3

SBLC pump flow rate is determined by measuring the time it takes for each pump to pump down at least 20 inches of test tank level. A graduated sight glass is used to determine tank level. A stopwatch, which is started when the meniscus passes through an inch mark on the sight glass and stopped when the meniscus passes through a second inch mark after at least 20 inches, is used to measure time. The change in tank level (in inches) is then divided by the elapsed time and multiplied by a conversion factor of 294 (gal·sec)/(in·min). This conversion factor is based on the inside diameter of the test tank (38 inches) and is calculated as follows:

$$\frac{\frac{\pi}{4} \cdot (38 \cdot \text{in})^2 \cdot \text{in}}{\text{in_of_tank}} \cdot \left(\frac{\text{ft}}{12 \cdot \text{in}} \right)^3 \cdot \frac{7.48 \cdot \text{gal}}{\text{ft}^3} \cdot \frac{60 \text{sec}}{\text{min}} = 294.555 \frac{\text{gal} \cdot \text{sec}}{\text{in} \cdot \text{min}}$$

The stopwatch used during this test has an accuracy of ± 0.2 sec/hour with typical elapsed time of 205 seconds. This corresponds to an accuracy in gallons per minute of:

$$\frac{.2 \cdot \text{sec}}{\text{hr}} \cdot \frac{\text{hr}}{3600 \cdot \text{sec}} \cdot \frac{20 \text{in}}{205 \cdot \text{sec}} \cdot 294.555 \frac{\text{gal} \cdot \text{sec}}{\text{in} \cdot \text{min}} = 1.597 \times 10^{-3} \frac{\text{gal}}{\text{min}}$$

Readability of the test tank sight glass is assumed to be ± 0.1 inches when the stopwatch is started and stopped. This corresponds to an accuracy in gallons per minute of:

$$\frac{.1 \cdot \text{in}}{205 \cdot \text{sec}} \cdot 294.555 \frac{\text{gal} \cdot \text{sec}}{\text{in} \cdot \text{min}} = 0.144 \frac{\text{gal}}{\text{min}}$$

Total accuracy of SBLC flow measurement is as follows:

$$A_{\text{SBLC_F}} := \sqrt{(.0015 \text{gpm})^2 + 2 \cdot (.144 \text{gpm})^2}$$

$$A_{\text{SBLC_F}} = 0.204 \text{gpm}$$

In percent of the reference value this corresponds to:

$$\frac{.204 \text{gpm}}{28.8 \text{gpm}} = 0.708 \%$$

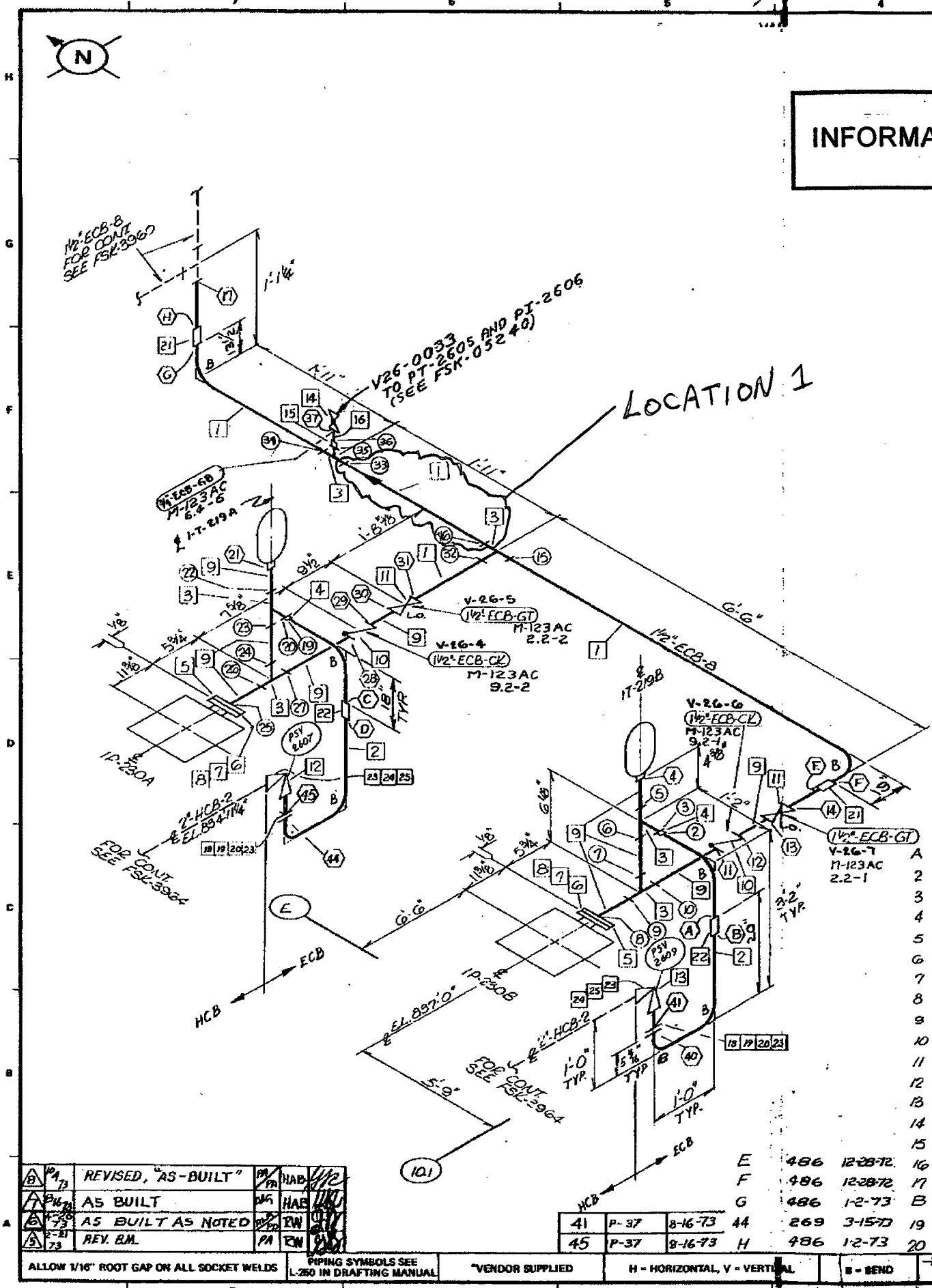
Since the portion of the test tank where the flow measurement is taken has a straight wall, the volume of water per inch of tank does not change as tank level changes. Therefore, the correlation curve of tank level versus tank volume would be a straight line. This correlation curve is not currently available. The change in level over measured time will be converted to flow rate using the formula (with the conversion factor of 294 (gal·sec)/(in·min)) as described in the original relief request submitted on May 8, 2006, and therefore, a correlation curve is not required. The correlation in terms of tank volume to level is 4.91 gal/inch. The tank level gage is 36 inches long, which allows for approximately 6 minutes of measured flow. Since the SBLC pumps are positive displacement pumps, suction and discharge parameters do not impact flow, and therefore, a minimum pump run time prior to testing is not required.

Attachment To Enclosure For Response To Request For Additional Information
Related To Request For Relief Concerning Flow Measurement
For the Standby Liquid Control Pumps

This Attachment contains the following diagrams:

ISO-HCB-002-01 Rev. 8
FSK-03959 Rev. 9
FSK-3960 Rev. 8
FSK-3963 Rev. 1
FSK-3989 Rev. 2
FSK-3990 Rev. 2
FSK-3991 Rev. 2
FSK-3992 Rev. 4
FSK-3993 Rev. 5
FSK-3734 Rev. 16

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INFORMATION ONLY

REVISED, "AS-BUILT"	PA	HA	12/2
AS BUILT	PA	HA	12/2
AS BUILT AS NOTED	PA	HA	12/2
REV. RM.	PA	HA	12/2

41	P-37	8-16-73	44	269	3-15-73	19	567	12-21-72	D	486	12-21-72
45	P-37	8-16-73	H	486	12-73	20	125	12-15-72	40	269	3-14-73

ALLOW 1/16" ROOT GAP ON ALL SOCKET WELDS PIPING SYMBOLS SEE L-250 IN DRAFTING MANUAL VENDOR SUPPLIED H - HORIZONTAL, V - VERTICAL B - BEND F.T.F. - FIELD TO FIT F.W. FIELD WELD


BILL OF MATERIAL						
QTY.	SIZE AND DESCRIPTION	ASTM	GR.	PC. No.	HEAT No.	
15'	1 1/2" PIPE SCH. 80S	A182	304	1	F4803	
12'	1" PIPE SCH. 80S	A182	304	2	F10710	
6	1 1/2" TEE 3000# S.W.	A-182	304	3	F11065	
2	1 1/2" x 1" RED. INSERT 3000# S.W.	A-182	304	4	F3584	
2	1 1/2" R.F. FLG. 600# S.W.	A182	316	5	F14587	
2	1 1/2" FLEXITALLIC GASKET TYPE CG			6		
8	3/4" x 4" LG. STUD BOLTS	A193	B7	7		
16	HEXHEAD NUTS 3/4"	A194	2H	8		
10	1 1/2" NIPPLE x 3/4" LG. SCH. 80S	A182	304	9	F4803	
2	1 1/2" ECB-CK 600# S.W.	A-182	316	10	92-142	
2	1 1/2" ECB-GT 600# S.W.	A-182	316	11	22-142	
1	2" x 1" PSV-2607			12		
1	2" x 1" PSV-2609			13		
1	3/4" ECB-GB 600# S.W.	A-182	316	14	64-6	
1	1 1/2" x 3/4" RED. INSERT 3000# S.W.	A182	304	15	F12921	
1	3/4" x 3/4" LG. NIPPLE SCH. 80S	A182	304	16	F3584	
4	1" 600# S.W. FLG.	A-182	F316	18	F15865	
2	1" FLEXIT - CG - GSKT			19		
8	3/4" x 3/4" LG. STUD	A-193	B7	20		
2	1 1/2" CPLG. 3000# S.W.	A-182	304	21	F12904	
2	1" CPLG. 3000# S.W.	A-182	304	22	F12904	
32	5/8" NUTS, HEX., SEMI. FIN.	A-194	2H	23		
2	2" FLEXIT - GSKT, CG			24		
16	4" x 5" - BOLTS 3/4" RF	A-193	B7	25		

QUALITY CONTROL DATA					
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REQ'D <input checked="" type="checkbox"/>	NOT REQ'D <input type="checkbox"/>	REQ'D <input checked="" type="checkbox"/>	NOT REQ'D <input type="checkbox"/>		
WELDING REQUIREMENTS: P37, P46, P547					
WELDING PROC.: PR-TAG R-11		WELDERS NAME: C125, P269, P470			
FILLER METAL: ER-308		WELDERS QUALIF.: P8-T-AG			
PREHEAT TEMP.: 60° min.		WELD No's REV. 5: 147, 198, 143, 145			
REV. 9: 445					
NONDESTRUCTIVE EXAM.					
VISUAL: DATE: 4-24-72, INITIAL: D.L.C.		RADIOGRAPHIC: DATE: 4-24-72, INITIAL: D.L.C.			
LIQUID PENET.: DATE: 4-24-72, INITIAL: D.L.C.		ULTRASONIC: DATE: 4-24-72, INITIAL: D.L.C.			
MAGN. PARTIAL: DATE: 4-24-72, INITIAL: D.L.C.		INSTALLATION INSPECTION			
INSTALL PER REV. 3: 147, 143, 145		CLEANLINESS: 12-21-72, 74A			
AS BUILT: 8-16-73, 74B		HANGER: 12-21-72, 74A			
HYDRO TEST		CERTIFIED CORRECT:			
CODE INSPECTOR:		HANGER DET. DWG:			
SHOP FAB'D <input checked="" type="checkbox"/> FIELD FAB'D <input type="checkbox"/>		START-UP No.: 53			
COST CODE:		INSUL. CL.: THICK:			
P & I Dwg.: M-126, REV. 9 FI		PLANT DESIGN DWG.: M-251			
UNIT: 1		ELEV.: 833'-6"			
AREA: 4		ADDED TEMP. VALVE 1 BM			
RELOCATED PI & PT CONN.		ADDED SEISMIC REQMT.			
ADDED PI & PT CONN.		REV PER ODC-1650			
NO. DATE		DESCRIPTION			
DRAWN: JAW		CHECKED: JAW			
APPR.		APPR.			

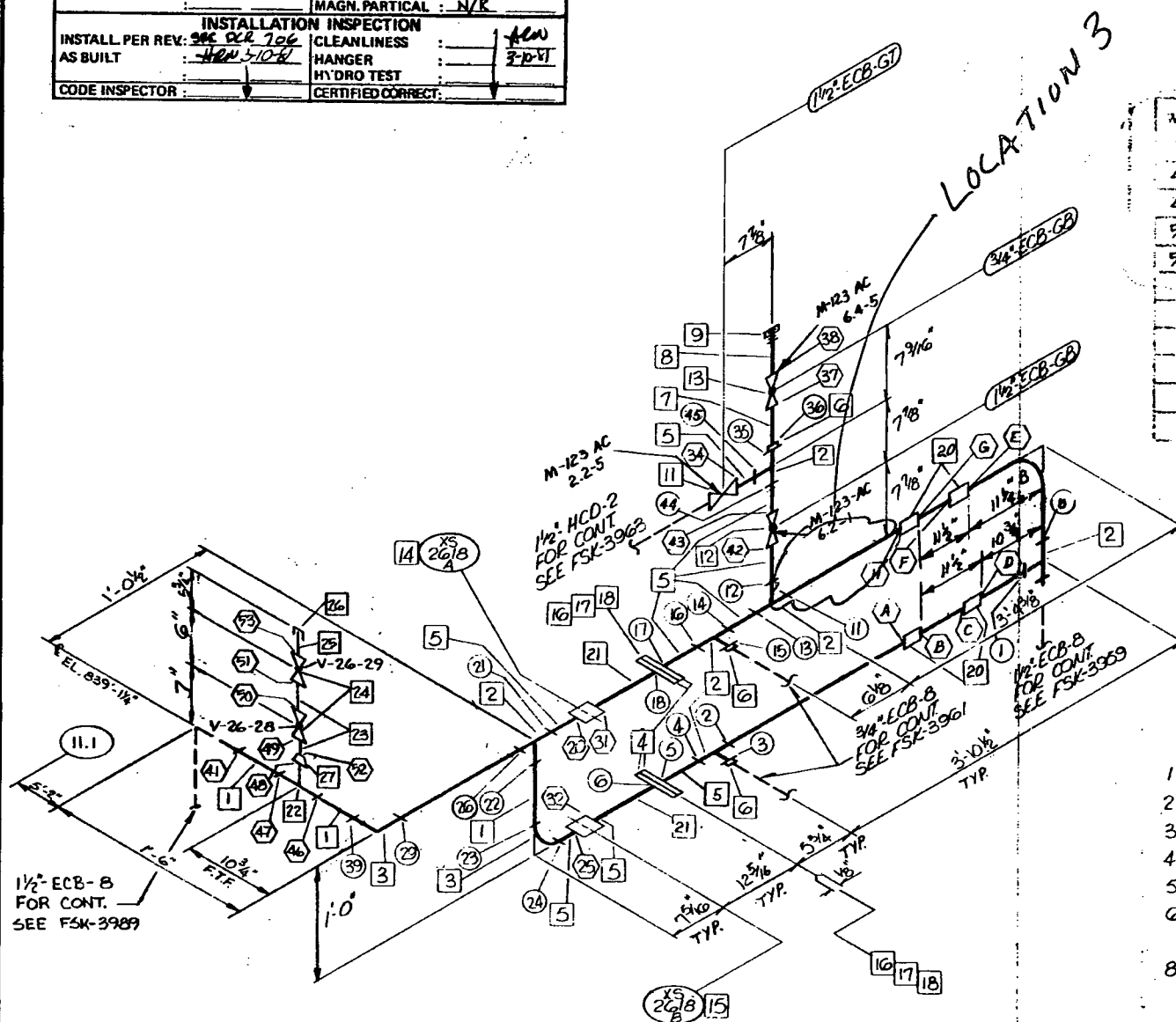
BECHTEL SAN FRANCISCO		
IOWA ELECTRIC POWER & LIGHT DUANE ARNOLD ENERGY PLANT		
REACTOR BLDG. - AREA #1 STANDBY LIQUID CONTROL PUMP DISCHARGE TO VESSEL		
JOB No.	DRAWING No.	REV.
7884-	FSK-03959	9



INFORMATION ONLY

BECHTEL SAN FRANCISCO			
IOWA ELECTRIC POWER & LIGHT DUANE ARNOLD ENERGY PLANT			
<i>REACTOR BLDG. - AREA</i> <i>STANDBY LIQUID CONTROL</i> <i>PUMP DISCH. TO VESSEL</i>			
	JOB No.	DRAWING No.	REV
	7884-	<i>FSK-3960</i> <i>FSK-3965</i>	8

1	36	12-20-72	21	486	1-5-73
2	36	12-20-72	22	36	12-21-72
3	36	12-21-72	23	36	12-21-72
4	36	12-20-72	24	486	1-5-73
5	486	12-29-72	25	269	2-27-73
6	269	2-27-73	26	36	12-21-72
8	36	12-20-72	29	36	12-21-72
11	36	12-20-72	31	269	1-23-73
12	36	12-20-72	32	269	2-27-73
13	36	12-20-72			
14	36	12-20-72	34	470	2-8-73
15	36	12-21-72	35	36	12-21-72
16	36	12-20-72	36	486	1-5-73
17	486	1-2-73	37	486	1-2-73
18	269	1-23-73	38	486	1-2-73
			39	486	1-3-73
20	269	1-23-73			



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△	3/14/79	REVISED PER DCR-706	TNO	GC
△	11/5/79	"AS-BUILT"	PA	HAB
△	10/23/79	REMOVED FS-2614	PA	EW
△	4-26/79	AS BUILT AS NOTED	PA	EW
NO.	DATE	DESCRIPTION	DRAWN	CHK'D
				APPR.

ALLOW 1/16" ROOT GAP ON ALL SOCKET WELDS

**PIPING SYMBOLS SEE
1-260 IN DRAFTING MANUAL**

*VENDOR SUPPLIED

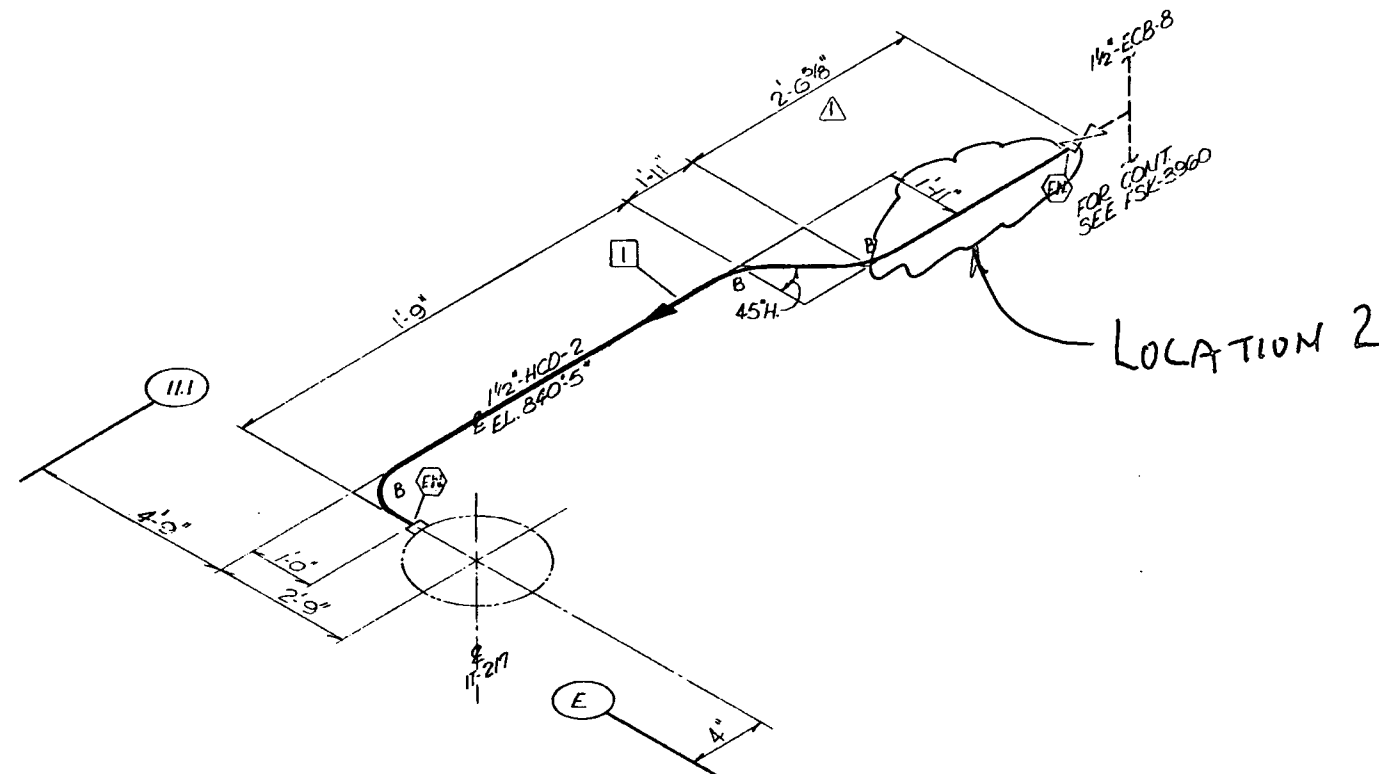
H = HORIZONTAL V = VERTICAL

R = BEND

* F.T.F. = FIELD TO FIT

~~X~~
F.W. FIELD WELD

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Q - DOCUMENTATION		SEISMIC ANALYSIS	
REQ'D <input type="checkbox"/>	NOT REQ'D <input checked="" type="checkbox"/>	REQ'D <input type="checkbox"/>	NOT REQ'D <input checked="" type="checkbox"/>

WELDING REQUIREMENTS			
WELDING PROC.	PR-T-AG Rev11	WELDERS NAME	:
FILLER METAL	ER-308	WELDERS QUALIF.	:
PREHEAT TEMP.	:	WELD No's	REV.
			REV.

DATE		INITIAL		DATE		INITIAL	
VISUAL	:			RADIOGRAPHIC	:	AR	
LIQUID PENET.	:	AR		ULTRASONIC	:	AR	
	:	AR		MAGN. PARTICAL	:	AR	

INSTALL. PER REV.:	CLEANLINESS :
AS BUILT	HANGER :
	HYDRO TEST :
CODE INSPECTOR :	CERTIFIED CORRECT:
	HANGER DET. DWG.:

SHOP FAB'D <input checked="" type="checkbox"/> FIELD FAB'D <input type="checkbox"/>		HANGER DET. DWG.:	
START-UP No.: <i>53</i>	COST CODE:	INSUL. CL.: <i>NONE</i>	THICK:
P & I D.: <i>M-126</i>	PLANT DESIGN DWG.: <i>M-251</i>		
UNIT: <i>1</i>	ELEV.: <i>833'-6</i>	AREA: <i>4</i>	

△						
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△	^{7/12}	CHANGED DIMEN.		LRH	EW	<i>[Signature]</i>
△	^{7/12}	ISSUED FOR CONSTRUCTION		LRH	EW	<i>[Signature]</i>
	NO. DATE	DESCRIPTION		DRAWN	CHECKD	APPR.

**IOWA ELECTRIC POWER & LIGHT
DUANE ARNOLD ENERGY PLANT**

REACTOR BLDG. - AREA 4
VENT OVERFLOW FROM 1 1/2" ECB-8
TO STANDBY LIQUID CONTROL TEST TANK

JOB No.	DRAWING No.	REV.
884-	FSK-3963	1

ALLOW 1/16" ROOT GAP ON ALL SOCKET WELDS

**PIPING SYMBOLS SEE
L-250 IN DRAFTING MANUAL**

*VENDOR SUPPLIED

H = HORIZONTAL, V = VERTICAL

B = BEND

*** F.T.F. = FIELD TO FIT**

FIELD WELD

INFORMATION ONLY

A	218	12-14-72
B	218	12-14-72
C	218	12-14-73
D	218	12-14-73
E	486	1-18-73
F	486	1-16-73

[illegible]


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QUALITY CONTROL DATA																																																																					
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WELDING REQUIREMENTS																																																																					
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FILLER METAL : <u>ER-308</u>					WELDERS QUAL. : <u>PA-TAG</u>																																																																
PREHEAT TEMP. : <u>600 min.</u>					WELD No's REV. : <u>1, 2, 3, 4, 5, 6, 7, 8, 9, 10</u>																																																																
NONDESTRUCTIVE EXAM.																																																																					
VISUAL : DATE <u>9-28-73</u> INITIAL <u>DLC</u>					RADIOGRAPHIC : <u>NR</u> <u>DLC</u>																																																																
LIQUID PENET. : <u>9-28-73</u> <u>DLC</u>					ULTRASONIC : <u>NR</u> <u>DLC</u>																																																																
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NO. DATE		DESCRIPTION					DRAWN CHECKED APPROV.																																																														

BECHTEL
SAN FRANCISCO

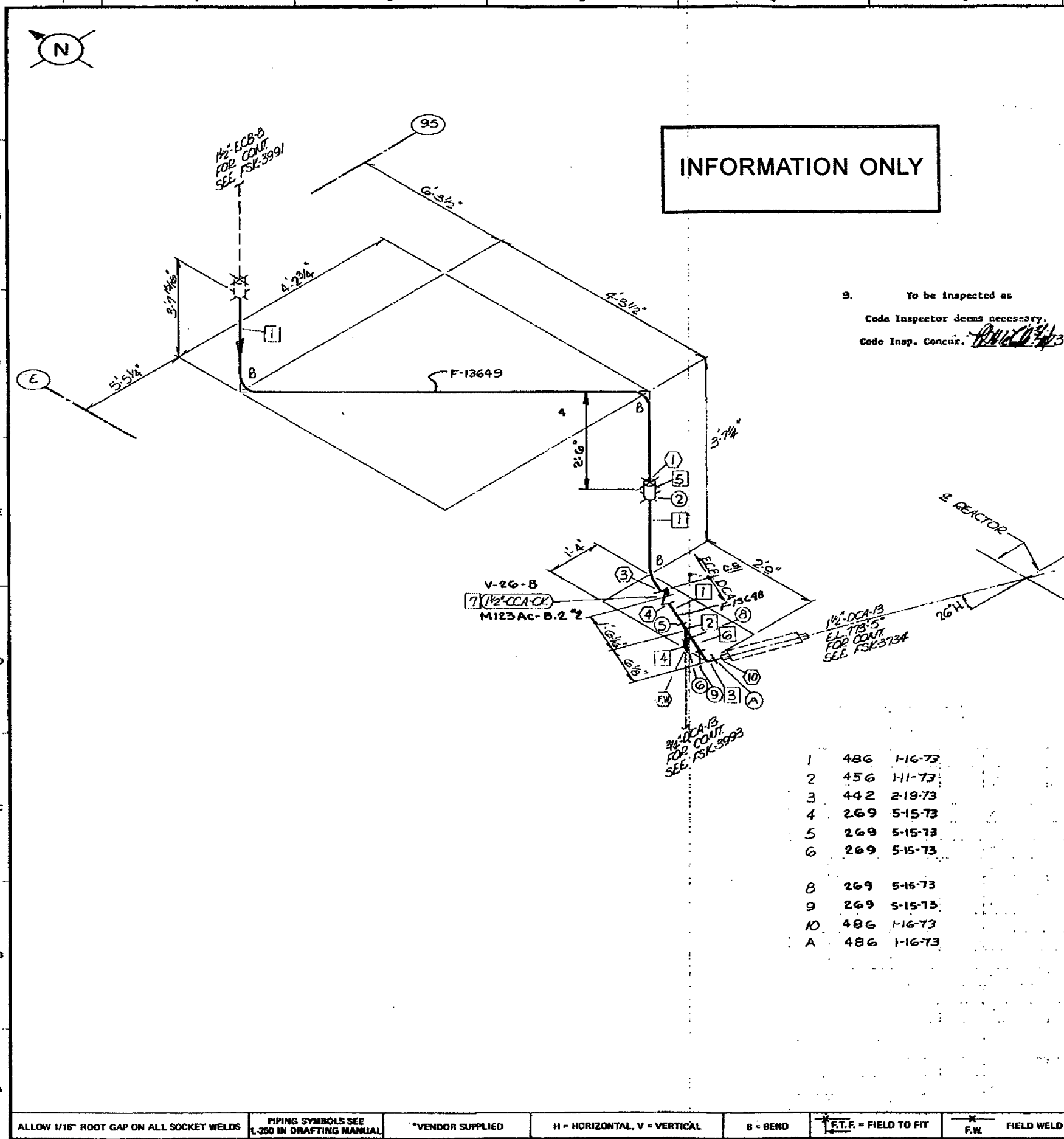
**IOWA ELECTRIC POWER & LIGHT
DUANE ARNOLD ENERGY PLANT**

REACTOR BLD'G - AREA 4
STANDBY LIQUID CONTROL TO
VESSEL

	JOB No.	DRAWING No.	REV.
	7884-	FSK-3991	2

1	486	1-9-73	B	486	1-11-73
2	256	1-8-73	C	486	1-11-73
3	256	1-8-73	11	256	1-5-73
4	486	1-10-73	12	486	1-10-73
5	256	1-5-73	D	486	1-11-73
6	256	1-5-73	E	486	1-10-73
7	256	1-5-73	F	486	1-11-73
8	256	1-5-73	G	486	1-11-73

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BILL OF MATERIAL						
QTY.	SIZE AND DESCRIPTION	ASTM	GR	PC. No.	HEAT No.	
16	1 1/2" PIPE SCH. 80s	A375	304	1	F1348	
1	1 1/2" TEE 3000" S.W.	A182	304	2	F1353	
1	1 1/2" 90° EL. 3000" S.W.			3	F1353	
1	1 1/2" 45° RED. INSERT 3000" S.W.			4	F1353	
1	1 1/2" COUPLING 3000" S.W.			5	F1353	
1	1 1/2" x 3/4" LG. ANGLE SCH. 80s	A375	304	6	F1348	
1	1 1/2" CCA-CK 1500" S.W.			7	NOTED	

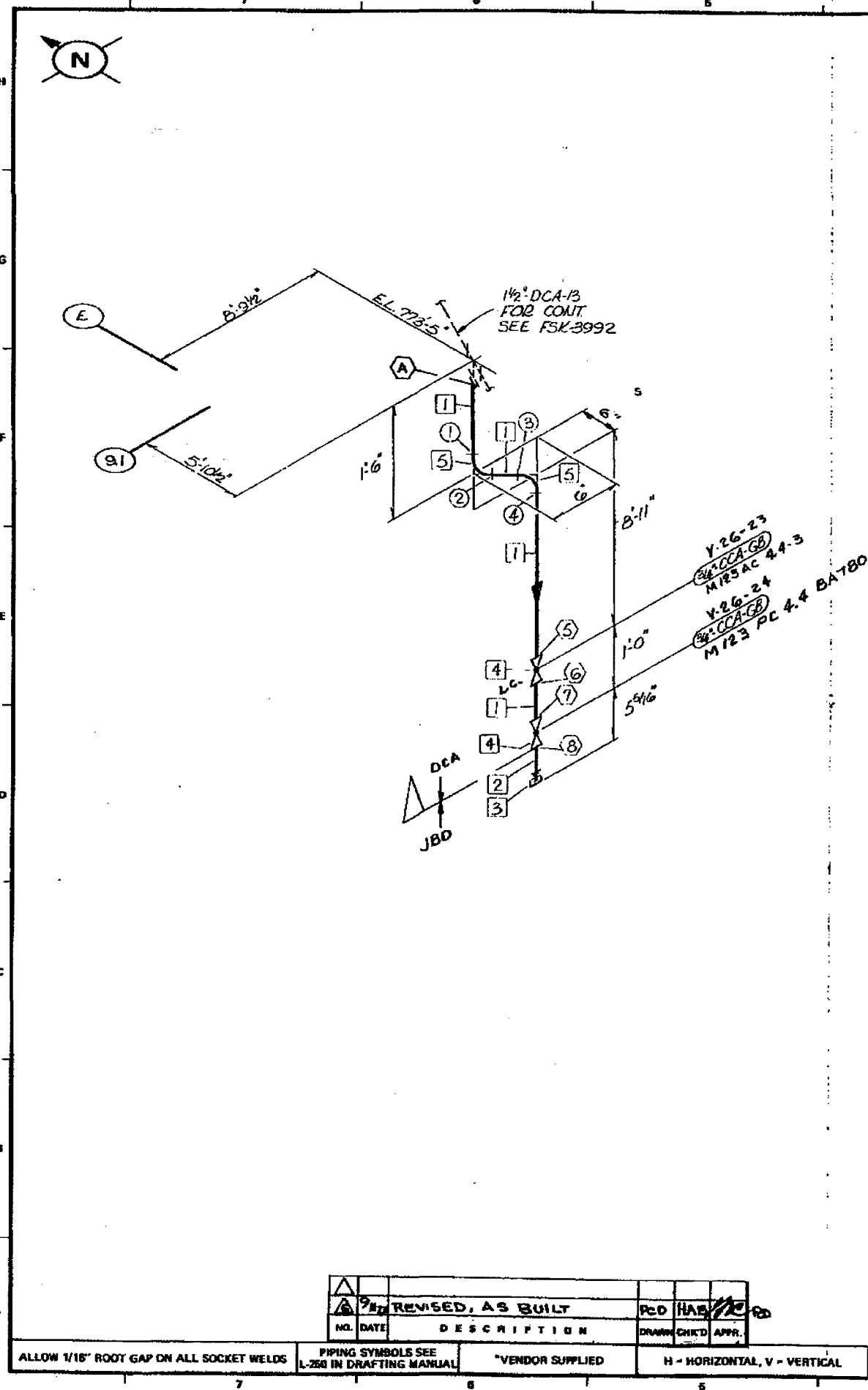
QUALITY CONTROL DATA			
Q - DOCUMENTATION		SEISMIC ANALYSIS	
REQ'D <input checked="" type="checkbox"/>	NOT REQ'D <input type="checkbox"/>	REQ'D <input checked="" type="checkbox"/>	NOT REQ'D <input type="checkbox"/>
WELDING REQUIREMENTS			
WELDING PROC. P-10, P-11		WELDERS NAME P-10, P-11	
FILLER METAL ER-308		WELDERS QUAL. P-10, P-11	
PREHEAT TEMP. 250°		WELD No's REV. 1, 2, 3, 4, 5, 6, 7, 8, 9, 10	
NONDESTRUCTIVE EXAM.			
VISUAL 100% OK		DATE 5/1/73 INITIAL OK	
LIQUID PENET. 100% OK		RADIOGRAPHIC 100% OK	
		ULTRASONIC 100% OK	
		MAGN. PARTIAL 100% OK	
INSTALLATION INSPECTION			
INSTALL. PER REV. 5/1/73		CLEANLINESS 5/1/73	
AS BUILT 5/1/73		HANGER 5/1/73	
CODE INSPECTOR SEE NOTE 9			
CERTIFIED CORRECT			
HANGER DET. DWG.			
SHOP FAB'D <input checked="" type="checkbox"/> FIELD FAB'D <input type="checkbox"/>			
START UP No. 53		COST CODE	
P.E.G. M-126 REV. 101		PLANT DESIGN DWG. M-248 REV.	
UNIT 1		ELEV. 757'-6"	
AREA 4		THICK. NONE	
REVISIONS			
REVISED AS BUILT		P.C.R. H.A.B.	
AS BUILT		P.C.R. H.A.B.	
REVISED PER NCR. 1175		P.C.R. H.A.B.	
AS BUILT		P.C.R. H.A.B.	
ISSUED FOR CONSTRUCTION		L.B.N. H.A.B.	
NO. DATE		DESCRIPTION	
7884-		FSK-3992	
REV. 4			

BECHTEL
SAN FRANCISCO

IOWA ELECTRIC POWER & LIGHT
DUANE ARNOLD ENERGY PLANT

REACTOR BLDG. - AREA 4
STANDBY LIQUID CONTROL TO
VESSEL

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INFORMATION ONLY

1	269	5-15-73
2	269	5-15-73
3	269	5-15-73
4	442	5-17-73
5	2 9	1-25-73
6	2 9	1-25-73
7	9	4-23-73
8	9	4-23-73
A	269	5-15-73

9. To be inspected as
Code Inspector deems necessary.
Code Insp. Concurrence: *[Signature]*

BILL OF MATERIAL					
QTY.	SIZE AND DESCRIPTION	ASTM	GR.	PC. No.	HEAT No.
106	3/4" PIPE SCH. 80s	A182	304	1	F7328
1	3/4" x 5/2" NIPPLE (10E) SCH. 80s	A182	304	1	F7328
1	3/4" SCRD CAP	A182	304	3	F3384
2	3/4" CCA-GB 1500" SW			4	NOTED
2	3/4" 90° ELL. 3000" SW	A182	304	5	F8205

QUALITY CONTROL DATA	
Q - DOCUMENTATION	SEISMIC ANALYSIS
REQ'D <input checked="" type="checkbox"/> NOT REQ'D <input type="checkbox"/>	REQ'D <input type="checkbox"/> NOT REQ'D <input type="checkbox"/>
WELDING REQUIREMENTS P. 49.1	
WELDING PROC. : PR-106 B.W.I.	WELDERS NAME : P. 9. REV. 9
FILLER METAL : ER-308	WELDERS QUALIF. : PR-T-AG
PREHEAT TEMP. : 60° MIN.	WELD No's REV. : 1. T. 8. 1. A
NONDESTRUCTIVE EXAM.	
VISUAL : DATE 8-20-73 INITIAL DEC	RADIOGRAPHIC : DATE 18 DEC
LIQUID PENET. : DATE 4-24-73 INITIAL DEC	ULTRASONIC : 18 DEC
	MAGN. PARTIAL : 18 DEC
INSTALLATION INSPECTION	
INSTALL PER REV. : 2/10/73 BA	CLEANLINESS : 5/11/73 BA
AS BUILT : 5/11/73 BA	HANGER :
CODE INSPECTOR : SEE NOTE 9	
CERTIFIED CORRECT :	
SHOP FAB'D <input checked="" type="checkbox"/> FIELD FAB'D <input type="checkbox"/>	HANGER DET. DWG. :
STARTUP NO. : 53	COST CODE :
INSUL. CL. :	THICK :
P & I D. : M-126, REV. 2F1	PLANT DESIGN DWG. : M-251
UNIT : 1	ELEV. : 833'-0"
AREA : 4	
AS BUILT	
REVISED PER NCR-1176	
AS BUILT	
APPROVED UNIQUE VALVE No.	
ISSUED FOR CONSTRUCTION	
NO. DATE	DESCRIPTION
DRAWN CHKD APPR.	

BECHTEL SAN FRANCISCO			
IOWA ELECTRIC POWER & LIGHT DUANE ARNOLD ENERGY PLANT			
REACTOR BLDG.-AREA STANDBY LIQUID CONTROL TEST CONN.			
JOB No.	DRAWING No.	REV.	
7884-	FSK-3993	5	

ALLOW 1/16" ROOT GAP ON ALL SOCKET WELDS PIPING SYMBOLS SEE L-250 IN DRAFTING MANUAL *VENDOR SUPPLIED H - HORIZONTAL, V - VERTICAL B - BEND F.T.F. - FIELD TO FIT F.W. FIELD WELD

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