

**SCIENTIFIC NOTEBOOK**  
**170-10E**

Scientific Notebook 170-10e

James Weldy

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20-1402-761

## Differential Analysis on TPA 3.2 for inclusion in the Sensitivity Studies Report

**Goal:** Perform a differential analysis on all sampled parameters in the TPA 3.2 Code. The analysis will include both base case parameters and disruptive event parameters and will start from seven different sets of baseline values. Since there is no compelling reason to bias the sampling of the baseline parameter set, these will be randomly sampled using LHS. Ideally, more sets of baseline values should be sampled in order to take an average sensitivity over all of parameter space, but time constraints do not make this feasible.

**Background:** Differential analysis is a technique that involves perturbing a single parameter in a code slightly while leaving all other sampled parameter constant to determine the impact on peak dose from that change in parameter. Sensitive parameters are those that have the largest relative impact on the peak dose, but can be defined as being based on their sampling range or not.

Two values will be calculated in this analysis,

$\frac{dD}{dx} \bullet \frac{\bar{x}}{\bar{D}}$ , where D represents dose and x represents the parameter value. This calculates the absolute impact of the parameter on dose and doesn't take into account the sampling range of the parameter.

$\frac{dD}{dx} \bullet \sigma_x$ , where  $\sigma_x$  represents the standard deviation in parameter x. This calculates the impact that the parameter has on the uncertainty in the results of the code calculation. This is the value that the results will be sorted by.

**Procedure:** (Note that all files listed here and all results are located in the following directory)

/home/jweldy/tpa32/sensanalTPA32

1. Set up a folder to run TPA Version 3.2 (call it tpa32)
2. Make two folders to hold the runs - one called base<something descriptive> to hold the output from the base values run and one called diff<something descriptive> to hold the differential output
3. Run a one realization, 7 subarea run of the code using tpa.inp.master as the input data with LHS sampling on and all disruptive events on. This is to create the samplpar.res file using LHS sampling which selects the baseline values for the differential analysis. If necessary, change the value of the seed in the tpa.inp file

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4. Run quantinp.f and select option 8 to use the values from an input file. This will create 2 important files. The first is tpa.inp.gen, which is a tpa.inp file consisting of all constant values from the samplpar.resfile. The second is vars.min.max.gen, which will be used later during the running of the awk script files.
5. Open vars.min.max.gen and delete any variable names that you do not wish to perform a differential analysis. Possible reasons for this include not testing disruptive events, removing variables that relate to a critical group distance that you are not interested in, etc. Add any variables that are constants in the input file that you are interested in testing in the appropriate format. Note the number of lines in the file when you are done as this is equal to the number of parameters that are being tested.
6. Modify tpa.inp.gen as appropriate for the analysis (time period of interest, disruptive events on/off, one realization, etc)and save as tpa.inp.<something descriptive> and tpa.inp
7. Run the TPA code using this input file.
8. Save all .res, .tpa, and .out files along with tpa.inp in the base folder
9. Modify the run.tpa.sh file if necessary to put the appropriate perturbationin each of the parameter value and the appropriate command to run the TPA code
10. Save vars.min.max.gen as vars.<something descriptive>
11. Type "run.tpa.sh tpa.inp.<something descriptive> diff<something descriptive> <number of parameters> vars.<something descriptive>" to start the TPA code running. That is "run.tpa.sh <input file> <output folder> <#> <vars file>."An example would be "run.tpa.sh tpa.inp.r1.10k diff10kr1 223 vars.r1". If you have a lot of parameters, this will take quite a while to run.
12. Once the script is finished, copy the following files to your diff folder: getsenssig.f, data.proc.sh, vars.<something descriptive>, tpa.inp.<something desc>, and stdevc22.out
13. Change directories to your diff folder.
14. Open your vars file. Replace all occurrences of / with another character (-). The slashwill cause errors in processing.
15. Open data.proc.sh. Change line 66 which should read MEAN\_pkdos = <#> to MEAN\_pkdos = <the dose calculated in your baseline run>.
16. Open getsenssig.f. Change the values for title, nparams, and meandose to the titleof the run, the number of parameters, and the dose calculated in yourbaseline run, respectively.
17. Type "data.proc.sh tpa.inp.<something descriptive> <# of parameters> vars.<something desc>Example: data.proc.sh tpa.inp.r1.10k 223 vars.r1
18. Compile and run getsenssig.f.
19. Congratulations, you are finished. Your output files are sens.out for the scaled sensitivitycoefficients, sens.sort, for sorted output of the same, sens.sigma, for the dD/dx \* sigma, and sigma.sort, for sorted output of the same.

The procedure was confirmed to be working correctly by performing hand calculations of selected parameters within the results.

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For example, the sensitivity coefficient for ArealAverageMeanAnnualInfiltration@Start for run1, 10 kyr, no disruptive events is calculated by the following:

Base Dose: 3.8512e-6 rem/yr      Base Parameter Value: 9.4474 mm/yr

Perturbed Dose: 3.9454e-6 rem/yr      Perturbed Parameter Value: 9.54187 mm/yr

Standard Deviation of Parameter Value: 2.7181 mm/yr

Therefore, the scaled sensitivity coefficient for this value is:

$$\frac{3.9454 \cdot 10^{-6} - 3.8512 \cdot 10^{-6}}{9.54187 - 9.4474} \cdot \frac{9.4474}{3.8512 \cdot 10^{-6}} = 2.446$$

and the sigma-weighted sensitivity coefficient for this value is:

$$\frac{3.9454 \cdot 10^{-6} - 3.8512 \cdot 10^{-6}}{9.54187 - 9.4474} \cdot 2.7181 = 2.71 \cdot 10^{-6}$$

These calculated values are the same as are output from the differential analysis runs. This confirms that the codes being used to calculate the sensitivity coefficients in the differential analysis are performing correctly. Note that a number of parameters were checked for several iterations of the differential analysis to be sure that it was working correctly.

The results for each set of baseline values were averaged in the files called TableE1-E2.xls, TableE3-E4.xls, and TableE5.xls located in the directory

D:\personal\excel files\sensanal99

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## Generation of an Improved Estimate of the Inventory of Radionuclides in the Repository

Goal: Generate an average inventory of radionuclides in all the waste packages based on actual burnup and enrichment values for the best estimate of spent fuel that will be disposed of in the repository.

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Software used:Origen 2.1 Isotope Generation and Depletion Code  
Microsoft Excel

Procedure: Input files were created for the Origen 2.1 program for PWR fuel with enrichments ranging from 1% to 5.5% U-235 and burnups ranging from 5 GWd/MTU to 70 GWd/MTU and for BWR fuel with enrichments ranging from 0.5% to 5.5% U-235 and burnups ranging from 5 GWd/MTU to 55 GWd/MTU. A sample input file is attached at the end of this notebook entry as attachment 1. All the input files generated are located at /home/jweldy/origen2/runs2/. All of the input files were run and the results were transferred to excel spreadsheets, bwrtotals.xls and pwrtotals.xls. The output files are located at /home/jweldy/origen2/runs2/. The input files were based on the sample input file provided with the Origen 2.1 code, which also provided output files for that run. This input file was for fuel enriched to 2.75% with a burnup of 27.5 GWd/MTU and was run to ensure that the output file generated matched the output file provided. The results matched precisely, so confidence was gained that the input file was correct and the code was functioning properly. In addition to the data sets that were directly generated, additional data points at 3.5% enrichment and burnup values of 35 and 45 GWd/MTU were generated using linear interpolation between the nearest data points. This is reasonable because the steps between data points are relatively small and therefore any error introduced due to the interpolation will be small.

After the radioactivity for the 43 chosen radionuclides were calculated, each value had to be weighted according to the abundance based on burnup and enrichment that is estimated to be present in the spent fuel that will be disposed of in the Yucca Mountain repository. This was done using data from “Characteristics of Potential Repository Waste” (Notz, et al., 1990) Figures 4.5 and 4.6 and Tables 4.22a and 4.22b. These abundance values were multiplied by the inventory for each radionuclide for each burnup and enrichment data point. All the results for each weighted burnup and enrichment data point were summed in order to get the average

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inventory for each radionuclide for all the PWR and BWR fuel that will be disposed of in the repository. Finally, the PWR and BWR fuel inventories were combined by weighing the PWR results by 65% and the BWR results by 35%, because these are the relative fractions that PWR and BWR fuel will make up the total repository inventory (CRWMS, 1997 - Characteristics of Fuel that will be Stored at the Yucca Mountain Repository).

Results:

The results of the calculations show an increase in the inventory for almost all radionuclides. For the fission products, this is primarily due to the increase in median burnup of the latest estimate of fuels destined for the repository. This causes about a 20%-30% increase in inventory for all fission products. For the actinides, this increase is due to the increased burnup effect and the averaging of inventories across all potential burnups and enrichments instead of just utilizing a median enrichment and burnup to calculate the inventory.

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<b>isotopes</b>	<b>bwr</b>	<b>pwr</b>	<b>Total (ci/MTU)</b>	<b>Current Inventory in TPA Code</b>	<b>Ratio of new value to old</b>
Ac 227	6.67E-06	8.666E-06	7.967E-06	5.19E-06	1.54E+00
Am 241	1.72E+03	2.294E+03	2.092E+03	1.64E+03	1.28E+00
Am 242m	1.08E+01	1.246E+01	1.189E+01	7.49E+00	1.59E+00
Am 243	2.08E+01	3.334E+01	2.894E+01	1.54E+01	1.88E+00
Cm 243	2.01E+01	3.528E+01	2.995E+01	1.53E+01	1.96E+00
Cm 244	1.97E+03	3.851E+03	3.191E+03	1.15E+03	2.78E+00
Cm 245	2.52E-01	5.891E-01	4.713E-01	1.25E-01	3.77E+00
Cm 246	7.56E-02	2.307E-01	1.764E-01	2.56E-02	6.89E+00
Np 237	3.12E-01	4.460E-01	3.992E-01	2.87E-01	1.39E+00
Pa 231	2.35E-05	3.085E-05	2.828E-05	1.95E-05	1.45E+00
Pb 210	5.61E-08	6.955E-08	6.485E-08	4.72E-08	1.37E+00
Pu 238	2.66E+03	4.212E+03	3.670E+03	2.11E+03	1.74E+00
Pu 239	2.99E+02	3.557E+02	3.357E+02	3.08E+02	1.09E+00
Pu 240	4.96E+02	5.605E+02	5.380E+02	5.08E+02	1.06E+00
Pu 241	7.44E+04	1.025E+05	9.264E+04	7.44E+04	1.25E+00
Pu 242	1.82E+00	2.673E+00	2.373E+00	1.60E+00	1.48E+00
Ra 226	3.93E-07	4.807E-07	4.501E-07	3.67E-07	1.23E+00
Th 229	2.56E-07	4.693E-07	3.947E-07	1.39E-07	2.84E+00
Th 230	1.25E-04	1.601E-04	1.479E-04	1.69E-04	8.75E-01
U 232	2.59E-02	5.722E-02	4.627E-02	2.48E-02	1.87E+00
U 233	2.32E-05	3.721E-05	3.232E-05	2.40E-05	1.35E+00
U 234	1.02E+00	1.369E+00	1.247E+00	1.13E+00	1.10E+00
U 235	1.70E-02	1.824E-02	1.782E-02	1.69E-02	1.05E+00
U 236	2.48E-01	3.217E-01	2.959E-01	2.40E-01	1.23E+00
U 238	3.18E-01	3.129E-01	3.147E-01	3.19E-01	9.86E-01
Ag 108m	1.26E-02	1.407E-02	1.356E-02	1.20E-02	1.13E+00
C 14	1.74E+00	1.693E+00	1.710E+00	1.33E+00	1.29E+00
Cl 36	1.23E-02	1.296E-02	1.274E-02	1.17E-02	1.09E+00
Cs 135	4.48E-01	5.308E-01	5.019E-01	3.51E-01	1.43E+00
Cs 137	7.91E+04	1.054E+05	9.620E+04	7.64E+04	1.26E+00
I 129	3.07E-02	4.087E-02	3.732E-02	2.95E-02	1.26E+00
Mo 93	6.74E-04	3.193E-02	2.099E-02	1.01E-02	2.08E+00

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Attachment 1. Sample Input File for Origen 2.1

```
-1
-1
-1
RDA * BURNUP OF BWR 4.5% UO2 FUEL & ASSY HDWARE, 45,000 MWD/MT
RDA ** CROSS SECTION LIBRARY = BWRU, 4 CYCLE
RDA *** SCOTT B. LUDWIG, OAK RIDGE NATIONAL LABORATORY
RDA **** (615) 574-7916, FTS 624-7916
RDA -1 = FRESH BWR FUEL WITH IMPURITIES (1 MT = 1000 KG)
RDA -2 = FRESH ZIRCALOY-4 COMPOSITION (1 KG)
RDA -3 = FRESH ZIRCALOY-2 COMPOSITION (1 KG)
RDA -4 = FRESH SS 304 COMPOSITION (1 KG)
RDA -5 = FRESH SS 302 COMPOSITION (1 KG)
RDA -6 = FRESH INCONEL X-750 COMPOSITION (1 KG)
RDA WARNING: VECTORS ARE CHANGED WITH RESPECT TO CONTENT.
RDA      THESE CHANGES WILL BE NOTED ON RDA CARDS.
CUT 5 1.0E-10 7 1.0E-14 9 1.0E-10 -1
LIP 0 0 0
RDA      DECAY LIB   XSECT LIB           VAR. XSECT
LIB 0 1 2 3  251 252 253  9 50 0 1    4
RDA      PHOTON LIB
PHO 101 102 103 10
TIT INITIAL COMP. OF UNIT AMOUNTS OF FUEL AND STRUCTURAL MAT'LS
RDA READ FUEL COMPOSITION INCLUDING IMPURITIES (1000 KG)
INP -1 1 -1 -1 1 1
RDA READ ZIRCALOY-4 COMPOSITION (1.0 KG)
INP -2 1 -1 -1 1 1
RDA READ ZIRCALOY-2 COMPOSITION (1.0 KG)
INP -3 1 -1 -1 1 1
RDA READ SS304 COMPOSITION (1.0 KG)
INP -4 1 -1 -1 1 1
RDA READ SS302 COMPOSITION (1.0 KG)
INP -5 1 -1 -1 1 1
RDA READ INCONEL X-750 COMPOSITION (1.0 KG)
INP -6 1 -1 -1 1 1
TIT IRRADIATION OF ONE METRIC TON OF BWRU FUEL
MOV -1 1 0 1.0
```

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PCH 1 1 1

HED 1 CHARGE

BUP

IRP 265.45 25.90 1 2 4 2 BURNUP= 6,875 MWD/MTIHM

DEC 371.45 2 3 4 0 DECAY FOR 106.0 DAYS

IRP 636.90 25.90 3 4 4 0 BURNUP=13,750 MWD/MTIHM

DEC 742.90 4 5 4 0 DECAY FOR 106.0 DAYS

IRP 1008.35 25.90 5 6 4 0 BURNUP=20,625 MWD/MTIHM

DEC 1114.35 6 7 4 0 DECAY FOR 106.0 DAYS

IRP 1379.80 25.90 7 8 4 0 BURNUP=27,500 MWD/MTIHM

DEC 1485.80 8 9 4 0 DECAY FOR 106.0 DAYS

IRP 1751.25 25.90 9 10 4 0 BURNUP=34,375 MWD/MTIHM

DEC 1857.25 10 11 4 0 DECAY FOR 106.0 DAYS

IRP 2122.70 25.90 11 12 4 0 BURNUP=41,250 MWD/MTIHM

DEC 2228.70 12 13 4 0 DECAY FOR 106.0 DAYS

IRP 2373.49 25.90 13 14 4 0 BURNUP=45,000 MWD/MTIHM

BUP

RDA -10 = IRRADIATED U FUEL AT DISCHARGE

MOV 14 -10 0 1.0

PCH -10 -10 -10

RDA IRRADIATION OF ZIRCALOY-2 CLADDING AT 1.000 FLUX

TIT IRRADIATION OF ZIRCALOY-2 CLADDING AT 1.000 FLUX

MOV -3 1 0 279.50 ZIRCALOY-2 CLAD

HED 1 CHARGE

IRF 265.45 -1.0 1 2 4 2 BURNUP= 6,875 MWD/MTIHM

DEC 371.45 2 3 4 0 DECAY FOR 106.0 DAYS

IRF 636.90 -1.0 3 4 4 0 BURNUP=13,750 MWD/MTIHM

DEC 742.90 4 5 4 0 DECAY FOR 106.0 DAYS

IRF 1008.35 -1.0 5 6 4 0 BURNUP=20,625 MWD/MTIHM

DEC 1114.35 6 7 4 0 DECAY FOR 106.0 DAYS

IRF 1379.80 -1.0 7 8 4 0 BURNUP=27,500 MWD/MTIHM

DEC 1485.80 8 9 4 0 DECAY FOR 106.0 DAYS

IRF 1751.25 -1.0 9 10 4 0 BURNUP=34,375 MWD/MTIHM

DEC 1857.25 10 11 4 0 DECAY FOR 106.0 DAYS

IRF 2122.70 -1.0 11 12 4 0 BURNUP=41,250 MWD/MTIHM

DEC 2228.70 12 13 4 0 DECAY FOR 106.0 DAYS

IRF 2373.49 -1.0 13 14 4 0 BURNUP=45,000 MWD/MTIHM

RDA -9 = IRRADIATED ZIRCALOY-2 CLADDING AT DISCHARGE

MOV 14 -9 0 1.0

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RDA IRRADIATION OF ZIRCALOY CLADDING AT 0.500 FLUX  
TIT IRRADIATION OF ZIRCALOY CLADDING AT 0.500 FLUX  
MOV -3 1 0 25.4 ZIRCALOY-2 CLAD  
MOV -3 2 0 304.90 TOTAL ZIRC-2 CLAD  
PCH 2 2 2  
HED 1 CHARGE  
IRF 265.45 -0.5 1 2 4 2 BURNUP= 6,875 MWD/MTIHM  
DEC 371.45 2 3 4 0 DECAY FOR 106.0 DAYS  
IRF 636.90 -0.5 3 4 4 0 BURNUP=13,750 MWD/MTIHM  
DEC 742.90 4 5 4 0 DECAY FOR 106.0 DAYS  
IRF 1008.35 -0.5 5 6 4 0 BURNUP=20,625 MWD/MTIHM  
DEC 1114.35 6 7 4 0 DECAY FOR 106.0 DAYS  
IRF 1379.80 -0.5 7 8 4 0 BURNUP=27,500 MWD/MTIHM  
DEC 1485.80 8 9 4 0 DECAY FOR 106.0 DAYS  
IRF 1751.25 -0.5 9 10 4 0 BURNUP=34,375 MWD/MTIHM  
DEC 1857.25 10 11 4 0 DECAY FOR 106.0 DAYS  
IRF 2122.70 -0.5 11 12 4 0 BURNUP=41,250 MWD/MTIHM  
DEC 2228.70 12 13 4 0 DECAY FOR 106.0 DAYS  
IRF 2373.49 -0.5 13 14 4 0 BURNUP=45,000 MWD/MTIHM  
RDA -9 = IRRADIATED ZIRCALOY CLADDING AT DISCHARGE  
ADD 14 -9 0 1.0 TOTAL IRRAD ZIRC-2 CLAD  
PCH -9 -9 -9  
RDA IRRADIATION OF ZIRCALOY-4 CHANNEL AT 1.000 FLUX  
TIT IRRADIATION OF ZIRCALOY-4 CHANNEL AT 1.000 FLUX  
MOV -2 1 0 227.50 ZIRCALOY-4 CHANNEL  
HED 1 CHARGE  
IRF 265.45 -1.0 1 2 4 2 BURNUP= 6,875 MWD/MTIHM  
DEC 371.45 2 3 4 0 DECAY FOR 106.0 DAYS  
IRF 636.90 -1.0 3 4 4 0 BURNUP=13,750 MWD/MTIHM  
DEC 742.90 4 5 4 0 DECAY FOR 106.0 DAYS  
IRF 1008.35 -1.0 5 6 4 0 BURNUP=20,625 MWD/MTIHM  
DEC 1114.35 6 7 4 0 DECAY FOR 106.0 DAYS  
IRF 1379.80 -1.0 7 8 4 0 BURNUP=27,500 MWD/MTIHM  
DEC 1485.80 8 9 4 0 DECAY FOR 106.0 DAYS  
IRF 1751.25 -1.0 9 10 4 0 BURNUP=34,375 MWD/MTIHM  
DEC 1857.25 10 11 4 0 DECAY FOR 106.0 DAYS  
IRF 2122.70 -1.0 11 12 4 0 BURNUP=41,250 MWD/MTIHM  
DEC 2228.70 12 13 4 0 DECAY FOR 106.0 DAYS  
IRF 2373.49 -1.0 13 14 4 0 BURNUP=45,000 MWD/MTIHM

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RDA -8 = IRRADIATED ZIRCALOY CHANNEL AT DISCHARGE  
MOV 14 -8 0 1.0  
RDA IRRADIATION OF ZIRCALOY-4 CHANNEL AT 0.500 FLUX  
TIT IRRADIATION OF ZIRCALOY-4 CHANNEL AT 0.500 FLUX  
MOV -2 1 0 20.70 ZIRCALOY-4 CHANNEL  
MOV -2 2 0 248.20 TOTAL ZIRCALOY-4 CHANNEL  
PCH 2 2 2  
HED 1 CHARGE  
IRF 265.45 -0.5 1 2 4 2 BURNUP= 6,875 MWD/MTIHM  
DEC 371.45 2 3 4 0 DECAY FOR 106.0 DAYS  
IRF 636.90 -0.5 3 4 4 0 BURNUP=13,750 MWD/MTIHM  
DEC 742.90 4 5 4 0 DECAY FOR 106.0 DAYS  
IRF 1008.35 -0.5 5 6 4 0 BURNUP=20,625 MWD/MTIHM  
DEC 1114.35 6 7 4 0 DECAY FOR 106.0 DAYS  
IRF 1379.80 -0.5 7 8 4 0 BURNUP=27,500 MWD/MTIHM  
DEC 1485.80 8 9 4 0 DECAY FOR 106.0 DAYS  
IRF 1751.25 -0.5 9 10 4 0 BURNUP=34,375 MWD/MTIHM  
DEC 1857.25 10 11 4 0 DECAY FOR 106.0 DAYS  
IRF 2122.70 -0.5 11 12 4 0 BURNUP=41,250 MWD/MTIHM  
DEC 2228.70 12 13 4 0 DECAY FOR 106.0 DAYS  
IRF 2373.49 -0.5 13 14 4 0 BURNUP=45,000 MWD/MTIHM  
RDA -8 = IRRADIATED ZIRCALOY CHANNEL AT DISCHARGE  
ADD 14 -8 0 1.0  
PCH -8 -8 -8  
RDA IRRADIATION OF ZIRCALOY GRID SPACERS AND INCONEL SPRINGS  
TIT IRRADIATION OF ZIRCALOY GRID SPACERS AND INCONEL SPRINGS  
MOV -2 1 0 10.60 ZIRCALOY GRIDS  
ADD -6 1 0 1.80 INCONEL SPRINGS  
PCH 1 1 1  
HED 1 CHARGE  
IRF 265.45 -1.0 1 2 4 2 BURNUP= 6,875 MWD/MTIHM  
DEC 371.45 2 3 4 0 DECAY FOR 106.0 DAYS  
IRF 636.90 -1.0 3 4 4 0 BURNUP=13,750 MWD/MTIHM  
DEC 742.90 4 5 4 0 DECAY FOR 106.0 DAYS  
IRF 1008.35 -1.0 5 6 4 0 BURNUP=20,625 MWD/MTIHM  
DEC 1114.35 6 7 4 0 DECAY FOR 106.0 DAYS  
IRF 1379.80 -1.0 7 8 4 0 BURNUP=27,500 MWD/MTIHM  
DEC 1485.80 8 9 4 0 DECAY FOR 106.0 DAYS  
IRF 1751.25 -1.0 9 10 4 0 BURNUP=34,375 MWD/MTIHM

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DEC 1857.25 10 11 4 0 DECAY FOR 106.0 DAYS  
IRF 2122.70 -1.0 11 12 4 0 BURNUP=41,250 MWD/MTIHM  
DEC 2228.70 12 13 4 0 DECAY FOR 106.0 DAYS  
IRF 2373.49 -1.0 13 14 4 0 BURNUP=45,000 MWD/MTIHM  
RDA -7 = IRRADIATED ZIRCALOY GRID SPACERS AND INCONEL SPRINGS  
RDA AT DISCHARGE  
MOV 14 -7 0 1.0  
PCH -7 -7 -7  
RDA IRRAD. OF SS 304 END PIECES & INCONEL SPRINGS AT 0.130 FLUX  
TIT IRRAD. OF SS 304 END PIECES & INCONEL SPRINGS AT 0.130 FLUX  
MOV -4 1 0 37.00 SS 304 IN END PIECES  
ADD -6 1 0 2.10 INCONEL X-750 EXPANSION SPRINGS  
PCH 1 1 1  
HED 1 CHARGE  
IRF 265.45 -0.13 1 2 4 2 BURNUP= 6,875 MWD/MTIHM  
DEC 371.45 2 3 4 0 DECAY FOR 106.0 DAYS  
IRF 636.90 -0.13 3 4 4 0 BURNUP=13,750 MWD/MTIHM  
DEC 742.90 4 5 4 0 DECAY FOR 106.0 DAYS  
IRF 1008.35 -0.13 5 6 4 0 BURNUP=20,625 MWD/MTIHM  
DEC 1114.35 6 7 4 0 DECAY FOR 106.0 DAYS  
IRF 1379.80 -0.13 7 8 4 0 BURNUP=27,500 MWD/MTIHM  
DEC 1485.80 8 9 4 0 DECAY FOR 106.0 DAYS  
IRF 1751.25 -0.13 9 10 4 0 BURNUP=34,375 MWD/MTIHM  
DEC 1857.25 10 11 4 0 DECAY FOR 106.0 DAYS  
IRF 2122.70 -0.13 11 12 4 0 BURNUP=41,250 MWD/MTIHM  
DEC 2228.70 12 13 4 0 DECAY FOR 106.0 DAYS  
IRF 2373.49 -0.13 13 14 4 0 BURNUP=45,000 MWD/MTIHM  
RDA -6 = IRRAD. SS 304 END PIECES & INCONEL SPRINGS AT DISCHARGE  
MOV 14 -6 0 1.0  
PCH -6 -6 -6  
RDA IRRADIATION OF SS 302 IN PLENUM SPRINGS AT 0.500 FLUX  
TIT IRRADIATION OF SS 302 IN PLENUM SPRINGS AT 0.500 FLUX  
MOV -5 1 0 6.00 SS302  
PCH 1 1 1  
HED 1 CHARGE  
IRF 265.45 -0.5 1 2 4 2 BURNUP= 6,875 MWD/MTIHM  
DEC 371.45 2 3 4 0 DECAY FOR 106.0 DAYS  
IRF 636.90 -0.5 3 4 4 0 BURNUP=13,750 MWD/MTIHM  
DEC 742.90 4 5 4 0 DECAY FOR 106.0 DAYS

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```
IRF 1008.35 -0.5 5 6 4 0 BURNUP=20,625 MWD/MTIHM
DEC 1114.35      6 7 4 0 DECAY FOR 106.0 DAYS
IRF 1379.80 -0.5 7 8 4 0 BURNUP=27,500 MWD/MTIHM
DEC 1485.80      8 9 4 0 DECAY FOR 106.0 DAYS
IRF 1751.25 -0.5 9 10 4 0 BURNUP=34,375 MWD/MTIHM
DEC 1857.25      10 11 4 0 DECAY FOR 106.0 DAYS
IRF 2122.70 -0.5 11 12 4 0 BURNUP=41,250 MWD/MTIHM
DEC 2228.70      12 13 4 0 DECAY FOR 106.0 DAYS
IRF 2373.49 -0.5 13 14 4 0 BURNUP=45,000 MWD/MTIHM
RDA -5 = IRRADIATED SS 302 IN PLENUM SPRINGS AT DISCHARGE
MOV 14 -5 0 1.0
PCH -5 -5 -5
RDA ***** OUTPUT MODULE *****
TIT TEST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)
BAS 1 MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM, 4 CYCLE
OPTL 6*8 7 8 8 8 14*8
OPTA 6*8 7 8 8 8 14*8
OPTF 6*8 7 8 8 8 14*8
MOV -10 1 0 1.0
ADD -9 1 0 1.0
ADD -8 1 0 1.0
ADD -7 1 0 1.0
ADD -6 1 0 1.0
ADD -5 1 0 1.0
HED 1 ASSY DIS
RDA ***** DECAY MODULE *****
DEC 0.5 1 2 5 2
DEC 1.0 2 3 5 0
DEC 2.0 3 4 5 0
DEC 5.0 4 5 5 0
DEC 10.0 5 6 5 0
DEC 26.0 6 7 5 0
OUT 7 1 -1 0
END
```

```
2 922340 247.0 922350 45000. 922380 954753. 0 0.0 FUEL 4.5%
4 030000 1.0 050000 1.0 060000 89.4 070000 25.0 FUEL IMPU
4 080000 134454. 090000 10.7 110000 15.0 120000 2.0 FUEL IMPU
4 130000 16.7 140000 12.1 150000 35.0 170000 5.3 FUEL IMPU
4 200000 2.0 220000 1.0 230000 3.0 240000 4.0 FUEL IMPU
```

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4 250000 1.7 260000 18.0 270000 1.0 280000 24.0 FUEL IMPU  
4 290000 1.0 300000 40.3 420000 10.0 470000 0.1 FUEL IMPU  
4 480000 25.0 490000 2.0 500000 4.0 640000 1573. FUEL IMPU  
4 740000 2.0 820000 1.0 830000 0.4 0 0.0 FUEL IMPU  
0  
4 400000 979.11 500000 16.0 260000 2.25 240000 1.25 ZIRC-4  
4 280000 0.02 130000 0.024 050000 0.00033 480000 0.00025 ZIRC-4  
4 060000 0.120 270000 0.010 290000 0.020 720000 0.078 ZIRC-4  
4 010000 0.013 250000 0.020 070000 0.080 080000 0.950 ZIRC-4  
4 160000 0.035 220000 0.020 740000 0.020 230000 0.020 ZIRC-4  
5 920000 0.0002 0 0.0 ZIRC-4  
0  
4 400000 979.63 500000 16.0 260000 1.5 240000 1.00 ZIRC-2  
4 280000 0.5 130000 0.024 050000 0.00033 480000 0.00025 ZIRC-2  
4 060000 0.120 270000 0.010 290000 0.020 720000 0.078 ZIRC-2  
4 010000 0.013 250000 0.020 070000 0.080 080000 0.950 ZIRC-2  
4 160000 0.035 220000 0.020 740000 0.020 230000 0.020 ZIRC-2  
5 920000 0.0002 0 0.0 ZIRC-2  
0  
4 260000 688.44 240000 190.0 280000 89.2 250000 20.0 SS-304  
4 060000 0.8 150000 0.45 160000 0.3 140000 10.0 SS-304  
4 070000 1.3 270000 0.8 0 0.0 SS-304  
0  
4 260000 697.74 240000 180.0 280000 89.2 250000 20.0 SS-302  
4 060000 1.5 150000 0.45 160000 0.3 140000 10.0 SS-302  
4 070000 1.3 270000 0.8 0 0.0 SS-302  
0  
4 260000 67.846 240000 149.66 280000 721.861 130000 7.982 INC-X-750  
4 060000 0.399 270000 6.485 290000 0.499 250000 6.984 INC-X-750  
4 070000 1.3 410000 8.98 160000 0.07 140000 2.993 INC-X-750  
4 220000 24.943 0 0.0 INC-X-750  
0

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Attachment 2. Sample Output File from Origen 2.1

1

```
*****
*          *
* OOOOO RRRR IIII GGGGG EEEEE N N 22222 *  
* O O R R I G E NN N 22 22 *  
* O O RRRR I G GG EEEE NNNN 22 *  
* O O R R I G G E N NN 22 *  
* OOOOO R R IIII GGGGGG EEEEE N N 2222222 *  
*          *  
*          Version 2.1 (8-1-91)          *  
*          *  
*          *  
* OOOOO AA K K          *  
* O O A A K K          *  
* O O AAAA KKK          *  
* O O A A K K          *  
* OOOOO A A K K          *  
*          *  
* RRRR III DDDDD GGGGG EEEEE          *  
* R R I D D G E          *  
* RRRR I D D G GG EEEE          *  
* R R I D D G G E          *  
* R R III DDDDD GGGGGG EEEEE          *  
*          *  
* N N AA TTTTT III OOOOO N N AA L          *  
* NN N AA T I O O NN N A A L          *  
* NNNN AAAA T I O O NNNN AAAA L          *  
* N NN A A T I O O N NN A A L          *  
* N N A A T III OOOOO N N A A LLLL *  
*          *  
* L AA BBBB OOOO RRRR AA TTTTT OOOO RRRR Y Y *  
* L A AB BO OR R A A T O OR R YY *  
* L AAAA BBBB O ORRRR AAAA T O ORRRR Y *  
* L A AB BO OR R A A T O OR R Y *  
* LLLL A AB BBBB OOOOR R A A T OOOOR R Y *  
*          *  
*          RSIC CODE PACKAGE NUMBER (CCC-371)          *
```

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\* \*  
\* ORIGEN2 VERSION 2.1 (8-1-91) UPDATES THE FOLLOWING: \*  
\* \*  
\* CCC-371(A) - MAINFRAMES \*  
\* CCC-371(E) - IBM PC (80386 W/80387 OR 80486) \*  
\* \*  
\* ORIGEN2 RUN DATE: Aug 20 1999 TIME 10:07:12 \*  
\* \*  
\* \*  
\*\*\*\*\*

1

OUTPUT UNIT = 6

PAGE 1

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

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\*\*\*\*\* ORIGEN2: A REVISED AND UPDATED VERSION OF  
THE ORIGEN COMPUTER CODE \*\*\*\*\*

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## INTRODUCTION

THIS TEXT IS INTENDED TO BE A BRIEF OUTLINE OF THE ORIGEN2 COMPUTER CODE, WHICH IS A REVISED AND UPDATED VERSION OF THE

ORIGEN DOCUMENTED IN REPORT ORNL-4628 (MAY 1973). INCLUDED HERE ARE A BRIEF DESCRIPTION OF THE FUNCTIONS OF ORIGEN2, A

LISTING OF THE MAJOR DATA SOURCES, A LISTING OF THE PUBLISHED DOCUMENTATION CONCERNING ORIGEN2, AND AN OUTLINE OF THE ORIGEN2

OUTPUT ORGANIZATION. ORIGEN2 IS AVAILABLE FROM THE ORNL RADIATION SHIELDING INFORMATION CENTER (RSIC) AT THE FOLLOWING

ADDRESS:

CODES COORDINATOR  
RADIATION SHIELDING INFORMATION CENTER

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BLDG. 6025  
OAK RIDGE NATIONAL LABORATORY  
OAK RIDGE, TENNESSEE 37830  
PHONE: (615) 574-6176

QUESTIONS CONCERNING ORIGEN2 SHOULD BE ADDRESSED TO RSIC.

-DESCRIPTION

ORIGEN2 IS A REVISION AND UPDATE OF THE ORIGEN COMPUTER CODE. SPECIFICALLY, THE INPUT, OUTPUT, CONTROL, AND DATA BASE ASPECTS

OF ORIGEN HAVE BEEN SIGNIFICANTLY REVISED AND UPDATED TO REFLECT CURRENT INFORMATION AND NEEDS. IT SHOULD BE NOTED THAT THE

MATHEMATICAL METHODS USED TO SOLVE THE NUCLIDE BUILDUP, DEPLETION, AND DECAY EQUATIONS ARE ESSENTIALLY UNCHANGED FROM THAT IN

ORIGEN. ORIGEN2 IS A COMPUTER CODE DESIGNED TO CALCULATE THE COMPOSITION AND CHARACTERISTICS OF NUCLEAR MATERIALS AS A

FUNCTION OF DECAY TIME AND THE CHANGES THE MATERIALS UNDERGO DURING VARIOUS FUEL CYCLE OPERATIONS. INPUT AND OUTPUT FEATURES

HAVE BEEN DESIGNED TO FACILITATE FLEXIBILITY IN THE TYPE OF CASES THAT CAN BE CONSIDERED AND IN CONTROLLING THE DETAIL OF THE

OUTPUT. FOR FURTHER INFORMATION, THE USER IS REFERRED TO THE DOCUMENTATION LISTED BELOW.

-MAJOR DATA SOURCES

VIRTUALLY ALL ASPECTS OF THE DATA INPUT TO ORIGEN2 HAVE BEEN UPDATED OR REVISED TO REFLECT CURRENT INFORMATION. THE

PRINCIPAL SOURCES OF CROSS SECTION DATA WERE THE ENDF/B-IV, ENDF/B-V, AND LENDL COMPILATIONS. DECAY AND PHOTON INFORMATION

WERE PRIMARILY BASED ON THE EVALUATED NUCLEAR STRUCTURE DATA FILE (ENSDF) AT ORNL AND ENDF/B-IV. DATA CONCERNING REACTOR

AND FUEL CHARACTERISTICS WERE OBTAINED FROM REFERENCE SAFETY ANALYSIS REPORTS AND, WHERE POSSIBLE, THE COMMERCIAL REACTOR VENDORS.

-DOCUMENTATION

THE FOLLOWING ITEMS CONSTITUTE THE ORIGEN2 DOCUMENTATION PUBLISHED AS OF THE DATE OF THIS CODE PACKAGE:

A.G. CROFF, "ORIGEN2 - A REVISED AND UPDATED VERSION OF THE OAK RIDGE ISOTOPE GENERATION AND DEPLETION CODE", ORNL-5621  
(JULY 1980).

A.G. CROFF, "A USER'S MANUAL FOR THE ORIGEN2 COMPUTER CODE", ORNL/TM-7175 (JULY 1980).

A.G. CROFF, M.A. BJRKE, G.W.MORRISON, AND L.M. PETRIE, "REVISED

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# URANIUM-PLUTONIUM CYCLE PWR AND BWR MODELS FOR THE ORIGEN COMPUTER CODE", ORNL/TM-6051 (SEPTEMBER 1978).

A.G. CROFF AND M.A. BJERKE, "ALTERNATIVE FUEL CYCLE PWR MODELS FOR THE ORIGEN COMPUTER CODE", ORNL/TM-7005 (FEB 1980).

A.G. CROFF, R.L. HAESE, AND N.B. GOVE, "UPDATED DECAY AND PHOTON LIBRARIES FOR THE ORIGEN CODE", ORNL/TM-6055 (FEB 1979)

A.G. CROFF, "ORIGEN2: A REVISED AND UPDATED VERSION OF ORIGEN", TRANS. AM. NUCL. SOC., VOL. 34, P. 349-50 (JUNE 1980).

1 OUTPUT UNIT = 6 PAGE 2

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\*\*\*\*\* ORIGEN2: A REVISED AND UPDATED VERSION OF  
THE ORIGEN COMPUTER CODE \*\*\*\*\*

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## ORGANIZATION OF ORIGIN2 OUTPUT

PAST EXPERIENCE HAS INDICATED THAT MANY USERS ENCOUNTER  
CONSIDERABLE DIFFICULTY IN FINDING THE DESIRED INFORMATION IN A

ORIGIN2 OUT PUT WHICH IS SOMETIMES RATHER MASSIVE. THIS SECTION IS INTENDED AS A BRIEF OUTLINE OF THE ORGANIZATION OF

ORIGEN2 OUTPUT. FOR DETAILS REFER TO THE USER'S MANUAL (ORNL/TM-7175, SECT. 8.2). THE ORIGEN2 OUTPUT IS EXTREMELY

HIERARCHICAL, AND IS ORGANIZED AS FOLLOWS:

## 0 CARD INPUT ECHO

## MISCELLANEOUS INPUT DATA (NEUTRON YIELDS, REPROCESSING LOSSES, ELEMENT CHEMICAL TOXICITIES)

## LISTING OF ORIGIN2 COMMANDS CURRENTLY BEING EXECUTED

## LISTING OF ORIGIN2 DATA LIBRARIES (IF SPECIFIED)

## DECAY LIBRARY

## ACTIVATION PRODUCTS

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ACTINIDES

FISSION PRODUCTS

CROSS SECTION/FISSION PRODUCT YIELD LIBRARY

ACTIVATION PRODUCTS, ACTINIDES, AND FISSION PRODUCTS

PHOTON LIBRARY

ACTIVATION PRODUCTS, ACTINIDES, AND FISSION PRODUCTS

OUTPUT 1

REACTIVITY AND BURNUP DATA

ACTIVATION PRODUCT TABLES

GRAM TABLES (NUCLIDE, ELEMENT, NUCLIDE SUMMARY, ELEMENT SUMMARY)

CURIE TABLES (NUCLIDE, ELEMENT, NUCLIDE SUMMARY, ELEMENT SUMMARY)

ETC. (DEPENDING ON THE OUTPUT OPTIONS SPECIFIED, MANY OF THESE TABLES MAY BE OMITTED

ACTINIDE TABLES

SAME SUBHEADINGS POSSIBLE AS UNDER ACTIVATION PRODUCT TABLES

FISSION PRODUCT TABLES

SAME SUBHEADINGS POSSIBLE AS UNDER ACTIVATION PRODUCT TABLES

NEUTRON PRODUCTION RATE TABLES: (ALPHA,N) AND SPONTANEOUS FISSION

PHOTON TABLES

ACTIVATION PRODUCTS (SUMMATION AND PRINCIPAL CONTRIBUTORS)

ACTINIDES (SUMMATION AND PRINCIPAL CONTRIBUTORS)

FISSION PRODUCTS (SUMMATION AND PRINCIPAL CONTRIBUTORS)

OUTPUT 2

SAME GENERAL CONTENT AND ORDER AS OUTPUT 1

OUTPUT N

SAME GENERAL CONTENT AND ORDER AS OUTPUT 1

TABLE OF CONTENTS (UNIT 12) FOR THE ABOVE (UNIT 6) OUTPUT

VARIABLE CROSS SECTION INFORMATION OUTPUT (UNIT 16)

DEBUGGING AND OTHER INTERNAL INFORMATION OUTPUT (UNIT 15)

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0 THE SCENARIO LISTED ABOVE CONSTITUTES A TYPICAL ORIGEN2 OUTPUT FOR MANY CASES. ONE POSSIBLE MODIFICATION IS THE USE OF AN

STP COMMAND TO EXECUTE AN ADDITIONAL SET OF INSTRUCTIONS AFTER THE FIRST SET HAS BEEN EXECUTED. IF THIS IS DONE, THE OUTPUT

WILL BEGIN WITH "MISCELLANEOUS INPUT DATA" IF NSTP=1, "ORIGEN2COMMANDS CURRENTLY BEING EXECUTED" IF NSTP=2, OR "OUTPUT 1"

FOR NSTP=3. ANOTHER OFTEN-USED OPTION IS TO EMPLOY BOTH THE PRIMARY (UNIT 6) AND ALTERNATE (UNIT 11) OUTPUT UNITS. IF BOTH

ARE ROUTED TO PAPER, THE TABLE OF CONTENTS FOR UNIT 11, WHICH IS ON UNIT 13, WILL IMMEDIATELY FOLLOW THE DEBUGGING AND

INTERNAL INFORMATION (UNIT 15) OUTPUT. THE "OUTPUT N" TABLES FOR UNIT 11 WILL BE PRINTED FOLLOWING THE TABLE OF CONTENTS.

1

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LISTING OF INPUT DATA ON UNIT = 5

INPUT UNIT	WRITE UNIT	CARD NUMBER	CARD IMAGE	
5	50	1	-1	
5	50	2	-1	
5	50	3	-1	
5	50	4	RDA *	BURNUP OF BWR 4.5% UO2 FUEL & ASSY HDWARE, 45,000
MWD/MT				
5	50	5	RDA	** CROSS SECTION LIBRARY = BWRU, 4 CYCLE
5	50	6	RDA	*** SCOTT B. LUDWIG, OAK RIDGE NATIONAL
LABORATORY				
5	50	7	RDA	**** (615) 574-7916, FTS 624-7916
5	50	8	RDA	-1 = FRESH BWR FUEL WITH IMPURITIES (1 MT = 1000 KG)
5	50	9	RDA	-2 = FRESH ZIRCALOY-4 COMPOSITION (1 KG)
5	50	10	RDA	-3 = FRESH ZIRCALOY-2 COMPOSITION (1 KG)
5	50	11	RDA	-4 = FRESH SS 304 COMPOSITION (1 KG)
5	50	12	RDA	-5 = FRESH SS 302 COMPOSITION (1 KG)
5	50	13	RDA	-6 = FRESH INCONEL X-750 COMPOSITION (1 KG)

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5 50 14 RDA WARNING: VECTORS ARE CHANGED WITH RESPECT TO  
CONTENT.

5 50 15 RDA THESE CHANGES WILL BE NOTED ON RDA CARDS.

5 50 16 CUT 5 1.0E-10 7 1.0E-14 9 1.0E-10 -1

5 50 17 LIP 0 0 0

5 50 18 RDA DECAY LIB XSECT LIB VAR. XSECT

5 50 19 LIB 0 1 2 3 251 252 253 9 50 0 1 4

5 50 20 RDA PHOTON LIB

5 50 21 PHO 101 102 103 10

5 50 22 TIT INITIAL COMP. OF UNIT AMOUNTS OF FUEL AND  
STRUCTURAL MAT'L'S

5 50 23 RDA READ FUEL COMPOSITION INCLUDING IMPURITIES (1000  
KG)

5 50 24 INP -1 1 -1 -1 1 1

5 50 25 RDA READ ZIRCALOY-4 COMPOSITION (1.0 KG)

5 50 26 INP -2 1 -1 -1 1 1

5 50 27 RDA READ ZIRCALOY-2 COMPOSITION (1.0 KG)

5 50 28 INP -3 1 -1 -1 1 1

5 50 29 RDA READ SS304 COMPOSITION (1.0 KG)

5 50 30 INP -4 1 -1 -1 1 1

5 50 31 RDA READ SS302 COMPOSITION (1.0 KG)

5 50 32 INP -5 1 -1 -1 1 1

5 50 33 RDA READ INCONEL X-750 COMPOSITION (1.0 KG)

5 50 34 INP -6 1 -1 -1 1 1

5 50 35 TIT IRRADIATION OF ONE METRIC TON OF BWRU FUEL

5 50 36 MOV -1 1 0 1.0

5 50 37 PCH 1 1 1

5 50 38 HED 1 CHARGE

5 50 39 BUP

5 50 40 IRP 265.45 25.90 1 2 4 2 BURNUP= 6,875 MWD/MTIHM

5 50 41 DEC 371.45 2 3 4 0 DECAY FOR 106.0 DAYS

5 50 42 IRP 636.90 25.90 3 4 4 0 BURNUP=13,750 MWD/MTIHM

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5 50 43 DEC 742.90 4 5 4 0 DECAY FOR 106.0 DAYS  
 5 50 44 IRP 1008.35 25.90 5 6 4 0 BURNUP=20,625 MWD/MTIHM

5 50 45 DEC 1114.35 6 7 4 0 DECAY FOR 106.0 DAYS  
 5 50 46 IRP 1379.80 25.90 7 8 4 0 BURNUP=27,500 MWD/MTIHM

5 50 47 DEC 1485.80 8 9 4 0 DECAY FOR 106.0 DAYS  
 5 50 48 IRP 1751.25 25.90 9 10 4 0 BURNUP=34,375 MWD/MTIHM

5 50 49 DEC 1857.25 10 11 4 0 DECAY FOR 106.0 DAYS  
 1 PAGE 4

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LISTING OF INPUT DATA ON UNIT = 5

INPUT UNIT	WRITE UNIT	CARD NUMBER	CARD IMAGE							
5 50	50	IRP	2122.70	25.90	11	12	4	0	BURNUP=41,250 MWD/MTIHM	
5 50	51	DEC	2228.70	12	13	4	0		DECAY FOR 106.0 DAYS	
5 50	52	IRP	2373.49	25.90	13	14	4	0	BURNUP=45,000 MWD/MTIHM	
5 50	53	BUP								
5 50	54	RDA	-10	=IRRADIATED U FUEL AT DISCHARGE						
5 50	55	MOV	14	-10	0	1.0				
5 50	56	PCH	-10	-10	-10					
5 50	57	RDA	IRRADIATION OF ZIRCALOY-2 CLADDING AT 1.000 FLUX							
5 50	58	TIT	IRRADIATION OF ZIRCALOY-2 CLADDING AT 1.000 FLUX							
5 50	59	MOV	-3	1	0	279.50	ZIRCALOY-2 CLAD			
5 50	60	HED	1				CHARGE			
5 50	61	IRF	265.45	-1.0	1	2	4	2	BURNUP= 6,875 MWD/MTIHM	
5 50	62	DEC	371.45	2	3	4	0		DECAY FOR 106.0 DAYS	
5 50	63	IRF	636.90	-1.0	3	4	4	0	BURNUP=13,750 MWD/MTIHM	
5 50	64	DEC	742.90	4	5	4	0		DECAY FOR 106.0 DAYS	
5 50	65	IRF	1008.35	-1.0	5	6	4	0	BURNUP=20,625 MWD/MTIHM	

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5 50 66 DEC 1114.35 6 7 4 0 DECAY FOR 106.0 DAYS  
5 50 67 IRF 1379.80 -1.0 7 8 4 0 BURNUP=27,500 MWD/MTIHM

5 50 68 DEC 1485.80 8 9 4 0 DECAY FOR 106.0 DAYS  
5 50 69 IRF 1751.25 -1.0 9 10 4 0 BURNUP=34,375 MWD/MTIHM

5 50 70 DEC 1857.25 10 11 4 0 DECAY FOR 106.0 DAYS  
5 50 71 IRF 2122.70 -1.0 11 12 4 0 BURNUP=41,250 MWD/MTIHM

5 50 72 DEC 2228.70 12 13 4 0 DECAY FOR 106.0 DAYS  
5 50 73 IRF 2373.49 -1.0 13 14 4 0 BURNUP=45,000 MWD/MTIHM

5 50 74 RDA -9 = IRRADIATED ZIRCALOY-2 CLADDING AT DISCHARGE

5 50 75 MOV 14 -9 0 1.0  
5 50 76 RDA IRRADIATION OF ZIRCALOY CLADDING AT 0.500 FLUX

5 50 77 TIT IRRADIATION OF ZIRCALOY CLADDING AT 0.500 FLUX

5 50 78 MOV -3 1 0 25.4 ZIRCALOY-2 CLAD  
5 50 79 MOV -3 2 0 304.90 TOTAL ZIRC-2 CLAD  
5 50 80 PCH 2 2 2  
5 50 81 HED 1 CHARGE  
5 50 82 IRF 265.45 -0.5 1 2 4 2 BURNUP= 6,875 MWD/MTIHM

5 50 83 DEC 371.45 2 3 4 0 DECAY FOR 106.0 DAYS  
5 50 84 IRF 636.90 -0.5 3 4 4 0 BURNUP=13,750 MWD/MTIHM

5 50 85 DEC 742.90 4 5 4 0 DECAY FOR 106.0 DAYS  
5 50 86 IRF 1008.35 -0.5 5 6 4 0 BURNUP=20,625 MWD/MTIHM

5 50 87 DEC 1114.35 6 7 4 0 DECAY FOR 106.0 DAYS  
5 50 88 IRF 1379.80 -0.5 7 8 4 0 BURNUP=27,500 MWD/MTIHM

5 50 89 DEC 1485.80 8 9 4 0 DECAY FOR 106.0 DAYS  
5 50 90 IRF 1751.25 -0.5 9 10 4 0 BURNUP=34,375 MWD/MTIHM

5 50 91 DEC 1857.25 10 11 4 0 DECAY FOR 106.0 DAYS

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5	50	92	IRF	2122.70	-0.5	11	12	4	0	BURNUP=41,250 MWD/MTIHM
5	50	93	DEC	2228.70		12	13	4	0	DECAY FOR 106.0 DAYS
5	50	94	IRF	2373.49	-0.5	13	14	4	0	BURNUP=45,000 MWD/MTIHM
5	50	95	RDA	-9	= IRRADIATED ZIRCALOY CLADDING AT DISCHARGE					
5	50	96	ADD	14	-9	0	1.0			TOTAL IRRAD ZIRC-2 CLAD
5	50	97	PCH	-9	-9	-9				
5	50	98	RDA							IRRADIATION OF ZIRCALOY-4 CHANNEL AT 1.000 FLUX
5	50	99	TIT							IRRADIATION OF ZIRCALOY-4 CHANNEL AT 1.000 FLUX

1

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LISTING OF INPUT DATA ON UNIT = 5

INPUT UNIT	WRITE UNIT	CARD NUMBER	CARD IMAGE								
5	50	100	MOV	-2	1	0	227.50	ZIRCALOY-4 CHANNEL			
5	50	101	HED	1				CHARGE			
5	50	102	IRF	265.45	-1.0	1	2	4	2	BURNUP= 6,875 MWD/MTIHM	
5	50	103	DEC	371.45		2	3	4	0	DECAY FOR 106.0 DAYS	
5	50	104	IRF	636.90	-1.0	3	4	4	0	BURNUP=13,750 MWD/MTIHM	
5	50	105	DEC	742.90		4	5	4	0	DECAY FOR 106.0 DAYS	
5	50	106	IRF	1008.35	-1.0	5	6	4	0	BURNUP=20,625 MWD/MTIHM	
5	50	107	DEC	1114.35		6	7	4	0	DECAY FOR 106.0 DAYS	
5	50	108	IRF	1379.80	-1.0	7	8	4	0	BURNUP=27,500 MWD/MTIHM	
5	50	109	DEC	1485.80		8	9	4	0	DECAY FOR 106.0 DAYS	
5	50	110	IRF	1751.25	-1.0	9	10	4	0	BURNUP=34,375 MWD/MTIHM	
5	50	111	DEC	1857.25		10	11	4	0	DECAY FOR 106.0 DAYS	
5	50	112	IRF	2122.70	-1.0	11	12	4	0	BURNUP=41,250 MWD/MTIHM	
5	50	113	DEC	2228.70		12	13	4	0	DECAY FOR 106.0 DAYS	

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5 50 114 IRF 2373.49 -1.0 13 14 4 0 BURNUP=45,000 MWD/MTIHM  
5 50 115 RDA -8 = IRRADIATED ZIRCALOY CHANNEL AT DISCHARGE  
5 50 116 MOV 14 -8 0 1.0  
5 50 117 RDA IRRADIATION OF ZIRCALOY-4 CHANNEL AT 0.500 FLUX  
5 50 118 TIT IRRADIATION OF ZIRCALOY-4 CHANNEL AT 0.500 FLUX  
5 50 119 MOV -2 1 0 20.70 ZIRCALOY-4 CHANNEL  
5 50 120 MOV -2 2 0 248.20 TOTAL ZIRCALOY-4 CHANNEL  
5 50 121 PCH 2 2 2  
5 50 122 HED 1 CHARGE  
5 50 123 IRF 265.45 -0.5 1 2 4 2 BURNUP= 6,875 MWD/MTIHM  
5 50 124 DEC 371.45 2 3 4 0 DECAY FOR 106.0 DAYS  
5 50 125 IRF 636.90 -0.5 3 4 4 0 BURNUP=13,750 MWD/MTIHM  
5 50 126 DEC 742.90 4 5 4 0 DECAY FOR 106.0 DAYS  
5 50 127 IRF 1008.35 -0.5 5 6 4 0 BURNUP=20,625 MWD/MTIHM  
5 50 128 DEC 1114.35 6 7 4 0 DECAY FOR 106.0 DAYS  
5 50 129 IRF 1379.80 -0.5 7 8 4 0 BURNUP=27,500 MWD/MTIHM  
5 50 130 DEC 1485.80 8 9 4 0 DECAY FOR 106.0 DAYS  
5 50 131 IRF 1751.25 -0.5 9 10 4 0 BURNUP=34,375 MWD/MTIHM  
5 50 132 DEC 1857.25 10 11 4 0 DECAY FOR 106.0 DAYS  
5 50 133 IRF 2122.70 -0.5 11 12 4 0 BURNUP=41,250 MWD/MTIHM  
5 50 134 DEC 2228.70 12 13 4 0 DECAY FOR 106.0 DAYS  
5 50 135 IRF 2373.49 -0.5 13 14 4 0 BURNUP=45,000 MWD/MTIHM  
5 50 136 RDA -8 = IRRADIATED ZIRCALOY CHANNEL AT DISCHARGE  
5 50 137 ADD 14 -8 0 1.0  
5 50 138 PCH -8 -8 -8  
5 50 139 RDA IRRADIATION OF ZIRCALOY GRID SPACERS AND INCONEL

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SPRINGS

5 50 140 TIT IRRADIATION OF ZIRCALOY GRID SPACERS AND INCONEL SPRINGS

5 50 141 MOV -2 1 0 10.60 ZIRCALOY GRIDS

5 50 142 ADD -6 1 0 1.80 INCONEL SPRINGS

5 50 143 PCH 1 1 1

5 50 144 HED 1 CHARGE

5 50 145 IRF 265.45 -1.0 1 2 4 2 BURNUP= 6,875 MWD/MTIHM

5 50 146 DEC 371.45 2 3 4 0 DECAY FOR 106.0 DAYS

5 50 147 IRF 636.90 -1.0 3 4 4 0 BURNUP=13,750 MWD/MTIHM

5 50 148 DEC 742.90 4 5 4 0 DECAY FOR 106.0 DAYS

5 50 149 IRF 1008.35 -1.0 5 6 4 0 BURNUP=20,625 MWD/MTIHM

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LISTING OF INPUT DATA ON UNIT = 5

INPUT UNIT	WRITE UNIT	CARD NUMBER	CARD IMAGE									
5 50	150	DEC	1114.35	6	7	4	0	DECAY FOR 106.0 DAYS				
5 50	151	IRF	1379.80	-1.0	7	8	4	0	BURNUP=27,500 MWD/MTIHM			
5 50	152	DEC	1485.80	8	9	4	0	DECAY FOR 106.0 DAYS				
5 50	153	IRF	1751.25	-1.0	9	10	4	0	BURNUP=34,375 MWD/MTIHM			
5 50	154	DEC	1857.25	10	11	4	0	DECAY FOR 106.0 DAYS				
5 50	155	IRF	2122.70	-1.0	11	12	4	0	BURNUP=41,250 MWD/MTIHM			
5 50	156	DEC	2228.70	12	13	4	0	DECAY FOR 106.0 DAYS				
5 50	157	IRF	2373.49	-1.0	13	14	4	0	BURNUP=45,000 MWD/MTIHM			
5 50	158	RDA	-7 = IRRADIATED ZIRCALOY GRID SPACERS AND INCONEL SPRINGS									
5 50	159	RDA	AT DISCHARGE									
5 50	160	MOV	14 -7 0 1.0									
5 50	161	PCH	-7 -7 -7									
5 50	162	RDA IRRAD. OF SS 304 END PIECES & INCONEL SPRINGS AT 0.130										

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FLUX

5 50 163 TIT IRRAD. OF SS 304 END PIECES & INCONEL SPRINGS AT 0.130

FLUX

5 50 164 MOV -4 1 0 37.00 SS 304 IN END PIECES

5 50 165 ADD -6 1 0 2.10 INCONEL X-750 EXPANSION SPRINGS

5 50 166 PCH 1 1 1

5 50 167 HED 1 CHARGE

5 50 168 IRF 265.45 -0.13 1 2 4 2 BURNUP= 6,875 MWD/MTIHM

5 50 169 DEC 371.45 2 3 4 0 DECAY FOR 106.0 DAYS

5 50 170 IRF 636.90 -0.13 3 4 4 0 BURNUP=13,750 MWD/MTIHM

5 50 171 DEC 742.90 4 5 4 0 DECAY FOR 106.0 DAYS

5 50 172 IRF 1008.35 -0.13 5 6 4 0 BURNUP=20,625 MWD/MTIHM

5 50 173 DEC 1114.35 6 7 4 0 DECAY FOR 106.0 DAYS

5 50 174 IRF 1379.80 -0.13 7 8 4 0 BURNUP=27,500 MWD/MTIHM

5 50 175 DEC 1485.80 8 9 4 0 DECAY FOR 106.0 DAYS

5 50 176 IRF 1751.25 -0.13 9 10 4 0 BURNUP=34,375 MWD/MTIHM

5 50 177 DEC 1857.25 10 11 4 0 DECAY FOR 106.0 DAYS

5 50 178 IRF 2122.70 -0.13 11 12 4 0 BURNUP=41,250 MWD/MTIHM

5 50 179 DEC 2228.70 12 13 4 0 DECAY FOR 106.0 DAYS

5 50 180 IRF 2373.49 -0.13 13 14 4 0 BURNUP=45,000 MWD/MTIHM

DISCHARGE  
5 50 181 RDA -6 = IRRAD. SS 304 END PIECES & INCONEL SPRINGS AT

5 50 182 MOV 14 -6 0 1.0

5 50 183 PCH -6 -6 -6

5 50 184 RDA IRRADIATION OF SS 302 IN PLENUM SPRINGS AT 0.500

FLUX

5 50 185 TIT IRRADIATION OF SS 302 IN PLENUM SPRINGS AT 0.500 FLUX

5 50 186 MOV -5 1 0 6.00 SS302

5 50 187 PCH 1 1 1

5 50 188 HED 1 CHARGE

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5	50	189	IRF	265.45	-0.5	1	2	4	2	BURNUP= 6,875 MWD/MTIHM
5	50	190	DEC	371.45		2	3	4	0	DECAY FOR 106.0 DAYS
5	50	191	IRF	636.90	-0.5	3	4	4	0	BURNUP=13,750 MWD/MTIHM
5	50	192	DEC	742.90		4	5	4	0	DECAY FOR 106.0 DAYS
5	50	193	IRF	1008.35	-0.5	5	6	4	0	BURNUP=20,625 MWD/MTIHM
5	50	194	DEC	1114.35		6	7	4	0	DECAY FOR 106.0 DAYS
5	50	195	IRF	1379.80	-0.5	7	8	4	0	BURNUP=27,500 MWD/MTIHM
5	50	196	DEC	1485.80		8	9	4	0	DECAY FOR 106.0 DAYS
5	50	197	IRF	1751.25	-0.5	9	10	4	0	BURNUP=34,375 MWD/MTIHM
5	50	198	DEC	1857.25		10	11	4	0	DECAY FOR 106.0 DAYS
5	50	199	IRF	2122.70	-0.5	11	12	4	0	BURNUP=41,250 MWD/MTIHM

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LISTING OF INPUT DATA ON UNIT = 5

INPUT	WRITE	CARD	CARD IMAGE											
UNIT	UNIT	NUMBER												
5	50	200	DEC	2228.70		12	13	4	0	DECAY FOR 106.0 DAYS				
5	50	201	IRF	2373.49	-0.5	13	14	4	0	BURNUP=45,000 MWD/MTIHM				
DISCHARGE														
5	50	202	RDA	-5	= IRRADIATED SS 302 IN PLENUM SPRINGS AT									
5	50	203	MOV	14	-5	0	1.0							
5	50	204	PCH	-5	-5	-5								
5	50	205	RDA	***** OUTPUT MODULE *****										
BURNUP (BWRU)														
5	50	206	TIT TEST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD											
5	50	207	BAS 1 MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM,											
4 CYCLE														
5	50	208	OPTL	6*8	7	8	8	8	14*8					
5	50	209	OPTA	6*8	7	8	8	8	14*8					
5	50	210	OPTF	6*8	7	8	8	8	14*8					
5	50	211	MOV	-10	1	0	1.0							

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```
5 50    212  ADD   -9  1  0  1.0
5 50    213  ADD   -8  1  0  1.0
5 50    214  ADD   -7  1  0  1.0
5 50    215  ADD   -6  1  0  1.0
5 50    216  ADD   -5  1  0  1.0
5 50    217  HED   1  ASSY DIS
5 50    218  RDA   ***** DECAY MODULE *****
5 50    219  DEC   0.5  1  2  5  2
5 50    220  DEC   1.0  2  3  5  0
5 50    221  DEC   2.0  3  4  5  0
5 50    222  DEC   5.0  4  5  5  0
5 50    223  DEC   10.0 5  6  5  0
5 50    224  DEC   26.0 6  7  5  0
5 50    225  OUT   7  1  -1  0
5 50    226  END
5 50    227  2 922340 247.0 922350 45000. 922380 954753. 0 0.0 FUEL 4.5%
5 50    228  4 030000 1.0 050000 1.0 060000 89.4 070000 25.0 FUEL IMPU
5 50    229  4 080000 134454. 090000 10.7 110000 15.0 120000 2.0 FUEL IMPU
5 50    230  4 130000 16.7 140000 12.1 150000 35.0 170000 5.3 FUEL IMPU
5 50    231  4 200000 2.0 220000 1.0 230000 3.0 240000 4.0 FUEL IMPU
5 50    232  4 250000 1.7 260000 18.0 270000 1.0 280000 24.0 FUEL IMPU
5 50    233  4 290000 1.0 300000 40.3 420000 10.0 470000 0.1 FUEL IMPU
5 50    234  4 480000 25.0 490000 2.0 500000 4.0 640000 1573. FUEL IMPU
5 50    235  4 740000 2.0 820000 1.0 830000 0.4 0 0.0 FUEL IMPU
5 50    236  0
5 50    237  4 400000 979.11 500000 16.0 260000 2.25 240000 1.25 ZIRC-4
5 50    238  4 280000 0.02 130000 0.024 050000 0.00033 480000 0.00025 ZIRC-4
5 50    239  4 060000 0.120 270000 0.010 290000 0.020 720000 0.078 ZIRC-4
```

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5 50 240 4 010000 0.013 250000 0.020 070000 0.080 080000 0.950 ZIRC-4  
5 50 241 4 160000 0.035 220000 0.020 740000 0.020 230000 0.020 ZIRC-4  
5 50 242 5 920000 0.0002 0 0.0 ZIRC-4  
5 50 243 0  
5 50 244 4 400000 979.63 500000 16.0 260000 1.5 240000 1.00 ZIRC-2  
5 50 245 4 280000 0.5 130000 0.024 050000 0.00033 480000 0.00025 ZIRC-2  
5 50 246 4 060000 0.120 270000 0.010 290000 0.020 720000 0.078 ZIRC-2  
5 50 247 4 010000 0.013 250000 0.020 070000 0.080 080000 0.950 ZIRC-2  
5 50 248 4 160000 0.035 220000 0.020 740000 0.020 230000 0.020 ZIRC-2  
5 50 249 5 920000 0.0002 0 0.0 ZIRC-2

1

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LISTING OF INPUT DATA ON UNIT = 5

INPUT UNIT	WRITE UNIT	CARD NUMBER	CARD IMAGE								
5	50	250	0								
5	50	251	4 260000 688.44	240000 190.0	280000 89.2	250000 20.0	SS-304				
5	50	252	4 060000 0.8	150000 0.45	160000 0.3	140000 10.0	SS-304				
5	50	253	4 070000 1.3	270000 0.8	0 0.0		SS-304				
5	50	254	0								
5	50	255	4 260000 697.74	240000 180.0	280000 89.2	250000 20.0	SS-302				
5	50	256	4 060000 1.5	150000 0.45	160000 0.3	140000 10.0	SS-302				
5	50	257	4 070000 1.3	270000 0.8	0 0.0		SS-302				
5	50	258	0								
5	50	259	4 260000 67.846	240000 149.66	280000 721.861	130000 7.982	INC-X-750				
5	50	260	4 060000 0.399	270000 6.485	290000 0.499	250000 6.984	INC-X-750				
5	50	261	4 070000 1.3	410000 8.98	160000 0.07	140000 2.993	INC-X-750				

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5 50 262 4 220000 24.943 0 0.0 INC-X-750  
5 50 263 0

1 OUTPUT UNIT = 6 PAGE 9

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NEUTRON YIELD PER NEUTRON-INDUCED FISSION

	NUCLIDE	YIELD								
	NUCLIDE	YIELD								
0	832090	0.0000	882230	0.0000	882260	0.0000	882280	0.0000	892270	
	0.0000	902270	0.0000							
0	902280	0.0000	902290	2.0490	902300	0.0000	902320	2.4180	902330	
	0.0000	902340	0.0000							
0	912310	0.0000	912320	0.0000	912330	2.6630	912341	0.0000	912340	
	0.0000	922300	0.0000							
0	922310	0.0000	922320	0.0000	922330	2.4990	922340	2.6310	922350	
	2.4210	922360	2.7340							
0	922370	0.0000	922380	2.8010	922390	0.0000	922400	0.0000	932360	
	0.0000	932370	3.0050							
0	932380	0.0000	932390	0.0000	942360	2.8700	942370	0.0000	942380	
	2.8330	942390	2.8750							
0	942400	3.1350	942410	2.9340	942420	3.2800	942430	0.0000	952410	
	3.2770	952421	3.1620							
0	952420	3.3600	952430	3.7320	952441	0.0000	952440	0.0000	962420	
	3.7460	962430	3.4340							
0	962440	3.7250	962450	3.8320	962460	3.8580	962470	3.5920	962480	
	3.7960	962490	0.0000							
0	972490	3.7600	982490	4.0620	982500	3.9700	982510	4.1400	982520	
	4.1260	982530	4.1500							
0	982540	0.0000	992530	0.0000	992541	0.0000	992540	0.0000	0	0.0000
	0	0.0000								

1 OUTPUT UNIT = 6 PAGE 10

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SPONTANEOUS FISSION NEUTRON YIELD, NEUT/FISSION

	NUCLIDE		NUCLIDE		NUCLIDE		NUCLIDE		NUCLIDE	
	NUCLIDE		NUCLIDE		NUCLIDE		NUCLIDE		NUCLIDE	
	922350	1.6950	922360	1.6500	922370	1.8720	922380	2.0000	922390	2.0480
	932361	1.7900								

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932360	1.7830	932370	1.8730	932380	1.9630	932390	2.0530	942360	2.2200
942370	1.8860								
942380	2.2800	942390	2.2400	942400	2.1600	942410	2.2500	942420	2.1500
942430	2.4300								
942440	2.3000	952400	2.2900	952410	2.3830	952420	2.4750	952421	2.5900
952430	2.5200								
952440	2.6570	952441	2.6650	962410	2.5000	962420	2.5900	962430	2.6870
962440	2.7600								
962450	2.8720	962460	3.0000	962480	3.3200	962500	3.5600	972490	3.7200
982490	3.4400								
982500	3.5600	982520	3.7250	982540	3.9000	992530	3.9200	992540	4.0400
992550	4.1600								

0THE REMAINING NEUTRON YIELDS ARE CALCULATED FROM THE EQUATION:  
NEUT/FISSION=(2.84+0.1225\*(AT WT-244)

1

OUTPUT UNIT = 6

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INDIVIDUAL ELEMENT FRACTIONAL RECOVERIES

ELEMENT	SET NUMBER									
	1	2	3	4	5	6	7	8	9	10
1	0.0000000	0.0000000	0.0005000	0.0000000	1.0000000	1.0000000	0.0000000	0.0000000	0.0000000	0.0000000
	0.0000000	0.9000000	1.0000000							
2	0.0000000	0.0000000	0.0005000	0.0000000	1.0000000	1.0000000	0.0000000	0.0000000	0.0000000	0.0000000
	0.0000000	0.0000000	1.0000000							
3	0.0000000	1.0000000	0.0005000	0.0000000	1.0000000	1.0000000	0.0000000	0.0000000	0.0000000	0.0000000
	0.0000000	0.0000000	1.0000000							
4	0.0000000	1.0000000	0.0005000	0.0000000	1.0000000	1.0000000	0.0000000	0.0000000	0.0000000	0.0000000
	0.0000000	0.0000000	1.0000000							
5	0.0000000	1.0000000	0.0005000	0.0000000	1.0000000	1.0000000	0.0000000	0.0000000	0.0000000	0.0000000
	0.0000000	0.0000000	1.0000000							
6	0.0000000	0.0000000	0.0005000	0.0000000	1.0000000	1.0000000	0.0000000	0.0000000	0.0000000	0.0000000
	0.0000000	0.0000000	1.0000000							
7	0.0000000	0.0000000	0.0005000	0.0000000	1.0000000	1.0000000	0.0000000	0.0000000	0.0000000	0.0000000
	0.0000000	0.0000000	1.0000000							
8	0.0000000	1.0000000	0.0005000	0.0000000	1.0000000	1.0000000	0.0000000	0.0000000	0.0000000	0.0000000
	0.0000000	0.0000000	1.0000000							
9	0.0000000	0.0010000	0.0005000	0.0000000	1.0000000	1.0000000	0.0000000	0.0000000	0.0000000	0.0000000
	0.0000000	0.0000000	1.0000000							

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10 00



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49 0.0000000 1.0000000 0.0005000 0.0000000 1.0000000 1.0000000 1.0000000  
0.0000000 0.0000000 1.0000000

1 OUTPUT UNIT = 6 PAGE 12

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INDIVIDUAL ELEMENT FRACTIONAL RECOVERIES

ELEMENT	SET NUMBER									
	1	2	3	4	5	6	7	8	9	10
50	0.0000000	1.0000000	0.0005000	0.0000000	1.0000000	1.0000000	1.0000000	1.0000000	0.0000000	0.0000000
51	0.0000000	1.0000000	0.0005000	0.0000000	1.0000000	1.0000000	1.0000000	1.0000000	0.0000000	0.0000000
52	0.0000000	1.0000000	0.0005000	0.0000000	1.0000000	1.0000000	1.0000000	1.0000000	0.0000000	0.0000000
53	0.0000000	0.0010000	0.0005000	0.0000000	1.0000000	1.0000000	1.0000000	1.0000000	0.0000000	0.0000000
54	0.0000000	0.0000000	0.0005000	0.0000000	1.0000000	1.0000000	0.0000000	0.0000000	0.0000000	0.0000000
55	0.0000000	1.0000000	0.0005000	0.0000000	1.0000000	1.0000000	1.0000000	1.0000000	0.0000000	0.0000000
56	0.0000000	1.0000000	0.0005000	0.0000000	1.0000000	1.0000000	1.0000000	1.0000000	0.0000000	0.0000000
57	0.0000000	1.0000000	0.0005000	0.0000000	1.0000000	1.0000000	1.0000000	1.0000000	0.0000000	0.0000000
58	0.0000000	1.0000000	0.0005000	0.0000000	1.0000000	1.0000000	1.0000000	1.0000000	0.0000000	0.0000000
59	0.0000000	1.0000000	0.0005000	0.0000000	1.0000000	1.0000000	1.0000000	1.0000000	0.0000000	0.0000000
60	0.0000000	1.0000000	0.0005000	0.0000000	1.0000000	1.0000000	1.0000000	1.0000000	0.0000000	0.0000000
61	0.0000000	1.0000000	0.0005000	0.0000000	1.0000000	1.0000000	1.0000000	1.0000000	0.0000000	0.0000000
62	0.0000000	1.0000000	0.0005000	0.0000000	1.0000000	1.0000000	1.0000000	1.0000000	0.0000000	0.0000000
63	0.0000000	1.0000000	0.0005000	0.0000000	1.0000000	1.0000000	1.0000000	1.0000000	0.0000000	0.0000000
64	0.0000000	1.0000000	0.0005000	0.0000000	1.0000000	1.0000000	1.0000000	1.0000000	0.0000000	0.0000000

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65 0.0

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0.0000000	0.0000000	1.0000000								
85	0.0000000	1.0000000	0.0005000	0.0000000	1.0000000	1.0000000	1.0000000	1.0000000		
0.0000000	0.0000000	1.0000000								
86	0.0000000	0.0000000	0.0005000	0.0000000	1.0000000	1.0000000	1.0000000	0.0000000		
0.0000000	0.0000000	1.0000000								
87	0.0000000	1.0000000	0.0005000	0.0000000	1.0000000	1.0000000	1.0000000	1.0000000		
0.0000000	0.0000000	1.0000000								
88	0.0000000	1.0000000	0.0005000	0.0000000	1.0000000	1.0000000	1.0000000	1.0000000		
0.0000000	0.0000000	1.0000000								
89	0.0000000	1.0000000	0.0005000	0.0000000	1.0000000	1.0000000	1.0000000	1.0000000		
0.0000000	0.0000000	1.0000000								
90	0.0000000	1.0000000	0.0005000	0.0000000	1.0000000	1.0000000	1.0000000	1.0000000		
0.0000000	0.0000000	1.0000000								
91	0.0000000	1.0000000	0.0005000	0.0000000	1.0000000	1.0000000	1.0000000	1.0000000		
0.0000000	0.0000000	1.0000000								
92	0.9950000	1.0000000	0.0005000	0.9990000	1.0000000	0.2000000	0.6000000			
1.0000000	0.0000000	1.0000000								
93	0.0000000	1.0000000	0.0005000	0.0000000	0.0500000	0.0500000	0.0000000			
0.0000000	0.0000000	1.0000000								
94	0.9950000	1.0000000	0.0005000	0.9999000	1.0000000	0.0200000	0.0000000			
0.0000000	0.0000000	1.0000000								
95	0.0000000	1.0000000	0.0005000	0.0000000	0.0010000	0.0010000	0.0000000			
0.0000000	0.0000000	1.0000000								
96	0.0000000	1.0000000	0.0005000	0.0000000	0.0010000	0.0010000	0.0000000			
0.0000000	0.0000000	1.0000000								
97	0.0000000	1.0000000	0.0005000	0.0000000	0.0010000	0.0010000	0.0000000			
0.0000000	0.0000000	1.0000000								
98	0.0000000	1.0000000	0.0005000	0.0000000	0.0010000	0.0010000	0.0000000			
0.0000000	0.0000000	1.0000000								
99	0.0000000	1.0000000	0.0005000	0.0000000	0.0010000	0.0010000	0.0000000			
0.0000000	0.0000000	1.0000000								

1

OUTPUT UNIT = 6

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GROUP FRACTIONAL RECOVERIES

| GROUP      | SET NUMBER |
|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| SET NUMBER |
| 1          | 2          | 3          | 4          | 5          | 6          | 7          | 8          | 9          | 10         |            |
| 1          | 0.0000000  | 1.0000000  | 0.0005000  | 0.0000000  | 1.0000000  | 1.0000000  | 1.0000000  | 1.0000000  | 1.0000000  |            |

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0.0000000	0.0000000	0.0000000						
2	0.0000000	1.0000000	0.0005000	0.0000000	1.0000000	1.0000000	0.0000000	
0.0000000	0.0000000	0.0000000						
3	0.0000000	1.0000000	0.0005000	0.0000000	1.0000000	1.0000000	0.0000000	
0.0000000	0.0000000	0.0000000						
4	0.9950000	1.0000000	0.0005000	0.9990000	1.0000000	0.2000000	0.6000000	
1.0000000	0.0000000	0.0000000						
5	0.0000000	1.0000000	0.0005000	0.0000000	0.0500000	0.0500000	0.0000000	
0.0000000	0.0000000	0.0000000						
6	0.9950000	1.0000000	0.0005000	0.9999000	1.0000000	0.0200000	0.0000000	
0.0000000	0.0000000	0.0000000						
7	0.0000000	1.0000000	0.0005000	0.0000000	0.0010000	0.0010000	0.0000000	
0.0000000	0.0000000	0.0000000						
8	0.0000000	1.0000000	0.0005000	0.0000000	0.0010000	0.0010000	0.0000000	
0.0000000	0.0000000	0.0000000						
9	0.0000000	1.0000000	0.0005000	0.0000000	0.0010000	0.0010000	0.0000000	
0.0000000	0.0000000	0.0000000						
10	0.0000000	1.0000000	0.0005000	0.0000000	0.0010000	0.0010000	0.0000000	
0.0000000	0.0000000	0.0000000						
11	0.0000000	1.0000000	0.0005000	0.0000000	0.0010000	0.0010000	0.0000000	
0.0000000	0.0000000	0.0000000						
12	0.0000000	0.0010000	0.0005000	0.0000000	1.0000000	1.0000000	1.0000000	
0.0000000	0.0000000	0.0000000						
13	0.0000000	0.0000000	0.0005000	0.0000000	1.0000000	1.0000000	0.0000000	
0.0000000	0.0000000	0.0000000						
14	0.0000000	0.0000000	0.0005000	0.0000000	1.0000000	1.0000000	0.0000000	
0.0000000	0.9000000	0.0000000						
15	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	
0.0000000	0.0000000	0.0000000						
16	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	
0.0000000	0.0000000	0.0000000						
17	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	
0.0000000	0.0000000	0.0000000						
18	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	
0.0000000	0.0000000	0.0000000						
19	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	
0.0000000	0.0000000	0.0000000						
20	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	
0.0000000	0.0000000	0.0000000						

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ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

ELEMENT ASSIGNMENTS TO FRACTIONAL RECOVERY GROUPS

0 ELEM GROUP ELEM GROUP ELEM GROUP ELEM GROUP ELEM GROUP ELEM  
GROUP ELEM GROUP ELEM GROUP ELEM GROUP ELEM GROUP

1	14	2	13	3	1	4	1	5	1	6	13	7	13	8	1	9	12		
10	13	11	1	12	1	13	1	14	1	15	1	16	1	17	12	18	13		
19	1	20	1	21	1	22	1	23	1	24	1	25	1	26	1	27	1		
28	1	29	1	30	1	31	1	32	1	33	1	34	1	35	12	36	13		
37	1	38	1	39	1	40	1	41	1	42	1	43	1	44	1	45	1		
46	1	47	1	48	1	49	1	50	1	51	1	52	1	53	12	54	13		
55	1	56	1	57	1	58	1	59	1	60	1	61	1	62	1	63	1		
64	1	65	1	66	1	67	1	68	1	69	1	70	1	71	1	72	1		
73	1	74	1	75	1	76	1	77	1	78	1	79	1	80	1	81	1		
82	1	83	1	84	1	85	1	86	13	87	1	88	1	89	1	90	2		
91	3	92	4	93	5	94	6	95	7	96	8	97	9	98	10	99	11		

1

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ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

CHEMICAL TOXICITIES, GRAMS PER M\*\*\*3 WATER

ONUCLIDE	TOXICITY	NUCLIDE																	
1	3.50E+03	2	2.00E-01	3	5.00E+00	4	1.00E+00	5	1.00E+00	6									
4.00E+02																			
7	1.00E-02	8	9.45E+05	9	1.00E+00	10	1.00E+00	11	1.00E+03	12									
1.00E+01																			
13	1.00E-02	14	5.00E+00	15	1.00E-02	16	5.00E+01	17	1.50E-01	18									
1.00E+01																			
19	1.00E+03	20	3.00E+01	21	5.00E-01	22	1.00E-01	23	1.00E-01	24									
2.00E-02																			
25	1.00E-02	26	5.00E-02	27	5.00E-02	28	5.00E-02	29	1.00E-02	30									
5.00E-02																			
31	2.00E-01	32	5.00E-01	33	1.00E-02	34	1.00E-02	35	3.00E+00	36									
4.00E+01																			
37	5.00E+01	38	1.00E+01	39	1.00E-03	40	1.00E+00	41	2.00E-02	42									
5.00E-01																			
43	1.00E+02	44	1.00E+00	45	5.00E-02	46	5.00E-02	47	1.00E-03	48									
1.00E-02																			
49	2.00E-02	50	5.00E-02	51	5.00E-02	52	2.00E-01	53	1.00E+01	54									

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1.50E+02

55	5.00E+00	56	5.00E-01	57	1.00E+00	58	2.00E+00	59	1.00E+00	60
2.00E-01										
61	1.00E+00	62	2.00E-01	63	2.00E-01	64	2.00E-01	65	5.00E-01	66
1.00E+00										
67	1.00E+00	68	1.00E-01	69	2.00E-01	70	1.00E-01	71	1.00E-01	72
5.00E-02										
73	1.00E+00	74	1.00E+02	75	1.00E+01	76	1.00E+00	77	8.00E-01	78
3.00E-01										
79	2.00E-02	80	2.00E-03	81	5.00E-03	82	1.00E-02	83	1.00E-01	84
2.00E-01										
85	1.00E+01	86	5.00E+02	87	5.00E+00	88	1.00E-03	89	2.00E-02	90
5.00E-04										
91	5.00E-03	92	5.00E-01	93	8.00E-03	94	8.00E-04	95	4.00E-02	96
5.00E-01										
97	5.00E-03	98	1.00E-02	99	1.00E-02					

1 OUTPUT UNIT = 6 PAGE 16

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

1 0 RDA \* RDA \* BURNUP OF BWR 4.5% UO2 FUEL & ASSY HDWARE, 45,000  
MWD/MT \*

2 0 RDA \* RDA \*\*\* CROSS SECTION LIBRARY = BWRU, 4 CYCLE

\*

3 0 RDA \* RDA \*\*\* SCOTT B. LUDWIG, OAK RIDGE NATIONAL LABORATORY

\*

4 0 RDA \* RDA \*\*\*\* (615) 574-7916, FTS 624-7916 \*

5 0 RDA \* RDA -1 = FRESH BWR FUEL WITH IMPURITIES (1 MT = 1000 KG)

\*

6 0 RDA \* RDA -2 = FRESH ZIRCALOY-4 COMPOSITION (1 KG) \*

7 0 RDA \* RDA -3 = FRESH ZIRCALOY-2 COMPOSITION (1 KG) \*

8 0 RDA \* RDA -4 = FRESH SS 304 COMPOSITION (1 KG) \*

9 0 RDA \* RDA -5 = FRESH SS 302 COMPOSITION (1 KG) \*

10 0 RDA \* RDA -6 = FRESH INCONEL X-750 COMPOSITION (1 KG) \*

\*

11 0 RDA \* RDA WARNING: VECTORS ARE CHANGED WITH RESPECT TO  
CONTENT. \*

12 0 RDA \* RDA THESE CHANGES WILL BE NOTED ON RDA CARDS.

\*

13 0 CUT \* CUT 5 1.0E-10 7 1.0E-14 9 1.0E-10 -1 \*

14 0 LIP \* LIP 0 0 0 \*

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```

15 0 RDA * RDA    DECAY LIB  XSECT LIB      VAR. XSECT      *
16 0 LIB * LIB   0 1 2 3  251 252 253  9 50 0 1   4      *
17 0 RDA * RDA    PHOTON LIB                  *
18 0 PHO * PHO   101 102 103 10                  *
19 0 TIT * TIT    INITIAL COMP. OF UNIT AMOUNTS OF FUEL AND STRUCTURAL
MAT'LS      *
20 0 RDA * RDA    READ FUEL COMPOSITION INCLUDING IMPURITIES (1000 KG)
*
21 0 INP * INP   -1 1 -1 -1 1 1                  *
22 0 RDA * RDA    READ ZIRCALOY-4 COMPOSITION (1.0 KG)      *
23 0 INP * INP   -2 1 -1 -1 1 1                  *
24 0 RDA * RDA    READ ZIRCALOY-2 COMPOSITION (1.0 KG)      *
25 0 INP * INP   -3 1 -1 -1 1 1                  *
26 0 RDA * RDA    READ SS304 COMPOSITION (1.0 KG)      *
27 0 INP * INP   -4 1 -1 -1 1 1                  *
28 0 RDA * RDA    READ SS302 COMPOSITION (1.0 KG)      *
29 0 INP * INP   -5 1 -1 -1 1 1                  *
30 0 RDA * RDA    READ INCONEL X-750 COMPOSITION (1.0 KG)
*
31 0 INP * INP   -6 1 -1 -1 1 1                  *
32 0 TIT * TIT    IRRADIATION OF ONE METRIC TON OF BWRU FUEL
*
33 0 MOV * MOV   -1 1 0 1.0                  *
34 0 PCH * PCH   1 1 1                  *
35 0 HED * HED   1                      CHARGE      *
36 0 BUP * BUP                  *
37 0 IRP * IRP   265.45 25.90 1 2 4 2 BURNUP=6,875 MWD/MTIHM      *
38 0 DEC * DEC   371.45     2 3 4 0 DECAY FOR 106.0 DAYS      *
39 0 IRP * IRP   636.90 25.90 3 4 4 0 BURNUP=13,750 MWD/MTIHM      *
40 0 DEC * DEC   742.90     4 5 4 0 DECAY FOR 106.0 DAYS      *
41 0 IRP * IRP   1008.35 25.90 5 6 4 0 BURNUP=20,625 MWD/MTIHM      *
42 0 DEC * DEC   1114.35     6 7 4 0 DECAY FOR 106.0 DAYS      *
43 0 IRP * IRP   1379.80 25.90 7 8 4 0 BURNUP=27,500 MWD/MTIHM      *
44 0 DEC * DEC   1485.80     8 9 4 0 DECAY FOR 106.0 DAYS      *
45 0 IRP * IRP   1751.25 25.90 9 10 4 0 BURNUP=34,375 MWD/MTIHM      *
46 0 DEC * DEC   1857.25     10 11 4 0 DECAY FOR 106.0 DAYS      *
47 0 IRP * IRP   2122.70 25.90 11 12 4 0 BURNUP=41,250 MWD/MTIHM      *
48 0 DEC * DEC   2228.70     12 13 4 0 DECAY FOR 106.0 DAYS      *
49 0 IRP * IRP   2373.49 25.90 13 14 4 0 BURNUP=45,000 MWD/MTIHM      *

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ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

```

50 0 BUP * BUP *
51 0 RDA * RDA -10 = IRRADIATED U FUEL AT DISCHARGE *
52 0 MOV * MOV 14 -10 0 1.0 *
53 0 PCH * PCH -10 -10 -10 *
54 0 RDA * RDA IRRADIATION OF ZIRCALOY-2 CLADDING AT 1.000 FLUX *
55 0 TIT * TIT IRRADIATION OF ZIRCALOY-2 CLADDING AT 1.000 FLUX *
56 0 MOV * MOV -3 1 0 279.50 ZIRCALOY-2 CLAD *
57 0 HED * HED 1 CHARGE *
58 0 IRF * IRF 265.45 -1.0 1 2 4 2 BURNUP= 6,875 MWD/MTIHM *
59 0 DEC * DEC 371.45 2 3 4 0 DECAY FOR 106.0 DAYS *
60 0 IRF * IRF 636.90 -1.0 3 4 4 0 BURNUP=13,750 MWD/MTIHM *
61 0 DEC * DEC 742.90 4 5 4 0 DECAY FOR 106.0 DAYS *
62 0 IRF * IRF 1008.35 -1.0 5 6 4 0 BURNUP=20,625 MWD/MTIHM *
63 0 DEC * DEC 1114.35 6 7 4 0 DECAY FOR 106.0 DAYS *
64 0 IRF * IRF 1379.80 -1.0 7 8 4 0 BURNUP=27,500 MWD/MTIHM *
65 0 DEC * DEC 1485.80 8 9 4 0 DECAY FOR 106.0 DAYS *
66 0 IRF * IRF 1751.25 -1.0 9 10 4 0 BURNUP=34,375 MWD/MTIHM *
67 0 DEC * DEC 1857.25 10 11 4 0 DECAY FOR 106.0 DAYS *
68 0 IRF * IRF 2122.70 -1.0 11 12 4 0 BURNUP=41,250 MWD/MTIHM *
69 0 DEC * DEC 2228.70 12 13 4 0 DECAY FOR 106.0 DAYS *
70 0 IRF * IRF 2373.49 -1.0 13 14 4 0 BURNUP=45,000 MWD/MTIHM *
71 0 RDA * RDA -9 = IRRADIATED ZIRCALOY-2 CLADDING AT DISCHARGE *
72 0 MOV * MOV 14 -9 0 1.0 *
73 0 RDA * RDA IRRADIATION OF ZIRCALOY CLADDING AT 0.500 FLUX *
74 0 TIT * TIT IRRADIATION OF ZIRCALOY CLADDING AT 0.500 FLUX *
75 0 MOV * MOV -3 1 0 25.4 ZIRCALOY-2 CLAD *
76 0 MOV * MOV -3 2 0 304.90 TOTAL ZIRC-2 CLAD *
77 0 PCH * PCH 2 2 2 *
78 0 HED * HED 1 CHARGE *
79 0 IRF * IRF 265.45 -0.5 1 2 4 2 BURNUP= 6,875 MWD/MTIHM *
80 0 DEC * DEC 371.45 2 3 4 0 DECAY FOR 106.0 DAYS *
81 0 IRF * IRF 636.90 -0.5 3 4 4 0 BURNUP=13,750 MWD/MTIHM *

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```

82 0 DEC * DEC 742.90 4 5 4 0 DECAY FOR 106.0 DAYS      *
83 0 IRF * IRF 1008.35 -0.5 5 6 4 0 BURNUP=20,625 MWD/MTIHM   *
84 0 DEC * DEC 1114.35 6 7 4 0 DECAY FOR 106.0 DAYS      *
85 0 IRF * IRF 1379.80 -0.5 7 8 4 0 BURNUP=27,500 MWD/MTIHM   *
86 0 DEC * DEC 1485.80 8 9 4 0 DECAY FOR 106.0 DAYS      *
87 0 IRF * IRF 1751.25 -0.5 9 10 4 0 BURNUP=34,375 MWD/MTIHM   *
88 0 DEC * DEC 1857.25 10 11 4 0 DECAY FOR 106.0 DAYS      *
89 0 IRF * IRF 2122.70 -0.5 11 12 4 0 BURNUP=41,250 MWD/MTIHM   *
90 0 DEC * DEC 2228.70 12 13 4 0 DECAY FOR 106.0 DAYS      *
91 0 IRF * IRF 2373.49 -0.5 13 14 4 0 BURNUP=45,000 MWD/MTIHM   *
92 0 RDA * RDA -9 = IRRADIATED ZIRCALOY CLADDING AT DISCHARGE
* 
93 0 ADD * ADD 14 -9 0 1.0 TOTAL IRRAD ZIRC-2 CLAD      *
94 0 PCH * PCH -9 -9 -9                                *
95 0 RDA * RDA IRRADIATION OF ZIRCALOY-4 CHANNEL AT 1.000 FLUX
*
96 0 TIT * TIT IRRADIATION OF ZIRCALOY-4 CHANNEL AT 1.000 FLUX
*
97 0 MOV * MOV -2 1 0 227.50 ZIRCALOY-4 CHANNEL      *
98 0 HED * HED 1 CHARGE                                *
99 0 IRF * IRF 265.45 -1.0 1 2 4 2 BURNUP= 6,875 MWD/MTIHM      *
1                               OUTPUT UNIT = 6          PAGE 18
ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12
100 0 DEC * DEC 371.45 2 3 4 0 DECAY FOR 106.0 DAYS      *
101 0 IRF * IRF 636.90 -1.0 3 4 4 0 BURNUP=13,750 MWD/MTIHM   *
102 0 DEC * DEC 742.90 4 5 4 0 DECAY FOR 106.0 DAYS      *
103 0 IRF * IRF 1008.35 -1.0 5 6 4 0 BURNUP=20,625 MWD/MTIHM   *
104 0 DEC * DEC 1114.35 6 7 4 0 DECAY FOR 106.0 DAYS      *
105 0 IRF * IRF 1379.80 -1.0 7 8 4 0 BURNUP=27,500 MWD/MTIHM   *
106 0 DEC * DEC 1485.80 8 9 4 0 DECAY FOR 106.0 DAYS      *
107 0 IRF * IRF 1751.25 -1.0 9 10 4 0 BURNUP=34,375 MWD/MTIHM   *
108 0 DEC * DEC 1857.25 10 11 4 0 DECAY FOR 106.0 DAYS      *
109 0 IRF * IRF 2122.70 -1.0 11 12 4 0 BURNUP=41,250 MWD/MTIHM   *
110 0 DEC * DEC 2228.70 12 13 4 0 DECAY FOR 106.0 DAYS      *
111 0 IRF * IRF 2373.49 -1.0 13 14 4 0 BURNUP=45,000 MWD/MTIHM   *
112 0 RDA * RDA -8 = IRRADIATED ZIRCALOY CHANNEL AT DISCHARGE
*
113 0 MOV * MOV 14 -8 0 1.0                                *
114 0 RDA * RDA IRRADIATION OF ZIRCALOY-4 CHANNEL AT 0.500 FLUX

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\*

115 0 TIT \* TIT IRRADIATION OF ZIRCALOY-4 CHANNEL AT 0.500 FLUX

\*

116 0 MOV \* MOV -2 1 0 20.70 ZIRCALOY-4 CHANNEL \*

117 0 MOV \* MOV -2 2 0 248.20 TOTAL ZIRCALOY-4 CHANNEL

\*

118 0 PCH \* PCH 2 2 2

\*

119 0 HED \* HED 1 CHARGE \*

120 0 IRF \* IRF 265.45 -0.5 1 2 4 2 BURNUP= 6,875 MWD/MTIHM \*

121 0 DEC \* DEC 371.45 2 3 4 0 DECAY FOR 106.0 DAYS \*

122 0 IRF \* IRF 636.90 -0.5 3 4 4 0 BURNUP=13,750 MWD/MTIHM \*

123 0 DEC \* DEC 742.90 4 5 4 0 DECAY FOR 106.0 DAYS \*

124 0 IRF \* IRF 1008.35 -0.5 5 6 4 0 BURNUP=20,625 MWD/MTIHM \*

125 0 DEC \* DEC 1114.35 6 7 4 0 DECAY FOR 106.0 DAYS \*

126 0 IRF \* IRF 1379.80 -0.5 7 8 4 0 BURNUP=27,500 MWD/MTIHM \*

127 0 DEC \* DEC 1485.80 8 9 4 0 DECAY FOR 106.0 DAYS \*

128 0 IRF \* IRF 1751.25 -0.5 9 10 4 0 BURNUP=34,375 MWD/MTIHM \*

129 0 DEC \* DEC 1857.25 10 11 4 0 DECAY FOR 106.0 DAYS \*

130 0 IRF \* IRF 2122.70 -0.5 11 12 4 0 BURNUP=41,250 MWD/MTIHM \*

131 0 DEC \* DEC 2228.70 12 13 4 0 DECAY FOR 106.0 DAYS \*

132 0 IRF \* IRF 2373.49 -0.5 13 14 4 0 BURNUP=45,000 MWD/MTIHM \*

133 0 RDA \* RDA -8 = IRRADIATED ZIRCALOY CHANNEL AT DISCHARGE

\*

134 0 ADD \* ADD 14 -8 0 1.0

\*

135 0 PCH \* PCH -8 -8 -8

\*

136 0 RDA \* RDA IRRADIATION OF ZIRCALOY GRID SPACERS AND INCONEL SPRINGS \*

137 0 TIT \* TIT IRRADIATION OF ZIRCALOY GRID SPACERS AND INCONEL SPRINGS \*

138 0 MOV \* MOV -2 1 0 10.60 ZIRCALOY GRIDS \*

139 0 ADD \* ADD -6 1 0 1.80 INCONEL SPRINGS \*

140 0 PCH \* PCH 1 1 1

\*

141 0 HED \* HED 1 CHARGE \*

142 0 IRF \* IRF 265.45 -1.0 1 2 4 2 BURNUP= 6,875 MWD/MTIHM \*

143 0 DEC \* DEC 371.45 2 3 4 0 DECAY FOR 106.0 DAYS \*

144 0 IRF \* IRF 636.90 -1.0 3 4 4 0 BURNUP=13,750 MWD/MTIHM \*

145 0 DEC \* DEC 742.90 4 5 4 0 DECAY FOR 106.0 DAYS \*

146 0 IRF \* IRF 1008.35 -1.0 5 6 4 0 BURNUP=20,625 MWD/MTIHM \*

147 0 DEC \* DEC 1114.35 6 7 4 0 DECAY FOR 106.0 DAYS \*

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148	0 IRF * IRF	1379.80	-1.0	7	8	4	0	BURNUP=27,500 MWD/MTIHM	*
149	0 DEC * DEC	1485.80		8	9	4	0	DECAY FOR 106.0 DAYS	*
1								OUTPUT UNIT = 6	PAGE 19
ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12									
150	0 IRF * IRF	1751.25	-1.0	9	10	4	0	BURNUP=34,375 MWD/MTIHM	*
151	0 DEC * DEC	1857.25		10	11	4	0	DECAY FOR 106.0 DAYS	*
152	0 IRF * IRF	2122.70	-1.0	11	12	4	0	BURNUP=41,250 MWD/MTIHM	*
153	0 DEC * DEC	2228.70		12	13	4	0	DECAY FOR 106.0 DAYS	*
154	0 IRF * IRF	2373.49	-1.0	13	14	4	0	BURNUP=45,000 MWD/MTIHM	*
155	0 RDA * RDA	-7	= IRRADIATED ZIRCALOY GRID SPACERS AND INCONEL SPRINGS	*					
156	0 RDA * RDA		AT DISCHARGE						*
157	0 MOV * MOV	14	-7	0	1.0				*
158	0 PCH * PCH	-7	-7	-7					*
159	0 RDA * RDA	IRRAD. OF SS 304 END PIECES & INCONEL SPRINGS AT 0.130 FLUX	*						
160	0 TIT * TIT	IRRAD. OF SS 304 END PIECES & INCONEL SPRINGS AT 0.130 FLUX	*						
161	0 MOV * MOV	-4	1	0	37.00	SS 304 IN END PIECES			*
162	0 ADD * ADD	-6	1	0	2.10	INCONEL X-750 EXPANSION SPRINGS			
*									
163	0 PCH * PCH	1	1	1					*
164	0 HED * HED	1				CHARGE			*
165	0 IRF * IRF	265.45	-0.13	1	2	4	2	BURNUP= 6,875 MWD/MTIHM	*
166	0 DEC * DEC	371.45		2	3	4	0	DECAY FOR 106.0 DAYS	*
167	0 IRF * IRF	636.90	-0.13	3	4	4	0	BURNUP=13,750 MWD/MTIHM	*
168	0 DEC * DEC	742.90		4	5	4	0	DECAY FOR 106.0 DAYS	*
169	0 IRF * IRF	1008.35	-0.13	5	6	4	0	BURNUP=20,625 MWD/MTIHM	*
170	0 DEC * DEC	1114.35		6	7	4	0	DECAY FOR 106.0 DAYS	*
171	0 IRF * IRF	1379.80	-0.13	7	8	4	0	BURNUP=27,500 MWD/MTIHM	*
172	0 DEC * DEC	1485.80		8	9	4	0	DECAY FOR 106.0 DAYS	*
173	0 IRF * IRF	1751.25	-0.13	9	10	4	0	BURNUP=34,375 MWD/MTIHM	*
174	0 DEC * DEC	1857.25		10	11	4	0	DECAY FOR 106.0 DAYS	*
175	0 IRF * IRF	2122.70	-0.13	11	12	4	0	BURNUP=41,250 MWD/MTIHM	*
*									
176	0 DEC * DEC	2228.70		12	13	4	0	DECAY FOR 106.0 DAYS	*
177	0 IRF * IRF	2373.49	-0.13	13	14	4	0	BURNUP=45,000 MWD/MTIHM	*
*									
178	0 RDA * RDA	-6	= IRRAD. SS 304 END PIECES & INCONEL SPRINGS AT						

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DISCHARGE \*

179 0 MOV \* MOV 14 -6 0 1.0 \*  
180 0 PCH \* PCH -6 -6 -6 \*  
181 0 RDA \* RDA IRRADIATION OF SS 302 IN PLENUM SPRINGS AT 0.500 FLUX  
\*  
182 0 TIT \* TIT IRRADIATION OF SS 302 IN PLENUM SPRINGS AT 0.500 FLUX  
\*  
183 0 MOV \* MOV -5 1 0 6.00 SS302 \*  
184 0 PCH \* PCH 1 1 1 \*  
185 0 HED \* HED 1 CHARGE \*  
186 0 IRF \* IRF 265.45 -0.5 1 2 4 2 BURNUP= 6,875 MWD/MTIHM \*  
187 0 DEC \* DEC 371.45 2 3 4 0 DECAY FOR 106.0 DAYS \*  
188 0 IRF \* IRF 636.90 -0.5 3 4 4 0 BURNUP=13,750 MWD/MTIHM \*  
189 0 DEC \* DEC 742.90 4 5 4 0 DECAY FOR 106.0 DAYS \*  
190 0 IRF \* IRF 1008.35 -0.5 5 6 4 0 BURNUP=20,625 MWD/MTIHM \*  
191 0 DEC \* DEC 1114.35 6 7 4 0 DECAY FOR 106.0 DAYS \*  
192 0 IRF \* IRF 1379.80 -0.5 7 8 4 0 BURNUP=27,500 MWD/MTIHM \*  
193 0 DEC \* DEC 1485.80 8 9 4 0 DECAY FOR 106.0 DAYS \*  
194 0 IRF \* IRF 1751.25 -0.5 9 10 4 0 BURNUP=34,375 MWD/MTIHM \*  
195 0 DEC \* DEC 1857.25 10 11 4 0 DECAY FOR 106.0 DAYS \*  
196 0 IRF \* IRF 2122.70 -0.5 11 12 4 0 BURNUP=41,250 MWD/MTIHM \*  
197 0 DEC \* DEC 2228.70 12 13 4 0 DECAY FOR 106.0 DAYS \*  
198 0 IRF \* IRF 2373.49 -0.5 13 14 4 0 BURNUP=45,000 MWD/MTIHM \*  
199 0 RDA \* RDA -5 = IRRADIATED SS 302 IN PLENUM SPRINGS AT DISCHARGE  
\*

1

OUTPUT UNIT = 6

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ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

200 0 MOV \* MOV 14 -5 0 1.0 \*  
201 0 PCH \* PCH -5 -5 -5 \*  
202 0 RDA \* RDA \*\*\*\*\* OUTPUT MODULE \*\*\*\*\* \*  
203 0 TIT \* TIT TEST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP  
(BWRU) \*  
204 0 BAS \* BAS 1 MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM, 4  
CYCLE \*  
205 0 OPTL \* OPTL 6\*8 7 8 8 8 14\*8 \*  
206 0 OPTA \* OPTA 6\*8 7 8 8 8 14\*8 \*  
207 0 OPTF \* OPTF 6\*8 7 8 8 8 14\*8 \*  
208 0 MOV \* MOV -10 1 0 1.0 \*  
209 0 ADD \* ADD -9 1 0 1.0 \*

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210	0 ADD	*	ADD	-8	1	0	1.0		*
211	0 ADD	*	ADD	-7	1	0	1.0		*
212	0 ADD	*	ADD	-6	1	0	1.0		*
213	0 ADD	*	ADD	-5	1	0	1.0		*
214	0 HED	*	HED	1	ASSY	DIS		*	
215	0 RDA	*	RDA	***** DECAY MODULE *****					*
216	0 DEC	*	DEC	0.5	1	2	5	2	*
217	0 DEC	*	DEC	1.0	2	3	5	0	*
218	0 DEC	*	DEC	2.0	3	4	5	0	*
219	0 DEC	*	DEC	5.0	4	5	5	0	*
220	0 DEC	*	DEC	10.0	5	6	5	0	*
221	0 DEC	*	DEC	26.0	6	7	5	0	*
222	0 OUT	*	OUT	7	1	-1	0		*
223	0 END	*	END						*
OSUM OF YIELDS FOR EACH FISSILE ISOTOPE:								0.0000E+00	0.0000E+00
2.0003E+00 1.9997E+00 2.0006E+00 2.0001E+00									
0ISOTOPES FOR WHICH YIELDS ARE EXPLICITLY ACCOUNTED FOR: 922350 922380									
942390 942410									
1	OUTPUT UNIT = 6							PAGE 21	
ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12									

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)

POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC

0 REACTIVITY AND BURNUP DATA

BASIS=MTIHM 4.5% UO2 FUEL ASSY;BURNUP=45,000 MWD/MTIHM, 4 CYCLE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

TIME, SEC	0.00E+00	1.58E+07	3.16E+07	6.31E+07	1.58E+08	3.16E+08	8.20E+08
NEUT. FLUX	0.00E+00						
SP POW,MW	0.00E+00						
BURNUP,MWD	0.00E+00						
K INFINITY	0.00000	0.87373	0.87064	0.86466	0.84837	0.82636	0.78554
NEUT PRODN	0.00E+00	8.45E+03	8.42E+03	8.37E+03	8.22E+03	8.01E+03	7.60E+03
NEUT DESTN	0.00E+00	9.67E+03	9.68E+03	9.68E+03	9.69E+03	9.69E+03	9.68E+03
TOT BURNUP	0.00E+00						
AVG N FLUX	0.00E+00						

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AVG SP POW 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00

SIZE OF MMAX(I): MMAX= 1 #= 876 MMAX= 2 #= 432 MMAX= 3 #= 142 MMAX= 4 #= 50 MMAX= 5 #= 85 MMAX= 6 #= 58  
MMAX= 7 #= 46 MMAX= 8 #= 0 MMAX= 9 #= 0 MMAX=10 #= 0 MMAX=11  
#= 0 MMAX=12 #= 0

THE NUMBER OF NON-ZERO TERMS IN A=6466

THE NUMBER OF NON-ZERO FISSION PRODUCT YIELDS=3242

ILITE= 688 IACT= 129 IFP= 879 ITOT=1696

THE NUMBER OF NON-ZERO NATURAL ABUNDANCES= 437

THE NUMBER OF NON-ZERO PHOTON YIELDS= 7903

THE MAXIMUM NUMBER OF TERMS IN AP= 396

1 OUTPUT UNIT = 6 PAGE 22

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)

+ ACTIVATION PRODUCTS

POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC

0 7 SUMMARY TABLE: RADIOACTIVITY, CURIES

MTIHM 4.5% UO2 FUEL ASSY;BURNUP=45,000 MWD/MTIHM, 4 CYCLE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

H 3	2.734E+02	2.659E+02	2.585E+02	2.444E+02	2.065E+02	1.560E+02	6.354E+01
H 4	3.761E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
HE 6	1.588E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
LI 8	2.031E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BE 8	2.051E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BE 10	1.493E-06						
BE 11	2.495E-06	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
B 12	1.763E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
C 14	1.964E+00	1.964E+00	1.964E+00	1.964E+00	1.963E+00	1.962E+00	1.958E+00
C 15	2.421E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
N 16	1.516E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
O 19	3.176E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00

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F 20	3.131E+00	0.000E+00						
NE 23	9.322E-01	0.000E+00						
NA 24	2.460E+02	0.000E+00						
NA 24M	1.025E+02	0.000E+00						
NA 25	1.541E-02	0.000E+00						
MG 27	5.128E+00	0.000E+00						
AL 28	1.745E+02	0.000E+00						
AL 29	4.078E-01	0.000E+00						
AL 30	3.944E-04	0.000E+00						
SI 31	4.116E+01	0.000E+00						
SI 32	1.602E-08	1.601E-08	1.600E-08	1.598E-08	1.593E-08	1.585E-08	1.558E-08	
P 32	1.210E+02	1.732E-02	2.494E-06	1.598E-08	1.593E-08	1.585E-08	1.558E-08	
P 33	4.311E-03	2.727E-05	1.724E-07	6.896E-12	4.410E-25	0.000E+00	0.000E+00	
P 34	5.747E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
S 35	1.970E+01	4.674E+00	1.109E+00	6.245E-02	1.115E-05	6.310E-12	6.845E-32	
S 37	1.469E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
CL 36	1.395E-02							
CL 38	6.339E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
CL 38M	7.546E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
AR 37	3.323E-01	8.949E-03	2.410E-04	1.749E-07	6.677E-17	2.282E-32	0.000E+00	
AR 39	7.207E-05	7.198E-05	7.188E-05	7.170E-05	7.115E-05	7.024E-05	6.740E-05	
AR 41	6.769E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
K 40	3.928E-09							
K 42	6.699E-03	2.867E-13	2.837E-13	2.778E-13	2.608E-13	2.348E-13	1.678E-13	
K 43	2.060E-04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
K 44	7.826E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
CA 41	2.237E-04							
CA 45	3.027E-01	1.392E-01	6.402E-02	1.354E-02	1.281E-04	5.421E-08	8.687E-19	
CA 47	5.925E-04	4.493E-16	3.407E-28	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
CA 49	3.946E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
SC 46	1.078E+00	2.379E-01	5.252E-02	2.560E-03	2.964E-07	8.151E-14	0.000E+00	
SC 46M	8.778E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
SC 47	2.035E+00	1.799E-15	1.304E-27	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
SC 48	1.900E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
SC 49	2.319E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
SC 50	3.255E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
TI 51	5.065E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
V 52	6.451E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
V 53	4.082E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	

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OUTPUT UNIT = 6

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ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)

+

ACTIVATION PRODUCTS

POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC

0

7 SUMMARY TABLE: RADIOACTIVITY, CURIES

MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM, 4 CYCLE

	ASSY DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
--	----------	-------	-------	-------	-------	--------	--------

V 54	4.455E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CR 51	1.152E+04	1.195E+02	1.240E+00	1.334E-04	1.663E-16	0.000E+00	0.000E+00
CR 55	1.681E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
MN 54	2.791E+02	1.862E+02	1.242E+02	5.522E+01	4.860E+00	8.460E-02	1.986E-07
MN 56	2.138E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
MN 57	1.069E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
MN 58	3.317E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
FE 55	2.960E+03	2.591E+03	2.268E+03	1.737E+03	7.806E+02	2.058E+02	2.891E+00
FE 59	1.630E+02	9.781E+00	5.871E-01	2.115E-03	9.891E-11	6.004E-23	0.000E+00
CO 58	1.161E+03	1.941E+02	3.245E+01	9.072E-01	1.982E-05	3.385E-13	0.000E+00
CO 60	2.746E+03	2.571E+03	2.407E+03	2.111E+03	1.423E+03	7.370E+02	8.984E+01
CO 60M	4.350E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CO 61	3.453E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CO 62	1.414E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NI 59	1.335E+00						
NI 63	1.996E+02	1.989E+02	1.981E+02	1.966E+02	1.923E+02	1.851E+02	1.641E+02
NI 65	2.244E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NI 66	1.188E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CU 64	2.780E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CU 66	6.167E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CU 67	8.332E-05	3.909E-26	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZN 65	8.289E+01	4.933E+01	2.935E+01	1.039E+01	4.615E-01	2.569E-03	1.570E-10
ZN 69	8.058E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZN 69M	5.417E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZN 71	1.203E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZN 71M	1.261E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GA 70	1.191E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00

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GA 72 4.412E-03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
GA 72M 1.363E-04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
GE 71 5.714E-03 1.253E-07 2.748E-12 1.322E-21 0.000E+00 0.000E+00 0.000E+00  
GE 71M 4.663E-04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SR 89 6.159E+01 5.021E+00 4.094E-01 2.721E-03 7.993E-10 1.037E-20 0.000E+00  
SR 90 3.346E-03 3.307E-03 3.268E-03 3.191E-03 2.971E-03 2.638E-03 1.802E-03  
SR 91 1.324E+01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SR 93 4.553E-02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
Y 89M 4.496E-04 6.810E-21 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
Y 90 2.521E+03 3.308E-03 3.269E-03 3.192E-03 2.972E-03 2.638E-03 1.803E-03  
Y 90M 1.828E-04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
Y 91 1.517E+02 1.744E+01 2.004E+00 2.646E-02 6.091E-08 2.445E-17 0.000E+00  
Y 92 3.118E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
Y 93 4.553E-02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
Y 94 9.471E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
Y 96 6.060E-02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
ZR 89 4.503E-04 6.820E-21 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
ZR 93 3.860E-01 3.860E-01 3.860E-01 3.860E-01 3.860E-01 3.860E-01 3.860E-01  
ZR 95 6.888E+04 9.525E+03 1.317E+03 2.518E+01 1.761E-04 4.500E-13 0.000E+00  
ZR 97 1.172E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
NB 92 1.324E-01 5.139E-07 1.995E-12 3.006E-23 0.000E+00 0.000E+00 0.000E+00  
NB 93M 5.003E-02 5.800E-02 6.577E-02 8.072E-02 1.213E-01 1.765E-01 2.825E-01  
NB 94 3.969E-02 3.968E-02 3.968E-02 3.968E-02 3.967E-02 3.965E-02  
NB 95 5.911E+04 1.858E+04 2.853E+03 5.781E+01 3.909E-04 9.991E-13 0.000E+00

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OUTPUT UNIT = 6

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ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)

+

ACTIVATION PRODUCTS

POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC

0

7 SUMMARY TABLE: RADIOACTIVITY, CURIES

MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM, 4 CYCLE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

NB 95M 4.841E+02 7.066E+01 9.771E+00 1.868E-01 1.306E-06 3.339E-15 0.000E+00

NB 96 5.486E+01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

NB 97 1.172E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

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NB 97M	1.109E+05	0.000E+00									
NB 98	2.411E-04	0.000E+00									
NB100	9.326E-06	0.000E+00									
MO 93M	3.511E-02	0.000E+00									
MO 93	7.669E-04	7.669E-04	7.668E-04	7.666E-04	7.662E-04	7.654E-04	7.630E-04				
MO 99	1.440E+02	1.469E-18	0.000E+00								
MO101	6.111E+00	0.000E+00									
TC 98	5.111E-11										
TC 99	1.563E-04	1.569E-04									
TC100	3.461E+00	0.000E+00									
TC101	6.111E+00	0.000E+00									
RU103	1.602E-03	6.387E-05	2.545E-06	4.043E-09	1.621E-17	1.597E-31	0.000E+00				
RU105	1.154E-08	0.000E+00									
RH104	7.505E-05	0.000E+00									
RH104M	3.477E-06	0.000E+00									
RH105	1.082E-08	0.000E+00									
RH106	9.204E-06	4.699E-15	3.332E-15	1.675E-15	2.129E-16	6.851E-18	1.142E-22				
PD107	1.145E-11										
PD107M	1.277E-07	0.000E+00									
PD109	5.120E-02	0.000E+00									
PD109M	8.327E-04	0.000E+00									
PD111	1.043E-03	0.000E+00									
PD111M	1.452E-04	0.000E+00									
AG106	5.710E-04	1.945E-10	6.625E-17	7.689E-30	0.000E+00						
AG108	1.027E+01	1.331E-03	1.328E-03	1.320E-03	1.299E-03	1.264E-03	1.158E-03				
AG108M	1.500E-02	1.496E-02	1.492E-02	1.484E-02	1.459E-02	1.420E-02	1.301E-02				
AG109M	9.704E-01	6.998E-01	5.327E-01	3.087E-01	6.007E-02	3.925E-03	6.345E-07				
AG110	2.310E+01	7.797E-03	4.698E-03	1.706E-03	8.164E-05	5.151E-07	4.696E-14				
AG110M	9.729E-01	5.862E-01	3.532E-01	1.283E-01	6.138E-03	3.873E-05	3.531E-12				
AG111	1.180E-01	4.932E-09	2.061E-16	3.651E-31	0.000E+00						
AG111M	5.905E-02	0.000E+00									
AG112	9.672E-05	0.000E+00									
CD107	1.100E+00	0.000E+00									
CD109	9.193E-01	6.998E-01	5.327E-01	3.087E-01	6.007E-02	3.925E-03	6.345E-07				
CD111M	1.874E+00	0.000E+00									
CD115	2.424E+02	0.000E+00									
CD115M	1.899E+01	1.111E+00	6.502E-02	2.226E-04	8.929E-12	4.198E-24	0.000E+00				
CD117	7.318E+00	0.000E+00									
CD117M	2.766E-01	0.000E+00									

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CD119 1.257E-03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CD121 3.786E-04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
IN113M 1.193E+03 3.975E+02 1.323E+02 1.467E+01 2.007E-02 3.360E-07 1.748E-22  
IN114 5.944E+02 1.765E+01 1.369E+00 8.240E-03 1.795E-09 1.416E-20 0.000E+00  
IN114M 2.378E+02 1.845E+01 1.431E+00 8.610E-03 1.876E-09 1.479E-20 0.000E+00  
IN116 6.093E+01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
IN116M 4.863E+01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
IN117 4.405E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
IN117M 6.927E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

1 OUTPUT UNIT = 6 PAGE 25

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)  
+ ACTIVATION PRODUCTS  
POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC  
0 7 SUMMARY TABLE: RADIOACTIVITY, CURIES  
MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM, 4 CYCLE

	ASSY DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
IN118	1.654E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
IN119	1.207E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
IN119M	1.257E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
IN121	3.105E-04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SN113	1.193E+03	3.972E+02	1.323E+02	1.466E+01	2.006E-02	3.358E-07	1.747E-22
SN113M	6.836E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SN117M	1.194E+04	1.417E+00	1.683E-04	2.371E-12	0.000E+00	0.000E+00	0.000E+00
SN119M	8.741E+03	5.215E+03	3.111E+03	1.107E+03	4.988E+01	2.845E-01	1.881E-08
SN121	5.698E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SN121M	1.596E+00	1.585E+00	1.574E+00	1.552E+00	1.489E+00	1.389E+00	1.112E+00
SN123	4.300E+02	1.614E+02	6.057E+01	8.532E+00	2.382E-02	1.321E-06	3.170E-20
SN123M	2.244E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SN125	3.715E+03	7.365E-03	1.460E-08	5.736E-20	0.000E+00	0.000E+00	0.000E+00
SN125M	2.942E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SB122	8.037E+02	3.512E-18	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SB122M	7.087E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SB124	3.793E+01	4.631E+00	5.655E-01	8.432E-03	2.795E-08	2.059E-17	0.000E+00
SB124M	1.315E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00

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SB125 3.118E+03 2.783E+03 2.456E+03 1.912E+03 9.024E+02 2.582E+02 4.711E+00  
SB126 6.920E+01 2.542E-03 9.335E-08 1.259E-16 0.000E+00 0.000E+00 0.000E+00  
SB126M 6.902E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
TE123M 6.109E+00 2.121E+00 7.366E-01 8.882E-02 1.553E-04 3.958E-09 7.900E-24  
TE125M 6.846E+02 6.694E+02 5.980E+02 4.665E+02 2.202E+02 6.301E+01 1.149E+00  
TE127 9.462E-01 1.818E-02 5.692E-03 5.580E-04 5.255E-07 4.755E-12 3.453E-28  
TE127M 5.929E-02 1.856E-02 5.811E-03 5.696E-04 5.365E-07 4.854E-12 3.525E-28  
TE129 2.450E-06 1.020E-09 2.357E-11 1.259E-14 1.917E-24 0.000E+00 0.000E+00  
TE129M 6.780E-08 1.567E-09 3.621E-11 1.934E-14 2.946E-24 0.000E+00 0.000E+00  
I128 4.229E-02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
I130 6.735E-08 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
I130M 2.854E-08 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
XE127 8.465E-08 2.617E-09 8.091E-11 7.733E-14 6.752E-23 0.000E+00 0.000E+00  
XE129M 1.382E-05 1.856E-12 2.493E-19 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
PM149 7.734E-09 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
PM151 7.999E-04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
PM152 4.499E-06 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SM151 6.023E-06 6.029E-06 6.006E-06 5.960E-06 5.823E-06 5.603E-06 4.954E-06  
SM153 5.095E-03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SM155 8.907E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
EU152 1.210E-03 1.179E-03 1.150E-03 1.092E-03 9.375E-04 7.266E-04 3.215E-04  
EU152M 2.164E-06 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
EU154 1.458E+02 1.401E+02 1.345E+02 1.241E+02 9.747E+01 6.514E+01 1.794E+01  
EU155 8.869E+01 8.270E+01 7.712E+01 6.706E+01 4.409E+01 2.192E+01 2.342E+00  
EU156 1.729E+03 4.145E-01 9.934E-05 5.707E-12 0.000E+00 0.000E+00 0.000E+00  
GD153 2.690E+02 1.594E+02 9.449E+01 3.320E+01 1.439E+00 7.704E-03 4.146E-10  
GD155M 4.243E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
GD159 3.240E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
GD161 3.294E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
GD162 7.630E-01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
TB160 7.555E+03 1.312E+03 2.278E+02 6.868E+00 1.883E-04 4.691E-12 0.000E+00  
TB161 4.454E+03 5.065E-05 5.759E-13 7.443E-29 0.000E+00 0.000E+00 0.000E+00  
TB162 7.478E-01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

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OUTPUT UNIT = 6

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ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)

+

ACTIVATION PRODUCTS

POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00

Scientific Notebook #170-10e

James Weldy

12/27/00

20-1402-762

N/CM\*\*2-SEC

0            7 SUMMARY TABLE: RADIOACTIVITY, CURIES  
MTIHM 4.5% UO2 FUEL ASSY;BURNUP=45,000 MWD/MTIHM, 4 CYCLE

	ASSY DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
DY165	9.257E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
DY165M	4.047E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
DY166	2.467E+00	1.596E-16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
HO166	1.583E+02	2.378E-16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
HO166M	3.232E-03	3.231E-03	3.230E-03	3.228E-03	3.223E-03	3.213E-03	3.184E-03
ER167M	2.098E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ER169	2.063E-02	2.924E-08	4.145E-14	8.329E-26	0.000E+00	0.000E+00	0.000E+00
ER171	7.485E-09	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TM170	1.411E-03	5.271E-04	1.969E-04	2.750E-05	7.470E-08	3.963E-12	8.260E-26
TM170M	2.246E-04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TM171	1.201E-05	1.002E-05	8.369E-06	5.833E-06	1.975E-06	3.248E-07	1.006E-09
TM172	4.930E-06	8.858E-27	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TM173	4.487E-06	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
YB175	3.751E-08	2.837E-21	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
YB175M	2.654E-08	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
LU176	7.235E-11						
LU176M	1.215E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
LU177	4.938E+00	1.110E-03	4.904E-04	9.577E-05	7.131E-07	2.024E-10	9.047E-22
LU177M	1.092E-02	4.826E-03	2.133E-03	4.165E-04	3.101E-06	8.803E-10	3.934E-21
HF175	1.819E+01	2.981E+00	4.887E-01	1.313E-02	2.547E-07	3.568E-15	0.000E+00
HF178M	2.481E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
HF179M	4.082E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
HF180M	4.750E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
HF181	8.724E+02	4.405E+01	2.225E+00	5.673E-03	9.408E-11	1.015E-23	0.000E+00
HF182	6.681E-07						
TA182	9.061E+01	3.014E+01	1.003E+01	1.109E+00	1.503E-03	6.930E-07	6.681E-07
TA182M	1.617E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TA183	2.237E+02	3.717E-09	6.175E-20	0.000E+00	0.000E+00	0.000E+00	0.000E+00
W181	1.297E+00	4.564E-01	1.606E-01	1.988E-02	3.768E-05	1.095E-09	3.328E-24
W183M	2.256E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
W185	4.037E+01	7.482E+00	1.387E+00	4.763E-02	1.931E-06	9.234E-14	0.000E+00
W185M	5.438E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
W187	8.248E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00

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James Weldy

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W188	1.574E+00	2.540E-01	4.099E-02	1.068E-03	1.885E-08	2.257E-16	0.000E+00
RE186	3.383E+01	9.390E-14	2.606E-28	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RE187	4.186E-08	4.191E-08	4.191E-08	4.191E-08	4.191E-08	4.191E-08	4.191E-08
RE188	3.190E+02	2.567E-01	4.142E-02	1.079E-03	1.904E-08	2.280E-16	0.000E+00
RE188M	3.106E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RE189	1.298E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
OS190M	3.693E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
OS191	4.226E-02	1.172E-05	3.165E-09	2.307E-16	0.000E+00	0.000E+00	0.000E+00
OS191M	3.163E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
OS193	1.115E-06	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
OS194	3.788E-10	3.575E-10	3.375E-10	3.007E-10	2.126E-10	1.193E-10	1.879E-11
IR192	1.307E-02	2.363E-03	4.273E-04	1.399E-05	1.855E-08	1.780E-08	1.700E-08
IR192M	1.830E-08	1.828E-08	1.825E-08	1.820E-08	1.804E-08	1.778E-08	1.698E-08
IR194	4.843E-04	3.577E-10	3.376E-10	3.008E-10	2.127E-10	1.194E-10	1.880E-11
IR194M	2.552E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
PT193	1.903E-07	1.910E-07	1.909E-07	1.906E-07	1.898E-07	1.885E-07	1.844E-07
PT193M	3.752E-05	6.155E-18	1.004E-30	0.000E+00	0.000E+00	0.000E+00	0.000E+00
PT195M	3.237E-08	1.005E-25	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00

1

OUTPUT UNIT = 6

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ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)

+

ACTIVATION PRODUCTS

POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC

0

7 SUMMARY TABLE: RADIOACTIVITY, CURIES

MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM, 4 CYCLE

ASSY DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
----------	-------	-------	-------	-------	--------	--------

TL206	2.029E-08	2.029E-08	2.029E-08	2.029E-08	2.029E-08	2.029E-08
PB205	2.192E-09	2.192E-09	2.192E-09	2.192E-09	2.192E-09	2.192E-09
PB209	4.784E-04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BI208	2.282E-08	2.282E-08	2.282E-08	2.282E-08	2.282E-08	2.282E-08
BI210	3.358E-02	3.600E-13	3.860E-24	0.000E+00	0.000E+00	0.000E+00
BI210M	2.037E-08	2.037E-08	2.037E-08	2.037E-08	2.037E-08	2.037E-08
BI211	2.643E-08	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
PO210	2.419E-02	1.020E-02	4.088E-03	6.564E-04	2.717E-06	3.716E-10
PO211	2.923E-07	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00

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James Weldy

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SUMTOT 6.253E+05 4.584E+04 1.655E+04 8.200E+03 3.928E+03 1.698E+03 3.517E+02

0TOTAL 6.253E+05 4.584E+04 1.655E+04 8.200E+03 3.928E+03 1.698E+03 3.517E+02

1 OUTPUT UNIT = 6 PAGE 28

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)

+ ACTIVATION PRODUCTS

POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC

0 7 SUMMARY TABLE: RADIOACTIVITY, CURIES  
MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM, 4 CYCLE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

H	2.772E+02	2.659E+02	2.585E+02	2.444E+02	2.065E+02	1.560E+02	6.354E+01
HE	1.588E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
LI	2.031E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BE	2.051E+00	1.493E-06	1.493E-06	1.493E-06	1.493E-06	1.493E-06	1.493E-06
B	1.763E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
C	2.618E+01	1.964E+00	1.964E+00	1.964E+00	1.963E+00	1.962E+00	1.958E+00
N	1.516E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
O	3.176E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
F	3.131E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NE	9.322E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NA	3.485E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
MG	5.128E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
AL	1.749E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SI	4.116E+01	1.601E-08	1.600E-08	1.598E-08	1.593E-08	1.585E-08	1.558E-08
P	1.211E+02	1.735E-02	2.666E-06	1.599E-08	1.593E-08	1.585E-08	1.558E-08
S	1.971E+01	4.674E+00	1.109E+00	6.245E-02	1.115E-05	6.310E-12	6.845E-32
CL	6.428E+00	1.395E-02	1.395E-02	1.395E-02	1.395E-02	1.395E-02	1.395E-02
AR	3.324E-01	9.021E-03	3.129E-04	7.187E-05	7.115E-05	7.024E-05	6.740E-05
K	6.984E-03	3.928E-09	3.928E-09	3.928E-09	3.928E-09	3.928E-09	3.928E-09
CA	3.430E-01	1.394E-01	6.425E-02	1.376E-02	3.518E-04	2.238E-04	2.237E-04
SC	3.547E+00	2.379E-01	5.252E-02	2.560E-03	2.964E-07	8.151E-14	0.000E+00
TI	5.065E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
V	6.455E+02	7.841E-15	7.841E-15	7.841E-15	7.841E-15	7.841E-15	7.841E-15
CR	1.169E+04	1.195E+02	1.240E+00	1.334E-04	1.663E-16	0.000E+00	0.000E+00
MN	2.166E+04	1.862E+02	1.242E+02	5.522E+01	4.860E+00	8.460E-02	1.986E-07

## Scientific Notebook #170-10e

James Weldy

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FE	3.123E+03	2.601E+03	2.268E+03	1.737E+03	7.806E+02	2.058E+02	2.891E+00
CO	8.291E+03	2.765E+03	2.440E+03	2.112E+03	1.423E+03	7.370E+02	8.984E+01
NI	4.254E+02	2.002E+02	1.995E+02	1.980E+02	1.936E+02	1.865E+02	1.655E+02
CU	3.396E+02	3.909E-26	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZN	1.690E+02	4.933E+01	2.935E+01	1.039E+01	4.615E-01	2.569E-03	1.570E-10
GA	1.196E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GE	6.180E-03	1.253E-07	2.748E-12	1.322E-21	0.000E+00	0.000E+00	0.000E+00
SR	7.488E+01	5.025E+00	4.127E-01	5.912E-03	2.971E-03	2.638E-03	1.802E-03
Y	2.994E+03	1.744E+01	2.007E+00	2.965E-02	2.972E-03	2.638E-03	1.803E-03
ZR	1.860E+05	9.525E+03	1.317E+03	2.557E+01	3.861E-01	3.860E-01	3.860E-01
NB	2.877E+05	1.865E+04	2.863E+03	5.812E+01	1.613E-01	2.161E-01	3.222E-01
MO	1.501E+02	7.669E-04	7.668E-04	7.666E-04	7.662E-04	7.654E-04	7.630E-04
TC	9.573E+00	1.569E-04	1.569E-04	1.569E-04	1.569E-04	1.569E-04	1.569E-04
RU	1.602E-03	6.387E-05	2.545E-06	4.043E-09	2.290E-16	6.851E-18	1.142E-22
RH	8.775E-05	3.170E-11	2.813E-11	2.215E-11	1.081E-11	3.272E-12	7.145E-14
PD	5.322E-02	1.145E-11	1.145E-11	1.145E-11	1.145E-11	1.145E-11	1.145E-11
AG	3.551E+01	1.310E+00	9.069E-01	4.548E-01	8.218E-02	1.943E-02	1.417E-02
CD	2.728E+02	1.811E+00	5.977E-01	3.089E-01	6.007E-02	3.925E-03	6.345E-07
IN	2.147E+03	4.336E+02	1.351E+02	1.469E+01	2.007E-02	3.360E-07	1.150E-13
SN	3.535E+04	5.776E+03	3.305E+03	1.132E+03	5.141E+01	1.673E+00	1.112E+00
SB	4.043E+03	2.787E+03	2.456E+03	1.912E+03	9.024E+02	2.582E+02	4.711E+00
TE	6.917E+02	6.716E+02	5.988E+02	4.666E+02	2.202E+02	6.301E+01	1.149E+00
I	4.229E-02	7.731E-14	7.732E-14	7.732E-14	7.732E-14	7.732E-14	7.732E-14
XE	1.391E-05	2.619E-09	8.091E-11	7.733E-14	6.752E-23	0.000E+00	0.000E+00
PM	8.044E-04	7.097E-14	6.152E-14	4.721E-14	2.137E-14	5.702E-15	8.319E-17
SM	5.190E-03	6.029E-06	6.006E-06	5.960E-06	5.823E-06	5.603E-06	4.954E-06
EU	1.964E+03	2.232E+02	2.117E+02	1.912E+02	1.416E+02	8.706E+01	2.028E+01
GD	3.597E+04	1.594E+02	9.449E+01	3.320E+01	1.439E+00	7.704E-03	4.152E-10
TB	1.201E+04	1.312E+03	2.278E+02	6.868E+00	1.883E-04	4.691E-12	0.000E+00
DY	1.333E+03	1.596E-16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
HO	1.583E+02	3.231E-03	3.230E-03	3.228E-03	3.223E-03	3.213E-03	3.184E-03
ER	2.119E+00	2.924E-08	4.145E-14	8.329E-26	0.000E+00	0.000E+00	0.000E+00
TM	1.657E-03	5.371E-04	2.053E-04	3.333E-05	2.049E-06	3.248E-07	1.006E-09
YB	6.405E-08	2.837E-21	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
LU	1.710E+01	5.936E-03	2.623E-03	5.122E-04	3.814E-06	1.155E-09	7.235E-11
HF	5.022E+03	4.703E+01	2.713E+00	1.880E-02	9.229E-07	6.681E-07	6.681E-07
TA	3.145E+02	3.014E+01	1.003E+01	1.109E+00	1.503E-03	6.930E-07	6.681E-07
W	8.704E+02	8.192E+00	1.588E+00	6.858E-02	3.963E-05	1.095E-09	3.328E-24
RE	6.634E+02	2.567E-01	4.142E-02	1.079E-03	6.095E-08	4.191E-08	4.191E-08

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OS	7.393E-02	1.172E-05	3.502E-09	3.007E-10	2.126E-10	1.193E-10	1.879E-11
IR	1.358E-02	2.363E-03	4.273E-04	1.401E-05	3.680E-08	3.570E-08	3.400E-08
PT	3.774E-05	1.910E-07	1.909E-07	1.906E-07	1.898E-07	1.885E-07	1.844E-07
TL	2.029E-08	2.029E-08	2.029E-08	2.029E-08	2.029E-08	2.029E-08	2.029E-08
PB	4.784E-04	2.192E-09	2.192E-09	2.192E-09	2.192E-09	2.192E-09	2.192E-09
BI	3.358E-02	4.319E-08	4.319E-08	4.319E-08	4.319E-08	4.319E-08	4.319E-08
PO	2.419E-02	1.020E-02	4.088E-03	6.564E-04	2.717E-06	3.716E-10	8.147E-11
SUMTOT	6.253E+05	4.584E+04	1.655E+04	8.200E+03	3.928E+03	1.698E+03	3.517E+02
0TOTAL	6.253E+05	4.584E+04	1.655E+04	8.200E+03	3.928E+03	1.698E+03	3.517E+02
0	CUMULATIVE TABLE TOTALS						

AP+FP	6.253E+05	4.584E+04	1.655E+04	8.200E+03	3.928E+03	1.698E+03	3.517E+02
ACT+FP	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
AP+ACT+FP	6.253E+05	4.584E+04	1.655E+04	8.200E+03	3.928E+03	1.698E+03	3.517E+02
1	OUTPUT UNIT = 6						PAGE 29
ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12							

*	ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)						
+	ACTINIDES+DAUGHTERS						
	POWER=	1.00000E+00	MW,	BURNUP=	1.00000E+00	MWD,	FLUX= 1.00E+00
	N/CM**2-SEC						
0	7 SUMMARY TABLE: RADIOACTIVITY, CURIES						
	MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM, 4 CYCLE						

	ASSY DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
TL207	1.704E-06	2.117E-06	2.560E-06	3.499E-06	6.026E-06	9.969E-06	2.079E-05
TL208	2.628E-03	3.540E-03	4.482E-03	6.332E-03	1.086E-02	1.453E-02	1.444E-02
TL209	2.845E-08	9.983E-09	9.985E-09	1.001E-08	1.013E-08	1.041E-08	1.208E-08
PB209	1.321E-06	4.622E-07	4.623E-07	4.634E-07	4.688E-07	4.821E-07	5.594E-07
PB210	9.788E-09	1.125E-08	1.258E-08	1.574E-08	3.011E-08	7.525E-08	5.012E-07
PB211	1.708E-06	2.123E-06	2.568E-06	3.508E-06	6.043E-06	9.997E-06	2.085E-05
PB212	7.316E-03	9.852E-03	1.247E-02	1.762E-02	3.023E-02	4.043E-02	4.019E-02
PB214	8.094E-08	9.174E-08	1.035E-07	1.295E-07	2.290E-07	4.689E-07	1.919E-06
BI210	9.846E-09	1.126E-08	1.259E-08	1.575E-08	3.012E-08	7.526E-08	5.012E-07
BI211	1.708E-06	2.123E-06	2.568E-06	3.508E-06	6.043E-06	9.997E-06	2.085E-05
BI212	7.316E-03	9.852E-03	1.247E-02	1.762E-02	3.023E-02	4.043E-02	4.019E-02
BI213	1.317E-06	4.622E-07	4.623E-07	4.634E-07	4.688E-07	4.821E-07	5.594E-07
BI214	8.094E-08	9.174E-08	1.035E-07	1.295E-07	2.290E-07	4.689E-07	1.919E-06

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PO210	7.498E-09	9.326E-09	1.083E-08	1.382E-08	2.686E-08	7.527E-08	5.012E-07
PO211	4.784E-09	5.945E-09	7.189E-09	9.824E-09	1.692E-08	2.799E-08	5.837E-08
PO212	4.687E-03	6.312E-03	7.992E-03	1.129E-02	1.937E-02	2.590E-02	2.575E-02
PO213	1.289E-06	4.522E-07	4.523E-07	4.534E-07	4.587E-07	4.717E-07	5.473E-07
PO214	1.946E-07	9.198E-08	1.034E-07	1.295E-07	2.290E-07	4.688E-07	1.918E-06
PO215	1.708E-06	2.123E-06	2.568E-06	3.508E-06	6.043E-06	9.997E-06	2.085E-05
PO216	7.316E-03	9.852E-03	1.247E-02	1.762E-02	3.023E-02	4.043E-02	4.019E-02
PO218	8.096E-08	9.176E-08	1.035E-07	1.296E-07	2.291E-07	4.690E-07	1.919E-06
AT217	1.317E-06	4.622E-07	4.623E-07	4.634E-07	4.688E-07	4.821E-07	5.594E-07
RN219	1.708E-06	2.123E-06	2.568E-06	3.508E-06	6.043E-06	9.997E-06	2.085E-05
RN220	7.316E-03	9.852E-03	1.247E-02	1.762E-02	3.023E-02	4.043E-02	4.019E-02
RN222	8.096E-08	9.176E-08	1.035E-07	1.296E-07	2.291E-07	4.690E-07	1.919E-06
FR221	1.317E-06	4.622E-07	4.623E-07	4.634E-07	4.688E-07	4.821E-07	5.594E-07
FR223	2.399E-08	3.016E-08	3.627E-08	4.833E-08	8.329E-08	1.378E-07	2.875E-07
RA223	1.708E-06	2.123E-06	2.568E-06	3.508E-06	6.043E-06	9.997E-06	2.085E-05
RA224	7.316E-03	9.852E-03	1.247E-02	1.762E-02	3.023E-02	4.043E-02	4.019E-02
RA225	1.316E-06	4.616E-07	4.621E-07	4.634E-07	4.688E-07	4.821E-07	5.594E-07
RA226	8.090E-08	9.176E-08	1.035E-07	1.296E-07	2.291E-07	4.690E-07	1.919E-06
AC225	1.317E-06	4.622E-07	4.623E-07	4.634E-07	4.688E-07	4.821E-07	5.594E-07
AC227	1.738E-06	2.185E-06	2.628E-06	3.502E-06	6.036E-06	9.985E-06	2.083E-05
AC228	2.071E-05	1.845E-11	2.193E-11	2.976E-11	5.922E-11	1.230E-10	3.862E-10
TH227	1.680E-06	2.090E-06	2.528E-06	3.460E-06	5.960E-06	9.859E-06	2.056E-05
TH228	7.271E-03	9.820E-03	1.243E-02	1.758E-02	3.020E-02	4.040E-02	4.019E-02
TH229	4.608E-07	4.614E-07	4.620E-07	4.634E-07	4.688E-07	4.821E-07	5.594E-07
TH230	4.824E-05	5.222E-05	5.623E-05	6.434E-05	8.935E-05	1.333E-04	2.917E-04
TH231	1.032E+00	1.827E-02	1.827E-02	1.827E-02	1.827E-02	1.828E-02	1.828E-02
TH232	7.353E-11	8.284E-11	9.216E-11	1.108E-10	1.667E-10	2.598E-10	5.581E-10
TH233	3.696E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TH234	3.126E-01	3.124E-01	3.124E-01	3.124E-01	3.124E-01	3.124E-01	3.124E-01
PA231	2.986E-05	3.014E-05	3.034E-05	3.072E-05	3.188E-05	3.381E-05	3.999E-05
PA232	7.613E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
PA233	5.021E-01	4.965E-01	4.965E-01	4.967E-01	4.976E-01	5.002E-01	5.148E-01
PA234M	3.179E-01	3.124E-01	3.124E-01	3.124E-01	3.124E-01	3.124E-01	3.124E-01
PA234	5.712E-03	4.061E-04	4.061E-04	4.061E-04	4.061E-04	4.061E-04	4.061E-04
U231	2.532E-05	2.064E-18	1.597E-31	0.000E+00	0.000E+00	0.000E+00	0.000E+00
U232	2.097E-02	2.413E-02	2.688E-02	3.138E-02	3.935E-02	4.323E-02	3.922E-02
U233	1.166E-05	1.275E-05	1.383E-05	1.623E-05	2.299E-05	3.389E-05	6.935E-05
U234	8.816E-01	8.878E-01	8.941E-01	9.070E-01	9.452E-01	1.007E+00	1.189E+00

Scientific Notebook #170-10e

James Weldy

12/27/00

20-1402-762

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)

+ ACTINIDES+DAUGHTERS

POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC

0 7 SUMMARY TABLE: RADIOACTIVITY, CURIES

MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM, 4 CYCLE

	ASSY DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
--	----------	-------	-------	-------	-------	--------	--------

U235	1.827E-02	1.827E-02	1.827E-02	1.827E-02	1.828E-02	1.828E-02	
U236	3.776E-01	3.776E-01	3.776E-01	3.776E-01	3.777E-01	3.777E-01	3.780E-01
U237	8.707E+05	3.312E+00	3.227E+00	3.076E+00	2.662E+00	2.093E+00	9.687E-01
U238	3.124E-01						
U239	1.428E+07	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
U240	2.763E+01	5.311E-07	5.311E-07	5.311E-07	5.311E-07	5.311E-07	5.311E-07
U241	2.824E-04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NP235	6.568E-03	4.771E-03	3.466E-03	1.829E-03	2.688E-04	1.100E-05	3.977E-10
NP236M	7.073E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NP236	6.687E-06	6.687E-06	6.687E-06	6.687E-06	6.687E-06	6.686E-06	6.686E-06
NP237	4.889E-01	4.964E-01	4.965E-01	4.967E-01	4.976E-01	5.002E-01	5.148E-01
NP238	3.937E+05	7.794E-02	7.777E-02	7.741E-02	7.636E-02	7.464E-02	6.939E-02
NP239	1.426E+07	2.442E+01	2.442E+01	2.441E+01	2.441E+01	2.440E+01	2.436E+01
NP240M	3.056E+03	5.311E-07	5.311E-07	5.311E-07	5.311E-07	5.311E-07	5.311E-07
NP240	1.213E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NP241	2.824E-04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
PU236	7.110E-01	6.324E-01	5.600E-01	4.391E-01	2.117E-01	6.279E-02	1.284E-03
PU237	5.905E-01	3.680E-02	2.293E-03	8.890E-06	5.191E-13	4.563E-25	0.000E+00
PU238	4.249E+03	4.446E+03	4.515E+03	4.537E+03	4.446E+03	4.275E+03	3.769E+03
PU239	2.994E+02	3.032E+02	3.032E+02	3.032E+02	3.032E+02	3.032E+02	3.031E+02
PU240	5.522E+02	5.524E+02	5.525E+02	5.528E+02	5.534E+02	5.544E+02	5.562E+02
PU241	1.380E+05	1.348E+05	1.316E+05	1.254E+05	1.085E+05	8.530E+04	3.949E+04
PU242	2.153E+00	2.154E+00	2.154E+00	2.154E+00	2.154E+00	2.154E+00	2.154E+00
PU243	3.074E+05	2.112E-07	2.112E-07	2.112E-07	2.112E-07	2.112E-07	2.112E-07
PU244	5.317E-07	5.318E-07	5.318E-07	5.318E-07	5.318E-07	5.318E-07	5.318E-07
PU245	6.108E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
PU246	1.499E-04	1.285E-09	2.268E-14	1.166E-14	1.166E-14	1.166E-14	1.165E-14
AM239	1.388E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00

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AM240 3.808E-01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
AM241 2.445E+02 3.536E+02 4.601E+02 6.651E+02 1.222E+03 1.983E+03 3.437E+03  
AM242M 1.562E+01 1.559E+01 1.555E+01 1.548E+01 1.527E+01 1.493E+01 1.388E+01  
AM242 1.274E+05 1.551E+01 1.547E+01 1.540E+01 1.520E+01 1.485E+01 1.381E+01  
AM243 2.439E+01 2.442E+01 2.442E+01 2.441E+01 2.441E+01 2.440E+01 2.436E+01  
AM244M 9.931E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
AM244 5.215E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
AM245 6.108E-01 2.030E-08 1.367E-08 6.198E-09 5.774E-10 1.106E-11 3.520E-17  
AM246 1.499E-04 1.287E-09 2.270E-14 1.166E-14 1.166E-14 1.166E-14 1.165E-14  
CM241 1.482E-02 4.404E-04 1.308E-05 1.155E-08 7.942E-18 0.000E+00 0.000E+00  
CM242 6.797E+04 3.150E+04 1.451E+04 3.085E+03 4.185E+01 1.230E+01 1.142E+01  
CM243 3.243E+01 3.204E+01 3.165E+01 3.089E+01 2.871E+01 2.543E+01 1.723E+01  
CM244 3.140E+03 3.082E+03 3.023E+03 2.910E+03 2.594E+03 2.142E+03 1.161E+03  
CM245 2.610E-01 2.610E-01 2.610E-01 2.610E-01 2.609E-01 2.608E-01 2.605E-01  
CM246 6.608E-02 6.608E-02 6.607E-02 6.606E-02 6.603E-02 6.598E-02 6.583E-02  
CM247 2.112E-07 2.112E-07 2.112E-07 2.112E-07 2.112E-07 2.112E-07 2.112E-07  
CM248 5.648E-07 5.649E-07 5.649E-07 5.650E-07 5.650E-07 5.651E-07 5.651E-07  
CM249 1.414E-02 6.682E-12 5.477E-15 3.680E-21 0.000E+00 0.000E+00 0.000E+00  
BK249 2.076E-03 1.400E-03 9.426E-04 4.273E-04 3.981E-05 7.624E-07 2.427E-12  
BK250 4.826E-03 1.281E-08 8.097E-09 3.232E-09 2.056E-10 2.092E-12 6.527E-15  
BK251 1.809E-06 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CF249 1.177E-06 2.873E-06 4.012E-06 5.291E-06 6.225E-06 6.260E-06 6.067E-06  
CF250 3.097E-05 3.029E-05 2.950E-05 2.798E-05 2.387E-05 1.831E-05 7.843E-06

1

OUTPUT UNIT = 6

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ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)

+ ACTINIDES+DAUGHTERS  
POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC

0 7 SUMMARY TABLE: RADIOACTIVITY, CURIES  
MTIHM 4.5% UO2 FUEL ASSY;BURNUP=45,000 MWD/MTIHM, 4 CYCLE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

CF251 1.796E-07 1.796E-07 1.795E-07 1.794E-07 1.789E-07 1.782E-07 1.761E-07  
CF252 3.859E-05 3.383E-05 2.967E-05 2.281E-05 1.037E-05 2.788E-06 4.164E-08  
CF253 2.623E-06 2.150E-09 1.762E-12 1.184E-18 0.000E+00 0.000E+00 0.000E+00  
CF254 3.039E-08 3.750E-09 4.627E-10 7.046E-12 2.488E-17 2.037E-26 0.000E+00

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ES253 1.869E-06 2.564E-08 7.084E-11 3.435E-16 2.282E-32 0.000E+00 0.000E+00

ES254 2.027E-08 1.281E-08 8.093E-09 3.231E-09 2.055E-10 2.084E-12 8.669E-19

SUMTOT 3.057E+07 1.751E+05 1.550E+05 1.375E+05 1.178E+05 9.468E+04 4.883E+04

OTOTAL 3.057E+07 1.751E+05 1.550E+05 1.375E+05 1.178E+05 9.468E+04 4.883E+04

1 OUTPUT UNIT = 6 PAGE 32

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)

+ ACTINIDES+DAUGHTERS

POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC

0 7 SUMMARY TABLE: RADIOACTIVITY, CURIES  
MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM, 4 CYCLE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

TL 2.630E-03 3.542E-03 4.484E-03 6.336E-03 1.087E-02 1.454E-02 1.446E-02

PB 7.319E-03 9.854E-03 1.248E-02 1.763E-02 3.023E-02 4.044E-02 4.022E-02

BI 7.319E-03 9.854E-03 1.248E-02 1.763E-02 3.023E-02 4.044E-02 4.022E-02

PO 1.201E-02 1.617E-02 2.047E-02 2.892E-02 4.960E-02 6.634E-02 6.597E-02

AT 1.317E-06 4.622E-07 4.623E-07 4.634E-07 4.688E-07 4.821E-07 5.594E-07

RN 7.317E-03 9.854E-03 1.248E-02 1.763E-02 3.023E-02 4.044E-02 4.022E-02

FR 1.341E-06 4.923E-07 4.985E-07 5.117E-07 5.521E-07 6.199E-07 8.469E-07

RA 7.319E-03 9.854E-03 1.248E-02 1.763E-02 3.023E-02 4.044E-02 4.022E-02

AC 2.376E-05 2.647E-06 3.090E-06 3.966E-06 6.505E-06 1.047E-05 2.139E-05

TH 1.389E+00 3.406E-01 3.432E-01 3.483E-01 3.610E-01 3.712E-01 3.712E-01

PA 1.587E+00 8.093E-01 8.093E-01 8.096E-01 8.105E-01 8.131E-01 8.277E-01

U 1.515E+07 4.932E+00 4.857E+00 4.722E+00 4.355E+00 3.851E+00 2.906E+00

NP 1.467E+07 2.500E+01 2.499E+01 2.499E+01 2.498E+01 2.497E+01 2.494E+01

PU 4.506E+05 1.401E+05 1.369E+05 1.308E+05 1.138E+05 9.044E+04 4.412E+04

AM 2.322E+05 4.091E+02 5.155E+02 7.204E+02 1.277E+03 2.037E+03 3.489E+03

CM 7.114E+04 3.461E+04 1.756E+04 6.026E+03 2.665E+03 2.180E+03 1.190E+03

BK 6.904E-03 1.400E-03 9.426E-04 4.273E-04 3.981E-05 7.624E-07 2.433E-12

CF 7.356E-05 6.718E-05 6.336E-05 5.626E-05 4.064E-05 2.754E-05 1.413E-05

ES 1.999E-06 3.848E-08 8.165E-09 3.231E-09 2.055E-10 2.084E-12 8.669E-19

SUMTOT 3.057E+07 1.751E+05 1.550E+05 1.375E+05 1.178E+05 9.468E+04 4.883E+04

OTOTAL 3.057E+07 1.751E+05 1.550E+05 1.375E+05 1.178E+05 9.468E+04 4.883E+04

0 CUMULATIVE TABLE TOTALS

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AP+FP 6.253E+05 4.584E+04 1.655E+04 8.200E+03 3.928E+03 1.698E+03 3.517E+02  
ACT+FP 3.057E+07 1.751E+05 1.550E+05 1.375E+05 1.178E+05 9.468E+04 4.883E+04  
AP+ACT+FP 3.119E+07 2.210E+05 1.716E+05 1.457E+05 1.217E+05 9.638E+04 4.918E+04

1 OUTPUT UNIT = 6 PAGE 33

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)

+ FISSION PRODUCTS  
POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC

0 7 SUMMARY TABLE: RADIOACTIVITY, CURIES  
MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM, 4 CYCLE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

H 3	6.497E+02	6.317E+02	6.142E+02	5.807E+02	4.907E+02	3.706E+02	1.510E+02
BE 10	3.952E-06						
C 14	1.593E-04	1.593E-04	1.593E-04	1.593E-04	1.592E-04	1.591E-04	1.588E-04
CU 66	4.574E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CO 72	8.647E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NI 72	1.724E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CU 72	3.543E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZN 72	4.257E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GA 72	4.273E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CO 73	2.736E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NI 73	1.382E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CU 73	4.518E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZN 73	8.038E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GA 73	8.526E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GE 73M	8.533E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CO 74	5.424E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NI 74	8.670E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CU 74	6.274E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZN 74	1.560E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GA 74	1.680E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CO 75	7.191E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NI 75	3.512E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CU 75	6.207E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZN 75	2.890E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00

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GA 75 3.526E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
GE 75 3.575E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
GE 75M 1.645E+01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
NI 76 9.190E-01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CU 76 4.754E+01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
ZN 76 4.997E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
GA 76 7.733E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
AS 76 2.950E+01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
NI 77 1.537E-01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CU 77 2.156E+01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
ZN 77 5.462E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
GA 77 1.400E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
GE 77 6.459E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
GE 77M 1.400E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
AS 77 1.759E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SE 77M 5.220E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
NI 78 1.791E-02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CU 78 7.781E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
ZN 78 5.397E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
GA 78 2.470E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
GE 78 3.981E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
AS 78 4.102E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CU 79 2.094E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
ZN 79 3.240E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
GA 79 2.668E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
GE 79 8.209E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
AS 79 9.674E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

1

OUTPUT UNIT = 6

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ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)

+

FISSION PRODUCTS

POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC

0 7 SUMMARY TABLE: RADIOACTIVITY, CURIES

MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM, 4 CYCLE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

Scientific Notebook #170-10e

James Weldy

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20-1402-762

SE 79	5.517E-01	5.517E-01	5.517E-01	5.517E-01	5.516E-01	5.516E-01	5.515E-01
SE 79M	9.711E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BR 79M	1.335E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CU 80	2.248E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZN 80	1.192E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GA 80	2.682E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GE 80	1.613E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
AS 80	2.111E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BR 80	6.761E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BR 80M	4.149E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CU 81	1.633E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZN 81	2.637E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GA 81	1.527E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GE 81	1.885E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
AS 81	3.275E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SE 81	3.533E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SE 81M	9.753E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
KR 81	6.208E-07						
KR 81M	2.817E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZN 82	3.385E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GA 82	5.546E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GE 82	1.600E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
AS 82	2.791E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
AS 82M	1.187E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BR 82	5.005E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BR 82M	2.084E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZN 83	3.103E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GA 83	1.502E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GE 83	1.132E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
AS 83	4.939E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SE 83	3.114E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SE 83M	4.603E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BR 83	7.899E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
KR 83M	7.928E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GA 84	1.820E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GE 84	3.446E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
AS 84	3.944E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SE 84	1.298E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BR 84	1.350E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00

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BR 84M 5.274E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
GE 85 8.658E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
AS 85 2.284E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SE 85 7.438E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SE 85M 5.565E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
BR 85 1.621E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
KR 85 1.166E+04 1.129E+04 1.093E+04 1.024E+04 8.439E+03 6.107E+03 2.171E+03  
KR 85M 1.645E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
GE 86 1.611E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
AS 86 1.203E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SE 86 1.442E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
BR 86 1.152E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

1 OUTPUT UNIT = 6 PAGE 35

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)  
+ FISSION PRODUCTS  
POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC  
0 7 SUMMARY TABLE: RADIOACTIVITY, CURIES  
MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM, 4 CYCLE

	ASSY DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
BR 86M	1.157E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB 86	1.958E+03	2.221E+00	2.494E-03	3.190E-09	6.672E-27	0.000E+00	0.000E+00
RB 86M	2.154E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GE 87	2.241E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
AS 87	5.943E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SE 87	1.165E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BR 87	2.622E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
KR 87	3.119E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB 87	3.039E-05						
SR 87M	6.971E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GE 88	7.974E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
AS 88	4.479E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SE 88	4.266E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BR 88	2.747E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
KR 88	4.380E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00

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RB 88	4.461E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
AS 89	4.585E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SE 89	1.195E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BR 89	1.881E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
KR 89	5.290E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB 89	5.696E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SR 89	5.312E+05	4.332E+04	3.532E+03	2.348E+01	6.897E-06	8.952E-17	0.000E+00
Y 89M	3.757E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SE 90	3.615E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BR 90	1.177E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
KR 90	5.213E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB 90	5.500E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB 90M	1.329E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SR 90	9.915E+04	9.797E+04	9.681E+04	9.454E+04	8.802E+04	7.815E+04	5.340E+04
Y 90	1.030E+05	9.800E+04	9.684E+04	9.456E+04	8.804E+04	7.816E+04	5.341E+04
Y 90M	1.337E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZR 90M	3.413E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SE 91	5.058E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BR 91	4.003E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
KR 91	3.852E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB 91	6.926E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SR 91	7.486E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Y 91	6.760E+05	7.830E+04	8.997E+03	1.188E+02	2.735E-04	1.098E-13	0.000E+00
Y 91M	4.345E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SE 92	2.582E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BR 92	4.243E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
KR 92	1.899E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB 92	6.097E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SR 92	8.210E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Y 92	8.250E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BR 93	7.651E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
KR 93	6.948E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB 93	4.640E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SR 93	9.441E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Y 93	9.698E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZR 93	2.518E+00	2.519E+00	2.519E+00	2.519E+00	2.519E+00	2.519E+00	2.519E+00

1

OUTPUT UNIT = 6

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ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

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20-1402-762

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)

+

FISSION PRODUCTS

POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC

0 7 SUMMARY TABLE: RADIOACTIVITY, CURIES  
MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM, 4 CYCLE

	ASSY DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
--	----------	-------	-------	-------	-------	--------	--------

NB 93M	3.862E-01	4.367E-01	4.859E-01	5.806E-01	8.376E-01	1.187E+00	1.860E+00
BR 94	6.322E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
KR 94	2.450E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB 94	2.444E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SR 94	8.990E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Y 94	9.902E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NB 94	1.682E-04	1.682E-04	1.682E-04	1.682E-04	1.682E-04	1.681E-04	
NB 94M	8.393E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BR 95	4.732E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
KR 95	3.018E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB 95	1.187E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SR 95	8.313E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Y 95	1.072E+06	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZR 95	9.575E+05	1.324E+05	1.831E+04	3.501E+02	2.448E-03	6.257E-12	0.000E+00
NB 95	8.371E+05	2.587E+05	3.968E+04	8.037E+02	5.434E-03	1.389E-11	0.000E+00
NB 95M	6.805E+03	9.823E+02	1.358E+02	2.597E+00	1.816E-05	4.642E-14	0.000E+00
BR 96	2.475E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
KR 96	4.590E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB 96	3.388E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SR 96	5.761E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Y 96	1.022E+06	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NB 96	1.569E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
KR 97	2.655E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB 97	6.454E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SR 97	3.014E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Y 97	8.805E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZR 97	1.126E+06	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NB 97	1.136E+06	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NB 97M	1.068E+06	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
KR 98	2.982E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00

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RB 98	1.345E+03	0.000E+00						
SR 98	1.162E+05	0.000E+00						
Y 98	6.228E+05	0.000E+00						
ZR 98	1.140E+06	0.000E+00						
NB 98	1.161E+06	0.000E+00						
NB 98M	1.211E+04	0.000E+00						
TC 98	6.701E-06							
RB 99	1.319E+02	0.000E+00						
SR 99	3.096E+04	0.000E+00						
Y 99	3.528E+05	0.000E+00						
ZR 99	1.131E+06	0.000E+00						
NB 99	1.180E+06	0.000E+00						
NB 99M	4.963E+04	0.000E+00						
MO 99	1.282E+06	1.309E-14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TC 99	1.753E+01	1.758E+01						
TC 99M	1.122E+06	1.261E-14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB100	1.102E+01	0.000E+00						
SR100	5.905E+03	0.000E+00						
Y100	1.566E+05	0.000E+00						
ZR100	1.040E+06	0.000E+00						
NB100	6.590E+05	0.000E+00						

1

OUTPUT UNIT = 6

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ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)

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FISSION PRODUCTS

POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC

0

7 SUMMARY TABLE: RADIOACTIVITY, CURIES

MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM, 4 CYCLE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

NB100M	6.590E+05	0.000E+00						
TC100	3.884E+05	0.000E+00						
SR101	8.168E+02	0.000E+00						
Y101	4.975E+04	0.000E+00						
ZR101	6.609E+05	0.000E+00						
NB101	1.089E+06	0.000E+00						

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MO101	1.169E+06	0.000E+00									
TC101	1.170E+06	0.000E+00									
SR102	7.370E+01	0.000E+00									
Y102	1.210E+04	0.000E+00									
ZR102	3.719E+05	0.000E+00									
NB102	9.266E+05	0.000E+00									
MO102	1.120E+06	0.000E+00									
TC102	1.122E+06	0.000E+00									
TC102M	1.368E+03	0.000E+00									
RH102	1.155E+00	1.025E+00	9.094E-01	7.161E-01	3.496E-01	1.058E-01	2.310E-03				
SR103	2.490E+00	0.000E+00									
Y103	1.730E+03	0.000E+00									
ZR103	1.368E+05	0.000E+00									
NB103	6.463E+05	0.000E+00									
MO103	1.091E+06	0.000E+00									
TC103	1.108E+06	0.000E+00									
RU103	1.051E+06	4.187E+04	1.669E+03	2.650E+00	1.062E-08	1.075E-22	0.000E+00				
RH103M	9.461E+05	3.775E+04	1.505E+03	2.390E+00	9.575E-09	9.687E-23	0.000E+00				
SR104	1.029E-01	0.000E+00									
Y104	1.567E+02	0.000E+00									
ZR104	3.234E+04	0.000E+00									
NB104	3.131E+05	0.000E+00									
MO104	8.825E+05	0.000E+00									
TC104	9.448E+05	0.000E+00									
RH104	7.976E+05	0.000E+00									
RH104M	5.930E+04	0.000E+00									
Y105	8.105E+00	0.000E+00									
ZR105	4.394E+03	0.000E+00									
NB105	1.066E+05	0.000E+00									
MO105	6.329E+05	0.000E+00									
TC105	7.818E+05	0.000E+00									
RU105	7.968E+05	0.000E+00									
RH105	7.458E+05	0.000E+00									
RH105M	2.231E+05	0.000E+00									
ZR106	5.165E+02	0.000E+00									
NB106	2.876E+04	0.000E+00									
MO106	3.471E+05	0.000E+00									
TC106	5.598E+05	0.000E+00									
RU106	3.846E+05	2.727E+05	1.934E+05	9.722E+04	1.236E+04	3.969E+02	6.613E-03				

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RH106 4.189E+05 2.727E+05 1.934E+05 9.722E+04 1.236E+04 3.969E+02 6.613E-03  
RH106M 1.725E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
Y107 4.908E-03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
ZR107 2.321E+01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
NB107 4.470E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
MO107 1.300E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

1 OUTPUT UNIT = 6 PAGE 38

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)

+

FISSION PRODUCTS

POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC

0 7 SUMMARY TABLE: RADIOACTIVITY, CURIES

MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM, 4 CYCLE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

TC107	3.162E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RU107	4.770E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RH107	4.793E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
PD107	1.340E-01	1.340E-01	1.340E-01	1.340E-01	1.340E-01	1.340E-01
PD107M	8.721E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZR108	5.145E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NB108	7.310E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
MO108	3.426E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TC108	1.815E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RU108	3.312E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RH108	3.343E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RH108M	3.120E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
AG108	1.218E+00	3.437E-06	3.427E-06	3.409E-06	3.353E-06	3.263E-06
AG108M	3.872E-05	3.862E-05	3.851E-05	3.830E-05	3.768E-05	3.667E-05
ZR109	3.741E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NB109	1.354E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
MO109	9.935E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TC109	8.087E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RU109	2.023E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RH109	2.111E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RH109M	1.055E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00

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PD109	2.605E+05	0.000E+00									
PD109M	1.064E+05	0.000E+00									
AG109M	2.604E+05	8.269E-04	6.295E-04	3.648E-04	7.098E-05	4.638E-06	7.498E-10				
CD109	1.086E-03	8.269E-04	6.295E-04	3.648E-04	7.098E-05	4.638E-06	7.498E-10				
NB110	1.471E+01	0.000E+00									
MO110	1.736E+03	0.000E+00									
TC110	1.889E+04	0.000E+00									
RU110	8.748E+04	0.000E+00									
RH110	9.450E+04	0.000E+00									
RH110M	7.025E+03	0.000E+00									
AG110	1.265E+05	2.915E+01	1.757E+01	6.378E+00	3.052E-01	1.926E-03	1.756E-10				
AG110M	3.638E+03	2.192E+03	1.321E+03	4.795E+02	2.295E+01	1.448E-01	1.320E-08				
NB111	1.246E+00	0.000E+00									
MO111	3.382E+02	0.000E+00									
TC111	5.470E+03	0.000E+00									
RU111	3.670E+04	0.000E+00									
RH111	5.102E+04	0.000E+00									
PD111	5.249E+04	0.000E+00									
PD111M	8.270E+02	0.000E+00									
AG111	5.315E+04	2.227E-03	9.302E-11	1.624E-25	0.000E+00						
AG111M	5.255E+04	0.000E+00									
CD111M	2.812E+01	0.000E+00									
MO112	6.101E+01	0.000E+00									
TC112	1.693E+03	0.000E+00									
RU112	1.455E+04	0.000E+00									
RH112	2.432E+04	0.000E+00									
PD112	2.620E+04	0.000E+00									
AG112	2.626E+04	0.000E+00									
MO113	4.328E+00	0.000E+00									
TC113	4.353E+02	0.000E+00									

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ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)  
FISSION PRODUCTS

+  
POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC

0 7 SUMMARY TABLE: RADIOACTIVITY, CURIES  
MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM, 4 CYCLE

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	ASSY	DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
RU113	7.238E+03	0.000E+00						
RH113	1.638E+04	0.000E+00						
PD113	2.012E+04	0.000E+00						
AG113	1.814E+04	0.000E+00						
AG113M	2.043E+03	0.000E+00						
CD113M	6.072E+01	5.931E+01	5.791E+01	5.523E+01	4.789E+01	3.776E+01	1.766E+01	
IN113M	3.344E-06	0.000E+00						
MO114	4.408E-01	0.000E+00						
TC114	9.544E+01	0.000E+00						
RU114	3.027E+03	0.000E+00						
RH114	8.859E+03	0.000E+00						
PD114	1.338E+04	0.000E+00						
AG114	1.359E+04	0.000E+00						
IN114	1.266E+01	3.704E-01	2.873E-02	1.729E-04	3.765E-11	2.970E-22	0.000E+00	
IN114M	4.989E+00	3.870E-01	3.002E-02	1.806E-04	3.935E-11	3.103E-22	0.000E+00	
MO115	2.935E-02	0.000E+00						
TC115	2.001E+01	0.000E+00						
RU115	1.357E+03	0.000E+00						
RH115	6.213E+03	0.000E+00						
PD115	1.215E+04	0.000E+00						
AG115	9.145E+03	0.000E+00						
AG115M	3.545E+03	0.000E+00						
CD115	1.213E+04	0.000E+00						
CD115M	1.084E+03	6.345E+01	3.712E+00	1.272E-02	5.103E-10	2.399E-22	0.000E+00	
IN115M	1.215E+04	4.459E-03	2.609E-04	8.940E-07	3.586E-14	1.686E-26	0.000E+00	
TC116	1.233E+00	0.000E+00						
RU116	3.011E+02	0.000E+00						
RH116	2.888E+03	0.000E+00						
PD116	9.095E+03	0.000E+00						
AG116	5.153E+03	0.000E+00						
AG116M	5.154E+03	0.000E+00						
IN116	7.003E+03	0.000E+00						
IN116M	5.634E+03	0.000E+00						
TC117	5.251E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
RU117	4.493E+01	0.000E+00						
RH117	1.618E+03	0.000E+00						

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PD117 7.868E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
AG117 5.004E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
AG117M 5.003E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CD117 6.656E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CD117M 3.620E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
IN117 6.152E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
IN117M 7.783E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SN117M 7.749E+01 9.198E-03 1.092E-06 1.539E-14 0.000E+00 0.000E+00 0.000E+00  
RU118 2.893E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
RH118 2.281E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
PD118 6.220E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
AG118 6.627E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
AG118M 4.547E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CD118 1.017E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
IN118 1.018E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

1 OUTPUT UNIT = 6 PAGE 40

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)

+ FISSION PRODUCTS  
POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC

0 7 SUMMARY TABLE: RADIOACTIVITY, CURIES  
MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM, 4 CYCLE

	ASSY DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
IN118M	4.923E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RH119	2.054E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
PD119	4.806E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
AG119	9.207E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CD119	5.063E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CD119M	5.063E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
IN119	2.916E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
IN119M	7.598E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SN119M	1.343E+02	8.014E+01	4.781E+01	1.701E+01	7.665E-01	4.372E-03	2.890E-10
RU120	6.085E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RH120	2.805E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
PD120	1.644E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00

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AG120	6.049E+03	0.000E+00						
CD120	9.939E+03	0.000E+00						
IN120	5.088E+03	0.000E+00						
IN120M	5.088E+03	0.000E+00						
RH121	4.401E+00	0.000E+00						
PD121	6.351E+02	0.000E+00						
AG121	4.110E+03	0.000E+00						
CD121	9.770E+03	0.000E+00						
IN121	8.358E+03	0.000E+00						
IN121M	2.115E+03	0.000E+00						
SN121	1.050E+04	0.000E+00						
SN121M	2.497E-01	2.479E-01	2.462E-01	2.428E-01	2.329E-01	2.173E-01	1.741E-01	
RH122	5.322E-01	0.000E+00						
PD122	1.922E+02	0.000E+00						
AG122	2.492E+03	0.000E+00						
CD122	9.236E+03	0.000E+00						
IN122	1.004E+04	0.000E+00						
IN122M	8.039E+02	0.000E+00						
SB122	1.638E+03	7.156E-18	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SB122M	1.453E+01	0.000E+00						
RH123	4.538E-02	0.000E+00						
PD123	4.342E+01	0.000E+00						
AG123	1.292E+03	0.000E+00						
CD123	8.707E+03	0.000E+00						
IN123	8.289E+03	0.000E+00						
IN123M	3.581E+03	0.000E+00						
SN123	1.913E+03	7.178E+02	2.694E+02	3.795E+01	1.061E-01	5.881E-06	1.411E-19	
SN123M	9.851E+03	0.000E+00						
TE123M	1.295E+01	4.496E+00	1.561E+00	1.882E-01	3.293E-04	8.392E-09	1.675E-23	
PD124	8.252E+00	0.000E+00						
AG124	5.949E+02	0.000E+00						
CD124	7.920E+03	0.000E+00						
IN124	1.352E+04	0.000E+00						
SB124	1.003E+03	1.225E+02	1.496E+01	2.230E-01	7.391E-07	5.446E-16	0.000E+00	
SB124M	8.457E+00	0.000E+00						
AG125	1.892E+02	0.000E+00						
CD125	5.780E+03	0.000E+00						
IN125	8.848E+03	0.000E+00						
IN125M	6.562E+03	0.000E+00						

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James Weldy

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OUTPUT UNIT = 6

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ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)

+

FISSION PRODUCTS

POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC

0 7 SUMMARY TABLE: RADIOACTIVITY, CURIES

MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM, 4 CYCLE

	ASSY	DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
--	------	-----	-------	-------	-------	-------	--------	--------

SN125	9.039E+03	1.792E-02	3.552E-08	1.396E-19	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SN125M	1.465E+04	0.000E+00						
SB125	1.162E+04	1.033E+04	9.115E+03	7.097E+03	3.350E+03	9.585E+02	1.749E+01	
TE125M	2.557E+03	2.486E+03	2.220E+03	1.731E+03	8.173E+02	2.339E+02	4.267E+00	
PD126	1.290E-01	0.000E+00						
AG126	5.988E+01	0.000E+00						
CD126	4.349E+03	0.000E+00						
IN126	2.008E+04	0.000E+00						
SN126	9.186E-01	9.186E-01	9.186E-01	9.185E-01	9.185E-01	9.185E-01	9.184E-01	
SB126	7.436E+02	1.559E-01	1.286E-01	1.286E-01	1.286E-01	1.286E-01	1.286E-01	
SB126M	3.569E+02	9.186E-01	9.186E-01	9.185E-01	9.185E-01	9.185E-01	9.184E-01	
CD127	2.591E+03	0.000E+00						
IN127	1.226E+04	0.000E+00						
IN127M	1.227E+04	0.000E+00						
SN127	4.757E+04	0.000E+00						
SN127M	2.304E+04	0.000E+00						
SB127	7.556E+04	4.014E-10	2.102E-24	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TE127	7.297E+04	2.586E+03	8.098E+02	7.937E+01	7.475E-02	6.764E-07	4.912E-23	
TE127M	8.044E+03	2.641E+03	8.267E+02	8.103E+01	7.632E-02	6.906E-07	5.015E-23	
XE127	4.539E-02	1.403E-03	4.338E-05	4.146E-08	3.620E-17	2.282E-32	0.000E+00	
AG128	2.674E+00	0.000E+00						
CD128	9.945E+02	0.000E+00						
IN128	2.009E+04	0.000E+00						
SN128	1.120E+05	0.000E+00						
SB128	1.057E+04	0.000E+00						
SB128M	1.223E+05	0.000E+00						
I128	1.032E+04	0.000E+00						

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CD129 3.796E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
IN129 1.648E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SN129 7.617E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SN129M 8.554E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SB129 2.250E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
TE129 2.207E+05 4.825E+02 1.115E+01 5.956E-03 9.072E-13 3.941E-29 0.000E+00  
TE129M 3.192E+04 7.413E+02 1.713E+01 9.149E-03 1.394E-12 6.056E-29 0.000E+00  
I129 3.982E-02 4.002E-02 4.002E-02 4.002E-02 4.002E-02 4.002E-02 4.002E-02  
XE129M 6.940E+00 9.320E-07 1.252E-13 2.257E-27 0.000E+00 0.000E+00 0.000E+00  
CD130 3.246E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
IN130 1.757E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SN130 2.420E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SB130 7.454E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SB130M 3.225E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
I130 3.545E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
I130M 1.493E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CD131 5.013E+01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
IN131 6.205E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SN131 2.093E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SB131 5.696E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
TE131 6.091E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
TE131M 1.009E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
I131 6.891E+05 1.033E-01 1.502E-08 3.177E-22 0.000E+00 0.000E+00 0.000E+00  
XE131M 7.683E+03 5.748E-01 1.383E-05 7.939E-15 0.000E+00 0.000E+00 0.000E+00

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OUTPUT UNIT = 6

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ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)

+

FISSION PRODUCTS

POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC

0

7 SUMMARY TABLE: RADIOACTIVITY, CURIES

MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM, 4 CYCLE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

CD132 4.472E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
IN132 1.511E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SN132 1.091E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

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SB132 3.319E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SB132M 2.221E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
TE132 9.744E+05 1.304E-11 1.745E-28 0.000E+00 0.000E+00 0.000E+00  
I132 9.909E+05 1.344E-11 1.798E-28 0.000E+00 0.000E+00 0.000E+00  
CS132 2.087E+02 6.738E-07 2.175E-15 2.282E-32 0.000E+00 0.000E+00  
IN133 1.628E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SN133 3.166E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SB133 3.799E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
TE133 8.117E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
TE133M 4.957E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
I133 1.385E+06 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
I133M 4.414E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
XE133 1.389E+06 5.642E-05 1.865E-15 0.000E+00 0.000E+00 0.000E+00  
XE133M 4.365E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
IN134 8.905E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SN134 4.193E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SB134 6.330E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SB134M 5.911E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
TE134 1.116E+06 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
I134 1.519E+06 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
I134M 1.559E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
XE134M 1.093E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CS134 1.838E+05 1.554E+05 1.314E+05 9.385E+04 3.423E+04 6.375E+03 2.941E+01  
CS134M 4.994E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SN135 4.519E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SB135 3.383E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
TE135 5.880E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
I135 1.300E+06 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
XE135 3.774E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
XE135M 2.775E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CS135 7.004E-01 7.010E-01 7.010E-01 7.010E-01 7.010E-01 7.010E-01 7.010E-01  
CS135M 2.767E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
BA135M 2.007E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SN136 3.812E+01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SB136 6.388E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
TE136 3.038E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
I136 6.102E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
I136M 3.619E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CS136 5.585E+04 3.556E+00 2.265E-04 9.182E-13 0.000E+00 0.000E+00 0.000E+00

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BA136M 9.204E+03 5.861E-01 3.732E-05 1.513E-13 0.000E+00 0.000E+00 0.000E+00  
SB137 8.897E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
TE137 8.310E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
I137 5.887E+05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
XE137 1.211E+06 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CS137 1.351E+05 1.336E+05 1.320E+05 1.290E+05 1.204E+05 1.072E+05 7.410E+04  
BA137M 1.280E+05 1.264E+05 1.249E+05 1.220E+05 1.139E+05 1.015E+05 7.010E+04  
SB138 1.061E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
TE138 1.953E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

1 OUTPUT UNIT = 6 PAGE 43

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)  
+ FISSION PRODUCTS  
POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC  
0 7 SUMMARY TABLE: RADIOACTIVITY, CURIES  
MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM, 4 CYCLE

	ASSY DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
I138	2.866E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
XE138	1.126E+06	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CS138	1.253E+06	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CS138M	6.136E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SB139	7.700E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TE139	3.650E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
I139	1.243E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
XE139	8.740E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CS139	1.186E+06	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BA139	1.227E+06	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TE140	4.312E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
I140	3.381E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
XE140	5.620E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CS140	1.067E+06	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BA140	1.183E+06	5.947E+01	2.991E-03	7.563E-12	0.000E+00	0.000E+00	0.000E+00
LA140	1.235E+06	6.844E+01	3.442E-03	8.703E-12	0.000E+00	0.000E+00	0.000E+00
PR140	1.881E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TE141	1.918E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00

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I141	5.397E+03	0.000E+00									
XE141	1.952E+05	0.000E+00									
CS141	7.856E+05	0.000E+00									
BA141	1.110E+06	0.000E+00									
LA141	1.115E+06	0.000E+00									
CE141	1.087E+06	2.227E+04	4.537E+02	1.883E-01	1.346E-11	1.658E-28	0.000E+00				
TE142	1.975E+00	0.000E+00									
I142	7.356E+02	0.000E+00									
XE142	6.446E+04	0.000E+00									
CS142	4.695E+05	0.000E+00									
BA142	1.047E+06	0.000E+00									
LA142	1.073E+06	0.000E+00									
CE142	3.713E-05	3.714E-05									
PR142	8.181E+04	0.000E+00									
PR142M	1.784E+04	0.000E+00									
I143	4.778E+01	0.000E+00									
XE143	1.074E+04	0.000E+00									
CS143	2.265E+05	0.000E+00									
BA143	9.109E+05	0.000E+00									
LA143	1.017E+06	0.000E+00									
CE143	1.025E+06	0.000E+00									
PR143	1.020E+06	1.006E+02	8.907E-03	6.984E-11	0.000E+00						
I144	3.750E+00	0.000E+00									
XE144	1.786E+03	0.000E+00									
CS144	6.467E+04	0.000E+00									
BA144	6.808E+05	0.000E+00									
LA144	8.940E+05	0.000E+00									
CE144	7.021E+05	4.498E+05	2.881E+05	1.182E+05	8.173E+03	9.515E+01	6.161E-05				
PR144	7.073E+05	4.498E+05	2.881E+05	1.182E+05	8.173E+03	9.515E+01	6.161E-05				
PR144M	8.435E+03	5.397E+03	3.458E+03	1.419E+03	9.808E+01	1.142E+00	7.393E-07				
XE145	1.828E+02	0.000E+00									
CS145	1.586E+04	0.000E+00									
BA145	3.484E+05	0.000E+00									

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OUTPUT UNIT = 6

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ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)

+

FISSION PRODUCTS

POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00

Scientific Notebook #170-10e

James Weldy

12/27/00

20-1402-762

N/CM\*\*2-SEC

0            7 SUMMARY TABLE: RADIOACTIVITY, CURIES  
MTIHM 4.5% UO2 FUEL ASSY;BURNUP=45,000 MWD/MTIHM, 4 CYCLE

	ASSY	DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
LA145	6.473E+05	0.000E+00						
CE145	6.972E+05	0.000E+00						
PR145	6.975E+05	0.000E+00						
XE146	1.153E+01	0.000E+00						
CS146	2.236E+03	0.000E+00						
BA146	1.272E+05	0.000E+00						
LA146	4.223E+05	0.000E+00						
CE146	5.598E+05	0.000E+00						
PR146	5.621E+05	0.000E+00						
PM146	2.518E+00	2.365E+00	2.220E+00	1.957E+00	1.341E+00	7.142E-01	9.508E-02	
SM146	4.437E-07	4.482E-07	4.524E-07	4.600E-07	4.779E-07	4.962E-07	5.142E-07	
XE147	9.836E-01	0.000E+00						
CS147	3.368E+02	0.000E+00						
BA147	2.843E+04	0.000E+00						
LA147	2.054E+05	0.000E+00						
CE147	4.346E+05	0.000E+00						
PR147	4.470E+05	0.000E+00						
ND147	4.503E+05	4.823E+00	5.161E-05	5.909E-15	0.000E+00	0.000E+00	0.000E+00	
PM147	1.161E+05	1.063E+05	9.318E+04	7.155E+04	3.239E+04	8.642E+03	1.261E+02	
SM147	3.336E-06	3.704E-06	4.027E-06	4.557E-06	5.517E-06	6.100E-06	6.308E-06	
CS148	2.119E+01	0.000E+00						
BA148	4.766E+03	0.000E+00						
LA148	7.615E+04	0.000E+00						
CE148	3.190E+05	0.000E+00						
PR148	3.563E+05	0.000E+00						
PM148	1.823E+05	6.582E+01	3.070E+00	6.686E-03	6.883E-11	3.352E-24	0.000E+00	
PM148M	2.505E+04	1.169E+03	5.450E+01	1.187E-01	1.222E-09	5.951E-23	0.000E+00	
BA149	5.159E+02	0.000E+00						
LA149	1.857E+04	0.000E+00						
CE149	1.772E+05	0.000E+00						
PR149	2.506E+05	0.000E+00						
ND149	2.672E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
PM149	3.909E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	

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CS150	1.949E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BA150	3.761E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
LA150	3.465E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CE150	8.194E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
PR150	1.690E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
PM150	3.678E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
EU150	3.145E-05	3.115E-05	3.085E-05	3.026E-05	2.856E-05	2.594E-05	1.906E-05
LA151	4.262E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CE151	2.432E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
PR151	9.441E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ND151	1.416E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
PM151	1.419E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SM151	4.049E+02	4.085E+02	4.069E+02	4.038E+02	3.946E+02	3.797E+02	3.357E+02
BA152	9.540E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
LA152	4.509E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CE152	5.179E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
PR152	4.188E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ND152	9.855E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00

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OUTPUT UNIT = 6

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ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)

+

FISSION PRODUCTS

POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00

N/CM\*\*2-SEC

0

7 SUMMARY TABLE: RADIOACTIVITY, CURIES

MTIHM 4.5% UO<sub>2</sub> FUEL ASSY; BURNUP=45,000 MWD/MTIHM, 4 CYCLE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

PM152	1.010E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
PM152M	1.911E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
EU152	1.379E+01	1.344E+01	1.310E+01	1.245E+01	1.069E+01	8.282E+00
EU152M	1.309E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
LA153	4.445E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CE153	8.502E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
PR153	1.312E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ND153	5.836E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
PM153	6.644E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00

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James Weldy

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SM153	3.877E+05	0.000E+00										
GD153	8.905E+01	5.278E+01	3.128E+01	1.099E+01	4.765E-01	2.551E-03	1.373E-10					
LA154	2.033E-01	0.000E+00										
CE154	9.477E+01	0.000E+00										
PR154	3.123E+03	0.000E+00										
ND154	3.083E+04	0.000E+00										
PM154	3.803E+04	0.000E+00										
PM154M	6.547E+03	0.000E+00										
EU154	1.468E+04	1.410E+04	1.354E+04	1.249E+04	9.811E+03	6.557E+03	1.806E+03					
CE155	1.040E+01	0.000E+00										
PR155	6.011E+02	0.000E+00										
ND155	1.193E+04	0.000E+00										
PM155	2.425E+04	0.000E+00										
SM155	2.898E+04	0.000E+00										
EU155	8.732E+03	8.143E+03	7.593E+03	6.603E+03	4.341E+03	2.158E+03	2.306E+02					
GD155M	1.616E+00	0.000E+00										
CE156	9.652E-01	0.000E+00										
PR156	1.093E+02	0.000E+00										
ND156	4.306E+03	0.000E+00										
PM156	1.370E+04	0.000E+00										
SM156	1.829E+04	0.000E+00										
EU156	1.829E+05	4.395E+01	1.054E-02	6.053E-10	0.000E+00							
CE157	7.332E-02	0.000E+00										
PR157	1.576E+01	0.000E+00										
ND157	1.186E+03	0.000E+00										
PM157	6.680E+03	0.000E+00										
SM157	1.220E+04	0.000E+00										
EU157	1.873E+04	0.000E+00										
PR158	1.111E+00	0.000E+00										
ND158	1.789E+02	0.000E+00										
PM158	2.189E+03	0.000E+00										
SM158	6.722E+03	0.000E+00										
EU158	7.193E+03	0.000E+00										
PR159	4.204E-02	0.000E+00										
ND159	1.685E+01	0.000E+00										
PM159	4.974E+02	0.000E+00										
SM159	3.187E+03	0.000E+00										
EU159	3.863E+03	0.000E+00										
GD159	5.087E+03	0.000E+00										

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ND160 1.193E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

PM160 7.975E+01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

SM160 1.142E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

1 OUTPUT UNIT = 6 PAGE 46

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)

+

FISSION PRODUCTS

POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC

0 7 SUMMARY TABLE: RADIOACTIVITY, CURIES

MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM, 4 CYCLE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

EU160 1.750E+03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

TB160 8.205E+02 1.425E+02 2.474E+01 7.459E-01 2.045E-05 5.095E-13 0.000E+00

ND161 7.609E-02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

PM161 8.805E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

SM161 3.073E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

EU161 7.525E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

GD161 8.794E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

TB161 1.006E+03 1.145E-05 1.301E-13 1.682E-29 0.000E+00 0.000E+00 0.000E+00

PM162 3.465E-01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

SM162 3.642E+01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

EU162 2.100E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

GD162 3.880E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

TB162 3.843E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

TB162M 1.184E+01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

SM163 3.810E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

EU163 4.711E+01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

GD163 1.526E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

TB163 1.650E+02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

SM164 3.073E-01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

EU164 8.865E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

GD164 5.836E+01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

TB164 7.309E+01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

SM165 1.800E-02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

EU165 1.303E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

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GD165	1.872E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TB165	3.134E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
DY165	4.521E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
DY165M	1.988E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
DY166	2.215E+01	1.433E-15	9.127E-32	0.000E+00	0.000E+00	0.000E+00	0.000E+00
HO166	1.338E+02	2.135E-15	1.369E-31	0.000E+00	0.000E+00	0.000E+00	0.000E+00
HO166M	3.608E-03	3.607E-03	3.606E-03	3.604E-03	3.597E-03	3.587E-03	3.554E-03
ER167M	3.219E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ER169	2.451E-01	3.474E-07	4.925E-13	9.895E-25	0.000E+00	0.000E+00	0.000E+00
TM170	4.873E-02	1.821E-02	6.803E-03	9.498E-04	2.582E-06	1.370E-10	2.855E-24
TM170M	5.781E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TM171	7.627E-04	6.367E-04	5.316E-04	3.705E-04	1.254E-04	2.063E-05	6.394E-08
TM172	5.576E-05	1.002E-25	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SUMTOT	1.185E+08	2.842E+06	1.764E+06	1.079E+06	5.458E+05	3.978E+05	2.559E+05
0TOTAL	1.185E+08	2.842E+06	1.764E+06	1.079E+06	5.458E+05	3.978E+05	2.559E+05

1 OUTPUT UNIT = 6 PAGE 47

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

\*ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)

+ FISSION PRODUCTS  
POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC

0 7 SUMMARY TABLE: RADIOACTIVITY, CURIES  
MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM, 4 CYCLE

	ASSY DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
H	6.497E+02	6.317E+02	6.142E+02	5.807E+02	4.907E+02	3.706E+02	1.510E+02
BE	3.952E-06						
C	1.593E-04	1.593E-04	1.593E-04	1.593E-04	1.592E-04	1.591E-04	1.588E-04
CO	1.200E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NI	4.434E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CU	2.846E+02	2.282E-32	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZN	2.627E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GA	1.289E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GE	8.150E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
AS	2.393E+05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SE	7.026E+05	5.517E-01	5.517E-01	5.517E-01	5.516E-01	5.516E-01	5.515E-01
BR	1.507E+06	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00

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KR	2.728E+06	1.129E+04	1.093E+04	1.024E+04	8.439E+03	6.107E+03	2.171E+03
RB	3.872E+06	2.221E+00	2.524E-03	3.040E-05	3.039E-05	3.039E-05	3.039E-05
SR	5.906E+06	1.413E+05	1.003E+05	9.456E+04	8.802E+04	7.815E+04	5.340E+04
Y	8.169E+06	1.763E+05	1.058E+05	9.468E+04	8.804E+04	7.816E+04	5.341E+04
ZR	6.601E+06	1.324E+05	1.831E+04	3.526E+02	2.521E+00	2.519E+00	2.519E+00
NB	9.885E+06	2.597E+05	3.981E+04	8.069E+02	8.432E-01	1.188E+00	1.860E+00
MO	6.701E+06	1.309E-14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TC	7.803E+06	1.758E+01	1.758E+01	1.758E+01	1.758E+01	1.758E+01	1.758E+01
RU	3.393E+06	3.146E+05	1.950E+05	9.723E+04	1.236E+04	3.969E+02	6.613E-03
RH	4.557E+06	3.105E+05	1.949E+05	9.723E+04	1.236E+04	3.970E+02	8.923E-03
PD	5.226E+05	1.340E-01	1.340E-01	1.340E-01	1.340E-01	1.340E-01	1.340E-01
AG	6.244E+05	2.221E+03	1.338E+03	4.859E+02	2.326E+01	1.468E-01	3.660E-05
CD	1.039E+05	1.228E+02	6.163E+01	5.524E+01	4.789E+01	3.776E+01	1.766E+01
IN	2.384E+05	7.618E-01	5.901E-02	3.544E-04	9.025E-11	1.321E-11	1.321E-11
SN	9.872E+05	7.992E+02	3.184E+02	5.612E+01	2.024E+00	1.140E+00	1.092E+00
SB	2.513E+06	1.045E+04	9.131E+03	7.098E+03	3.351E+03	9.596E+02	1.853E+01
TE	5.442E+06	8.942E+03	3.886E+03	1.892E+03	8.174E+02	2.339E+02	4.267E+00
I	8.157E+06	1.433E-01	4.002E-02	4.002E-02	4.002E-02	4.002E-02	4.002E-02
XE	6.151E+06	5.762E-01	5.721E-05	4.146E-08	3.620E-17	2.282E-32	0.000E+00
CS	5.584E+06	2.890E+05	2.634E+05	2.229E+05	1.546E+05	1.136E+05	7.413E+04
BA	6.804E+06	1.264E+05	1.249E+05	1.220E+05	1.139E+05	1.015E+05	7.010E+04
LA	6.708E+06	6.844E+01	3.442E-03	1.571E-10	1.484E-10	1.484E-10	1.484E-10
CE	5.114E+06	4.720E+05	2.886E+05	1.182E+05	8.173E+03	9.515E+01	9.874E-05
PR	4.471E+06	4.553E+05	2.916E+05	1.197E+05	8.271E+03	9.629E+01	6.235E-05
ND	1.065E+06	4.823E+00	5.161E-05	2.207E-09	2.247E-09	2.250E-09	2.250E-09
PM	1.121E+06	1.076E+05	9.324E+04	7.155E+04	3.239E+04	8.643E+03	1.262E+02
SM	4.590E+05	4.085E+02	4.069E+02	4.038E+02	3.946E+02	3.797E+02	3.357E+02
EU	2.390E+05	2.230E+04	2.115E+04	1.911E+04	1.416E+04	8.723E+03	2.040E+03
GD	6.675E+03	5.278E+01	3.128E+01	1.099E+01	4.765E-01	2.551E-03	1.383E-10
TB	2.492E+03	1.425E+02	2.474E+01	7.459E-01	2.045E-05	5.095E-13	0.000E+00
DY	6.731E+02	1.433E-15	9.127E-32	0.000E+00	0.000E+00	0.000E+00	0.000E+00
HO	1.338E+02	3.607E-03	3.606E-03	3.604E-03	3.597E-03	3.587E-03	3.554E-03
ER	3.464E+00	3.474E-07	4.925E-13	9.895E-25	0.000E+00	0.000E+00	0.000E+00
TM	5.532E-02	1.884E-02	7.334E-03	1.320E-03	1.280E-04	2.063E-05	6.394E-08
SUMTOT	1.185E+08	2.842E+06	1.764E+06	1.079E+06	5.458E+05	3.978E+05	2.559E+05
0TOTAL	1.185E+08	2.842E+06	1.764E+06	1.079E+06	5.458E+05	3.978E+05	2.559E+05
0	CUMULATIVE TABLE TOTALS						

AP+FP 1.191E+08 2.888E+06 1.780E+06 1.087E+06 5.498E+05 3.995E+05 2.563E+05

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ACT+FP 1.490E+08 3.018E+06 1.919E+06 1.217E+06 6.636E+05 4.925E+05 3.047E+05  
AP+ACT+FP 1.497E+08 3.063E+06 1.935E+06 1.225E+06 6.676E+05 4.942E+05 3.051E+05  
1 OUTPUT UNIT = 6 PAGE 48

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)

(ALPHA,N) NEUTRON SOURCE, NEUTRONS/SEC

BASIS=MTIHM 4.5% UO2 FUEL ASSY;BURNUP=45,000 MWD/MTIHM, 4 CYCLE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

PU238	4.043E+06	4.230E+06	4.295E+06	4.317E+06	4.230E+06	4.067E+06	3.586E+06
PU239	2.181E+05	2.209E+05	2.209E+05	2.209E+05	2.209E+05	2.208E+05	2.207E+05
PU240	4.184E+05	4.185E+05	4.186E+05	4.188E+05	4.194E+05	4.201E+05	4.214E+05
AM241	2.345E+05	3.392E+05	4.413E+05	6.380E+05	1.172E+06	1.902E+06	3.296E+06
AM243	2.081E+04	2.083E+04	2.083E+04	2.083E+04	2.082E+04	2.081E+04	2.078E+04
CM242	9.124E+07	4.228E+07	1.948E+07	4.142E+06	5.618E+04	1.651E+04	1.533E+04
CM243	4.317E+04	4.265E+04	4.214E+04	4.112E+04	3.823E+04	3.385E+04	2.294E+04
CM244	3.584E+06	3.517E+06	3.450E+06	3.320E+06	2.960E+06	2.445E+06	1.325E+06
0-							

TOTALS

TABLE	9.980E+07	5.107E+07	2.837E+07	1.312E+07	9.122E+06	9.129E+06	8.912E+06
ACTUAL	9.980E+07	5.107E+07	2.837E+07	1.312E+07	9.122E+06	9.129E+06	8.912E+06
1					OUTPUT UNIT = 6		PAGE 49

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP (BWRU)

SPONTANEOUS FISSION NEUTRON SOURCE, NEUTRONS/SEC

BASIS=MTIHM 4.5% UO2 FUEL ASSY;BURNUP=45,000 MWD/MTIHM, 4

CYCLE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

PU238	6.593E+05	6.898E+05	7.005E+05	7.040E+05	6.899E+05	6.633E+05	5.847E+05
PU240	2.206E+06	2.206E+06	2.207E+06	2.208E+06	2.211E+06	2.214E+06	2.222E+06
PU242	9.504E+05						
CM242	4.427E+08	2.052E+08	9.450E+07	2.010E+07	2.726E+05	8.013E+04	7.438E+04
CM244	4.315E+08	4.234E+08	4.154E+08	3.998E+08	3.564E+08	2.943E+08	1.595E+08
CM246	1.914E+06	1.913E+06	1.913E+06	1.913E+06	1.912E+06	1.911E+06	1.906E+06

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0-----

TOTALS

TABLE 8.801E+08 6.345E+08 5.158E+08 4.258E+08 3.625E+08 3.002E+08 1.653E+08

ACTUAL 8.801E+08 6.345E+08 5.158E+08 4.258E+08 3.625E+08 3.002E+08 1.653E+08

0-----

OVERALL

TOTALS

TABLE 9.799E+08 6.856E+08 5.442E+08 4.389E+08 3.716E+08 3.093E+08 1.742E+08

ACTUAL 9.799E+08 6.856E+08 5.442E+08 4.389E+08 3.716E+08 3.093E+08 1.742E+08

1-----

OUTPUT UNIT = 6

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ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

PHOTON SPECTRUM FOR ACTIVATION PRODUCTS

0 ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP  
(BWRU)

POWER= 1.00 MW, BURNUP= 1. MWD, FLUX= 1.00E+00

N/CM\*\*2-SEC

0 18 GROUP PHOTON RELEASE RATES, PHOTONS/SECOND  
BASIS=MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM,

4 CYCLE

EMEAN

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

1.000E-02 4.482E+15 7.899E+13 2.790E+13 1.343E+13 6.402E+12 2.754E+12 3.563E+11

2.500E-02 1.422E+15 1.733E+14 1.174E+14 6.693E+13 2.391E+13 6.769E+12 1.690E+11

3.750E-02 6.044E+14 3.107E+13 2.259E+13 1.574E+13 7.392E+12 2.579E+12 2.317E+11

5.750E-02 8.829E+14 1.811E+13 5.064E+12 1.748E+12 8.563E+11 4.272E+11 7.061E+10

8.500E-02 5.289E+14 1.236E+13 4.136E+12 1.679E+12 7.862E+11 3.746E+11 4.410E+10

1.250E-01 3.346E+14 6.384E+12 3.957E+12 2.954E+12 1.974E+12 1.194E+12 2.890E+11

2.250E-01 9.057E+14 3.043E+13 1.018E+13 4.860E+12 2.348E+12 7.915E+11 6.751E+10

3.750E-01 4.616E+14 3.916E+13 3.312E+13 2.561E+13 1.210E+13 3.483E+12 7.260E+10

5.750E-01 5.417E+15 5.206E+13 4.314E+13 3.328E+13 1.583E+13 4.661E+12 1.442E+11

8.500E-01 8.894E+15 9.766E+14 1.516E+14 7.160E+12 1.900E+12 1.155E+12 3.193E+11

1.250E+00 6.716E+14 2.095E+14 1.841E+14 1.589E+14 1.071E+14 5.579E+13 6.996E+12

1.750E+00 3.182E+14 2.035E+11 9.620E+10 7.345E+10 5.699E+10 3.807E+10 1.048E+10

2.250E+00 1.203E+14 1.286E+10 2.095E+09 8.448E+08 5.578E+08 2.890E+08 3.522E+07

2.750E+00 2.413E+13 1.001E+07 3.762E+06 2.573E+06 1.726E+06 8.941E+05 1.090E+05

3.500E+00 1.355E+12 6.641E-02 2.661E-02 4.274E-03 1.792E-05 2.237E-07 1.963E-07

Scientific Notebook #170-10e

James Weldy

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20-1402-762

5.000E+00 2.524E+10 1.977E-02 7.923E-03 1.272E-03 5.306E-06 4.005E-08 3.949E-08  
7.000E+00 3.680E+12 1.283E-03 5.141E-04 8.256E-05 3.442E-07 2.593E-09 2.557E-09  
9.500E+00 3.853E+09 8.112E-05 3.251E-05 5.221E-06 2.177E-08 1.642E-10 1.619E-10  
0 TOTAL 2.507E+16 1.628E+15 6.033E+14 3.323E+14 1.807E+14 8.002E+13 8.771E+12  
0MEV/SEC 1.306E+16 1.153E+15 4.039E+14 2.376E+14 1.511E+14 7.545E+13 9.220E+12  
0 18 GROUP SPECIFIC ENERGY RELEASE RATES, MEV/WATT-SEC  
BASIS=MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM,

4 CYCLE

EMEAN

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

1.000E-02 4.482E+07 7.899E+05 2.790E+05 1.343E+05 6.402E+04 2.754E+04 3.563E+03  
2.500E-02 3.556E+07 4.333E+06 2.935E+06 1.673E+06 5.978E+05 1.692E+05 4.226E+03  
3.750E-02 2.267E+07 1.165E+06 8.470E+05 5.903E+05 2.772E+05 9.670E+04 8.690E+03  
5.750E-02 5.076E+07 1.041E+06 2.912E+05 1.005E+05 4.923E+04 2.456E+04 4.060E+03  
8.500E-02 4.495E+07 1.051E+06 3.516E+05 1.427E+05 6.683E+04 3.184E+04 3.748E+03  
1.250E-01 4.183E+07 7.980E+05 4.946E+05 3.692E+05 2.467E+05 1.492E+05 3.612E+04  
2.250E-01 2.038E+08 6.847E+06 2.289E+06 1.094E+06 5.284E+05 1.781E+05 1.519E+04  
3.750E-01 1.731E+08 1.469E+07 1.242E+07 9.603E+06 4.539E+06 1.306E+06 2.723E+04  
5.750E-01 3.115E+09 2.993E+07 2.481E+07 1.914E+07 9.103E+06 2.680E+06 8.292E+04  
8.500E-01 7.560E+09 8.301E+08 1.288E+08 6.086E+06 1.615E+06 9.820E+05 2.714E+05  
1.250E+00 8.395E+08 2.619E+08 2.302E+08 1.986E+08 1.339E+08 6.974E+07 8.745E+06  
1.750E+00 5.568E+08 3.561E+05 1.683E+05 1.285E+05 9.973E+04 6.662E+04 1.835E+04  
2.250E+00 2.707E+08 2.893E+04 4.714E+03 1.901E+03 1.255E+03 6.501E+02 7.925E+01  
2.750E+00 6.637E+07 2.752E+01 1.035E+01 7.077E+00 4.746E+00 2.459E+00 2.997E-01  
3.500E+00 4.744E+06 2.324E-07 9.314E-08 1.496E-08 6.272E-11 7.831E-13 6.871E-13  
5.000E+00 1.262E+05 9.886E-08 3.962E-08 6.362E-09 2.653E-11 2.003E-13 1.974E-13  
7.000E+00 2.576E+07 8.980E-09 3.599E-09 5.779E-10 2.410E-12 1.815E-14 1.790E-14  
9.500E+00 3.661E+04 7.707E-10 3.088E-10 4.960E-11 2.068E-13 1.560E-15 1.538E-15  
0 TOTAL 1.306E+10 1.153E+09 4.039E+08 2.376E+08 1.511E+08 7.545E+07 9.220E+06  
0 GAM POW 2.093E+03 1.848E+02 6.474E+01 3.809E+01 2.422E+01 1.209E+01 1.478E+00

1 OUTPUT UNIT = 6 PAGE 51

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

0 PRINCIPAL PHOTON SOURCES IN GROUP 1,PHOTONS/SEC  
MEAN ENERGY= 0.010MEV

NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

Scientific Notebook #170-10e

James Weldy

12/27/00

20-1402-762

CR 51	4.774E+13	4.953E+11	5.138E+09	5.528E+05	6.888E-07	9.935E-27	0.000E+00
MN 54	1.425E+12	9.503E+11	6.338E+11	2.819E+11	2.481E+10	4.318E+08	1.014E+03
MN 56	3.882E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CO 58	9.704E+12	1.622E+12	2.713E+11	7.584E+09	1.657E+05	2.830E-03	0.000E+00
CO 60	5.383E+12	5.041E+12	4.720E+12	4.138E+12	2.789E+12	1.445E+12	1.761E+11
NI 63	4.084E+10	4.068E+10	4.053E+10	4.022E+10	3.933E+10	3.787E+10	3.357E+10
ZN 65	9.843E+11	5.857E+11	3.485E+11	1.234E+11	5.480E+09	3.051E+07	1.864E+00
Y 90	5.250E+13	6.888E+07	6.807E+07	6.647E+07	6.189E+07	5.494E+07	3.754E+07
ZR 95	1.661E+14	2.297E+13	3.176E+12	6.074E+10	4.246E+05	1.085E-03	0.000E+00
ZR 97	1.798E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NB 95	4.592E+13	1.443E+13	2.216E+12	4.490E+10	3.036E+05	7.761E-04	0.000E+00
NB 95M	1.331E+13	1.942E+12	2.685E+11	5.135E+09	3.590E+04	9.175E-05	0.000E+00
NB 97	1.209E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NB 97M	9.063E+13	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SN119M	1.329E+13	7.927E+12	4.729E+12	1.683E+12	7.582E+10	4.326E+08	2.859E+01
SN123	5.011E+12	1.881E+12	7.058E+11	9.941E+10	2.775E+08	1.539E+04	3.693E-10
SN125	6.665E+13	1.321E+08	2.619E+02	1.029E-09	0.000E+00	0.000E+00	0.000E+00
SN125M	5.049E+13	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SB125	7.647E+12	6.825E+12	6.022E+12	4.689E+12	2.213E+12	6.333E+11	1.155E+10
TE125M	1.441E+12	1.409E+12	1.259E+12	9.818E+11	4.634E+11	1.326E+11	2.419E+09
EU154	9.872E+11	9.482E+11	9.107E+11	8.402E+11	6.597E+11	4.409E+11	1.214E+11
EU155	2.369E+11	2.209E+11	2.060E+11	1.791E+11	1.178E+11	5.854E+10	6.255E+09
GD153	1.403E+12	8.315E+11	4.928E+11	1.731E+11	7.506E+09	4.018E+07	2.162E+00
GD159	2.097E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TB160	5.282E+13	9.171E+12	1.593E+12	4.802E+10	1.316E+06	3.280E-02	0.000E+00

0 PRINCIPAL PHOTON SOURCES IN GROUP 2,PHOTONS/SEC  
MEAN ENERGY= 0.025MEV

#### NUCLIDE

	ASSY DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
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MN 56	8.302E+13	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CO 60	9.304E+11	8.712E+11	8.157E+11	7.152E+11	4.820E+11	2.497E+11	3.044E+10
NI 63	2.488E+09	2.479E+09	2.470E+09	2.451E+09	2.396E+09	2.308E+09	2.046E+09
ZR 95	2.955E+13	4.087E+12	5.651E+11	1.081E+10	7.555E+04	1.931E-04	0.000E+00
ZR 97	3.792E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NB 95	6.275E+12	1.972E+12	3.029E+11	6.137E+09	4.150E+04	1.061E-04	0.000E+00
NB 97	2.470E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SN113	3.169E+13	1.055E+13	3.513E+12	3.894E+11	5.326E+08	8.918E+03	4.640E-12

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SN117M	2.995E+14	3.555E+10	4.220E+06	5.946E-02	0.000E+00	0.000E+00	0.000E+00
SN119M	1.416E+14	8.448E+13	5.040E+13	1.793E+13	8.081E+11	4.610E+09	3.047E+02
SN125	1.429E+13	2.833E+07	5.616E+01	2.207E-10	0.000E+00	0.000E+00	0.000E+00
SB125	4.879E+13	4.354E+13	3.842E+13	2.991E+13	1.412E+13	4.041E+12	7.371E+10
TE125M	2.608E+13	2.550E+13	2.278E+13	1.777E+13	8.389E+12	2.400E+12	4.379E+10
EU154	1.456E+11	1.399E+11	1.344E+11	1.240E+11	9.734E+10	6.505E+10	1.792E+10
GD159	4.170E+13	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00

1 OUTPUT UNIT = 6 PAGE 52

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

0 PRINCIPAL PHOTON SOURCES IN GROUP 3,PHOTONS/SEC  
MEAN ENERGY= 0.038MEV

#### NUCLIDE

	ASSY	DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
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MN 56	5.519E+13	0.000E+00						
CO 60	5.312E+11	4.974E+11	4.657E+11	4.083E+11	2.752E+11	1.426E+11	1.738E+10	
Y 90	7.479E+12	9.812E+06	9.696E+06	9.468E+06	8.816E+06	7.827E+06	5.348E+06	
ZR 95	1.735E+13	2.399E+12	3.318E+11	6.344E+09	4.435E+04	1.134E-04	0.000E+00	
ZR 97	2.487E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
NB 95	2.974E+12	9.346E+11	1.435E+11	2.908E+09	1.966E+04	5.026E-05	0.000E+00	
NB 97	1.595E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
SN125	9.455E+12	1.874E+07	3.715E+01	1.460E-10	0.000E+00	0.000E+00	0.000E+00	
SN125M	7.084E+12	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
SB125	1.338E+13	1.194E+13	1.054E+13	8.204E+12	3.872E+12	1.108E+12	2.021E+10	
TE125M	6.052E+12	5.918E+12	5.287E+12	4.124E+12	1.947E+12	5.570E+11	1.016E+10	
EU154	1.343E+12	1.290E+12	1.239E+12	1.143E+12	8.977E+11	5.999E+11	1.652E+11	
EU155	6.889E+11	6.424E+11	5.990E+11	5.209E+11	3.425E+11	1.703E+11	1.819E+10	
EU156	9.658E+12	2.315E+09	5.549E+05	3.188E-02	0.000E+00	0.000E+00	0.000E+00	
GD153	1.065E+13	6.310E+12	3.740E+12	1.314E+12	5.696E+10	3.049E+08	1.641E+01	
GD159	2.636E+13	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
TB160	3.996E+12	6.939E+11	1.205E+11	3.633E+09	9.958E+04	2.481E-03	0.000E+00	

0 PRINCIPAL PHOTON SOURCES IN GROUP 4,PHOTONS/SEC  
MEAN ENERGY= 0.058MEV

#### NUCLIDE

	ASSY	DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
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MN 56	8.065E+13	0.000E+00						
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Scientific Notebook #170-10e

James Weldy

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CO 60	5.993E+11	5.611E+11	5.254E+11	4.606E+11	3.105E+11	1.608E+11	1.961E+10
Y 90	1.100E+13	1.444E+07	1.427E+07	1.393E+07	1.297E+07	1.152E+07	7.868E+06
ZR 95	2.056E+13	2.843E+12	3.932E+11	7.518E+09	5.256E+04	1.343E-04	0.000E+00
ZR 97	3.597E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NB 95	2.296E+12	7.216E+11	1.108E+11	2.245E+09	1.518E+04	3.881E-05	0.000E+00
NB 97	2.245E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SN119M	2.215E+11	1.321E+11	7.882E+10	2.805E+10	1.264E+09	7.209E+06	4.765E-01
SN123	9.576E+11	3.594E+11	1.349E+11	1.900E+10	5.304E+07	2.941E+03	7.058E-11
SN125	1.388E+13	2.751E+07	5.454E+01	2.143E-10	0.000E+00	0.000E+00	0.000E+00
SN125M	1.031E+13	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SB125	6.493E+11	5.795E+11	5.114E+11	3.982E+11	1.879E+11	5.378E+10	9.811E+08
EU154	3.603E+11	3.461E+11	3.324E+11	3.067E+11	2.408E+11	1.609E+11	4.432E+10
EU155	2.077E+11	1.936E+11	1.806E+11	1.570E+11	1.032E+11	5.132E+10	5.484E+09
GD153	2.278E+12	1.350E+12	8.004E+11	2.812E+11	1.219E+10	6.525E+07	3.512E+00
GD159	3.583E+13	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TB160	5.310E+13	9.220E+12	1.601E+12	4.827E+10	1.323E+06	3.297E-02	0.000E+00
HF181	1.113E+13	5.622E+11	2.839E+10	7.240E+07	1.201E+00	1.295E-13	0.000E+00
TA182	3.030E+12	1.008E+12	3.352E+11	3.709E+10	5.024E+07	2.317E+04	2.234E+04
W187	9.641E+12	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00

1

OUTPUT UNIT = 6

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ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

0

PRINCIPAL PHOTON SOURCES IN GROUP 5,PHOTONS/SEC  
MEAN ENERGY= 0.085MEV

#### NUCLIDE

	ASSY	DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
MN 56	5.045E+13	0.000E+00						
CO 60	2.356E+11	2.206E+11	2.066E+11	1.811E+11	1.221E+11	6.324E+10	7.709E+09	
Y 90	6.836E+12	8.968E+06	8.862E+06	8.654E+06	8.057E+06	7.153E+06	4.888E+06	
ZR 95	8.892E+12	1.230E+12	1.700E+11	3.251E+09	2.273E+04	5.810E-05	0.000E+00	
ZR 97	2.193E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
NB 97	1.309E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
SN123	5.663E+11	2.125E+11	7.976E+10	1.123E+10	3.137E+07	1.739E+03	4.174E-11	
SN125	8.589E+12	1.703E+07	3.375E+01	1.326E-10	0.000E+00	0.000E+00	0.000E+00	
SN125M	6.344E+12	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
SB125	2.906E+11	2.594E+11	2.289E+11	1.782E+11	8.412E+10	2.407E+10	4.391E+08	
EU154	6.905E+10	6.632E+10	6.370E+10	5.877E+10	4.615E+10	3.084E+10	8.493E+09	
EU155	1.037E+12	9.667E+11	9.014E+11	7.838E+11	5.154E+11	2.562E+11	2.738E+10	

Scientific Notebook #170-10e

James Weldy

12/27/00

20-1402-762

EU156 7.611E+12 1.824E+09 4.373E+05 2.512E-02 0.000E+00 0.000E+00 0.000E+00  
GD153 3.403E+12 2.017E+12 1.195E+12 4.199E+11 1.821E+10 9.745E+07 5.245E+00  
GD159 1.977E+13 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
TB160 4.052E+13 7.036E+12 1.222E+12 3.684E+10 1.010E+06 2.516E-02 0.000E+00

0 PRINCIPAL PHOTON SOURCES IN GROUP 6,PHOTONS/SEC  
MEAN ENERGY= 0.125MEV

NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

MN 56 3.384E+13 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CO 60 9.050E+10 8.474E+10 7.934E+10 6.957E+10 4.688E+10 2.429E+10 2.961E+09  
Y 90 4.579E+12 6.007E+06 5.936E+06 5.797E+06 5.397E+06 4.792E+06 3.274E+06  
ZR 95 3.898E+12 5.390E+11 7.454E+10 1.425E+09 9.964E+03 2.547E-05 0.000E+00  
ZR 97 1.456E+14 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
NB 97 8.234E+13 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SN123 3.611E+11 1.355E+11 5.086E+10 7.164E+09 2.000E+07 1.109E+03 2.661E-11  
SN125 5.744E+12 1.139E+07 2.257E+01 8.869E-11 0.000E+00 0.000E+00 0.000E+00  
SN125M 4.201E+12 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SB125 5.052E+11 4.509E+11 3.978E+11 3.098E+11 1.462E+11 4.184E+10 7.633E+08  
TE125M 6.255E+10 6.116E+10 5.464E+10 4.262E+10 2.012E+10 5.757E+09 1.050E+08  
EU154 2.196E+12 2.109E+12 2.026E+12 1.869E+12 1.467E+12 9.806E+11 2.701E+11  
EU155 5.708E+11 5.323E+11 4.963E+11 4.316E+11 2.838E+11 1.411E+11 1.507E+10  
GD153 1.731E+12 1.026E+12 6.082E+11 2.137E+11 9.263E+09 4.958E+07 2.668E+00  
GD159 1.168E+13 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
TB160 1.503E+12 2.611E+11 4.533E+10 1.367E+09 3.746E+04 9.336E-04 0.000E+00  
HF181 1.759E+13 8.881E+11 4.485E+10 1.144E+08 1.897E+00 2.045E-13 0.000E+00  
TA182 6.100E+11 2.029E+11 6.749E+10 7.467E+09 1.012E+07 4.665E+03 4.498E+03  
W187 3.387E+12 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

1 OUTPUT UNIT = 6 PAGE 54

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

0 PRINCIPAL PHOTON SOURCES IN GROUP 7,PHOTONS/SEC  
MEAN ENERGY= 0.225MEV

NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

MN 56 4.792E+13 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CO 60 2.976E+10 2.787E+10 2.609E+10 2.288E+10 1.542E+10 7.987E+09 9.736E+08

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ZR 97 2.826E+14 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
NB 95M 4.871E+12 7.109E+11 9.830E+10 1.880E+09 1.314E+04 3.359E-05 0.000E+00  
NB 97 1.031E+14 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SN113 1.059E+12 3.527E+11 1.174E+11 1.302E+10 1.780E+07 2.981E+02 1.551E-13  
SN117M 2.752E+14 3.267E+10 3.878E+06 5.464E-02 0.000E+00 0.000E+00 0.000E+00  
SB125 7.012E+12 6.258E+12 5.522E+12 4.300E+12 2.030E+12 5.808E+11 1.060E+10  
EU154 4.537E+11 4.357E+11 4.185E+11 3.861E+11 3.032E+11 2.026E+11 5.580E+10  
GD159 1.222E+13 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
TB160 1.246E+14 2.164E+13 3.758E+12 1.133E+11 3.106E+06 7.739E-02 0.000E+00

0 PRINCIPAL PHOTON SOURCES IN GROUP 8,PHOTONS/SEC  
MEAN ENERGY= 0.375MEV

NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

CR 51 3.564E+13 3.697E+11 3.835E+09 4.127E+05 5.142E-07 7.416E-27 0.000E+00  
MN 56 2.253E+13 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
ZR 97 1.933E+14 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
NB 97 3.328E+13 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SN125 5.662E+12 1.122E+07 2.225E+01 8.742E-11 0.000E+00 0.000E+00 0.000E+00  
SN125M 9.903E+13 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SB125 4.163E+13 3.716E+13 3.279E+13 2.553E+13 1.205E+13 3.448E+12 6.291E+10  
EU154 7.228E+10 6.943E+10 6.669E+10 6.152E+10 4.831E+10 3.229E+10 8.891E+09  
TB160 7.070E+12 1.228E+12 2.132E+11 6.428E+09 1.762E+05 4.390E-03 0.000E+00

0 PRINCIPAL PHOTON SOURCES IN GROUP 9,PHOTONS/SEC  
MEAN ENERGY= 0.575MEV

NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

CO 58 1.146E+13 1.917E+12 3.205E+11 8.960E+09 1.958E+05 3.343E-03 0.000E+00  
ZR 97 3.346E+14 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
NB 97 4.897E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SB125 5.351E+13 4.776E+13 4.214E+13 3.281E+13 1.549E+13 4.432E+12 8.086E+10  
EU154 5.108E+11 4.907E+11 4.713E+11 4.348E+11 3.414E+11 2.282E+11 6.284E+10  
HF181 2.346E+13 1.185E+12 5.982E+10 1.526E+08 2.530E+00 2.728E-13 0.000E+00

1 OUTPUT UNIT = 6 PAGE 55

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

0 PRINCIPAL PHOTON SOURCES IN GROUP 10,PHOTONS/SEC

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MEAN ENERGY= 0.850MEV

NUCLIDE

	ASSY DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
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MN 54	1.014E+13	6.762E+12	4.510E+12	2.006E+12	1.765E+11	3.073E+09	7.212E+03
MN 56	7.836E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZR 95	2.214E+15	3.062E+14	4.234E+13	8.095E+11	5.659E+06	1.447E-02	0.000E+00
ZR 97	1.070E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NB 95	1.970E+15	6.192E+14	9.509E+13	1.927E+12	1.303E+07	3.330E-02	0.000E+00
NB 97M	3.514E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
EU154	2.568E+12	2.466E+12	2.369E+12	2.185E+12	1.716E+12	1.147E+12	3.158E+11
TB160	2.015E+14	3.499E+13	6.075E+12	1.832E+11	5.021E+06	1.251E-01	0.000E+00

0 PRINCIPAL PHOTON SOURCES IN GROUP 11,PHOTONS/SEC

MEAN ENERGY= 1.250MEV

NUCLIDE

	ASSY DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
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NA 24	9.917E+12	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
V 52	2.768E+13	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CO 60	2.031E+14	1.902E+14	1.781E+14	1.562E+14	1.052E+14	5.452E+13	6.646E+12
ZR 97	2.656E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NB 97	1.231E+13	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SN125	1.869E+13	3.705E+07	7.344E+01	2.886E-10	0.000E+00	0.000E+00	0.000E+00
EU154	2.843E+12	2.731E+12	2.623E+12	2.420E+12	1.900E+12	1.270E+12	3.497E+11
EU156	2.731E+13	6.546E+09	1.569E+06	9.015E-02	0.000E+00	0.000E+00	0.000E+00
TB160	8.440E+13	1.465E+13	2.545E+12	7.672E+10	2.103E+06	5.240E-02	0.000E+00

0 PRINCIPAL PHOTON SOURCES IN GROUP 12,PHOTONS/SEC

MEAN ENERGY= 1.750MEV

NUCLIDE

	ASSY DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
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AL 28	6.583E+12	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
MN 56	2.230E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CO 58	2.125E+11	3.554E+10	5.942E+09	1.661E+08	3.629E+03	6.198E-05	0.000E+00
ZR 97	7.454E+13	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NB 97	5.634E+12	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00

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AG110M 4.463E+09 2.689E+09 1.620E+09 5.883E+08 2.815E+07 1.776E+05 1.620E-02  
SB124 6.706E+11 8.189E+10 9.999E+09 1.491E+08 4.941E+02 3.641E-07 0.000E+00  
EU154 8.523E+10 8.186E+10 7.863E+10 7.254E+10 5.696E+10 3.807E+10 1.048E+10  
EU156 6.121E+12 1.467E+09 3.517E+05 2.020E-02 0.000E+00 0.000E+00 0.000E+00

1 OUTPUT UNIT = 6 PAGE 56

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

0 PRINCIPAL PHOTON SOURCES IN GROUP 13,PHOTONS/SEC  
MEAN ENERGY= 2.250MEV

#### NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

MN 56 1.067E+14 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CO 60 1.077E+09 1.008E+09 9.439E+08 8.276E+08 5.578E+08 2.890E+08 3.522E+07  
SN125 2.927E+12 5.802E+06 1.150E+01 4.520E-11 0.000E+00 0.000E+00 0.000E+00  
SB124 7.716E+10 9.422E+09 1.150E+09 1.715E+07 5.686E+01 4.189E-08 0.000E+00  
EU156 1.011E+13 2.422E+09 5.806E+05 3.336E-02 0.000E+00 0.000E+00 0.000E+00

0 PRINCIPAL PHOTON SOURCES IN GROUP 14,PHOTONS/SEC  
MEAN ENERGY= 2.750MEV

#### NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

NA 24 9.098E+12 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
MN 56 1.494E+13 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CO 60 3.331E+06 3.119E+06 2.921E+06 2.561E+06 1.726E+06 8.941E+05 1.090E+05  
SB124 5.640E+07 6.887E+06 8.409E+05 1.254E+04 4.156E-02 3.062E-11 0.000E+00

0 PRINCIPAL PHOTON SOURCES IN GROUP 15,PHOTONS/SEC  
MEAN ENERGY= 3.500MEV

#### NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

N 16 5.401E+10 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
K 42 2.552E+03 1.092E-07 1.081E-07 1.058E-07 9.938E-08 8.947E-08 6.393E-08  
MN 56 1.281E+12 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
BI210M 1.318E-07 1.318E-07 1.318E-07 1.318E-07 1.318E-07 1.318E-07 1.318E-07  
PO210 1.575E-01 6.641E-02 2.661E-02 4.273E-03 1.769E-05 2.419E-09 5.304E-10  
0 PRINCIPAL PHOTON SOURCES IN GROUP 16,PHOTONS/SEC

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MEAN ENERGY= 5.000MEV

NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

LI 8 2.276E+09 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

C 15 2.696E+09 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

N 16 2.019E+10 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

BI210M 3.933E-08 3.933E-08 3.933E-08 3.933E-08 3.933E-08 3.933E-08 3.933E-08

PO210 4.689E-02 1.977E-02 7.923E-03 1.272E-03 5.266E-06 7.203E-10 1.579E-10

0 PRINCIPAL PHOTON SOURCES IN GROUP 17,PHOTONS/SEC

MEAN ENERGY= 7.000MEV

NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

N 16 3.679E+12 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

BI210M 2.547E-09 2.547E-09 2.547E-09 2.547E-09 2.547E-09 2.547E-09 2.547E-09

PO210 3.043E-03 1.283E-03 5.141E-04 8.256E-05 3.417E-07 4.674E-11 1.025E-11

1 OUTPUT UNIT = 6 PAGE 57

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

0 PRINCIPAL PHOTON SOURCES IN GROUP 18,PHOTONS/SEC

MEAN ENERGY= 9.500MEV

NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

LI 8 8.112E+07 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

N 16 3.769E+09 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

BI210M 1.612E-10 1.612E-10 1.612E-10 1.612E-10 1.612E-10 1.612E-10 1.612E-10

PO210 1.924E-04 8.112E-05 3.251E-05 5.220E-06 2.161E-08 2.955E-12 6.479E-13

1 OUTPUT UNIT = 6 PAGE 58

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

PHOTON SPECTRUM FOR ACTINIDES + DAUGHTERS

0 ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP  
(BWRU)

POWER= 1.00 MW, BURNUP= 1. MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC

0 18 GROUP PHOTON RELEASE RATES, PHOTONS/SECOND

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BASIS=MTIHM 4.5% UO2 FUEL ASSY;BURNUP=45,000 MWD/MTIHM,

4 CYCLE

EMEAN

ASSY DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
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1.000E-02	7.712E+17	2.442E+14	1.426E+14	7.483E+13	5.843E+13	6.050E+13	6.303E+13
2.500E-02	3.395E+16	3.577E+11	4.572E+11	6.489E+11	1.170E+12	1.880E+12	3.239E+12
3.750E-02	4.895E+16	6.559E+11	4.245E+11	2.778E+11	2.723E+11	3.218E+11	4.128E+11
5.750E-02	4.805E+16	4.959E+12	6.422E+12	9.242E+12	1.690E+13	2.735E+13	4.734E+13
8.500E-02	3.417E+17	9.559E+11	9.540E+11	9.501E+11	9.382E+11	9.195E+11	8.698E+11
1.250E-01	2.710E+17	9.042E+11	8.869E+11	8.698E+11	8.430E+11	8.058E+11	7.121E+11
2.250E-01	1.920E+17	7.273E+11	7.155E+11	7.009E+11	6.705E+11	6.265E+11	5.187E+11
3.750E-01	2.083E+16	3.984E+10	3.984E+10	3.985E+10	3.987E+10	3.989E+10	3.997E+10
5.750E-01	3.568E+15	3.628E+09	2.046E+09	1.066E+09	1.097E+09	1.436E+09	1.803E+09
8.500E-01	9.808E+15	2.528E+09	2.191E+09	1.979E+09	1.963E+09	1.972E+09	1.805E+09
1.250E+00	3.136E+15	1.172E+09	1.063E+09	9.823E+08	9.304E+08	8.777E+08	7.431E+08
1.750E+00	1.210E+12	2.449E+08	2.049E+08	1.788E+08	1.726E+08	1.642E+08	1.182E+08
2.250E+00	1.803E+08	1.282E+08	1.031E+08	8.427E+07	7.154E+07	5.930E+07	3.281E+07
2.750E+00	1.965E+08	1.985E+08	2.170E+08	2.711E+08	4.227E+08	5.442E+08	5.259E+08
3.500E+00	9.377E+07	6.676E+07	5.375E+07	4.395E+07	3.732E+07	3.093E+07	1.710E+07
5.000E+00	4.011E+07	2.856E+07	2.299E+07	1.880E+07	1.596E+07	1.323E+07	7.308E+06
7.000E+00	4.615E+06	3.288E+06	2.649E+06	2.167E+06	1.840E+06	1.525E+06	8.420E+05
9.500E+00	5.315E+05	3.783E+05	3.046E+05	2.490E+05	2.114E+05	1.751E+05	9.670E+04
0 TOTAL	1.744E+18	2.528E+14	1.525E+14	8.756E+13	7.927E+13	9.246E+13	1.162E+14
0 MEV/SEC	1.414E+17	3.141E+12	2.197E+12	1.673E+12	1.952E+12	2.577E+12	3.749E+12
0	18 GROUP SPECIFIC ENERGY RELEASE RATES, MEV/WATT-SEC						

BASIS=MTIHM 4.5% UO2 FUEL ASSY;BURNUP=45,000 MWD/MTIHM,

4 CYCLE

EMEAN

ASSY DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
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1.000E-02	7.712E+09	2.442E+06	1.426E+06	7.483E+05	5.843E+05	6.050E+05	6.303E+05
2.500E-02	8.487E+08	8.943E+03	1.143E+04	1.622E+04	2.924E+04	4.701E+04	8.099E+04
3.750E-02	1.836E+09	2.460E+04	1.592E+04	1.042E+04	1.021E+04	1.207E+04	1.548E+04
5.750E-02	2.763E+09	2.851E+05	3.693E+05	5.314E+05	9.718E+05	1.573E+06	2.722E+06
8.500E-02	2.905E+10	8.125E+04	8.109E+04	8.076E+04	7.974E+04	7.816E+04	7.394E+04
1.250E-01	3.388E+10	1.130E+05	1.109E+05	1.087E+05	1.054E+05	1.007E+05	8.901E+04
2.250E-01	4.319E+10	1.637E+05	1.610E+05	1.577E+05	1.509E+05	1.410E+05	1.167E+05
3.750E-01	7.811E+09	1.494E+04	1.494E+04	1.494E+04	1.495E+04	1.496E+04	1.499E+04

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5.750E-01 2.052E+09 2.086E+03 1.177E+03 6.132E+02 6.306E+02 8.256E+02 1.037E+03  
8.500E-01 8.337E+09 2.149E+03 1.862E+03 1.682E+03 1.669E+03 1.676E+03 1.534E+03  
1.250E+00 3.920E+09 1.465E+03 1.329E+03 1.228E+03 1.163E+03 1.097E+03 9.289E+02  
1.750E+00 2.117E+06 4.285E+02 3.585E+02 3.129E+02 3.020E+02 2.874E+02 2.069E+02  
2.250E+00 4.056E+02 2.885E+02 2.321E+02 1.896E+02 1.610E+02 1.334E+02 7.382E+01  
2.750E+00 5.405E+02 5.458E+02 5.969E+02 7.455E+02 1.162E+03 1.497E+03 1.446E+03  
3.500E+00 3.282E+02 2.337E+02 1.881E+02 1.538E+02 1.306E+02 1.082E+02 5.983E+01  
5.000E+00 2.006E+02 1.428E+02 1.150E+02 9.399E+01 7.980E+01 6.613E+01 3.654E+01  
7.000E+00 3.231E+01 2.302E+01 1.854E+01 1.517E+01 1.288E+01 1.067E+01 5.894E+00  
9.500E+00 5.049E+00 3.594E+00 2.893E+00 2.366E+00 2.008E+00 1.664E+00 9.186E-01  
0 TOTAL 1.414E+11 3.141E+06 2.197E+06 1.673E+06 1.952E+06 2.577E+06 3.749E+06  
0 GAM POW 2.267E+04 5.035E-01 3.521E-01 2.683E-01 3.129E-01 4.132E-01 6.010E-01

1

OUTPUT UNIT = 6

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ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

0 PRINCIPAL PHOTON SOURCES IN GROUP 1,PHOTONS/SEC  
MEAN ENERGY= 0.010MEV

NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

U237 2.689E+16 1.023E+11 9.968E+10 9.499E+10 8.222E+10 6.463E+10 2.992E+10  
U239 2.376E+17 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
NP238 9.741E+15 1.929E+09 1.924E+09 1.916E+09 1.890E+09 1.847E+09 1.717E+09  
NP239 4.884E+17 8.363E+11 8.363E+11 8.362E+11 8.360E+11 8.356E+11 8.343E+11  
PU238 2.468E+13 2.582E+13 2.622E+13 2.635E+13 2.582E+13 2.483E+13 2.189E+13  
PU239 6.324E+11 6.405E+11 6.405E+11 6.404E+11 6.404E+11 6.403E+11 6.401E+11  
PU240 3.064E+12 3.065E+12 3.065E+12 3.067E+12 3.071E+12 3.076E+12 3.086E+12  
PU241 1.940E+12 1.894E+12 1.849E+12 1.762E+12 1.525E+12 1.199E+12 5.550E+11  
AM241 1.999E+12 2.891E+12 3.761E+12 5.437E+12 9.991E+12 1.621E+13 2.809E+13  
CM242 4.098E+14 1.899E+14 8.747E+13 1.860E+13 2.523E+11 7.417E+10 6.885E+10  
CM243 1.050E+12 1.037E+12 1.024E+12 9.997E+11 9.294E+11 8.230E+11 5.577E+11  
CM244 1.742E+13 1.710E+13 1.677E+13 1.614E+13 1.439E+13 1.189E+13 6.443E+12

0

PRINCIPAL PHOTON SOURCES IN GROUP 2,PHOTONS/SEC  
MEAN ENERGY= 0.025MEV

NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

U237 9.984E+14 3.798E+09 3.701E+09 3.527E+09 3.052E+09 2.400E+09 1.111E+09

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U239 2.566E+16 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
NP238 3.800E+14 7.525E+07 7.508E+07 7.474E+07 7.372E+07 7.206E+07 6.699E+07  
NP239 6.383E+15 1.093E+10 1.093E+10 1.093E+10 1.092E+10 1.092E+10 1.090E+10  
AM241 2.288E+11 3.309E+11 4.305E+11 6.225E+11 1.144E+12 1.855E+12 3.216E+12  
AM242 6.881E+13 8.376E+09 8.357E+09 8.319E+09 8.206E+09 8.021E+09 7.457E+09

0 PRINCIPAL PHOTON SOURCES IN GROUP 3,PHOTONS/SEC

MEAN ENERGY= 0.038MEV

NUCLIDE

	ASSY	DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
--	------	-----	-------	-------	-------	-------	--------	--------

U239	4.377E+16	0.000E+00						
NP239	4.336E+15	7.424E+09	7.424E+09	7.423E+09	7.421E+09	7.417E+09	7.406E+09	
PU238	7.104E+10	7.433E+10	7.548E+10	7.586E+10	7.434E+10	7.147E+10	6.301E+10	
AM241	1.872E+10	2.708E+10	3.523E+10	5.093E+10	9.358E+10	1.518E+11	2.631E+11	
AM242	4.571E+13	5.565E+09	5.552E+09	5.527E+09	5.452E+09	5.329E+09	4.954E+09	
AM243	5.865E+10	5.871E+10	5.870E+10	5.870E+10	5.868E+10	5.865E+10	5.857E+10	
CM242	9.603E+11	4.450E+11	2.050E+11	4.359E+10	5.914E+08	1.738E+08	1.613E+08	
CM244	3.450E+10	3.385E+10	3.321E+10	3.196E+10	2.850E+10	2.353E+10	1.276E+10	

1 OUTPUT UNIT = 6 PAGE 60

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0 PRINCIPAL PHOTON SOURCES IN GROUP 4,PHOTONS/SEC

MEAN ENERGY= 0.058MEV

NUCLIDE

	ASSY	DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
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U237	1.262E+16	4.803E+10	4.680E+10	4.460E+10	3.860E+10	3.034E+10	1.405E+10	
U239	2.292E+16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
NP239	1.171E+16	2.005E+10	2.005E+10	2.005E+10	2.004E+10	2.003E+10	2.000E+10	
AM241	3.364E+12	4.866E+12	6.331E+12	9.152E+12	1.682E+13	2.728E+13	4.729E+13	
0	PRINCIPAL PHOTON SOURCES IN GROUP 5,PHOTONS/SEC							
	MEAN ENERGY= 0.085MEV							

NUCLIDE

	ASSY	DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
--	------	-----	-------	-------	-------	-------	--------	--------

U237	5.861E+15	2.230E+10	2.173E+10	2.071E+10	1.792E+10	1.409E+10	6.521E+09	
U239	2.455E+17	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	

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NP239	8.703E+16	1.490E+11	1.490E+11	1.490E+11	1.490E+11	1.489E+11	1.487E+11
PU238	1.366E+10	1.429E+10	1.451E+10	1.458E+10	1.429E+10	1.374E+10	1.211E+10
AM241	2.207E+09	3.192E+09	4.152E+09	6.003E+09	1.103E+10	1.789E+10	3.102E+10
AM242	2.300E+14	2.800E+10	2.793E+10	2.781E+10	2.743E+10	2.681E+10	2.492E+10
AM243	5.261E+11	5.266E+11	5.265E+11	5.265E+11	5.263E+11	5.261E+11	5.253E+11
CM243	2.015E+11	1.991E+11	1.967E+11	1.919E+11	1.784E+11	1.580E+11	1.071E+11
0	PRINCIPAL PHOTON SOURCES IN GROUP 6,PHOTONS/SEC						
	MEAN ENERGY= 0.125MEV						

NUCLIDE

	ASSY	DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
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U237	1.021E+16	3.884E+10	3.784E+10	3.606E+10	3.121E+10	2.454E+10	1.136E+10
U239	8.924E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NP239	2.511E+17	4.299E+11	4.299E+11	4.299E+11	4.297E+11	4.295E+11	4.289E+11
AM241	2.107E+09	3.048E+09	3.965E+09	5.733E+09	1.053E+10	1.709E+10	2.962E+10
AM242	3.676E+14	4.475E+10	4.465E+10	4.444E+10	4.384E+10	4.285E+10	3.984E+10
CM242	5.129E+10	2.377E+10	1.095E+10	2.328E+09	3.158E+07	9.282E+06	8.617E+06
CM243	3.538E+11	3.496E+11	3.453E+11	3.370E+11	3.133E+11	2.775E+11	1.880E+11
0	PRINCIPAL PHOTON SOURCES IN GROUP 7,PHOTONS/SEC						
	MEAN ENERGY= 0.225MEV						

NUCLIDE

	ASSY	DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
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U237	7.697E+15	2.928E+10	2.853E+10	2.719E+10	2.353E+10	1.850E+10	8.564E+09	
U239	9.769E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
NP239	1.741E+17	2.980E+11	2.980E+11	2.980E+11	2.979E+11	2.978E+11	2.973E+11	
CM242	2.615E+10	1.212E+10	5.581E+09	1.187E+09	1.610E+07	4.732E+06	4.393E+06	
CM243	3.862E+11	3.816E+11	3.770E+11	3.679E+11	3.420E+11	3.028E+11	2.052E+11	
1	OUTPUT UNIT = 6						PAGE 61	
ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12								
0	PRINCIPAL PHOTON SOURCES IN GROUP 8,PHOTONS/SEC							
	MEAN ENERGY= 0.375MEV							

NUCLIDE

	ASSY	DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
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PA233	7.411E+09	7.328E+09	7.328E+09	7.331E+09	7.344E+09	7.383E+09	7.598E+09
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U237	4.541E+14	1.727E+09	1.683E+09	1.604E+09	1.388E+09	1.091E+09	5.052E+08
U239	3.311E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NP239	1.677E+16	2.872E+10	2.872E+10	2.872E+10	2.871E+10	2.870E+10	2.865E+10
PU239	7.066E+08	7.156E+08	7.156E+08	7.156E+08	7.155E+08	7.155E+08	7.152E+08
AM241	1.140E+08	1.648E+08	2.144E+08	3.100E+08	5.696E+08	9.240E+08	1.602E+09
CM243	6.789E+08	6.707E+08	6.626E+08	6.467E+08	6.012E+08	5.323E+08	3.607E+08
0	PRINCIPAL PHOTON SOURCES IN GROUP 9,PHOTONS/SEC						
	MEAN ENERGY= 0.575MEV						

NUCLIDE

	ASSY	DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
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TL208	1.040E+08	1.401E+08	1.774E+08	2.506E+08	4.298E+08	5.749E+08	5.716E+08
PA234M	1.541E+08	1.514E+08	1.514E+08	1.514E+08	1.514E+08	1.514E+08	1.514E+08
U239	3.115E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NP238	5.242E+13	1.038E+07	1.036E+07	1.031E+07	1.017E+07	9.939E+06	9.240E+06
NP239	7.227E+13	1.237E+08	1.237E+08	1.237E+08	1.237E+08	1.236E+08	1.234E+08
NP240M	4.160E+13	7.229E+03	7.229E+03	7.229E+03	7.229E+03	7.229E+03	7.229E+03
NP240	2.737E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
PU239	2.603E+07	2.636E+07	2.636E+07	2.636E+07	2.636E+07	2.635E+07	2.634E+07
AM241	6.249E+07	9.039E+07	1.176E+08	1.700E+08	3.124E+08	5.067E+08	8.784E+08
AM243	1.317E+07	1.319E+07	1.319E+07	1.318E+07	1.318E+07	1.317E+07	1.315E+07
CM242	6.587E+09	3.052E+09	1.406E+09	2.990E+08	4.056E+06	1.192E+06	1.107E+06
0	PRINCIPAL PHOTON SOURCES IN GROUP 10,PHOTONS/SEC						
	MEAN ENERGY= 0.850MEV						

NUCLIDE

	ASSY	DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
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TL208	1.390E+07	1.872E+07	2.371E+07	3.349E+07	5.745E+07	7.683E+07	7.639E+07
BI212	3.545E+07	4.774E+07	6.044E+07	8.540E+07	1.465E+08	1.959E+08	1.948E+08
PA234M	8.326E+07	8.181E+07	8.181E+07	8.182E+07	8.181E+07	8.181E+07	8.181E+07
PA234	3.000E+08	2.133E+07	2.133E+07	2.133E+07	2.133E+07	2.133E+07	2.133E+07
U239	4.615E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NP238	4.849E+15	9.601E+08	9.579E+08	9.535E+08	9.406E+08	9.194E+08	8.547E+08
NP240	3.343E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
PU238	7.670E+07	8.025E+07	8.150E+07	8.190E+07	8.026E+07	7.717E+07	6.803E+07
AM241	1.836E+07	2.655E+07	3.455E+07	4.994E+07	9.177E+07	1.489E+08	2.581E+08
CM242	1.400E+09	6.489E+08	2.989E+08	6.356E+07	8.623E+05	2.534E+05	2.353E+05

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CM244 6.436E+08 6.315E+08 6.195E+08 5.962E+08 5.316E+08 4.390E+08 2.379E+08  
1 OUTPUT UNIT = 6 PAGE 62  
ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12  
0 PRINCIPAL PHOTON SOURCES IN GROUP 11,PHOTONS/SEC  
MEAN ENERGY= 1.250MEV

NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

BI212 2.411E+06 3.247E+06 4.111E+06 5.808E+06 9.962E+06 1.332E+07 1.325E+07  
PA234M 7.209E+07 7.084E+07 7.084E+07 7.084E+07 7.084E+07 7.084E+07 7.084E+07  
U239 5.439E+13 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
NP238 3.043E+15 6.026E+08 6.012E+08 5.985E+08 5.903E+08 5.770E+08 5.364E+08  
NP240 3.523E+13 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CM242 4.123E+08 1.911E+08 8.801E+07 1.872E+07 2.539E+05 7.462E+04 6.927E+04  
CM244 2.997E+08 2.941E+08 2.885E+08 2.777E+08 2.476E+08 2.044E+08 1.108E+08  
0 PRINCIPAL PHOTON SOURCES IN GROUP 12,PHOTONS/SEC  
MEAN ENERGY= 1.750MEV

NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

BI212 9.146E+06 1.232E+07 1.560E+07 2.203E+07 3.779E+07 5.054E+07 5.025E+07  
PA234M 1.044E+07 1.026E+07 1.026E+07 1.026E+07 1.026E+07 1.026E+07 1.026E+07  
NP240M 1.209E+12 2.102E+02 2.102E+02 2.102E+02 2.102E+02 2.102E+02 2.102E+02  
CM242 1.622E+08 7.515E+07 3.461E+07 7.361E+06 9.985E+04 2.935E+04 2.724E+04  
CM244 1.464E+08 1.436E+08 1.409E+08 1.356E+08 1.209E+08 9.984E+07 5.412E+07  
0 PRINCIPAL PHOTON SOURCES IN GROUP 13,PHOTONS/SEC  
MEAN ENERGY= 2.250MEV

NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

PU240 5.638E+05 5.639E+05 5.640E+05 5.643E+05 5.650E+05 5.660E+05 5.678E+05  
CM242 9.402E+07 4.357E+07 2.007E+07 4.268E+06 5.790E+04 1.702E+04 1.580E+04  
CM244 8.480E+07 8.321E+07 8.163E+07 7.857E+07 7.004E+07 5.784E+07 3.135E+07  
CM246 3.471E+05 3.471E+05 3.470E+05 3.470E+05 3.468E+05 3.466E+05 3.458E+05  
0 PRINCIPAL PHOTON SOURCES IN GROUP 14,PHOTONS/SEC  
MEAN ENERGY= 2.750MEV

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NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

TL208 9.227E+07 1.243E+08 1.573E+08 2.223E+08 3.812E+08 5.099E+08 5.069E+08

CM242 5.430E+07 2.517E+07 1.159E+07 2.465E+06 3.344E+04 9.828E+03 9.123E+03

CM244 4.914E+07 4.822E+07 4.730E+07 4.553E+07 4.059E+07 3.352E+07 1.817E+07

0 PRINCIPAL PHOTON SOURCES IN GROUP 15,PHOTONS/SEC

MEAN ENERGY= 3.500MEV

NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

PU240 2.921E+05 2.922E+05 2.922E+05 2.924E+05 2.927E+05 2.933E+05 2.942E+05

CM242 4.877E+07 2.260E+07 1.041E+07 2.214E+06 3.003E+04 8.827E+03 8.194E+03

CM244 4.426E+07 4.343E+07 4.260E+07 4.100E+07 3.656E+07 3.019E+07 1.636E+07

CM246 1.804E+05 1.804E+05 1.804E+05 1.803E+05 1.803E+05 1.801E+05 1.797E+05

1 OUTPUT UNIT = 6 PAGE 63

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

0 PRINCIPAL PHOTON SOURCES IN GROUP 16,PHOTONS/SEC

MEAN ENERGY= 5.000MEV

NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

PU240 1.250E+05 1.250E+05 1.251E+05 1.251E+05 1.253E+05 1.255E+05 1.259E+05

CM242 2.087E+07 9.670E+06 4.454E+06 9.472E+05 1.285E+04 3.777E+03 3.506E+03

CM244 1.893E+07 1.858E+07 1.823E+07 1.754E+07 1.564E+07 1.292E+07 7.001E+06

CM246 7.724E+04 7.723E+04 7.723E+04 7.722E+04 7.718E+04 7.713E+04 7.695E+04

0 PRINCIPAL PHOTON SOURCES IN GROUP 17,PHOTONS/SEC

MEAN ENERGY= 7.000MEV

NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

PU240 1.434E+04 1.434E+04 1.435E+04 1.435E+04 1.437E+04 1.440E+04 1.444E+04

CM242 2.396E+06 1.110E+06 5.114E+05 1.088E+05 1.475E+03 4.336E+02 4.025E+02

CM244 2.184E+06 2.143E+06 2.102E+06 2.023E+06 1.804E+06 1.490E+06 8.075E+05

CM246 8.922E+03 8.921E+03 8.920E+03 8.919E+03 8.915E+03 8.909E+03 8.888E+03

0 PRINCIPAL PHOTON SOURCES IN GROUP 18,PHOTONS/SEC

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MEAN ENERGY= 9.500MEV

NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

PU240 1.646E+03 1.647E+03 1.647E+03 1.648E+03 1.650E+03 1.653E+03 1.658E+03

CM242 2.765E+05 1.282E+05 5.903E+04 1.255E+04 1.703E+02 5.005E+01 4.646E+01

CM244 2.509E+05 2.462E+05 2.415E+05 2.325E+05 2.073E+05 1.712E+05 9.277E+04

CM246 1.027E+03 1.027E+03 1.026E+03 1.026E+03 1.026E+03 1.025E+03 1.023E+03

1 OUTPUT UNIT = 6 PAGE 64

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

PHOTON SPECTRUM FOR FISSION PRODUCTS

0 ST OF ORIGEN2 V2.1 - BWR FUEL ASSY - STANDARD BURNUP

(BWRU)

POWER= 1.00 MW, BURNUP= 1. MWD, FLUX= 1.00E+00

N/CM\*\*2-SEC

0 18 GROUP PHOTON RELEASE RATES, PHOTONS/SECOND

BASIS=MTIHM 4.5% UO2 FUEL ASSY; BURNUP=45,000 MWD/MTIHM,

4 CYCLE

EMEAN

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

1.000E-02 1.492E+18 2.750E+16 1.817E+16 9.842E+15 3.570E+15 2.501E+15 1.646E+15

2.500E-02 3.903E+17 6.185E+15 4.081E+15 2.243E+15 8.132E+14 5.336E+14 3.381E+14

3.750E-02 3.191E+17 6.341E+15 4.249E+15 2.348E+15 9.277E+14 6.552E+14 4.051E+14

5.750E-02 3.215E+17 5.651E+15 3.771E+15 2.022E+15 7.012E+14 4.830E+14 3.140E+14

8.500E-02 2.362E+17 3.946E+15 2.647E+15 1.400E+15 4.603E+14 3.014E+14 1.866E+14

1.250E-01 2.534E+17 4.969E+15 3.046E+15 1.549E+15 4.684E+14 2.879E+14 1.459E+14

2.250E-01 5.487E+17 3.414E+15 2.290E+15 1.204E+15 3.802E+14 2.495E+14 1.583E+14

3.750E-01 4.042E+17 1.810E+15 1.236E+15 6.625E+14 2.017E+14 1.125E+14 6.609E+13

5.750E-01 6.675E+17 1.811E+16 1.422E+16 1.072E+16 6.264E+15 4.259E+15 2.713E+15

8.500E-01 6.778E+17 1.876E+16 6.790E+15 3.485E+15 1.321E+15 3.391E+14 4.323E+13

1.250E+00 3.870E+17 1.060E+15 8.440E+14 5.868E+14 2.854E+14 1.471E+14 3.875E+13

1.750E+00 1.450E+17 8.769E+13 5.926E+13 3.141E+13 8.755E+12 4.297E+12 1.322E+12

2.250E+00 7.286E+16 1.420E+14 9.165E+13 3.857E+13 2.973E+12 4.841E+10 2.981E+07

2.750E+00 3.113E+16 2.367E+12 1.611E+12 8.030E+11 1.003E+11 3.180E+09 5.260E+04

3.500E+00 1.572E+16 2.842E+11 2.010E+11 1.011E+11 1.284E+10 4.125E+08 6.873E+03

5.000E+00 6.919E+15 7.916E-05 7.979E-05 8.082E-05 8.268E-05 8.381E-05 8.421E-05

7.000E+00 6.170E+13 5.137E-06 5.177E-06 5.244E-06 5.365E-06 5.438E-06 5.464E-06

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9.500E+00 1.302E+10 3.248E-07 3.274E-07 3.316E-07 3.392E-07 3.439E-07 3.455E-07  
0 TOTAL 5.969E+18 9.798E+16 6.150E+16 3.613E+16 1.540E+16 9.874E+15 6.056E+15  
0MEV/SEC 2.419E+18 3.156E+16 1.756E+16 1.120E+16 5.494E+15 3.180E+15 1.800E+15  
0 18 GROUP SPECIFIC ENERGY RELEASE RATES, MEV/WATT-SEC  
BASIS=MTIHM 4.5% UO2 FUEL ASSY;BURNUP=45,000 MWD/MTIHM,

4 CYCLE

EMEAN

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

1.000E-02 1.492E+10 2.750E+08 1.817E+08 9.842E+07 3.570E+07 2.501E+07 1.646E+07  
2.500E-02 9.758E+09 1.546E+08 1.020E+08 5.607E+07 2.033E+07 1.334E+07 8.452E+06  
3.750E-02 1.197E+10 2.378E+08 1.593E+08 8.804E+07 3.479E+07 2.457E+07 1.519E+07  
5.750E-02 1.849E+10 3.249E+08 2.168E+08 1.162E+08 4.032E+07 2.777E+07 1.806E+07  
8.500E-02 2.008E+10 3.354E+08 2.250E+08 1.190E+08 3.912E+07 2.562E+07 1.586E+07  
1.250E-01 3.168E+10 6.211E+08 3.807E+08 1.936E+08 5.854E+07 3.598E+07 1.824E+07  
2.250E-01 1.234E+11 7.682E+08 5.152E+08 2.708E+08 8.555E+07 5.614E+07 3.562E+07  
3.750E-01 1.516E+11 6.786E+08 4.634E+08 2.485E+08 7.565E+07 4.219E+07 2.478E+07  
5.750E-01 3.838E+11 1.042E+10 8.177E+09 6.165E+09 3.602E+09 2.449E+09 1.560E+09  
8.500E-01 5.761E+11 1.594E+10 5.772E+09 2.963E+09 1.123E+09 2.883E+08 3.675E+07  
1.250E+00 4.838E+11 1.326E+09 1.055E+09 7.336E+08 3.568E+08 1.839E+08 4.844E+07  
1.750E+00 2.538E+11 1.535E+08 1.037E+08 5.496E+07 1.532E+07 7.520E+06 2.314E+06  
2.250E+00 1.639E+11 3.194E+08 2.062E+08 8.679E+07 6.688E+06 1.089E+05 6.708E+01  
2.750E+00 8.560E+10 6.508E+06 4.429E+06 2.208E+06 2.759E+05 8.745E+03 1.447E-01  
3.500E+00 5.504E+10 9.946E+05 7.035E+05 3.537E+05 4.495E+04 1.444E+03 2.406E-02  
5.000E+00 3.460E+10 3.958E-10 3.989E-10 4.041E-10 4.134E-10 4.190E-10 4.211E-10  
7.000E+00 4.319E+08 3.596E-11 3.624E-11 3.671E-11 3.755E-11 3.807E-11 3.825E-11  
9.500E+00 1.237E+05 3.086E-12 3.110E-12 3.150E-12 3.223E-12 3.267E-12 3.282E-12  
0 TOTAL 2.419E+12 3.156E+10 1.756E+10 1.120E+10 5.494E+09 3.180E+09 1.800E+09  
0 GAM POW 3.878E+05 5.059E+03 2.815E+03 1.795E+03 8.806E+02 5.097E+02 2.885E+02

1 OUTPUT UNIT = 6 PAGE 65

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

0 PRINCIPAL PHOTON SOURCES IN GROUP 1,PHOTONS/SEC  
MEAN ENERGY= 0.010MEV

NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

KR 85 6.382E+13 6.180E+13 5.983E+13 5.609E+13 4.620E+13 3.344E+13 1.188E+13  
RB 88 1.980E+16 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

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KR 89	1.599E+16	0.000E+00										
SR 89	6.917E+15	5.641E+14	4.599E+13	3.057E+11	8.980E+04	1.166E-06	0.000E+00					
KR 90	1.630E+16	0.000E+00										
RB 90	2.197E+16	0.000E+00										
SR 90	4.181E+14	4.131E+14	4.082E+14	3.986E+14	3.712E+14	3.295E+14	2.252E+14					
Y 90	2.145E+15	2.041E+15	2.017E+15	1.969E+15	1.834E+15	1.628E+15	1.112E+15					
Y 91	9.077E+15	1.051E+15	1.208E+14	1.595E+12	3.673E+06	1.474E-03	0.000E+00					
RB 92	4.420E+16	0.000E+00										
Y 92	2.630E+16	0.000E+00										
Y 93	2.529E+16	0.000E+00										
RB 94	1.962E+16	0.000E+00										
Y 94	3.663E+16	0.000E+00										
ZR 95	2.309E+15	3.194E+14	4.416E+13	8.444E+11	5.903E+06	1.509E-02	0.000E+00					
Y 96	6.047E+16	0.000E+00										
ZR 97	1.728E+16	0.000E+00										
NB 98	4.982E+16	0.000E+00										
NB 99	4.019E+16	0.000E+00										
ZR101	3.911E+16	0.000E+00										
MO101	7.656E+16	0.000E+00										
TC102	3.850E+16	0.000E+00										
TC104	3.530E+16	0.000E+00										
RH104	1.744E+16	0.000E+00										
RH106	1.297E+16	8.444E+15	5.987E+15	3.010E+15	3.825E+14	1.229E+13	2.047E+08					
I134	2.078E+16	0.000E+00										
CS134	6.174E+14	5.219E+14	4.412E+14	3.152E+14	1.150E+14	2.141E+13	9.878E+10					
TE135	3.067E+16	0.000E+00										
I136	2.754E+16	0.000E+00										
I136M	1.727E+16	0.000E+00										
XE137	4.702E+16	0.000E+00										
CS137	4.943E+14	4.886E+14	4.830E+14	4.720E+14	4.404E+14	3.923E+14	2.711E+14					
I138	1.940E+16	0.000E+00										
XE138	1.770E+16	0.000E+00										
CS138	3.300E+16	0.000E+00										
XE139	3.330E+16	0.000E+00										
CS139	4.376E+16	0.000E+00										
BA139	2.418E+16	0.000E+00										
BA141	2.159E+16	0.000E+00										
LA141	2.331E+16	0.000E+00										
LA142	2.000E+16	0.000E+00										

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CE144	1.389E+15	8.900E+14	5.702E+14	2.340E+14	1.617E+13	1.883E+11	1.219E+05
PR144	1.878E+16	1.195E+16	7.652E+15	3.140E+15	2.171E+14	2.527E+12	1.636E+06
PM147	1.391E+14	1.274E+14	1.117E+14	8.575E+13	3.881E+13	1.036E+13	1.511E+11
EU154	9.937E+13	9.544E+13	9.167E+13	8.457E+13	6.641E+13	4.438E+13	1.222E+13

1 OUTPUT UNIT = 6 PAGE 66

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

0 PRINCIPAL PHOTON SOURCES IN GROUP 2,PHOTONS/SEC  
MEAN ENERGY= 0.025MEV

#### NUCLIDE

	ASSY	DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
KR 85	1.251E+13	1.211E+13	1.172E+13	1.099E+13	9.052E+12	6.551E+12	2.328E+12	
RB 88	4.439E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
SR 89	1.444E+15	1.178E+14	9.603E+12	6.384E+10	1.875E+04	2.434E-07	0.000E+00	
RB 90	4.903E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
SR 90	7.995E+13	7.900E+13	7.807E+13	7.623E+13	7.098E+13	6.301E+13	4.306E+13	
Y 90	4.610E+14	4.386E+14	4.334E+14	4.232E+14	3.941E+14	3.498E+14	2.390E+14	
Y 91	1.903E+15	2.204E+14	2.533E+13	3.344E+11	7.699E+05	3.090E-04	0.000E+00	
RB 92	1.006E+16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
Y 92	5.798E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
Y 93	5.488E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
RB 94	4.493E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
Y 94	8.132E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
Y 96	1.361E+16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
NB 98	1.104E+16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
NB 99	8.858E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
ZR101	8.825E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
TC102	8.505E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
RH103M	2.212E+15	8.825E+13	3.517E+12	5.587E+09	2.238E+01	2.265E-13	0.000E+00	
TC104	7.723E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
RH106	2.851E+15	1.856E+15	1.316E+15	6.617E+14	8.409E+13	2.701E+12	4.501E+07	
SB125	1.818E+14	1.616E+14	1.426E+14	1.110E+14	5.241E+13	1.500E+13	2.736E+11	
TE125M	9.742E+13	9.473E+13	8.458E+13	6.597E+13	3.114E+13	8.910E+12	1.626E+11	
SN130	4.869E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
TE131	4.687E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
SB132M	4.035E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
TE132	2.361E+16	3.160E-01	4.229E-18	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
TE134	1.279E+16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	

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I134 4.971E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
I134M 3.980E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CS134 1.170E+14 9.886E+13 8.357E+13 5.971E+13 2.178E+13 4.056E+12 1.871E+10  
TE135 6.873E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
I136 6.140E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
I136M 4.954E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
XE137 1.039E+16 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CS137 9.346E+13 9.239E+13 9.133E+13 8.924E+13 8.326E+13 7.418E+13 5.125E+13  
I138 4.421E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CS138 7.183E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
XE139 7.371E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CS139 9.691E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
BA139 5.127E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
BA140 8.968E+15 4.510E+11 2.268E+07 5.735E-02 0.000E+00 0.000E+00 0.000E+00  
BA141 4.597E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
LA141 4.991E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
LA142 4.285E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CE144 1.922E+14 1.231E+14 7.887E+13 3.237E+13 2.237E+12 2.604E+10 1.686E+04

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PR144 4.081E+15 2.595E+15 1.663E+15 6.823E+14 4.716E+13 5.491E+11 3.555E+05  
EU154 1.466E+13 1.408E+13 1.353E+13 1.248E+13 9.798E+12 6.548E+12 1.803E+12

0 PRINCIPAL PHOTON SOURCES IN GROUP 3,PHOTONS/SEC

MEAN ENERGY= 0.038MEV

#### NUCLIDE

	ASSY	DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
--	------	-----	-------	-------	-------	-------	--------	--------

SR 89	9.412E+14	7.676E+13	6.258E+12	4.160E+10	1.222E+04	1.586E-07	0.000E+00	
RB 90	3.336E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
SR 90	4.914E+13	4.856E+13	4.799E+13	4.686E+13	4.363E+13	3.873E+13	2.647E+13	
Y 90	3.055E+14	2.907E+14	2.873E+14	2.805E+14	2.612E+14	2.319E+14	1.584E+14	
Y 91	1.243E+15	1.439E+14	1.654E+13	2.184E+11	5.028E+05	2.018E-04	0.000E+00	
RB 92	6.901E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
Y 92	3.875E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
Y 93	3.659E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
Y 94	5.494E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
Y 96	9.298E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
NB 98	7.472E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	

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NB 99	5.978E+15	0.000E+00									
ZR101	6.038E+15	0.000E+00									
TC102	5.725E+15	0.000E+00									
TC104	5.172E+15	0.000E+00									
RH106	1.906E+15	1.241E+15	8.798E+14	4.423E+14	5.621E+13	1.806E+12	3.009E+07				
SB125	4.986E+13	4.432E+13	3.911E+13	3.045E+13	1.437E+13	4.113E+12	7.503E+10				
TE132	4.109E+15	5.500E-02	7.360E-19	0.000E+00							
XE133	2.056E+16	8.348E+05	2.759E-05	2.995E-26	0.000E+00						
CS134	1.163E+14	9.829E+13	8.308E+13	5.936E+13	2.165E+13	4.032E+12	1.860E+10				
TE135	4.676E+15	0.000E+00									
I136	4.176E+15	0.000E+00									
XE137	7.164E+15	0.000E+00									
CS137	5.698E+13	5.632E+13	5.567E+13	5.440E+13	5.076E+13	4.522E+13	3.125E+13				
BA137M	3.082E+14	3.043E+14	3.008E+14	2.939E+14	2.742E+14	2.443E+14	1.688E+14				
XE138	3.531E+15	0.000E+00									
CS138	4.820E+15	0.000E+00									
XE139	4.978E+15	0.000E+00									
CS139	6.534E+15	0.000E+00									
BA139	5.172E+15	0.000E+00									
BA141	5.459E+15	0.000E+00									
LA141	3.321E+15	0.000E+00									
CE141	7.117E+15	1.458E+14	2.970E+12	1.233E+09	8.814E-02	1.086E-18	0.000E+00				
BA142	8.169E+15	0.000E+00									
CE143	2.418E+16	0.000E+00									
CE144	2.805E+15	1.797E+15	1.151E+15	4.724E+14	3.265E+13	3.801E+11	2.461E+05				
PR144	2.721E+15	1.730E+15	1.108E+15	4.549E+14	3.144E+13	3.660E+11	2.370E+05				
CE145	1.460E+16	0.000E+00									
ND147	8.179E+15	8.759E+10	9.373E+05	1.073E-04	0.000E+00						
ND149	3.707E+15	0.000E+00									
SM153	7.902E+15	0.000E+00									
EU154	1.352E+14	1.299E+14	1.247E+14	1.151E+14	9.036E+13	6.039E+13	1.663E+13				
EU155	6.783E+13	6.325E+13	5.898E+13	5.129E+13	3.372E+13	1.677E+13	1.791E+12				

1

OUTPUT UNIT = 6

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ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

0

PRINCIPAL PHOTON SOURCES IN GROUP 4,PHOTONS/SEC  
MEAN ENERGY= 0.058MEV

NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

## Scientific Notebook #170-10e

James Weldy

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KR 85	1.044E+13	1.010E+13	9.783E+12	9.171E+12	7.554E+12	5.467E+12	1.943E+12
BR 88	3.333E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB 88	4.587E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
KR 89	3.502E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SR 89	1.346E+15	1.098E+14	8.950E+12	5.950E+10	1.748E+04	2.268E-07	0.000E+00
KR 90	3.220E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB 90	5.066E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SR 90	6.344E+13	6.269E+13	6.195E+13	6.050E+13	5.633E+13	5.001E+13	3.417E+13
Y 90	4.496E+14	4.277E+14	4.227E+14	4.127E+14	3.843E+14	3.412E+14	2.331E+14
Y 91	1.778E+15	2.059E+14	2.366E+13	3.125E+11	7.193E+05	2.887E-04	0.000E+00
RB 92	1.067E+16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Y 92	5.828E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Y 93	5.453E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB 94	4.801E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Y 94	8.278E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Y 96	1.425E+16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZR 97	3.456E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NB 98	1.134E+16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NB 99	8.945E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZR101	9.241E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TC102	8.588E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TC104	7.793E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RH104	3.629E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RH106	2.851E+15	1.856E+15	1.316E+15	6.617E+14	8.409E+13	2.701E+12	4.501E+07
SN130	4.234E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TE132	4.577E+15	6.127E-02	8.199E-19	0.000E+00	0.000E+00	0.000E+00	0.000E+00
I134	4.089E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CS134	9.316E+13	7.875E+13	6.656E+13	4.756E+13	1.735E+13	3.231E+12	1.490E+10
TE135	7.156E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
I136	6.320E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
I136M	3.990E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
XE137	1.061E+16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CS137	7.247E+13	7.164E+13	7.081E+13	6.920E+13	6.456E+13	5.752E+13	3.974E+13
I138	4.665E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
XE138	3.314E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CS138	7.137E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
XE139	7.532E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CS139	9.867E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00

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BA139	4.991E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BA141	4.433E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
LA141	4.867E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
LA142	4.166E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CE143	6.064E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CE144	1.615E+14	1.035E+14	6.629E+13	2.720E+13	1.880E+12	2.189E+10	1.417E+04
PR144	4.055E+15	2.579E+15	1.652E+15	6.780E+14	4.686E+13	5.455E+11	3.532E+05

1 OUTPUT UNIT = 6 PAGE 69

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

CE145	5.674E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
EU154	3.627E+13	3.484E+13	3.346E+13	3.087E+13	2.424E+13	1.620E+13	4.462E+12
EU155	2.045E+13	1.907E+13	1.778E+13	1.546E+13	1.016E+13	5.054E+12	5.400E+11

0 PRINCIPAL PHOTON SOURCES IN GROUP 5,PHOTONS/SEC

MEAN ENERGY= 0.085MEV

## NUCLIDE

	ASSY	DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
--	------	-----	-------	-------	-------	-------	--------	--------

RB 88	3.003E+15	0.000E+00						
SR 89	8.056E+14	6.570E+13	5.357E+12	3.561E+10	1.046E+04	1.358E-07	0.000E+00	0.000E+00
RB 90	3.316E+15	0.000E+00						
SR 90	3.224E+13	3.185E+13	3.148E+13	3.074E+13	2.862E+13	2.541E+13	1.736E+13	
Y 90	2.793E+14	2.657E+14	2.626E+14	2.564E+14	2.387E+14	2.119E+14	1.448E+14	
Y 91	1.068E+15	1.237E+14	1.421E+13	1.876E+11	4.320E+05	1.734E-04	0.000E+00	
RB 92	7.149E+15	0.000E+00						
Y 92	3.753E+15	0.000E+00						
Y 93	3.447E+15	0.000E+00						
RB 94	3.237E+15	0.000E+00						
Y 94	5.348E+15	0.000E+00						
Y 96	9.449E+15	0.000E+00						
NB 98	7.386E+15	0.000E+00						
NB 99	5.760E+15	0.000E+00						
ZR101	6.136E+15	0.000E+00						
MO101	3.145E+15	0.000E+00						
TC102	5.518E+15	0.000E+00						
TC104	5.032E+15	0.000E+00						
RH106	1.828E+15	1.190E+15	8.441E+14	4.244E+14	5.393E+13	1.732E+12	2.886E+07	
TE133M	2.567E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
XE133	1.840E+16	7.471E+05	2.469E-05	2.680E-26	0.000E+00	0.000E+00	0.000E+00	

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TE134 8.707E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
I134 2.466E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CS134 4.801E+13 4.058E+13 3.430E+13 2.451E+13 8.940E+12 1.665E+12 7.680E+09  
TE135 4.720E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
I136 4.153E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
I136M 2.611E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
XE137 6.896E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CS137 3.613E+13 3.572E+13 3.531E+13 3.450E+13 3.219E+13 2.868E+13 1.982E+13  
I138 3.117E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CS138 4.519E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
XE139 4.946E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CS139 6.402E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
BA139 3.090E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
BA141 2.754E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
LA141 3.040E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
BA142 5.304E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
LA142 2.595E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CE144 6.440E+14 4.126E+14 2.643E+14 1.085E+14 7.497E+12 8.728E+10 5.651E+04  
PR144 2.572E+15 1.635E+15 1.048E+15 4.300E+14 2.972E+13 3.460E+11 2.240E+05  
ND147 5.180E+15 5.548E+10 5.937E+05 6.798E-05 0.000E+00 0.000E+00 0.000E+00  
EU154 6.950E+12 6.676E+12 6.412E+12 5.916E+12 4.645E+12 3.104E+12 8.549E+11

1 OUTPUT UNIT = 6 PAGE 70

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

EU155 1.021E+14 9.518E+13 8.876E+13 7.718E+13 5.074E+13 2.523E+13 2.696E+12

0 PRINCIPAL PHOTON SOURCES IN GROUP 6,PHOTONS/SEC

MEAN ENERGY= 0.125MEV

#### NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

KR 90 8.177E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SR 90 1.716E+13 1.696E+13 1.676E+13 1.637E+13 1.524E+13 1.353E+13 9.243E+12  
Y 90 1.871E+14 1.780E+14 1.759E+14 1.717E+14 1.599E+14 1.420E+14 9.700E+13  
Y 91 6.877E+14 7.965E+13 9.152E+12 1.208E+11 2.782E+05 1.117E-04 0.000E+00  
KR 92 3.779E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
RB 92 5.142E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
Y 92 2.591E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
Y 94 3.736E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
Y 96 6.728E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

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NB 98 5.196E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
NB 99 3.988E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
MO 99 3.338E+15 3.408E-05 3.477E-25 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
TC 99M 4.152E+16 4.663E-04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
ZR101 4.376E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
TC102 3.833E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
TC104 3.565E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
RH106 1.261E+15 8.212E+14 5.823E+14 2.927E+14 3.720E+13 1.195E+12 1.991E+07  
TE131 1.935E+16 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SB132M 2.983E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
I134 4.314E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CS134 2.618E+13 2.213E+13 1.871E+13 1.337E+13 4.875E+12 9.079E+11 4.188E+09  
TE135 3.328E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
I136 2.912E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
XE137 4.791E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CS137 1.894E+13 1.872E+13 1.851E+13 1.809E+13 1.688E+13 1.503E+13 1.039E+13  
CS138 3.898E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
XE139 3.621E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CS139 4.429E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CE141 2.256E+16 4.621E+14 9.415E+12 3.908E+09 2.794E-01 3.441E-18 0.000E+00  
CE144 3.012E+15 1.930E+15 1.236E+15 5.074E+14 3.507E+13 4.083E+11 2.643E+05  
PR144 1.755E+15 1.116E+15 7.151E+14 2.935E+14 2.029E+13 2.362E+11 1.529E+05  
SM153 3.442E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
EU154 2.210E+14 2.123E+14 2.039E+14 1.881E+14 1.477E+14 9.871E+13 2.718E+13  
EU155 5.620E+13 5.241E+13 4.887E+13 4.250E+13 2.794E+13 1.389E+13 1.484E+12

1

OUTPUT UNIT = 6

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ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

0 PRINCIPAL PHOTON SOURCES IN GROUP 7,PHOTONS/SEC  
MEAN ENERGY= 0.225MEV

NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

KR 89 6.711E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
SR 89 6.642E+14 5.416E+13 4.416E+12 2.936E+10 8.623E+03 1.119E-07 0.000E+00  
SR 90 1.357E+13 1.341E+13 1.325E+13 1.294E+13 1.205E+13 1.070E+13 7.308E+12  
Y 90 2.633E+14 2.505E+14 2.475E+14 2.417E+14 2.250E+14 1.998E+14 1.365E+14  
Y 91 8.902E+14 1.031E+14 1.185E+13 1.564E+11 3.602E+05 1.446E-04 0.000E+00  
RB 92 8.367E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

Scientific Notebook #170-10e

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Y 93 6.313E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
Y 94 5.714E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
Y 96 1.077E+16 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
NB 98 8.031E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
NB 99 6.022E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
ZR101 3.887E+16 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
MO101 9.516E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
TC102 5.808E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
TC104 7.444E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
RH106 1.875E+15 1.221E+15 8.655E+14 4.351E+14 5.530E+13 1.776E+12 2.960E+07  
SB125 2.613E+13 2.323E+13 2.050E+13 1.596E+13 7.533E+12 2.156E+12 3.933E+10  
SN130 7.715E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
TE132 3.222E+16 4.313E-01 5.772E-18 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
TE133M 6.711E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
TE134 2.992E+16 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
I134M 5.589E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CS134 2.400E+13 2.029E+13 1.715E+13 1.225E+13 4.470E+12 8.324E+11 3.840E+09  
TE135 8.418E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
XE135 1.410E+16 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
I136M 1.126E+16 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
XE137 7.433E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CS137 1.504E+13 1.487E+13 1.470E+13 1.436E+13 1.340E+13 1.194E+13 8.250E+12  
XE138 2.040E+16 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CS138 5.608E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
XE139 4.073E+16 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CS139 6.841E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
BA139 1.025E+16 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
BA141 3.070E+16 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
BA142 1.649E+16 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CE143 2.293E+16 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
PR144 2.564E+15 1.630E+15 1.044E+15 4.286E+14 2.963E+13 3.449E+11 2.233E+05  
ND149 6.811E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
EU154 4.567E+13 4.386E+13 4.213E+13 3.887E+13 3.052E+13 2.040E+13 5.617E+12

1

OUTPUT UNIT = 6

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ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

0

PRINCIPAL PHOTON SOURCES IN GROUP 8,PHOTONS/SEC  
MEAN ENERGY= 0.375MEV

NUCLIDE

Scientific Notebook #170-10e

James Weldy

12/27/00

20-1402-762

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

KR 87	6.807E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SR 89	2.535E+14	2.067E+13	1.685E+12	1.120E+10	3.291E+03	4.272E-08	0.000E+00
SR 90	1.339E+12	1.323E+12	1.307E+12	1.276E+12	1.188E+12	1.055E+12	7.209E+11
Y 90	1.212E+14	1.153E+14	1.139E+14	1.112E+14	1.036E+14	9.194E+13	6.282E+13
Y 91	3.476E+14	4.026E+13	4.626E+12	6.108E+10	1.406E+05	5.645E-05	0.000E+00
RB 92	5.029E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Y 96	6.198E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NB 98	4.423E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZR101	7.945E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TC101	3.167E+16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TC104	3.365E+16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RU105	6.160E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RH105	5.683E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RH106	9.978E+14	6.497E+14	4.607E+14	2.316E+14	2.943E+13	9.454E+11	1.575E+07
RH107	1.459E+16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RH108	7.259E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SB125	1.552E+14	1.379E+14	1.217E+14	9.476E+13	4.473E+13	1.280E+13	2.335E+11
I131	2.024E+16	3.033E+09	4.412E+02	9.331E-12	0.000E+00	0.000E+00	0.000E+00
TE133	2.852E+16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TE134	9.161E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
I134	8.876E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
I136M	1.740E+16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CS137	2.254E+12	2.228E+12	2.203E+12	2.152E+12	2.008E+12	1.789E+12	1.236E+12
XE138	1.462E+16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CS138	5.144E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
XE139	5.496E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
LA140	9.459E+15	5.240E+11	2.635E+07	6.664E-02	0.000E+00	0.000E+00	0.000E+00
BA141	1.589E+16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BA142	7.123E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
PR144	1.266E+15	8.052E+14	5.158E+14	2.117E+14	1.463E+13	1.704E+11	1.103E+05
CE145	5.622E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CE146	5.550E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
PR148	1.069E+16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
EU154	7.276E+12	6.989E+12	6.713E+12	6.193E+12	4.863E+12	3.250E+12	8.950E+11

0 PRINCIPAL PHOTON SOURCES IN GROUP 9,PHOTONS/SEC

MEAN ENERGY= 0.575MEV



## Scientific Notebook #170-10e

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12/27/00

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## NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

1

**OUTPUT UNIT = 6**

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ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

SB132	1.842E+16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SB132M	1.002E+16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
I132	3.995E+16	5.418E-01	7.250E-18	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TE133M	3.117E+16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TE134	1.964E+16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
I134	1.056E+17	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CS134	5.997E+15	5.070E+15	4.285E+15	3.062E+15	1.117E+15	2.080E+14	9.595E+11
LA140	1.901E+16	1.053E+12	5.296E+07	1.339E-01	0.000E+00	0.000E+00	0.000E+00
BA142	1.158E+16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
PR144	2.773E+14	1.764E+14	1.130E+14	4.636E+13	3.205E+12	3.731E+10	2.416E+04
CE145	1.653E+16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
EU154	2.585E+14	2.483E+14	2.385E+14	2.200E+14	1.727E+14	1.154E+14	3.179E+13

1

## PRINCIPAL PHOTON SOURCES IN GROUP II PHOTONS/SEC

MEAN ENERGY = 1.250 MEV

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NUCLIDE

	ASSY	DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
KR 89	4.852E+15	0.000E+00						
RB 89	1.941E+16	0.000E+00						
KR 90	7.868E+15	0.000E+00						
Y 90	6.591E+12	6.271E+12	6.197E+12	6.051E+12	5.634E+12	5.002E+12	3.418E+12	
SR 91	8.334E+15	0.000E+00						
SR 92	3.098E+16	0.000E+00						
Y 94	5.494E+15	0.000E+00						
MO101	1.574E+16	0.000E+00						
TC102	4.771E+15	0.000E+00						
TC104	7.059E+15	0.000E+00						
RH106	3.966E+14	2.583E+14	1.831E+14	9.206E+13	1.170E+13	3.758E+11	6.262E+06	
AG110M	4.319E+13	2.603E+13	1.568E+13	5.694E+12	2.725E+11	1.719E+09	1.568E+02	
SB130M	5.834E+15	0.000E+00						
SB131	5.541E+15	0.000E+00						
I132	8.576E+15	1.163E-01	1.556E-18	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TE133	6.876E+15	0.000E+00						
I134	1.792E+16	0.000E+00						
CS134	3.964E+14	3.351E+14	2.833E+14	2.024E+14	7.383E+13	1.375E+13	6.342E+10	
I135	3.554E+16	0.000E+00						
I136	2.280E+16	0.000E+00						
I136M	1.446E+16	0.000E+00						
CS138	5.422E+16	0.000E+00						
XE139	3.944E+15	0.000E+00						
CS139	4.955E+15	0.000E+00						
BA141	5.747E+15	0.000E+00						
BA142	1.827E+16	0.000E+00						
LA142	7.182E+15	0.000E+00						
PR144	2.203E+14	1.401E+14	8.974E+13	3.683E+13	2.546E+12	2.964E+10	1.919E+04	
EU154	2.862E+14	2.749E+14	2.640E+14	2.436E+14	1.912E+14	1.278E+14	3.520E+13	

1

OUTPUT UNIT = 6

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ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

0

PRINCIPAL PHOTON SOURCES IN GROUP 12,PHOTONS/SEC  
MEAN ENERGY= 1.750MEV

NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

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KR 88	2.106E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB 88	3.960E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
KR 89	4.011E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
KR 90	3.741E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Y 90	5.143E+11	4.894E+11	4.836E+11	4.722E+11	4.397E+11	3.903E+11	2.667E+11
Y 94	2.513E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
MO101	5.666E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TC104	9.820E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RH106	7.390E+13	4.812E+13	3.412E+13	1.715E+13	2.180E+12	7.002E+10	1.167E+06
AG110M	1.668E+13	1.005E+13	6.058E+12	2.199E+12	1.053E+11	6.641E+08	6.055E+01
SB124	1.774E+13	2.166E+12	2.644E+11	3.943E+09	1.307E+04	9.628E-06	0.000E+00
SB131	3.666E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SB132	1.522E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TE133	1.847E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TE133M	2.035E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
I134	8.089E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
I135	1.159E+16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
XE138	8.328E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
XE139	2.564E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CS139	1.456E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
LA140	3.985E+16	2.208E+12	1.110E+08	2.807E-01	0.000E+00	0.000E+00	0.000E+00
BA141	2.003E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
LA142	8.729E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
PR144	2.556E+13	1.625E+13	1.041E+13	4.273E+12	2.954E+11	3.439E+09	2.226E+03
EU154	8.579E+12	8.240E+12	7.915E+12	7.302E+12	5.734E+12	3.832E+12	1.055E+12
0	PRINCIPAL PHOTON SOURCES IN GROUP 13,PHOTONS/SEC						
	MEAN ENERGY= 2.250MEV						

#### NUCLIDE

	ASSY	DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
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KR 88	9.996E+15	0.000E+00						
KR 89	1.152E+15	0.000E+00						
RB 89	3.308E+15	0.000E+00						
Y 90	5.677E+07	5.401E+07	5.337E+07	5.212E+07	4.852E+07	4.308E+07	2.944E+07	
Y 94	9.121E+14	0.000E+00						
MO101	3.824E+15	0.000E+00						
TC104	2.607E+15	0.000E+00						

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RH106 2.278E+13 1.483E+13 1.051E+13 5.286E+12 6.718E+11 2.158E+10 3.596E+05  
SB131 1.766E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
TE133M 1.216E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
I135 1.255E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
I136 4.289E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
XE138 8.619E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
CS138 7.276E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
XE139 1.691E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

1 OUTPUT UNIT = 6 PAGE 76

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

CS139 1.088E+15 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
LA142 1.409E+16 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00  
PR144 1.991E+14 1.266E+14 8.111E+13 3.329E+13 2.301E+12 2.678E+10 1.734E+04  
EU156 1.069E+15 2.569E+11 6.157E+07 3.537E+00 0.000E+00 0.000E+00 0.000E+00

0 PRINCIPAL PHOTON SOURCES IN GROUP 14,PHOTONS/SEC  
MEAN ENERGY= 2.750MEV

#### NUCLIDE

	ASSY	DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
KR 87	1.465E+15	0.000E+00						
BR 88	7.784E+14	0.000E+00						
RB 88	3.878E+14	0.000E+00						
KR 89	1.100E+15	0.000E+00						
RB 89	2.381E+15	0.000E+00						
RB 90M	8.013E+14	0.000E+00						
RB 92	4.037E+14	0.000E+00						
Y 94	4.945E+14	0.000E+00						
NB 99M	3.286E+14	0.000E+00						
TC104	2.321E+15	0.000E+00						
RH106	3.331E+12	2.169E+12	1.538E+12	7.732E+11	9.826E+10	3.156E+09	5.259E+04	
SB132M	3.188E+14	0.000E+00						
I136	2.641E+15	0.000E+00						
CS138	3.633E+15	0.000E+00						
XE139	9.536E+14	0.000E+00						
CS139	5.350E+14	0.000E+00						
LA140	1.517E+15	8.405E+10	4.227E+06	1.069E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00
LA142	8.491E+15	0.000E+00						
PR144	1.784E+11	1.135E+11	7.269E+10	2.983E+10	2.062E+09	2.400E+07	1.554E+01	

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James Weldy

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0 PRINCIPAL PHOTON SOURCES IN GROUP 15,PHOTONS/SEC  
MEAN ENERGY= 3.500MEV

NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

BR 84	7.388E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BR 88	1.240E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
KR 89	1.880E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB 89	2.971E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB 90	3.621E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB 90M	1.160E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB 92	3.067E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB 94	1.853E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
TC104	1.241E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RH106	4.354E+11	2.835E+11	2.010E+11	1.011E+11	1.284E+10	4.125E+08	6.873E+03
I136	4.627E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CS138	2.410E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
XE139	2.066E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CS139	2.921E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
LA142	3.067E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00

1 OUTPUT UNIT = 6 PAGE 77

ORIGEN2 V2.1 (8-1-91), Run on Aug 20 1999 at 10:07:12

0 PRINCIPAL PHOTON SOURCES IN GROUP 16,PHOTONS/SEC  
MEAN ENERGY= 5.000MEV

NUCLIDE

ASSY DIS 0.5YR 1.0YR 2.0YR 5.0YR 10.0YR 26.0YR

BR 88	1.524E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
KR 89	1.387E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB 90	4.191E+15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB 90M	1.844E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB 92	7.352E+14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CE142	7.198E-05	7.198E-05	7.198E-05	7.198E-05	7.198E-05	7.198E-05
SM147	6.466E-06	7.180E-06	7.805E-06	8.833E-06	1.069E-05	1.182E-05

0 PRINCIPAL PHOTON SOURCES IN GROUP 17,PHOTONS/SEC  
MEAN ENERGY= 7.000MEV

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NUCLIDE

	ASSY	DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
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RB 92	5.796E+13	0.000E+00						
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RB 94	3.607E+12	0.000E+00						
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CE142	4.670E-06							
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SM147	4.196E-07	4.659E-07	5.065E-07	5.732E-07	6.939E-07	7.671E-07	7.934E-07	
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0 PRINCIPAL PHOTON SOURCES IN GROUP 18,PHOTONS/SEC

MEAN ENERGY= 9.500MEV

NUCLIDE

	ASSY	DIS	0.5YR	1.0YR	2.0YR	5.0YR	10.0YR	26.0YR
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RB 94	1.302E+10	0.000E+00						
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CE142	2.953E-07							
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SM147	2.653E-08	2.946E-08	3.203E-08	3.624E-08	4.388E-08	4.851E-08	5.017E-08	
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Scientific Notebook #170

Issued to: S. Mohanty

Issue Date: Apr. 3, 1996

Account Number: 20-01402-762

Title: DCAGS

Participants: J. Weldy

12/27/00 - Modifications to Module DCAGS

The DCAGS Module was modified to account for a time-dependent mass-loading factor, which decreases exponentially following a volcanic event.

This modification is made for both critical groups and both the current and pluvial biospheres.

Modifications made:

added line 150: dimension tmassload(maxntime)

replaced line 166: name = 'AirborneMassLoadForVolcanismDoseCalculation[g/m3]'

with lines 171: name = 'AirborneMassLoadAboveFreshAshBlanket[g/m3]'

added lines 187-195: call clearchar( 60, name )

name = 'AirborneMassLoadAboveSoil[g/m3]'

isoilmassload = ispquery( name )

call clearchar( 60, name )

name = 'RateOfReductionOfMassLoadingFactor[1/yr]'

ireductionrate = ispquery( name )

added lines 274, 275: soilmassload=valuesp( isoilmassload )

reductionrate=valuesp( ireductionrate )

added lines 305, 306: tmassload(it)=(dmassload-soilmassload)\*exp(-reductionrate

& \*(tim(it)-tim(itee))+soilmassload

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replaced lines 449-450, 499-500, 553-554, and 599-600 (all identical lines):

```
dcf(it,k)=dcfde(k)+dcfinh(k)/(gramsashpercm2*1.d+04)*dmassload  
& *occupancy*resuspendablefraction(it)+dcfinga(k)+dcfingp(k)
```

with lines 479-481, 533-535, 590-592, and 639-641 (all identical lines):

```
dcf(it,k)=dcfde(k)+dcfinh(k)/(gramsashpercm2*1.d+04)  
& *tmassload(it)*occupancy*resuspendablefraction(it)  
& +dcfinga(k)+dcfingp(k)
```

New Parameters and Justification for Initial Values:

1. AirborneMassLoadAboveFreshAshBlanket[g/m3]: this parameter is identical to the AirborneMassLoadForVolcanismDoseCalculation[g/m3] parameter in TPA 3.3 and represents the mass load in the year following the volcanic eruption. The range of a loguniform distribution from  $10^{-4}$  to  $10^{-2}$  is kept based on literature search and result of experiments above the Cerro Negro ash blanket.
2. AirborneMassLoadAboveSoil[g/m3]: this parameter represents the mass load above the ash blanket at very long times after the event so that the ash material is essentially soil and is set to a value of  $10^{-4}$  to be consistent with the parameter used to calculate the DCFs in the GENII Code and based on data in Anspaugh, 1975.

Anspaugh, L.R., J.H. Shinn, P.L. Phelps, and N.C. Kennedy. 1975. Resuspension and Redistribution of Plutonium in Soils. *Health Physics*. Vol. 29, pp. 571-582.

3. RateOfReductionOfMassLoadingFactor[1/yr]: this parameter specifies how quickly the mass loading factor drops and is set to a value of  $2e-2$ , which was calculated by fitting a curve to two points, a mass load of  $1e-3$  in the year of the event and a mass load of  $1e-4$  at 1000 years after the event.

Tests:

1. Set the decrease rate of the mass loading factor to essentially zero. This should cause the results to be identical to the results running TPA 3.3.

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Title: DCAGW

Participants: J. Weldy

2/7/00 - Modifications to Module DCAGW

Objectives:

1) The DCAGW Module was modified to use a different well pumping rate under pluvial conditions. This is done in the calculations of the DCFs, so to be consistent, it should be done to determine the concentration of RNs in the groundwater. Per discussions with R. Fedors and D. Farrell, implementation should only be done for the 20 km receptor group, as the 10 km receptor group uses most of their water for personal uses, not irrigation of crops, so the pumping rate will not change much under pluvial conditions. Additionally, changing the pumping rate does not affect any other parameters used in the TPA code.

2) Allow the user to specify the time at which pluvial conditions occur. This change is being implemented to replace the current methodology of determining when pluvial conditions occur of using the current precipitation and temperature values and switch to pluvial conditions when the climate state switches from arid to semi-arid. This method was leading to a change to pluvial conditions much too early, when conditions were not consistent with the rainfall and temperature assumptions used to derive the pluvial pumping rates and DCFs.

3) Add the calculation of the leach factor from Kd values to the TPA code prior to running the GENII code. This change will give the user more control to modify these values to determine the sensitivity they have on the results. Currently, the leach rate is specified as a default value in the file gftrans.dat. This modification will cause this value to be changes for the TPA radionuclides when the data is transferred to the file gftrans.inp.

Modifications made:

Added two new parameters and got their values with the function valuesp. The two new parameters

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are PluvialWellPumpingRateAtReceptorGroup20km[gal/day] and PluvialSwitchTime[yr].

Convert pluvial pump rate to m<sup>3</sup>/yr by multiplying by (365.25 day/yr) \* (1 m<sup>3</sup>/264.172 gal).

Replace pluvial cutoff time determination with a set time. Add parameter to remember the dKG value at the cutoff time so the code can return to current conditions when the temperature and rainfall return to current values. The pump rate should be a pluvial pump rate when the time is greater than the switch time, the dKG value is smaller than the value at the switch time, and the receptor group is specified as the 20 km group. Otherwise, the pump rate should be the current conditions pump rate.

For the calculations of the leach rate, insert the calculation in the subroutine gentpa between the lines where the values from the file gftrans.dat are read and where they are written to the file gftrans.inp. The formula that should be used to calculate the leach rate is the formula from Baes and Sharp (1981):

$$\lambda_{leach} = \frac{P + I - E}{d(1 + \frac{\rho}{\theta} K_d)}$$

where,

P = Annual precipitation [m/yr]

I = Irrigation rate [m/yr]

E = Annual evapotranspiration rate [m/yr]

d = Depth of rooting zone [m]

$\rho$  = Density of soil [g/cm<sup>3</sup>]

$\theta$  = Soil volumetric water content [mL/cm<sup>3</sup>] or []

K<sub>d</sub> = Distribution coefficient [cm<sup>3</sup>/g]

New Parameters and Justification for Initial Values:

1. PluvialWellPumpingRateAtReceptorGroup20km. Laplante et al., 1997 states that the irrigation rate at Blackfoot ID (which was determined to be an analog to pluvial conditions at Amargosa Valley) is about 71% of the current irrigation rate at Amargosa Valley. Therefore, multiply the range of current pumping rates by 0.71 to get a range of 3.2e6 to 9.23e6. Note that this should be strongly correlated to the current pump rate and to the irrigation rate (pluvial) used for GENII, if this parameter is sampled.

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2. PluvialSwitchTime: The current climato2.dat file reaches 50% of full pluvial conditions at about 13,000 years. This seems like a logical initial value for the parameter..
3. KD values for radionuclides in soil. These values were taken from Sheppard and Thibault (1990) for a sandy soil. Note that Sheppard and Thibault does not list a Kd for Cl-36, so this parameter was taken from the UZ and SZ retardation in the mountain and given a Kd of 0.
4. Current precipitation rate. 0.085 m/yr at Amargosa Valley (from Wilson et. al., 1993). More current AMRs indicate similar rates (0.09-0.1 m/yr).
5. Current irrigation rate. 1.52 m/yr at Amargosa Valley (Laplante et al., 1997).
6. Current evapotranspiration rate. 0.8 m/yr (Laplante, et al., 1997).
7. Depth of the rooting zone. 0.15 m (LaPlante et al., 1997).
8. Density of surface soil. 1.5 g/cm<sup>3</sup> (LaPlante et al., 1997).
9. Soil volumetric water content. 0.35 (Laplante et al., 1997).

Tests:

1. Check that the code switches to pluvial conditions at the time set by the user.
2. Change the Pluvial Switch Time to a time beyond the end of the calculational period and ensure that the code does not switch to pluvial conditions.
3. Set the pluvial pump rate to a very small value and ensure that the doses become much larger when pluvial conditions are reached.
4. For base case, confirm that all values calculated in the code are identical to those values in gftrans.def. The one exception to this is for Cl-36, which is somewhat different due to different assumptions in the retardation factor for Cl-36 between here and Laplante, 1997.
5. Change the Kds for all RNs in the TPA code to a unique value and make sure that this change shows up for all of the TPA RNs in the gftrans.inp file.

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Definition of Mass Loading Parameters for DCAGS modified for version 5.0

Objective:

Three parameters have to be defined for the implementation of DCAGS in TPA:

AirborneMassLoadAboveFreshAshBlanket[g/m<sup>3</sup>], AirborneMassLoadAboveSoil[g/m<sup>3</sup>], and RateOfReductionOfMassLoad[1/yr].

AirborneMassLoadAboveFreshAshBlanket[g/m<sup>3</sup>] - Calculated based on an **initial** value for plowing between **0.1 and 0.2 g/m<sup>3</sup>** (1-2 times the value humans can barely tolerate (Stewart, 1964)). The initial value decays with a **half-life of 140 days in the first year** (Data from thin film deposits, such as Chernobyl, would support a decay by a factor of 100 in the first year. See also Anspaugh (1975) which cites Langham (1969) and Kathren (1968)] for half-lives of 35 and 45 days, respectively). This is somewhat longer than the value for thin film deposits due to the thicker deposits associated with the tephra deposit, and is consistent with data from Yakima, WA following the Mt. St. Helens eruption presented at the Igneous Activity Issue Closure Technical Exchange, which indicates a drop in the mass load in the months following the event with a half-life of about 140 days). For the very high mass loads encountered in early years following deposition, consideration needs to be taken for the time that plowing/activity that would create the very dusty conditions is occurring. It seems realistic to assume that farmers plow their fields for 1 to 3 work weeks of dusty conditions (40 to 120 hours per year). To have very dusty conditions requires not only high winds or aggressive physical activity such as plowing, but a dry soil. If they can avoid it, farmers do not typically plow during very windy and dry conditions, because they do not want to lose their soils from the farming areas. Therefore, the values calculated by a model such as that given above need to multiplied by a plowing time factor.

Plowing Time Factor = 0.0046 - 0.0137.

The rest of the time that people are exposed to the airborne radionuclides outdoors, it is assumed that they are walking over the ash blanket. All other time, it is assumed that they are exposed to indoor air concentrations, which is between 0.2 and 0.7 times the undisturbed outdoor concentration (NUREG/CR-5512). Data from Nicaragua indicates that the mass load over a surface being disturbed by an individual walking on it is about an order of magnitude smaller than the mass load over a surface that is being heavily disturbed and the undisturbed mass load is about an order of magnitude below that.

Performing the integration (the average concentration of a decaying exponential function with a lambda of 1.8/yr over one year is 0.464 times the initial value) and weighting for the fraction of the year that plowing occurs yields the following first year range:

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Min: 1.21E-3

Max: 3.64E-3

A lognormal distribution may be assumed.

Activity	Fraction of Year	Average Mass Load (g/m <sup>3</sup> )
Plowing	0.0046 - 0.0137	4.64e-2 – 9.28e-2
Walking Outside	0.2	4.64e-3 – 9.28e-3
Indoors	0.55	9.28e-5 – 6.5e-4
Offsite (since tephra deposit is widely distributed, assume that receptor is still exposed to ash while offsite. Assume receptor works or spends time indoors while offsite.)	0.236 – 0.245	9.28e-5 – 6.5e-4

Note that corrections for exposure times in the code would have to be divided back out of this range since it is already weighted for occupancy time. Since the current value for the occupancy factor in the TPA Code is 0.605, this range needs to be divided by 0.605 to ensure that the code is using the proper value. This results in the following range which should be used as the input distribution for the mass loading value in the TPA Code:

### Lognormal Distribution

Min: 2.0E-3 g/m<sup>3</sup>

Max: 6.0E-3 g/m<sup>3</sup>

RateOfReductionOfMassLoad[1/yr] - A long-term **half-life of 10 yr** starting at year 1 (lambda = 0.0693). Chernobyl data would easily support a half-life of 1.0 yr or less. Sehmel and Orgill (1974) and NRC (1975) also would support a half-life on the order of 1.0 yr. However, there is significantly more material released in a volcanic event than the studies on which this data is based, with the potential for replacement of fine material due to fluvial redistribution or deposition from other areas. Therefore, assume an order of magnitude longer half-life to account for this.

Note that Nicaragua data would indicate that for a range of plowing times of 1-3 weeks and

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similar behaviors as assumed for the critical group for Yucca Mountain, the average mass load would be between 2.9E-4 and 4.4E-4 g/m<sup>3</sup>. Decaying our initial range (before dividing by the 0.605 occupancy factor) by the 6 year age of the ash blanket yields a range from 2.8e-4 to 8.3e-4 g/m<sup>3</sup>. Considering that Nicaragua is a much wetter environment than the Yucca Mountain environment, this provides confidence that these values are credible.

AirborneMassLoadAboveSoil[g/m3] - From the list of references for mass loads originally compiled by B. Eid, 5 references were selected as appearing to be applicable to the Amargosa Valley region. These references are listed in the following table, along with justification as to why they are applicable and the range of mass loading values reported:

Reference	Justification for applicability	Min Mass Load Reported (g/m3)	Max Mass Load Reported (g/m3)
Sehmel (1977)	Data collected at the Hanford Site, which is an arid climate with sparse vegetation, similar to the Amargosa Valley region. Includes information on level of disturbance, particle size distribution, and height of measurements.	2.8e-5	0.23
Tegen and Fung (1994)	Data collected in areas of high dust loading such as deserts and eroding cultivated areas.	1e-4	1e-4
Anspaugh (1975)	Data collected in Nevada on the Nevada Test Site. Information on measurement height and level of disturbance, but particle size distribution is unknown.	1e-4	5e-3
Rognon (1991)	Data collected in a desert region, which would likely have soil similar to the Amargosa Valley region.	1.6e-6	1.3e-5
Soldat (1973)	Data collected for Retrievable Surface Storage Facility in Hanford, WA which has similar soil characteristics to Amargosa Valley.	1e-4	1e-4

The Sehmel (1977) paper was investigated to determine why the high value was so much higher than the other sources. Investigation revealed that the maximum value in Table 6 included

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particle sizes up to 230 microns and were measured at a height of only 30 cm. Particles above 100 microns are not inhalable by human beings and therefore should not be included in the mass load value used to determine dose to humans. Additionally, human breathe air at a height of almost 2 m, so the mass load at 30 cm is not what will be inhaled by people. Sehmel (1977) divided the measurements by particle size, and the maximum concentration of dust in the air smaller than 100 microns was 4.51e-2 g/m<sup>3</sup> at 30 cm. The minimum concentration of dust in the air smaller than 100 microns was 2.6e-5 g/m<sup>3</sup>. Investigation of Figure 10 showed that the maximum concentration at 30 cm ranged from between 4 and 6 times the maximum concentration at 2 m. Therefore, the maximum concentration was divided by a factor of 4 to yield a value of 1.13e-2 g/m<sup>3</sup>.

To determine a range from these varying estimates of mass load, each of the references was assigned a median value based on assuming that the distribution of estimates within a reference is log-uniform. Therefore, the following median values were determined for the references : Sehmel - 5.5e-4, Rognon - 4.6e-6, Tegen and Fung - 1e-4, Anspaugh - 7.1e-4, Soldat - 1e-4. The geometric means of these values is 1.12e-4, with a geometric standard error of the mean of 2.5. To define the range of the parameter, assume a log-uniform range to maximize the entropy of the distribution with a range of plus or minus the standard error of the mean. The final distribution for the parameter is:

loguniform

AirborneMassLoadAboveSoil[g/m<sup>3</sup>]

5e-5, 3e-4

\*\* Note that I recently was able to acquire the Rognon (1991) paper and am evaluating whether the data is in fact appropriate to use in the development of the mass loading value above soil for Yucca Mountain. If it was excluded from the calculation, the result would be:

loguniform

AirborneMassLoadAboveSoil[g/m<sup>3</sup>]

1.72e-4, 3.62e-4

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Title: TPA 4.0 Testing

Participants: J. Weldy

3/7/00      Testing of changes to TPA 4.0

### **SCR 301**

Functional Tests:

#### Test 2

This test is for whether the DCFs are properly switching to the pluvial DCFs at the proper time. The test will consist of running a case of adult dose for 100,000 years (so that the pluvial DCFs will kick in and return to current conditions). Then an Excel spreadsheet will be used to multiply the releases from SZFT (in dcagw.ech) by the DCF (in gw\_cb\_ad.dat and gw\_pb\_ad.dat) and divide by the proper pumping rate (from tpa.inp) to check that both are switching at the pluvial time.

Test routine: Run a base case for the adult receptor group. Compare the DCFs calculated for the base case to the DCFs calculated for the other age groups. Confirm that the ratio of the total DCFs are consistent with Smith et al. (2000). Confirm that the ratio of the pathway-specific DCFs are consistent with the Excel calculations.

Files needed for test: gw\_cb\_ad.dat for 6 age groups

Test conducted by JRW on 3/7/00

The following table shows how the doses were compared for U-234 and U-238.

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Time	U238		U234											
0.00e+00	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00						
2.31e+01	0.00e+00	0.00e+00	8750000	1.2e+07	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15		
4.67e+01	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15		
7.09e+01	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15		
9.57e+01	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15		
1.21e+02	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15		
1.47e+02	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15		
1.74e+02	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15		
2.01e+02	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15		
2.28e+02	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15		

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3.16e+03	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
3.25e+03	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
3.35e+03	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
3.45e+03	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
3.56e+03	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
3.66e+03	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
3.77e+03	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
3.88e+03	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
4.00e+03	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
4.12e+03	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
4.24e+03	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
4.36e+03	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
4.48e+03	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
4.61e+03	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
4.74e+03	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
4.88e+03	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
5.01e+03	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
5.15e+03	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
5.30e+03	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
5.44e+03	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
5.59e+03	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
5.75e+03	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
5.91e+03	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
6.07e+03	0.00e+00	0.00e+00	8750000	12096623	585000	635000	0.00e+00	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
6.23e+03	9.23e-28	0.00e+00	8750000	12096623	585000	635000	4.46e-29	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
6.40e+03	2.23e-26	0.00e+00	8750000	12096623	585000	635000	1.08e-27	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15

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6.58e+03	2.39e-25	0.00e+00	8750000	12096623	585000	635000	1.16e-26	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
6.75e+03	1.80e-24	0.00e+00	8750000	12096623	585000	635000	8.72e-26	0.00e+00	1.00e-15	1.00e-15	1e-15	1e-15
6.93e+03	9.70e-24	1.02e-23	8750000	12096623	585000	635000	4.69e-25	5.36e-25	1.00e-15	1.00e-15	1e-15	1e-15
7.12e+03	4.11e-23	6.13e-23	8750000	12096623	585000	635000	1.99e-24	3.22e-24	1.00e-15	1.00e-15	1e-15	1e-15
7.31e+03	1.54e-22	3.04e-22	8750000	12096623	585000	635000	7.46e-24	1.59e-23	1.00e-15	1.00e-15	1e-15	1e-15
7.50e+03	5.08e-22	1.19e-21	8750000	12096623	585000	635000	2.46e-23	6.25e-23	1.00e-15	1.00e-15	1e-15	1e-15
7.70e+03	1.51e-21	4.05e-21	8750000	12096623	585000	635000	7.32e-23	2.12e-22	1.00e-15	1.00e-15	1e-15	1e-15
7.91e+03	4.14e-21	1.22e-20	8750000	12096623	585000	635000	2.00e-22	6.38e-22	1.00e-15	1.00e-15	1e-15	1e-15
8.11e+03	1.06e-20	3.35e-20	8750000	12096623	585000	635000	5.12e-22	1.76e-21	1.00e-15	1.00e-15	1e-15	1e-15
8.33e+03	2.52e-20	8.41e-20	8750000	12096623	585000	635000	1.22e-21	4.41e-21	1.00e-15	1.00e-15	1e-15	1e-15
8.54e+03	5.66e-20	1.97e-19	8750000	12096623	585000	635000	2.74e-21	1.03e-20	1.00e-15	1.00e-15	1e-15	1e-15
8.77e+03	1.22e-19	4.37e-19	8750000	12096623	585000	635000	5.89e-21	2.29e-20	1.00e-15	1.00e-15	1e-15	1e-15
9.00e+03	2.50e-19	9.18e-19	8750000	12096623	585000	635000	1.21e-20	4.82e-20	1.00e-15	1.00e-15	1e-15	1e-15
9.23e+03	4.91e-19	1.84e-18	8750000	12096623	585000	635000	2.38e-20	9.66e-20	1.00e-15	1.00e-15	1e-15	1e-15
9.47e+03	9.32e-19	3.54e-18	8750000	12096623	585000	635000	4.51e-20	1.86e-19	1.00e-15	1.00e-15	1e-15	1e-15
9.71e+03	1.71e-18	6.58e-18	8750000	12096623	585000	635000	8.27e-20	3.45e-19	1.00e-15	1.00e-15	1e-15	1e-15
9.96e+03	3.04e-18	1.18e-17	8750000	12096623	585000	635000	1.47e-19	6.20e-19	1.00e-15	1.00e-15	1e-15	1e-15
1.02e+04	5.29e-18	2.07e-17	8750000	12096623	585000	635000	2.56e-19	1.09e-18	1.00e-15	1.00e-15	1e-15	1e-15
1.05e+04	8.95e-18	3.52e-17	8750000	12096623	585000	635000	4.33e-19	1.85e-18	1.00e-15	1.00e-15	1e-15	1e-15
1.08e+04	1.48e-17	5.86e-17	8750000	12096623	585000	635000	7.16e-19	3.08e-18	1.00e-15	1.00e-15	1e-15	1e-15
1.10e+04	2.40e-17	9.56e-17	8750000	12096623	585000	635000	1.16e-18	5.02e-18	1.00e-15	1.01e-15	1e-15	1e-15
1.13e+04	3.82e-17	1.52e-16	8750000	12096623	585000	635000	1.85e-18	8.00e-18	1.00e-15	1.01e-15	1e-15	1e-15
1.16e+04	5.98e-17	2.40e-16	8750000	12096623	585000	635000	2.89e-18	1.26e-17	1.00e-15	1.01e-15	1e-15	1e-15
1.19e+04	9.22e-17	3.70e-16	8750000	12096623	585000	635000	4.46e-18	1.94e-17	1.00e-15	1.02e-15	1e-15	1e-15
1.22e+04	1.40e-16	5.64e-16	8750000	12096623	585000	635000	6.77e-18	2.96e-17	1.01e-15	1.03e-15	1e-15	1e-15
1.25e+04	2.10e-16	8.46e-16	8750000	12096623	585000	635000	1.01e-17	4.44e-17	1.01e-15	1.04e-15	1e-15	1e-15

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1.28e+04	3.10e-16	1.25e-15	8750000	12096623	585000	635000	1.50e-17	6.58e-17	1.01e-15	1.07e-15	1e-15	1e-15
1.31e+04	4.53e-16	1.84e-15	6215000	8592058.8	436000	475000	2.30e-17	1.02e-16	1.02e-15	1.10e-15	1e-15	1e-15
1.35e+04	6.56e-16	2.66e-15	6215000	8592058.8	436000	475000	3.33e-17	1.47e-16	1.03e-15	1.15e-15	1e-15	1e-15
1.38e+04	9.39e-16	3.81e-15	6215000	8592058.8	436000	475000	4.76e-17	2.11e-16	1.05e-15	1.21e-15	1e-15	1e-15
1.42e+04	1.33e-15	5.41e-15	6215000	8592058.8	436000	475000	6.75e-17	2.99e-16	1.07e-15	1.30e-15	1e-15	1e-15
1.45e+04	1.87e-15	7.61e-15	6215000	8592058.8	436000	475000	9.49e-17	4.21e-16	1.09e-15	1.42e-15	1e-15	1e-15
1.49e+04	2.61e-15	1.06e-14	6215000	8592058.8	436000	475000	1.32e-16	5.87e-16	1.13e-15	1.59e-15	1e-15	1e-15
1.52e+04	3.60e-15	1.47e-14	6215000	8592058.8	436000	475000	1.83e-16	8.12e-16	1.18e-15	1.81e-15	1e-15	1e-15
1.56e+04	4.94e-15	2.02e-14	6215000	8592058.8	436000	475000	2.51e-16	1.11e-15	1.25e-15	2.11e-15	1e-15	1e-15
1.60e+04	6.74e-15	2.75e-14	6215000	8592058.8	436000	475000	3.42e-16	1.52e-15	1.34e-15	2.52e-15	1e-15	1e-15
1.64e+04	9.12e-15	3.72e-14	6215000	8592058.8	436000	475000	4.63e-16	2.06e-15	1.46e-15	3.06e-15	1e-15	1e-15
1.68e+04	1.23e-14	5.01e-14	6215000	8592058.8	436000	475000	6.22e-16	2.77e-15	1.62e-15	3.77e-15	1e-15	1e-15
1.72e+04	1.64e-14	6.69e-14	6215000	8592058.8	436000	475000	8.31e-16	3.70e-15	1.83e-15	4.70e-15	1e-15	1e-15
1.77e+04	2.18e-14	8.89e-14	6215000	8592058.8	436000	475000	1.10e-15	4.91e-15	2.10e-15	5.91e-15	1e-15	1e-15
1.81e+04	2.88e-14	1.17e-13	6215000	8592058.8	436000	475000	1.46e-15	6.49e-15	2.46e-15	7.49e-15	1e-15	1e-15
1.85e+04	3.78e-14	1.54e-13	6215000	8592058.8	436000	475000	1.92e-15	8.53e-15	2.92e-15	9.53e-15	1e-15	1e-15
1.90e+04	4.94e-14	2.02e-13	6215000	8592058.8	436000	475000	2.51e-15	1.12e-14	3.51e-15	1.22e-14	1e-15	1e-15
1.95e+04	6.43e-14	2.63e-13	6215000	8592058.8	436000	475000	3.26e-15	1.45e-14	4.26e-15	1.55e-14	1e-15	1e-15
1.99e+04	8.33e-14	3.40e-13	6215000	8592058.8	436000	475000	4.23e-15	1.88e-14	5.22e-15	1.98e-14	1e-15	1e-15
2.04e+04	1.07e-13	4.38e-13	6215000	8592058.8	436000	475000	5.45e-15	2.42e-14	6.45e-15	2.52e-14	1e-15	1e-15
2.09e+04	1.38e-13	5.63e-13	6215000	8592058.8	436000	475000	7.00e-15	3.11e-14	7.99e-15	3.21e-14	1e-15	1e-15
2.15e+04	1.76e-13	7.19e-13	6215000	8592058.8	436000	475000	8.94e-15	3.97e-14	9.94e-15	4.07e-14	1e-15	1e-15
2.20e+04	2.24e-13	9.15e-13	6215000	8592058.8	436000	475000	1.14e-14	5.06e-14	1.24e-14	5.15e-14	1e-15	9e-16
2.25e+04	2.85e-13	1.16e-12	6215000	8592058.8	436000	475000	1.44e-14	6.41e-14	1.54e-14	6.51e-14	1e-15	1e-15
2.31e+04	3.60e-13	1.47e-12	6215000	8592058.8	436000	475000	1.83e-14	8.10e-14	1.93e-14	8.19e-14	1e-15	9e-16
2.36e+04	4.53e-13	1.84e-12	6215000	8592058.8	436000	475000	2.30e-14	1.02e-13	2.40e-14	1.03e-13	1e-15	1e-15

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2.42e+04	5.69e-13	2.31e-12	6215000	8592058.8	436000	475000	2.89e-14	1.28e-13	2.98e-14	1.29e-13	9e-16	1e-15
2.48e+04	7.11e-13	2.89e-12	6215000	8592058.8	436000	475000	3.61e-14	1.60e-13	3.71e-14	1.61e-13	1e-15	1e-15
2.54e+04	8.86e-13	3.60e-12	6215000	8592058.8	436000	475000	4.50e-14	1.99e-13	4.59e-14	2.00e-13	9e-16	1e-15
2.60e+04	1.10e-12	4.46e-12	6215000	8592058.8	436000	475000	5.59e-14	2.47e-13	5.68e-14	2.48e-13	9e-16	1e-15
2.66e+04	1.36e-12	5.52e-12	6215000	8592058.8	436000	475000	6.92e-14	3.05e-13	7.02e-14	3.06e-13	1e-15	8e-16
2.73e+04	1.68e-12	6.81e-12	6215000	8592058.8	436000	475000	8.54e-14	3.76e-13	8.64e-14	3.77e-13	1e-15	6e-16
2.80e+04	2.07e-12	8.37e-12	6215000	8592058.8	436000	475000	1.05e-13	4.63e-13	1.06e-13	4.63e-13	8e-16	2e-16
2.86e+04	2.54e-12	1.03e-11	6215000	8592058.8	436000	475000	1.29e-13	5.67e-13	1.30e-13	5.68e-13	9e-16	7e-16
2.93e+04	3.11e-12	1.25e-11	6215000	8592058.8	436000	475000	1.58e-13	6.93e-13	1.59e-13	6.94e-13	1e-15	6e-16
3.00e+04	3.80e-12	1.53e-11	6215000	8592058.8	436000	475000	1.93e-13	8.45e-13	1.94e-13	8.45e-13	1e-15	-1e-17
3.08e+04	4.62e-12	1.86e-11	6215000	8592058.8	436000	475000	2.35e-13	1.03e-12	2.35e-13	1.03e-12	4e-16	3e-15
3.15e+04	5.61e-12	2.25e-11	6215000	8592058.8	436000	475000	2.85e-13	1.24e-12	2.86e-13	1.24e-12	1e-15	-4e-15
3.23e+04	6.79e-12	2.72e-11	6215000	8592058.8	436000	475000	3.45e-13	1.50e-12	3.45e-13	1.50e-12	5e-16	-4e-15
3.30e+04	8.20e-12	3.28e-11	6215000	8592058.8	436000	475000	4.16e-13	1.81e-12	4.17e-13	1.81e-12	1e-15	-2e-15
3.38e+04	9.87e-12	3.94e-11	6215000	8592058.8	436000	475000	5.01e-13	2.18e-12	5.01e-13	2.18e-12	3e-16	2e-15
3.47e+04	1.19e-11	4.72e-11	6215000	8592058.8	436000	475000	6.01e-13	2.61e-12	6.02e-13	2.61e-12	7e-16	-4e-16
3.55e+04	1.42e-11	5.65e-11	6215000	8592058.8	436000	475000	7.20e-13	3.12e-12	7.21e-13	3.12e-12	7e-16	-1e-15
3.63e+04	1.70e-11	6.73e-11	6215000	8592058.8	436000	475000	8.61e-13	3.72e-12	8.61e-13	3.72e-12	5e-16	-2e-15
3.72e+04	2.02e-11	8.01e-11	6215000	8592058.8	436000	475000	1.03e-12	4.43e-12	1.03e-12	4.42e-12	5e-15	-6e-15
3.81e+04	2.40e-11	9.50e-11	6215000	8592058.8	436000	475000	1.22e-12	5.25e-12	1.22e-12	5.25e-12	7e-16	-2e-15
3.90e+04	2.85e-11	1.12e-10	6215000	8592058.8	436000	475000	1.45e-12	6.21e-12	1.45e-12	6.21e-12	4e-15	-4e-15
4.00e+04	3.37e-11	1.33e-10	6215000	8592058.8	436000	475000	1.71e-12	7.34e-12	1.71e-12	7.33e-12	-5e-16	-5e-15
4.09e+04	3.98e-11	1.56e-10	6215000	8592058.8	436000	475000	2.02e-12	8.64e-12	2.02e-12	8.63e-12	1e-15	-7e-15
4.19e+04	4.68e-11	1.84e-10	6215000	8592058.8	436000	475000	2.38e-12	1.01e-11	2.38e-12	1.01e-11	3e-15	-5e-14
4.29e+04	5.50e-11	2.15e-10	6215000	8592058.8	436000	475000	2.79e-12	1.19e-11	2.79e-12	1.19e-11	-2e-15	1e-14
4.39e+04	6.45e-11	2.51e-10	6215000	8592058.8	436000	475000	3.27e-12	1.39e-11	3.27e-12	1.39e-11	-2e-15	6e-15

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4.50e+04	7.54e-11	2.93e-10	6215000	8592058.8	436000	475000	3.82e-12	1.62e-11	3.82e-12	1.62e-11	-5e-15	-9e-16
4.61e+04	8.79e-11	3.41e-10	6215000	8592058.8	436000	475000	4.46e-12	1.88e-11	4.46e-12	1.88e-11	-2e-15	-5e-14
4.72e+04	1.02e-10	3.96e-10	6215000	8592058.8	436000	475000	5.19e-12	2.19e-11	5.19e-12	2.19e-11	-2e-15	3e-14
4.83e+04	1.19e-10	4.58e-10	6215000	8592058.8	436000	475000	6.03e-12	2.53e-11	6.02e-12	2.53e-11	-7e-15	-2e-14
4.95e+04	1.38e-10	5.29e-10	6215000	8592058.8	436000	475000	6.98e-12	2.92e-11	6.98e-12	2.92e-11	-1e-15	-4e-14
5.06e+04	1.59e-10	6.09e-10	6215000	8592058.8	436000	475000	8.07e-12	3.37e-11	8.06e-12	3.37e-11	-8e-15	2e-14
5.18e+04	1.83e-10	7.00e-10	6215000	8592058.8	436000	475000	9.30e-12	3.87e-11	9.30e-12	3.87e-11	-1e-15	-2e-14
5.31e+04	2.11e-10	8.03e-10	6215000	8592058.8	436000	475000	1.07e-11	4.44e-11	1.07e-11	4.44e-11	5e-16	1e-14
5.43e+04	2.42e-10	9.18e-10	6215000	8592058.8	436000	475000	1.23e-11	5.08e-11	1.23e-11	5.07e-11	2e-14	-8e-14
5.56e+04	2.77e-10	1.05e-09	6215000	8592058.8	436000	475000	1.41e-11	5.79e-11	1.41e-11	5.79e-11	4e-14	-4e-14
5.70e+04	3.16e-10	1.19e-09	6215000	8592058.8	436000	475000	1.61e-11	6.60e-11	1.61e-11	6.59e-11	4e-14	-5e-14
5.83e+04	3.61e-10	1.35e-09	6215000	8592058.8	436000	475000	1.83e-11	7.49e-11	1.83e-11	7.48e-11	-3e-15	-9e-14
5.97e+04	4.10e-10	1.53e-09	6215000	8592058.8	436000	475000	2.08e-11	8.48e-11	2.08e-11	8.48e-11	-9e-15	-4e-14
6.11e+04	4.65e-10	1.73e-09	6215000	8592058.8	436000	475000	2.36e-11	9.59e-11	2.36e-11	9.58e-11	-3e-15	-7e-14
6.26e+04	5.26e-10	1.95e-09	6215000	8592058.8	436000	475000	2.67e-11	1.08e-10	2.67e-11	1.08e-10	-9e-15	-7e-14
6.41e+04	5.94e-10	2.20e-09	6215000	8592058.8	436000	475000	3.02e-11	1.22e-10	3.01e-11	1.21e-10	-5e-14	-5e-13
6.56e+04	6.69e-10	2.47e-09	6215000	8592058.8	436000	475000	3.40e-11	1.36e-10	3.39e-11	1.36e-10	-6e-14	-3e-13
6.72e+04	7.52e-10	2.76e-09	6215000	8592058.8	436000	475000	3.82e-11	1.52e-10	3.81e-11	1.52e-10	-5e-14	-5e-13
6.88e+04	8.43e-10	3.08e-09	6215000	8592058.8	436000	475000	4.28e-11	1.70e-10	4.27e-11	1.70e-10	-6e-14	-1e-13
7.04e+04	9.42e-10	3.43e-09	6215000	8592058.8	436000	475000	4.78e-11	1.89e-10	4.78e-11	1.89e-10	2e-15	-4e-13
7.21e+04	1.05e-09	3.80e-09	6215000	8592058.8	436000	475000	5.33e-11	2.10e-10	5.33e-11	2.10e-10	-7e-15	-2e-13
7.38e+04	1.17e-09	4.21e-09	6215000	8592058.8	436000	475000	5.93e-11	2.33e-10	5.93e-11	2.33e-10	-6e-17	2e-13
7.55e+04	1.30e-09	4.65e-09	6215000	8592058.8	436000	475000	6.58e-11	2.57e-10	6.58e-11	2.57e-10	5e-15	-9e-14
7.73e+04	1.44e-09	5.12e-09	8750000	12096623	585000	635000	6.94e-11	2.69e-10	7.28e-11	2.83e-10	3e-12	1e-11
7.91e+04	1.59e-09	5.64e-09	8750000	12096623	585000	635000	7.68e-11	2.96e-10	7.67e-11	2.96e-10	-9e-14	-2e-14
8.10e+04	1.83e-09	6.47e-09	8750000	12096623	585000	635000	8.86e-11	3.40e-10	8.85e-11	3.40e-10	-8e-14	2e-13

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8.29e+04	2.64e-09	9.29e-09	8750000	12096623	585000	635000	1.28e-10	4.88e-10	1.28e-10	4.88e-10	3e-13	5e-13
8.49e+04	4.66e-09	1.63e-08	8750000	12096623	585000	635000	2.25e-10	8.56e-10	2.25e-10	8.56e-10	-4e-13	-7e-14
8.69e+04	7.40e-09	2.58e-08	8750000	12096623	585000	635000	3.58e-10	1.35e-09	3.58e-10	1.35e-09	-4e-15	-3e-12
8.90e+04	1.01e-08	3.49e-08	8750000	12096623	585000	635000	4.87e-10	1.83e-09	4.87e-10	1.83e-09	-4e-14	2e-13
9.11e+04	1.26e-08	4.35e-08	8750000	12096623	585000	635000	6.11e-10	2.28e-09	6.10e-10	2.28e-09	-7e-13	-1e-12
9.32e+04	1.52e-08	5.20e-08	8750000	12096623	585000	635000	7.36e-10	2.73e-09	7.35e-10	2.73e-09	-9e-13	-2e-12
9.54e+04	1.78e-08	6.06e-08	8750000	12096623	585000	635000	8.63e-10	3.18e-09	8.62e-10	3.18e-09	-8e-13	-2e-12
9.77e+04	2.05e-08	6.93e-08	8750000	12096623	585000	635000	9.92e-10	3.64e-09	9.92e-10	3.64e-09	-4e-13	3e-12
1.00e+05	2.33e-08	7.82e-08	8750000	12096623	585000	635000	1.13e-09	4.10e-09	1.13e-09	4.10e-09	3e-12	-3e-12

The difference between the two doses never exceeds 1e-11 and therefore is acceptable. Similar testing was conducted for other radionuclides as is shown in the following table:

Nuclide	Ratio of SZ						Actual ratio					
	Rel ea se in			Actual ratio do se in								
	Pluv ye Ratio of SZ			Expected Rel	Expected Ratio	Actual ratio ye						
Current DC	Ratio of Plu to Curr	Pluvial year	Ratio of SZ	Expected Rel	Expected Ratio	Actual ratio ye	do	se	in	ye	ar	ar
F	Plu vial	to Curr	13	eas	of	13	77					
(re	(re	to Well	10	e in	Dose	10	30					
m/	Pluvial DCF	Cu Pu	0	year	at	0	0					
yr/	(re	rre	773	year	at	0	0					
Ci/	m/yr	mpi	7730	year	year	12	79					
m3	m3	nt	ye	1310	7730	ye	ye					
)	/Ci/	DC	ar	7730	0 to	0 to	0 to					
	m3)	F	12	year	0 to	0 to	0 to					
		es	791	year	year	year	12	79				
			80	7910	1280	7910	80	10				
			0	00	0	0	0	0				

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NOTE: difference in value is because 1e-15 mrem added to calculated dose to avoid reporting zero dose. This will have no effect on the reported results, since it is many orders of magnitude below total calculated doses.

U238	5.847e+05	4.358e+05	7.454e-01	7.103e-01	1.462e+00	9.038e-01	<b>1.534e+00</b>	9.485e-01	<b>1.010e+00</b>	9.492e-01
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Cm246	7.739e+06	5.837e+06	7.542e-01	7.103e-01			<b>0.000e+00</b>	0.000e+00		
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Pu242	7.016e+06	5.298e+06	7.552e-01	7.103e-01			<b>0.000e+00</b>	0.000e+00		
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Am242	m7.384e+06	5.571e+06	7.544e-01	7.103e-01			<b>0.000e+00</b>	0.000e+00		
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Pu238	6.694e+06	5.046e+06	7.539e-01	7.103e-01			<b>0.000e+00</b>	0.000e+00		
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NOTE: difference in value is because 1e-15 mrem added to calculated

U234	6.354e+05	4.747e+05	7.471e-01	7.103e-01	1.464e+00	9.083e-01	<b>1.540e+00</b>	9.555e-01	<b>1.028e+00</b>	9.561e-01
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Th230	1.158e+06	8.738e+05	7.545e-01	7.103e-01	8.771e-01	<b>0.000e+00</b>	9.317e-01
Ra226	3.265e+06	2.409e+06	7.378e-01	7.103e-01	8.719e-01	<b>0.000e+00</b>	9.056e-01
Pb210	1.245e+07	9.317e+06	7.485e-01	7.103e-01	8.719e-01	<b>0.000e+00</b>	9.188e-01
Cm243	5.312e+06	3.998e+06	7.527e-01	7.103e-01		<b>0.000e+00</b>	0.000e+00
Am243	7.696e+06	5.800e+06	7.536e-01	7.103e-01		<b>0.000e+00</b>	0.000e+00
Pu239	7.386e+06	5.578e+06	7.552e-01	7.103e-01		<b>0.000e+00</b>	0.000e+00
U235	6.688e+05	4.966e+05	7.425e-01	7.103e-01		<b>0.000e+00</b>	0.000e+00
Pa231	2.233e+07	1.690e+07	7.572e-01	7.103e-01		<b>0.000e+00</b>	0.000e+00
Ac227	3.059e+07	2.301e+07	7.522e-01	7.103e-01		<b>0.000e+00</b>	0.000e+00
Cm245	7.869e+06	5.932e+06	7.539e-01	7.103e-01		<b>0.000e+00</b>	0.000e+00
Pu241	1.430e+05	1.079e+05	7.549e-01	7.103e-01		<b>0.000e+00</b>	0.000e+00
Am241	7.631e+06	5.755e+06	7.542e-01	7.103e-01		<b>0.000e+00</b>	0.000e+00
Np237	9.701e+06	7.300e+06	7.524e-01	7.103e-01	9.672e-01	<b>0.000e+00</b>	1.025e+00
U233	6.472e+05	4.842e+05	7.482e-01	7.103e-01		<b>0.000e+00</b>	0.000e+00
Th229	8.013e+06	5.969e+06	7.450e-01	7.103e-01		<b>0.000e+00</b>	0.000e+00
Cm244	4.218e+06	3.142e+06	7.450e-01	7.103e-01		<b>0.000e+00</b>	0.000e+00
Pu240	7.386e+06	5.578e+06	7.552e-01	7.103e-01		<b>0.000e+00</b>	0.000e+00
U236	6.015e+05	4.495e+05	7.473e-01	7.103e-01		<b>0.000e+00</b>	0.000e+00
U232	3.083e+06	2.307e+06	7.481e-01	7.103e-01		<b>0.000e+00</b>	0.000e+00
Sm151	9.815e+02	7.232e+02	7.368e-01	7.103e-01		<b>0.000e+00</b>	0.000e+00
Cs137	3.735e+05	2.546e+05	6.816e-01	7.103e-01		<b>0.000e+00</b>	0.000e+00
Cs135	5.448e+04	3.620e+04	6.645e-01	7.103e-01		<b>0.000e+00</b>	0.000e+00

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I129	1.932e+06	1.295e+06	6.701e-01	7.103e-01	9.614e-01	1.508e+00	<b>9.071e-01</b>	1.423e+00	<b>9.01</b>
Sn126	1.183e+06	8.267e+05	6.990e-01	7.103e-01			<b>0.000e+00</b>	0.000e+00	
Sn121m	2.063e+04	1.358e+04	6.580e-01	7.103e-01			<b>0.000e+00</b>	0.000e+00	
Ag108m	8.260e+05	5.782e+05	7.000e-01	7.103e-01			<b>0.000e+00</b>	0.000e+00	
Pd107	8.019e+02	5.618e+02	7.006e-01	7.103e-01			<b>0.000e+00</b>	0.000e+00	
Tc99	4.101e+03	3.042e+03	7.417e-01	7.103e-01	9.522e-01	8.856e-01	<b>9.943e-01</b>	9.248e-01	<b>9.94</b>
Mo93	8.329e+03	5.990e+03	7.192e-01	7.103e-01			<b>0.000e+00</b>	0.000e+00	
Nb94	8.378e+05	6.019e+05	7.184e-01	7.103e-01			<b>0.000e+00</b>	0.000e+00	
Zr93	3.758e+03	2.827e+03	7.522e-01	7.103e-01			<b>0.000e+00</b>	0.000e+00	
Sr90	6.575e+05	4.663e+05	7.091e-01	7.103e-01			<b>0.000e+00</b>	0.000e+00	
Se79	3.646e+04	2.562e+04	7.026e-01	7.103e-01		1.011e+00	<b>0.000e+00</b>	9.999e-01	
Ni63	3.460e+03	2.359e+03	6.818e-01	7.103e-01			<b>0.000e+00</b>	0.000e+00	
Ni59	1.263e+03	8.605e+02	6.813e-01	7.103e-01		9.769e-01	<b>0.000e+00</b>	9.371e-01	
Cl36	6.887e+04	4.837e+04	7.023e-01	7.103e-01	9.562e-01	1.602e+00	<b>9.454e-01</b>	1.584e+00	<b>9.41</b>
C14	1.740e+04	1.159e+04	6.661e-01	7.103e-01					

All of the files used for this test (dcagw.ech, pluvdcfreadtest.xls, regsa.tpa, gw\_cb\_ad.dat, gw\_pb\_ad.dat, rgwna.tpa, and tpa.inp) are contained in the following directory: /home/jweldy/tpa40m/TEST/301/test2

Results: This shows that for a number of representative radionuclides, the pluvial DCF switch is being conducted properly. Therefore, it can be concluded that the code is switching from base to pluvial DCFs at the proper time.

Test 3

Test 3: This test is to ensure that the parameters in tpa.inp for the GENII code are being sampled properly. This test will consist of running a series of 100 realizations of the TPA code and checking to see that the distribution of values generated by the sampling routine is appropriate for the distribution sampled. The tpa.inp file will be used to set up the distributions of the parameters that are sampled and the sp.tpa file will be checked to ensure that the values are sampled properly.

				Expected
	Min	Max	Mean	Me an
InterceptionFraction		1.05e-01	9.31e-01	4.86e-01
LeafyVegetableIrrigationRatePB[in	2.49e+01	4.30e+01	3.63e+01	36.3
OtherVegetableIrrigationRatePB[in	2.48e+01	4.29e+01	3.63e+01	36.3

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FruitIrrigationRatePB[in]	2.43e+01	4.30e+01	3.63e+01	36.3
GrainIrrigationRatePB[in]	2.41e+01	4.29e+01	3.63e+01	36.3
HomeIrrigationRatePB[in]	1.82e+01	6.47e+01	4.15e+01	41.5
PoultryFeedIrrigationRatePB[in]	2.47e+01	4.30e+01	3.63e+01	36.3
HenFeedIrrigationRatePB[in]	2.42e+01	4.29e+01	3.63e+01	36.3
LeafyVegetableIrrigationTimePB[mo]	3.06e+00	9.97e+00	6.50e+00	6.5
OtherVegetableIrrigationTimePB[mo]	2.06e+00	9.98e+00	6.00e+00	6
FruitIrrigationTimePB[mo]	2.00e+00	5.96e+00	4.00e+00	4
GrainIrrigationTimePB[mo]	6.01e+00	7.99e+00	7.00e+00	7
HomeIrrigationTimePB[mo]	9.02e+00	1.20e+01	1.05e+01	10.5
PoultryFeedIrrigationTimePB[mo]	6.01e+00	7.98e+00	7.00e+00	7
HenFeedIrrigationTimePB[mo]	6.02e+00	7.99e+00	7.00e+00	7
LeafyVegetableIrrigationRateCB[in]	3.17e+01	5.99e+01	5.03e+01	50.3
OtherVegetableIrrigationRateCB[in]	3.35e+01	6.00e+01	5.04e+01	50.3
FruitIrrigationRateCB[in]	3.12e+01	5.99e+01	5.03e+01	50.3
GrainIrrigationRateCB[in]	3.22e+01	6.00e+01	5.03e+01	50.3
HomeIrrigationRateCB[in]	2.61e+01	9.09e+01	5.85e+01	58.5
PoultryFeedIrrigationRateCB[in]	3.35e+01	5.99e+01	5.03e+01	50.3
HenFeedIrrigationRateCB[in]	3.36e+01	5.99e+01	5.03e+01	50.3
LeafyVegetableIrrigationTimeCB[mo]	3.02e+00	7.96e+00	5.50e+00	5.5
OtherVegetableIrrigationTimeCB[mo]	2.02e+00	8.00e+00	5.00e+00	5
FruitIrrigationTimeCB[mo]	2.00e+00	3.00e+00	2.50e+00	2.5
GrainIrrigationTimeCB[mo]	6.01e+00	7.98e+00	7.00e+00	7
HomeIrrigationTimeCB[mo]	6.04e+00	1.20e+01	9.00e+00	9
PoultryFeedIrrigationTimeCB[mo]	6.01e+00	7.98e+00	7.00e+00	7
HenFeedIrrigationTimeCB[mo]	6.01e+00	7.98e+00	7.00e+00	7
PoultryFeedGrowTime[day]	6.02e+01	9.00e+01	7.50e+01	75
HenFeedGrowTime[day]	6.01e+01	9.00e+01	7.50e+01	75
BeefFreshForageDietFraction	2.07e-01	8.81e-01	5.50e-01	0.55
MilkFreshForageDietFraction	1.20e-01	9.80e-01	5.50e-01	0.55
BeefFreshForageGrowTime[day]	3.02e+01	6.19e+01	4.60e+01	46
MilkFreshForageGrowTime[day]	3.02e+01	6.20e+01	4.60e+01	46
BeefFreshForageIrrigationRatePB[in]	2.45e+01	4.30e+01	3.63e+01	36.3
MilkFreshForageIrrigationRatePB[in]	2.44e+01	4.30e+01	3.63e+01	36.3
BeefFreshForageIrrigationTimePB[mo]	3.06e+00	9.93e+00	6.50e+00	6.5
MilkFreshForageIrrigationTimePB[mo]	3.05e+00	9.94e+00	6.50e+00	6.5
BeefFreshForageIrrigationRateCB[in]	3.37e+01	6.00e+01	5.03e+01	50.3
MilkFreshForageIrrigationRateCB[in]	3.37e+01	5.99e+01	5.03e+01	50.3
BeefFreshForageIrrigationTimeCB[mo]	3.01e+00	7.98e+00	5.50e+00	5.5
MilkFreshForageIrrigationTimeCB[mo]	3.05e+00	7.96e+00	5.50e+00	5.5

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DrinkingWaterConsumptionRate1[L]	1.93e+01	4.16e+02	1.10e+02	110
DrinkingWaterConsumptionRate2[L]	5.23e+01	9.11e+02	2.84e+02	284
DrinkingWaterConsumptionRate3[L]	5.00e+01	8.34e+02	2.84e+02	284
DrinkingWaterConsumptionRate4[L]	5.83e+01	1.22e+03	3.72e+02	372
DrinkingWaterConsumptionRate5[L]	1.37e+02	2.02e+03	5.46e+02	546
LeafyVegetableConsumptionRate6[kg]	3.15e+00	4.88e+01	1.25e+01	12.5
OtherVegetableConsumptionRate6[kg]	5.74e+00	3.59e+02	7.15e+01	71.5
FruitConsumptionRate6[kg]	6.31e+00	3.95e+02	6.52e+01	65.2
GrainConsumptionRate6[kg]	9.19e+00	7.21e+02	9.83e+01	98.3
BeefConsumptionRate6[kg]	1.37e+01	2.58e+02	6.64e+01	66.4
PoultryConsumptionRate6[kg]	1.70e+00	2.01e+01	6.78e+00	6.78
MilkConsumptionRate6[kg]	9.70e+00	8.82e+02	1.41e+02	141
PlantUptakeScaleFactor	1.00e-01	8.60e+00	1.31e+00	1.31
AnimalUptakeScaleFactor	1.51e-01	6.04e+00	1.29e+00	1.29
KD_Soil_Cm[cm <sup>3</sup> ]	6.04e+00	1.10e+07	1.54e+05	1.53e+05
KD_Soil_Pu[cm <sup>3</sup> ]	6.92e+00	9.75e+04	3.08e+03	3080
KD_Soil_U[cm <sup>3</sup> ]	1.20e-03	2.55e+05	4.18e+03	4180
KD_Soil_Am[cm <sup>3</sup> ]	4.92e-01	1.32e+06	4.50e+04	4.50e+04
KD_Soil_Np[cm <sup>3</sup> ]	2.76e-02	3.68e+02	2.13e+01	21.3
KD_Soil_Th[cm <sup>3</sup> ]	1.06e+01	1.24e+06	3.30e+04	3.30e+04
KD_Soil_Ra[cm <sup>3</sup> ]	1.66e-01	2.38e+06	5.07e+04	5.06e+04
KD_Soil_Pb[cm <sup>3</sup> ]	4.68e-01	5.20e+05	7.56e+03	7560
KD_Soil_Cs[cm <sup>3</sup> ]	4.38e-01	1.00e+06	1.38e+04	1.38e+04
KD_Soil_I[cm <sup>3</sup> ]	2.38e-03	2.51e+02	9.98e+00	9.98
KD_Soil_Tc[cm <sup>3</sup> ]	7.09e-04	1.61e+01	5.83e-01	0.582
KD_Soil_Ni[cm <sup>3</sup> ]	8.81e+00	2.06e+04	1.29e+03	1290
KD_Soil_C[cm <sup>3</sup> ]	5.59e-01	4.30e+01	7.17e+00	7.17
KD_Soil_Se[cm <sup>3</sup> ]	2.07e+01	1.62e+02	6.14e+01	61.4

The calculated means correspond very closely to the means predicted by theory.

Therefore, it can be concluded that the sampling routine is sampling the biosphere values correctly.

Files associated with this test (gdefault.inp, gftrans.inp, ggenii.inp, spread.tpa, sp.tpa, spread.xls, and tpa.inp) can be found in the following directory:  
 /home/jweldy/tpa40m/TEST/301/test3.

Test 4

Test 4: This test is to ensure that the appropriate GENII files are updated between realizations based on new values that are sampled for the GENII code. This test will consist of running a single realization run and a two realization run. For both

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runs, it will be confirmed that the values written to ggenii.inp and gftrans.inp are correctly being transferred from the sampled value contained in sp.tpa to these GENII input files.

Files inspected for the test: default.inp, gftrans.inp, ggenii.inp, sp.tpa, tpa.inp

Procedure: The sampled value of the biosphere parameters were looked up in the sp.tpa file. For the appropriate realization, these values were compared to the values that ended up in the input files for GENII (gdefault.inp, gftrans.inp, ggenii.inp). Note that these files are overwritten for each realization of the TPA code, so only the values from the last realization will be saved at the end of a run. Therefore, only one realization and two realization run of the TPA code was made.

Results: The values in the GENII input files corresponded precisely to the values sampled in the sp.tpa file. The files used for this test (gdefault.inp, gdefault.inp.1, gdefault.inp.2, gftrans.inp, gftrans.inp.1, gftrans.inp.2, ggenii.inp, ggenii.inp.1, ggenii.inp.2, sp.tpa.1, sp.tpa.2, tpa.inp.1, and tpa.inp.2) can be located in the following directory:

/home/jweldy/tpa40m/TEST/301/test4

### **Reasonableness Tests**

#### Test 1

This test is for whether the age-specific DCFs are implemented properly in the TPA code. The test will consist of running a base case of adult DCFs which will be compared to the DCFs for the other age groups. The results will be compared to age-specific dose calculations performed earlier using an Excel spreadsheet by Weldy by comparing the products of the intake quantity times the appropriate age DCF. This spreadsheet only indicates the changes to pathway specific dose, not overall dose.

Method: Perform a single run of the TPA code for each age group. Compare gw\_cb\_ad.dat files generated for each age group to get ratio of DCFs for each radionuclide. The comparisons are done using an Excel spreadsheet (gentpatest.xls) using data from an old spreadsheet (agedepdcf.xls). Note that the ratio generated is between the age group of interest and age group 5 in the tpa.inp file (ICRP 72 adult) since that is the ratio that the comparison data is available for.

Results: All adult to other age group ratios correspond to within a reasonable tolerance band (<10% difference) with a few exceptions. Note that the exceptions do not necessarily indicate that there is an error in the code since we are summing pathways with different differences in intakes and concentrations (indicated by 'Pathway' in the table) and the reference data does not include the effects of daughters, which sometimes contribute significantly to the total DCF (indicated by 'Daughters' in the table). Where there are exceptions, they are investigated further, either by looking at whether the daughters are contributing significantly to the DCF or by looking at the env.out file to determine the actual intake of

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radionuclides for the adult and reference age group and comparing that ratio to the reference adult to other age group ratio.

Age	Radio	Pathway	Reason for Dif fer en ce	Predicted ratio from Env.out (age group DCF/ adult DCF)	Code ratio (age grou p DCF/ adult DCF )
Infant	Ac-227	Milk	Daughters		
Infant	Th-229	Milk	Daughters		
Infant	Zr-93	Milk	Daughters		
Toddler	Cl-36	Crops	Pathway	3.16	3.27
Toddler	Zr-93	Animal	Daughters		
Toddler	Nb-94	Animal	Pathway	2.0	1.92
Toddler	Tc-99	Animal	Pathway	3.35	3.27
Toddler	U-232	Animal	Pathway	0.98	0.927
Toddler	U-236	Animal	Pathway	1.06	0.992
Toddler	Th-229	Animal	Daughters		
Toddler	Tc-99	Crops	Pathway	2.98	2.98
Toddler	Ac-227	Animal	Daughters		
Toddler	U-235	Animal	Pathway	1.06	1.00
Toddler	Pb-210	Animal	Daughters		
Toddler	U-234	Animal	Pathway	1.03	0.968
Toddler	U-238	Animal	Pathway	1.03	0.983
Pre-Teen	Most	Crops	Pathway	All U + Pu isotopes checked - assume all others are correct	All U + Pu isoto pes deter mine d to be corre ct
Pre-Teen	Ac-227	Milk	Daughters		
Pre-Teen	Th-229	Milk	Daughters		
Pre-Teen	Zr-93	Milk	Daughters		
Pre-Teen	U-238	Animal	Pathway	1.14	1.08
Pre-Teen	U-234	Animal	Pathway	1.14	1.08

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Pre-Teen	U-235	Animal	Pathway	1.14	1.08	
Pre-Teen	Ac-227	Animal	Daughters			
Pre-Teen	U-233	Animal	Pathway	1.14	1.08	
Pre-Teen	Th-229	Animal	Daughters			
Pre-Teen	U-236	Animal	Pathway	1.13	1.08	
Pre-Teen	U-232	Animal	Pathway	1.31	1.25	
Pre-Teen	Tc-99	Animal	Pathway	1.88	1.85	
Pre-Teen	Nb-94	Animal	Pathway	1.52	1.45	
Pre-Teen	Zr-93	Animal	Daughters			
Pre-Teen	C-14	Animal	Pathway	0.901	0.859	
Teen	U-238	Animal	Pathway	1.49	1.44	
Teen	Pb-210	Animal	Daughters			
Teen	U-235	Animal	Pathway	1.49	1.44	
Teen	Ac-227	Animal	Daughters			
Teen	Th-229	Animal	Daughters			
Teen	U-236	Animal	Pathway	1.49	1.45	
Teen	U-232	Animal	Pathway	1.49	1.45	
Teen	Tc-99	Animal	Pathway	1.42	1.42	
Teen	Nb-94	Animal	Pathway	1.21	1.2	
Teen	Zr-93	Animal	Daughters			
Teen	Pb-210	Crops	Daughters			
Teen	Th-229	Crops	Daughters			
Teen	Sr-90	Crops	Pathway	2.5	2.55	
Teen	Ac-227	Crops	Daughters			
Teen	Th-229	Crops	Daughters			

Results: The DCFs for all age groups appear to be reasonable. It can be concluded that the code is properly calculating the DCFs for all age groups. All files used in this test (gentpatest.xls and agedepdcf.xls) can be found in the directory:  
d:\personal\excel files\TPA Files\40 Test on the computer Kraken

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Test 5

This test is to ensure that the pluvial DCFs calculated in the current implementation of the TPA code match the DCFs calculated for TPA 3.3 when the same input data is used. This test will consist of setting all the gentpa values in tpa.inp to constant values that match the values used in Laplante, et al. (1997) and ensure that the pluvial DCFs match those in the same reference. Files used in the test include tpa.inp, for the input data, and gw\_pb\_ad.dat to check the DCF.

Method: Visual comparison between the DCF values generated in the file gw\_pb\_ad.dat and the results in Laplante, et al. (1997).

Results: All generated pluvial DCFs matched the values in Laplante, et al. (1997). Therefore, it can be concluded that the implementation of the calculation of the pluvial DCFs using GENII in TPA is correct. Files used for this test (tpa.inp, gw\_pb\_ad.dat) are located in the directory /home/jweldy/tpa40m/TEST/301/test5.

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**SCR 311**

### Test 1

This test will make sure that the switch that was put in the volcano module properly switches between a geometric method to calculate the number of WPs ejected by a volcano based on the diameter of the cone and a user specified distribution of WPs ejected. Two single realizations were run for this test. For both realizations, the number of WPs ejected based on the geometric method is very small (1) and the number of WPs ejected based on the user input method is higher (75) to tell the difference between the two.

Results:

FROM SCREEN.OUT.1

=====

=====

*exec: Welcome to TPA Version 4.0betaM*

*Job started: Mon Jun 19 13:39:48 2000*

=====

=====

#### *REPOSITORY DESIGN INFORMATION*

*Subarea Area Waste Number of WP*

#	[m <sup>2</sup> ]	[MTU]	
1	723591.3	14200.8	1455
2	784763.0	15303.7	1568
3	390372.0	7564.0	775
4	207581.3	4157.8	426
5	378972.8	7417.6	760
6	424872.5	8305.8	851
7	163938.3	3152.5	323
8	393468.9	7944.6	814

*Total Area [acre] = 856.82238463061*

*Total Buried Waste [MTU] = 68046.7200000000*

*Repository AML [MTU/acre] = 79.417532992367*

*Specified Global Parameters:*

*Compliance Period = 100000.0 (yr)*

*Maximum Simulation Time = 100000.0 (yr)*

*Number Of Realizations = 1*

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*Number Of Subareas = 8  
Volcanism scenario = 1 (yes=1, no=0)  
Faulting scenario = 0 (yes=1, no=0)  
Seismic scenario = 1 (yes=1, no=0)*

*Distance to Receptor Group = 20.0 (km)*

**\*\*>>> CAUTION: CHECKING OF NUCLIDES AND CHAINS IS DISABLED**

*<<<\*\*\**

*\*\*>>> You may not be using the standard chains specified <<<\*\*\**

*\*\*>>> in the invent module. <<<\*\*\**

*\*\*>>> (see "CheckNuclidesAndChains(yes=1,no=0)" in tpa.inp)<<<\*\*\**

*\*\*\*>>> NOTE: When running with volcanism, verify that <<<\*\*\**

*\*\*\*>>> the maximum value of the PDF for parameter <<<\*\*\**

*\*\*\*>>> TimeOfNextVolcanicEventinRegionOfInterest[yr] is <<<\*\*\**

*\*\*\*>>> equal to the parameter MaximumTime[yr]. <<<\*\*\**

*The specified path for data = \$TPA\_DATA/*

*The specified path for codes = \$TPA\_TEST/*

*\*\*To modify global parameters or the path, stop code execution using  
control-C\*\**

*\*\*\*>>> WARNING: THE APPEND OPTION IS SELECTED <<<\*\*\*  
(see "OutputMode(0=None,1=All,2=UserDefined)" in tpa.inp)*

*For "SelectAppendFiles", a value of 0 (all append files) was set in tpa.inp.  
By selecting this option, files are written which may require 6 megs of disk  
space.*

*(more disk space could be needed)*

---

*subarea 1 of 8 realization 1 of 1*

---

*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

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\*\*\* No Corrosion WP Failure \*\*\*

exec: calling seismo

exec: calling volcano

\*\*\* failed WPs: 0 out of 1455 \*\*\*

exec: calling ebsrel

There is no EBS release

exec: calling uzft

There is no UZ release

exec: calling szft

There is no SZ release

---

subarea 2 of 8 realization 1 of 1

---

exec: calling uzflow

exec: calling nfenv

exec: calling ebsfail

\*\*\* No Corrosion WP Failure \*\*\*

exec: failed WPs from VOLCANIC event = 1307 at time = 1874.3 yr

(includes ejected WPs)

\*\*\* failed WPs: 1307 out of 1568 \*\*\*

\*\*\* ejected WPs: 75

exec: calling ebsrel

Highest release rates from Sub Area 2

Tc99 1.1926E+00 [Ci/yr/SA] at 3.665E+03 yr

C14 5.8096E-01 [Ci/yr/SA] at 3.665E+03 yr

Cs135 2.0689E-01 [Ci/yr/SA] at 3.665E+03 yr

Se79 1.7658E-01 [Ci/yr/SA] at 3.665E+03 yr

Ni59 5.3418E-02 [Ci/yr/SA] at 3.665E+03 yr

Am243 1.4004E-02 [Ci/yr/SA] at 1.451E+04 yr

exec: calling uzft

\*\*\* NEFTRAN is skipped for this UZ path since no layers have significant ground water travel time. \*\*\*

Highest release rates from UZ

Tc99 1.1926E+00 [Ci/yr/SA] at 3.665E+03 yr

Cs135 2.0689E-01 [Ci/yr/SA] at 3.665E+03 yr

Se79 1.7658E-01 [Ci/yr/SA] at 3.665E+03 yr

Ni59 5.3418E-02 [Ci/yr/SA] at 3.665E+03 yr

Am243 1.4004E-02 [Ci/yr/SA] at 1.451E+04 yr

I129 1.3793E-02 [Ci/yr/SA] at 3.665E+03 yr

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*exec: calling szft*

*Highest release rates from SZ*

Tc99	1.5815E-01 [Ci/yr/SA] at 8.113E+03 yr
I129	2.0465E-03 [Ci/yr/SA] at 5.444E+03 yr
Cl36	1.3768E-03 [Ci/yr/SA] at 4.742E+03 yr
Se79	7.8871E-04 [Ci/yr/SA] at 9.713E+03 yr
Np237	2.5981E-04 [Ci/yr/SA] at 1.000E+05 yr
U234	4.7980E-06 [Ci/yr/SA] at 8.293E+04 yr

---

*subarea 3 of 8 realization 1 of 1*

---

*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

*\*\*\* No Corrosion WP Failure \*\*\**

*\*\*\* failed WPs: 0 out of 775 \*\*\**

*exec: calling ebsrel*

*There is no EBS release*

*exec: calling uzft*

*There is no UZ release*

*exec: calling szft*

*There is no SZ release*

---

*subarea 4 of 8 realization 1 of 1*

---

*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

*\*\*\* No Corrosion WP Failure \*\*\**

*\*\*\* failed WPs: 0 out of 426 \*\*\**

*exec: calling ebsrel*

*There is no EBS release*

*exec: calling uzft*

*There is no UZ release*

*exec: calling szft*

*There is no SZ release*

---

*subarea 5 of 8 realization 1 of 1*

---

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*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

\*\*\* No Corrosion WP Failure \*\*\*

\*\*\* failed WPs: 0 out of 760 \*\*\*

*exec: calling ebsrel*

There is no EBS release

*exec: calling uzft*

There is no UZ release

*exec: calling szft*

There is no SZ release

---

subarea 6 of 8 realization 1 of 1

---

*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

\*\*\* No Corrosion WP Failure \*\*\*

\*\*\* failed WPs: 0 out of 851 \*\*\*

*exec: calling ebsrel*

There is no EBS release

*exec: calling uzft*

There is no UZ release

*exec: calling szft*

There is no SZ release

---

subarea 7 of 8 realization 1 of 1

---

*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

\*\*\* No Corrosion WP Failure \*\*\*

\*\*\* failed WPs: 0 out of 323 \*\*\*

*exec: calling ebsrel*

There is no EBS release

*exec: calling uzft*

There is no UZ release

*exec: calling szft*

There is no SZ release

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---

subarea 8 of 8 realization 1 of 1

---

exec: calling uzflow

exec: calling nfenv

exec: calling ebsfail

\*\*\* No Corrosion WP Failure \*\*\*

\*\*\* failed WPs: 0 out of 814 \*\*\*

exec: calling ebsrel

There is no EBS release

exec: calling uzft

There is no UZ release

exec: calling szft

There is no SZ release

exec: calling dcagw

Highest annual dose GW pathway

I129 2.5904E+00 [mrem/yr] at 5.444E+03 yr

Np237 2.6855E-01 [mrem/yr] at 1.000E+05 yr

Tc99 1.6397E-01 [mrem/yr] at 8.113E+03 yr

Cl36 3.6800E-02 [mrem/yr] at 4.742E+03 yr

Se79 1.5629E-02 [mrem/yr] at 1.314E+04 yr

U234 5.8073E-04 [mrem/yr] at 7.730E+04 yr

At end of TPI, annual dose GW pathway

Np237 2.6855E-01 [mrem/yr]

I129 7.1826E-03 [mrem/yr]

Se79 2.1254E-03 [mrem/yr]

Tc99 1.8349E-03 [mrem/yr]

U234 3.0712E-04 [mrem/yr]

U238 8.7956E-05 [mrem/yr]

sum 2.8013E-01 [mrem/yr]

exec: calling ashplumo

exec: calling ashrmovo

exec: calling dcags

Highest annual dose from GS

Pu240 7.5988E+03 [mrem/yr] at 1.874E+03 yr

Pu239 5.9059E+03 [mrem/yr] at 1.874E+03 yr

Am241 4.4295E+03 [mrem/yr] at 1.874E+03 yr

Am243 3.8242E+02 [mrem/yr] at 1.874E+03 yr

Pu242 3.3754E+01 [mrem/yr] at 1.874E+03 yr

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Np237 3.0382E+01 [mrem/yr] at 1.874E+03 yr  
exec: end realizations

exec: Run Successfully Completed

---

FROM SCREEN.OUT.2

=====

=====

exec: Welcome to TPA Version 4.0betaM

Job started: Mon Jun 19 13:44:06 2000

=====

=====

#### REPOSITORY DESIGN INFORMATION

Subarea Area Waste Number of WP

#	[m <sup>2</sup> ]	[MTU]	
1	723591.3	14200.8	1455
2	784763.0	15303.7	1568
3	390372.0	7564.0	775
4	207581.3	4157.8	426
5	378972.8	7417.6	760
6	424872.5	8305.8	851
7	163938.3	3152.5	323
8	393468.9	7944.6	814

Total Area [acre] = 856.82238463061

Total Buried Waste [MTU] = 68046.720000000

Repository AML [MTU/acre] = 79.417532992367

Specified Global Parameters:

Compliance Period = 100000.0 (yr)

Maximum Simulation Time = 100000.0 (yr)

Number Of Realizations = 1

Number Of Subareas = 8

Volcanism scenario = 1 (yes=1, no=0)

Faulting scenario = 0 (yes=1, no=0)

Seismic scenario = 1 (yes=1, no=0)

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*Distance to Receptor Group = 20.0 (km)*

\*\*>>> CAUTION: CHECKING OF NUCLIDES AND CHAINS IS DISABLED  
    <<<\*\*

\*\*>>> You may not be using the standard chains specified <<<\*\*

\*\*>>> in the invent module. <<<\*\*

\*\*>>> (see "CheckNuclidesAndChains(yes=1,no=0)" in tpa.inp)<<<\*\*

\*\*\*>>> NOTE: When running with volcanism, verify that <<<\*\*\*

\*\*\*>>> the maximum value of the PDF for parameter <<<\*\*\*

\*\*\*>>> TimeOfNextVolcanicEventinRegionOfInterest[yr] is <<<\*\*\*

\*\*\*>>> equal to the parameter MaximumTime[yr]. <<<\*\*\*

The specified path for data = \$TPA\_DATA/

The specified path for codes = \$TPA\_TEST/

\*\*To modify global parameters or the path, stop code execution using  
control-C\*\*

\*\*\*>>> WARNING: THE APPEND OPTION IS SELECTED <<<\*\*\*

(see "OutputMode(0=None,1=All,2=UserDefined)" in tpa.inp)

For "SelectAppendFiles", a value of 0 (all append files) was set in tpa.inp.

By selecting this option, files are written which may require 6 megs of disk  
space.

(more disk space could be needed)

---

-----  
subarea 1 of 8 realization 1 of 1

---

exec: calling uzflow

exec: calling nfenv

exec: calling ebsfail

\*\*\* No Corrosion WP Failure \*\*\*

exec: calling seismo

exec: calling volcano

\*\*\* failed WPs: 0 out of 1455 \*\*\*

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*exec: calling ebsrel*

*There is no EBS release*

*exec: calling uzft*

*There is no UZ release*

*exec: calling szft*

*There is no SZ release*

---

subarea 2 of 8 realization 1 of 1

---

*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

*\*\*\* No Corrosion WP Failure \*\*\**

*exec: failed WPs from VOLCANIC event = 9 at time = 1874.3 yr (includes ejected WPs)*

*exec: failed WPs from INITIAL event = 1 at time = 4875.7 yr*

*\*\*\* failed WPs: 10 out of 1568 \*\*\**

*\*\*\* ejected WPs: 1*

*exec: calling ebsrel*

*Highest release rates from Sub Area 2*

*Tc99 7.7439E-03 [Ci/yr/SA] at 3.665E+03 yr*

*C14 3.7725E-03 [Ci/yr/SA] at 3.665E+03 yr*

*Cs135 1.3435E-03 [Ci/yr/SA] at 3.665E+03 yr*

*Se79 1.1467E-03 [Ci/yr/SA] at 3.665E+03 yr*

*Ni59 3.4687E-04 [Ci/yr/SA] at 3.665E+03 yr*

*Am243 9.6823E-05 [Ci/yr/SA] at 1.451E+04 yr*

*exec: calling uzft*

*\*\*\* NEFTRAN is skipped for this UZ path since no layers have significant ground water travel time. \*\*\**

*Highest release rates from UZ*

*Tc99 7.7439E-03 [Ci/yr/SA] at 3.665E+03 yr*

*Cs135 1.3435E-03 [Ci/yr/SA] at 3.665E+03 yr*

*Se79 1.1467E-03 [Ci/yr/SA] at 3.665E+03 yr*

*Ni59 3.4687E-04 [Ci/yr/SA] at 3.665E+03 yr*

*Am243 9.6823E-05 [Ci/yr/SA] at 1.451E+04 yr*

*I129 8.9562E-05 [Ci/yr/SA] at 3.665E+03 yr*

*exec: calling szft*

*Highest release rates from SZ*

*Tc99 1.0269E-03 [Ci/yr/SA] at 8.113E+03 yr*

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*I129 1.3289E-05 [Ci/yr/SA] at 5.444E+03 yr  
Cl36 8.9406E-06 [Ci/yr/SA] at 4.742E+03 yr  
Se79 5.2263E-06 [Ci/yr/SA] at 1.641E+04 yr  
Np237 1.6874E-06 [Ci/yr/SA] at 1.000E+05 yr  
U234 3.5031E-08 [Ci/yr/SA] at 8.293E+04 yr*

---

*subarea 3 of 8 realization 1 of 1*

---

*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

*\*\*\* No Corrosion WP Failure \*\*\**

*exec: failed WPs from VOLCANIC event = 2 at time = 1874.3 yr*

*\*\*\* failed WPs: 2 out of 775 \*\*\**

*exec: calling ebsrel*

*Highest release rates from Sub Area 3*

*Tc99 1.0288E-03 [Ci/yr/SA] at 3.665E+03 yr  
C14 5.0273E-04 [Ci/yr/SA] at 3.665E+03 yr  
Cs135 1.7794E-04 [Ci/yr/SA] at 3.665E+03 yr  
Se79 1.5187E-04 [Ci/yr/SA] at 3.665E+03 yr  
Ni59 4.6545E-05 [Ci/yr/SA] at 3.665E+03 yr  
Am243 2.1157E-05 [Ci/yr/SA] at 1.562E+04 yr*

*exec: calling uzft*

*Highest release rates from UZ*

*Tc99 4.0151E-04 [Ci/yr/SA] at 4.116E+03 yr  
Se79 7.8001E-06 [Ci/yr/SA] at 1.601E+04 yr  
I129 4.4907E-06 [Ci/yr/SA] at 4.116E+03 yr  
Cm245 3.7163E-06 [Ci/yr/SA] at 4.357E+03 yr  
Cl36 2.7689E-06 [Ci/yr/SA] at 4.116E+03 yr  
Cs135 2.6523E-06 [Ci/yr/SA] at 2.540E+04 yr*

*exec: calling szft*

*Highest release rates from SZ*

*Tc99 1.5081E-04 [Ci/yr/SA] at 8.544E+03 yr  
I129 1.8690E-06 [Ci/yr/SA] at 5.907E+03 yr  
Cl36 1.1730E-06 [Ci/yr/SA] at 5.297E+03 yr  
Se79 9.0086E-07 [Ci/yr/SA] at 2.796E+04 yr  
U234 6.5795E-09 [Ci/yr/SA] at 9.323E+04 yr  
U238 2.0371E-09 [Ci/yr/SA] at 9.543E+04 yr*

---

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subarea 4 of 8 realization 1 of 1

---

exec: calling uzflow

exec: calling nfenv

exec: calling ebsfail

\*\*\* No Corrosion WP Failure \*\*\*

exec: failed WPs from VOLCANIC event = 1 at time = 1874.3 yr

\*\*\* failed WPs: 1 out of 426 \*\*\*

exec: calling ebsrel

Highest release rates from Sub Area 4

Tc99 5.3679E-04 [Ci/yr/SA] at 3.774E+03 yr

C14 2.6116E-04 [Ci/yr/SA] at 3.774E+03 yr

Cs135 9.4048E-05 [Ci/yr/SA] at 3.774E+03 yr

Se79 8.0266E-05 [Ci/yr/SA] at 3.774E+03 yr

Ni59 2.3240E-05 [Ci/yr/SA] at 3.774E+03 yr

Am243 9.6647E-06 [Ci/yr/SA] at 1.524E+04 yr

exec: calling uzft

Highest release rates from UZ

Tc99 2.5341E-04 [Ci/yr/SA] at 4.116E+03 yr

Se79 5.5431E-06 [Ci/yr/SA] at 1.451E+04 yr

Cs135 4.8164E-06 [Ci/yr/SA] at 1.854E+04 yr

I129 2.9470E-06 [Ci/yr/SA] at 4.116E+03 yr

Cl36 1.8268E-06 [Ci/yr/SA] at 4.116E+03 yr

Cm245 1.2321E-06 [Ci/yr/SA] at 4.235E+03 yr

exec: calling szft

Highest release rates from SZ

Tc99 8.8477E-05 [Ci/yr/SA] at 8.544E+03 yr

I129 1.1251E-06 [Ci/yr/SA] at 5.749E+03 yr

Cl36 7.1428E-07 [Ci/yr/SA] at 5.153E+03 yr

Se79 4.7660E-07 [Ci/yr/SA] at 2.363E+04 yr

U234 3.1466E-09 [Ci/yr/SA] at 9.107E+04 yr

U238 9.6422E-10 [Ci/yr/SA] at 9.323E+04 yr

---

subarea 5 of 8 realization 1 of 1

---

exec: calling uzflow

exec: calling nfenv

exec: calling ebsfail

\*\*\* No Corrosion WP Failure \*\*\*

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*exec: failed WPs from VOLCANIC event = 6 at time = 1874.3 yr*

*\*\*\* failed WPs: 6 out of 760 \*\*\**

*exec: calling ebsrel*

*Highest release rates from Sub Area 5*

*Tc99 3.1121E-03 [Ci/yr/SA] at 3.665E+03 yr*

*C14 1.6443E-03 [Ci/yr/SA] at 3.665E+03 yr*

*Cs135 5.7765E-04 [Ci/yr/SA] at 3.665E+03 yr*

*Se79 4.9303E-04 [Ci/yr/SA] at 3.665E+03 yr*

*Ni59 1.1519E-04 [Ci/yr/SA] at 3.774E+03 yr*

*Am243 5.7513E-05 [Ci/yr/SA] at 1.347E+04 yr*

*exec: calling uzft*

*Highest release rates from UZ*

*Tc99 1.1536E-03 [Ci/yr/SA] at 4.235E+03 yr*

*Se79 2.1428E-05 [Ci/yr/SA] at 1.854E+04 yr*

*I129 1.4006E-05 [Ci/yr/SA] at 4.235E+03 yr*

*Cl36 8.7275E-06 [Ci/yr/SA] at 4.235E+03 yr*

*Cs135 5.7340E-06 [Ci/yr/SA] at 3.722E+04 yr*

*Cm245 5.3459E-06 [Ci/yr/SA] at 4.483E+03 yr*

*exec: calling szft*

*Highest release rates from SZ*

*Tc99 6.5663E-04 [Ci/yr/SA] at 9.713E+03 yr*

*I129 8.8267E-06 [Ci/yr/SA] at 6.233E+03 yr*

*Cl36 5.6528E-06 [Ci/yr/SA] at 5.595E+03 yr*

*Se79 4.8302E-06 [Ci/yr/SA] at 3.384E+04 yr*

*U234 2.2045E-08 [Ci/yr/SA] at 9.323E+04 yr*

*U238 6.8685E-09 [Ci/yr/SA] at 9.769E+04 yr*

---

*subarea 6 of 8 realization 1 of 1*

---

*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

*\*\*\* No Corrosion WP Failure \*\*\**

*exec: failed WPs from VOLCANIC event = 1 at time = 1874.3 yr*

*\*\*\* failed WPs: 1 out of 851 \*\*\**

*exec: calling ebsrel*

*Highest release rates from Sub Area 6*

*Tc99 8.5525E-04 [Ci/yr/SA] at 3.774E+03 yr*

*C14 4.2134E-04 [Ci/yr/SA] at 3.774E+03 yr*

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*Cs135 1.5044E-04 [Ci/yr/SA] at 3.774E+03 yr  
Se79 1.2839E-04 [Ci/yr/SA] at 3.774E+03 yr  
Ni59 3.6496E-05 [Ci/yr/SA] at 3.774E+03 yr  
I129 1.0029E-05 [Ci/yr/SA] at 3.774E+03 yr*

*exec: calling uzft*

*Highest release rates from UZ*

*Tc99 2.0975E-04 [Ci/yr/SA] at 4.235E+03 yr  
I129 2.4580E-06 [Ci/yr/SA] at 4.235E+03 yr  
Se79 1.6786E-06 [Ci/yr/SA] at 2.540E+04 yr  
Cl36 1.5245E-06 [Ci/yr/SA] at 4.235E+03 yr  
Cs135 1.4471E-06 [Ci/yr/SA] at 3.812E+04 yr  
Cm245 7.2552E-07 [Ci/yr/SA] at 4.483E+03 yr*

*exec: calling szft*

*Highest release rates from SZ*

*Tc99 1.3859E-04 [Ci/yr/SA] at 9.713E+03 yr  
I129 1.7363E-06 [Ci/yr/SA] at 6.402E+03 yr  
Cl36 1.0799E-06 [Ci/yr/SA] at 5.595E+03 yr  
Se79 7.1985E-07 [Ci/yr/SA] at 3.997E+04 yr  
U234 3.5952E-09 [Ci/yr/SA] at 9.543E+04 yr  
U238 1.1288E-09 [Ci/yr/SA] at 1.000E+05 yr*

---

*subarea 7 of 8 realization 1 of 1*

---

*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

*\*\*\* No Corrosion WP Failure \*\*\**

*\*\*\* failed WPs: 0 out of 323 \*\*\**

*exec: calling ebsrel*

*There is no EBS release*

*exec: calling uzft*

*There is no UZ release*

*exec: calling szft*

*There is no SZ release*

---

*subarea 8 of 8 realization 1 of 1*

---

*exec: calling uzflow*

*exec: calling nfenv*

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*exec: calling ebsfail*

\*\*\* No Corrosion WP Failure \*\*\*

*exec: failed WPs from VOLCANIC event = 2 at time = 1874.3 yr*

\*\*\* failed WPs: 2 out of 814 \*\*\*

*exec: calling ebsrel*

Highest release rates from Sub Area 8

Tc99 1.3483E-03 [Ci/yr/SA] at 3.774E+03 yr

C14 6.7689E-04 [Ci/yr/SA] at 3.774E+03 yr

Cs135 2.4292E-04 [Ci/yr/SA] at 3.774E+03 yr

Se79 2.0733E-04 [Ci/yr/SA] at 3.774E+03 yr

Ni59 5.2470E-05 [Ci/yr/SA] at 3.774E+03 yr

Am243 1.7838E-05 [Ci/yr/SA] at 1.451E+04 yr

*exec: calling uzft*

\*\*\* NEFTRAN is skipped for this UZ path since no layers have significant ground water travel time. \*\*\*

Highest release rates from UZ

Tc99 1.3483E-03 [Ci/yr/SA] at 3.774E+03 yr

Cs135 2.4292E-04 [Ci/yr/SA] at 3.774E+03 yr

Se79 2.0733E-04 [Ci/yr/SA] at 3.774E+03 yr

Ni59 5.2470E-05 [Ci/yr/SA] at 3.774E+03 yr

Am243 1.7838E-05 [Ci/yr/SA] at 1.451E+04 yr

I129 1.6195E-05 [Ci/yr/SA] at 3.774E+03 yr

*exec: calling szft*

Highest release rates from SZ

Tc99 1.9776E-04 [Ci/yr/SA] at 8.113E+03 yr

I129 2.7996E-06 [Ci/yr/SA] at 5.444E+03 yr

Cl36 1.8024E-06 [Ci/yr/SA] at 4.876E+03 yr

Se79 1.0439E-06 [Ci/yr/SA] at 9.713E+03 yr

Np237 3.1761E-07 [Ci/yr/SA] at 1.000E+05 yr

U234 6.2571E-09 [Ci/yr/SA] at 8.293E+04 yr

*exec: calling dcagw*

Highest annual dose GW pathway

I129 2.2483E-02 [mrem/yr] at 6.233E+03 yr

Np237 2.0728E-03 [mrem/yr] at 1.000E+05 yr

Tc99 1.3839E-03 [mrem/yr] at 8.113E+03 yr

Cl36 3.2565E-04 [mrem/yr] at 5.444E+03 yr

Se79 2.3009E-04 [mrem/yr] at 3.227E+04 yr

U234 8.9509E-06 [mrem/yr] at 7.730E+04 yr

At end of TPI, annual dose GW pathway

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```
Np237 2.0728E-03 [mrem/yr]
I129 1.2435E-04 [mrem/yr]
Se79 3.4523E-05 [mrem/yr]
Tc99 3.1601E-05 [mrem/yr]
U234 5.2857E-06 [mrem/yr]
U238 1.5227E-06 [mrem/yr]
sum 2.2709E-03 [mrem/yr]
```

*exec: calling ashplumo*

*exec: calling ashrmovo*

*exec: calling dcags*

*Highest annual dose from GS*

```
Pu240 1.4890E+02 [mrem/yr] at 1.874E+03 yr
Pu239 1.1573E+02 [mrem/yr] at 1.874E+03 yr
Am241 8.6800E+01 [mrem/yr] at 1.874E+03 yr
Am243 7.4940E+00 [mrem/yr] at 1.874E+03 yr
Pu242 6.6144E-01 [mrem/yr] at 1.874E+03 yr
Np237 5.9537E-01 [mrem/yr] at 1.874E+03 yr
```

*exec: end realizations*

*exec: Run Successfully Completed*

---

---

The ratio of the peak dose in the year of the eruption in rgssa.tpa was compared, and was noted to be 75, which is correct because the user distribution model released 75 waste packages and the geometric model released 1.

Results: The test was completed successfully. The files that were used for this test (rgssa.tpa.1, rgssa.tpa.2, screen.out.1, screen.out.2, tpa.inp.1, and tpa.inp.2) are located in the directory:

/home/jweldy/tpa40m/TEST/311/test1

## Test 2

This test will make sure that the code properly uses the input values for number of WPs failed and ejected by a volcanic event when user specified parameters are used. One single realization was run for this test. For the realization, the number of WPs ejected is 10 and the number of WPs failed is 30. The screen output will be examined to ensure that the proper number of WPs are reported as having been failed and ejected by the

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volcanic event. Files needed for testing include tpa.inp and screen.out (a capture of the screen output) for the realization.

Output from screen.out:

```
=====
=====
exec: Welcome to TPA Version 4.0betaM
Job started: Mon Jun 19 13:53:47 2000
=====
=====
REPOSITORY DESIGN INFORMATION
Subarea Area Waste Number of WP
# [m^2] [MTU]
1 723591.3 14200.8 1455
2 784763.0 15303.7 1568
3 390372.0 7564.0 775
4 207581.3 4157.8 426
5 378972.8 7417.6 760
6 424872.5 8305.8 851
7 163938.3 3152.5 323
8 393468.9 7944.6 814

Total Area [acre] = 856.82238463061
Total Buried Waste [MTU] = 68046.720000000
Repository AML [MTU/acre] = 79.417532992367
```

*Specified Global Parameters:*

Compliance Period = 100000.0 (yr)  
Maximum Simulation Time = 100000.0 (yr)  
Number Of Realizations = 1  
Number Of Subareas = 8  
Volcanism scenario = 1 (yes=1, no=0)  
Faulting scenario = 0 (yes=1, no=0)  
Seismic scenario = 1 (yes=1, no=0)  
Distance to Receptor Group = 20.0 (km)

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\*\*>>> CAUTION: CHECKING OF NUCLIDES AND CHAINS IS DISABLED  
    <<<\*\*

\*\*>>> You may not be using the standard chains specified <<<\*\*

\*\*>>> in the invent module.                          <<<\*\*

\*\*>>> (see "CheckNuclidesAndChains(yes=1,no=0)" in tpa.inp)<<<\*\*

\*\*\*>>> NOTE: When running with volcanism, verify that <<<\*\*\*

\*\*\*>>> the maximum value of the PDF for parameter <<<\*\*\*

\*\*\*>>> TimeOfNextVolcanicEventinRegionOfInterest[yr] is <<<\*\*\*

\*\*\*>>> equal to the parameter MaximumTime[yr].          <<<\*\*\*

The specified path for data = \$TPA\_DATA/

The specified path for codes = \$TPA\_TEST/

\*\*To modify global parameters or the path, stop code execution using  
control-C\*\*

\*\*\*>>> WARNING: THE APPEND OPTION IS SELECTED <<<\*\*\*

(see "OutputMode(0=None,1=All,2=UserDefined)" in tpa.inp)

For "SelectAppendFiles", a value of 0 (all append files) was set in tpa.inp.

By selecting this option, files are written which may require 6 megs of disk  
space.

(more disk space could be needed)

---

-----  
subarea 1 of 8 realization 1 of 1

---

exec: calling uzflow

exec: calling nfenv

exec: calling ebsfail

\*\*\* No Corrosion WP Failure \*\*\*

exec: calling seismo

exec: calling volcano

\*\*\* failed WPs: 0 out of 1455 \*\*\*

exec: calling ebsrel

There is no EBS release

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exec: calling uzft

*There is no UZ release*

exec: calling szft

*There is no SZ release*

---

subarea 2 of 8 realization 1 of 1

---

exec: calling uzflow

exec: calling nfenv

exec: calling ebsfail

\*\*\* No Corrosion WP Failure \*\*\*

exec: failed WPs from VOLCANIC event = 40 at time = 1874.3 yr  
(includes ejected WPs)

exec: failed WPs from INITIAL event = 1 at time = 4875.7 yr

\*\*\* failed WPs: 41 out of 1568 \*\*\*

\*\*\* ejected WPs: 10

exec: calling ebsrel

Highest release rates from Sub Area 2

Tc99 2.9040E-02 [Ci/yr/SA] at 3.665E+03 yr

C14 1.4147E-02 [Ci/yr/SA] at 3.665E+03 yr

Cs135 5.0379E-03 [Ci/yr/SA] at 3.665E+03 yr

Se79 4.2999E-03 [Ci/yr/SA] at 3.665E+03 yr

Ni59 1.3008E-03 [Ci/yr/SA] at 3.665E+03 yr

Am243 3.4689E-04 [Ci/yr/SA] at 1.451E+04 yr

exec: calling uzft

\*\*\* NEFTRAN is skipped for this UZ path since no layers have significant ground water travel time. \*\*\*

Highest release rates from UZ

Tc99 2.9040E-02 [Ci/yr/SA] at 3.665E+03 yr

Cs135 5.0379E-03 [Ci/yr/SA] at 3.665E+03 yr

Se79 4.2999E-03 [Ci/yr/SA] at 3.665E+03 yr

Ni59 1.3008E-03 [Ci/yr/SA] at 3.665E+03 yr

Am243 3.4689E-04 [Ci/yr/SA] at 1.451E+04 yr

I129 3.3586E-04 [Ci/yr/SA] at 3.665E+03 yr

exec: calling szft

Highest release rates from SZ

Tc99 3.8511E-03 [Ci/yr/SA] at 8.113E+03 yr

I129 4.9833E-05 [Ci/yr/SA] at 5.444E+03 yr

Cl36 3.3526E-05 [Ci/yr/SA] at 4.742E+03 yr

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*Se79 1.9206E-05 [Ci/yr/SA] at 9.713E+03 yr  
Np237 6.3268E-06 [Ci/yr/SA] at 1.000E+05 yr  
U234 1.2071E-07 [Ci/yr/SA] at 8.293E+04 yr*

---

*subarea 3 of 8 realization 1 of 1*

---

*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

*\*\*\* No Corrosion WP Failure \*\*\**

*\*\*\* failed WPs: 0 out of 775 \*\*\**

*exec: calling ebsrel*

*There is no EBS release*

*exec: calling uzft*

*There is no UZ release*

*exec: calling szft*

*There is no SZ release*

---

*subarea 4 of 8 realization 1 of 1*

---

*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

*\*\*\* No Corrosion WP Failure \*\*\**

*\*\*\* failed WPs: 0 out of 426 \*\*\**

*exec: calling ebsrel*

*There is no EBS release*

*exec: calling uzft*

*There is no UZ release*

*exec: calling szft*

*There is no SZ release*

---

*subarea 5 of 8 realization 1 of 1*

---

*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

*\*\*\* No Corrosion WP Failure \*\*\**

*\*\*\* failed WPs: 0 out of 760 \*\*\**

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*exec: calling ebsrel*

*There is no EBS release*

*exec: calling uzft*

*There is no UZ release*

*exec: calling szft*

*There is no SZ release*

---

*subarea 6 of 8 realization 1 of 1*

---

*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

*\*\*\* No Corrosion WP Failure \*\*\**

*\*\*\* failed WPs: 0 out of 851 \*\*\**

*exec: calling ebsrel*

*There is no EBS release*

*exec: calling uzft*

*There is no UZ release*

*exec: calling szft*

*There is no SZ release*

---

*subarea 7 of 8 realization 1 of 1*

---

*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

*\*\*\* No Corrosion WP Failure \*\*\**

*\*\*\* failed WPs: 0 out of 323 \*\*\**

*exec: calling ebsrel*

*There is no EBS release*

*exec: calling uzft*

*There is no UZ release*

*exec: calling szft*

*There is no SZ release*

---

*subarea 8 of 8 realization 1 of 1*

---

*exec: calling uzflow*

*exec: calling nfenv*

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*exec: calling ebsfail*

\*\*\* No Corrosion WP Failure \*\*\*

\*\*\* failed WPs: 0 out of 814 \*\*\*

*exec: calling ebsrel*

There is no EBS release

*exec: calling uzft*

There is no UZ release

*exec: calling szft*

There is no SZ release

*exec: calling dcagw*

Highest annual dose GW pathway

I129 6.3078E-02 [mrem/yr] at 5.444E+03 yr

Np237 6.5408E-03 [mrem/yr] at 1.000E+05 yr

Tc99 3.9928E-03 [mrem/yr] at 8.113E+03 yr

Cl36 8.9611E-04 [mrem/yr] at 4.742E+03 yr

Se79 3.8170E-04 [mrem/yr] at 1.314E+04 yr

U234 1.4642E-05 [mrem/yr] at 7.730E+04 yr

At end of TPI, annual dose GW pathway

Np237 6.5408E-03 [mrem/yr]

I129 1.8363E-04 [mrem/yr]

Se79 5.4407E-05 [mrem/yr]

Tc99 4.6745E-05 [mrem/yr]

U234 7.7427E-06 [mrem/yr]

U238 2.2173E-06 [mrem/yr]

sum 6.8368E-03 [mrem/yr]

*exec: calling ashplumo*

*exec: calling ashrmovo*

*exec: calling dcags*

Highest annual dose from GS

Pu240 2.6130E+04 [mrem/yr] at 1.874E+03 yr

Pu239 2.0309E+04 [mrem/yr] at 1.874E+03 yr

Am241 1.5243E+04 [mrem/yr] at 1.874E+03 yr

Am243 1.3172E+03 [mrem/yr] at 1.874E+03 yr

Pu242 1.1606E+02 [mrem/yr] at 1.874E+03 yr

Np237 1.0595E+02 [mrem/yr] at 1.874E+03 yr

*exec: end realizations*

*exec: Run Successfully Completed*

---

---

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Results: The screen output indicates that the correct number of waste packages  
are failed and ejected. The files used for this test (screen.out, tpa.inp) are  
located in the following directory:

/home/jweldy/tpa40m/TEST/311/test2

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Test 3

This test will make sure that the code puts the volcanic event in the correct subarea as specified in the input file when user specified parameters are used. Two single realizations were run for this test. For the first realization, the number of WPs ejected is 10 and the number of WPs failed is 30. The subarea in which the event occurs is changed from the base value of 2 to the test value of 3. The second realization is the same as the first, but the switch is returned to the geometric value to ensure that the code does not place the volcano in subarea 3 using this model. The screen output will be examined to ensure that the WPs are failed in the proper subarea. Additionally, the file uzft.ech will be examined to ensure that the release of radionuclides to subarea 3 is larger than the other subareas, since more WPs have failed in that subarea. Files needed for testing include tpa.inp and screen.out (a capture of the screen output) for the realization.

The screen output for the first run looked as follows:

```
=====
=====
exec: Welcome to TPA Version 4.0betaM
Job started: Mon Jun 19 16:00:45 2000
=====
=====
REPOSITORY DESIGN INFORMATION
Subarea Area Waste Number of WP
# [m^2] [MTU]
1 723591.3 14200.8 1455
2 784763.0 15303.7 1568
3 390372.0 7564.0 775
4 207581.3 4157.8 426
5 378972.8 7417.6 760
6 424872.5 8305.8 851
7 163938.3 3152.5 323
8 393468.9 7944.6 814

Total Area [acre]      = 856.82238463061
Total Buried Waste [MTU] = 68046.7200000000
Repository AML [MTU/acre] = 79.417532992367
```

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*Specified Global Parameters:*

Compliance Period = 10000.0 (yr)  
Maximum Simulation Time = 10000.0 (yr)  
Number Of Realizations = 1  
Number Of Subareas = 8  
Volcanism scenario = 1 (yes=1, no=0)  
Faulting scenario = 0 (yes=1, no=0)  
Seismic scenario = 1 (yes=1, no=0)  
Distance to Receptor Group = 20.0 (km)

\*\*\*>>> CAUTION: CHECKING OF NUCLIDES AND CHAINS IS DISABLED <<<\*\*

\*\*\*>>> You may not be using the standard chains specified <<<\*\*

\*\*\*>>> in the invent module. <<<\*\*

\*\*\*>>> (see "CheckNuclidesAndChains(yes=1,no=0)" in tpa.inp)<<<\*\*

\*\*\*>>> NOTE: When running with volcanism, verify that <<<\*\*\*

\*\*\*>>> the maximum value of the PDF for parameter <<<\*\*\*

\*\*\*>>> TimeOfNextVolcanicEventinRegionOfInterest[yr] is <<<\*\*\*

\*\*\*>>> equal to the parameter MaximumTime[yr]. <<<\*\*\*

The specified path for data = \$TPA\_DATA/

The specified path for codes = \$TPA\_TEST/

\*\*To modify global parameters or the path, stop code execution using control-C\*\*

\*\*\*>>> WARNING: THE APPEND OPTION IS SELECTED <<<\*\*\*

(see "OutputMode(0=None,1=All,2=UserDefined)" in tpa.inp)

For "SelectAppendFiles", a value of 0 (all append files) was set in tpa.inp.

By selecting this option, files are written which may require 6 megs of disk space.  
(more disk space could be needed)

---

-----  
subarea 1 of 8 realization 1 of 1

---

exec: calling uzflow

exec: calling nfenv

exec: calling ebsfail

\*\*\* No Corrosion WP Failure \*\*\*

exec: calling seismo

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*exec: calling volcano*

\*\*\* failed WPs: 0 out of 1455 \*\*\*

*exec: calling ebsrel*

*There is no EBS release*

*exec: calling uzft*

*There is no UZ release*

*exec: calling szft*

*There is no SZ release*

---

subarea 2 of 8 realization 1 of 1

---

*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

\*\*\* No Corrosion WP Failure \*\*\*

*exec: failed WPs from INITIAL event = 1 at time = 4945.1 yr*

\*\*\* failed WPs: 1 out of 1568 \*\*\*

*exec: calling ebsrel*

*Highest release rates from Sub Area 2*

Tc99 6.8075E-05 [Ci/yr/SA] at 8.101E+03 yr

C14 2.0837E-05 [Ci/yr/SA] at 8.101E+03 yr

Cs135 1.2523E-05 [Ci/yr/SA] at 8.101E+03 yr

Se79 1.0674E-05 [Ci/yr/SA] at 8.101E+03 yr

Am243 8.0686E-06 [Ci/yr/SA] at 1.000E+04 yr

Ni59 2.5015E-06 [Ci/yr/SA] at 8.101E+03 yr

*exec: calling uzft*

\*\*\* NEFTRAN is skipped for this UZ path since no layers have significant ground water travel time. \*\*\*

*Highest release rates from UZ*

Tc99 6.8075E-05 [Ci/yr/SA] at 8.101E+03 yr

Cs135 1.2523E-05 [Ci/yr/SA] at 8.101E+03 yr

Se79 1.0674E-05 [Ci/yr/SA] at 8.101E+03 yr

Am243 8.0686E-06 [Ci/yr/SA] at 1.000E+04 yr

Ni59 2.5015E-06 [Ci/yr/SA] at 8.101E+03 yr

Pu239 1.3068E-06 [Ci/yr/SA] at 1.000E+04 yr

*exec: calling szft*

*Highest release rates from SZ*

I129 4.1998E-07 [Ci/yr/SA] at 1.000E+04 yr

C136 3.5321E-07 [Ci/yr/SA] at 1.000E+04 yr

U234 8.4551E-17 [Ci/yr/SA] at 1.000E+04 yr

U238 2.0439E-17 [Ci/yr/SA] at 1.000E+04 yr

Np237 2.6563E-18 [Ci/yr/SA] at 1.000E+04 yr

Th230 1.4160E-23 [Ci/yr/SA] at 1.000E+04 yr

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---

*subarea 3 of 8 realization 1 of 1*

---

*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

*\*\*\* No Corrosion WP Failure \*\*\**

***exec: failed WPs from VOLCANIC event = 40 at time = 1900.0 yr***

*\*\*\* failed WPs: 40 out of 775 \*\*\**

*\*\*\* ejected WPs: 10*

*exec: calling ebsrel*

*Highest release rates from Sub Area 3*

*Tc99 2.6053E-02 [Ci/yr/SA] at 3.722E+03 yr*

*C14 1.2423E-02 [Ci/yr/SA] at 3.722E+03 yr*

*Cs135 4.4652E-03 [Ci/yr/SA] at 3.722E+03 yr*

*Se79 3.8109E-03 [Ci/yr/SA] at 3.722E+03 yr*

*Ni59 1.2156E-03 [Ci/yr/SA] at 3.722E+03 yr*

*I129 2.9767E-04 [Ci/yr/SA] at 3.722E+03 yr*

*exec: calling uzft*

*Highest release rates from UZ*

*Tc99 8.2281E-03 [Ci/yr/SA] at 4.191E+03 yr*

*I129 9.2408E-05 [Ci/yr/SA] at 4.191E+03 yr*

*Cl36 5.6999E-05 [Ci/yr/SA] at 4.191E+03 yr*

*Cm245 5.2683E-05 [Ci/yr/SA] at 4.394E+03 yr*

*Cm246 8.2421E-06 [Ci/yr/SA] at 4.394E+03 yr*

*Nb94 9.5308E-07 [Ci/yr/SA] at 1.000E+04 yr*

*exec: calling szft*

*Highest release rates from SZ*

*Tc99 3.1168E-03 [Ci/yr/SA] at 8.691E+03 yr*

*I129 3.8339E-05 [Ci/yr/SA] at 5.971E+03 yr*

*Cl36 2.3925E-05 [Ci/yr/SA] at 5.308E+03 yr*

*U238 7.7831E-17 [Ci/yr/SA] at 1.000E+04 yr*

*Np237 5.5218E-17 [Ci/yr/SA] at 1.000E+04 yr*

*The remaining 15 nuclide(s) have zero release*

---

*subarea 4 of 8 realization 1 of 1*

---

*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

*\*\*\* No Corrosion WP Failure \*\*\**

*\*\*\* failed WPs: 0 out of 426 \*\*\**

*exec: calling ebsrel*

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*There is no EBS release*

*exec: calling uzft*

*There is no UZ release*

*exec: calling szft*

*There is no SZ release*

---

subarea 5 of 8 realization 1 of 1

---

*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

*\*\*\* No Corrosion WP Failure \*\*\**

*\*\*\* failed WPs: 0 out of 760 \*\*\**

*exec: calling ebsrel*

*There is no EBS release*

*exec: calling uzft*

*There is no UZ release*

*exec: calling szft*

*There is no SZ release*

---

subarea 6 of 8 realization 1 of 1

---

*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

*\*\*\* No Corrosion WP Failure \*\*\**

*\*\*\* failed WPs: 0 out of 851 \*\*\**

*exec: calling ebsrel*

*There is no EBS release*

*exec: calling uzft*

*There is no UZ release*

*exec: calling szft*

*There is no SZ release*

---

subarea 7 of 8 realization 1 of 1

---

*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

*\*\*\* No Corrosion WP Failure \*\*\**

*\*\*\* failed WPs: 0 out of 323 \*\*\**

*exec: calling ebsrel*

*There is no EBS release*

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*exec: calling uzft*

*There is no UZ release*

*exec: calling szft*

*There is no SZ release*

---

*subarea 8 of 8 realization 1 of 1*

---

*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

*\*\*\* No Corrosion WP Failure \*\*\**

*\*\*\* failed WPs: 0 out of 814 \*\*\**

*exec: calling ebsrel*

*There is no EBS release*

*exec: calling uzft*

*There is no UZ release*

*exec: calling szft*

*There is no SZ release*

*exec: calling dcagw*

*Highest annual dose GW pathway*

*I129 4.8529E-02 [mrem/yr] at 5.971E+03 yr*

*Tc99 3.2315E-03 [mrem/yr] at 8.691E+03 yr*

*Cl36 6.3948E-04 [mrem/yr] at 5.308E+03 yr*

*Np237 5.9832E-14 [mrem/yr] at 1.000E+04 yr*

*U238 6.9055E-15 [mrem/yr] at 1.000E+04 yr*

*U234 6.4747E-15 [mrem/yr] at 1.000E+04 yr*

*At end of TPI, annual dose GW pathway*

*I129 1.4276E-03 [mrem/yr]*

*Tc99 9.2041E-04 [mrem/yr]*

*Cl36 1.4622E-05 [mrem/yr]*

*Np237 5.9832E-14 [mrem/yr]*

*U238 6.9055E-15 [mrem/yr]*

*U234 6.4747E-15 [mrem/yr]*

*sum 2.3626E-03 [mrem/yr]*

*exec: calling ashplumo*

*exec: calling ashrmovo*

*exec: calling dcags*

*Highest annual dose from GS*

*Pu240 2.6059E+04 [mrem/yr] at 1.900E+03 yr*

*Pu239 2.0295E+04 [mrem/yr] at 1.900E+03 yr*

*Am241 1.4628E+04 [mrem/yr] at 1.900E+03 yr*

*Am243 1.3140E+03 [mrem/yr] at 1.900E+03 yr*

*Pu242 1.1605E+02 [mrem/yr] at 1.900E+03 yr*

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*Np237 1.0610E+02 [mrem/yr] at 1.900E+03 yr  
exec: end realizations*

*exec: Run Successfully Completed*

---

Therefore, it appears that the input value to move the volcanic event from subarea to subarea is working correctly. The second test was run to ensure that the geometric model still placed the volcano at the center of the repository, i.e., in subarea two.

=====

=====

*exec: Welcome to TPA Version 4.0betaM*

*Job started: Mon Jun 19 16:30:23 2000*

=====

=====

#### *REPOSITORY DESIGN INFORMATION*

*Subarea Area Waste Number of WP*

#	[m <sup>2</sup> ]	[MTU]	
1	723591.3	14200.8	1455
2	784763.0	15303.7	1568
3	390372.0	7564.0	775
4	207581.3	4157.8	426
5	378972.8	7417.6	760
6	424872.5	8305.8	851
7	163938.3	3152.5	323
8	393468.9	7944.6	814

*Total Area [acre] = 856.82238463061*

*Total Buried Waste [MTU] = 68046.720000000*

*Repository AML [MTU/acre] = 79.417532992367*

*Specified Global Parameters:*

*Compliance Period = 10000.0 (yr)*

*Maximum Simulation Time = 10000.0 (yr)*

*Number Of Realizations = 1*

*Number Of Subareas = 8*

*Volcanism scenario = 1 (yes=1, no=0)*

*Faulting scenario = 0 (yes=1, no=0)*

*Seismic scenario = 1 (yes=1, no=0)*

*Distance to Receptor Group = 20.0 (km)*

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\*\*\*>>> CAUTION: CHECKING OF NUCLIDES AND CHAINS IS DISABLED <<<\*\*  
\*\*\*>>> You may not be using the standard chains specified <<<\*\*  
\*\*\*>>> in the invent module. <<<\*\*  
\*\*\*>>> (see "CheckNuclidesAndChains(yes=1,no=0)" in tpa.inp)<<<\*\*

\*\*\*>>> NOTE: When running with volcanism, verify that <<<\*\*\*  
\*\*\*>>> the maximum value of the PDF for parameter <<<\*\*\*  
\*\*\*>>> TimeOfNextVolcanicEventinRegionOfInterest[yr] is <<<\*\*\*  
\*\*\*>>> equal to the parameter MaximumTime[yr]. <<<\*\*\*

The specified path for data = \$TPA\_DATA/  
The specified path for codes = \$TPA\_TEST/

\*\*To modify global parameters or the path, stop code execution using control-C\*\*

\*\*\*>>> WARNING: THE APPEND OPTION IS SELECTED <<<\*\*\*  
(see "OutputMode(0=None,1=All,2=UserDefined)" in tpa.inp)  
For "SelectAppendFiles", a value of 0 (all append files) was set in tpa.inp.  
By selecting this option, files are written which may require 6 megs of disk space.  
(more disk space could be needed)

---

-----  
subarea 1 of 8 realization 1 of 1

---

exec: calling uzflow  
exec: calling nfenv  
exec: calling ebsfail  
    \*\*\* No Corrosion WP Failure \*\*\*  
exec: calling seismo  
exec: calling volcano  
    \*\*\* failed WPs: 0 out of 1455 \*\*\*  
exec: calling ebsrel

    There is no EBS release

exec: calling uzft

    There is no UZ release

exec: calling szft

    There is no SZ release

---

-----  
subarea 2 of 8 realization 1 of 1

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---

*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

\*\*\* No Corrosion WP Failure \*\*\*

**exec: failed WPs from VOLCANIC event = 9 at time = 1900.0 yr (includes ejected WPs)**

*exec: failed WPs from INITIAL event = 1 at time = 4945.1 yr*

\*\*\* failed WPs: 10 out of 1568 \*\*\*

\*\*\* ejected WPs: 1

*exec: calling ebsrel*

Highest release rates from Sub Area 2

Tc99 7.1951E-03 [Ci/yr/SA] at 3.722E+03 yr

C14 3.5236E-03 [Ci/yr/SA] at 3.722E+03 yr

Cs135 1.2546E-03 [Ci/yr/SA] at 3.722E+03 yr

Se79 1.0709E-03 [Ci/yr/SA] at 3.722E+03 yr

Ni59 3.1659E-04 [Ci/yr/SA] at 3.722E+03 yr

I129 8.3644E-05 [Ci/yr/SA] at 3.722E+03 yr

*exec: calling uzft*

\*\*\* NEFTRAN is skipped for this UZ path since no layers have significant ground water travel time. \*\*\*

Highest release rates from UZ

Tc99 7.1951E-03 [Ci/yr/SA] at 3.722E+03 yr

Cs135 1.2546E-03 [Ci/yr/SA] at 3.722E+03 yr

Se79 1.0709E-03 [Ci/yr/SA] at 3.722E+03 yr

Ni59 3.1659E-04 [Ci/yr/SA] at 3.722E+03 yr

I129 8.3644E-05 [Ci/yr/SA] at 3.722E+03 yr

Am243 7.2664E-05 [Ci/yr/SA] at 1.000E+04 yr

*exec: calling szft*

Highest release rates from SZ

Tc99 1.1249E-03 [Ci/yr/SA] at 8.101E+03 yr

I129 1.5118E-05 [Ci/yr/SA] at 5.434E+03 yr

Cl36 9.8699E-06 [Ci/yr/SA] at 4.830E+03 yr

Se79 5.7029E-06 [Ci/yr/SA] at 9.769E+03 yr

U234 2.6837E-12 [Ci/yr/SA] at 1.000E+04 yr

U238 6.4881E-13 [Ci/yr/SA] at 1.000E+04 yr

---

subarea 3 of 8 realization 1 of 1

---

*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

\*\*\* No Corrosion WP Failure \*\*\*

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*exec: failed WPs from VOLCANIC event = 2 at time = 1900.0 yr*

*\*\*\* failed WPs: 2 out of 775 \*\*\**

*exec: calling ebsrel*

*Highest release rates from Sub Area 3*

*Tc99 1.7368E-03 [Ci/yr/SA] at 3.722E+03 yr*

*C14 8.2822E-04 [Ci/yr/SA] at 3.722E+03 yr*

*Cs135 2.9767E-04 [Ci/yr/SA] at 3.722E+03 yr*

*Se79 2.5406E-04 [Ci/yr/SA] at 3.722E+03 yr*

*Ni59 8.1041E-05 [Ci/yr/SA] at 3.722E+03 yr*

*I129 1.9845E-05 [Ci/yr/SA] at 3.722E+03 yr*

*exec: calling uzft*

*Highest release rates from UZ*

*Tc99 5.4854E-04 [Ci/yr/SA] at 4.191E+03 yr*

*I129 6.1606E-06 [Ci/yr/SA] at 4.191E+03 yr*

*Cl36 3.7999E-06 [Ci/yr/SA] at 4.191E+03 yr*

*Cm245 3.5123E-06 [Ci/yr/SA] at 4.394E+03 yr*

*Cm246 5.4948E-07 [Ci/yr/SA] at 4.394E+03 yr*

*Nb94 6.3539E-08 [Ci/yr/SA] at 1.000E+04 yr*

*exec: calling szft*

*Highest release rates from SZ*

*Tc99 2.0778E-04 [Ci/yr/SA] at 8.691E+03 yr*

*I129 2.5559E-06 [Ci/yr/SA] at 5.971E+03 yr*

*Cl36 1.5949E-06 [Ci/yr/SA] at 5.308E+03 yr*

*U238 5.1888E-18 [Ci/yr/SA] at 1.000E+04 yr*

*Np237 3.6813E-18 [Ci/yr/SA] at 1.000E+04 yr*

*The remaining 15 nuclide(s) have zero release*

---

*subarea 4 of 8 realization 1 of 1*

---

*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

*\*\*\* No Corrosion WP Failure \*\*\**

*exec: failed WPs from VOLCANIC event = 1 at time = 1900.0 yr*

*\*\*\* failed WPs: 1 out of 426 \*\*\**

*exec: calling ebsrel*

*Highest release rates from Sub Area 4*

*Tc99 9.4339E-04 [Ci/yr/SA] at 3.722E+03 yr*

*C14 4.7234E-04 [Ci/yr/SA] at 3.722E+03 yr*

*Cs135 1.6882E-04 [Ci/yr/SA] at 3.722E+03 yr*

*Se79 1.4408E-04 [Ci/yr/SA] at 3.722E+03 yr*

*Ni59 3.7721E-05 [Ci/yr/SA] at 3.722E+03 yr*

*I129 1.1255E-05 [Ci/yr/SA] at 3.722E+03 yr*

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exec: calling uzft

Highest release rates from UZ

Tc99 3.8490E-04 [Ci/yr/SA] at 4.093E+03 yr  
I129 4.5435E-06 [Ci/yr/SA] at 4.093E+03 yr  
Cl36 2.8218E-06 [Ci/yr/SA] at 4.093E+03 yr  
Cm245 1.2655E-06 [Ci/yr/SA] at 4.291E+03 yr  
Cm246 2.0277E-07 [Ci/yr/SA] at 4.291E+03 yr  
Nb94 2.9851E-08 [Ci/yr/SA] at 1.000E+04 yr

exec: calling szft

Highest release rates from SZ

Tc99 1.2191E-04 [Ci/yr/SA] at 8.490E+03 yr  
I129 1.6238E-06 [Ci/yr/SA] at 5.832E+03 yr  
Cl36 1.0189E-06 [Ci/yr/SA] at 5.308E+03 yr  
U238 2.2530E-18 [Ci/yr/SA] at 1.000E+04 yr  
Np237 1.6293E-18 [Ci/yr/SA] at 1.000E+04 yr  
U234 9.5988E-21 [Ci/yr/SA] at 1.000E+04 yr

---

subarea 5 of 8 realization 1 of 1

---

exec: calling uzflow

exec: calling nfenv

exec: calling ebsfail

\*\*\* No Corrosion WP Failure \*\*\*

exec: failed WPs from VOLCANIC event = 6 at time = 1900.0 yr

\*\*\* failed WPs: 6 out of 760 \*\*\*

exec: calling ebsrel

Highest release rates from Sub Area 5

Tc99 4.3686E-03 [Ci/yr/SA] at 3.722E+03 yr  
C14 2.2904E-03 [Ci/yr/SA] at 3.722E+03 yr  
Cs135 8.1043E-04 [Ci/yr/SA] at 3.722E+03 yr  
Se79 6.9170E-04 [Ci/yr/SA] at 3.722E+03 yr  
Ni59 1.4929E-04 [Ci/yr/SA] at 3.722E+03 yr  
I129 5.4028E-05 [Ci/yr/SA] at 3.722E+03 yr

exec: calling uzft

Highest release rates from UZ

Tc99 1.5259E-03 [Ci/yr/SA] at 4.191E+03 yr  
I129 1.8748E-05 [Ci/yr/SA] at 4.191E+03 yr  
Cl36 1.1701E-05 [Ci/yr/SA] at 4.191E+03 yr  
Cm245 5.0716E-06 [Ci/yr/SA] at 4.499E+03 yr  
Cm246 7.8941E-07 [Ci/yr/SA] at 4.499E+03 yr  
Nb94 1.9503E-07 [Ci/yr/SA] at 1.000E+04 yr

exec: calling szft

Highest release rates from SZ

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Tc99 8.0113E-04 [Ci/yr/SA] at 9.543E+03 yr  
I129 1.0924E-05 [Ci/yr/SA] at 6.258E+03 yr  
Cl36 6.9980E-06 [Ci/yr/SA] at 5.564E+03 yr  
U238 4.9299E-18 [Ci/yr/SA] at 1.000E+04 yr  
Np237 2.8747E-18 [Ci/yr/SA] at 1.000E+04 yr

The remaining 15 nuclide(s) have zero release

---

subarea 6 of 8 realization 1 of 1

---

exec: calling uzflow

exec: calling nfenv

exec: calling ebsfail

\*\*\* No Corrosion WP Failure \*\*\*

exec: failed WPs from VOLCANIC event = 1 at time = 1900.0 yr

\*\*\* failed WPs: 1 out of 851 \*\*\*

exec: calling ebsrel

Highest release rates from Sub Area 6

Tc99 7.0265E-04 [Ci/yr/SA] at 3.722E+03 yr  
C14 3.5142E-04 [Ci/yr/SA] at 3.722E+03 yr  
Cs135 1.2489E-04 [Ci/yr/SA] at 3.722E+03 yr  
Se79 1.0659E-04 [Ci/yr/SA] at 3.722E+03 yr  
Ni59 2.8836E-05 [Ci/yr/SA] at 3.722E+03 yr  
I129 8.3256E-06 [Ci/yr/SA] at 3.722E+03 yr

exec: calling uzft

Highest release rates from UZ

Tc99 2.1550E-04 [Ci/yr/SA] at 4.291E+03 yr  
I129 2.5272E-06 [Ci/yr/SA] at 4.291E+03 yr  
Cl36 1.5674E-06 [Ci/yr/SA] at 4.291E+03 yr  
Cm245 7.6162E-07 [Ci/yr/SA] at 4.607E+03 yr  
Cm246 1.1768E-07 [Ci/yr/SA] at 4.607E+03 yr  
Nb94 3.1175E-08 [Ci/yr/SA] at 1.000E+04 yr

exec: calling szft

Highest release rates from SZ

Tc99 1.3451E-04 [Ci/yr/SA] at 9.769E+03 yr  
I129 1.6941E-06 [Ci/yr/SA] at 6.407E+03 yr  
Cl36 1.0628E-06 [Ci/yr/SA] at 5.696E+03 yr  
U238 7.5683E-19 [Ci/yr/SA] at 1.000E+04 yr  
Np237 4.3307E-19 [Ci/yr/SA] at 1.000E+04 yr

The remaining 15 nuclide(s) have zero release

---

subarea 7 of 8 realization 1 of 1

---

exec: calling uzflow

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*exec: calling nfenv*

*exec: calling ebsfail*

\*\*\* No Corrosion WP Failure \*\*\*

\*\*\* failed WPs: 0 out of 323 \*\*\*

*exec: calling ebsrel*

There is no EBS release

*exec: calling uzft*

There is no UZ release

*exec: calling szft*

There is no SZ release

---

subarea 8 of 8 realization 1 of 1

---

*exec: calling uzflow*

*exec: calling nfenv*

*exec: calling ebsfail*

\*\*\* No Corrosion WP Failure \*\*\*

*exec: failed WPs from VOLCANIC event = 2 at time = 1900.0 yr*

\*\*\* failed WPs: 2 out of 814 \*\*\*

*exec: calling ebsrel*

Highest release rates from Sub Area 8

Tc99 1.5992E-03 [Ci/yr/SA] at 3.722E+03 yr

C14 8.2342E-04 [Ci/yr/SA] at 3.722E+03 yr

Cs135 2.9291E-04 [Ci/yr/SA] at 3.722E+03 yr

Se79 2.5000E-04 [Ci/yr/SA] at 3.722E+03 yr

Ni59 5.7980E-05 [Ci/yr/SA] at 3.722E+03 yr

I129 1.9527E-05 [Ci/yr/SA] at 3.722E+03 yr

*exec: calling uzft*

\*\*\* NEFTRAN is skipped for this UZ path since no layers have significant ground water travel time. \*\*\*

Highest release rates from UZ

Tc99 1.5992E-03 [Ci/yr/SA] at 3.722E+03 yr

Cs135 2.9291E-04 [Ci/yr/SA] at 3.722E+03 yr

Se79 2.5000E-04 [Ci/yr/SA] at 3.722E+03 yr

Ni59 5.7980E-05 [Ci/yr/SA] at 3.722E+03 yr

I129 1.9527E-05 [Ci/yr/SA] at 3.722E+03 yr

Am243 1.2457E-05 [Ci/yr/SA] at 1.000E+04 yr

*exec: calling szft*

Highest release rates from SZ

Tc99 2.2917E-04 [Ci/yr/SA] at 8.293E+03 yr

I129 3.3224E-06 [Ci/yr/SA] at 5.434E+03 yr

Cl36 2.1791E-06 [Ci/yr/SA] at 4.830E+03 yr

Se79 1.2468E-06 [Ci/yr/SA] at 9.769E+03 yr

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*U234 5.0123E-13 [Ci/yr/SA] at 1.000E+04 yr*

*U238 1.2118E-13 [Ci/yr/SA] at 1.000E+04 yr*

*exec: calling dcagw*

*Highest annual dose GW pathway*

*I129 2.6933E-02 [mrem/yr] at 6.258E+03 yr*

*Tc99 1.5603E-03 [mrem/yr] at 8.293E+03 yr*

*Cl36 3.9021E-04 [mrem/yr] at 5.434E+03 yr*

*Se79 1.1806E-04 [mrem/yr] at 9.769E+03 yr*

*Np237 4.3299E-10 [mrem/yr] at 1.000E+04 yr*

*U234 2.4389E-10 [mrem/yr] at 1.000E+04 yr*

*At end of TPI, annual dose GW pathway*

*Tc99 1.0452E-03 [mrem/yr]*

*I129 1.0038E-03 [mrem/yr]*

*Se79 1.1786E-04 [mrem/yr]*

*Cl36 1.2194E-05 [mrem/yr]*

*Np237 4.3299E-10 [mrem/yr]*

*U234 2.4389E-10 [mrem/yr]*

*sum 2.1791E-03 [mrem/yr]*

*exec: calling ashplumo*

*exec: calling ashrmovo*

*exec: calling dcags*

*Highest annual dose from GS*

*Pu240 3.8296E+03 [mrem/yr] at 1.900E+03 yr*

*Pu239 2.9825E+03 [mrem/yr] at 1.900E+03 yr*

*Am241 2.1497E+03 [mrem/yr] at 1.900E+03 yr*

*Am243 1.9311E+02 [mrem/yr] at 1.900E+03 yr*

*Pu242 1.7055E+01 [mrem/yr] at 1.900E+03 yr*

*Np237 1.5592E+01 [mrem/yr] at 1.900E+03 yr*

*exec: end realizations*

*exec: Run Successfully Completed*

---

The waste packages affected are still in subarea 2, so the code is working properly.

Results: The code correctly moves the volcano to the subarea specified by the user for the user distribution model, but leaves the volcano in subarea 2 for the geometric model. Therefore, the code is working properly. The files for this test are located in the following directory:  
/home/jweldy/tpa40m/TEST/311/test3

#### Test 4

This test is to ensure that the code returns an error if more WPs are released from a subarea than the total number of WPs in the subarea. This will be checked by

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setting the number of WPs ejected in subarea 2 to 2000 and then setting the number of WPs failed by magma in subarea 2 to 2000. Since there are only ~1500 WPs in subarea 2, this should result in an error. The screen output will be checked for this test.

The first run set the number of WPs ejected to 2000. The following screen output was recorded:

```
=====
=====
exec: Welcome to TPA Version 4.0betaM
Job started: Mon Jun 19 16:53:21 2000
=====
=====
REPOSITORY DESIGN INFORMATION
Subarea Area Waste Number of WP
# [m^2] [MTU]
1 723591.3 14200.8 1455
2 784763.0 15303.7 1568
3 390372.0 7564.0 775
4 207581.3 4157.8 426
5 378972.8 7417.6 760
6 424872.5 8305.8 851
7 163938.3 3152.5 323
8 393468.9 7944.6 814

Total Area [acre] = 856.82238463061
Total Buried Waste [MTU] = 68046.720000000
Repository AML [MTU/acre] = 79.417532992367
```

*Specified Global Parameters:*

Compliance Period = 10000.0 (yr)  
Maximum Simulation Time = 10000.0 (yr)  
Number Of Realizations = 1  
Number Of Subareas = 8  
Volcanism scenario = 1 (yes=1, no=0)  
Faulting scenario = 0 (yes=1, no=0)  
Seismic scenario = 1 (yes=1, no=0)  
Distance to Receptor Group = 20.0 (km)

\*\*>>> CAUTION: CHECKING OF NUCLIDES AND CHAINS IS DISABLED <<<\*\*  
\*\*>>> You may not be using the standard chains specified <<<\*\*

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\*\*>>> in the invent module. <<<\*\*

\*\*>>> (see "CheckNuclidesAndChains(yes=1,no=0)" in tpa.inp)<<<\*\*

\*\*\*>>> NOTE: When running with volcanism, verify that <<<\*\*\*

\*\*\*>>> the maximum value of the PDF for parameter <<<\*\*\*

\*\*\*>>> TimeOfNextVolcanicEventinRegionOfInterest[yr] is <<<\*\*\*

\*\*\*>>> equal to the parameter MaximumTime[yr]. <<<\*\*\*

The specified path for data = \$TPA\_DATA/

The specified path for codes = \$TPA\_TEST/

\*\*To modify global parameters or the path, stop code execution using control-C\*\*

\*\*\*>>> WARNING: THE APPEND OPTION IS SELECTED <<<\*\*\*

(see "OutputMode(0=None,1=All,2=UserDefined)" in tpa.inp)

For "SelectAppendFiles", a value of 0 (all append files) was set in tpa.inp.

By selecting this option, files are written which may require 6 megs of disk space.  
(more disk space could be needed)

---

-----  
subarea 1 of 8 realization 1 of 1  
-----

exec: calling uzflow

exec: calling nfenv

exec: calling ebsfail

\*\*\* No Corrosion WP Failure \*\*\*

exec: calling seismo

exec: calling volcano

\*\*\*>>> Error in volcano <<<\*\*\*

nfailed .gt. nwpinfa

nfailed = 2030

wpentrained = 2000.0000000000

wpfailuredindrift = 30.000000000000

nwpinsa = 1568

---

---

The code crashed, so therefore, it is working properly. The second run had the following screen output:

---

---

=====

exec: Welcome to TPA Version 4.0betaM

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*Job started: Mon Jun 19 16:55:24 2000*

=====

=====

**REPOSITORY DESIGN INFORMATION**

*Subarea Area Waste Number of WP*

#	[m^2]	[MTU]	
1	723591.3	14200.8	1455
2	784763.0	15303.7	1568
3	390372.0	7564.0	775
4	207581.3	4157.8	426
5	378972.8	7417.6	760
6	424872.5	8305.8	851
7	163938.3	3152.5	323
8	393468.9	7944.6	814

*Total Area [acre] = 856.82238463061*

*Total Buried Waste [MTU] = 68046.7200000000*

*Repository AML [MTU/acre] = 79.417532992367*

*Specified Global Parameters:*

*Compliance Period = 10000.0 (yr)*

*Maximum Simulation Time = 10000.0 (yr)*

*Number Of Realizations = 1*

*Number Of Subareas = 8*

*Volcanism scenario = 1 (yes=1, no=0)*

*Faulting scenario = 0 (yes=1, no=0)*

*Seismic scenario = 1 (yes=1, no=0)*

*Distance to Receptor Group = 20.0 (km)*

**\*\*\*>>> CAUTION: CHECKING OF NUCLIDES AND CHAINS IS DISABLED <<<\*\***

**\*\*\*>>> You may not be using the standard chains specified <<<\*\***

**\*\*\*>>> in the invent module. <<<\*\***

**\*\*\*>>> (see "CheckNuclidesAndChains(yes=1,no=0)" in tpa.inp)<<<\*\***

**\*\*\*>>> NOTE: When running with volcanism, verify that <<<\*\***

**\*\*\*>>> the maximum value of the PDF for parameter <<<\*\***

**\*\*\*>>> TimeOfNextVolcanicEventinRegionOfInterest[yr] is <<<\*\***

**\*\*\*>>> equal to the parameter MaximumTime[yr]. <<<\*\***

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*The specified path for data = \$TPA\_DATA/*

*The specified path for codes = \$TPA\_TEST/*

*\*\*To modify global parameters or the path, stop code execution using control-C\*\**

*\*\*\*>>> WARNING: THE APPEND OPTION IS SELECTED <<<\*\*\**

*(see "OutputMode(0=None,1=All,2=UserDefined)" in tpa.inp)*

*For "SelectAppendFiles", a value of 0 (all append files) was set in tpa.inp.*

*By selecting this option, files are written which may require 6 megs of disk space.  
(more disk space could be needed)*

---

subarea 1 of 8 realization 1 of 1

---

exec: calling uzflow

exec: calling nfenv

exec: calling ebsfail

\*\*\* No Corrosion WP Failure \*\*\*

exec: calling seismo

exec: calling volcano

\*\*\*>>> Error in volcano <<<\*\*\*

nfailed.gt. nwpinsa

nfailed = 2010

wpentrained = 10.00000000000000

wpfailedindrift = 2000.0000000000

nwpinsa = 1568

---

Again, the code crashed, so it is working properly.

Results: The code crashed when too many waste packages were specified to fail due to the igneous intrusion. Therefore, the code successfully passed the test. Files used in this test are located in the following directory:

/home/jweldy/tpa40m/TEST/311/test4

### Test 5

This test is to compare the magnitude of the doses between a mean values run with TPA 3.3 and TPA 4.0 for the direct release only run. Both cases were run for a single realization with all parameters at their mean values. The results in rgssa.tpa were then compared to ensure that the change in dose was reasonable.

Results: The first year dose from volcanism in TPA 4.0 is about two orders of magnitude higher than in TPA 3.3. However, in years after the eruption, the TPA 4.0 dose is only about 5 times as large as the TPA 3.3 dose. The first year dose is so much larger because the

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mean value of the number of waste packages failed increased by almost a factor of ten, the first year mass load increased by a factor of a few, and the occupancy time increased by about a factor of two. The later doses are less large because of the time dependence of the mass loading factor, which drops off rapidly with time. The two rgssa.tpa files are listed below.

*Mean value input file tpa.inp for TPA Version 3.3 Code.*

*Parent file is the modified base case data set Rev 3.3, Nov. 1999*

*TPA 3.3 PVM capable, Job started: Mon Jun 19 17:05:15 2000*

*AEDE[rem/yr], GroundSurface Pathway*

*summed over all nuclides, averaged over all realizations*

```
0.461E+04 0.100E-14
0.472E+04 0.100E-14
0.483E+04 0.100E-14
0.495E+04 0.148E+01
0.506E+04 0.122E+01
0.518E+04 0.101E+01
0.531E+04 0.830E+00
0.543E+04 0.679E+00
0.556E+04 0.553E+00
0.570E+04 0.448E+00
0.583E+04 0.362E+00
0.597E+04 0.291E+00
0.611E+04 0.232E+00
0.626E+04 0.185E+00
0.641E+04 0.146E+00
0.656E+04 0.115E+00
0.672E+04 0.899E-01
0.687E+04 0.691E-01
0.704E+04 0.473E-01
0.721E+04 0.323E-01
0.738E+04 0.220E-01
0.755E+04 0.149E-01
0.773E+04 0.101E-01
0.791E+04 0.686E-02
0.810E+04 0.465E-02
0.829E+04 0.315E-02
0.849E+04 0.214E-02
0.869E+04 0.145E-02
0.890E+04 0.990E-03
0.911E+04 0.674E-03
0.932E+04 0.460E-03
```

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$0.954E+04$   $0.313E-03$

$0.977E+04$   $0.213E-03$

$0.100E+05$   $0.145E-03$

---

---

*Input file tpa.inp as supplied with TPA Version 4.0betaM Code.*

*Base case*

*TPA 4.0betaM, Job started: Mon Jun 19 17:04:42 2000*

*AEDE[rem/yr], GroundSurface Pathway*

*summed over all nuclides, averaged over all realizations*

$0.439E+04$   $0.100E-14$   
 $0.450E+04$   $0.100E-14$   
 $0.461E+04$   $0.100E-14$   
 $0.472E+04$   $0.100E-14$   
 $0.483E+04$   $0.100E-14$   
 $0.495E+04$   $0.130E+03$   
 $0.506E+04$   $0.791E+01$   
 $0.518E+04$   $0.675E+01$   
 $0.531E+04$   $0.575E+01$   
 $0.543E+04$   $0.489E+01$   
 $0.556E+04$   $0.414E+01$   
 $0.570E+04$   $0.349E+01$   
 $0.583E+04$   $0.294E+01$   
 $0.597E+04$   $0.246E+01$   
 $0.611E+04$   $0.205E+01$   
 $0.626E+04$   $0.170E+01$   
 $0.641E+04$   $0.141E+01$   
 $0.656E+04$   $0.116E+01$   
 $0.672E+04$   $0.951E+00$   
 $0.687E+04$   $0.776E+00$   
 $0.704E+04$   $0.631E+00$   
 $0.721E+04$   $0.510E+00$   
 $0.738E+04$   $0.411E+00$   
 $0.755E+04$   $0.329E+00$   
 $0.773E+04$   $0.263E+00$   
 $0.791E+04$   $0.208E+00$   
 $0.810E+04$   $0.165E+00$   
 $0.829E+04$   $0.129E+00$   
 $0.849E+04$   $0.101E+00$   
 $0.869E+04$   $0.775E-01$   
 $0.890E+04$   $0.586E-01$

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*0.911E+04 0.442E-01  
0.932E+04 0.332E-01  
0.954E+04 0.248E-01  
0.977E+04 0.185E-01  
0.100E+05 0.137E-01*

The files for these tests are located in the following directory:

/home/jweldy/tpa40m/TEST/311/test5

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Scientific Notebook #170

Issued to: S. Mohanty

Issue Date: Apr. 3, 1996

Account Number: 20-01402-762

Title: Inventory

Participants: J. Weldy

5/16/00 Correction to the Initial Inventory of Se-79 in the Repository

Reason: The current value of the initial inventory of Se-79 is calculated using a half-life of  $6.52 \times 10^4$  years in the Origen 2.1 computer code. However, recent experiments have identified the Se-79 half-life as  $1.1 \times 10^6$  years. Since the Origen 2.1 code calculates the quantity of radionuclides in grams/number of atoms and then converts this value to radioactivity using the half-life, the inventory needs to be corrected for this change.

Software used: Origen 2.1 Isotope Generation and Depletion Code

Procedure: A recent paper (Songsheng, et al., 1997) indicates that new measurements of the half-life of Se-79 is  $1.1 \times 10^6$  years, not  $6.5 \times 10^4$  as had been previously reported. The acceptance of this paper was checked at the National Nuclear Data Center (<http://www.nndc.bnl.gov/>) to ensure that the scientific community had accepted this value. The NNDC has incorporated this new value for the half-life of Se-79, so this is the value that should be used in our calculations.

As specified in p. 338 of Croft (1983), Origen 2.1 calculates quantities of radionuclides in units of g-atoms, which is then converted into other units of interest, such as activity. In order to determine the half-life used by the Origen 2.1 code, the output from the run listed below was examined. The inventory of Se-79 at t=0 was 6.998 g/MTU and the inventory at t=1000

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years was 6.924 g/MTU. Using the formula:

$$M(t) = M_0 * \exp(-\lambda t)$$

where

M(t) = Mass of radionuclide at time t

M<sub>0</sub> = Mass of radionuclide at time 0

$\lambda$  = Decay constant (1/yr)

This yields a half life of  $6.5 \times 10^4$  years as the value used in Origen 2.1.

Also, using the output from the run listed below, the mass of Se-79 at t=0 is 6.998 grams/MTU and the activity is 0.4877 Ci/MTU. Using the formula:

$$A = \frac{M * 6.022E23 * \frac{\ln(2)}{T_{1/2}}}{MW * 3.7E10}$$

where

A = Activity (Ci/MTU)

M = Mass (g/MTU)

T<sub>1/2</sub> = Half-life (sec)

MW = Molecular weight (g/mol)

This yields a half life of 2.05e12 sec which equals 6.5e4 yr.

Since inventory in curies is inversely proportional to half life, the initial inventory used in the TPA Code (0.458 Ci/MTU) should be multiplied by

$$\frac{6.5 * 10^4 \text{ years}}{1.1 * 10^6 \text{ years}}$$

Results: The new initial inventory for Se-79 is 0.0271 Ci/MTU.

References:

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Croff, A.G. ORIGEN2: A Versatile Computer Code for Calculating the Nuclide Compositions and Characteristics of Nuclear Materials. Nuclear Technology. Vol. 62, pp. 335-352. 1983.

Songsheng, J., G. Jingru, J. Shan, L. Chunsheng, C. Anzhi, H. Ming, W. Shaoyong, and L. Shilin. Determination of the half-life of  $^{79}\text{Se}$  with the Accelerator Mass Spectrometry Technique. Nuclear Instruments and Methods in Physics Research. 8:123 (1997), pp. 405-409.

### Input File - p3.040

```
-1
-1
-1
RDA * BURNUP OF PWR 3.0% UO2 FUEL & ASSY HDWARE, 40,000
      MWD/MT
RDA ** CROSS SECTION LIBRARY = PWRU50, 6 CYCLE
RDA *** SCOTT B. LUDWIG, OAK RIDGE NATIONAL
      LABORATORY
RDA **** (615) 574-7916, FTS 624-7916
RDA -1 = FRESH PWR FUEL WITH IMPURITIES (1 MT = 1000 KG)
RDA -2 = FRESH ZIRCALOY COMPOSITION (1 KG)
RDA -3 = FRESH SS 304 COMPOSITION (1 KG)
RDA -4 = FRESH SS 302 COMPOSITION (1 KG)
RDA -5 = FRESH INCONEL COMPOSITION (1 KG)
RDA -6 = FRESH NICROBRAZE COMPOSITION (1 KG)
RDA WARNING: VECTORS ARE CHANGED WITH RESPECT TO
      CONTENT.
RDA      THESE CHANGES WILL BE NOTED ON RDA CARDS.
CUT 5 1.0E-10 7 1.0E-10 9 1.0E-10 -1
LIP 0 0 0
RDA      DECAY LIB   XSECT LIB           VAR. XSECT
LIB 0 1 2 3 219 220 221 9 50 0 1 9
RDA      PHOTON LIB
PHO 101 102 103 10
TIT INITIAL COMP. OF UNIT AMOUNTS OF FUEL AND STRUCTURAL
      MAT'LS
RDA      READ FUEL COMPOSITION INCLUDING IMPURITIES (1000 KG)
INP -1 1 -1 -1 1 1
```

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RDA READ ZIRCALOY COMPOSITION (1.0 KG)  
INP -2 1 -1 -1 1 1  
RDA READ SS304 COMPOSITION (1.0 KG)  
INP -3 1 -1 -1 1 1  
RDA READ SS302 COMPOSITION (1.0 KG)  
INP -4 1 -1 -1 1 1  
RDA READ INCONEL 718 COMPOSITION (1.0 KG)  
INP -5 1 -1 -1 1 1  
RDA READ NICROBRAZE 50 COMPOSITION (1.0 KG)  
INP -6 1 -1 -1 1 1  
TIT IRRADIATION OF ONE METRIC TON OF PWRU FUEL  
MOV -1 1 0 1.0  
PCH 1 1 1  
HED 1 CHARGE  
BUP  
IRP 266.7 37.5 1 2 4 2 BURNUP=10,000 MWD/MTIHM  
DEC 372.7 2 3 4 0 DECAY FOR 106.0 DAYS  
IRP 639.3 37.5 3 4 4 0 BURNUP=20,000 MWD/MTIHM  
DEC 745.3 4 5 4 0 DECAY FOR 106.0 DAYS  
IRP 1012.0 37.5 5 6 4 0 BURNUP=30,000 MWD/MTIHM  
DEC 1118.0 6 7 4 0 DECAY FOR 106.0 DAYS  
IRP 1384.7 37.5 7 8 4 0 BURNUP=40,000 MWD/MTIHM  
BUP  
RDA -10 = IRRADIATED U FUEL AT DISCHARGE  
MOV 8 -10 0 1.0  
PCH -10 -10 -10  
RDA IRRADIATION OF ZIRCALOY AT 1.000 FLUX  
TIT IRRADIATION OF ZIRCALOY AT 1.000 FLUX  
MOV -2 1 0 223.0 ZIRCALOY  
PCH 1 1 1  
HED 1 CHARGE  
IRF 266.7 -1.0 1 2 4 2 BURNUP=10,000 MWD/MTIHM  
DEC 372.7 2 3 4 0 DECAY FOR 106.0 DAYS  
IRF 639.3 -1.0 3 4 4 0 BURNUP=20,000 MWD/MTIHM  
DEC 745.3 4 5 4 0 DECAY FOR 106.0 DAYS  
IRF 1012.0 -1.0 5 6 4 0 BURNUP=30,000 MWD/MTIHM  
DEC 1118.0 6 7 4 0 DECAY FOR 106.0 DAYS  
IRF 1384.7 -1.0 7 8 4 0 BURNUP=40,000 MWD/MTIHM  
RDA -9 = IRRADIATED ZIRCALOY

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MOV 8 -9 0 1.0

PCH -9 -9 -9

RDA IRRADIATION OF INCONEL + NICROBRAZE 50 AT 1.000 FLUX

TIT IRRADIATION OF INCONEL + NICROBRAZE 50 AT 1.000 FLUX

MOV -5 1 0 12.8 INCONEL

ADD -6 1 0 2.6 NICROBRAZE 50

PCH 1 1 1

HED 1 CHARGE

IRF 266.7 -1.0 1 2 4 2 BURNUP=10,000 MWD/MTIHM

DEC 372.7 2 3 4 0 DECAY FOR 106.0 DAYS

IRF 639.3 -1.0 3 4 4 0 BURNUP=20,000 MWD/MTIHM

DEC 745.3 4 5 4 0 DECAY FOR 106.0 DAYS

IRF 1012.0 -1.0 5 6 4 0 BURNUP=30,000 MWD/MTIHM

DEC 1118.0 6 7 4 0 DECAY FOR 106.0 DAYS

IRF 1384.7 -1.0 7 8 4 0 BURNUP=40,000 MWD/MTIHM

RDA -8 = IRRADIATED INCONEL AND NICROBRAZE

MOV 8 -8 0 1.0

PCH -8 -8 -8

RDA IRRADIATION OF SS 304 AT 1.000 FLUX

TIT IRRADIATION OF SS 304 AT 1.000 FLUX

MOV -3 1 0 9.9 SS 304

PCH 1 1 1

HED 1 CHARGE

IRF 266.7 -1.0 1 2 4 2 BURNUP=10,000 MWD/MTIHM

DEC 372.7 2 3 4 0 DECAY FOR 106.0 DAYS

IRF 639.3 -1.0 3 4 4 0 BURNUP=20,000 MWD/MTIHM

DEC 745.3 4 5 4 0 DECAY FOR 106.0 DAYS

IRF 1012.0 -1.0 5 6 4 0 BURNUP=30,000 MWD/MTIHM

DEC 1118.0 6 7 4 0 DECAY FOR 106.0 DAYS

IRF 1384.7 -1.0 7 8 4 0 BURNUP=40,000 MWD/MTIHM

RDA -7 = IRRADIATED SS 304

MOV 8 -7 0 1.0

PCH -7 -7 -7

RDA IRRADIATION OF SS 304 END PIECES AT 0.011 FLUX

TIT IRRADIATION OF SS 304 END PIECES AT 0.011 FLUX

MOV -3 1 0 27.2 SS 304

PCH 1 1 1

HED 1 CHARGE

IRF 266.7 -0.011 1 2 4 2 BURNUP=10,000 MWD/MTIHM

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DEC 372.7 2 3 4 0 DECAY FOR 106.0 DAYS  
IRF 639.3 -0.011 3 4 4 0 BURNUP=20,000 MWD/MTIHM  
DEC 745.3 4 5 4 0 DECAY FOR 106.0 DAYS  
IRF 1012.0 -0.011 5 6 4 0 BURNUP=30,000 MWD/MTIHM  
DEC 1118.0 6 7 4 0 DECAY FOR 106.0 DAYS  
IRF 1384.7 -0.011 7 8 4 0 BURNUP=40,000 MWD/MTIHM  
RDA -6 = IRRADIATED SS 304 END PIECES AT DISCHARGE  
MOV 8 -6 0 1.0  
PCH -6 -6 -6  
RDA IRRADIATION OF SS302 PLENUM SPRINGS AT 0.042 FLUX  
TIT IRRADIATION OF SS302 PLENUM SPRINGS AT 0.042 FLUX  
MOV -4 1 0 4.2 SS 302  
ADD -2 1 0 12.0 ZR IN PLENUM  
PCH 1 1 1  
HED 1 CHARGE  
IRF 266.7 -0.042 1 2 4 2 BURNUP=10,000 MWD/MTIHM  
DEC 372.7 2 3 4 0 DECAY FOR 106.0 DAYS  
IRF 639.3 -0.042 3 4 4 0 BURNUP=20,000 MWD/MTIHM  
DEC 745.3 4 5 4 0 DECAY FOR 106.0 DAYS  
IRF 1012.0 -0.042 5 6 4 0 BURNUP=30,000 MWD/MTIHM  
DEC 1118.0 6 7 4 0 DECAY FOR 106.0 DAYS  
IRF 1384.7 -0.042 7 8 4 0 BURNUP=40,000 MWD/MTIHM  
RDA -5 = IRRADIATED SS 302 IN PLENUM SPRINGS AT DISCHARGE  
MOV 8 -5 0 1.0  
PCH -5 -5 -5  
RDA \*\*\*\*\* OUTPUT MODULE \*\*\*\*\*  
TIT TEST OF ORIGEN2 V2.1 - PWR FUEL ASSY-EXTENDED BURNUP  
(PWRU50)  
BAS 1 MTIHM 3.0% UO2 FUEL ASSY;BURNUP=40,000 MWD/MTIHM, 6  
CYCLE  
OPTL 4\*8 7 8 7 8 8 8 14\*8  
OPTA 4\*8 7 8 7 8 8 8 14\*8  
OPTF 4\*8 7 8 7 8 8 8 14\*8  
MOV -10 1 0 1.0  
ADD -9 1 0 1.0  
ADD -8 1 0 1.0  
ADD -7 1 0 1.0  
ADD -6 1 0 1.0  
ADD -5 1 0 1.0

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HED 1 ASSY DIS  
RDA \*\*\*\*\* DECRY MODULE \*\*\*\*\*  
DEC 1.0 1 2 5 2  
DEC 10.0 2 3 5 0  
DEC 100.0 3 4 5 0  
DEC 1.0 4 5 7 0  
DEC 10.0 5 6 7 0  
OUT 5 1 -1 0  
END  
2 922340 376.0 922350 30000. 922380 969624. 0 0.0 FUEL 3.0%  
4 030000 1.0 050000 1.0 060000 89.4 070000 25.0 FUEL IMPU  
4 080000 134454. 090000 10.7 110000 15.0 120000 2.0 FUEL IMPU  
4 130000 16.7 140000 12.1 150000 35.0 170000 5.3 FUEL IMPU  
4 200000 2.0 220000 1.0 230000 3.0 240000 4.0 FUEL IMPU  
4 250000 1.7 260000 18.0 270000 1.0 280000 24.0 FUEL IMPU  
4 290000 1.0 300000 40.3 420000 10.0 470000 0.1 FUEL IMPU  
4 480000 25.0 490000 2.0 500000 4.0 640000 2.5 FUEL IMPU  
4 740000 2.0 820000 1.0 830000 0.4 0 0.0 FUEL IMPU  
0  
4 400000 979.11 500000 16.0 260000 2.25 240000 1.25 ZIRC-4  
4 280000 0.02 130000 0.024 050000 0.00033 480000 0.00025 ZIRC-4  
4 060000 0.120 270000 0.010 290000 0.020 720000 0.078 ZIRC-4  
4 010000 0.013 250000 0.020 070000 0.080 080000 0.950 ZIRC-4  
4 160000 0.035 220000 0.020 740000 0.020 230000 0.020 ZIRC-4  
5 920000 0.0002 0 0.0 ZIRC-4  
0  
4 260000 688.44 240000 190.0 280000 89.2 250000 20.0 SS-304  
4 060000 0.8 150000 0.45 160000 0.3 140000 10.0 SS-304  
4 070000 1.3 270000 0.8 0 0.0 SS-304  
0  
4 260000 697.74 240000 180.0 280000 89.2 250000 20.0 SS-302  
4 060000 1.5 150000 0.45 160000 0.3 140000 10.0 SS-302  
4 070000 1.3 270000 0.8 0 0.0 SS-302  
0  
4 260000 179.766 240000 189.753 280000 519.625 130000 5.992 INC-718  
4 060000 0.4 270000 4.694 290000 0.999 250000 1.997 INC-718  
4 420000 29.961 070000 1.3 410000 55.458 160000 0.07 INC-718  
4 140000 1.997 220000 7.99 0 0.0 INC-718  
0

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4

```

4 130000 0.1 050000 0.05 060000 0.1 270000 0.381 NICR-50
4 250000 0.1 070000 0.066 080000 0.043 150000 103.244 NICR-50
4 160000 0.1 140000 0.511 220000 0.1 740000 0.1 NICR-50
0

```

## **Output File - p3.040o.mass**

1

```

*****
* OOOOO RRRR IIII GGGGG EEEEE N N 22222 * 
* O O R R I G E NN N 22 22 *
* O O RRRR I G GG EEEE N NNNN 22 *
* O O R R I G G E N NN 22 *
* OOOOO R R IIII GGGGGG EEEEE N N 2222222 *
*
* Version 2.1 (8-1-91) *
*
*
*
* OOOOO AA K K *
* O O A A K K *
* O O AAAA KKK *
* O O A A K K *
* OOOOO A A K K *
*
* RRRR III DDDDD GGGGG EEEEE * 
* R R I D D G E * 
* RRRR I D D G GG EEEE * 
* R R I D D G G E * 
* R R III DDDDD GGGGGG EEEEE * 
*
* N N AA TTTT III OOOOO N N AA L * 
* NN N A A T I O O NN N A A L * 
* NNNN AAAA T I O O N NNNN AAAA L * 
* N NN A A T I O O N NN A A L * 
* N N A A T III OOOOO N N A A LLLL * 
*
* L AA BBBB OOOO RRRR AA TTTT OOOO RRRR Y Y * 
* L A AB BO OR R A A T O OR R YY * 
* L AAAA BBBB O ORRRR AAAA T O ORRRR Y * 
* L A AB BO OR R A A T O OR R Y * 
* LLLL A A BBBB OOOOR R A A T OOOOR R Y * 
*
* RSIC CODE PACKAGE NUMBER (CCC-371) *

```

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\* \*  
\* ORIGEN2 VERSION 2.1 (8-1-91) UPDATES THE FOLLOWING: \*  
\* CCC-371(A) - MAINFRAMES \*  
\* CCC-371(E) - IBM PC (80386 W/80387 OR 80486) \*  
\* \*  
\* ORIGEN2 RUN DATE: May 16 2000 TIME 10:41:42 \*  
\* \*  
\* \*  
\*\*\*\*\*

1 OUTPUT UNIT = 6 PAGE 1  
ORIGEN2 V2.1 (8-1-91), Run on May 16 2000 at 10:41:42

0\*\*\*\*\*  
\*\*\*\*\*

\*\*\*\*\* ORIGEN2: A REVISED AND UPDATED VERSION OF  
THE ORIGEN COMPUTER CODE \*\*\*\*\*

\*\*\*\*\*  
\*\*\*\*\*  
\*\*\*\*\*  
\*\*\*\*\*

## INTRODUCTION

THIS TEXT IS INTENDED TO BE A BRIEF OUTLINE OF THE ORIGEN2 COMPUTER CODE, WHICH IS A REVISED AND UPDATED VERSION OF THE ORIGEN DOCUMENTED IN REPORT ORNL-4628 (MAY 1973). INCLUDED HERE ARE A BRIEF DESCRIPTION OF THE FUNCTIONS OF ORIGEN2, A LISTING OF THE MAJOR DATA SOURCES, A LISTING OF THE PUBLISHED DOCUMENTATION CONCERNING ORIGEN2, AND AN OUTLINE OF THE ORIGEN2

OUTPUT ORGANIZATION. ORIGEN2 IS AVAILABLE FROM THE ORNL RADIATION SHIELDING INFORMATION CENTER (RSIC) AT THE FOLLOWING ADDRESS:

CODES COORDINATOR  
RADIATION SHIELDING INFORMATION CENTER  
BLDG. 6025  
OAK RIDGE NATIONAL LABORATORY  
OAK RIDGE, TENNESSEE 37830  
PHONE: (615) 574-6176

QUESTIONS CONCERNING ORIGEN2 SHOULD BE ADDRESSED TO RSIC.

## -DESCRIPTION

ORIGEN2 IS A REVISION AND UPDATE OF THE ORIGEN COMPUTER CODE. SPECIFICALLY, THE INPUT, OUTPUT, CONTROL, AND DATA BASE ASPECTS

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OF ORIGEN HAVE BEEN SIGNIFICANTLY REVISED AND UPDATED TO REFLECT CURRENT INFORMATION AND NEEDS. IT SHOULD BE NOTED THAT THE MATHEMATICAL METHODS USED TO SOLVE THE NUCLIDE BUILDUP, DEPLETION, AND DECAY EQUATIONS ARE ESSENTIALLY UNCHANGED FROM THAT IN ORIGEN. ORIGEN2 IS A COMPUTER CODE DESIGNED TO CALCULATE THE COMPOSITION AND CHARACTERISTICS OF NUCLEAR MATERIALS AS A FUNCTION OF DECAY TIME AND THE CHANGES THE MATERIALS UNDERGO DURING VARIOUS FUEL CYCLE OPERATIONS. INPUT AND OUTPUT FEATURES HAVE BEEN DESIGNED TO FACILITATE FLEXIBILITY IN THE TYPE OF CASES THAT CAN BE CONSIDERED AND IN CONTROLLING THE DETAIL OF THE OUTPUT. FOR FURTHER INFORMATION, THE USER IS REFERRED TO THE DOCUMENTATION LISTED BELOW.

-MAJOR DATA SOURCES

VIRTUALLY ALL ASPECTS OF THE DATA INPUT TO ORIGEN2 HAVE BEEN UPDATED OR REVISED TO REFLECT CURRENT INFORMATION. THE PRINCIPAL SOURCES OF CROSS SECTION DATA WERE THE ENDF/B-IV, ENDF/B-V, AND LENDL COMPILATIONS. DECAY AND PHOTON INFORMATION WERE PRIMARILY BASED ON THE EVALUATED NUCLEAR STRUCTURE DATA FILE (ENSDF) AT ORNL AND ENDF/B-IV. DATA CONCERNING REACTOR AND FUEL CHARACTERISTICS WERE OBTAINED FROM REFERENCE SAFETY ANALYSIS REPORTS AND, WHERE POSSIBLE, THE COMMERCIAL REACTOR

VENDORS.

-DOCUMENTATION

THE FOLLOWING ITEMS CONSTITUTE THE ORIGEN2 DOCUMENTATION PUBLISHED AS OF THE DATE OF THIS CODE PACKAGE:

A.G. CROFF, "ORIGEN2 - A REVISED AND UPDATED VERSION OF THE OAK RIDGE ISOTOPE GENERATION AND DEPLETION CODE", ORNL-5621

(JULY 1980).

A.G. CROFF, "A USER'S MANUAL FOR THE ORIGEN2 COMPUTER CODE", ORNL/TM-7175 (JULY 1980).

A.G. CROFF, M.A. BJRKE, G.W.MORRISON, AND L.M. PETRIE, "REVISED URANIUM-PLUTONIUM CYCLE PWR AND BWR MODELS FOR THE ORIGEN COMPUTER CODE", ORNL/TM-6051 (SEPTEMBER 1978).

A.G. CROFF AND M.A. BJRKE, "ALTERNATIVE FUEL CYCLE PWR MODELS FOR THE ORIGEN COMPUTER CODE", ORNL/TM-7005 (FEB 1980).

A.G. CROFF, R.L. HAESE, AND N.B. GOVE, "UPDATED DECAY AND PHOTON LIBRARIES FOR THE ORIGEN CODE", ORNL/TM-6055 (FEB 1979)

A.G. CROFF, "ORIGEN2: A REVISED AND UPDATED VERSION OF ORIGEN", TRANS. AM. NUCL. SOC., VOL. 34, P. 349-50 (JUNE 1980).

1

OUTPUT UNIT = 6

PAGE 2

ORIGEN2 V2.1 (8-1-91), Run on May 16 2000 at 10:41:42

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\*\*\*\*\* ORIGEN2: A REVISED AND UPDATED VERSION OF

Scientific Notebook #170-10e

James Weldy

12/27/00

20-1402-762

THE ORIGEN COMPUTER CODE \*\*\*\*\*

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#### ORGANIZATION OF ORIGEN2 OUTPUT

PAST EXPERIENCE HAS INDICATED THAT MANY USERS ENCOUNTER  
CONSIDERABLE DIFFICULTY IN FINDING THE DESIRED INFORMATION IN A

ORIGEN2 OUT PUT WHICH IS SOMETIMES RATHER MASSIVE. THIS SECTION IS  
INTENDED AS A BRIEF OUTLINE OF THE ORGANIZATION OF  
ORIGEN2 OUTPUT. FOR DETAILS REFER TO THE USER'S MANUAL (ORNL/TM-7175,  
SECT. 8.2). THE ORIGEN2 OUTPUT IS EXTREMELY  
HIERARCHICAL, AND IS ORGANIZED AS FOLLOWS:

- 0 CARD INPUT ECHO
  - MISCELLANEOUS INPUT DATA (NEUTRON YIELDS, REPROCESSING LOSSES,ELEMENT CHEMICAL TOXICITIES)
  - LISTING OF ORIGEN2 COMMANDS CURRENTLY BEING EXECUTED
  - LISTING OF ORIGEN2 DATA LIBRARIES (IF SPECIFIED)
  - DECAY LIBRARY
    - ACTIVATION PRODUCTS
    - ACTINIDES
    - FISSION PRODUCTS
    - CROSS SECTION/FISSION PRODUCT YIELD LIBRARY
      - ACTIVATION PRODUCTS, ACTINIDES, AND FISSION PRODUCTS
    - PHOTON LIBRARY
      - ACTIVATION PRODUCTS, ACTINIDES, AND FISSION PRODUCTS
  - OUTPUT 1
    - REACTIVITY AND BURNUP DATA
    - ACTIVATION PRODUCT TABLES
      - GRAM TABLES (NUCLIDE, ELEMENT, NUCLIDE SUMMARY, ELEMENT SUMMARY)
      - CURIE TABLES (NUCLIDE, ELEMENT, NUCLIDE SUMMARY, ELEMENT SUMMARY)
      - ETC. (DEPENDING ON THE OUTPUT OPTIONS SPECIFIED, MANY OF THESE TABLES MAY BE OMITTED)
  - ACTINIDE TABLES
    - SAME SUBHEADINGS POSSIBLE AS UNDER ACTIVATION PRODUCT TABLES
  - FISSION PRODUCT TABLES
    - SAME SUBHEADINGS POSSIBLE AS UNDER ACTIVATION PRODUCT TABLES
  - NEUTRON PRODUCTION RATE TABLES: (ALPHA,N) AND SPONTANEOUS FISSION

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PHOTON TABLES

ACTIVATION PRODUCTS (SUMMATION AND PRINCIPAL CONTRIBUTORS)

ACTINIDES (SUMMATION AND PRINCIPAL CONTRIBUTORS)

FISSION PRODUCTS (SUMMATION AND PRINCIPAL CONTRIBUTORS)

OUTPUT 2

SAME GENERAL CONTENT AND ORDER AS OUTPUT 1

OUTPUT N

SAME GENERAL CONTENT AND ORDER AS OUTPUT 1

TABLE OF CONTENTS (UNIT 12) FOR THE ABOVE (UNIT 6) OUTPUT

VARIABLE CROSS SECTION INFORMATION OUTPUT (UNIT 16)

DEBUGGING AND OTHER INTERNAL INFORMATION OUTPUT (UNIT 15)

- 0 THE SCENARIO LISTED ABOVE CONSTITUTES A TYPICAL ORIGEN2 OUTPUT FOR MANY CASES. ONE POSSIBLE MODIFICATION IS THE USE OF AN STP COMMAND TO EXECUTE AN ADDITIONAL SET OF INSTRUCTIONS AFTER THE FIRST SET HAS BEEN EXECUTED. IF THIS IS DONE, THE OUTPUT WILL BEGIN WITH "MISCELLANEOUS INPUT DATA" IF NSTP=1, "ORIGEN2COMMANDS CURRENTLY BEING EXECUTED" IF NSTP=2, OR "OUTPUT 1" FOR NSTP=3. ANOTHER OFTEN-USED OPTION IS TO EMPLOY BOTH THE PRIMARY (UNIT 6) AND ALTERNATE (UNIT 11) OUTPUT UNITS. IF BOTH ARE ROUTED TO PAPER, THE TABLE OF CONTENTS FOR UNIT 11, WHICH IS ON UNIT 13, WILL IMMEDIATELY FOLLOW THE DEBUGGING AND INTERNAL INFORMATION (UNIT 15) OUTPUT. THE "OUTPUT N" TABLES FOR UNIT 11 WILL BE PRINTED FOLLOWING THE TABLE OF CONTENTS.

1

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ORIGEN2 V2.1 (8-1-91), Run on May 16 2000 at 10:41:42

\*EST OF ORIGEN2 V2.1 - PWR FUEL ASSY-EXTENDED BURNUP (PWRU50)

FISSION PRODUCTS

+ POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC

0 5 SUMMARY TABLE: CONCENTRATIONS, GRAMS

MTIHM 3.0% UO2 FUEL ASSY;BURNUP=40,000 MWD/MTIHM, 6 CYCLE

ASSY DIS 1.0YR 10.0YR 100.0YR 1.0KY

H 3 7.045E-02 6.660E-02 4.019E-02 2.571E-04 0.000E+00

LI 6 1.939E-04 1.939E-04 1.939E-04 1.939E-04 1.939E-04

LI 7 1.229E-05 1.229E-05 1.229E-05 1.229E-05 1.229E-05

BE 9 2.364E-05 2.364E-05 2.364E-05 2.364E-05 2.364E-05

BE 10 1.579E-04 1.579E-04 1.579E-04 1.579E-04 1.578E-04

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C 14	3.193E-05	3.192E-05	3.189E-05	3.154E-05	2.829E-05
ZN 72	8.174E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GA 72	2.487E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GE 72	2.877E-02	2.888E-02	2.888E-02	2.888E-02	2.888E-02
GA 73	1.648E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GE 73	5.680E-02	5.682E-02	5.682E-02	5.682E-02	5.682E-02
GE 74	1.227E-01	1.227E-01	1.227E-01	1.227E-01	1.227E-01
GE 75	1.821E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00
AS 75	2.451E-01	2.451E-01	2.451E-01	2.451E-01	2.451E-01
GE 76	5.970E-01	5.970E-01	5.970E-01	5.970E-01	5.970E-01
AS 76	3.002E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SE 76	9.045E-03	9.075E-03	9.075E-03	9.075E-03	9.075E-03
GE 77	2.525E-04	0.000E+00	0.000E+00	0.000E+00	0.000E+00
AS 77	2.348E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SE 77	1.198E+00	1.201E+00	1.201E+00	1.201E+00	1.201E+00
GE 78	2.035E-04	0.000E+00	0.000E+00	0.000E+00	0.000E+00
AS 78	2.192E-04	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SE 78	2.956E+00	2.956E+00	2.956E+00	2.956E+00	2.956E+00
AS 79	5.112E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SE 79	6.998E+00	6.998E+00	6.998E+00	6.991E+00	6.924E+00
SE 79M	2.218E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BR 79	1.521E-04	2.268E-04	8.989E-04	7.616E-03	7.443E-02
SE 80	1.576E+01	1.576E+01	1.576E+01	1.576E+01	1.576E+01
KR 80	3.109E-04	3.110E-04	3.110E-04	3.110E-04	3.110E-04
AS 81	1.009E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SE 81	3.800E-04	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SE 81M	3.035E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BR 81	2.496E+01	2.496E+01	2.496E+01	2.496E+01	2.496E+01
KR 81	3.675E-05	3.675E-05	3.675E-05	3.674E-05	3.663E-05
AS 82	5.457E-06	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SE 82	3.877E+01	3.877E+01	3.877E+01	3.877E+01	3.877E+01
BR 82	6.213E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BR 82M	7.256E-06	0.000E+00	0.000E+00	0.000E+00	0.000E+00
KR 82	1.475E+00	1.481E+00	1.481E+00	1.481E+00	1.481E+00
AS 83	6.077E-06	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SE 83	4.144E-04	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SE 83M	3.071E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BR 83	6.592E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00
KR 83	4.441E+01	4.442E+01	4.442E+01	4.442E+01	4.442E+01
KR 83M	5.067E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SE 84	2.437E-04	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BR 84	2.454E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00
BR 84M	2.051E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00
KR 84	1.318E+02	1.318E+02	1.318E+02	1.318E+02	1.318E+02
SE 85	2.688E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SE 85M	9.795E-06	0.000E+00	0.000E+00	0.000E+00	0.000E+00

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1 OUTPUT UNIT = 6 PAGE 46  
ORIGEN2 V2.1 (8-1-91), Run on May 16 2000 at 10:41:42

\*EST OF ORIGEN2 V2.1 - PWR FUEL ASSY-EXTENDED BURNUP (PWRU50)  
FISSION PRODUCTS

POWER= 1.00000E+00 MW, BURNUP= 1.00000E+00 MWD, FLUX= 1.00E+00  
N/CM\*\*2-SEC

## 7 SUMMARY TABLE: RADIOACTIVITY, CURIES

MTIHM 3.0% UO<sub>2</sub> FUEL ASSY; BURNUP=40,000 MWD/MTIHM, 6 CYCLE

ASSY DIS 1.0YR 10.0YR 100.0YR 1.0KY

H 3	6.801E+02	6.430E+02	3.880E+02	2.483E+00	0.000E+00
BE 10	3.530E-06	3.530E-06	3.530E-06	3.530E-06	3.528E-06
C 14	1.424E-04	1.423E-04	1.422E-04	1.406E-04	1.261E-04
CO 72	1.681E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NI 72	3.238E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CU 72	6.448E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZN 72	7.654E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GA 72	7.681E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CO 73	5.481E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NI 73	2.695E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CU 73	8.232E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZN 73	1.373E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GA 73	1.450E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GE 73M	1.452E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CO 74	1.032E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NI 74	1.553E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CU 74	1.043E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZN 74	2.496E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GA 74	2.686E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NI 75	6.264E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CU 75	1.014E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZN 75	4.456E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GA 75	5.435E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GE 75	5.515E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GE 75M	2.549E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NI 76	1.582E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CU 76	7.315E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZN 76	7.137E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GA 76	1.109E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00
AS 76	4.706E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NI 77	2.716E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CU 77	3.369E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZN 77	7.700E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GA 77	1.931E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GE 77	9.096E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00

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GE 77M	1.952E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00
AS 77	2.463E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SE 77M	7.401E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
NI 78	3.165E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CU 78	1.194E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZN 78	7.205E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GA 78	3.232E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GE 78	5.642E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00
AS 78	5.828E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00
CU 79	3.772E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
ZN 79	5.099E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GA 79	3.799E+03	0.000E+00	0.000E+00	0.000E+00	0.000E+00
GE 79	1.163E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00
AS 79	1.352E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00
SE 79	4.877E-01	4.877E-01	4.877E-01	4.872E-01	4.826E-01
SE 79M	1.358E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00

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Scientific Notebook #170

Issued to: S. Mohanty

Issue Date: Apr. 3, 1996

Account Number: 20-01402-762

Title: Modifications to ASHRMOVO and DCAGW to correct the formula to calculate the leaching factor

Participants: J. Weldy

9/11/00 - Correction of formula to calculate the leaching factor in DCAGW and ASHRMOVO

Rationale: The formula used to calculate the leaching factor in ASHRMOVO and DCAGW is based on the following formula in Napier et al., 1988, which is taken from Baes and Sharp, 1981:

$$\lambda_l = \frac{V_w}{d(1 + \frac{\rho K_d}{\theta})}$$

where,

$\lambda$  = leaching factor (l/yr)

$V_w$  = Infiltration rate of water (m/yr)

$d$  = Thickness of rooting zone (m)

$\rho$  = Density of soil (g/cm<sup>3</sup>)

$\theta$  = Soil volumetric water content

However, in 1983, Baes and Sharp published a paper which documented the calculation of the leaching factor that resulted in a slightly different formula than in Baes and Sharp, 1981:

$$\lambda_l = \frac{V_w / \theta}{d(1 + \frac{\rho K_d}{\theta})}$$

where all symbols are the same as above

The difference in the formulae is that the 1981 paper used the infiltration rate of

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the water to compare the rate of movement of the contaminant whereas the 1983 paper used the more appropriate velocity of water in the subsurface. As such, the TPA code will be modified to utilize the formula developed in Baes and Sharp, 1983.

Objective:

Modify ASHRMOVO and DCAGW to calculate the leaching factor using the formula in Baes and Sharp, 1983.

Lines modified: ASHRMOVO

Line 658 - modified from

```
dll(i)=(precip*(1.d0-fpe)*fpsat+dirr*1.d0-
fie)*fisat)/(depthsoil*(1.d0+rhosoil/theta*dkd(i)))
```

to

```
dll(i)=(precip*(1.d0-fpe)*fpsat+dirr*1.d0-
fie)*fisat)/(depthsoil*theta*(1.d0+rhosoil/theta*dkd(i)))
```

Lines modified: DCAGW

Line 1834 - modified from

```
r2=(rain+water-et)/((doss/100)*1+sbd/svwc*retcoef)
```

to

```
r2=(rain+water-et)/(svwc*(doss/100)*1+sbd/svwc*retcoef))
```

## TESTING

To ensure that the changes were implemented correctly, two tests were conducted, one to test the changes to dcagw.f and one to test the changes to ashrmovo.f

For the dcagw test, the calculated leaching factors are directly written to the file

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gftrans.inp. Therefore, one realization of the code was run and the results for several nuclides in gftrans.inp were compared to results calculated using an Excel spreadsheet. The TPA files used for the test are located in the directory /home/jweldy/tpa40/dev/tpa41test/dcagwtest and the Excel spreadsheet is located on Kraken at d:\personal\excel files\Leachtest41.xls. The results are as follows:

There is very good agreement here, so the modifications are considered successful.

Radio nuclide	Kd (cm <sup>3</sup> /g)	Leaching Factor (1/yr)	TPA Calc Leaching Factor - DCAGW (1/yr)	Precip rate (m/yr)	Irrigation rate (m/yr)	Evapo rate (m/yr)	Depth of Soil (m)	Soil Volumetric Water Content	Soil Density (g/cm <sup>3</sup> )
Cm	4062	8.81E-04	8.80E-04	0.085	1.52	0.8	0.15	0.35	1.5
Pu	547.7	6.53E-03	6.50E-03						
U	34.8	1.02E-01	1.00E-01						
Am	1914	1.87E-03	1.90E-03						
Np	5	6.84E-01	6.90E-01						
Th	3200	1.12E-03	1.10E-03						
Ra	497	7.20E-03	7.20E-03						
Pb	269.8	1.32E-02	1.30E-02						
Cs	273.9	1.31E-02	1.30E-02						
I	1	2.90E+00	2.90E+00						
Tc	0.1	1.07E+01	1.10E+01						
Ni	403	8.87E-03	8.90E-03						
Cl	0.25	7.40E+00	7.40E+00						
C	5	6.84E-01	6.80E-01						
Se	56.1	6.35E-02	6.30E-02						
Nb	160	2.23E-02	2.20E-02						

The ASHRMOVO tests are more tricky because the calculated leaching factor is not directly output. The best way to determine the leaching factor is to set the erosion rate to zero and do a best fit curve on the dose through time

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curve, which will then only be affected by leaching and radioactive decay.

If the test radionuclides have a long enough half-life, the exponential curve fit should yield the leaching factor in the exponent. The TPA files used for the test are located in the directory

/home/jweldy/tpa40/dev/tpa41test/ashrmovotest and the Excel

spreadsheet is located on Kraken at d:\personal\excel

files\Leachtest41.xls. The results are as follows:

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Radio nudide	Kd (cm <sup>3</sup> /g)	TPA Calc lambda				Solubility (mol/L)	N (mol/m <sup>2</sup> )	S*R/lamb da	Ci/MTU
		Leaching Factor (1/yr)	(leach+rad) - ASHRMOVO (1/yr)	lambda rad (1/yr) / notes	lambda leach				
Cm	4000	<b>1.81E-04</b>	3.27E-04	0.000145772	<b>1.81E-04</b>	1.00E-06	<b>2.20E-04</b>	<b>8.40E-04</b>	0.015
Pu	550	<b>1.32E-03</b>	<b>1.30E-03</b>	solubility limited		5.00E-06	<b>2.93E+00</b>	<b>5.78E-04</b>	200
U	35	2.05E-02	1.35E-03	solubility limited		4.50E-05	<b>4.54E-03</b>	<b>3.33E-04</b>	0.31
Am	1900	<b>3.81E-04</b>	4.75E-04	9.4152E-05	<b>3.81E-04</b>	1.00E-04	<b>1.46E-02</b>	<b>1.11E-04</b>	1
Np	5	1.37E-01	5.77E-04	solubility limited		2.00E-03	<b>3.66E-02</b>	<b>1.68E-01</b>	2.5
Th	3200	<b>2.26E-04</b>	2.36E-04	9.19293E-06	<b>2.27E-04</b>				
Ra	500	1.45E-03	3.16E-04	buildup					
Pb	270	2.68E-03	3.19E-04	buildup					
Cs	280	<b>2.58E-03</b>	<b>2.59E-03</b>						
I	1	5.64E-01	high						
Tc	0.1	1.88E+00	high						
Ni	400	<b>1.81E-03</b>	<b>1.82E-03</b>						
Cl	0.25	1.35E+00	high						
C	5	1.37E-01	high						
Se	150	<b>4.82E-03</b>	<b>4.78E-03</b>						
Nb	160	<b>4.52E-03</b>	<b>4.55E-03</b>						

Precip rate (m/yr)	Fraction of Irrigation rate (m/yr)	Fraction of irrig lost to ET	Depth of Soil (m)	Soil Volumetric Water Content (g/cm <sup>3</sup> )	Soil Density	Fraction of precip lost to ET	Fraction of year blanket is sat due to precip	Fraction of year blanket is sat due to irrig	Recharge rate of water (m/yr)	MTU/m <sup>2</sup>
0.085	1.52	0.5	0.15	0.4	1.4	0.68	0.0054	0.2	0.15214688	1.17E-06

Again, there is very good agreement here, so the test is considered successful.

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References:

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Scientific Notebook #170

Issued to: S. Mohanty

Issue Date: Apr. 3, 1996

Account Number: 20-01402-762

Title: Testing of the modification to DCAGW to initialize the variable dKGvalue  
- PA-SCR-324

Participants: J. Weldy

9/12/00 - Description of tests conducted to ensure that the variable dKGvalue is initialized properly in DCAGW

Rationale:

The code was modified because in multiple realization runs, the variable dKGvalue was not being initialized properly and therefore, the time of the pluvial switch was not staying fixed at the year specified in the tpa.inp file.

Methodology:

The fix will be tested by running the code for 10 realizations with the original file with the input file modified to make the time of the switch to pluvial conditions obvious (by reducing the pluvial pumping rate significantly) and observing when the switch to pluvial conditions occurs by looking at the dose in rgwsr.tpa. The same 10 realizations will be run for the corrected code to ensure that the year of the switch to pluvial conditions occurs at year 13000 and then current conditions return in year 77500. This is the only location in the code that the variable dKGvalue is used, so this single test is sufficient to ensure that the code is working properly. The TPA files used for the test and the results of the tests (in the Excel spreadsheet dcagw2test1) are stored on vulcan at /home/jweldy/tpa40/dev/tpa41test/dcagw2 and the results are summarized below.

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Results:

Year	Dose 2 (r m/ yr)												* Note that Years in Pluvial Climate are in Bold	
	Dose 1 (r e m/ yr)			Dose 1 (r e m/ yr)			Dose 1 (r e m/ yr)			Dose 1 (r e m/ yr)				
	Dose 1 (r e m/ yr)													
2.31e+01	1.00e-15	* If code is Functioning Properly, Pluvial Climate												
4.67e+01	1.00e-15	* Should be Between 13000 and 77500 Years												
7.09e+01	1.00e-15	* For Every Realization												
9.57e+01	1.00e-15													
1.21e+02	1.00e-15													
1.47e+02	1.00e-15													
1.74e+02	1.00e-15													
2.01e+02	1.00e-15													
2.28e+02	1.00e-15													
2.57e+02	1.00e-15													

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2.86e+02	1.00e-15										
3.16e+02	1.00e-15										
3.46e+02	1.00e-15										
3.78e+02	1.00e-15										
4.09e+02	1.00e-15										
4.42e+02	1.00e-15										
4.76e+02	1.00e-15										
5.10e+02	1.00e-15	9.37e-12	1.00e-15	1.00e-15							
5.45e+02	1.00e-15	1.11e-09	1.00e-15	1.00e-15							
5.81e+02	1.00e-15	3.60e-07	1.00e-15	1.00e-15							
6.17e+02	1.00e-15	3.63e-06	1.00e-15	1.00e-15							
6.55e+02	1.00e-15	1.68e-05	1.00e-15	1.00e-15							
6.93e+02	1.00e-15	5.26e-05	1.00e-15	1.00e-15							
7.33e+02	1.00e-15	1.16e-04	1.00e-15	1.00e-15							
7.73e+02	1.00e-15	1.89e-04	1.00e-15	1.00e-15							
8.14e+02	1.00e-15	2.38e-04	1.00e-15	1.00e-15							
8.56e+02	1.00e-15	2.36e-04	1.00e-15	1.00e-15							
9.00e+02	1.00e-15	1.97e-04	1.00e-15	1.00e-15							
9.44e+02	1.00e-15	1.41e-04	1.00e-15	1.00e-15							
9.89e+02	1.00e-15	9.21e-05	1.00e-15	1.00e-15							
1.04e+03	1.00e-15	5.77e-05	1.00e-15	1.00e-15							
1.08e+03	1.00e-15	3.59e-05	1.00e-15	1.00e-15							
1.13e+03	1.00e-15	2.28e-05	1.00e-15	1.00e-15							
1.18e+03	1.00e-15	1.42e-05	1.00e-15	1.00e-15							
1.23e+03	1.00e-15	8.68e-06	1.00e-15	1.00e-15							
1.28e+03	1.00e-15	5.36e-06	1.00e-15	1.00e-15							
1.34e+03	1.00e-15	3.10e-06	1.00e-15	1.00e-15							
1.39e+03	1.00e-15	2.09e-15	1.00e-15	1.00e-15	1.00e-15	1.00e-15	1.00e-15	1.00e-15	1.67e-06	1.00e-15	1.00e-15
1.45e+03	1.00e-15	6.66e-12	1.00e-15	1.00e-15	1.00e-15	1.00e-15	1.00e-15	2.69e-09	8.73e-07	1.00e-15	1.00e-15

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1.50e+03	1.00e-15	3.51e-10	1.00e-15	1.00e-15	1.00e-15	1.00e-15	9.43e-08	4.70e-07	1.00e-15	1.00e-15
1.56e+03	1.00e-15	2.89e-09	1.00e-15	1.00e-15	1.00e-15	1.00e-15	6.88e-07	2.37e-07	1.00e-15	2.70e-05
1.62e+03	1.00e-15	8.49e-09	1.00e-15	1.00e-15	1.00e-15	1.00e-15	1.85e-06	1.14e-07	1.00e-15	2.53e-04
1.68e+03	1.00e-15	1.12e-08	1.00e-15	1.69e-09	1.00e-15	1.00e-15	3.06e-06	5.45e-08	1.00e-15	5.18e-04
1.74e+03	1.00e-15	8.39e-09	1.00e-15	3.86e-07	1.00e-15	1.00e-15	3.96e-06	2.76e-08	1.00e-15	4.92e-04
1.81e+03	1.00e-15	5.13e-09	1.00e-15	2.21e-05	1.00e-15	1.00e-15	4.57e-06	1.65e-08	1.00e-15	4.09e-04
1.87e+03	1.00e-15	3.53e-09	1.00e-15	8.03e-05	1.00e-15	1.00e-15	5.03e-06	1.23e-08	1.00e-15	3.23e-04
1.94e+03	1.00e-15	3.62e-09	1.00e-15	1.52e-04	1.00e-15	1.00e-15	5.37e-06	1.13e-08	1.00e-15	2.48e-04
2.01e+03	1.00e-15	4.22e-09	1.00e-15	1.89e-04	1.00e-15	5.16e-08	5.64e-06	1.15e-08	1.00e-15	1.88e-04
2.08e+03	1.00e-15	5.39e-09	1.00e-15	1.78e-04	1.00e-15	2.04e-05	5.83e-06	1.22e-08	1.00e-15	1.45e-04
2.15e+03	1.00e-15	6.81e-09	1.00e-15	1.42e-04	1.00e-15	9.32e-05	5.93e-06	1.31e-08	1.00e-15	1.12e-04
2.23e+03	1.00e-15	8.32e-09	1.00e-15	1.04e-04	1.00e-15	1.28e-04	5.95e-06	1.40e-08	1.00e-15	8.87e-05
2.30e+03	1.00e-15	9.88e-09	1.00e-15	7.46e-05	1.00e-15	1.36e-04	5.91e-06	1.44e-08	1.00e-15	7.22e-05
2.38e+03	1.00e-15	1.13e-08	1.00e-15	5.33e-05	1.00e-15	1.32e-04	5.86e-06	1.49e-08	1.00e-15	6.11e-05
2.46e+03	1.00e-15	1.26e-08	1.00e-15	3.83e-05	1.00e-15	1.21e-04	5.86e-06	1.55e-08	1.00e-15	5.36e-05
2.54e+03	1.00e-15	1.38e-08	1.00e-15	2.79e-05	1.00e-15	1.07e-04	5.96e-06	1.60e-08	1.00e-15	4.86e-05
2.62e+03	1.00e-15	1.47e-08	1.00e-15	2.11e-05	1.00e-15	9.20e-05	6.15e-06	1.64e-08	1.00e-15	4.49e-05
2.70e+03	1.00e-15	1.53e-08	1.00e-15	1.66e-05	1.00e-15	7.70e-05	6.42e-06	1.66e-08	1.00e-15	4.21e-05
2.79e+03	1.00e-15	1.58e-08	1.00e-15	1.35e-05	1.00e-15	6.31e-05	6.70e-06	1.68e-08	1.00e-15	3.98e-05
2.88e+03	1.00e-15	1.60e-08	1.00e-15	1.15e-05	1.00e-15	5.08e-05	6.97e-06	1.71e-08	1.00e-15	3.78e-05
2.97e+03	1.00e-15	1.61e-08	1.00e-15	1.01e-05	1.00e-15	4.03e-05	7.17e-06	1.73e-08	1.00e-15	3.61e-05
3.06e+03	1.00e-15	1.61e-08	1.00e-15	9.19e-06	1.00e-15	3.14e-05	7.30e-06	1.75e-08	1.00e-15	3.45e-05
3.16e+03	1.00e-15	1.61e-08	1.00e-15	8.50e-06	1.00e-15	2.42e-05	7.35e-06	1.77e-08	1.00e-15	3.31e-05
3.25e+03	1.00e-15	1.61e-08	1.00e-15	8.00e-06	1.00e-15	1.84e-05	7.32e-06	1.79e-08	1.00e-15	3.19e-05
3.35e+03	1.00e-15	1.61e-08	1.00e-15	7.60e-06	1.00e-15	1.38e-05	7.25e-06	1.82e-08	1.00e-15	3.07e-05
3.45e+03	1.00e-15	1.61e-08	1.00e-15	7.27e-06	1.00e-15	1.03e-05	7.16e-06	1.86e-08	1.00e-15	2.96e-05
3.56e+03	1.00e-15	1.61e-08	1.00e-15	6.99e-06	1.00e-15	7.52e-06	7.06e-06	1.92e-08	1.00e-15	2.85e-05
3.66e+03	1.83e-13	1.61e-08	1.44e-15	6.73e-06	1.00e-15	5.46e-06	6.96e-06	2.01e-08	1.00e-15	2.75e-05
3.77e+03	1.94e-10	1.61e-08	7.20e-13	6.49e-06	1.00e-15	3.93e-06	6.86e-06	2.13e-08	1.00e-15	2.67e-05

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3.88e+03	4.01e-08	1.62e-08	1.33e-08	6.28e-06	1.00e-15	2.81e-06	6.76e-06	2.30e-08	1.00e-15	2.60e-05
4.00e+03	3.89e-07	1.62e-08	2.92e-07	6.07e-06	1.00e-15	2.03e-06	6.67e-06	2.54e-08	1.00e-15	2.53e-05
4.12e+03	1.50e-06	1.62e-08	6.14e-07	5.87e-06	1.00e-15	1.53e-06	6.59e-06	2.86e-08	1.00e-15	2.47e-05
4.24e+03	3.21e-06	1.62e-08	4.74e-07	5.69e-06	1.00e-15	1.25e-06	6.51e-06	3.28e-08	1.00e-15	2.42e-05
4.36e+03	4.68e-06	1.62e-08	2.63e-07	5.52e-06	1.00e-15	1.12e-06	6.43e-06	3.85e-08	1.00e-15	2.35e-05
4.48e+03	4.85e-06	1.62e-08	2.27e-07	5.35e-06	1.00e-15	1.11e-06	6.36e-06	4.60e-08	1.00e-15	2.29e-05
4.61e+03	3.77e-06	1.63e-08	4.49e-07	5.19e-06	1.00e-15	1.19e-06	6.30e-06	5.57e-08	1.00e-15	2.23e-05
4.74e+03	2.36e-06	1.63e-08	9.02e-07	5.03e-06	1.00e-15	1.33e-06	6.24e-06	6.82e-08	1.00e-15	2.17e-05
4.88e+03	1.29e-06	1.63e-08	1.37e-06	4.90e-06	1.00e-15	1.53e-06	6.19e-06	8.40e-08	1.00e-15	2.11e-05
5.01e+03	6.87e-07	1.64e-08	1.64e-06	4.80e-06	1.00e-15	1.76e-06	6.15e-06	1.04e-07	1.00e-15	2.06e-05
5.15e+03	3.95e-07	1.64e-08	1.71e-06	4.82e-06	1.00e-15	2.03e-06	6.11e-06	1.28e-07	1.00e-15	2.01e-05
5.30e+03	2.53e-07	1.65e-08	1.69e-06	5.15e-06	1.00e-15	2.32e-06	6.07e-06	1.58e-07	1.00e-15	1.96e-05
5.44e+03	1.80e-07	1.65e-08	1.64e-06	6.07e-06	1.00e-15	2.64e-06	6.04e-06	1.95e-07	1.00e-15	1.91e-05
5.59e+03	1.38e-07	1.66e-08	1.58e-06	8.05e-06	1.00e-15	2.98e-06	6.02e-06	2.38e-07	1.00e-15	1.86e-05
5.75e+03	1.13e-07	1.67e-08	1.53e-06	1.13e-05	1.00e-15	3.33e-06	6.00e-06	2.88e-07	1.00e-15	1.82e-05
5.91e+03	9.79e-08	1.68e-08	1.47e-06	1.55e-05	1.00e-15	3.72e-06	5.98e-06	3.47e-07	1.00e-15	1.77e-05
6.07e+03	8.80e-08	1.68e-08	1.41e-06	2.03e-05	1.00e-15	4.15e-06	5.97e-06	4.15e-07	1.00e-15	1.72e-05
6.23e+03	8.17e-08	1.69e-08	1.36e-06	2.49e-05	1.00e-15	4.65e-06	5.97e-06	4.90e-07	1.00e-15	1.69e-05
6.40e+03	7.73e-08	1.70e-08	1.31e-06	2.87e-05	1.00e-15	5.18e-06	5.96e-06	5.75e-07	1.00e-15	1.65e-05
6.58e+03	7.43e-08	1.71e-08	1.26e-06	3.16e-05	1.00e-15	5.69e-06	5.97e-06	6.66e-07	1.00e-15	1.61e-05
6.75e+03	7.20e-08	1.72e-08	1.21e-06	3.36e-05	1.00e-15	6.16e-06	5.98e-06	7.64e-07	1.00e-15	1.58e-05
6.93e+03	7.01e-08	1.73e-08	1.16e-06	3.51e-05	1.00e-15	6.61e-06	5.99e-06	8.67e-07	1.00e-15	1.55e-05
7.12e+03	6.86e-08	1.75e-08	1.11e-06	3.62e-05	1.00e-15	7.07e-06	6.01e-06	9.73e-07	1.00e-15	1.52e-05
7.31e+03	6.72e-08	1.76e-08	1.06e-06	3.73e-05	1.00e-15	7.54e-06	6.04e-06	1.08e-06	1.00e-15	1.49e-05
7.50e+03	6.59e-08	1.78e-08	1.02e-06	3.82e-05	1.00e-15	8.01e-06	6.07e-06	1.18e-06	1.00e-15	1.46e-05
7.70e+03	6.47e-08	1.79e-08	9.71e-07	3.92e-05	1.00e-15	8.50e-06	6.10e-06	1.28e-06	1.00e-15	1.43e-05
7.91e+03	6.36e-08	1.81e-08	9.28e-07	4.02e-05	3.28e-10	9.00e-06	6.14e-06	1.37e-06	1.00e-15	1.40e-05
8.11e+03	6.25e-08	1.82e-08	8.87e-07	4.12e-05	1.95e-08	9.52e-06	6.19e-06	1.45e-06	1.00e-15	1.38e-05
8.33e+03	6.14e-08	1.84e-08	8.47e-07	4.21e-05	8.68e-08	1.00e-05	6.24e-06	1.52e-06	1.00e-15	1.35e-05

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8.54e+03	6.04e-08	1.86e-08	8.08e-07	4.32e-05	2.16e-07	1.06e-05	6.29e-06	1.56e-06	1.00e-15	1.33e-05
8.77e+03	5.94e-08	1.88e-08	7.71e-07	4.42e-05	4.14e-07	1.12e-05	6.35e-06	1.59e-06	1.00e-15	1.30e-05
9.00e+03	5.91e-08	1.90e-08	7.35e-07	4.52e-05	6.57e-07	1.17e-05	6.41e-06	1.60e-06	1.00e-15	1.28e-05
9.23e+03	6.40e-08	1.92e-08	7.01e-07	4.63e-05	9.32e-07	1.23e-05	6.48e-06	1.58e-06	1.00e-15	1.26e-05
9.47e+03	9.13e-08	1.95e-08	6.68e-07	4.75e-05	1.33e-06	1.29e-05	6.55e-06	1.55e-06	1.00e-15	1.23e-05
9.71e+03	1.72e-07	1.97e-08	6.36e-07	4.87e-05	1.92e-06	1.36e-05	6.62e-06	1.49e-06	1.00e-15	1.21e-05
9.96e+03	3.19e-07	2.00e-08	6.06e-07	4.99e-05	2.65e-06	1.42e-05	6.70e-06	1.41e-06	1.00e-15	1.19e-05
1.02e+04	5.12e-07	2.03e-08	5.77e-07	5.12e-05	3.46e-06	1.49e-05	6.79e-06	1.32e-06	1.00e-15	1.17e-05
1.05e+04	7.20e-07	2.06e-08	5.49e-07	5.25e-05	4.37e-06	1.56e-05	6.88e-06	1.22e-06	1.00e-15	1.15e-05
1.08e+04	9.32e-07	2.09e-08	5.23e-07	5.39e-05	5.38e-06	1.64e-05	6.97e-06	1.11e-06	1.00e-15	1.13e-05
1.10e+04	1.14e-06	2.12e-08	4.98e-07	5.54e-05	6.47e-06	1.71e-05	7.07e-06	9.92e-07	1.00e-15	1.11e-05
1.13e+04	1.36e-06	2.15e-08	4.74e-07	5.70e-05	7.60e-06	1.79e-05	7.17e-06	8.74e-07	1.00e-15	1.09e-05
1.16e+04	1.57e-06	2.19e-08	4.52e-07	5.86e-05	8.58e-06	1.87e-05	7.28e-06	7.58e-07	1.00e-15	1.07e-05
1.19e+04	1.78e-06	2.23e-08	4.31e-07	6.03e-05	9.41e-06	1.96e-05	7.39e-06	6.48e-07	1.00e-15	1.05e-05
1.22e+04	1.99e-06	2.27e-08	4.10e-07	6.21e-05	1.02e-05	2.04e-05	7.51e-06	5.45e-07	1.00e-15	1.03e-05
1.25e+04	2.21e-06	2.31e-08	3.91e-07	6.40e-05	1.08e-05	2.14e-05	7.64e-06	4.51e-07	1.00e-15	1.01e-05
1.28e+04	2.43e-06	2.35e-08	3.73e-07	6.60e-05	1.15e-05	2.23e-05	7.77e-06	3.68e-07	1.00e-15	9.88e-06
1.31e+04	<b>2.53e+01</b>	2.40e-08	<b>7.23e+00</b>	<b>3.07e+02</b>	1.21e-05	2.33e-05	7.91e-06	2.96e-07	1.00e-15	8.50e-06
1.35e+04	<b>2.74e+01</b>	2.44e-08	<b>6.90e+00</b>	<b>3.17e+02</b>	1.26e-05	2.43e-05	8.06e-06	2.35e-07	1.00e-15	3.67e-06
1.38e+04	<b>2.96e+01</b>	2.49e-08	<b>6.59e+00</b>	<b>3.27e+02</b>	1.26e-05	<b>3.15e+02</b>	8.21e-06	1.84e-07	1.00e-15	1.93e-06
1.42e+04	<b>3.17e+01</b>	2.54e-08	<b>6.29e+00</b>	<b>3.38e+02</b>	1.19e-05	<b>3.29e+02</b>	8.37e-06	1.43e-07	1.00e-15	1.58e-06
1.45e+04	<b>3.40e+01</b>	2.60e-08	<b>6.01e+00</b>	<b>3.50e+02</b>	1.08e-05	<b>3.44e+02</b>	8.54e-06	1.11e-07	1.00e-15	1.50e-06
1.49e+04	<b>3.62e+01</b>	2.65e-08	<b>5.75e+00</b>	<b>3.62e+02</b>	9.52e-06	<b>3.59e+02</b>	8.72e-06	8.58e-08	1.00e-15	1.48e-06
1.52e+04	<b>3.85e+01</b>	2.71e-08	<b>5.50e+00</b>	<b>3.75e+02</b>	8.28e-06	<b>3.75e+02</b>	8.90e-06	6.68e-08	1.00e-15	1.46e-06
1.56e+04	<b>4.09e+01</b>	2.77e-08	<b>5.27e+00</b>	<b>3.89e+02</b>	7.26e-06	<b>3.91e+02</b>	9.09e-06	5.29e-08	1.00e-15	1.43e-06
1.60e+04	<b>4.34e+01</b>	2.83e-08	<b>5.06e+00</b>	<b>4.03e+02</b>	6.38e-06	<b>4.08e+02</b>	9.29e-06	4.29e-08	1.00e-15	1.38e-06
1.64e+04	<b>4.59e+01</b>	2.89e-08	<b>4.87e+00</b>	<b>4.18e+02</b>	5.55e-06	<b>4.26e+02</b>	9.50e-06	3.60e-08	1.00e-15	1.33e-06
1.68e+04	<b>4.85e+01</b>	2.92e-08	<b>4.69e+00</b>	<b>4.34e+02</b>	4.85e-06	<b>4.44e+02</b>	9.72e-06	3.13e-08	1.00e-15	1.28e-06
1.72e+04	<b>5.11e+01</b>	2.98e-08	<b>4.53e+00</b>	<b>4.51e+02</b>	4.37e-06	<b>4.64e+02</b>	9.95e-06	2.83e-08	1.00e-15	1.23e-06

## Scientific Notebook #170-10e

James Weldy

12/27/00

20-1402-762

1.77e+04	<b>5.40e+01</b>	3.05e-08	<b>4.36e+00</b>	<b>4.68e+02</b>	<b>5.55e+01</b>	<b>4.84e+02</b>	1.02e-05	2.65e-08	1.00e-15	1.18e-06
1.81e+04	<b>5.76e+01</b>	3.13e-08	<b>4.20e+00</b>	<b>4.87e+02</b>	<b>5.25e+01</b>	<b>5.04e+02</b>	1.04e-05	2.55e-08	1.00e-15	<b>1.65e+01</b>
1.85e+04	<b>6.10e+01</b>	<b>5.82e-01</b>	<b>4.05e+00</b>	<b>5.06e+02</b>	<b>5.22e+01</b>	<b>5.26e+02</b>	1.07e-05	<b>3.59e-01</b>	1.00e-15	<b>1.58e+01</b>
1.90e+04	<b>6.39e+01</b>	<b>5.97e-01</b>	<b>3.91e+00</b>	<b>5.26e+02</b>	<b>5.40e+01</b>	<b>5.48e+02</b>	1.10e-05	<b>3.59e-01</b>	1.00e-15	<b>1.51e+01</b>
1.95e+04	<b>6.70e+01</b>	<b>6.11e-01</b>	<b>3.77e+00</b>	<b>5.47e+02</b>	<b>5.78e+01</b>	<b>5.72e+02</b>	1.13e-05	<b>3.63e-01</b>	1.00e-15	<b>1.45e+01</b>
1.99e+04	<b>7.01e+01</b>	<b>6.26e-01</b>	<b>3.65e+00</b>	<b>5.68e+02</b>	<b>6.36e+01</b>	<b>5.96e+02</b>	1.15e-05	<b>3.70e-01</b>	1.00e-15	<b>1.38e+01</b>
2.04e+04	<b>7.34e+01</b>	<b>6.41e-01</b>	<b>3.53e+00</b>	<b>5.91e+02</b>	<b>7.15e+01</b>	<b>6.20e+02</b>	1.18e-05	<b>3.78e-01</b>	1.00e-15	<b>1.32e+01</b>
2.09e+04	<b>7.67e+01</b>	<b>6.56e-01</b>	<b>3.42e+00</b>	<b>6.14e+02</b>	<b>8.04e+01</b>	<b>6.46e+02</b>	1.22e-05	<b>3.87e-01</b>	1.00e-15	<b>1.26e+01</b>
2.15e+04	<b>8.02e+01</b>	<b>6.71e-01</b>	<b>3.31e+00</b>	<b>6.38e+02</b>	<b>8.94e+01</b>	<b>6.72e+02</b>	1.25e-05	<b>3.97e-01</b>	1.00e-15	<b>1.20e+01</b>
2.20e+04	<b>8.38e+01</b>	<b>6.85e-01</b>	<b>3.21e+00</b>	<b>6.63e+02</b>	<b>9.79e+01</b>	<b>6.99e+02</b>	1.28e-05	<b>4.08e-01</b>	1.00e-15	<b>1.14e+01</b>
2.25e+04	<b>8.75e+01</b>	<b>7.00e-01</b>	<b>3.12e+00</b>	<b>6.89e+02</b>	<b>1.05e+02</b>	<b>7.27e+02</b>	1.31e-05	<b>4.20e-01</b>	1.00e-15	<b>1.08e+01</b>
2.31e+04	<b>9.14e+01</b>	<b>7.15e-01</b>	<b>3.03e+00</b>	<b>7.15e+02</b>	<b>1.12e+02</b>	<b>7.56e+02</b>	<b>1.64e+02</b>	<b>4.32e-01</b>	1.00e-15	<b>1.03e+01</b>
2.36e+04	<b>9.53e+01</b>	<b>7.30e-01</b>	<b>2.94e+00</b>	<b>7.42e+02</b>	<b>1.17e+02</b>	<b>7.85e+02</b>	<b>1.68e+02</b>	<b>4.45e-01</b>	1.00e-15	<b>9.74e+00</b>
2.42e+04	<b>9.75e+01</b>	<b>7.44e-01</b>	<b>2.86e+00</b>	<b>7.69e+02</b>	<b>1.22e+02</b>	<b>8.14e+02</b>	<b>1.73e+02</b>	<b>4.58e-01</b>	1.00e-15	<b>9.22e+00</b>
2.48e+04	<b>9.26e+01</b>	<b>7.58e-01</b>	<b>2.78e+00</b>	<b>7.95e+02</b>	<b>1.25e+02</b>	<b>8.45e+02</b>	<b>1.77e+02</b>	<b>4.72e-01</b>	1.00e-15	<b>8.72e+00</b>
2.54e+04	<b>8.45e+01</b>	<b>7.72e-01</b>	<b>2.71e+00</b>	<b>7.93e+02</b>	<b>1.27e+02</b>	<b>8.75e+02</b>	<b>1.82e+02</b>	<b>4.87e-01</b>	1.00e-15	<b>8.23e+00</b>
2.60e+04	<b>7.69e+01</b>	<b>7.85e-01</b>	<b>2.64e+00</b>	<b>7.29e+02</b>	<b>1.28e+02</b>	<b>9.06e+02</b>	<b>1.86e+02</b>	<b>5.02e-01</b>	1.00e-15	<b>7.76e+00</b>
2.66e+04	<b>7.00e+01</b>	<b>7.98e-01</b>	<b>2.57e+00</b>	<b>6.47e+02</b>	<b>1.29e+02</b>	<b>9.37e+02</b>	<b>1.91e+02</b>	<b>5.18e-01</b>	1.00e-15	<b>7.31e+00</b>
2.73e+04	<b>6.36e+01</b>	<b>8.10e-01</b>	<b>2.50e+00</b>	<b>5.72e+02</b>	<b>1.30e+02</b>	<b>9.68e+02</b>	<b>1.96e+02</b>	<b>5.35e-01</b>	1.00e-15	<b>6.87e+00</b>
2.80e+04	<b>5.78e+01</b>	<b>8.22e-01</b>	<b>2.44e+00</b>	<b>5.07e+02</b>	<b>1.31e+02</b>	<b>9.99e+02</b>	<b>2.01e+02</b>	<b>5.52e-01</b>	1.00e-15	<b>6.45e+00</b>
2.86e+04	<b>5.25e+01</b>	<b>8.33e-01</b>	<b>2.38e+00</b>	<b>4.50e+02</b>	<b>1.32e+02</b>	<b>1.03e+03</b>	<b>2.05e+02</b>	<b>5.70e-01</b>	1.00e-15	<b>6.05e+00</b>
2.93e+04	<b>4.78e+01</b>	<b>8.43e-01</b>	<b>2.33e+00</b>	<b>3.99e+02</b>	<b>1.33e+02</b>	<b>1.06e+03</b>	<b>2.10e+02</b>	<b>5.89e-01</b>	1.00e-15	<b>5.66e+00</b>
3.00e+04	<b>4.34e+01</b>	<b>8.53e-01</b>	<b>2.28e+00</b>	<b>3.56e+02</b>	<b>1.34e+02</b>	<b>1.09e+03</b>	<b>2.15e+02</b>	<b>6.08e-01</b>	1.00e-15	<b>5.30e+00</b>
3.08e+04	<b>3.95e+01</b>	<b>8.62e-01</b>	<b>2.22e+00</b>	<b>3.18e+02</b>	<b>1.35e+02</b>	<b>1.12e+03</b>	<b>2.20e+02</b>	<b>6.29e-01</b>	1.00e-15	<b>4.94e+00</b>
3.15e+04	<b>3.60e+01</b>	<b>8.70e-01</b>	<b>2.18e+00</b>	<b>2.85e+02</b>	<b>1.35e+02</b>	<b>1.15e+03</b>	<b>2.25e+02</b>	<b>6.49e-01</b>	1.00e-15	<b>4.60e+00</b>
3.23e+04	<b>3.29e+01</b>	<b>8.75e-01</b>	<b>2.13e+00</b>	<b>2.57e+02</b>	<b>1.36e+02</b>	<b>1.18e+03</b>	<b>2.29e+02</b>	<b>6.71e-01</b>	1.00e-15	<b>4.28e+00</b>
3.30e+04	<b>3.00e+01</b>	<b>7.84e-01</b>	<b>2.08e+00</b>	<b>2.32e+02</b>	<b>1.37e+02</b>	<b>1.20e+03</b>	<b>2.34e+02</b>	<b>6.93e-01</b>	1.00e-15	<b>3.98e+00</b>
3.38e+04	<b>2.75e+01</b>	<b>6.35e-01</b>	<b>2.04e+00</b>	<b>2.11e+02</b>	<b>1.38e+02</b>	<b>1.23e+03</b>	<b>2.39e+02</b>	<b>7.17e-01</b>	1.00e-15	<b>3.69e+00</b>
3.47e+04	<b>2.52e+01</b>	<b>5.17e-01</b>	<b>2.00e+00</b>	<b>1.93e+02</b>	<b>1.39e+02</b>	<b>1.26e+03</b>	<b>2.43e+02</b>	<b>7.53e-01</b>	1.00e-15	<b>3.41e+00</b>

## Scientific Notebook #170-10e

James Weldy

12/27/00

20-1402-762

3.55e+04	2.32e+01	4.25e-01	1.96e+00	1.78e+02	1.41e+02	1.28e+03	2.47e+02	8.54e-01	1.00e-15	3.15e+00
3.63e+04	2.14e+01	3.55e-01	1.93e+00	1.64e+02	1.43e+02	1.30e+03	2.52e+02	1.26e+00	1.00e-15	2.92e+00
3.72e+04	1.99e+01	3.01e-01	1.89e+00	1.53e+02	1.45e+02	1.32e+03	2.56e+02	2.77e+00	1.00e-15	4.22e+00
3.81e+04	1.85e+01	2.60e-01	1.85e+00	1.43e+02	1.48e+02	1.34e+03	2.60e+02	7.35e+00	1.00e-15	3.30e+01
3.90e+04	1.72e+01	2.29e-01	1.82e+00	1.35e+02	1.51e+02	1.36e+03	2.63e+02	1.87e+01	1.00e-15	1.53e+02
4.00e+04	1.61e+01	2.06e-01	1.79e+00	1.28e+02	1.56e+02	1.38e+03	2.67e+02	4.28e+01	1.00e-15	2.71e+02
4.09e+04	1.51e+01	1.88e-01	1.76e+00	1.22e+02	1.60e+02	1.39e+03	2.71e+02	8.37e+01	1.00e-15	3.07e+02
4.19e+04	1.43e+01	1.75e-01	1.73e+00	1.17e+02	1.66e+02	1.41e+03	2.74e+02	1.43e+02	1.00e-15	3.22e+02
4.29e+04	1.35e+01	1.65e-01	1.71e+00	1.12e+02	1.72e+02	1.42e+03	2.77e+02	2.17e+02	1.00e-15	3.38e+02
4.39e+04	1.29e+01	1.57e-01	1.68e+00	1.08e+02	1.79e+02	1.43e+03	2.80e+02	2.99e+02	1.00e-15	3.59e+02
4.50e+04	1.23e+01	1.51e-01	1.65e+00	1.04e+02	1.87e+02	1.44e+03	2.83e+02	3.81e+02	1.00e-15	3.83e+02
4.61e+04	1.18e+01	1.47e-01	1.63e+00	9.85e+01	1.96e+02	1.45e+03	2.86e+02	4.59e+02	1.00e-15	4.11e+02
4.72e+04	1.13e+01	1.43e-01	1.61e+00	9.51e+01	2.05e+02	1.46e+03	2.89e+02	5.32e+02	1.00e-15	4.44e+02
4.83e+04	1.09e+01	1.40e-01	1.59e+00	9.22e+01	2.15e+02	1.47e+03	2.91e+02	6.02e+02	1.00e-15	4.82e+02
4.95e+04	1.06e+01	1.38e-01	1.57e+00	8.22e+01	2.25e+02	1.48e+03	2.94e+02	6.71e+02	1.00e-15	5.25e+02
5.06e+04	1.02e+01	1.36e-01	1.56e+00	6.45e+01	2.36e+02	1.48e+03	2.96e+02	7.42e+02	1.00e-15	5.72e+02
5.18e+04	9.97e+00	1.34e-01	1.53e+00	4.83e+01	2.46e+02	1.49e+03	2.98e+02	1.86e+04	1.30e-01	6.23e+02
5.31e+04	9.73e+00	1.32e-01	1.51e+00	3.59e+01	2.56e+02	1.50e+03	3.00e+02	4.22e+04	3.96e+02	6.77e+02
5.43e+04	9.51e+00	1.31e-01	1.49e+00	2.65e+01	2.66e+02	1.50e+03	3.02e+02	3.75e+04	6.97e+02	7.35e+02
5.56e+04	9.31e+00	1.29e-01	1.48e+00	1.95e+01	2.75e+02	1.51e+03	3.04e+02	3.55e+04	1.07e+03	7.95e+02
5.70e+04	9.13e+00	1.28e-01	1.46e+00	1.42e+01	2.83e+02	3.13e+04	3.05e+02	3.47e+04	3.88e+03	8.57e+02
5.83e+04	8.97e+00	1.26e-01	1.44e+00	1.04e+01	2.90e+02	5.44e+04	3.07e+02	3.48e+04	6.49e+03	9.18e+02
5.97e+04	8.82e+00	1.25e-01	1.42e+00	7.54e+00	2.97e+02	8.70e+04	3.08e+02	3.58e+04	8.44e+03	9.78e+02
6.11e+04	8.68e+00	1.24e-01	1.40e+00	5.48e+00	3.03e+02	1.22e+05	3.09e+02	3.69e+04	9.88e+03	1.04e+03
6.26e+04	8.55e+00	1.23e-01	1.38e+00	3.99e+00	3.07e+02	1.53e+05	3.10e+02	3.74e+04	1.09e+04	1.09e+03
6.41e+04	8.43e+00	1.22e-01	1.37e+00	2.92e+00	3.12e+02	1.80e+05	3.10e+02	3.73e+04	1.16e+04	1.14e+03
6.56e+04	8.32e+00	1.21e-01	1.35e+00	2.78e+03	3.15e+02	2.02e+05	3.09e+02	3.68e+04	1.21e+04	1.18e+03
6.72e+04	8.21e+00	1.19e-01	1.34e+00	4.05e+03	3.18e+02	2.20e+05	3.08e+02	2.88e+04	1.23e+04	1.22e+03
6.87e+04	8.13e+00	1.18e-01	1.33e+00	6.11e+03	3.20e+02	2.33e+05	2.53e-05	1.68e+04	1.24e+04	1.25e+03

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7.04e+04	8.06e+00	5.85e+01	1.31e+00	2.58e+04	3.22e+02	2.42e+05	2.50e-05	1.03e+04	1.24e+04	1.27e+03
7.21e+04	8.00e+00	1.61e+02	1.30e+00	4.49e+04	3.23e+02	2.47e+05	2.47e-05	7.91e+03	1.32e-03	1.29e+03
7.38e+04	7.96e+00	1.22e-05	1.29e+00	5.76e+04	2.09e-05	2.47e+05	2.42e-05	4.06e-04	1.30e-03	9.21e-05
7.55e+04	7.93e+00	1.34e-05	1.27e+00	6.58e+04	2.09e-05	2.44e+05	2.36e-05	3.22e-04	1.26e-03	9.27e-05
7.73e+04	7.91e+00	1.37e-05	1.61e+00	7.09e+04	2.09e-05	1.95e-02	2.29e-05	2.37e-04	1.22e-03	9.31e-05
7.91e+04	8.27e-07	1.35e-05	1.60e-04	1.64e-02	2.09e-05	1.86e-02	2.21e-05	1.75e-04	1.18e-03	9.33e-05
8.10e+04	8.28e-07	1.31e-05	2.52e-04	1.67e-02	2.06e-05	1.67e-02	8.30e-05	1.42e-04	1.13e-03	9.34e-05
8.29e+04	8.30e-07	1.25e-05	2.66e-04	1.69e-02	1.99e-05	1.47e-02	3.08e-04	1.28e-04	1.07e-03	9.35e-05
8.49e+04	8.33e-07	1.16e-05	2.67e-04	1.69e-02	1.85e-05	1.32e-02	5.30e-04	1.23e-04	1.01e-03	9.35e-05
8.69e+04	8.38e-07	1.05e-05	2.61e-04	1.67e-02	1.68e-05	1.17e-02	7.39e-04	1.26e-04	9.56e-04	9.40e-05
8.90e+04	8.44e-07	9.53e-06	2.51e-04	1.65e-02	1.55e-05	1.04e-02	9.29e-04	2.32e-04	9.01e-04	9.41e-05
9.11e+04	8.52e-07	8.66e-06	2.44e-04	1.61e-02	1.44e-05	9.13e-03	1.10e-03	1.10e-03	8.52e-04	9.41e-05
9.32e+04	8.59e-07	8.00e-06	2.46e-04	1.51e-02	1.36e-05	8.02e-03	1.25e-03	3.75e-03	8.12e-04	9.41e-05
9.54e+04	8.67e-07	7.59e-06	2.52e-04	1.37e-02	1.29e-05	7.06e-03	1.39e-03	7.21e-03	7.85e-04	9.38e-05
9.77e+04	8.75e-07	7.47e-06	2.67e-04	1.25e-02	1.23e-05	6.29e-03	1.53e-03	9.62e-03	7.79e-04	9.32e-05
1.00e+05	8.83e-07	7.53e-06	2.88e-04	1.18e-02	1.18e-05	5.72e-03	1.65e-03	1.07e-02	7.98e-04	9.21e-05
1.10e+05	1.00e-15									

It can be seen that in the original code, the time of the pluvial switch jumps around. In the corrected version of the code, the following results can be seen:

Year	Dose 1	Dose 2	Dose 3								Dose 4		Dose 5		Dose 6		Dose 7		Dose 8		Dose 9		Dose 10	
	(r e m / y r)	(r e m / y r)	(r e m / y r)								(re e m/ m/y yr)													

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2.31e+01	1.00e-15	* Note that Years in Pluvial Climate are in Bold											
4.67e+01	1.00e-15	* If code is Functioning Properly, Pluvial Climate											
7.09e+01	1.00e-15	* Should be Between 13000 and 77500 Years											
9.57e+01	1.00e-15	* For Every Realization											
1.21e+02	1.00e-15												
1.47e+02	1.00e-15												
1.74e+02	1.00e-15												
2.01e+02	1.00e-15												
2.28e+02	1.00e-15												
2.57e+02	1.00e-15												
2.86e+02	1.00e-15												
3.16e+02	1.00e-15												
3.46e+02	1.00e-15												
3.78e+02	1.00e-15												
4.09e+02	1.00e-15												
4.42e+02	1.00e-15												

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4.76e+02	1.00e-15										
5.10e+02	1.00e-15	9.37e-12	1.00e-15	1.00e-15							
5.45e+02	1.00e-15	1.12e-09	1.00e-15	1.00e-15							
5.81e+02	1.00e-15	4.12e-07	1.00e-15	1.00e-15							
6.17e+02	1.00e-15	4.12e-06	1.00e-15	1.00e-15							
6.55e+02	1.00e-15	1.83e-05	1.00e-15	1.00e-15							
6.93e+02	1.00e-15	5.60e-05	1.00e-15	1.00e-15							
7.33e+02	1.00e-15	1.22e-04	1.00e-15	1.00e-15							
7.73e+02	1.00e-15	1.98e-04	1.00e-15	1.00e-15							
8.14e+02	1.00e-15	2.50e-04	1.00e-15	1.00e-15							
8.56e+02	1.00e-15	2.49e-04	1.00e-15	1.00e-15							
9.00e+02	1.00e-15	2.10e-04	1.00e-15	1.00e-15							
9.44e+02	1.00e-15	1.53e-04	1.00e-15	1.00e-15							
9.89e+02	1.00e-15	1.02e-04	1.00e-15	1.00e-15							
1.04e+03	1.00e-15	6.57e-05	1.00e-15	1.00e-15							
1.08e+03	1.00e-15	4.18e-05	1.00e-15	1.00e-15							
1.13e+03	1.00e-15	2.70e-05	1.00e-15	1.00e-15							
1.18e+03	1.00e-15	1.70e-05	1.00e-15	1.00e-15							
1.23e+03	1.00e-15	1.04e-05	1.00e-15	1.00e-15							
1.28e+03	1.00e-15	6.46e-06	1.00e-15	1.00e-15							
1.34e+03	1.00e-15	3.74e-06	1.00e-15	1.00e-15							
1.39e+03	1.00e-15	2.09e-15	1.00e-15	1.00e-15	1.00e-15	1.00e-15	1.00e-15	1.00e-15	2.02e-06	1.00e-15	1.00e-15
1.45e+03	1.00e-15	6.67e-12	1.00e-15	1.00e-15	1.00e-15	1.00e-15	1.00e-15	3.53e-09	1.05e-06	1.00e-15	1.00e-15
1.50e+03	1.00e-15	3.51e-10	1.00e-15	1.00e-15	1.00e-15	1.00e-15	1.00e-15	1.13e-07	5.66e-07	1.00e-15	1.00e-15
1.56e+03	1.00e-15	2.92e-09	1.00e-15	1.00e-15	1.00e-15	1.00e-15	1.00e-15	8.14e-07	2.85e-07	1.00e-15	4.11e-05
1.62e+03	1.00e-15	8.72e-09	1.00e-15	1.00e-15	1.00e-15	1.00e-15	1.00e-15	2.18e-06	1.37e-07	1.00e-15	3.85e-04
1.68e+03	1.00e-15	1.15e-08	1.00e-15	4.23e-09	1.00e-15	1.00e-15	3.60e-06	6.45e-08	1.00e-15	7.85e-04	
1.74e+03	1.00e-15	8.58e-09	1.00e-15	9.62e-07	1.00e-15	1.00e-15	4.69e-06	3.19e-08	1.00e-15	7.29e-04	
1.81e+03	1.00e-15	5.22e-09	1.00e-15	5.45e-05	1.00e-15	1.00e-15	5.45e-06	1.82e-08	1.00e-15	5.82e-04	

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1.87e+03	1.00e-15	3.60e-09	1.00e-15	1.91e-04	1.00e-15	1.00e-15	6.03e-06	1.30e-08	1.00e-15	4.47e-04
1.94e+03	1.00e-15	3.69e-09	1.00e-15	3.46e-04	1.00e-15	1.00e-15	6.47e-06	1.16e-08	1.00e-15	3.39e-04
2.01e+03	1.00e-15	4.28e-09	1.00e-15	4.15e-04	1.00e-15	7.32e-08	6.81e-06	1.17e-08	1.00e-15	2.54e-04
2.08e+03	1.00e-15	5.45e-09	1.00e-15	3.90e-04	1.00e-15	3.03e-05	7.05e-06	1.23e-08	1.00e-15	1.94e-04
2.15e+03	1.00e-15	6.87e-09	1.00e-15	3.19e-04	1.00e-15	1.34e-04	7.19e-06	1.32e-08	1.00e-15	1.49e-04
2.23e+03	1.00e-15	8.37e-09	1.00e-15	2.43e-04	1.00e-15	1.78e-04	7.22e-06	1.40e-08	1.00e-15	1.17e-04
2.30e+03	1.00e-15	9.93e-09	1.00e-15	1.79e-04	1.00e-15	1.86e-04	7.18e-06	1.45e-08	1.00e-15	9.45e-05
2.38e+03	1.00e-15	1.13e-08	1.00e-15	1.29e-04	1.00e-15	1.80e-04	7.11e-06	1.50e-08	1.00e-15	7.98e-05
2.46e+03	1.00e-15	1.27e-08	1.00e-15	9.35e-05	1.00e-15	1.65e-04	7.10e-06	1.55e-08	1.00e-15	7.00e-05
2.54e+03	1.00e-15	1.38e-08	1.00e-15	6.80e-05	1.00e-15	1.46e-04	7.18e-06	1.60e-08	1.00e-15	6.33e-05
2.62e+03	1.00e-15	1.48e-08	1.00e-15	5.10e-05	1.00e-15	1.25e-04	7.35e-06	1.65e-08	1.00e-15	5.84e-05
2.70e+03	1.00e-15	1.54e-08	1.00e-15	3.97e-05	1.00e-15	1.05e-04	7.59e-06	1.67e-08	1.00e-15	5.47e-05
2.79e+03	1.00e-15	1.58e-08	1.00e-15	3.21e-05	1.00e-15	8.61e-05	7.85e-06	1.69e-08	1.00e-15	5.17e-05
2.88e+03	1.00e-15	1.60e-08	1.00e-15	2.70e-05	1.00e-15	6.96e-05	8.08e-06	1.71e-08	1.00e-15	4.91e-05
2.97e+03	1.00e-15	1.62e-08	1.00e-15	2.37e-05	1.00e-15	5.53e-05	8.26e-06	1.74e-08	1.00e-15	4.68e-05
3.06e+03	1.00e-15	1.62e-08	1.00e-15	2.14e-05	1.00e-15	4.33e-05	8.36e-06	1.75e-08	1.00e-15	4.48e-05
3.16e+03	1.00e-15	1.62e-08	1.00e-15	1.97e-05	1.00e-15	3.35e-05	8.38e-06	1.77e-08	1.00e-15	4.30e-05
3.25e+03	1.00e-15	1.62e-08	1.00e-15	1.85e-05	1.00e-15	2.56e-05	8.32e-06	1.79e-08	1.00e-15	4.14e-05
3.35e+03	1.00e-15	1.62e-08	1.00e-15	1.76e-05	1.00e-15	1.93e-05	8.22e-06	1.83e-08	1.00e-15	3.99e-05
3.45e+03	1.00e-15	1.62e-08	1.00e-15	1.68e-05	1.00e-15	1.44e-05	8.09e-06	1.87e-08	1.00e-15	3.84e-05
3.56e+03	1.00e-15	1.62e-08	1.00e-15	1.61e-05	1.00e-15	1.06e-05	7.95e-06	1.93e-08	1.00e-15	3.70e-05
3.66e+03	1.84e-13	1.62e-08	1.54e-15	1.55e-05	1.00e-15	7.73e-06	7.82e-06	2.02e-08	1.00e-15	3.58e-05
3.77e+03	1.95e-10	1.62e-08	7.51e-13	1.49e-05	1.00e-15	5.58e-06	7.69e-06	2.14e-08	1.00e-15	3.47e-05
3.88e+03	4.04e-08	1.62e-08	1.40e-08	1.44e-05	1.00e-15	4.00e-06	7.56e-06	2.31e-08	1.00e-15	3.37e-05
4.00e+03	3.93e-07	1.62e-08	3.10e-07	1.39e-05	1.00e-15	2.89e-06	7.45e-06	2.55e-08	1.00e-15	3.28e-05
4.12e+03	1.51e-06	1.62e-08	6.55e-07	1.35e-05	1.00e-15	2.14e-06	7.33e-06	2.87e-08	1.00e-15	3.20e-05
4.24e+03	3.27e-06	1.62e-08	5.06e-07	1.30e-05	1.00e-15	1.68e-06	7.23e-06	3.30e-08	1.00e-15	3.12e-05
4.36e+03	4.79e-06	1.63e-08	2.81e-07	1.26e-05	1.00e-15	1.42e-06	7.13e-06	3.87e-08	1.00e-15	3.04e-05
4.48e+03	5.00e-06	1.63e-08	2.36e-07	1.23e-05	1.00e-15	1.33e-06	7.03e-06	4.62e-08	1.00e-15	2.95e-05

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4.61e+03	3.92e-06	1.63e-08	4.56e-07	1.19e-05	1.00e-15	1.34e-06	6.95e-06	5.60e-08	1.00e-15	2.87e-05
4.74e+03	2.48e-06	1.63e-08	9.11e-07	1.15e-05	1.00e-15	1.44e-06	6.87e-06	6.85e-08	1.00e-15	2.80e-05
4.88e+03	1.37e-06	1.64e-08	1.38e-06	1.12e-05	1.00e-15	1.61e-06	6.80e-06	8.44e-08	1.00e-15	2.72e-05
5.01e+03	7.36e-07	1.64e-08	1.65e-06	1.09e-05	1.00e-15	1.83e-06	6.73e-06	1.04e-07	1.00e-15	2.65e-05
5.15e+03	4.26e-07	1.65e-08	1.73e-06	1.07e-05	1.00e-15	2.09e-06	6.68e-06	1.29e-07	1.00e-15	2.58e-05
5.30e+03	2.74e-07	1.65e-08	1.70e-06	1.09e-05	1.00e-15	2.38e-06	6.62e-06	1.59e-07	1.00e-15	2.52e-05
5.44e+03	1.93e-07	1.66e-08	1.65e-06	1.16e-05	1.00e-15	2.69e-06	6.58e-06	1.96e-07	1.00e-15	2.45e-05
5.59e+03	1.48e-07	1.66e-08	1.59e-06	1.35e-05	1.00e-15	3.03e-06	6.54e-06	2.39e-07	1.00e-15	2.39e-05
5.75e+03	1.20e-07	1.67e-08	1.54e-06	1.66e-05	1.00e-15	3.39e-06	6.51e-06	2.90e-07	1.00e-15	2.33e-05
5.91e+03	1.03e-07	1.68e-08	1.48e-06	2.07e-05	1.00e-15	3.78e-06	6.48e-06	3.49e-07	1.00e-15	2.27e-05
6.07e+03	9.22e-08	1.69e-08	1.43e-06	2.54e-05	1.00e-15	4.23e-06	6.45e-06	4.17e-07	1.00e-15	2.21e-05
6.23e+03	8.52e-08	1.69e-08	1.37e-06	2.99e-05	1.00e-15	4.74e-06	6.43e-06	4.93e-07	1.00e-15	2.16e-05
6.40e+03	8.05e-08	1.70e-08	1.32e-06	3.36e-05	1.00e-15	5.29e-06	6.42e-06	5.78e-07	1.00e-15	2.11e-05
6.58e+03	7.71e-08	1.71e-08	1.27e-06	3.64e-05	1.00e-15	5.81e-06	6.41e-06	6.70e-07	1.00e-15	2.06e-05
6.75e+03	7.46e-08	1.73e-08	1.21e-06	3.83e-05	1.00e-15	6.29e-06	6.41e-06	7.69e-07	1.00e-15	2.02e-05
6.93e+03	7.27e-08	1.74e-08	1.16e-06	3.97e-05	1.00e-15	6.75e-06	6.42e-06	8.73e-07	1.00e-15	1.97e-05
7.12e+03	7.10e-08	1.75e-08	1.12e-06	4.08e-05	1.00e-15	7.22e-06	6.43e-06	9.79e-07	1.00e-15	1.93e-05
7.31e+03	6.96e-08	1.76e-08	1.07e-06	4.17e-05	1.00e-15	7.69e-06	6.44e-06	1.09e-06	1.00e-15	1.89e-05
7.50e+03	6.82e-08	1.78e-08	1.02e-06	4.26e-05	1.00e-15	8.17e-06	6.47e-06	1.19e-06	1.00e-15	1.86e-05
7.70e+03	6.70e-08	1.79e-08	9.78e-07	4.35e-05	1.00e-15	8.67e-06	6.49e-06	1.29e-06	1.00e-15	1.82e-05
7.91e+03	6.58e-08	1.81e-08	9.35e-07	4.43e-05	3.30e-10	9.18e-06	6.53e-06	1.38e-06	1.00e-15	1.78e-05
8.11e+03	6.46e-08	1.83e-08	8.93e-07	4.52e-05	1.96e-08	9.70e-06	6.56e-06	1.46e-06	1.00e-15	1.75e-05
8.33e+03	6.35e-08	1.84e-08	8.53e-07	4.62e-05	8.72e-08	1.02e-05	6.61e-06	1.53e-06	1.00e-15	1.72e-05
8.54e+03	6.24e-08	1.86e-08	8.14e-07	4.71e-05	2.17e-07	1.08e-05	6.65e-06	1.57e-06	1.00e-15	1.69e-05
8.77e+03	6.14e-08	1.88e-08	7.77e-07	4.81e-05	4.16e-07	1.14e-05	6.71e-06	1.60e-06	1.00e-15	1.66e-05
9.00e+03	6.11e-08	1.90e-08	7.40e-07	4.91e-05	6.61e-07	1.20e-05	6.77e-06	1.61e-06	1.00e-15	1.62e-05
9.23e+03	6.60e-08	1.93e-08	7.06e-07	5.01e-05	9.37e-07	1.26e-05	6.83e-06	1.59e-06	1.00e-15	1.60e-05
9.47e+03	9.36e-08	1.95e-08	6.72e-07	5.12e-05	1.33e-06	1.32e-05	6.89e-06	1.55e-06	1.00e-15	1.57e-05
9.71e+03	1.75e-07	1.98e-08	6.41e-07	5.23e-05	1.93e-06	1.38e-05	6.97e-06	1.50e-06	1.00e-15	1.54e-05

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9.96e+03	3.24e-07	2.00e-08	6.10e-07	5.35e-05	2.67e-06	1.45e-05	7.04e-06	1.42e-06	1.00e-15	1.51e-05
1.02e+04	5.19e-07	2.03e-08	5.81e-07	5.47e-05	3.48e-06	1.52e-05	7.12e-06	1.33e-06	1.00e-15	1.48e-05
1.05e+04	7.30e-07	2.06e-08	5.53e-07	5.60e-05	4.39e-06	1.59e-05	7.21e-06	1.23e-06	1.00e-15	1.46e-05
1.08e+04	9.45e-07	2.09e-08	5.27e-07	5.74e-05	5.42e-06	1.67e-05	7.30e-06	1.12e-06	1.00e-15	1.43e-05
1.10e+04	1.16e-06	2.12e-08	5.02e-07	5.88e-05	6.52e-06	1.74e-05	7.39e-06	9.98e-07	1.00e-15	1.40e-05
1.13e+04	1.37e-06	2.16e-08	4.78e-07	6.03e-05	7.65e-06	1.82e-05	7.49e-06	8.79e-07	1.00e-15	1.38e-05
1.16e+04	1.59e-06	2.19e-08	4.55e-07	6.19e-05	8.65e-06	1.91e-05	7.60e-06	7.63e-07	1.00e-15	1.35e-05
1.19e+04	1.80e-06	2.23e-08	4.34e-07	6.35e-05	9.48e-06	1.99e-05	7.71e-06	6.52e-07	1.00e-15	1.32e-05
1.22e+04	2.02e-06	2.27e-08	4.14e-07	6.53e-05	1.02e-05	2.08e-05	7.82e-06	5.48e-07	1.00e-15	1.30e-05
1.25e+04	2.24e-06	2.31e-08	3.94e-07	6.71e-05	1.09e-05	2.17e-05	7.95e-06	4.54e-07	1.00e-15	1.27e-05
1.28e+04	2.46e-06	2.35e-08	3.76e-07	6.91e-05	1.16e-05	2.27e-05	8.08e-06	3.70e-07	1.00e-15	1.25e-05
1.31e+04	<b>2.54e+01</b>	<b>4.35e-01</b>	<b>7.32e+00</b>	<b>3.27e+02</b>	<b>1.65e+02</b>	<b>2.95e+02</b>	<b>1.01e+02</b>	<b>4.59e+00</b>	<b>1.00e-15</b>	<b>1.70e+02</b>
1.35e+04	<b>2.75e+01</b>	<b>4.44e-01</b>	<b>6.98e+00</b>	<b>3.36e+02</b>	<b>1.73e+02</b>	<b>3.08e+02</b>	<b>1.03e+02</b>	<b>3.64e+00</b>	<b>1.00e-15</b>	<b>6.37e+01</b>
1.38e+04	<b>2.96e+01</b>	<b>4.53e-01</b>	<b>6.66e+00</b>	<b>3.46e+02</b>	<b>1.74e+02</b>	<b>3.22e+02</b>	<b>1.04e+02</b>	<b>2.84e+00</b>	<b>1.00e-15</b>	<b>3.08e+01</b>
1.42e+04	<b>3.18e+01</b>	<b>4.62e-01</b>	<b>6.37e+00</b>	<b>3.57e+02</b>	<b>1.64e+02</b>	<b>3.36e+02</b>	<b>1.06e+02</b>	<b>2.20e+00</b>	<b>1.00e-15</b>	<b>2.46e+01</b>
1.45e+04	<b>3.40e+01</b>	<b>4.72e-01</b>	<b>6.08e+00</b>	<b>3.69e+02</b>	<b>1.49e+02</b>	<b>3.51e+02</b>	<b>1.08e+02</b>	<b>1.69e+00</b>	<b>1.00e-15</b>	<b>2.33e+01</b>
1.49e+04	<b>3.63e+01</b>	<b>4.82e-01</b>	<b>5.82e+00</b>	<b>3.81e+02</b>	<b>1.31e+02</b>	<b>3.66e+02</b>	<b>1.10e+02</b>	<b>1.30e+00</b>	<b>1.00e-15</b>	<b>2.29e+01</b>
1.52e+04	<b>3.86e+01</b>	<b>4.93e-01</b>	<b>5.57e+00</b>	<b>3.94e+02</b>	<b>1.14e+02</b>	<b>3.82e+02</b>	<b>1.12e+02</b>	<b>1.01e+00</b>	<b>1.00e-15</b>	<b>2.26e+01</b>
1.56e+04	<b>4.10e+01</b>	<b>5.04e-01</b>	<b>5.33e+00</b>	<b>4.07e+02</b>	<b>1.00e+02</b>	<b>3.99e+02</b>	<b>1.15e+02</b>	<b>7.88e-01</b>	<b>1.00e-15</b>	<b>2.21e+01</b>
1.60e+04	<b>4.35e+01</b>	<b>5.15e-01</b>	<b>5.12e+00</b>	<b>4.22e+02</b>	<b>8.83e+01</b>	<b>4.16e+02</b>	<b>1.17e+02</b>	<b>6.34e-01</b>	<b>1.00e-15</b>	<b>2.13e+01</b>
1.64e+04	<b>4.60e+01</b>	<b>5.25e-01</b>	<b>4.92e+00</b>	<b>4.37e+02</b>	<b>7.68e+01</b>	<b>4.35e+02</b>	<b>1.20e+02</b>	<b>5.26e-01</b>	<b>1.00e-15</b>	<b>2.05e+01</b>
1.68e+04	<b>4.86e+01</b>	<b>5.32e-01</b>	<b>4.75e+00</b>	<b>4.53e+02</b>	<b>6.72e+01</b>	<b>4.53e+02</b>	<b>1.22e+02</b>	<b>4.54e-01</b>	<b>1.00e-15</b>	<b>1.97e+01</b>
1.72e+04	<b>5.12e+01</b>	<b>5.41e-01</b>	<b>4.58e+00</b>	<b>4.69e+02</b>	<b>6.07e+01</b>	<b>4.73e+02</b>	<b>1.25e+02</b>	<b>4.08e-01</b>	<b>1.00e-15</b>	<b>1.90e+01</b>
1.77e+04	<b>5.42e+01</b>	<b>5.55e-01</b>	<b>4.41e+00</b>	<b>4.87e+02</b>	<b>5.62e+01</b>	<b>4.93e+02</b>	<b>1.28e+02</b>	<b>3.81e-01</b>	<b>1.00e-15</b>	<b>1.82e+01</b>
1.81e+04	<b>5.77e+01</b>	<b>5.69e-01</b>	<b>4.25e+00</b>	<b>5.05e+02</b>	<b>5.32e+01</b>	<b>5.15e+02</b>	<b>1.31e+02</b>	<b>3.67e-01</b>	<b>1.00e-15</b>	<b>1.75e+01</b>
1.85e+04	<b>6.11e+01</b>	<b>5.84e-01</b>	<b>4.10e+00</b>	<b>5.24e+02</b>	<b>5.28e+01</b>	<b>5.37e+02</b>	<b>1.34e+02</b>	<b>3.61e-01</b>	<b>1.00e-15</b>	<b>1.68e+01</b>
1.90e+04	<b>6.41e+01</b>	<b>5.98e-01</b>	<b>3.95e+00</b>	<b>5.44e+02</b>	<b>5.46e+01</b>	<b>5.60e+02</b>	<b>1.37e+02</b>	<b>3.61e-01</b>	<b>1.00e-15</b>	<b>1.60e+01</b>
1.95e+04	<b>6.71e+01</b>	<b>6.13e-01</b>	<b>3.82e+00</b>	<b>5.65e+02</b>	<b>5.83e+01</b>	<b>5.83e+02</b>	<b>1.41e+02</b>	<b>3.65e-01</b>	<b>1.00e-15</b>	<b>1.53e+01</b>
1.99e+04	<b>7.03e+01</b>	<b>6.27e-01</b>	<b>3.69e+00</b>	<b>5.87e+02</b>	<b>6.41e+01</b>	<b>6.08e+02</b>	<b>1.44e+02</b>	<b>3.71e-01</b>	<b>1.00e-15</b>	<b>1.47e+01</b>

## Scientific Notebook #170-10e

James Weldy

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2.04e+04	7.35e+01	6.42e-01	3.57e+00	6.10e+02	7.20e+01	6.33e+02	1.48e+02	3.80e-01	1.00e-15	1.40e+01
2.09e+04	7.69e+01	6.57e-01	3.46e+00	6.33e+02	8.09e+01	6.59e+02	1.52e+02	3.89e-01	1.00e-15	1.33e+01
2.15e+04	8.04e+01	6.72e-01	3.35e+00	6.57e+02	8.99e+01	6.86e+02	1.55e+02	3.99e-01	1.00e-15	1.27e+01
2.20e+04	8.40e+01	6.87e-01	3.25e+00	6.82e+02	9.84e+01	7.14e+02	1.59e+02	4.10e-01	1.00e-15	1.21e+01
2.25e+04	8.77e+01	7.02e-01	3.15e+00	7.08e+02	1.06e+02	7.42e+02	1.64e+02	4.22e-01	1.00e-15	1.15e+01
2.31e+04	9.16e+01	7.17e-01	3.06e+00	7.34e+02	1.12e+02	7.71e+02	1.68e+02	4.34e-01	1.00e-15	1.09e+01
2.36e+04	9.55e+01	7.31e-01	2.98e+00	7.61e+02	1.18e+02	8.01e+02	1.72e+02	4.47e-01	1.00e-15	1.03e+01
2.42e+04	9.77e+01	7.46e-01	2.90e+00	7.89e+02	1.22e+02	8.31e+02	1.76e+02	4.60e-01	1.00e-15	9.78e+00
2.48e+04	9.28e+01	7.60e-01	2.82e+00	8.15e+02	1.26e+02	8.62e+02	1.81e+02	4.74e-01	1.00e-15	9.25e+00
2.54e+04	8.47e+01	7.73e-01	2.74e+00	8.12e+02	1.28e+02	8.93e+02	1.86e+02	4.89e-01	1.00e-15	8.73e+00
2.60e+04	7.71e+01	7.87e-01	2.67e+00	7.47e+02	1.29e+02	9.24e+02	1.90e+02	5.04e-01	1.00e-15	8.23e+00
2.66e+04	7.01e+01	8.00e-01	2.60e+00	6.64e+02	1.30e+02	9.56e+02	1.95e+02	5.20e-01	1.00e-15	7.75e+00
2.73e+04	6.37e+01	8.12e-01	2.53e+00	5.89e+02	1.31e+02	9.87e+02	2.00e+02	5.37e-01	1.00e-15	7.29e+00
2.80e+04	5.79e+01	8.24e-01	2.47e+00	5.22e+02	1.32e+02	1.02e+03	2.05e+02	5.54e-01	1.00e-15	6.85e+00
2.86e+04	5.27e+01	8.35e-01	2.41e+00	4.64e+02	1.33e+02	1.05e+03	2.09e+02	5.72e-01	1.00e-15	6.42e+00
2.93e+04	4.79e+01	8.45e-01	2.36e+00	4.13e+02	1.34e+02	1.08e+03	2.14e+02	5.91e-01	1.00e-15	6.01e+00
3.00e+04	4.35e+01	8.55e-01	2.30e+00	3.69e+02	1.35e+02	1.11e+03	2.19e+02	6.10e-01	1.00e-15	5.62e+00
3.08e+04	3.96e+01	8.64e-01	2.25e+00	3.30e+02	1.35e+02	1.14e+03	2.24e+02	6.30e-01	1.00e-15	5.24e+00
3.15e+04	3.61e+01	8.72e-01	2.20e+00	2.96e+02	1.36e+02	1.17e+03	2.29e+02	6.51e-01	1.00e-15	4.88e+00
3.23e+04	3.29e+01	8.77e-01	2.15e+00	2.68e+02	1.36e+02	1.20e+03	2.33e+02	6.73e-01	1.00e-15	4.54e+00
3.30e+04	3.01e+01	7.86e-01	2.11e+00	2.43e+02	1.37e+02	1.23e+03	2.38e+02	6.95e-01	1.00e-15	4.22e+00
3.38e+04	2.76e+01	6.37e-01	2.07e+00	2.21e+02	1.38e+02	1.26e+03	2.43e+02	7.19e-01	1.00e-15	3.91e+00
3.47e+04	2.53e+01	5.18e-01	2.03e+00	2.03e+02	1.40e+02	1.28e+03	2.47e+02	7.55e-01	1.00e-15	3.62e+00
3.55e+04	2.33e+01	4.26e-01	1.99e+00	1.87e+02	1.41e+02	1.30e+03	2.51e+02	8.59e-01	1.00e-15	3.34e+00
3.63e+04	2.15e+01	3.56e-01	1.95e+00	1.73e+02	1.43e+02	1.33e+03	2.56e+02	1.28e+00	1.00e-15	3.10e+00
3.72e+04	1.99e+01	3.02e-01	1.91e+00	1.62e+02	1.45e+02	1.35e+03	2.60e+02	2.84e+00	1.00e-15	4.50e+00
3.81e+04	1.85e+01	2.61e-01	1.87e+00	1.52e+02	1.48e+02	1.37e+03	2.64e+02	7.60e+00	1.00e-15	3.53e+01
3.90e+04	1.72e+01	2.30e-01	1.84e+00	1.43e+02	1.52e+02	1.39e+03	2.68e+02	1.94e+01	1.00e-15	1.64e+02
4.00e+04	1.61e+01	2.07e-01	1.81e+00	1.36e+02	1.56e+02	1.41e+03	2.71e+02	4.44e+01	1.00e-15	2.90e+02

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4.09e+04	1.52e+01	1.89e-01	1.78e+00	1.30e+02	1.61e+02	1.42e+03	2.75e+02	8.68e+01	1.00e-15	3.29e+02
4.19e+04	1.43e+01	1.76e-01	1.75e+00	1.24e+02	1.66e+02	1.44e+03	2.78e+02	1.48e+02	1.00e-15	3.45e+02
4.29e+04	1.36e+01	1.65e-01	1.73e+00	1.20e+02	1.73e+02	1.45e+03	2.82e+02	2.25e+02	1.00e-15	3.62e+02
4.39e+04	1.29e+01	1.58e-01	1.70e+00	1.16e+02	1.80e+02	1.46e+03	2.85e+02	3.10e+02	1.00e-15	3.84e+02
4.50e+04	1.23e+01	1.52e-01	1.67e+00	1.09e+02	1.88e+02	1.47e+03	2.88e+02	3.96e+02	1.00e-15	4.10e+02
4.61e+04	1.18e+01	1.47e-01	1.65e+00	1.01e+02	1.96e+02	1.48e+03	2.91e+02	4.76e+02	1.00e-15	4.41e+02
4.72e+04	1.13e+01	1.43e-01	1.63e+00	9.64e+01	2.06e+02	1.49e+03	2.93e+02	5.52e+02	1.00e-15	4.76e+02
4.83e+04	1.09e+01	1.40e-01	1.61e+00	9.35e+01	2.16e+02	1.50e+03	2.96e+02	6.25e+02	1.00e-15	5.17e+02
4.95e+04	1.06e+01	1.38e-01	1.59e+00	8.33e+01	2.26e+02	1.51e+03	2.98e+02	6.97e+02	1.00e-15	5.62e+02
5.06e+04	1.03e+01	1.36e-01	1.57e+00	6.54e+01	2.36e+02	1.51e+03	3.00e+02	7.71e+02	1.00e-15	6.13e+02
5.18e+04	1.00e+01	1.34e-01	1.55e+00	4.89e+01	2.47e+02	1.52e+03	3.03e+02	1.94e+04	1.42e-01	6.67e+02
5.31e+04	9.75e+00	1.32e-01	1.53e+00	3.64e+01	2.57e+02	1.53e+03	3.05e+02	4.42e+04	4.32e+02	7.26e+02
5.43e+04	9.53e+00	1.31e-01	1.51e+00	2.69e+01	2.67e+02	1.53e+03	3.07e+02	3.94e+04	7.62e+02	7.88e+02
5.56e+04	9.33e+00	1.29e-01	1.49e+00	1.97e+01	2.76e+02	1.54e+03	3.08e+02	3.74e+04	1.13e+03	8.52e+02
5.70e+04	9.15e+00	1.28e-01	1.47e+00	1.44e+01	2.84e+02	4.04e+04	3.10e+02	3.65e+04	3.96e+03	9.18e+02
5.83e+04	8.99e+00	1.27e-01	1.45e+00	1.05e+01	2.91e+02	6.94e+04	3.11e+02	3.66e+04	6.59e+03	9.84e+02
5.97e+04	8.84e+00	1.25e-01	1.43e+00	7.64e+00	2.98e+02	1.02e+05	3.13e+02	3.76e+04	8.56e+03	1.05e+03
6.11e+04	8.70e+00	1.24e-01	1.42e+00	5.55e+00	3.04e+02	1.38e+05	3.14e+02	3.87e+04	1.00e+04	1.11e+03
6.26e+04	8.57e+00	1.23e-01	1.40e+00	4.04e+00	3.08e+02	1.69e+05	3.14e+02	3.91e+04	1.10e+04	1.17e+03
6.41e+04	8.45e+00	1.22e-01	1.39e+00	2.96e+00	3.13e+02	1.96e+05	3.14e+02	3.90e+04	1.17e+04	1.22e+03
6.56e+04	8.34e+00	1.21e-01	1.37e+00	6.38e+03	3.16e+02	2.18e+05	3.14e+02	3.85e+04	1.22e+04	1.27e+03
6.72e+04	8.23e+00	1.20e-01	1.36e+00	9.38e+03	3.19e+02	2.36e+05	3.13e+02	3.01e+04	1.24e+04	1.30e+03
6.87e+04	8.15e+00	1.19e-01	1.34e+00	1.14e+04	3.21e+02	2.49e+05	3.11e+02	1.75e+04	1.25e+04	1.34e+03
7.04e+04	8.08e+00	5.90e+01	1.33e+00	3.12e+04	3.23e+02	2.58e+05	3.08e+02	1.06e+04	1.25e+04	1.36e+03
7.21e+04	8.02e+00	1.62e+02	1.31e+00	5.05e+04	3.24e+02	2.63e+05	3.03e+02	8.08e+03	1.24e+04	1.38e+03
7.38e+04	7.98e+00	2.16e+02	1.30e+00	6.33e+04	3.25e+02	2.63e+05	2.97e+02	6.80e+03	1.21e+04	1.39e+03
7.55e+04	7.95e+00	2.39e+02	1.29e+00	7.16e+04	3.26e+02	2.59e+05	2.90e+02	5.49e+03	1.18e+04	1.40e+03
7.73e+04	7.93e+00	2.46e+02	1.64e+00	7.67e+04	3.26e+02	2.52e+05	2.81e+02	4.15e+03	1.15e+04	1.41e+03
7.91e+04	8.36e-07	1.35e-05	1.65e-04	1.73e-02	2.09e-05	1.96e-02	2.24e-05	1.77e-04	1.21e-03	9.84e-05

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James Weldy

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8.10e+04	8.37e-07	1.31e-05	2.57e-04	1.76e-02	2.07e-05	1.74e-02	8.72e-05	1.44e-04	1.15e-03	9.85e-05
8.29e+04	8.39e-07	1.25e-05	2.70e-04	1.77e-02	1.99e-05	1.53e-02	3.17e-04	1.30e-04	1.10e-03	9.86e-05
8.49e+04	8.43e-07	1.16e-05	2.70e-04	1.77e-02	1.85e-05	1.35e-02	5.40e-04	1.25e-04	1.04e-03	9.86e-05
8.69e+04	8.48e-07	1.05e-05	2.63e-04	1.76e-02	1.69e-05	1.20e-02	7.52e-04	1.27e-04	9.80e-04	9.93e-05
8.90e+04	8.54e-07	9.54e-06	2.54e-04	1.73e-02	1.55e-05	1.06e-02	9.44e-04	2.35e-04	9.23e-04	9.94e-05
9.11e+04	8.61e-07	8.67e-06	2.46e-04	1.69e-02	1.45e-05	9.33e-03	1.12e-03	1.12e-03	8.73e-04	9.94e-05
9.32e+04	8.68e-07	8.01e-06	2.48e-04	1.59e-02	1.36e-05	8.19e-03	1.27e-03	3.81e-03	8.32e-04	9.93e-05
9.54e+04	8.76e-07	7.60e-06	2.54e-04	1.46e-02	1.29e-05	7.21e-03	1.41e-03	7.31e-03	8.05e-04	9.91e-05
9.77e+04	8.84e-07	7.47e-06	2.69e-04	1.34e-02	1.24e-05	6.42e-03	1.55e-03	9.76e-03	7.99e-04	9.85e-05
1.00e+05	8.92e-07	7.54e-06	2.90e-04	1.26e-02	1.18e-05	5.84e-03	1.68e-03	1.09e-02	8.18e-04	9.73e-05
1.10e+05	1.00e-15									

The time of switch to pluvial conditions no longer jumps around. Therefore, the fix has been implemented successfully.

Scientific Notebook #170-10e  
James Weldy  
20-1402-761

Issued to: S. Mohanty

Issue Date: Apr. 3, 1996

Account Number: 20-01402-761

Title: Dose from Criticality

Participants: J. Weldy

1-10-01

An analysis was performed to assess the consequences of a criticality event on the repository system. Ignoring the probability of occurrence for now, the goal of this analysis is to determine what the consequences are if a criticality event does occur. Two separate analyses will be conducted to determine this effect. First, the consequences of a steady-state criticality will be determined. The consequences associated with a steady-state criticality include an increase in radionuclide inventory in the waste packages that go critical and an increase in the temperature inside and around the critical waste packages. Second, the consequences of a transient criticality will be calculated. To avoid having to perform detailed calculations involving exactly how much power is generated and how much damage will be done by the event, an extreme case will be evaluated. The consequences that will be assessed will be the mechanical damage to the fuel, surrounding waste packages, drip shield, and invert around the critical waste package.

## 1. Steady-State Criticality

The steady-state criticality event will be modeled as a 10,000 year steady-state criticality that starts at year 5000. It is assumed that all waste packages that are initially defective go critical (an average of about 32) and that all waste packages that go critical are under drips (otherwise they could not go critical). The changes to the reference input file and data files include the following:

### Changes to tpa.inp to model only the waste packages that go critical

- Turn seismicity off to avoid failing any additional waste packages

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- Reduce the value of AA\_1\_1 by 3 orders of magnitude to prevent any corrosion failures
- Reduce the value of CoefforLocCorrOfOuterOverpack to 2.5e-8 to prevent any corrosion failures
- Set the SubareaWetFraction to 1
- Set the time of failure of the initially defective waste packages to 5000 years
- Increase the gap fraction by the percent increase in radionuclide inventory to assume that all radionuclides created by the criticality event are created in the gap (conservative) to match DOE analyses. See Table 1 for the new gap inventories for each radionuclide.

Changes to the file burnup.dat to model a steady-state criticality

- Modify the values of heat generation to produce a heat increase of about 25 degrees C between the years 5000 and 15000. The 25 degree C increase in temperature is taken from calculations performed by the DOE in the Disposal Criticality Topical Report (U.S. Department of Energy, 1998). Specifically, change the heat generation rate at year 5000 to 56.54 W/MTIHM for BWR fuel and 64.1 W/MTHM for PWR fuel. Change the heat generation rate at year 10000 to 35.52 W/MTIHM for BWR fuel and 46.27 W/MTIHM for PWR fuel. Add a line in the file for year 15000 and set the heat generation rate to 25.00 W/MTIHM for BWR fuel and 28.00 W/MTIHM for PWR fuel.

Changes to the file wpflow.dat to model a steady-state criticality

- Reduce the value of Fmult to 0 between t=7000 years and t=15000 years. While the criticality event is occurring, all of the water that enters the waste package will be evaporated, so there will be no release from the waste package. The value is set to 0 at 7000 years instead of 5000 years to allow the waste package to fill up so releases will occur immediately after the event ends. This will result in some small releases at early times when SFWettedFraction\_2 is sampled as a low value, but the releases will be minor and will not significantly affect the results.

Changes to the file nuclides.dat to model a steady-state criticality

- The goal is to get an increase in inventory at 15000 years that matches the 10,000 year criticality inventory increase in Table C-16 of the Topical Report for all TPA nuclides. For all radionuclides that are not daughter

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products in a chain decay series, this just means that the inventory at 10 years is increased by that same percentage. Chain nuclides need to consider effects of parent decay on inventory. If the inventory from the parent decay dominates the amount of radionuclide present at 15,000 years, only the inventory of the parent needs to be increased by the appropriate percentage. If the inventory of the daughter dominates, only the inventory of the daughter needs to be increased. If the contribution of the parent and daughter are comparable, changes to inventory will have to be divided between the two. Since <sup>129</sup>I and <sup>99</sup>Tc both increase in inventory by 4.1% after a 10,000 year criticality, it is assumed that all fission products/activation products increases by this same percentage. To be conservative, assume that actinide that are not listed in the Table increase by 4.1% as well.

Radionuclide	15000 year inventory dominated by:	Base Inventory (Ci/M TU)	% Increase	Post-Criticality Inventory (Ci/M TU)
Cm-246	self	7.62e-2	4.1	7.93e-2
U-238	self	0.316	No change - decreases with burnup (conservative)	0.316
Cm-245	self	0.366	2.1	0.374
Am-241	parent (Cm-245)	No change	No change	No change
Np-237	parent (Am-241)	No change	No change	No change
Am-243	self	26.4	4.1	27.5

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Pu-239	self	369	4.1	384
Pu-240	self	544	4.1	566
U-234	50% self, 50% Pu- 238	1.18	No change - increa se Pu- 238 invent ory by 25%	1.18
Th-230	parent (U- 234)	No change	No change	No change
Ra-226	parent (Th- 230)	No change	No change	No change
Pb-210	parent (Ra- 226)	No change	No change	No change
Cs-135	self	0.536	4.1	0.558
I-129	self	3.57e-2	4.1	3.72e-2
Tc-99	self	14.5	4.1	15.1
Ni-59	self	2.44	4.1	2.54
C-14	self	1.44	4.1	1.50
Se-79	self	0.458	4.1	0.477
Nb-94	self	0.848	4.1	0.883
Cl-36	self	1.15e-2	4.1	1.2e-2

## 2. Transient Criticality

The transient criticality will be modeled as an extreme event in which the fuel maintains its geometry and sufficient water remains in the waste package to generate a very large pressure pulse. This pressure pulse is assumed to be sufficient to very quickly degrade the spent fuel inside of the waste package, cause serious damage to the waste package such that the water contact model is a flow-through model, fail one waste package on either side of the

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critical waste package, and blast a hole in the invert material below the waste packages such that the performance of the invert is bypassed. The drip shield above the waste package would also be failed by the blast, but would have to already be failed for the waste package to accumulate water and go critical. The total number of fissions will be limited enough that changes in radionuclide inventory or long-term heat generation can be ignored.

The calculation requires two runs of the TPA code to perform the modeling - one for the waste package in which the transient criticality occurs and one for the two additional waste packages that are failed by the transient criticality. The results of the analysis can be added together along with the base case dose to compare the results to the base case.

Changes to tpa.inp to model the waste package in which the criticality event occurs:

- Reduce AA\_1\_1 and CoefForLocCorrOfOuterOverpack by 3 orders of magnitude to ensure that there are no corrosion failures
- Turn off seismicity to ensure that there are no seismic failures
- Set the SubareaWetFraction to 1 because the waste package has to be located under a drip to go critical
- Set the failure time of the initially defective waste packages to 5000 years. This time is simply an assumption, but is set considering that it will take a long period of time to fail the drip shield and fill up the waste package with water
- Set the defective fraction of waste packages to 4.3e-4 to ensure that only 1 waste package is failed initially (located in Subarea 2)
- Set the Invert Bypass Option to 1, which causes the code to bypass the invert and not take any credit for the performance of the invert
- Set the waste package failure type for initially defective waste packages to a flow-through model, since it is assumed that substantial damage is done to the waste package
- Change the fuel dissolution model (IModel) to model 3 (User-specified Leach Rate)
- Increase the User Specified Leach Rate by 4 orders of magnitude to ensure that all the fuel fully degrades within one TPA Code time step

Changes to tpa.inp to model the two waste packages next to the waste package in which the criticality occurs:

- Reduce AA\_1\_1 and CoefForLocCorrOfOuterOverpack by 3 orders of

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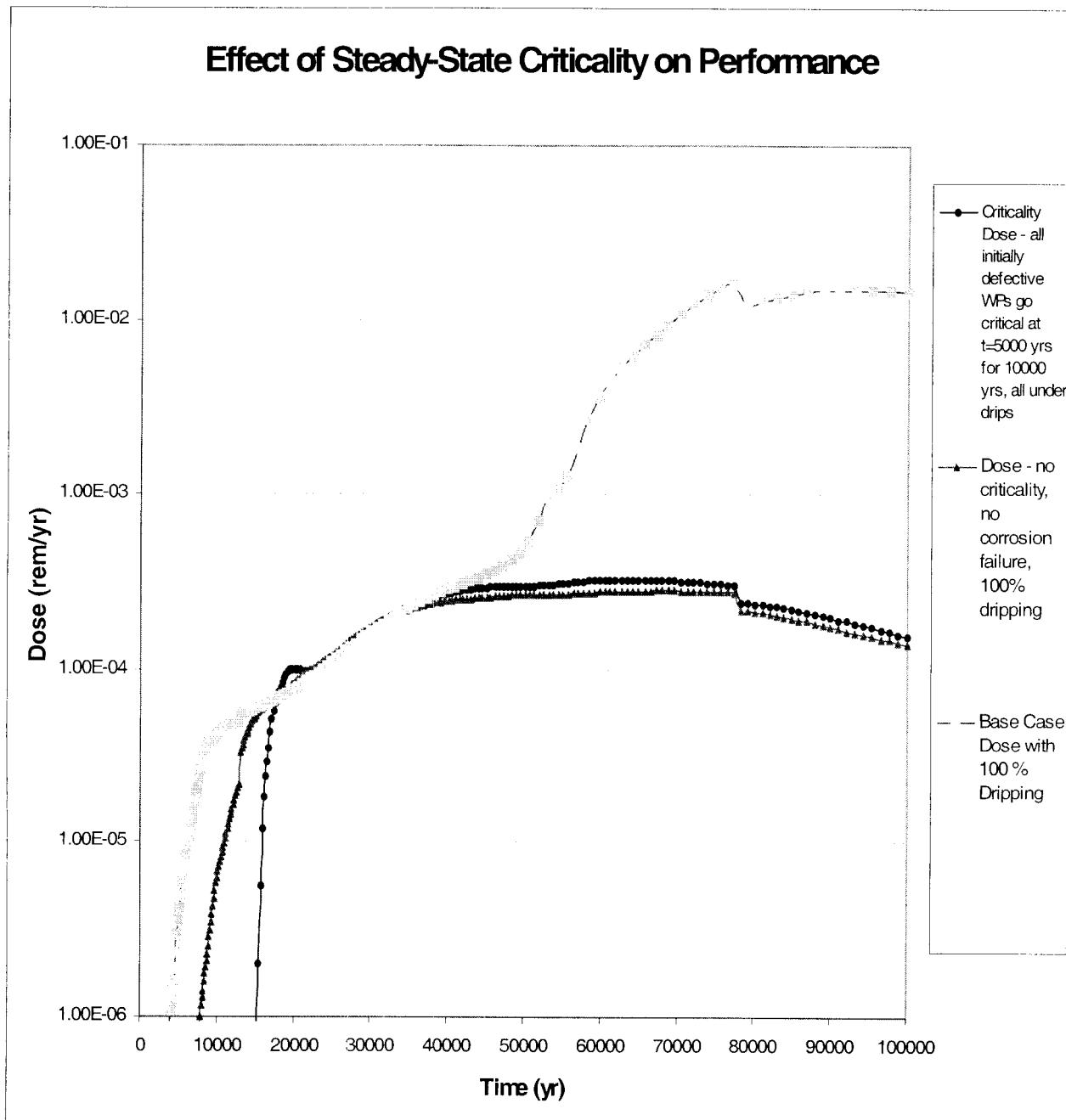
magnitude to ensure that there are no corrosion failures

- Turn off seismicity to ensure that there are no seismic failures
- Set the failure time of the initially defective waste packages to 5000 years.
- Set the defective fraction of waste packages to 4.5e-4 to ensure that only 2 waste packages are failed initially (one located in Subarea 2 and one located in Subarea 1)
- Set the Invert Bypass Option to 1, which causes the code to bypass the invert and not take any credit for the performance of the invert

## Results

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James Weldy  
20-1402-761

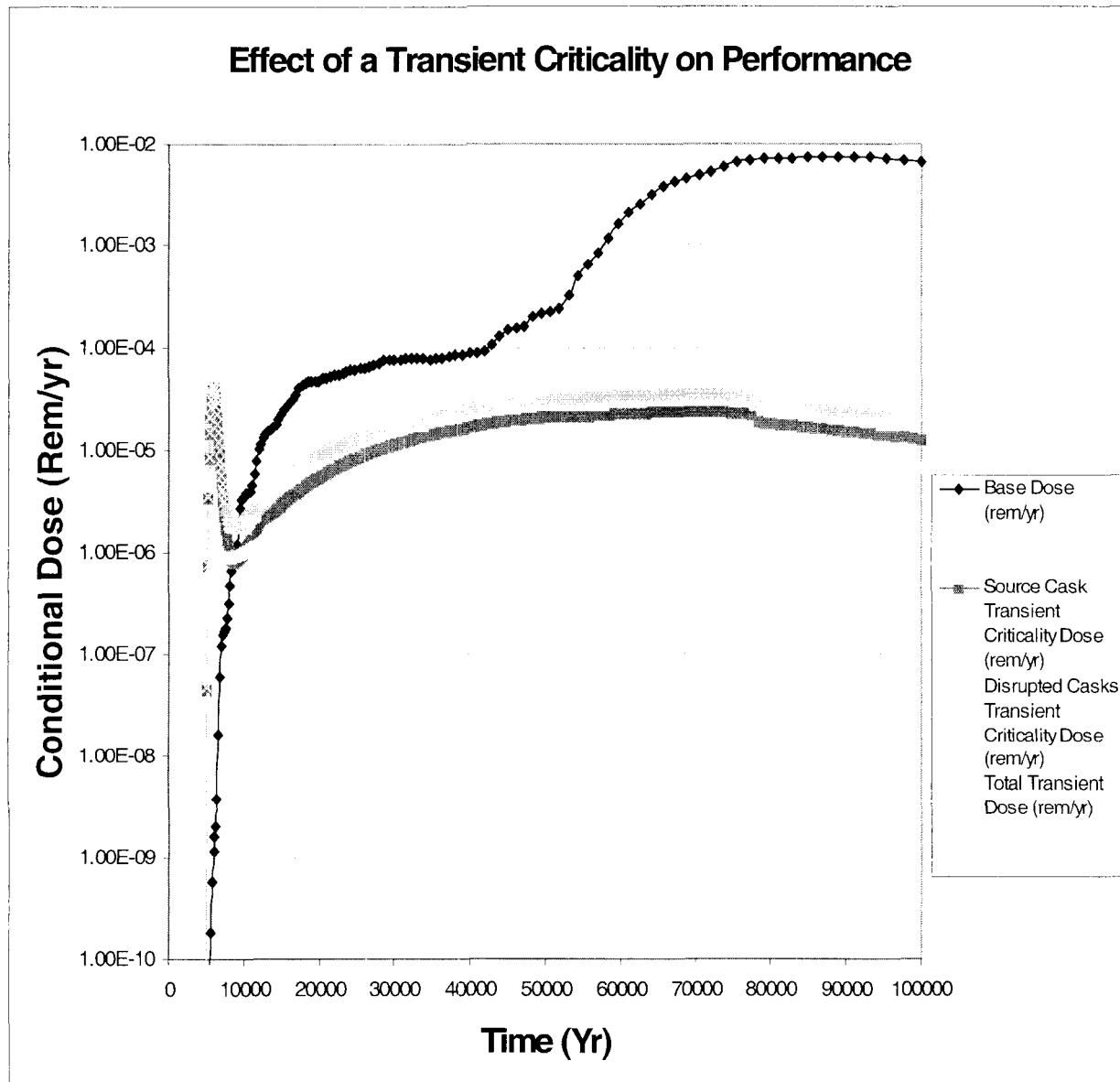
- Steady state criticality



Scientific Notebook #170-10e  
James Weldy  
20-1402-761

- Transient Criticality

It appears that even without the probability of occurrence factored into the results,



the effects of a steady-state criticality are relatively minor on the overall performance of the repository. Transient criticality effects are larger

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James Weldy

20-1402-761

immediately after the event, primarily due to the assumption that the fuel is destroyed by the event, and causes the dose to increase by a couple orders of magnitude. However, incorporating the probability of occurrence of a transient criticality into the results would likely cause the consequences of transient criticality to have little effect on the expected annual dose, especially considering that the base dose here does not include the volcanism scenario, which dominates the risk from the repository over the first 10,000 years.

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James Weldy  
20-1402-761

INITIALS JRW

state criticality are relatively minor on the overall performance of the repository. Transient criticality effects are larger immediately after the event, primarily due to the assumption that the fuel is destroyed by the event, and causes the dose to increase by a couple orders of magnitude. However, incorporating the probability of occurrence of a transient criticality into the results would likely cause the consequences of transient criticality to have little effect on the expected annual dose, especially considering that the base dose here does not include the volcanism scenario, which dominates the risk from the repository over the first 10,000 years.

255 JRW 12-2-05

Entries into Scientific Notebook #170 for pages 242 - 251 have been made by James Weldy.

No original text entered into this Scientific Notebook has been removed.

James L. Weldy \_\_\_\_\_  
date 7-9-01

254 255-A JRW  
12-2-05

Scientific Notebook #170-10e

James Weldy

20-1402-761

Issued to: S. Mohanty

Issue Date: Apr. 3, 1996

Account Number: 20-01402-761

Title: Dose from Criticality

Participants: J. Weldy

4-10-01

An analysis was performed to assess the consequences of a criticality event on the repository system. Ignoring the probability of occurrence for now, the goal of this analysis is to determine what the consequences are if a criticality event does occur. Two separate analyses will be conducted to determine this effect. First, the consequences of a steady-state criticality will be determined. The consequences associated with a steady-state criticality include an increase in radionuclide inventory in the waste packages that go critical and an increase in the temperature inside and around the critical waste packages. Second, the consequences of a transient criticality will be calculated. To avoid having to perform detailed calculations involving exactly how much power is generated and how much damage will be done by the event, an extreme case will be evaluated. The consequences that will be assessed will be the mechanical damage to the fuel, surrounding waste packages, drip shield, and invert around the critical waste package. This is a revised calculation from the previously documented one, which has been modified to explicitly calculate the sustainable power level and inventory increase instead of relying on DOE numbers.

## 1. Steady-State Criticality

From the TPA 4.1 User's Guide (Mohanty, et al., 2000) and Sonntag and van Wylen (1991), the power level in the waste package can be calculated by:

$${}_1Q_2 = {}_1W_2 + \dot{m}(h_2 - h_1) + P_{atm}(v_2 - v_1) \quad (1)$$

Neglect the volume change as it will be negligible compared to the other factors.

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From the TPA 4.1 User's Guide (Mohanty, et al., 2000), the heat loss can be calculated by:

$$_1W_2 = (G_{cond} + G_{conv} + G_{rad})(T_{wp} - T_{rock}) \quad (2)$$

The effective heat transfer coefficients can be calculated from the following formulae also in the TPA User's Guide:

$$G_{conv} = f_c \frac{2\pi k_{eff-nc} (L_{wp} + 2\delta)}{\ln(\frac{D_{rw}}{D_{wp}})} \quad (3)$$

where,

$f_c$  = fractional area not covered by the floor = 0.75 (Mohanty, et al., 2000)

$k_{eff-nc}$  = effective thermal conductivity for natural convection = 0.9 W/m-C (Mohanty, et al., 2000)

$D_{rw}$  = Diameter of drift = 5.5 m (TSPA-SR)

$D_{wp}$  = Diameter of waste package = 1.579 m (TSPA-SR)

$L_{wp}$  = Length of waste package = 5.275 m (TSPA-SR)

$\delta$  = Spacing between waste package = 0.1 m (TSPA-SR)

$$G_{cond} = (1 - f_c) \frac{2\pi k_{floor} (L_{wp} + 2\delta)}{\ln(\frac{D_{rw}}{D_{wp}})}$$

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(4)

where,

$f_c = \text{fractional area not covered by the floor} = 0.75$  (Mohanty, et al., 2000)

$k_{\text{floor}} = \text{thermal conductivity of floor} = 0.6 \text{ W/m-C}$  (Incropera and DeWitt, 1995)

$$G_{\text{rad}} = f_c \frac{4\sigma(273.15 + T_{\text{rock}})^3}{\frac{1 - \varepsilon_{wp}}{\varepsilon_{wp}\pi D_{wp}L_{wp}} + \frac{1}{F_{wp-rw}\pi D_{wp}(L_{wp} + 2\delta)} + \frac{1 - \varepsilon_{rw}}{\varepsilon_{rw}\pi D_{rw}(L_{wp} + 2\delta)}} \quad (5)$$

where,

$\sigma = \text{Stefan-Boltzmann constant} = 5.67 \times 10^{-8} \text{ W/m}^2\text{K}^4$  (Mohanty, et al., 2000)

$\varepsilon_{wp} = \text{emissivity of the waste package} = 0.87$  (Mohanty, et al., 2000)

$F_{wp-rw} = \text{radiative view factor from the WP to the rock wall} = 1$  (Mohanty, et al., 2000)

$T_{\text{rock}} = \text{Temperature of the rock (C)}$

Use a rock wall temperature at t=5000 years of 70 C from TPA results and an increase in the temperature of the waste package due to the criticality of 30 C from DOE calcs (DOE, 1998 - Disposal Criticality Topical Report). A reasonably conservative value for the flow rate of water into the waste package is 0.1 m<sup>3</sup>/yr (TSPA-SR, TPA code results). Obtain enthalpy values for 70 C water and 100 C steam from Sonntag and van Wylen (1991), Table A.1.2SI. This results in the calculation of a power level of 4.78 kW.

Use this power level in ORIGEN2 calculations for 10,000 years to calculate the inventory generation for this event (note that the ORIGEN2 calculations do not currently account for differences

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in moderator density or temperatures between a reactor and a waste package at this time, which could have a moderate effect on the results). The input and output files for the ORIGEN2 calculations are p3.040repb and p3.040repbo.

The steady-state criticality event will be modeled as a 10,000 year steady-state criticality that starts at year 5000. It is assumed that all waste packages that are initially defective go critical (an average of about 32) and that all waste packages that go critical are under drips (otherwise they could not go critical). The changes to the reference input file and data files include the following:

Changes to tpa.inp to model only the waste packages that go critical

- Turn seismicity off to avoid failing any additional waste packages
- Reduce the value of AA\_1\_1 by 3 orders of magnitude to prevent any corrosion failures
- Reduce the value of CoefforLocCorrOfOuterOverpack to 2.5e-8 to prevent any corrosion failures
- Set the SubareaWetFraction to 1
- Set the time of failure of the initially defective waste packages to 5000 years
- Increase the gap fraction by the percent increase in radionuclide inventory to assume that all radionuclides created by the criticality event are created in the gap (conservative) to match DOE analyses.

Changes to the file burnup.dat to model a steady-state criticality

- Modify the values of heat generation to produce a heat increase of about 25 degrees C between the years 5000 and 15000. The 25 degree C increase in temperature is taken from calculations performed by the DOE in the Disposal Criticality Topical Report (U.S. Department of Energy, 1998). Specifically, change the heat generation rate at year 5000 to 56.54 W/MTIHM for BWR fuel and 64.1 W/MTHM for PWR fuel. Change the heat generation rate at year 10000 to 35.52 W/MTIHM for BWR fuel and 46.27 W/MTIHM for PWR fuel. Add a line in the file for year 15000 and set the heat generation rate to 25.00 W/MTIHM for BWR fuel and 28.00 W/MTIHM for PWR fuel.

Changes to the file wpflow.dat to model a steady-state criticality

- Reduce the value of Fmult to 0 between t=7000 years and t=15000 years. While the criticality event is occurring, all of the water that enters the waste package will be evaporated, so there will be no release from the waste package. The value is set to 0 at 7000 years instead of 5000 years to allow the waste package to fill up so releases will occur immediately after the event ends. This will result in some small releases at early times when

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SFWettedFraction\_2 is sampled as a low value, but the releases will be minor and will not significantly affect the results.

Changes to the file nuclides.dat to model a steady-state criticality

- The goal is to get an increase in inventory at 15000 years that matches the 10,000 year criticality inventory increase calculated using ORIGEN2.1 for all TPA nuclides. For all radionuclides that are not daughter products in a chain decay series, this just means that the inventory at 10 years is increased by that same percentage. Chain nuclides need to consider effects of parent decay on inventory. If the inventory from the parent decay dominates the amount of radionuclide present at 15,000 years, only the inventory of the parent needs to be increased by the appropriate percentage. If the inventory of the daughter dominates, only the inventory of the daughter needs to be increased. If the contribution of the parent and daughter are comparable, changes to inventory will have to be divided between the two.

Radionuclide	15000 year inventory dominate d by:	Base Inventory (Ci/MTU )	% Increase	Post-Criticality Inventor y (Ci/MTU )
Cm-246	self	7.62e-2	374	0.361
U-238	self	0.315	-1.1	0.3115
Cm-245	self	0.366	Leave same - not important to performance.	No change
Am-241	parent (Cm-245)	2080	<b>Leave same - not important to performance.</b>	<b>No change</b>

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James Weldy

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Np-237	parent (Am-241)	<b>0.434</b>	<b>71 - 1.65</b> Ci/MTU from parents, need to increase initial inventor y to raise to 2.823 Ci/MTU at 15000 years	<b>1.173</b>
Am-243	self	26.4	313.7	109.2
Pu-239	self	369	28.8	475.4
Pu-240	self	544	160.2	1415
U-234	50% self, 50% Pu-238	<b>1.18</b>	<b>251 - 2.636</b> Ci/MTU from parents, need to increase initial inventor y to raise to 9.267 Ci/MTU at 15000 years	<b>6.63</b>

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Th-230	parent (U-234)	No change	No change	No change - inventor y will be wrong due to U-234 change. Model separate ly if necessar y.
Ra-226	parent (Th-230)	No change	No change	No change - inventor y will be wrong due to U-234 change. Model separate ly if necessar y.
Pb-210	parent (Ra-226)	No change	No change	No change - inventor y will be wrong due to U-234 change. Model separate ly if necessar y.
Cs-135	self	0.536	87.4	1.00

I-129	self	3.57e-2	22.1	4.36e-2
Tc-99	self	14.5	11.5	16.2
Ni-59	self	2.44	45	3.54
C-14	self	1.44	310.3	5.91
Se-79	self	0.458	11.2	0.509 (corrected to 0.03 due to half-life change)
Nb-94	self	0.848	65.1	1.4
Cl-36	self	1.15e-2	31.5	1.47e-2

## 2. Transient Criticality

The transient criticality will be modeled as an extreme event in which the fuel maintains its geometry and sufficient water remains in the waste package to generate a very large pressure pulse. This pressure pulse is assumed to be sufficient to very quickly degrade the spent fuel inside of the waste package, cause serious damage to the waste package such that the water contact model is a flow-through model, fail one waste package on either side of the critical waste package, and blast a hole in the invert material below the waste packages such that the performance of the invert is bypassed. The drip shield above the waste package would also be failed by the blast, but would have to already be failed for the waste package to accumulate water and go critical. The total number of fissions will be limited enough that changes in radionuclide inventory or long-term heat generation can be ignored.

The calculation requires two runs of the TPA code to perform the modeling - one for the waste package in which the transient criticality occurs and one for the two additional waste packages that are failed by the transient criticality. The results of the analysis can be added together along with the base case dose to compare the results to the base case.

Changes to tpa.inp to model the waste package in which the criticality event occurs:

- Reduce AA\_1\_1 and CoefForLocCorrOfOuterOverpack by 3 orders of magnitude to ensure that there are no corrosion failures
- Turn off seismicity to ensure that there are no seismic failures

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- Set the SubareaWetFraction to 1 because the waste package has to be located under a drip to go critical
- Set the failure time of the initially defective waste packages to 5000 years. This time is simply an assumption, but is set considering that it will take a long period of time to fail the drip shield and fill up the waste package with water
- Set the defective fraction of waste packages to 4.3e-4 to ensure that only 1 waste package is failed initially (located in Subarea 2)
- Set the Invert Bypass Option to 1, which causes the code to bypass the invert and not take any credit for the performance of the invert
- Set the waste package failure type for initially defective waste packages to a flow-through model, since it is assumed that substantial damage is done to the waste package
- Change the fuel dissolution model (IModel) to model 3 (User-specified Leach Rate)
- Increase the User Specified Leach Rate by 4 orders of magnitude to ensure that all the fuel fully degrades within one TPA Code time step

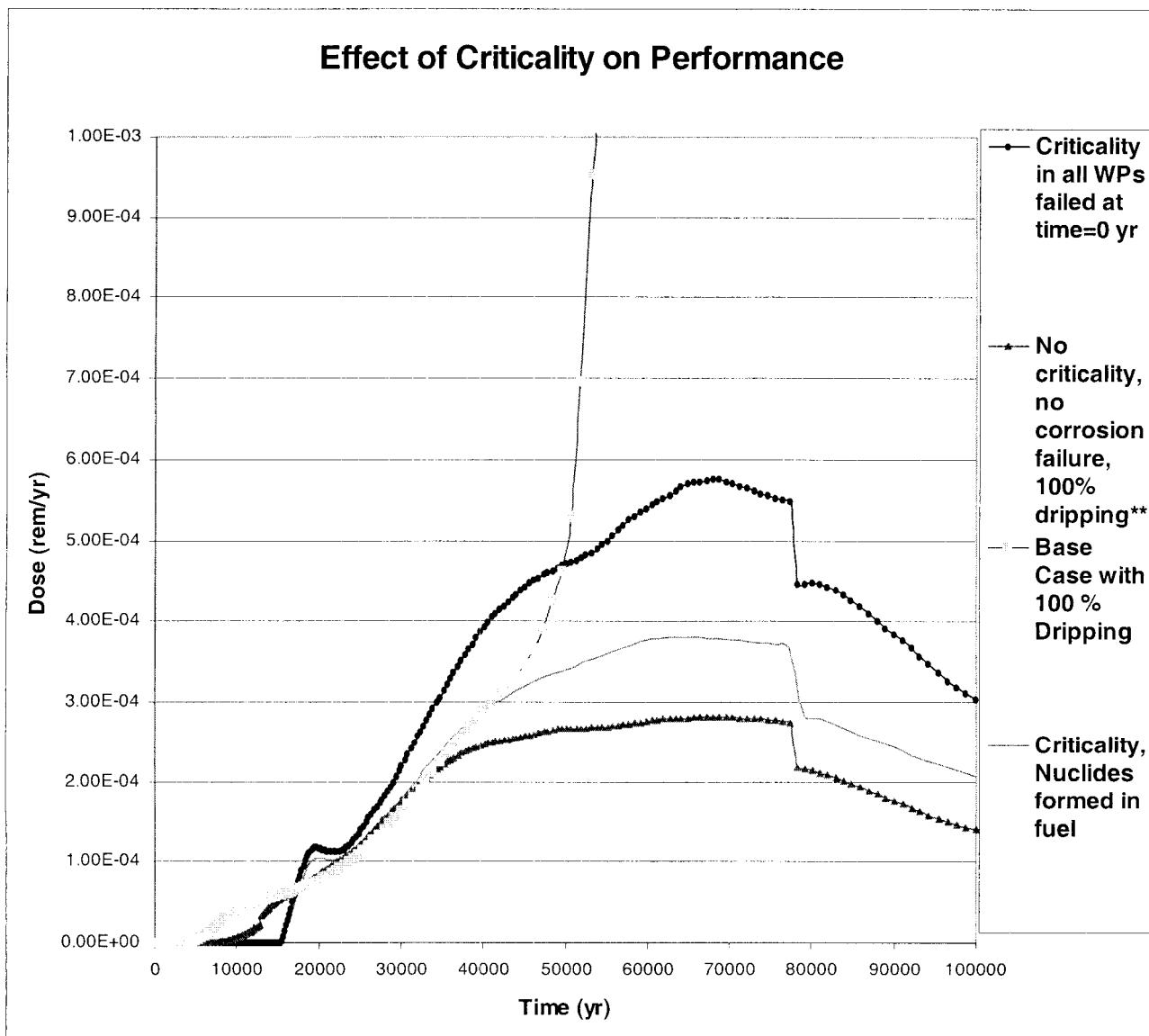
Changes to tpa.inp to model the two waste packages next to the waste package in which the criticality occurs:

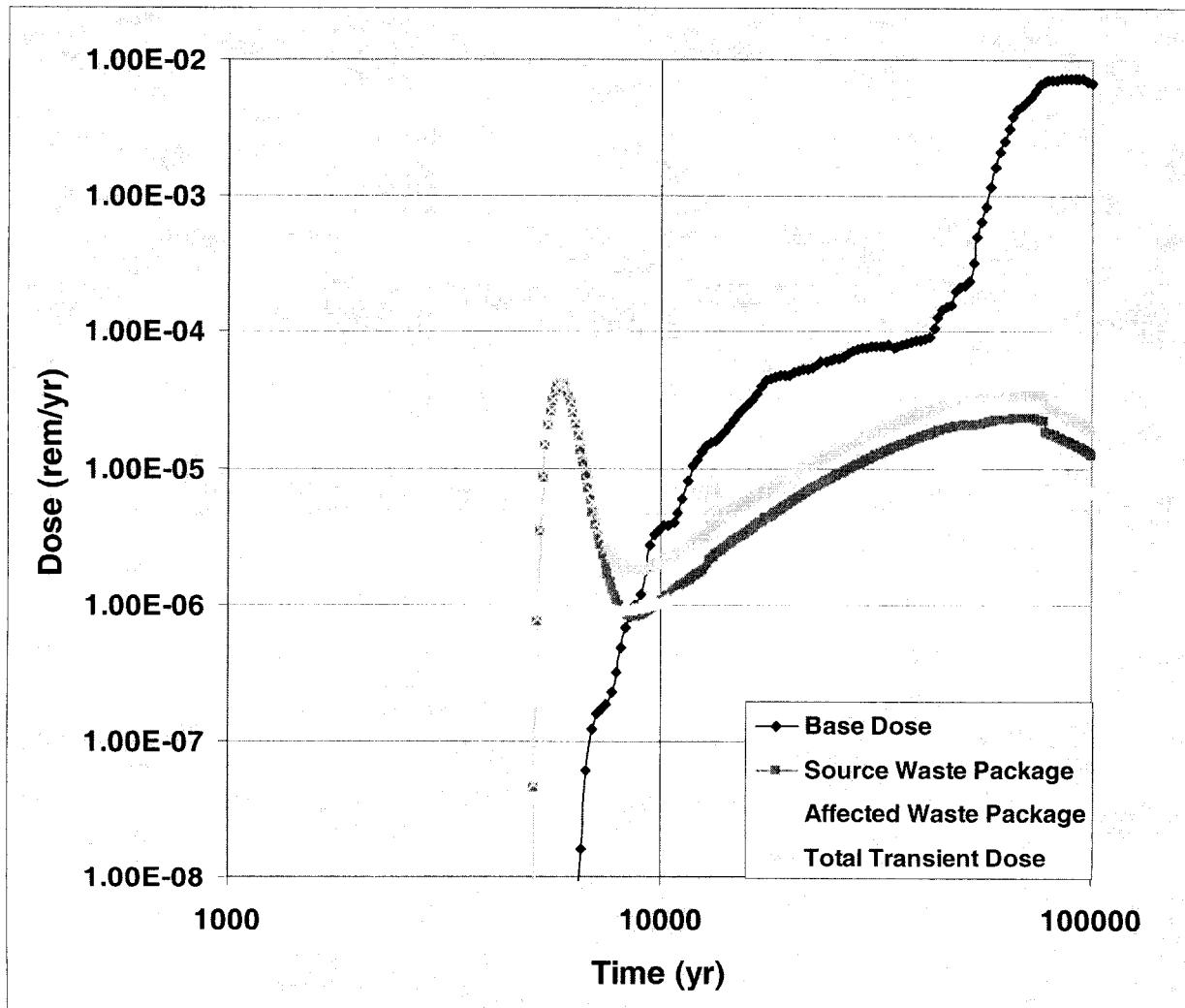
- Reduce AA\_1\_1 and CoefForLocCorrOfOuterOverpack by 3 orders of magnitude to ensure that there are no corrosion failures
- Turn off seismicity to ensure that there are no seismic failures
- Set the failure time of the initially defective waste packages to 5000 years.
- Set the defective fraction of waste packages to 4.5e-4 to ensure that only 2 waste packages are failed initially (one located in Subarea 2 and one located in Subarea 1)
- Set the Invert Bypass Option to 1, which causes the code to bypass the invert and not take any credit for the performance of the invert

## Results

Scientific Notebook #170-10e  
James Weldy  
20-1402-761

- Steady state criticality





- Transient criticality  
It appears that even without the probability of occurrence factored into the results, the effects of a steady-state criticality are relatively minor on the overall performance of the repository. Transient criticality effects are larger immediately after the event, primarily due to the assumption that the fuel is destroyed by the event, and causes the dose to increase by a couple orders of magnitude. However, incorporating the probability of occurrence of a transient

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20-1402-761

criticality into the results would likely cause the consequences of transient criticality to have little effect on the expected annual dose, especially considering that the base dose here does not include the volcanism scenario, which dominates the risk from the repository over the first 10,000 years.

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James Weldy  
20-1402-762

Scientific Notebook #170-10e

Issued to: S. Mohanty

Issue Date: Apr. 3, 1996

Account Number: 20-01402-762

Title: Dose from Swamp Coolers

Participants: J. Weldy, O. Povetko

7/18/01 Calculation of Dose from Swamp Coolers

Reason: The External Review of the TPA code identified a concern that dose from the use of evaporative coolers by members of the receptor group in Amargosa Valley could lead to significant dose.

Software used: MCNP version 4A Radiation Shielding and Transport Code

Procedure: There are two potential exposure pathways that the use of evaporative coolers could contribute to. First, the radionuclides may collect on the pad through which the water flows and evaporates during the lifetime of the pad and contribute to a direct exposure pathway. Second, as the radionuclides build up on the pad, some fraction of the material on the pad may 'flake-off' and be released to the air to contribute to an inhalation dose.

To calculate the dose from inhalation, the following data were used:

From the web site, <http://www.bigofan.com/products.html> the characteristics of a medium sized fan were determined - including an air flow rate of 5000 cubic feet per minute and a water tank size of 14 gallons. Assuming an average water use of 5 volumes of water tanks per day (which is confirmed by the results of a survey documented at: <http://www.ci.phoenix.az.us/WATER/evapcool.html> , allowed the daily volume of water used to be calculated. Based on the definition of a member of the critical group, it was assumed that the receptor is indoors for 55% of the day (Laplante and Poor, 1997). It was also assumed that the evaporative cooler was in use

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for 7 months of the year (Cannon Center for Research, 1997). Inhalation Dose Conversion Factors for different radionuclides were taken from Federal Guidance Report 11 (Eckerman, 1988). Finally, it was assumed that 1% of the material that collected on the pad would flake-off and be available to contribute to the inhalation pathway. Based on this input data, the dose to a member of the critical group from the airborne pathways would be:

$$Dose = \frac{Concentration(pCi/L) \times Water\ Use(L/yr)}{Air\ Flow(m^3/yr)} \times Breathing\ Rate(m^3/yr) \times f_{indoors} \times f_{use} \times DCF(rem/pCi)$$

To calculate the dose from direct exposure, the following methodology was used. The water use was the same as above and it was assumed that the pads were replaced every 10 years. <http://www.bigofan.com/products.html> indicates that the high-quality pads will last much longer than regular pads, which generally are recommended to be replaced every year. Therefore, assume that these pads last 10 years. For simplicity, dose was only calculated in the 10<sup>th</sup> year, after radionuclides had built up to their maximum concentration. Further, it was assumed that while the receptor was located inside the house, they were always 2 m away from a roof-mounted evaporative cooler and that they were not exposed at all while inside. The shielding calculations were performed using MCNP-4A (Los Alamos National Laboratory, 1995), and included the roof and the steel walls of the cooler. The files used in the calculations are contained in the directory /project/mcnp/povetko/Evaporative\_Cooler.

The sum of the external and the inhalation dose was compared to the current values of the DCFs from Laplante, et al. (1997) to determine whether this pathway would be a significant contributor to the overall dose from groundwater releases of radionuclides. The results of the calculation are summarized in the following tables:

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Radionucl de	Inhalation D	Breathing R	Large Fan - Qua ntity	Medium Fan - Quant ity of water	Small Fan - Quant ity of evapo rated wa ter	Large Fan Medium	F	Small Fan Ai	Fraction of da	Fraction of ye	Dose - Me diu m
C 14	0.00E+00	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	0.00E+00
PD107	8.10E+02	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	3.55E-09
NI 59	1.32E+03	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	5.80E-09
C 14	2.09E+03	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	9.14E-09
NI 63	3.10E+03	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	1.36E-08
CS135	4.55E+03	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	1.99E-08
TC 99	8.33E+03	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	3.65E-08
SE 79	9.84E+03	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	4.31E-08
SN121M	1.15E+04	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	5.04E-08
PD107	1.28E+04	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	5.59E-08
CL 36	2.19E+04	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	9.61E-08
MO 93	2.84E+04	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	1.25E-07
SM151	3.00E+04	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	1.31E-07
AG108M	3.01E+04	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	1.32E-07
CS137	3.19E+04	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	1.40E-07

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I129	1.74E+05	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	7.60E-07
AG108M	2.83E+05	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	1.24E-06
ZR 93	3.21E+05	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	1.41E-06
NB 94	4.14E+05	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	1.82E-06
SR 90	1.30E+06	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	5.69E-06
PU241	8.25E+06	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	3.62E-05
RA226	8.58E+06	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	3.76E-05
PB210	1.36E+07	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	5.95E-05
U238	1.18E+08	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	5.19E-04
U235	1.23E+08	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	5.38E-04
U236	1.25E+08	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	5.50E-04
U234	1.32E+08	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	5.80E-04
U233	1.35E+08	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	5.93E-04
CM244	2.48E+08	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	1.09E-03
CM243	3.07E+08	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	1.35E-03
TH230	3.26E+08	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	1.43E-03
PU238	3.92E+08	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	1.72E-03
PU242	4.11E+08	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	1.80E-03
AM242M	4.26E+08	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	1.86E-03
PU239	4.29E+08	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	1.88E-03
PU240	4.29E+08	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	1.88E-03
AM243	4.40E+08	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	1.93E-03
AM241	4.44E+08	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	1.95E-03
CM246	4.51E+08	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	1.98E-03
CM245	4.55E+08	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	1.99E-03
NP237	5.40E+08	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	2.37E-03
U232	6.59E+08	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	2.89E-03
PA231	1.28E+09	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	5.63E-03
TH229	2.15E+09	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	9.40E-03
AC227	6.70E+09	3.33E-04	378.5	264.95	56.775	3.91E+08	2.04E+08	8.97E+07	0.55	0.58333	2.93E-02

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Radionuclide	Dose - Dose Medium fan (rem/yr/yr/pCi/L)	Direct Exposure (rem/yr/pCi/L)	Current (rem/yr/pCi/L)	DCF Evaporative Cooler Dose/Current DCF
TC 99	3.65E-08	5.82E-11	4.80E-06	8.81E-05
I129	7.60E-07	1.30E-07	1.30E-03	1.06E-04
NB 94	1.82E-06	1.07E-04	6.60E-05	6.19E-01
NP237	2.37E-03	1.21E-06	9.10E-03	2.73E-03

#### Results:

It appears that the additional pathway from the use of evaporative coolers would not significantly increase the dose from the radionuclides that are the most significant contributors to dose in the TPA code (Tc-99, I-129, and Np-237). Other radionuclides, such as Nb-94, with a more significant external exposure component could be affected more by the inclusion of the evaporative cooler pathway.

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Entries into Scientific Notebook #170 for pages 266 - 286 have been made by James Weldy.

No original text entered into this Scientific Notebook has been removed.

James F. Weldy date 10-1-01

I have reviewed this scientific notebook and find it in compliance with QAP-0001+

James Weldy

James F. Weldy 10-9-05

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