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ICSP-LP-FP-1

# International Agreement Report

## TRAC-PF1 Code Assessment Using OECD LOFT LP-FP-1 Experiment

Prepared by  
F. J. Barbero

Centro de Investigaciones Energeticas  
Medioambientales y Tecnologicas  
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Madrid, Spain

Office of Nuclear Regulatory Research  
U.S. Nuclear Regulatory Commission  
Washington, DC 20555

April 1992

Prepared as part of  
The Agreement on Research Participation and Technical Exchange  
under the International Thermal-Hydraulic Code Assessment  
and Application Program (ICAP)

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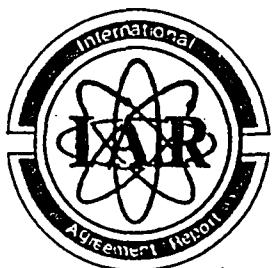
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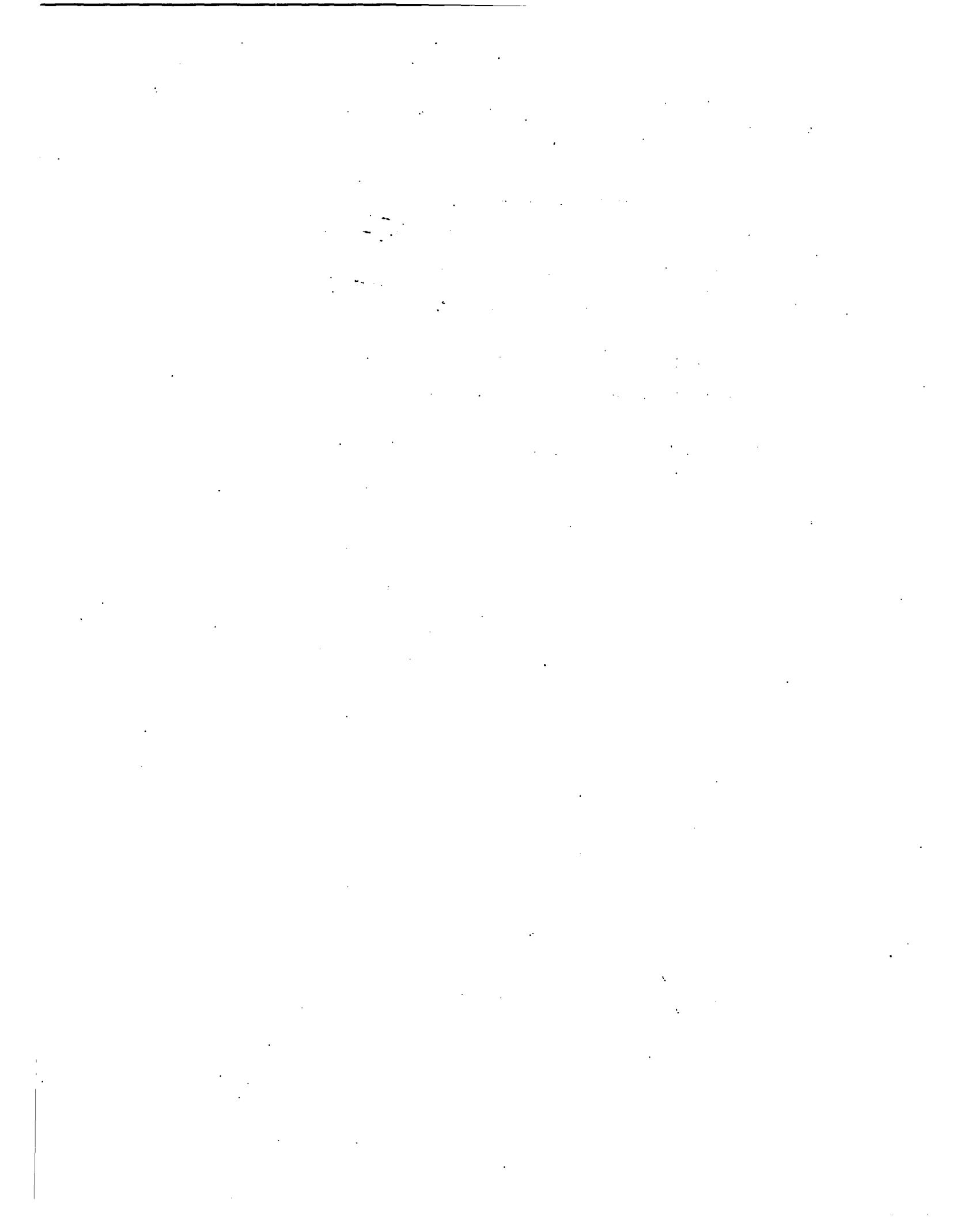
## **ABSTRACT**

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Document resumes the final calculations of the thermal-hydraulic aspects of the OECD LOFT-LP-FP-1 experiment, with emphasis in those related with the assessment of the TRAC-PF1 code.

LOFT LP-FP-1 experiment was carried out at the LOFT facility in INEL, sponsored by the OECD.

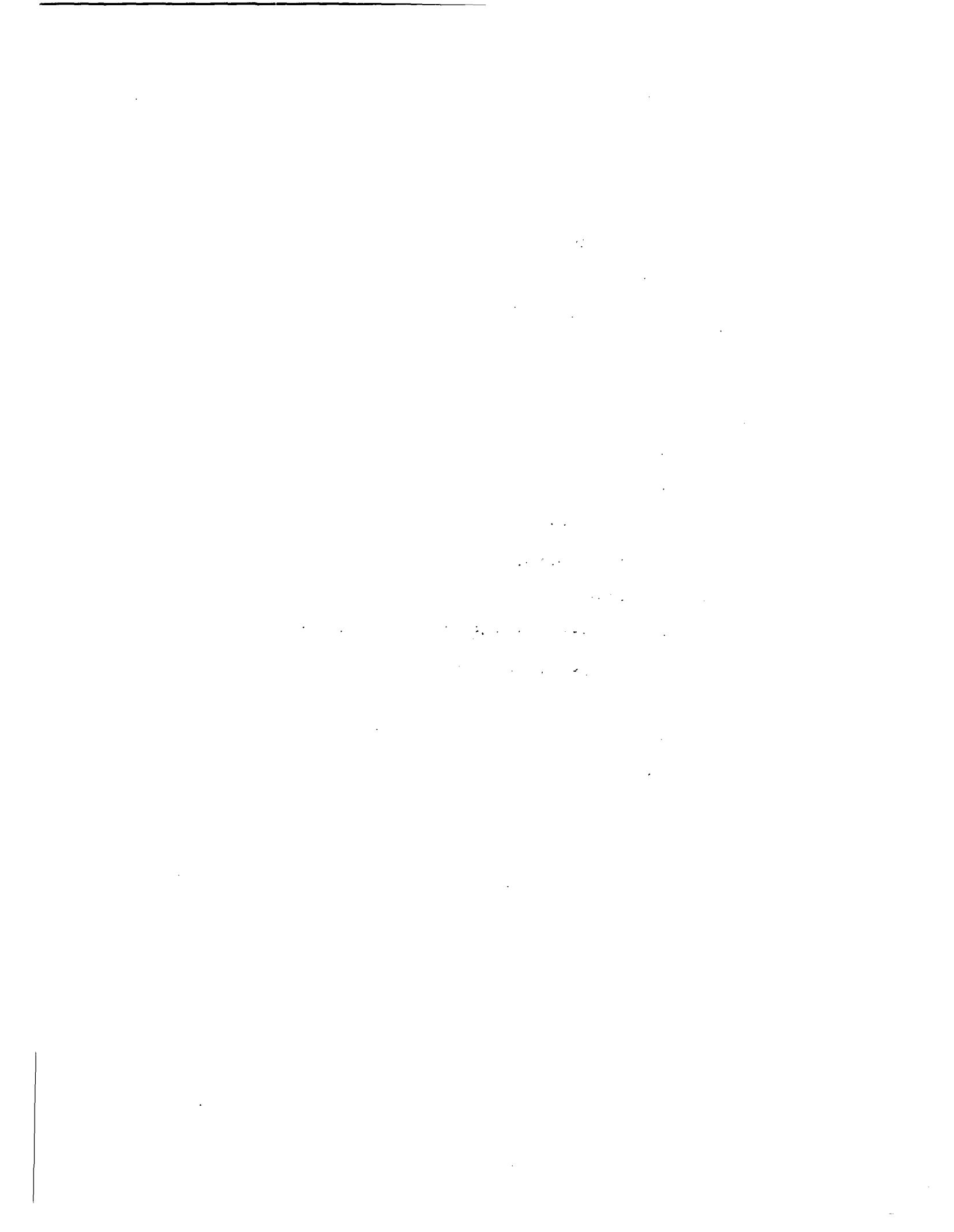
Code used for this simulation was TRAC-PF1/Mod 1 (version 11.0) running on a CDC Cyber 830 (O.S. NOS-BE).



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## FOREWORD

This report represents one of the assessment/application calculations submitted in fulfilment of the bilateral agreement for cooperation in thermalhydraulic activities between the Consejo de Seguridad Nuclear of Spain (CSN) and the United States Nuclear Regulatory Commission (US-NRC) in the form of Spanish contribution to the International Code Assessment and Applications Program (ICAP) of the US-NRC whose main purpose is the validation of the TRAC and RELAP system codes.

The Consejo de Seguridad Nuclear has promoted a coordinated Spanish Nuclear Industry effort (ICAP-SPAIN) aiming to satisfy the requirements of this agreement and to improve the quality of the technical support groups at the Spanish Utilities, Spanish Research Establishments, Regulatory Staff and Engineering Companies, for safety purposes.

This ICAP-SPAIN national program includes agreements between CSN and each of the following organizations:

- Unidad Eléctrica (UNESA)
- Unión Iberoamericana de Tecnología Eléctrica (UITESA)
- Empresa Nacional del Urano (ENUSA)
- Centro de Investigaciones Energéticas y Medioambientales (CIEMAT)
- TECNATOM
- LOFT-ESPAÑA

The program is executed by 12 working groups and a generic code review group and is coordinated by the "Comité de Coordinación". This committee has approved the distribution of this document for ICAP purposes.



## 1. INTRODUCTION

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The fission products release test LP-FP-1 was conducted on Dec 19, 1984. The first trial to conduct the test on Dec 12 had failed because of a defect in the position indicator of the hot leg QOBV (Quick Opening Blowdown Valve). The test was terminated by the PPS (Plant Protection System) action at about 10 s and the transient ended at 50 s. This test is designated as LP-FP-1A.

The thermal-hydraulic transient of the test LP-FP-1 has been initiated by the reactor scram and opening of the QOBV's with one second delay. This experiment simulates large break LOCA in the cold leg with delayed ECC injection to allow pin rupture and fission products release.

LP-FP-1 was specified to be similar to LOFT experiment L2-5 and OECD LOFT experiments LP-02-6 and LP-LB-1, except for initial primary pump operation, closure of the BLCL valve and ECCS operation for core recovery and fuel cladding quench.

From the thermal-hydraulic point of view, the following objectives were considered achievable:

- Determine system thermal-hydraulics and core thermal response for initial and boundary conditions similar to a large break design basis LOCA leading to and limited to fission product release from the fuel cladding gap region.
- Determine the fission product retention effectiveness of the ECCS operating in a mode representative of a German

PWR ECCS in nominal (best estimate) conditions for combined hot leg and cold leg injection.

During the conduct of FP-1, most of the water in the accumulator B line was unintentionally injected into the upper plenum during the blowdown. This water distorted the thermal behaviour of the core and delayed the burst of the pressurized fuel pins by more than 200 s. Also more than 60 % of the rods that were planned to burst, remained intact. the thermal-hydraulic conditions in the core at the time of fission product release are far less definite than was expected. In order to be able to analyse the test results and to carry out post-test calculations using advanced thermal hydraulic codes, one has to know the amount and the rate of water injected.

We have selected a history for this unexpected injection, based on previous studies. We have run a simulation of 400 s, covering blowdown, heat-up and reflood phases in order to compare the obtained results with the data measured along the experiment, both hydraulic and thermal variables.

A brief description of the LOFT facility, system configuration for LP-FP-1 experiment and test evolution are included in Section 2, together with initial conditions and operational set points.

Section 3 contains the input model for TRAC-PF1 code and nodalization details.

In Section 4, results obtained are checked against the measured data for a set of important parameters showing main physical phenomena that occurred during the experiment.

Run statistics in different regions of the transient are shown in Section 5.

Conclusions and recommendations arising from the study are resumed in Section 6.

Appendix A resumes the instrumentation nomenclature and location for the LOFT system, related with the assessment.

## 2. FACILITY AND TEST DESCRIPTION

---

### 2.1 System configuration

---

The LOFT facility was designed to simulate the major components and system responses of a commercial PWR during a LOCA. The experimental assembly includes five major subsystems which have been instrumented in such a way that the system variables can be measured and recorded during a LOCA simulation. The subsystems include:

- Reactor vessel
- Intact loop
- Broken loop
- Blowdown suppression tank (BST)
- ECC system

Complete information on the LOFT system is provided in ref [1].

The arrangement of the major LOFT components is shown in Figs 2.1 and 2.2. The intact loop simulates three loops of a commercial four-loop PWR and contains a steam generator, two primary coolant pumps in parallel, a pressurizer, a venturi flowmeter and connecting piping.

The broken loop consists of a hot and a cold legs, each of which are connected to the reactor vessel and the BST header. Primary coolant pump and steam generator simulators were installed in the broken loop hot leg to provide the flow resistance normally represented by these components in a

commercial PWR. Each broken leg contains a quick-opening blowdown valve, a recirculation line, an isolation valve, an orifice to represent the break plane, and connecting piping. The recirculation lines establish a small flow through the broken loop to maintain hot fluid conditions in these loops which otherwise are stagnant prior to initiation of the experiment.

The LOFT reactor vessel, shown in Figure 2.3 has an annular downcomer, a lower plenum, lower core support plates, a nuclear core and an upper plenum. The downcomer is connected to the cold legs of the intact and broken loops and the upper plenum is connected to the hot legs.

The core consists of 1300 enriched uranium fuel rods arranged in five square and four triangular fuel assemblies. The fuel rods were designed to commercial PWR specifications except that they are only 1.68 m long and several fuel rods have special instrumentation. Twenty-four fuel rods were enriched to 6 % (wt) U235, and twenty-two of these were pre-pressurized at cold conditions to 2.41 MPa. The other two fuel rods were unpressurized and were designed to be easily removed for PIE. All other fuel rods in the core were un-pressurized and enriched to 4 % (wt) U235. Fig 2.4 shows the fuel cladding thermocouple locations and Fig 2.5 shows all the central fuel assembly instrumentation, as well as the locations of the two fuel rods which were removed for PIE. Fig 2.6 shows the location for the thermocouples in the upper plenum. Nomenclature and location of the instruments may be seen in Appendix A.

The ECCS in FP-1 was designed to simulate the hot leg and cold leg ECC injection rates representative of the ECCS operation in a KWU 1300 Mwe reference PWR under nominal conditions. As mentioned, injection have to be delayed to allow fuel rupture and fission product release and transport in a vapour environment. Accumulator A was rooted to the intact loop cold leg (Fig 2.2) and was used to inject ECC scaled to the reference PWR best estimate cold leg accumulators and LPIS injection based on power scaling ( 1:100).

Accumulator B was rooted to the upper plenum (Fig 2.2) near the top of the center fuel assembly through a special piping configuration convenient to the LOFT system and not related to the reference PWR. Accumulator B was designed to inject ECC scaled to the reference PWR.

As the injection line enters the pressure vessel, it penetrates through the central fuel module and branches in the upper structure (see Fig 2.7). At station 203.17 (3.44 m) above reactor vessel bottom and about 42 cm above the top of fuel pins, 6 reflood injection nozzles are positioned to inject inside the flow shroud in the central fuel module. At station 191.82 (about 13 cm above the top of fuel pins) another 8 reflood nozzles are positioned in such a way as to inject outside the flow shroud and towards the peripheral elements. Details may be found in reference [2].

Accumulator B is connected to the pressure vessel by three lines. Injection in the hot leg, in downcomer or in the upper plenum can be activated. Direct injection in the downcomer is

only activated in case of PPS as happened in LP-FP-1A. The same lines are also used by the low pressure injection system (LPIS). See design of the injection line in Fig 2.8.

The upper plenum injection valve CV-P120-54 which is very near to the pressure vessel was then opened about 90 s before the test while the far valve CV-P120-33 was kept close. This means that the whole line between that valve and the nozzles in the upper plenum was subjected to the system pressure of 14.77 MPa during a period of 90 s before the test.

No accumulator blowdown and no venting of the primary system were performed after the failed experiment and no precautions were taken to prevent nitrogen injection. The injection line of accumulator B included large amount of nitrogen before system pressurization in the transient phase of FP-1. This nitrogen was then compressed to system pressure during the 90 s after opening CV-P120-54 and the gas bubble was moved towards the accumulator B, behind the flowmeter FE-P120-33.

The LOFT steam generator, located in the intact loop, is a vertical U-tube-design steam generator. Operation of the secondary coolant system approximates that of a commercial PWR.

## **2.2 Test description**

---

LP-FP-1 was defined to consist of four distinct phases which were designated as: fuel preconditioning, pretransient, transient and postransient. The four phases were continuous and had specific beginning and ending definitions.

The purpose of the fuel preconditioning phase, in conjunction with the pretransient phase, was to subject the 24.6 % (wt) enriched fuel rods in the new center assembly to the minimum required burnup condition of 1175 MWD/MTU prior to conducting the transient. This burnup is equivalent to power operation at a maximum linear heat generation rate of 52.2 Kw/m for 20 days on the enriched fuel rods. The preconditioning phase started at the begining of plant heatup prior to power operation and ended with termination of power operation after the calculated burnup fraction had been achieved. An additional period of preconditioning beyond that required for minimum burnup occurred after the first attempt of conducting the experiment. The delay of one week resulted in three more days of power operation, reaching 1417 MWD/MTU.

The pretransient phase consisted of a reactor shutdown interval of approximately five days, followed by a power operation interval. The final plant preparations were completed during the reactor shutdown interval. The power operation interval established the required minimum decay heat level (86 % of DH in commercial PWR fuel rods after one year of at 52 Kw/m), and the initial conditions for conducting the experiment. The requirement to build up the short lived

fission product inventory of 40 Equivalent Fission Product Hours was achieved by 70 %. The pretransient phase started at the termination of power operation in the preconditioning phase and ended with initiation of the transient by a reactor scram.

The transient phase of the experiment started with reactor scram, followed by the opening of the QOBV's and ended at the initiation of the closure of the broken loop hot leg (BLHL) QOBV. The BLCL-QOBV was closed at 68 s to ensure that positive core vapour flow existed for the transport of fission products, released from the fuel rod gap, along the intended path for fission product measurements. The unplanned injection of water in the upper plenum due to the expansion of non-condensable gases in the injection line from accumulator B have caused a delay in pin rupture, core reflood and system recovery, which commenced at 344 s instead of the expected value of 100 s on a peak cladding temperature trip of 1037 K in the peripheral fuel assemblies was accomplished with cold leg and upper plenum accumulator ECC injection. The maximum cladding temperature measured in the central fuel assembly was 1210 K.

The final (postransient) phase consisted of a 12 h time from the closure of the BLHL-QOBV, for measuring the redistribution of fission product inventory in gas and liquid in the BST and PCS.

The initial conditions are specified in Table 2.1 together with the measured system conditions immediately prior to the

transient phase of LP-FP-1. The operational setpoints specified are listed in Table 3 together with the measured values. Differences between specified and operational setpoints reflect in some cases the time elapsed between operator action and system response.

As shown in Table 2.2, the break apertures was taken as the initiation time of the experiment. The reactor was scrammed one second prior to the initiation of blowdown. This was done for avoiding early departure from nucleate boiling (DNB) on the 6 % fuel rods which would lead to excessive cladding temperatures early in the transient. The blowdown was the initiated by opening the QOBVs and the pumps were turned off and decoupled from their flywheels within 1 s.

The PCS quickly depressurized to saturation pressure in the upper plenum, broken hot and cold legs by 0.1, 1.1 and 3.5 s, respectively. A bottom-up partial core quench occurred between 6 and 7 s, followed at 12 to 18 s by a total top-down quench of the central fuel assembly. The lower part of some of the peripheral fuel rods did not completely quench at this time. This total top-down quench was the 1st indication that the upper plenum injection line was leaking. This unplanned injection of water in the upper plenum doesn't influence the pressure history.

The cold leg QOBV was closed by 68 s, forcing all break flow out the cold leg and core flow from bottom to top. A sustained heatup of most (not all) of the core started at 90 s, resulting in the rupture of some of the enriched fuel

rods beginning at 325 s. The ECCS was initiated at 344 s and the entire core was quenched by 365 s. A 12 h postexperiment sampling period followed and the experiment was then terminated with plant cleanup and sample removal for PIE.

**TABLE 2.1. Initial conditions for experiment LP-FP-1**

	Specified <sup>(a)</sup> Value	Measured Value
<b><u>PRIMARY COOLANT SYSTEM</u></b>		
Core delta T (K) .....	$14.4 \pm 0.1$	
Primary system pressure (hot leg) (MPa) .....	$14.95 \pm 0.1$	$14.77 \pm 0.07^{(b)}$ (-1.2 %)
Hot leg temperature (K) .....	$577 \pm 1.1$	$577.6 \pm 0.8$
Cold leg temperature (K) .....		$563.2 \pm 1.1$
Mass flow intact loop (kg/s) ....	$479 \pm 19$	$486.7 \pm 2.5^{(b)}$ (+1.6 %)
Boron concentration (ppm) .....		$612 \pm 15$
Primary coolant pump injection (both pumps) (L/s) .....	$0.127 \pm 0.016$	$0.126 \pm 0.003$
<b><u>REACTOR VESSEL</u></b>		
Power level (MW) .....	$38 \pm 1$	$37.0 \pm 1.2^{(b)}$ (-2.6 %)
Maximum linear heat generation rate (kW/m) .....	$\sim 52$	$51.2 \pm 3.6$
Control rod position (above full-in position) (m) .....	$1.37 \pm 0.01$	$1.38 \pm 0.002$
<b><u>STEAM GENERATOR</u></b>		
Secondary system pressure (MPa) .		$6.41 \pm 0.08$
Water level (m) <sup>(c)</sup> .....	$0.19 \pm 0.05$	$0.15 \pm 0.06^{(b)}$ (-21 %)
<b><u>PRESSURIZER</u></b>		
Liquid volume ( $m^3$ ) .....		$0.66 \pm 0.02$
Steam volume .....		$0.27 \pm 0.02$
Water temperature (K) .....		$616.2 \pm 5.8$
Pressure (MPa) .....		$14.73 \pm 0.11$
Liquid level (m) .....	$1.12 \pm 0.1$	$1.23 \pm 0.04^{(b)}$ (+9.8 %)
<b><u>BROKEN LOOP</u></b>		
Cold leg temperature (K) .....		$561.4 \pm 1.5$
Hot leg temperature (K) .....		$564.8 \pm 1.8$

... / ...

... / ...

	<u>Specified<sup>(a)</sup> Value</u>	<u>Measured Value</u>
<u>SUPRESSION TANK</u>		
Liquid level (m) .....	1.27 ± 0.127	1.52 ± 0.06 <sup>2)</sup> (+19.6 %)
Gas volume (m <sup>3</sup> ) .....		47.90 ± 2.11
Water temperature (K) .....		354.4 ± 3
Pressure (gas space) (kPa) .....		99.5 ± 3
Boron concentration (ppm) .....		3898 ± 15

EMERGENCY CORE COOLING SYSTEM

Borated water storage tank tem- perature (K) .....	303 ± 3	303.4 ± 7
Accumulator A liquid level (m) ..	2.15 ± 0.03	2.11 ± 0.01 <sup>2)</sup> (-1.8 %)
Accumulator A standpipe position (above inside bottom of tank) (m)		0.4 ± 0.03
Accumulator A pressure (MPa) ....	4.14 ± 0.17	4.30 ± 0.06 <sup>2)</sup> (+3.8 %)
Accumulator A liquid tempera- ture (K) .....	303 ± 3	300 ± 6 <sup>2)</sup> (-0.99 %)
Accumulator B liquid level (m) ..	2.1 ± 0.03	2.08 ± 0.01 <sup>2)</sup> (-0.9 %)
Accumulator B pressure (MPa) ....	4.14 ± 0.17	4.26 ± 0.06 <sup>2)</sup> (+2.8 %)
Accumulator B liquid tempera- ture (K) .....	303 ± 3	308 ± 6 <sup>2)</sup> (+1.6 %)

(a) If no value is listed, none was specified.

(b) These values were out of specification.

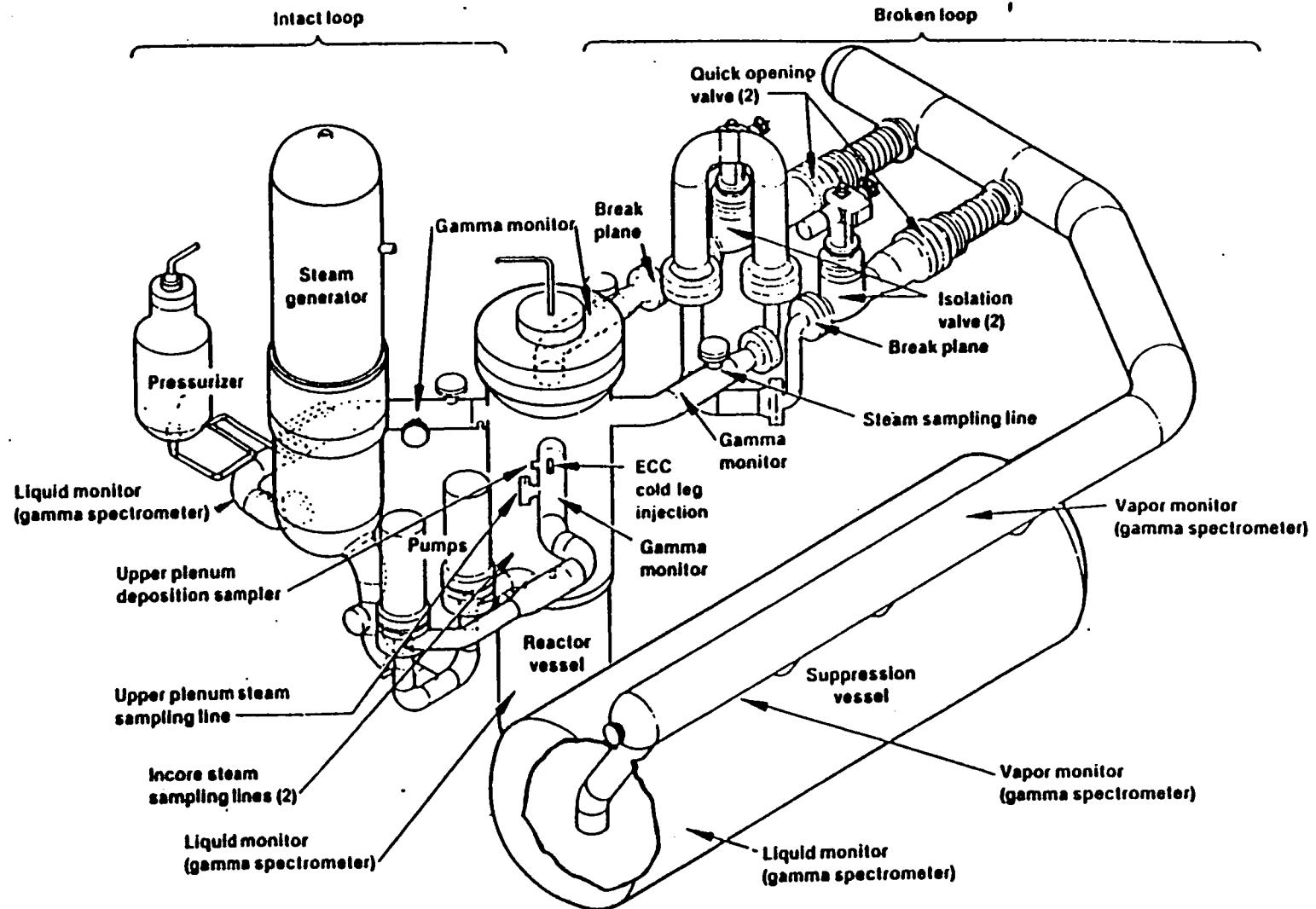
(c) Steam generator liquid level referenced to 2.95 m (116 in.) above top  
of tube sheet.

TABLE 2.2. Operational setpoints

Event	Specified (s)	Actual (s)
Reactor scram .....	1.0 ± 0.025	-0.99 ± 0.01
QOBV open .....	0	0
Primary pumps turned off .....	1.25 ± 0.25	0.91 ± 0.01
FPMS isolation valve opened .....	29 ± 2	29.2 ± 0.1
BLCL QOBV closed .....	49 ± 5	62.5 ± 0.1
FPMS incore isolation valves closed <sup>(a)</sup> .....	341	340.8 ± 0.05
Accumulator A & B injection started <sup>(b)</sup> .....	347 ± 1	344.3 ± 0.05
FPMS BLHL isolation valve closed <sup>(c)</sup> .....	371 ± 2	371.7 ± 0.05
Accumulator injection stopped <sup>(d)</sup> .....	507 ± 1	506.5 ± 0.5
HPIS injection starts <sup>(d)</sup> .....	507 ± 1	515.8 ± 0.5
BLHL QOBV closed <sup>(e)</sup> .....	<527	535 ± 1
QOBV isolation valves closed <sup>(f)</sup> .....	>527	695 ± 1

- (a) Defined as when 3 peripheral thermocouples measured 1037 K (1408 °F).
- (b) 5 to 7 s after FPMS incore isolation valves closed.
- (c) 30±2 s after FPMS incore isolation valve closure.
- (d) 160 s after accumulator injection initiation.
- (e) Within 20 s after accumulator injection termination.
- (f) After closure of BLHL QOBV.

Figure 2.1. Axonometric representation of LOFT system



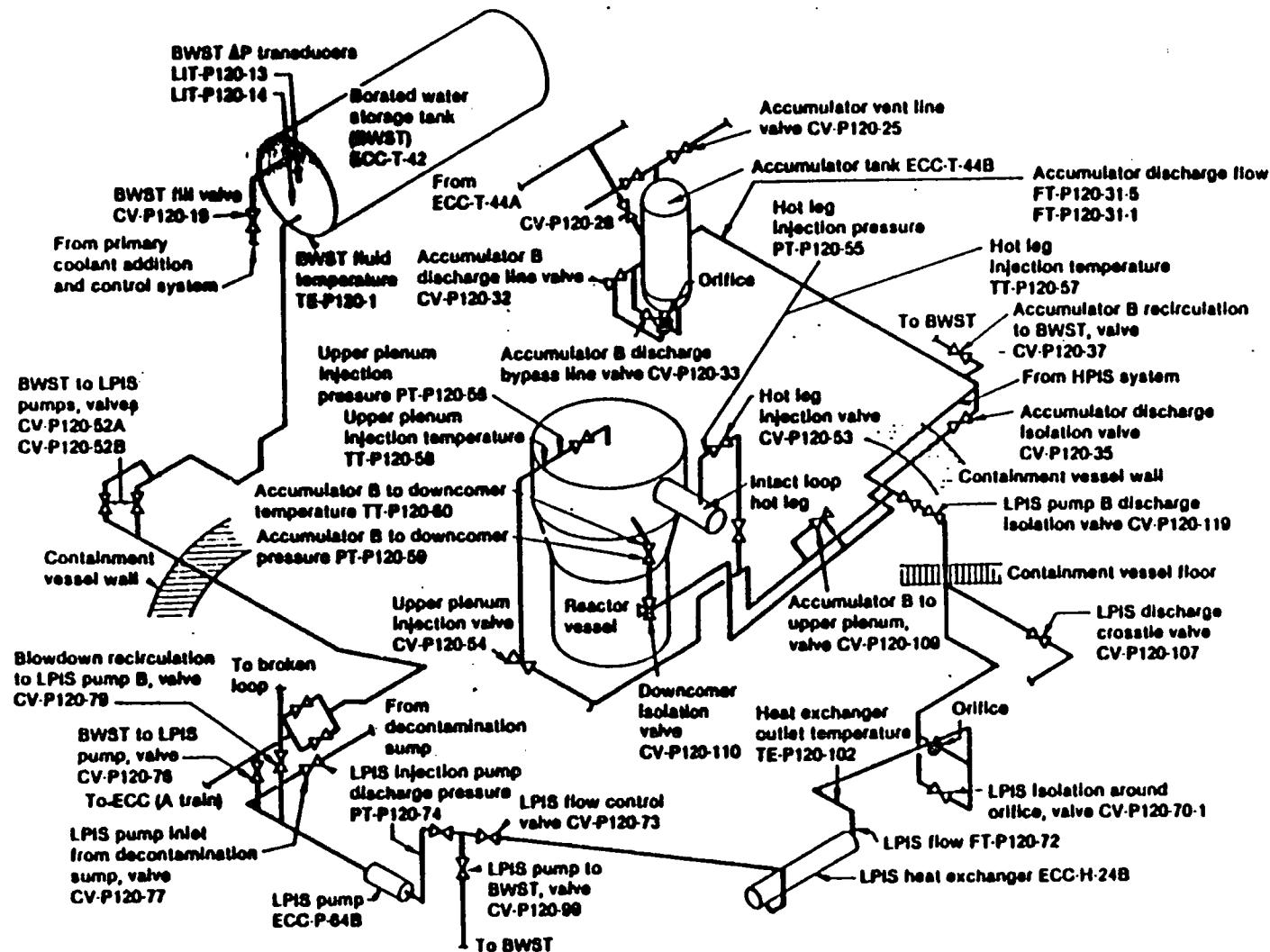


Figure 2.2. Emergency Core Cooling System

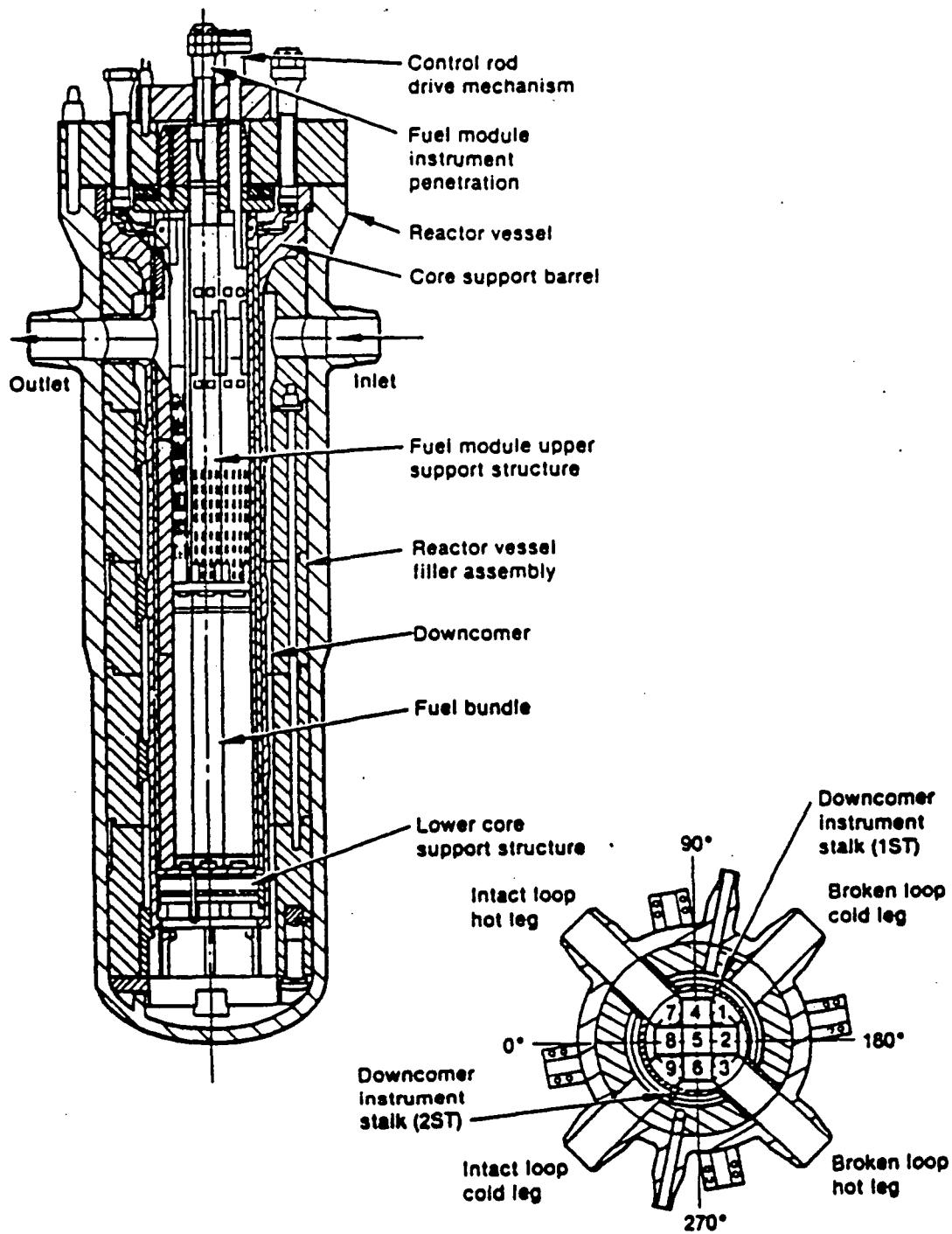
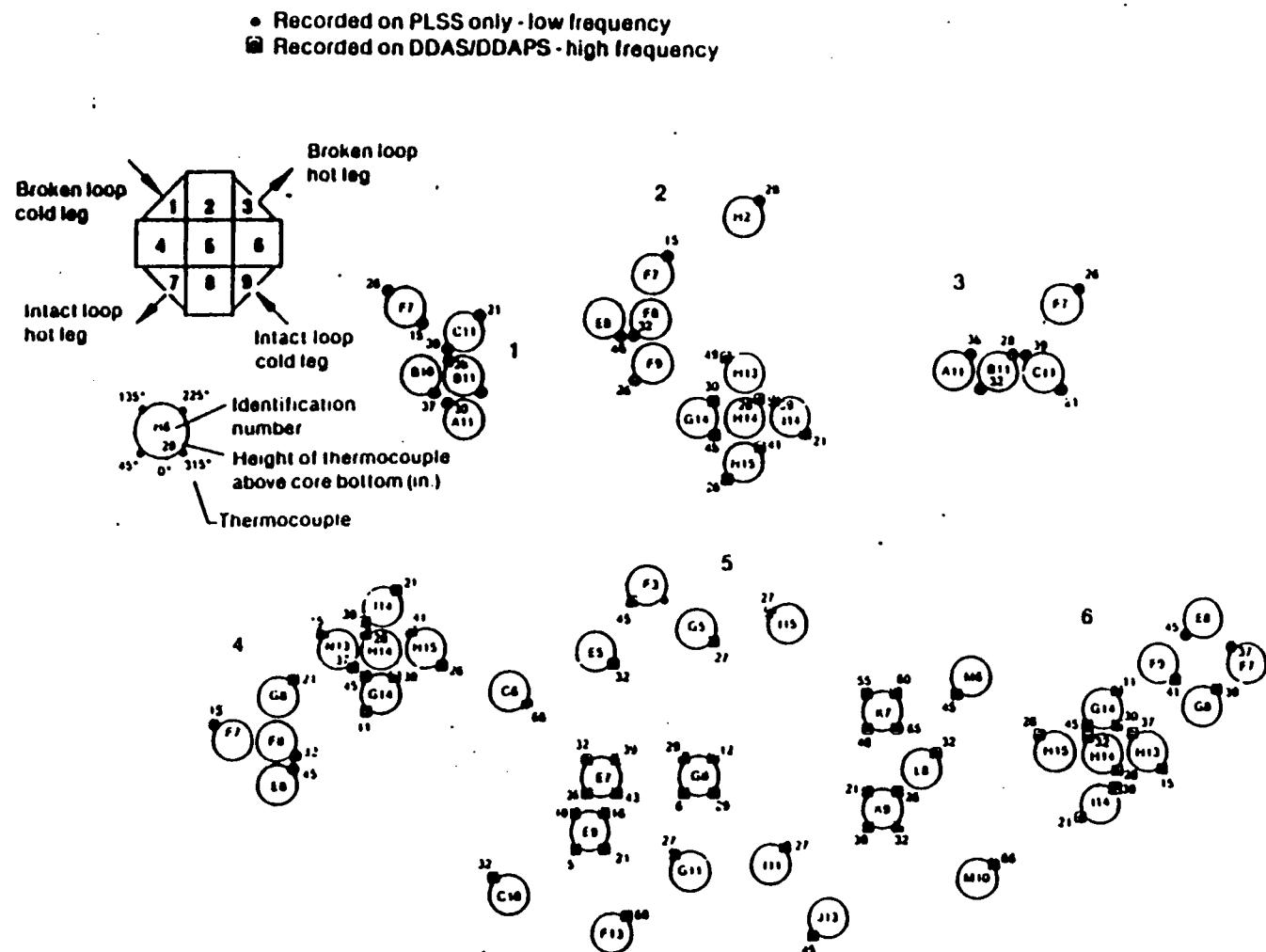


Figure 2.3. Loft reactor vessel

**Figure 2.4. Fuel cladding thermocouples in core**



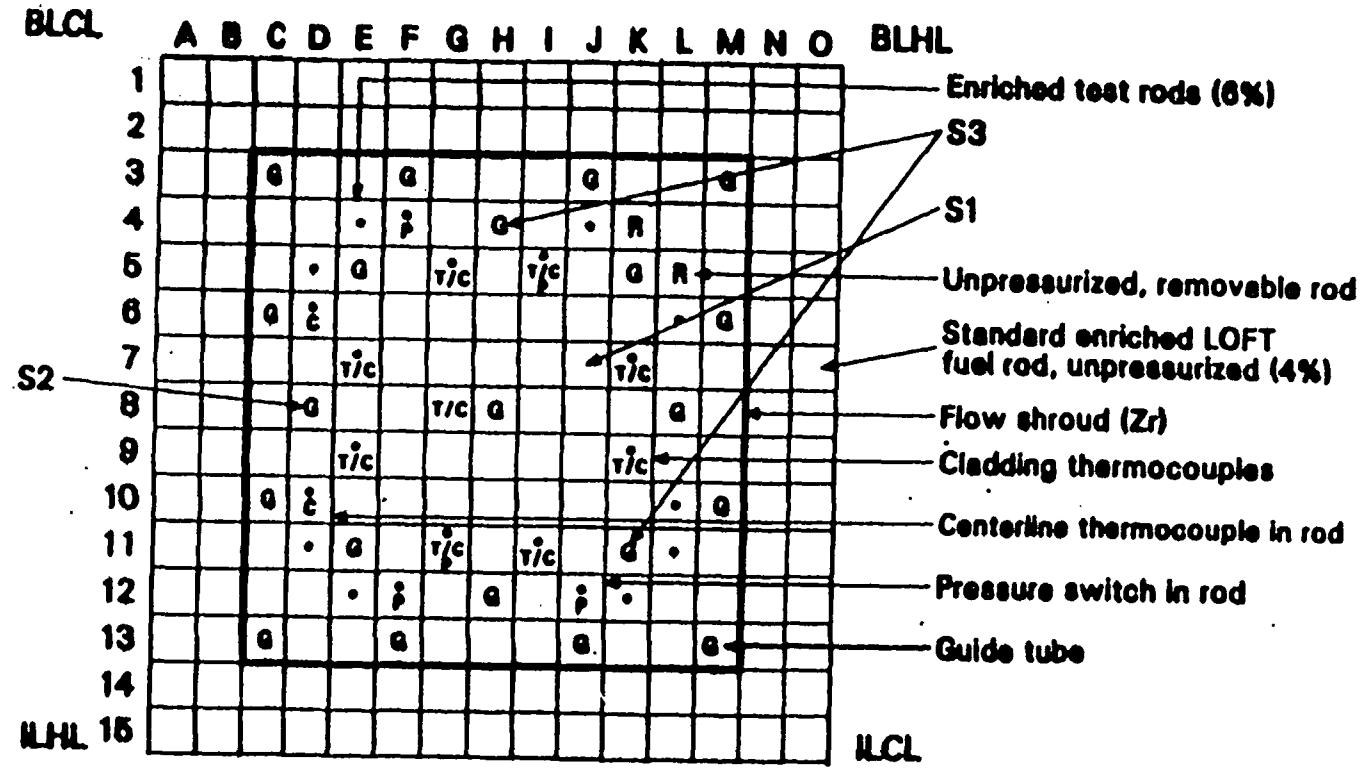
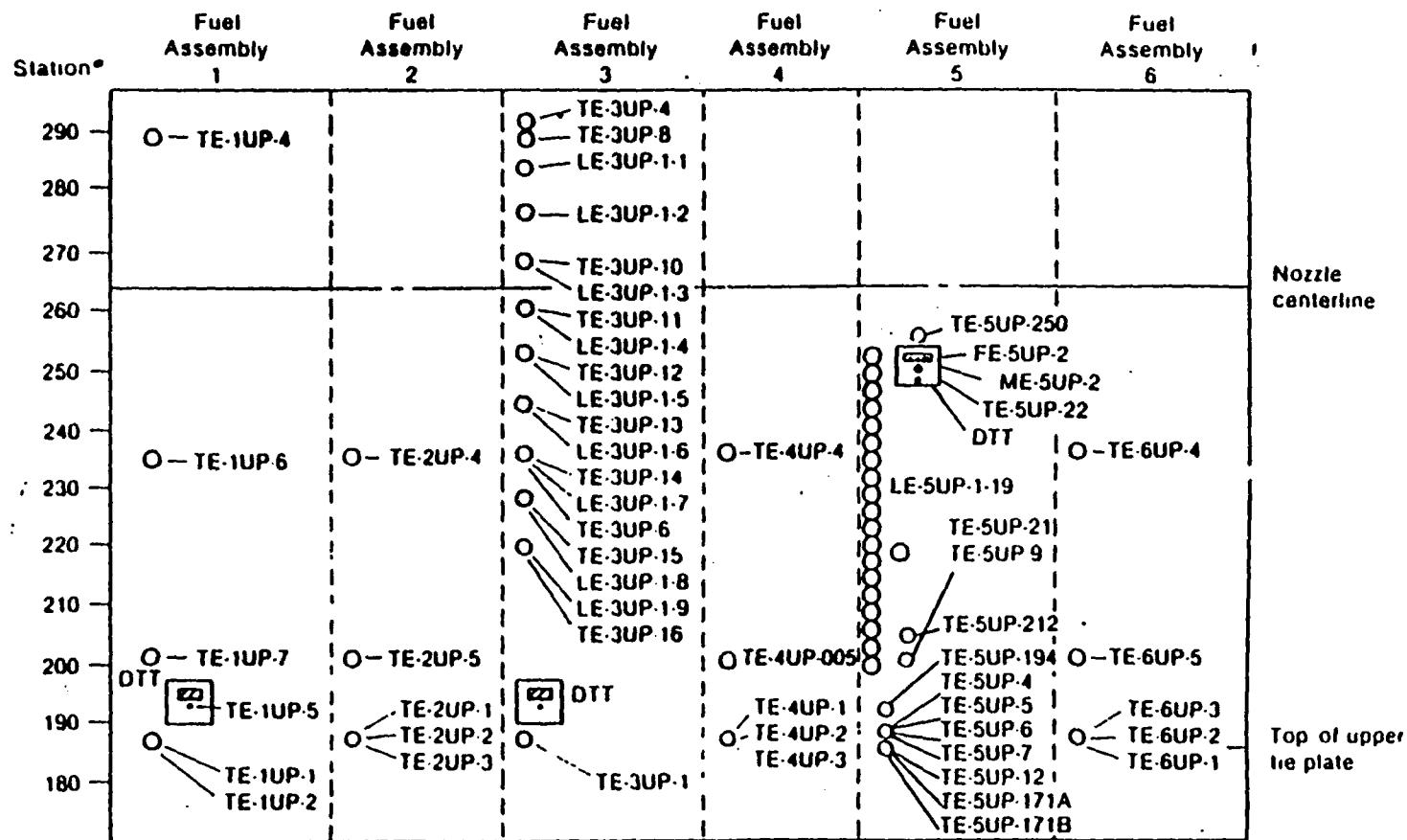


Figure 2.5. Central fuel assembly instrumentation



\*Station numbers are a dimensionless measure of relative elevation within the reactor vessel. They are assigned in increments of 25.4 mm with station 300.00 defined at the core barrel support ledge inside the reactor vessel flange.

Figure 2.6. Upper plenum thermocouples

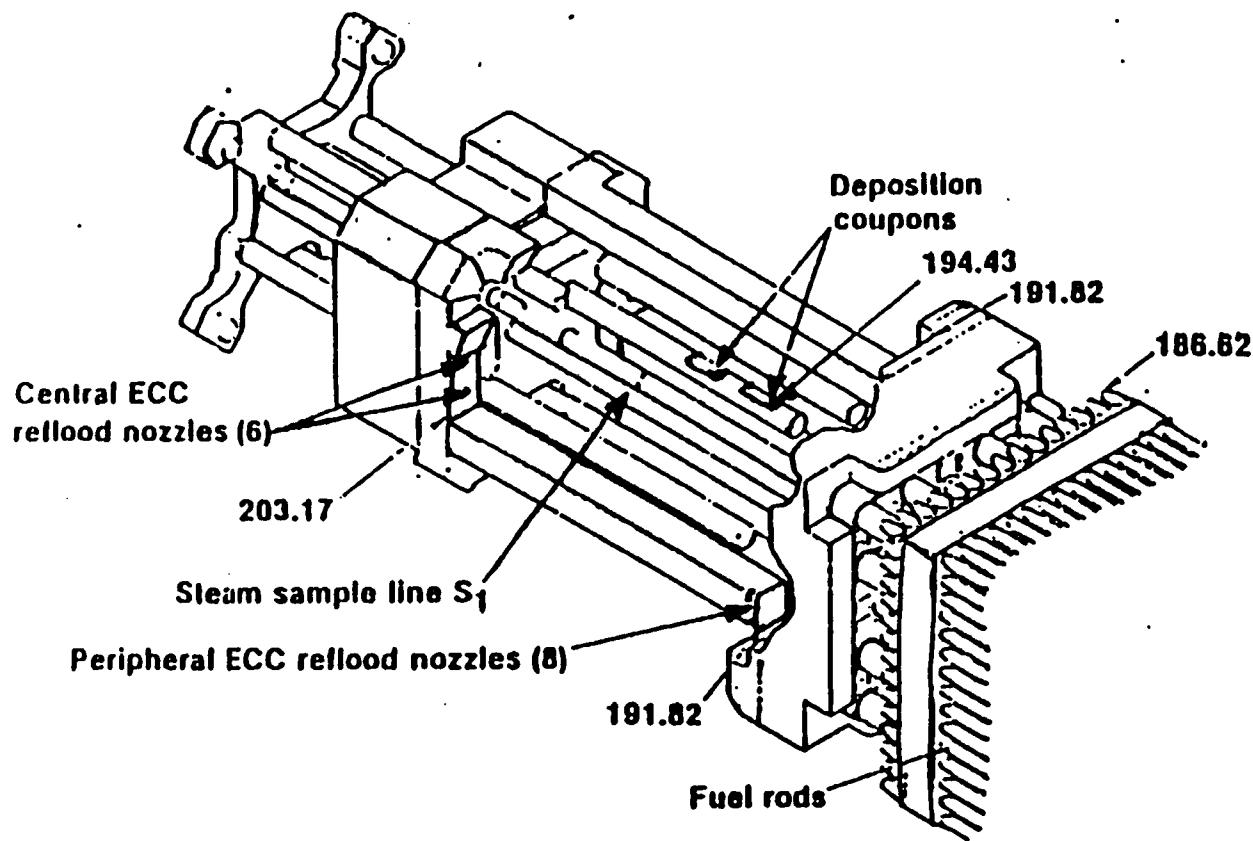


Figure 2.7. Accumulator B upper head injection

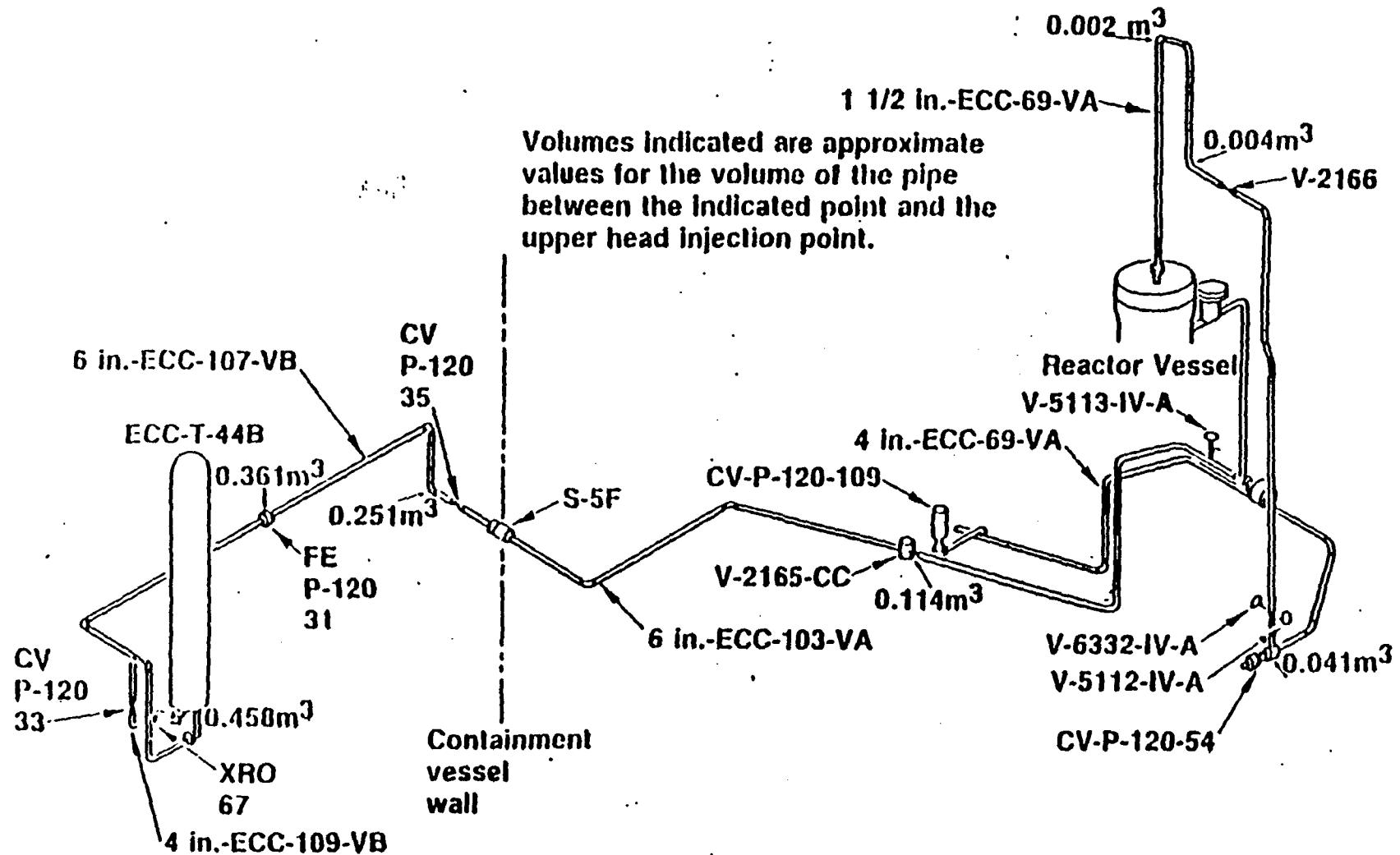


Figure 2.8. Accumulator B injection line

### **3. INPUT MODEL AND NODALIZATION**

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#### **3.1 Code**

---

Code used was TRAC-PF1/Mod 1 (version 11.0), installed on CDC Cyber 830.

The Transient Reactor Analysis Code (TRAC serie P) is an advanced best-estimate code for handling PWR accidents, having the capability to make a 3-D model in the reactor vessel. Code uses full two-fluid model with two-steps numerics in the one-dimensional components and may also handle a noncondensable gas field.

TRAC has the capability to treat the following physical phenomena:

1. ECC downcomer penetration and bypass, including the effects of countercurrent flow and hot walls
2. Lower plenum refill with entrainment and phase separation effects
3. Bottom-flood and falling-film reflood quench fronts
4. Multidimensional flow patterns in the core and plenum regions
5. Pool formation and countercurrent flow at the upper core support plate region
6. Pool formation in the upper plenum
7. Steam binding

8. Average rod and hot rod cladding temperature histories
9. Alternate ECC injection systems, including hot leg and upper head injection
10. Direct injection of subcooled ECC water, without artificial mixing zones
11. Critical flow (choking)
12. Liquid carryover during reflood
13. Metal-water reaction
14. Water-hammer effects
15. Wall friction losses
16. Horizontal stratified flow, including reflux cooling

Code has been used without any modification in models or components. No multiplicative factor for minimum stable film boiling temperature (MSFBT) has been introduced.

### 3.2 Nodalization

---

Nodalization of the LOFT system for the FP-1 test may be seen in Figures 3.1 to 3.6 and Table 3.1.

Input deck for determinig the plant steady state (actually - a first processing by TRAC), is in Table 3.2.

Reactor vessel is modelled as three-dimensional due to the non-homogeneous phenomena registered during the experiment. 3-inner rings represent the core and the 4th downcomer, which extends from level 3 to level 11. Core covers levels 4 to 8 and loops insert at level 11.

First ring simulates the central (11 x 11) fuel assembly and around, a zircaloy shroud. Second and third rings are the internal parts of the peripheral bundles. Vessel is nodalized in 192 cells.

Bypasses have been introduced in the nodalization for getting a better calculation of core liquid fraction (underestimated in pretest calculations). Description and calculations of these bypasses may be found in reference [3]:

- 4 bypasses connecting lower and upper plena, carrying 4.7 % of the flux through the intact loop in the steady state.
- 3 bypasses from downcomer to lower plenum, carrying 4.1 % of the above mentioned flux.

The existence of 1300 rods in the core was simulated using 18 "theoretical" TRAC rods:

- 12 standard rods, representing 4 % enriched fuel rods, one per internal cell.
- 4 rods with peak factor 1.25, simulate the 24 - 6 % fuel rods, one per cell in the central ring.
- 1 rod in cell 8 with peak factor 1.094
- 1 rod in cell 12 with peak factor 1.236

Rod axial dynamic renodalization factor is fixed in a value of 11, instead the initially selected of 60, due to high running times.

Decay heat used has been obtained from the previous power and burn-up histories and may be seen in Table 3.3.

Figure 3.4 shows the intact loop nodalization, including pressurizer, primary side of SG and ECCS with the roots of LPI and HPI systems:

- Accumulator A has been simulated as a PIPE component instead an ACCUM component for avoiding calculation time. Flow rates correspond to those of a 1300 MW scaled KWU reactor.
- Cold leg is fractioned in several cells for helping follow condensation when the accumulator begins to inject.
- Pressurizer has been simulated also as a PIPE for the same reason as before. FILL connected at the upper end represents a relief valve.

Steam generator secondary side is modelled as a STGEN component, including secondary downcomer, main steam line and steam control valve (see Figure 3.5).

Broken loop is shown in Fig 3.6. where secondary sides of TEES represent Reflood Assist Bypass Valve, connecting both legs. Hot leg, which includes simulators of steam generator and pumps, is nodalized in detail but the cold leg has been defined using the minimum number of nodes, due to the TRAC ability for modelling the choked flow.

Accumulator B has been nodalized as 12 independent FILLs (one for each cell) rooted on the vessel axial node 9, where the upper head injector is located. Each FILL has the same injection history (see Fig 3.7 and Table 3.4) but different weights. History has been defined to be azimuthally symmetric but non-homogeneous from one ring to another. During the blow-down and heatup phases, these weights are:

Ring	Weight	Weight per cell
1	0.33	0.0825
2	0.67	0.1675
3	0.	0.

Planned injection from 345 s on, follows the measured data from accumulators and the corresponding weights are:

Ring	Weight	Weight per cell
1	0.20	0.05
2	0.34	0.085
3	0.46	0.115

Unexpected injection history from accumulator B line has been selected through several parametric studies from different authors and from the data registered by thermocouples

such as TE-5UP-004 (see Fig 3.8), guide tubes and flowmeter FE-P120-31. Main characteristics of the selected injection were:

- Bulk of mass injection starts at 16 s, being preceeded of a slight mass flow of coolant.
- Duration of this injection expands up to 100 s.
- Mass flow doesn't cease during the heatup phase.
- A second injection peak exists at 270 s.
- Total unplanned mass water injected is 400.5 Kg.

Trips defined in TRAC to simulate the events occurred during the experiment, were:

t(s)	Event	Components
0.	SCRAM	50
1.	QOBVs aperture	32, 43
2.	Pumps disconnect	4, 5
63.5	QOBV (BLHL) closes	43
345.	Reflood begins	15

Accumulator B and BREAKS are inhibited during the plant steady state calculations. When this state is reached, code starts the transient using restart data and the input deck in Table 3.5.

TABLE 3.1. Nodalization elements of LOFT system

Component Number	Description	Number of Cells	
		Primary	Secondary
Intact	1 Hot leg--TEE .....	8	3
Loop	2 Steam generator--STGEN .....	10	5
	3 Steam generator to pump piping--TEE .....	3	3
	4 Pump--PUMP .....	2	-
	5 Pump--PUMP .....	2	-
	6 Pump discharge--TEE .....	2	1
	7 Cold leg--TEE .....	9	1
	8 Pressurizer--PRIZER .....	3	-
Steam	21 Header-TEE .....	2	1
Generator	22 Downcomer--TEE .....	4	1
Secondary	23 Exit valve--VALVE .....	6	-
	24 Water inlet--FILL .....	-	-
	25 Steam exit--BREAK .....	-	-
Vessel	50 Vessel		
	Axial levels .....	12	
	Radial segments .....	4	192
	Azimuthal sectors .....	4	
Broken	31 Hot leg--TEE <sup>(a)</sup> .....	26	3
Loop	41 Cold leg--TEE <sup>(a)</sup> .....	2	2
	32 Hot leg break--BREAK .....	-	-
	42 Cold leg break--BREAK .....	-	-
	43 Cold leg break--VALVE .....	4	-
Emergency	12 HPI connection and piping--TEE.	1	1
Core	13 LPI connection and piping--TEE.	1	1
Cooling	14 Accumulator check valve--VALVE.	2	-
Systems	15 Accumulator-ACCUM .....	3	-
	16 HPI--FILL .....	1	1
Upper Plenum	81-92 Upper plenum connections, Cells 1 through 12, Vessel Level 9--PIPE .....	1	-
ECCS	61-72 Upper plenum fills--FILL .....	-	-

(a) Secondary sides of hot and cold broken loops represent reflood assist bypass lines.

TABLE 3.3. Decay heat in LP-FP-1

t(s)	DH (MW)	t(s)	DH (MW)
0.	37.	4.	1.987
0.3	32.425	6.	1.875
0.9	9.875	8.	1.792
1.28	5.514	10.	1.726
1.38	3.990	15.	1.605
1.40	3.299	20.	1.518
1.46	2.996	30.	1.396
1.52	2.648	40.	1.309
1.59	2.332	60.	1.136
1.61	2.271	100.	1.070
2.	2.155	200.	0.950
3.	2.062	300.	0.840
		10.E4	0.053

TABLE 3.4. Unplanned injection history

t(s)	Mass flow rate (Kg/s)	Integrated flow (Kg)
0.	0.	0.
0.45	13.0	2.9
1.	0.	6.5
2.	0.67	6.8
16.	0.67	16.2
38.	7.2	102.8
40.	5.9	115.9
100.	0.	292.9
175.	0.5	311.6
255.	0.5	351.7
265.	0.	354.2
271.	1.8	359.6
277.	0.5	366.5
345.	0.5	400.5

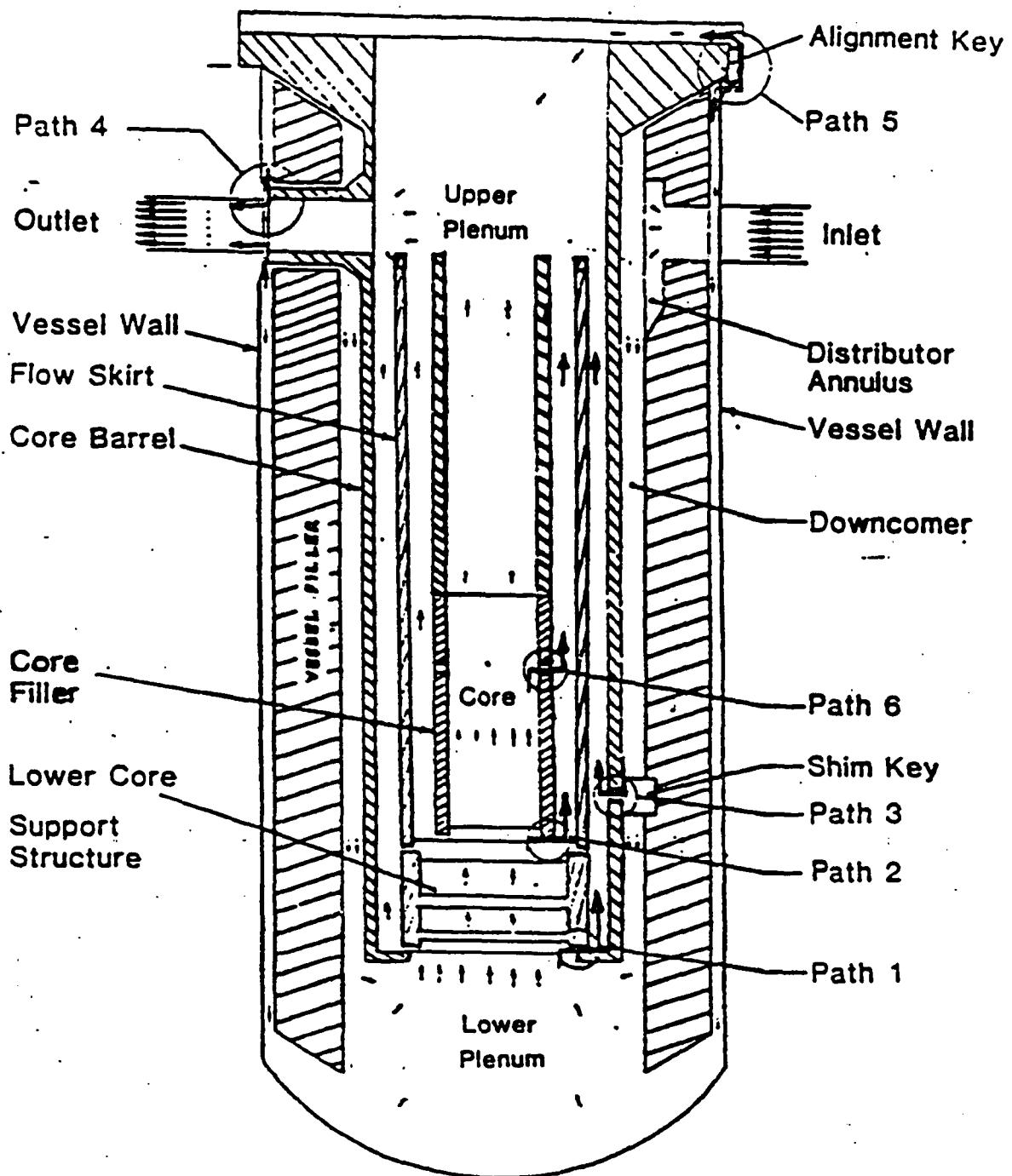


Figure 3.1. Section of LOFT reactor

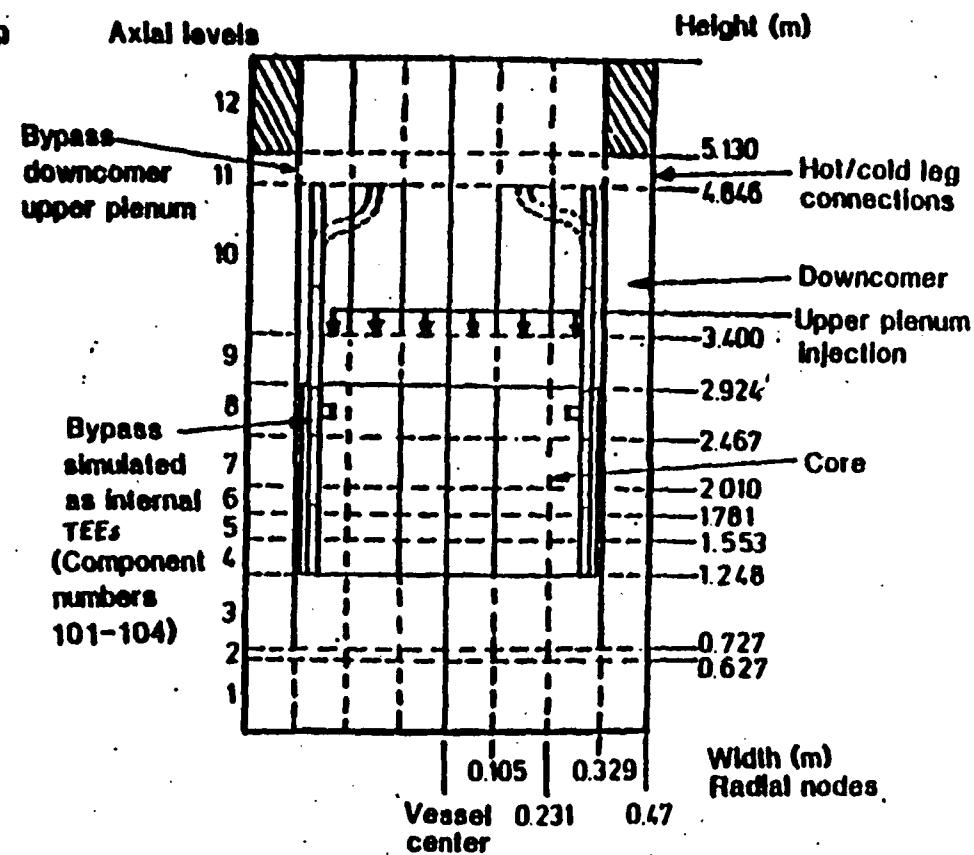
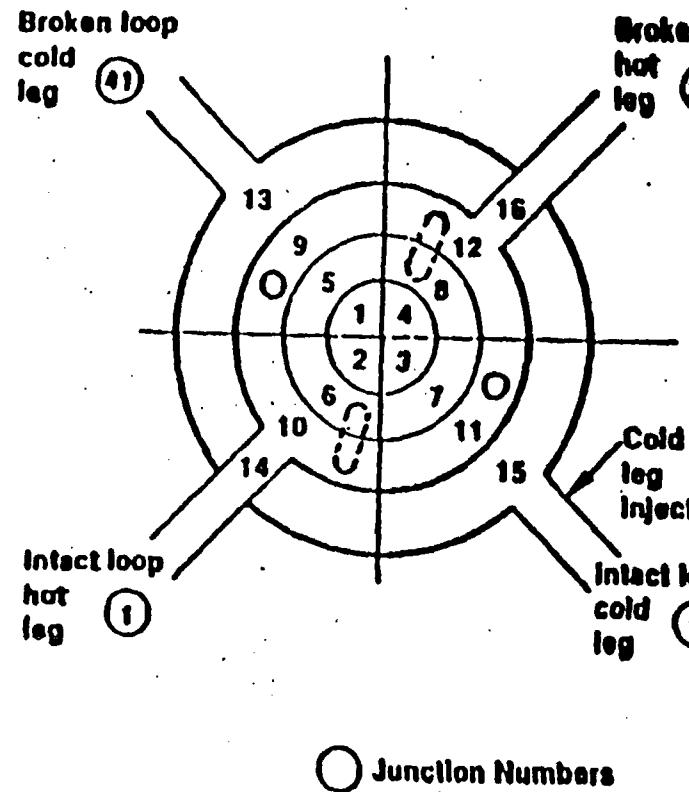


Figure 3.2. Vessel nodalization

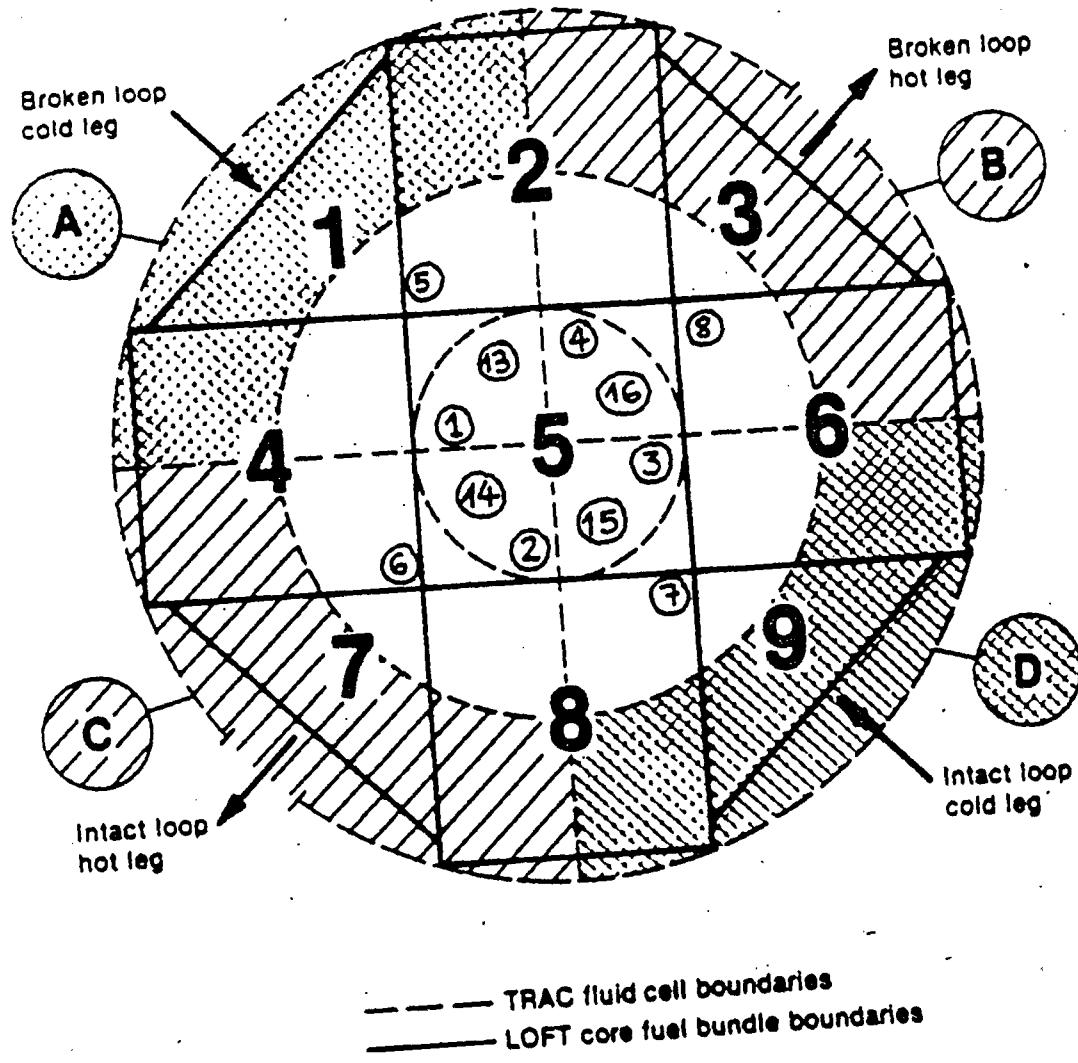


Figure 3.3. Simulated rods location

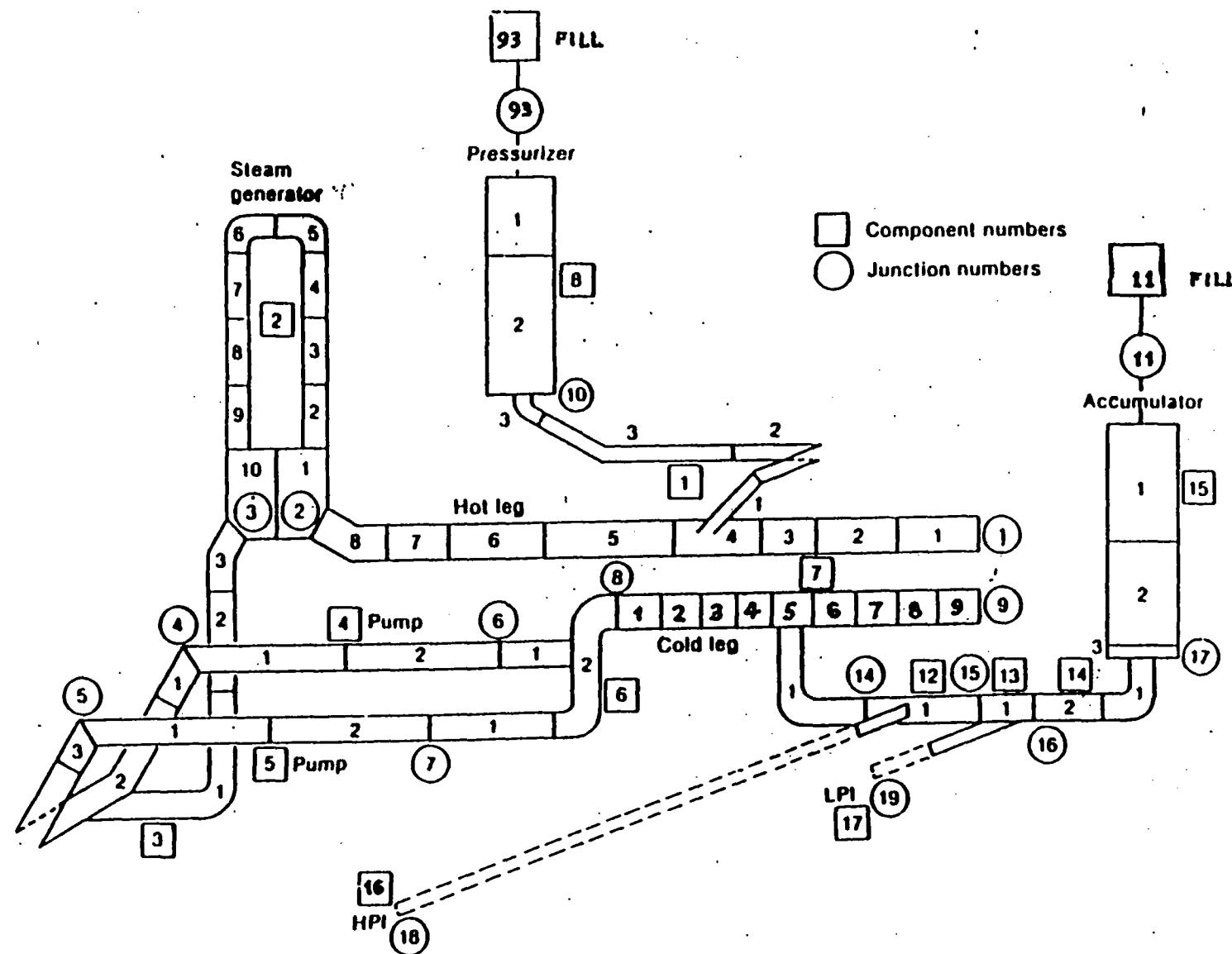


Figure 3.4. Intact loop nodalization

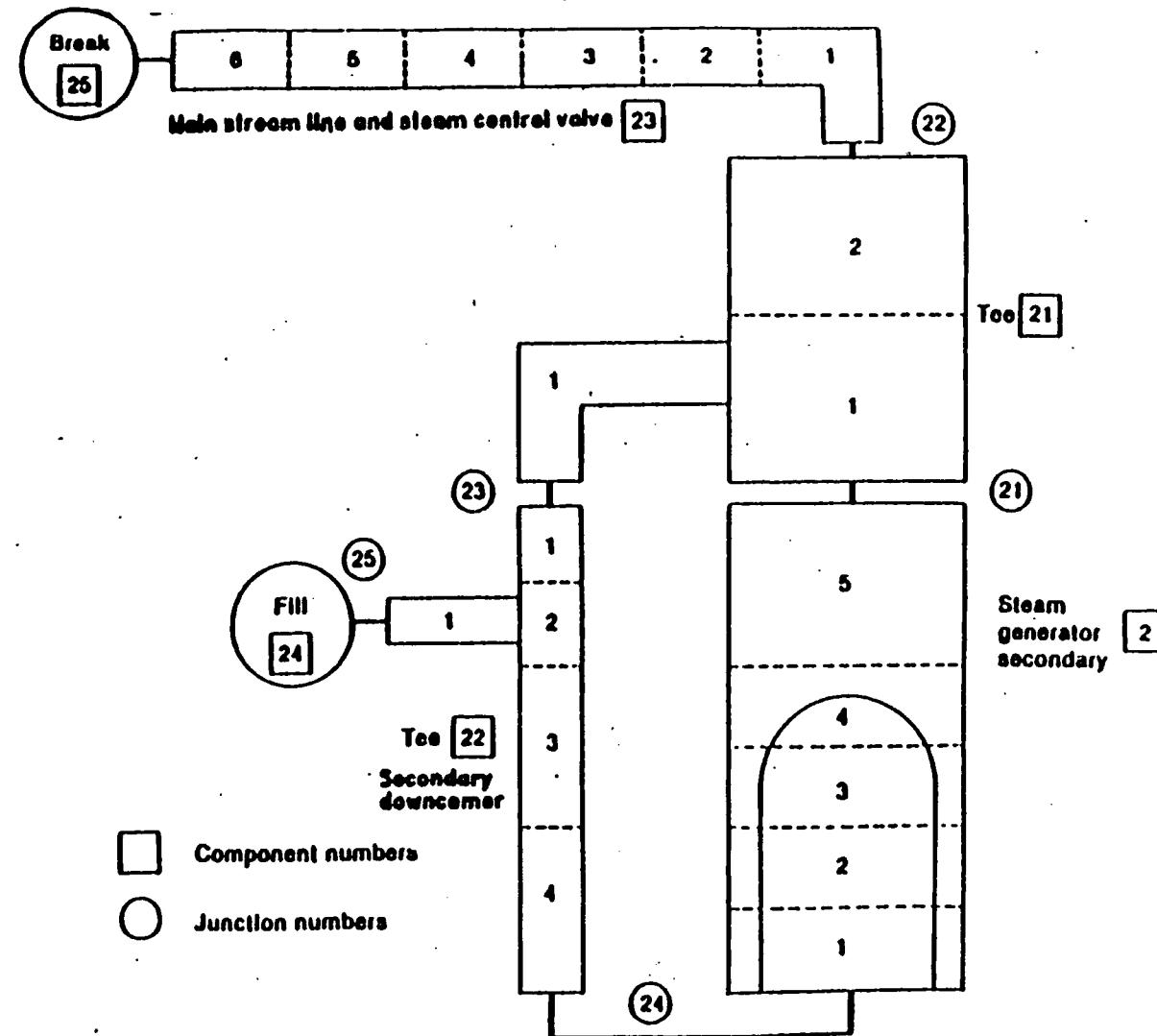


Figure 3.5. Steam generator secondary side nodalization

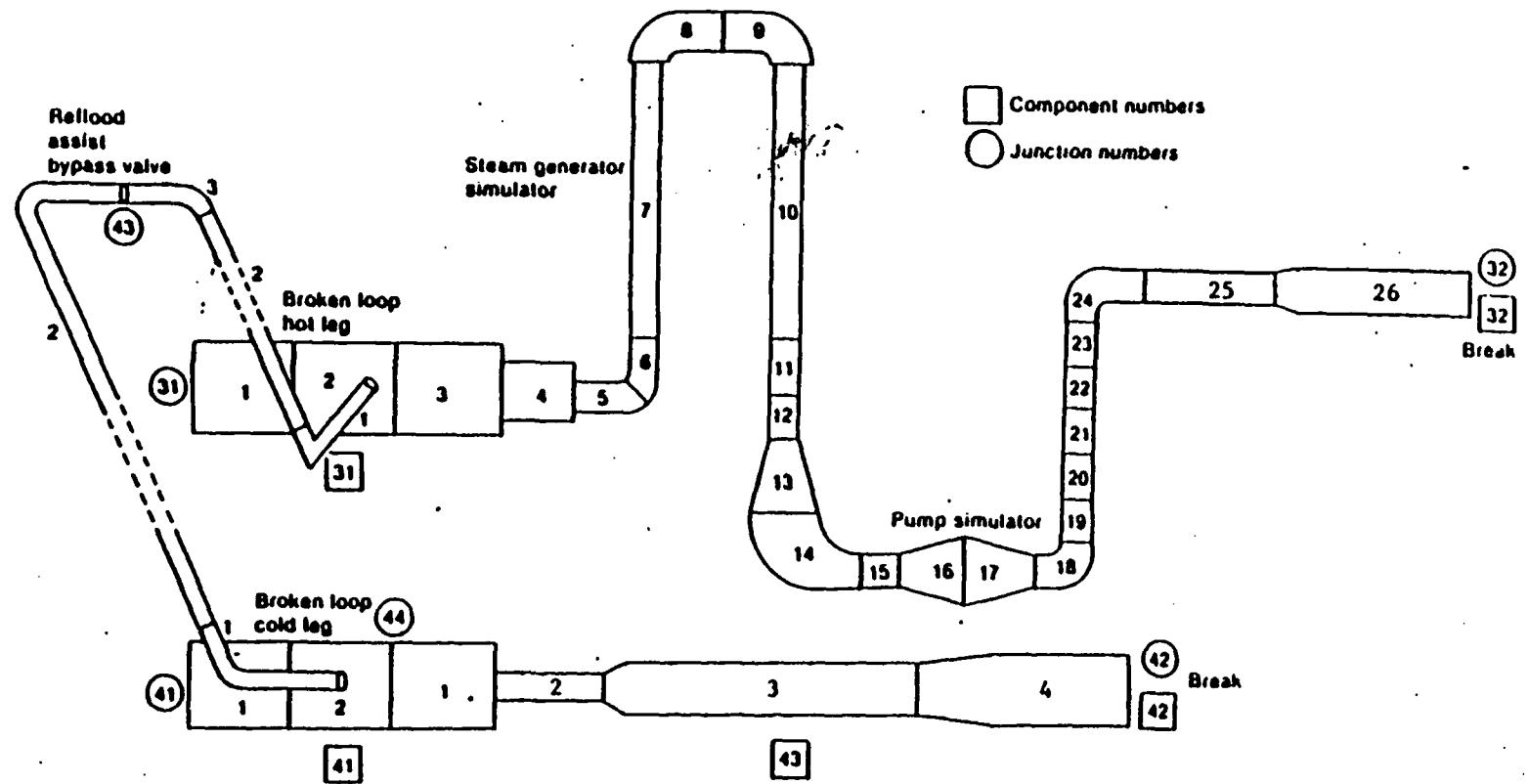


Figure 3.6. Broken loop nodalization

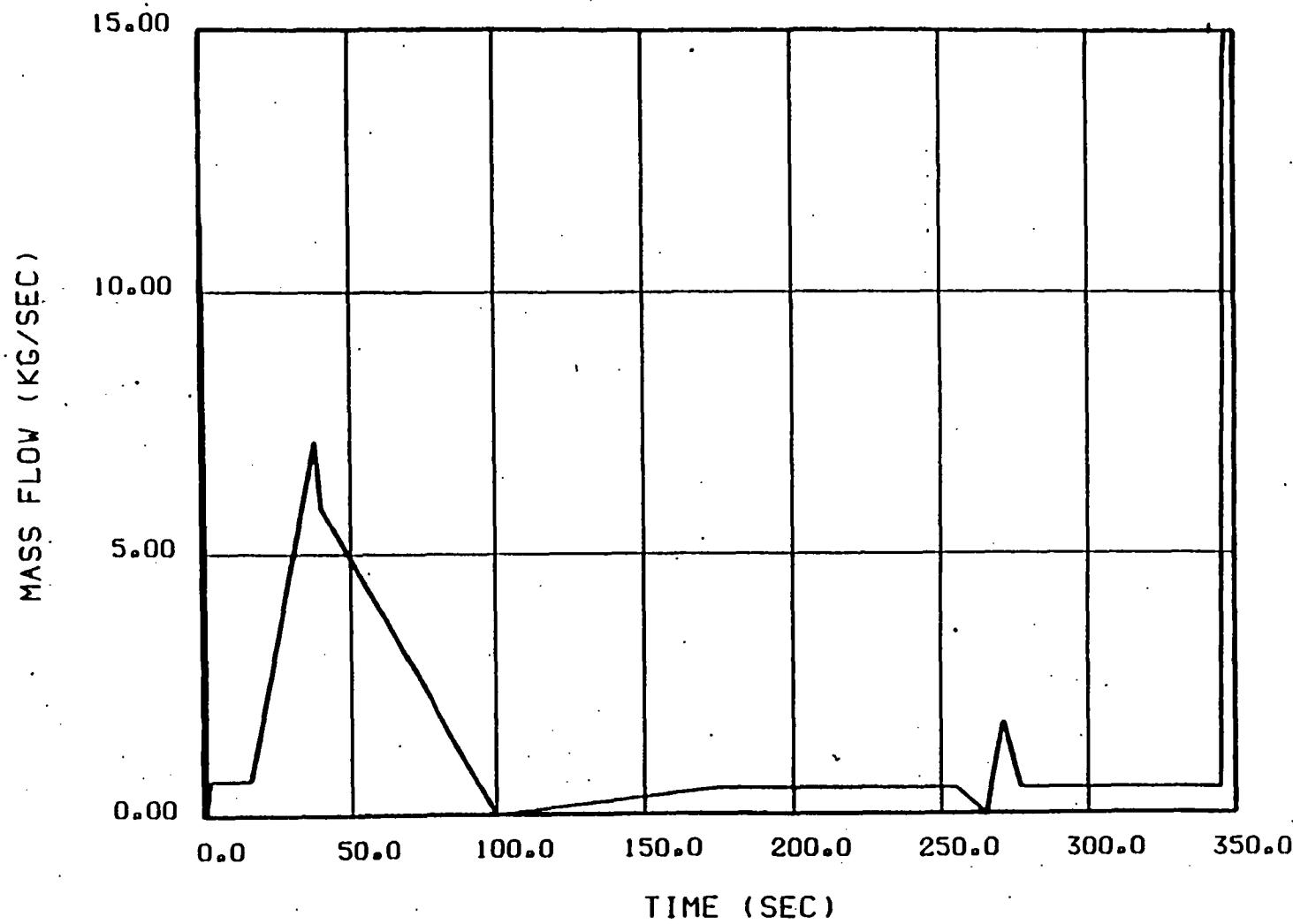


Figure 3.7. Unexpected injection history

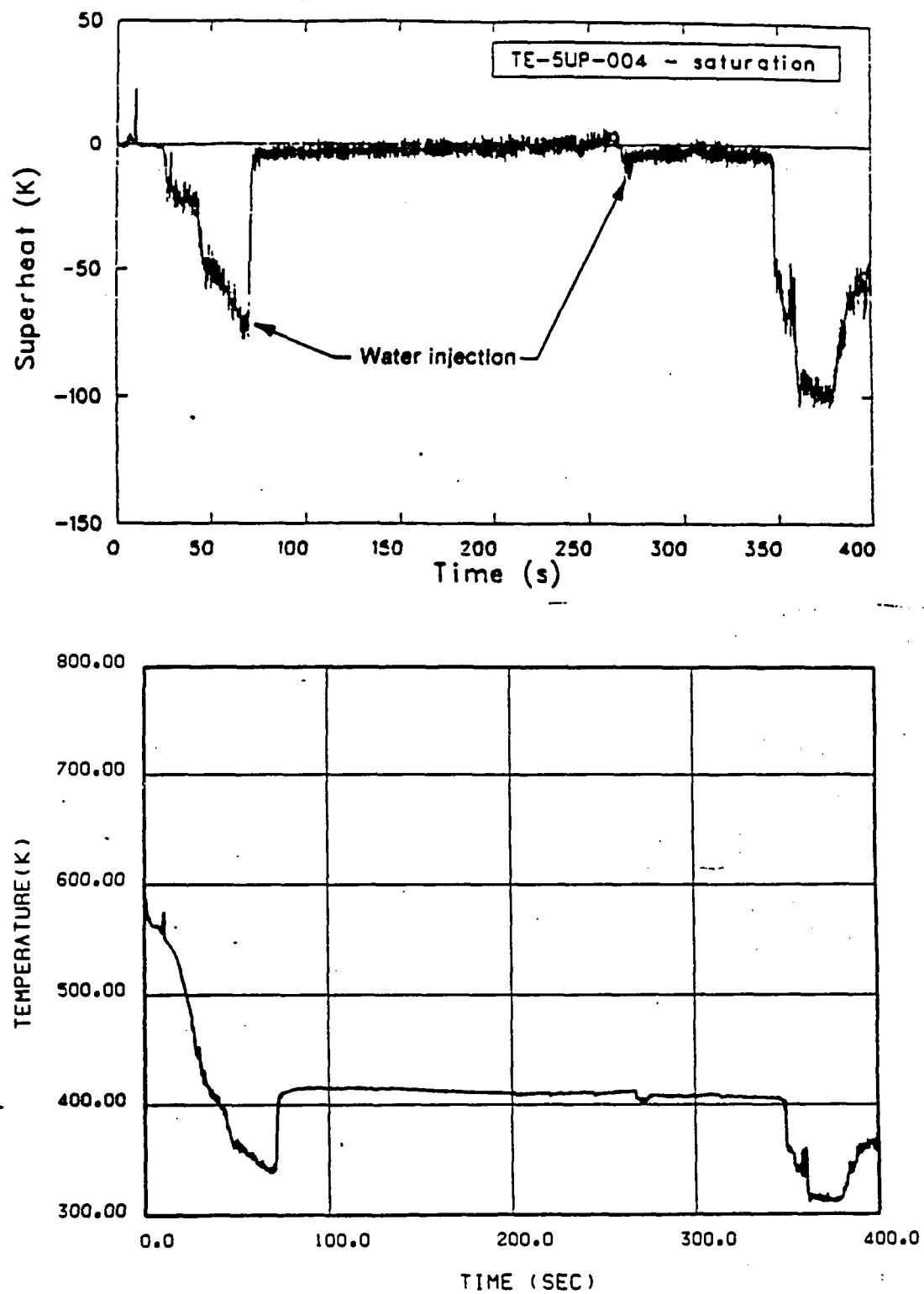


Figure 3.8. TE-5UP-004 measurements

## **4. RESULTS**

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### **4.1 Steady state**

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Plant steady state conditions have been determined after 52 s of "pseudo-transient" for starting the transient phase calculations, based on the referred input model.

Table 4.1 resumes the final values for a representative set of variables, compared with the equivalent measured ones. The agreement is good in general, except in the case of the steam generator dome pressure, which shows a minor convergence rate. The main consequence of this fact is to have a slightly higher temperature in the intact loop (maintaining differences between hot and cold legs), without influence on the transient evolution.

Convergence criteria used (also in transient) have been:

- Inner convergence : 5.0E-6
- Outer convergence : 5.0E-4
- Steady state convergence : 1.0E-5
- Maximum number of iterations in vessel : 50
- Maximum number of outer iterations : 10
- Maximum number of steady state iterations : 25

Total calculation time for this 52 s of pseudo-transient has been 89400 s of CPU.

#### **4.2 Transient**

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We analize in this chapter, results obtained after simulating 400 s of transient, compared with measured data along the experiment. In the case of hydraulic variables, comparison is done between registered data and the variable calculated in the TRAC node related to the detector actual location. For cladding temperatures, code provides information at fixed rod heights; measurements for each thermocouple is compared with the calculations in two adjacent levels and, in some cases, using a cosine law interpolation.

Analysis is mainly directed to explain the asymmetry in the damaged rods distribution and to determine vessel thermal-hydraulic conditions during the fuel rod rupture period (325-345 s), in connection with fission products generation and transport.

Start time of simulation begins at scram time in order to take into account its effects on the plant thermal-hydraulic state, mainly on rod temperatures. From simulation start point through the instant of QOBV apertures, cladding temperatures decrease remarkably, while hydraulic variables remain nearly constant.

#### 4.2.1. Exit flows

When QOBVs open, system pressure drops suddenly due to the subcooled flow through the breaks. Code slightly overestimates ( $\sim 7\%$ ) system pressure up to 16 s, when becomes lower than the observed one, partly because of the unplanned injection existence. The final pressure in the blowdown phase is well calculated (see Fig 4.1).

Figures 4.2 to 4.5 show mass flow rates through the loops, and figures 4.6 to 4.9 the corresponding densities.

Sudden aperture of QOBVs in the broken loop drives the fluid, initially subcooled, to flow out at high velocity, higher in the cold leg, a way with a lower resistance. As pressure continues decreasing, fluid in the broken loop suffer saturation conditions, reaching critical velocity and reducing the mass flow rate. Simultaneously in the intact loop, flow decreases but at lower rate so there is a net positive mass inventory in vessel, causing a bottom-up quench, starting at 4.5-5 s in simulation time (1 s less in real experiment time) (see Fig 4.10 for CORE).

Mass flow rate in the ILHL shows a good agreement with FR-PC-205 detector measurements up to 7 s, when code calculates a back flow from the pressurizer and steam generator. Total mass implied in this flow is about 500 Kg in 18 s, which causes a top-down quench. Fig 4.6 is a plot of the density in ILHL showing two peaks, one for each mentioned back flows (pressurizer and steam generator). First peak is underestimated and delayed, but the second one is simulated properly.

In the ILCL, there is no reference data, because detectors have been removed in this experiment.

Agreement of mass flow rates in BLHL with experimental data is exceptionally good, matching the peaks caused by the mentioned quenches.

Code underestimates the mass flow rate in the BLCL during the initial phase, causing a greater mass inventory and, consequently, a greater pressure as Fig 4.1 has showed (always in the range of the experimental data uncertainties).

Vessel liquid fraction for upper plenum, core and lower plenum may be seen in Fig 4.10, where all the referred initial hydraulic effects can be observed in timing and relative magnitude.

#### 4.2.2 Initial quenches

Loss of coolant and depressurization have as a direct consequence the interruption of fission processes and a drastic fall in the capability of cooling the fuel rods, from now on producing only decay heat.

Figures 4.11 to 4.14 show the evolution of cladding temperatures for the simulated 6 % fuel rods 13, 14, 15 and 16, at heights 0., 0.305, 0.533, 0.762, 1.219 and 1.676 m, during the blowdown phase. Fig 4.15 to 4.18 show, for the same rods and heights, the evolution in the whole transient (blowdown, heatup and reflood phases).

The explanation of the behaviour in cladding temperatures, can be derived from the comparison between this TRAC calculated variables and the corresponding measurements, such as in figures 4.19 and 4.20.

Code calculates an initial rod dry-out beginning at about 3 s (depending on the level). This first heat-up brings cladding temperatures up to the minimum stable film boiling temperature (MSFBT) or beyond, for almost the whole rod surface. A first (bottom-up) quench stops the rise in temperatures in the bar, but isn't able to destroy the film, as the experiment has showed.

After this slight cooling, temperature grows again (in film boiling regime) through the second quench (top-down at 16 s), which rewets all the bar, remaining yet in the same heat transfer mode, while experimental data show a second quench dropping the cladding temperature to saturation. Code predicts

a maximum temperature 2 or 3 s earlier than in the experiment.

Thermocouples remain at saturation several second, but a third dry-out occurs, irregular in timing and magnitude. An unexpected injection, actually non-homogeneous and asymmetric ends this phase. Code responds to the simulated injection only decreasing slowly cladding temperatures and, in some cases (as the 4 % fuel rods in central ring and 6 % fuel rods in cell 3) quenching the whole rod and getting the saturation temperature in the surface, when the MSFBT is reached, but in times delayed up to 40 s, compared with the measured in the experiment.

#### 4.2.3 Heat-up

After the blowdown phase and under the effects of a decreasing unexpected injection, calculated cladding temperatures for rewetted rods begins to departure from nucleate boiling in time very near to the observed. Several thermocouples - (such as 5G08 or 5I05) undergoes particular quench situations reaching the DNB point very late. Code, of course, cannot predict these special cases because simulated injection is defined to be symmetric.

DNB point is exceptionally well matched in rods 5G08, 5I11, 5E09 and 4G14, all of them starting from saturation.

Calculated mean heating rate, from DNB to reflood point, for 6 % fuel rods is about 3 K/s at peak power elevation, being 4-5 K/s a typical value for the initial rate. Calculated values are very near to measured data.

In those cases when cladding is in film boiling regime, the slope is nearly the same or lower, but starting at temperatures 200-300 K higher (see figure 26).

The effects of a second peak of injected water at 270 s, which provides about 12 Kg of coolant, are seen as a little decrease of 10-15 K in cladding temperatures. Actually, this was distributed in a very chaotic way, such as several thermocouples showed (including those in guide tubes).

Heat-up follows steadily from this point through the simultaneous injection from accumulators A and B at 345 s.

Table 4.2 resumes the maximum cladding temperatures reached in the TRAC simulated rods at peak power elevation (27 inch). Marked values correspond to those rods which remain in film boiling regime during the whole transient. Fig 4.23 to 4.25 show the behaviour of those instrumented 6 % fuel rods which ruptured, compared with the corresponding TRAC calculations. In the case of 5G11, the agreement is exceptionally good, because of heat-up starts from saturation.

For peripheral rods (Fig 4.26), when the simulated rod has descended from film boiling regime, the fitting in the final heat-up phase is sucessful.

Thermocouples cited above, show succesful fits between calculations and measured data along the final heat-up phase. In the case of 5G08 (4 % enriched fuel rod), predicted cladding temperature is lower than the registered during the final heat-up phase, so it's possible that the actual temperature in central element during the rod rupture period were slightly higher than the calculated one. This comment is derived from only one 4 % enriched rod and must be seen as an hypothesis.

#### 4.2.4. T/H conditions during rod rupture period

Results from TRAC shows that all the hydraulic variables were nearly constant during the period in which, eight 6 % fuel rods ruptured (325-345 s).

- A small quantity of water from accumulator B line was falling over the element during this phase, as some detectors showed (see Fig 3.8 for TE-5UP-004). We are feeding the system with 0.5 Kg/s of coolant in this period, which flows down among the rods, vaporizing partly.

Tables 4.3 to 4.4 resume the mean (ring averaged) vapor and liquid behaviour during the rod rupture period, when eight 6 % fuel rods failed. Fig 4.27 shows the flow patterns (also during rupture period, when 8 - 6 % fuel rods failed. Figure averaged per ring) through the vessel.

- One may see two possible and alternative paths for the generated fission products, both starting at peak power elevation (where there is a stagnation point) through BLHL:

- Ascending from this point to the upper plenum
- Descending from peak power elevation to the lower plenum and then, ascending through the peripheral bundles in ring 3.

Vapor in the upper plenum has a very asymmetric behaviour (Fig 4.28 and 4.29), which may be explained by the presence of the hot legs. Those cells near to the cold legs have near identical values.

In second ring (inner parts of peripheral bundles), vapor is nearly stagnant during this period.

#### 4.2.5. Combined injection

From 345 s on, both accumulators inject coolant for system recovery. Injection caused dramatic oscillations in all plant variables, except on cladding temperatures which drop steadily to the moment when the MSFBT is reached and the film is destroyed. Quenching is nearly instantaneous but happens with a great delay respect to the measured final quench times. Enriched fuel rods (6 %) doesn't have completed the rewetting phase at 400 s in TRAC calculations.

Some other characteristics of the reflood period are:

- Core liquid fraction rise from 0. to 0.8 at a rate of 4 Kg/s (see figure 4.30).
- Vapor temperature in the core, decreases at a rate of about 6.5 K/s near the peak power elevation.
- Cooling rates for cladding temperatures are about:
  - 7 K/s for 4 % enriched fuel rods in central element.
  - 10 K/s for 6 % enriched fuel rods in central element.
  - 10 K/s for 4 % enriched fuel rods in peripheral elements.

**TABLE 4.1. Plant calculated steady state**

	Measured	TRAC/PF1
Hot leg pressure (Mpa)	14.77 + 0.07	14.87
Hot leg temperature (K)	577.6 + 0.8	581.6
Cold leg temperature (K)	563.2 + 1.1	567.2
Mass flow in loop (Kg/s)	486.7 + 2.5	487.5
Steam generator secondary pressure (Mpa)	6.41 + 0.08	6.77
Pressurizer pressure (Mpa)	14.73 + 0.11	14.85
Pressurizer temperature (K)	616.2 + 5.8	614.3
Broken loop cold leg temperature (K)	561.4 + 1.5	562.0
Broken loop hot leg temperature (K)	564.8 + 1.8	565.0

**TABLE 4.2. Maximum cladding temperatures during rod rupture phase**

	4% Rod	T(K)	6% Rod	T(K)
Ring 1	1	1025	13	1254*
	2	1018	14	1238*
	3	1018	15	1167
	4	1048	16	1192
Ring 2	5	1076*		
	6	1173*		
	7	1165*		
	8	1176*		
Ring 3	10	950		
	11	933		
	12	940		
	13	952		

TABLE 4.3. Vapor axial velocity (m/s) in central ring during rod rupture phase

LEVEL	CELL			
	1	2	3	4
4	-0.75	-0.61	-0.71	-1.36
5	-0.41	-0.30	-0.39	-0.71
6	0.03	0.01	0.03	0.02
7	0.73	0.52	0.70	1.33
8	1.08	0.89	1.06	1.35

TABLE 4.4. Liquid axial velocity (m/s) in central ring during rod rupture phase

LEVEL	CELL			
	1	2	3	4
4	-3.60	-3.60	-3.60	-3.60
5	-3.51	-3.53	-3.51	-3.50
6	-3.45	-3.47	-3.45	-3.40
7	-3.35	-3.39	-3.35	-3.28
8	-3.26	-3.29	-3.26	-3.22

TABLE 4.5. Vapor temperature (K) in central ring during rod rupture phase

LEVEL	CELL			
	1	2	3	4
4	502	498	499	548
5	628	621	625	666
6	640	636	637	660
7	598	596	597	617
8	498	491	497	522

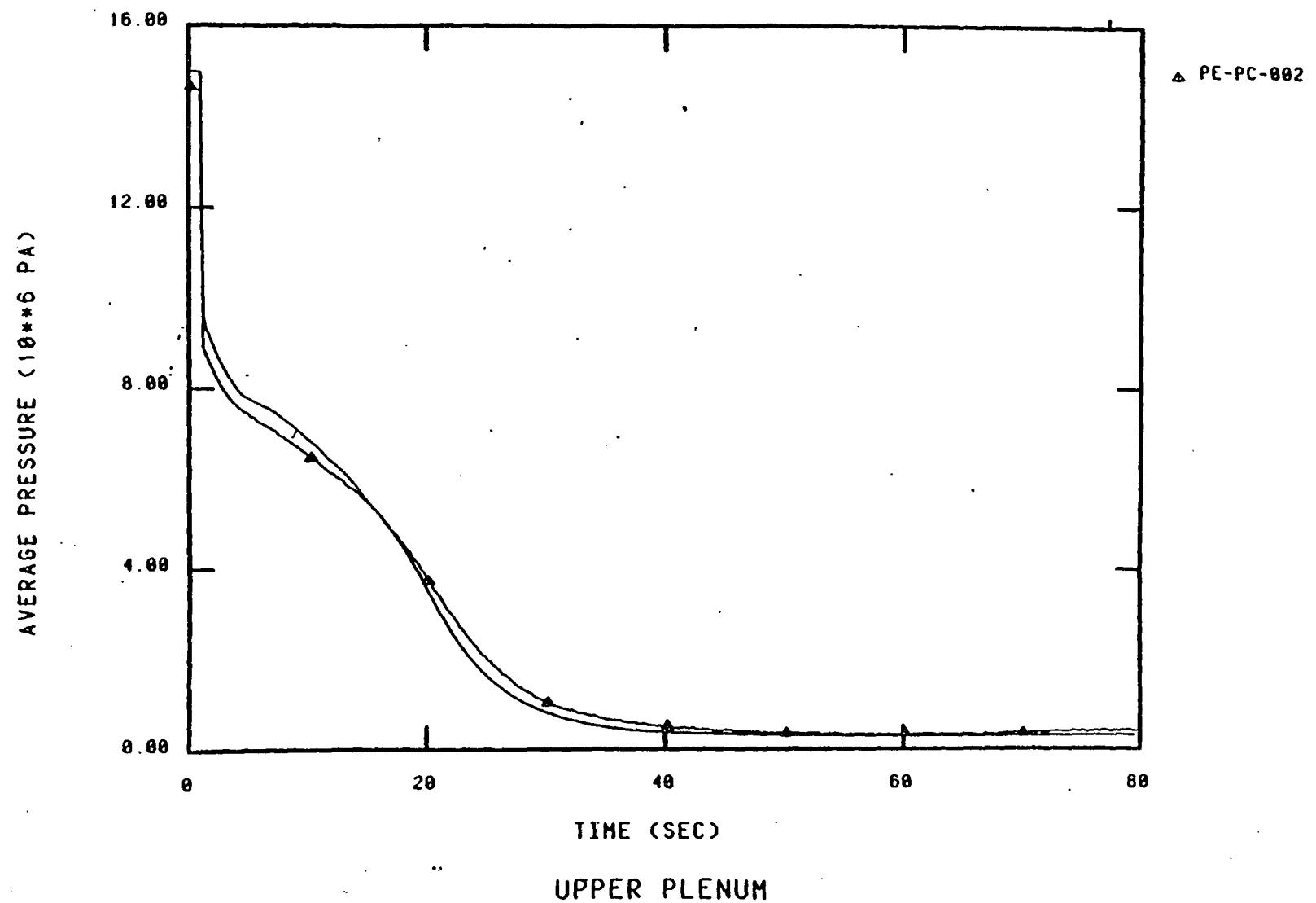


Figure 4.1. Upper plenum pressure

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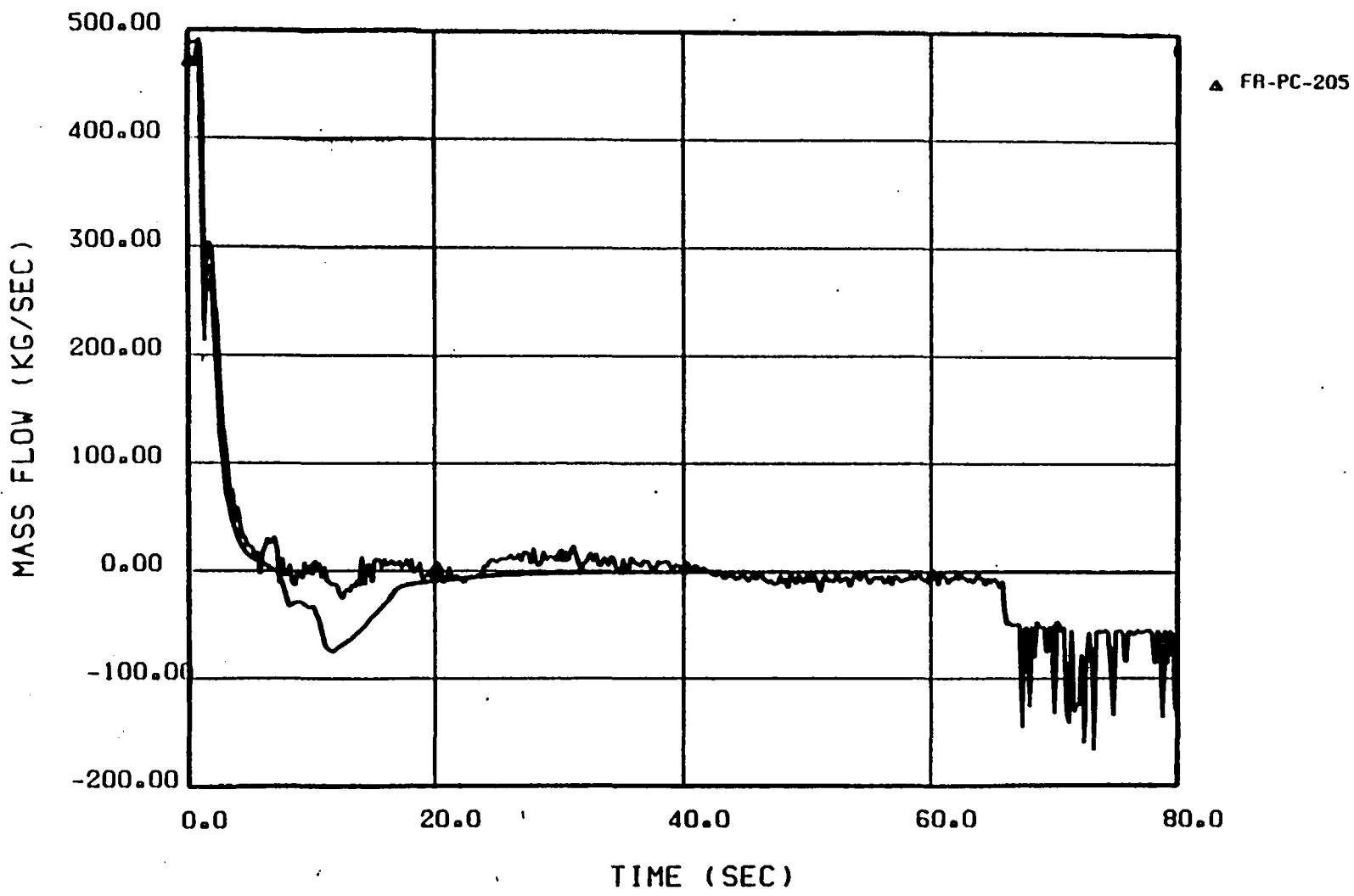
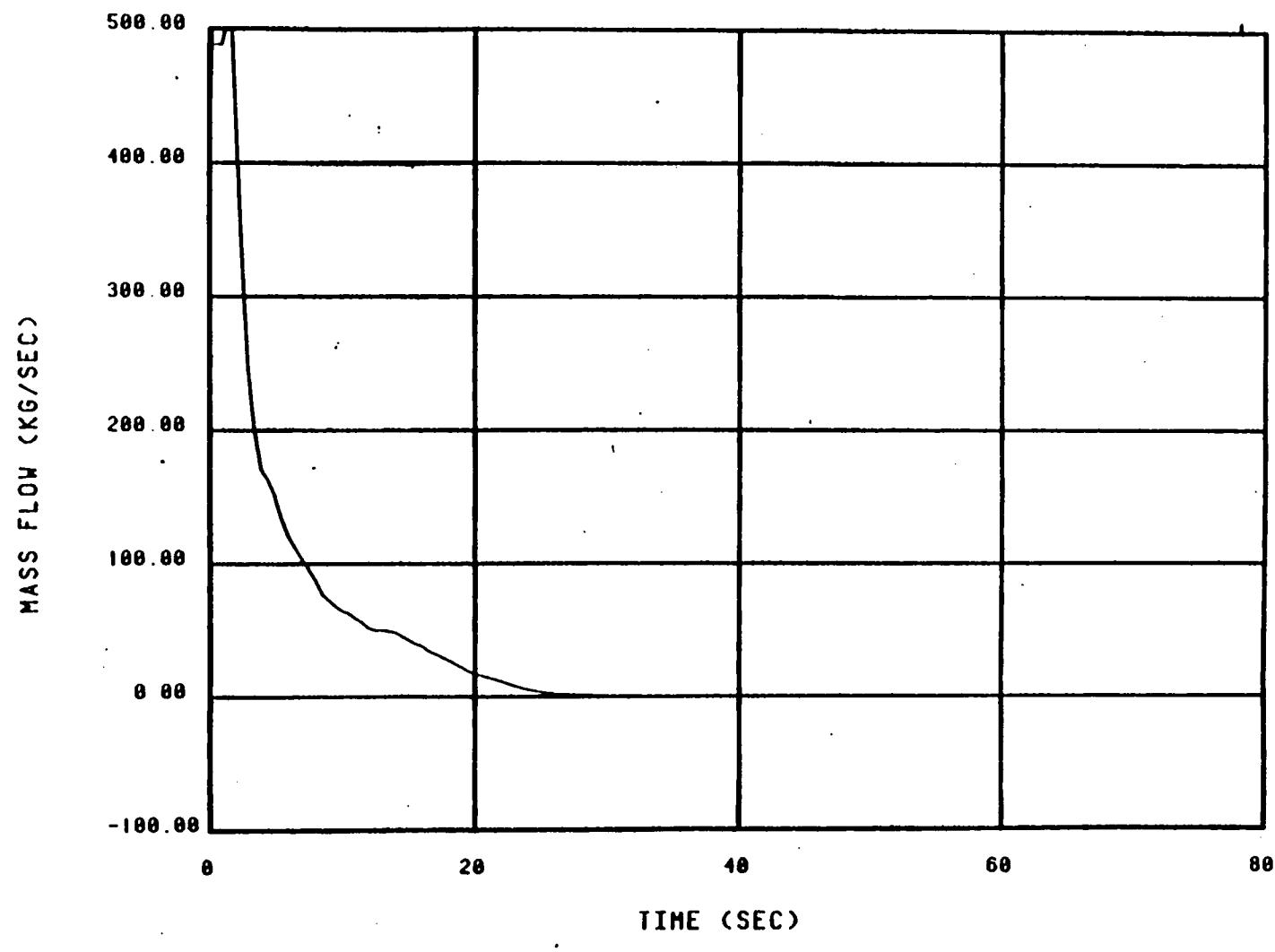


Figure 4.2. Intact loop hot leg (cell 3) mass flow



ILCL - CELL 2

Figure 4.3. Intact loop cold leg (cell 2) mass flow

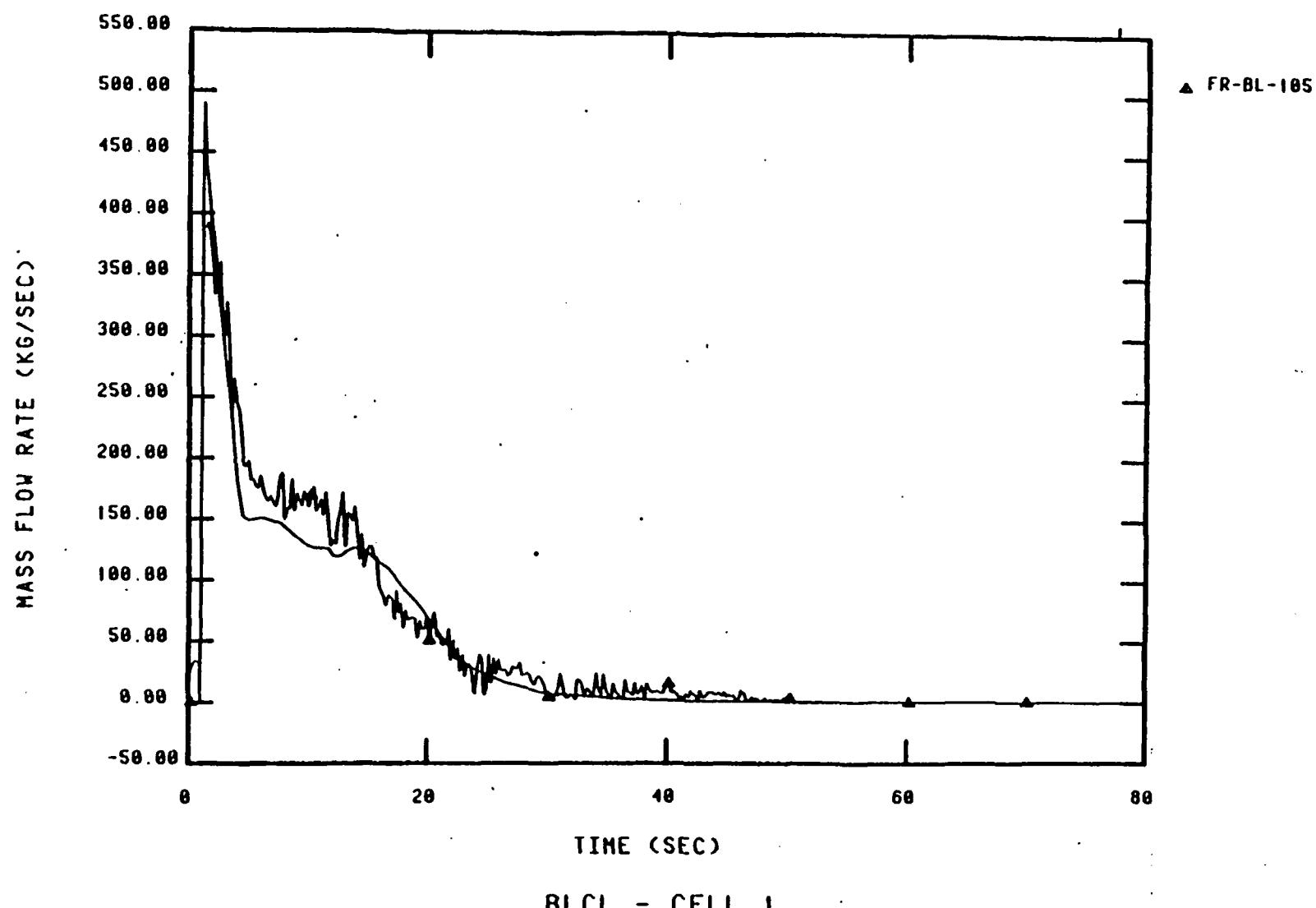


Figure 4.4. Broken loop cold leg (cell 1) mass flow

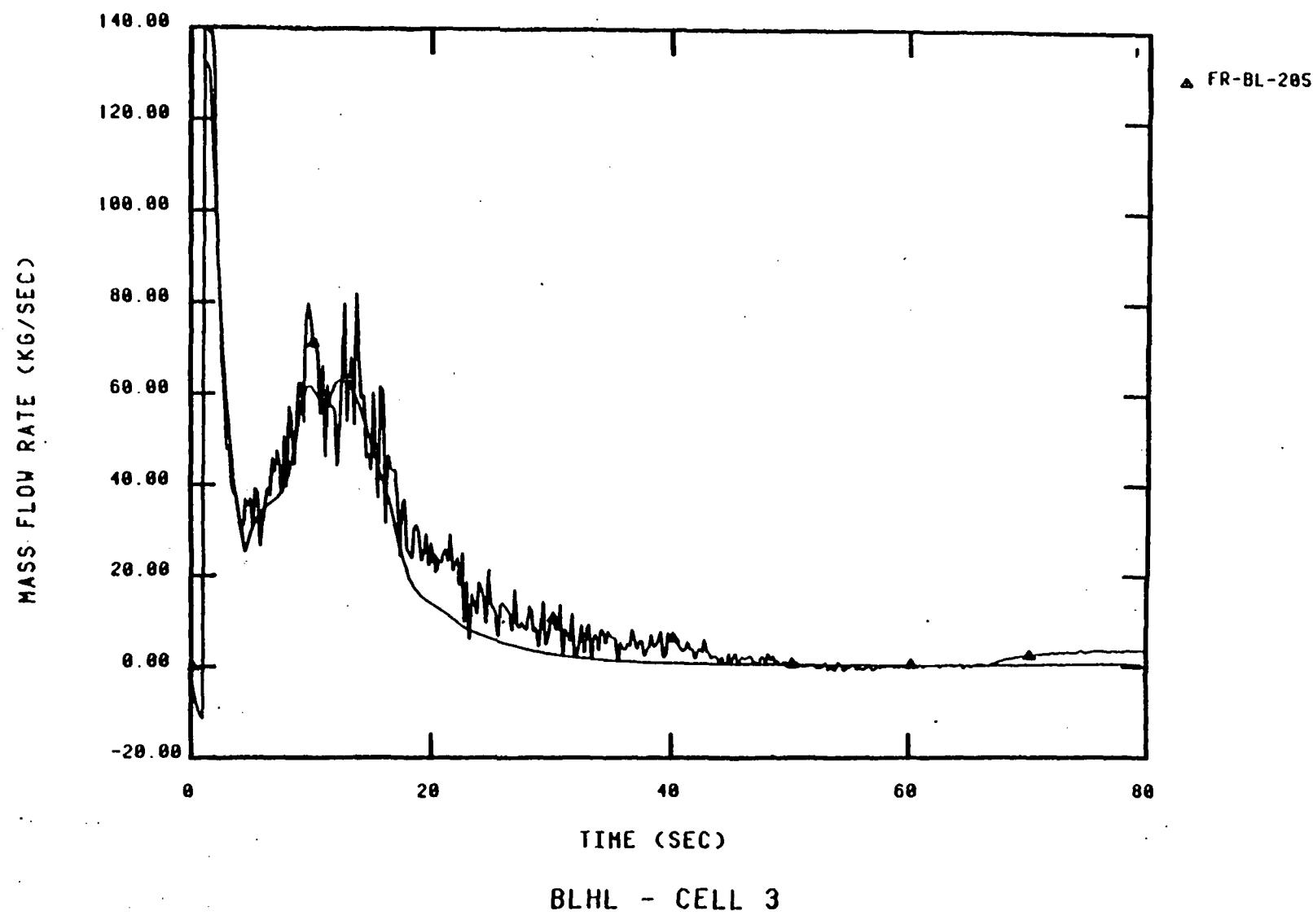


Figure 4.5. Broken loop hot leg (cell 3) mass flow

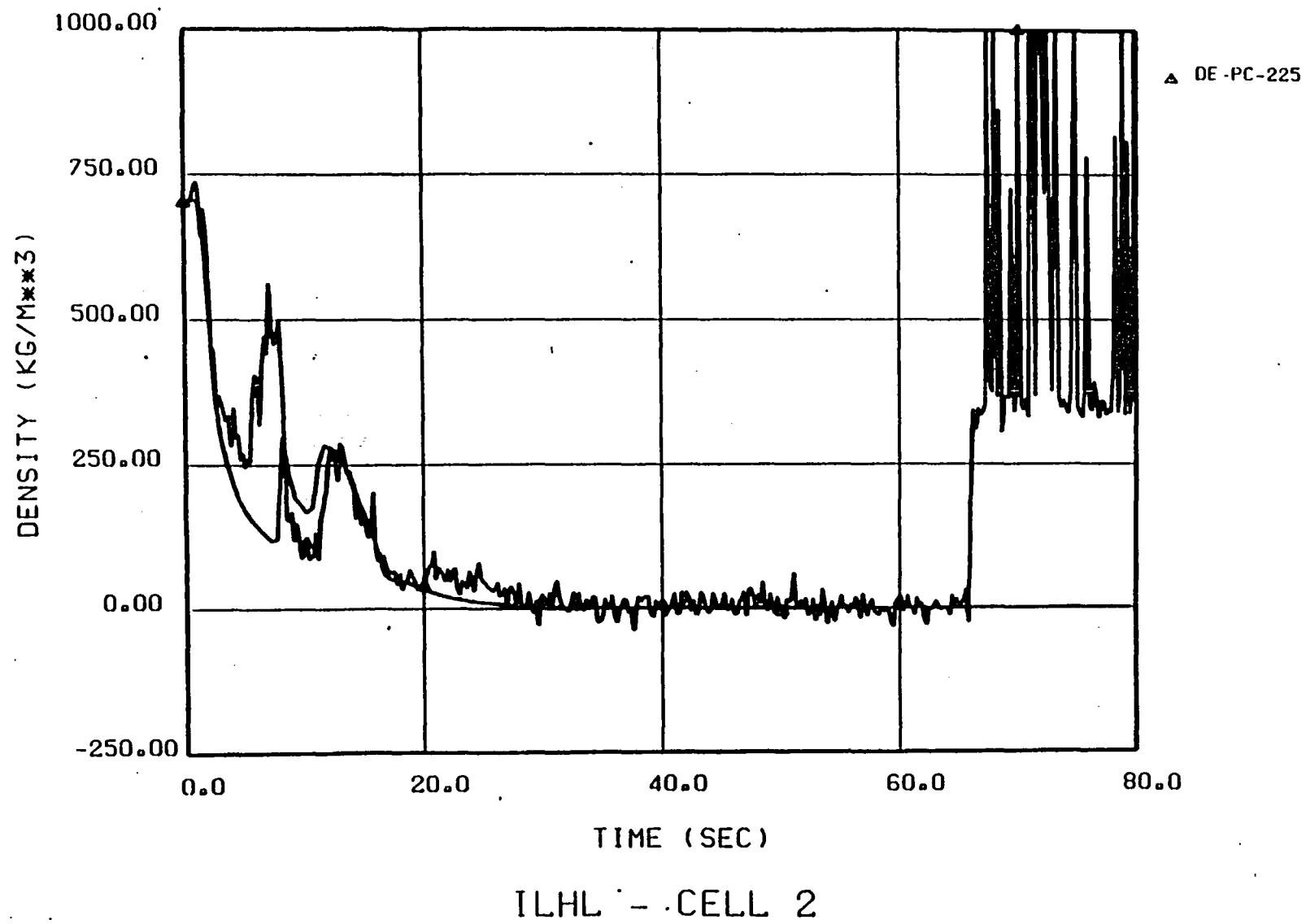
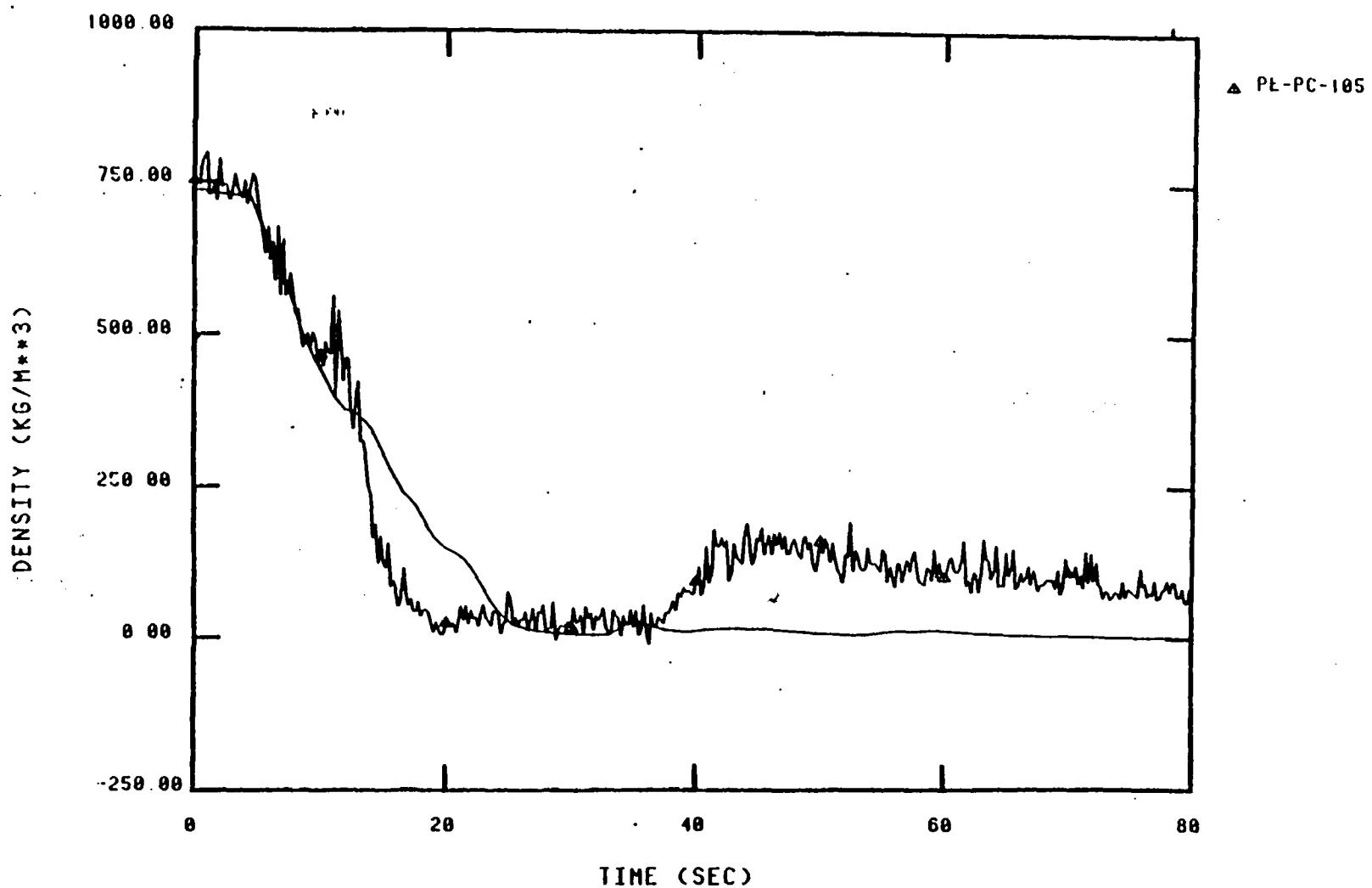


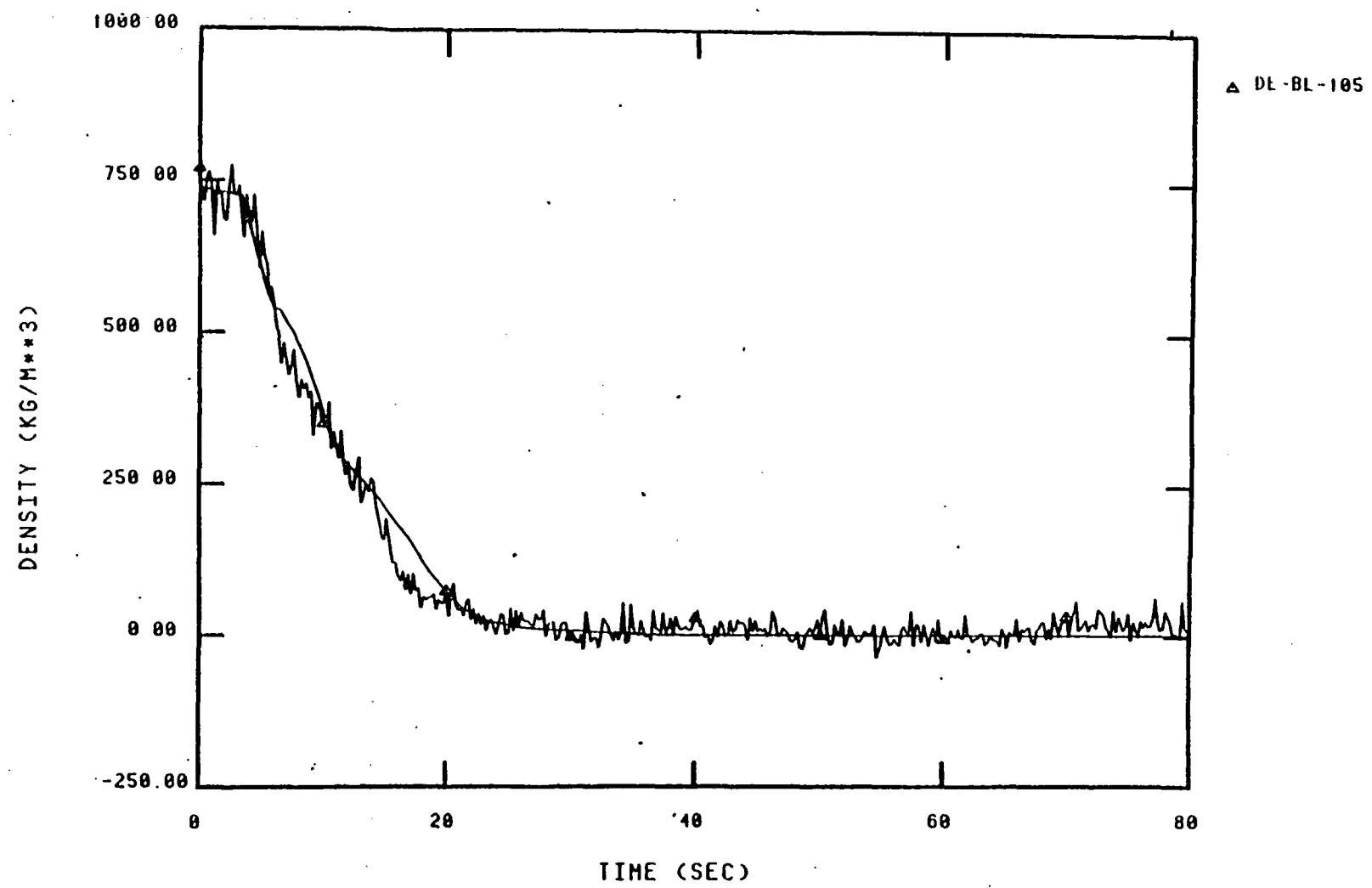
Figure 4.6. Intact loop hot leg (cell 2) density



ILCL - CELL 2

Figure 4.7. Intact loop cold leg (cell 2) density

65



FIGURA

Figure 4.8. Broken loop cold leg (cell 1) density

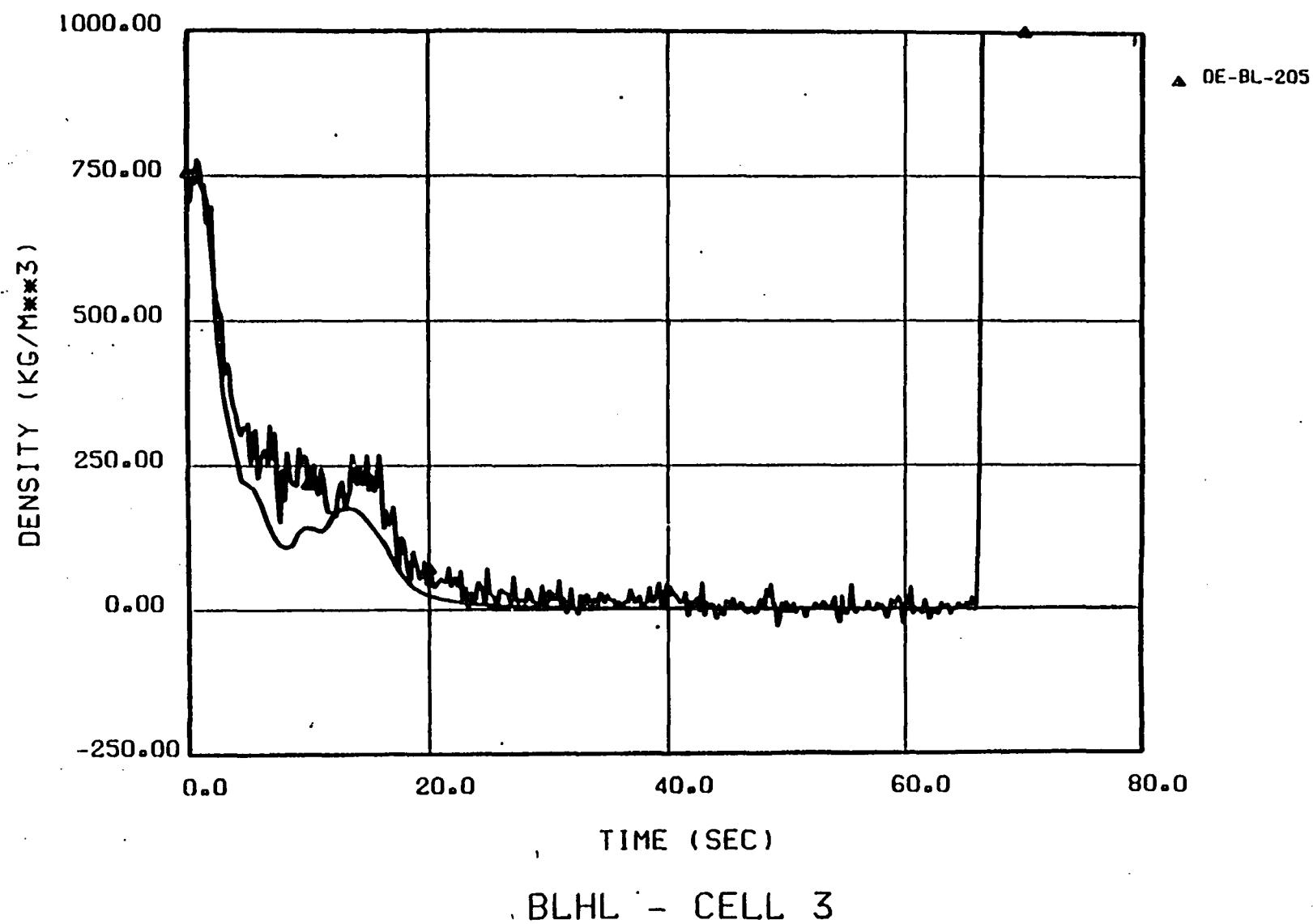


Figure 4.9. Broken loop hot leg (cell 3) density

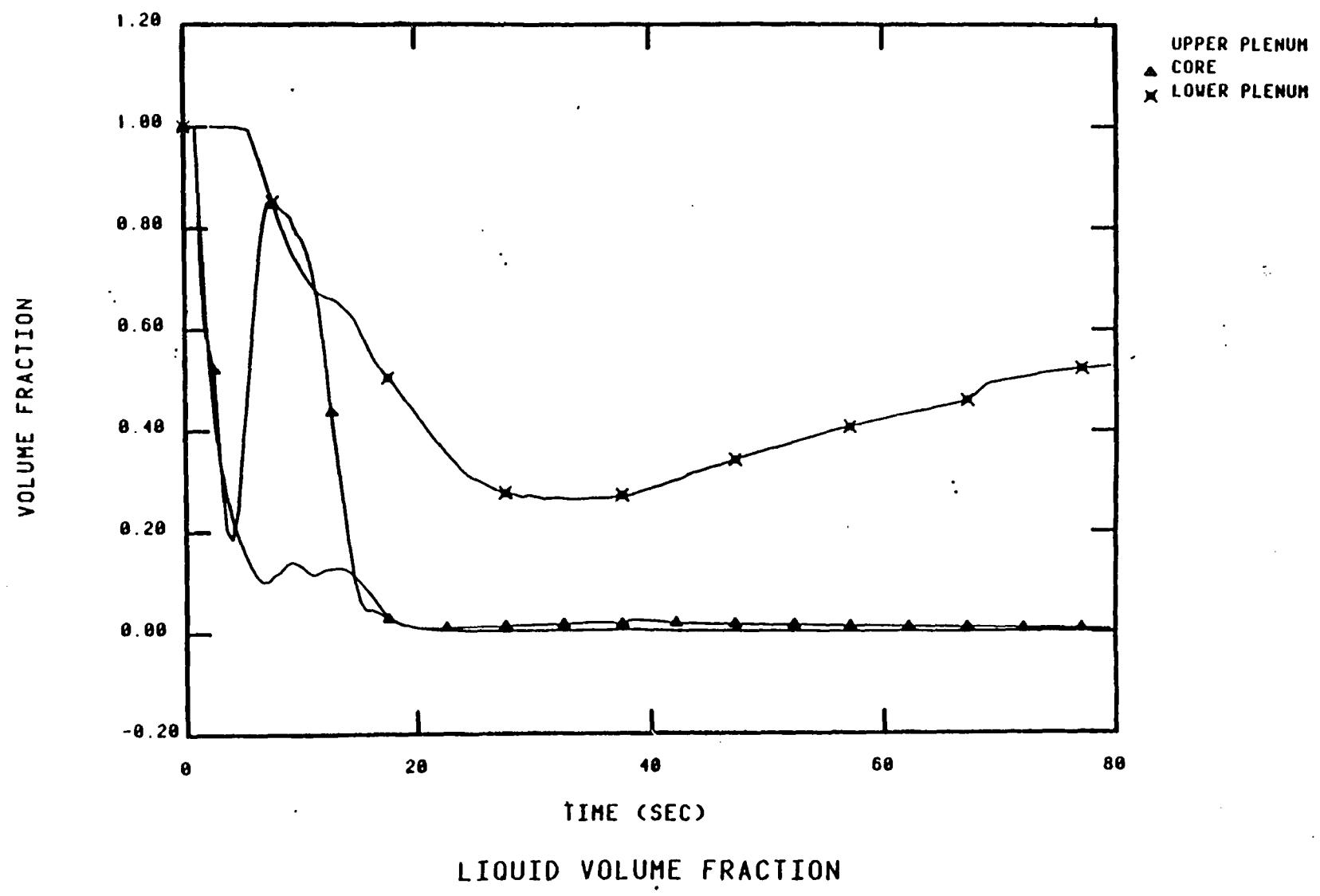


Figure 4.10. Vessel liquid fraction

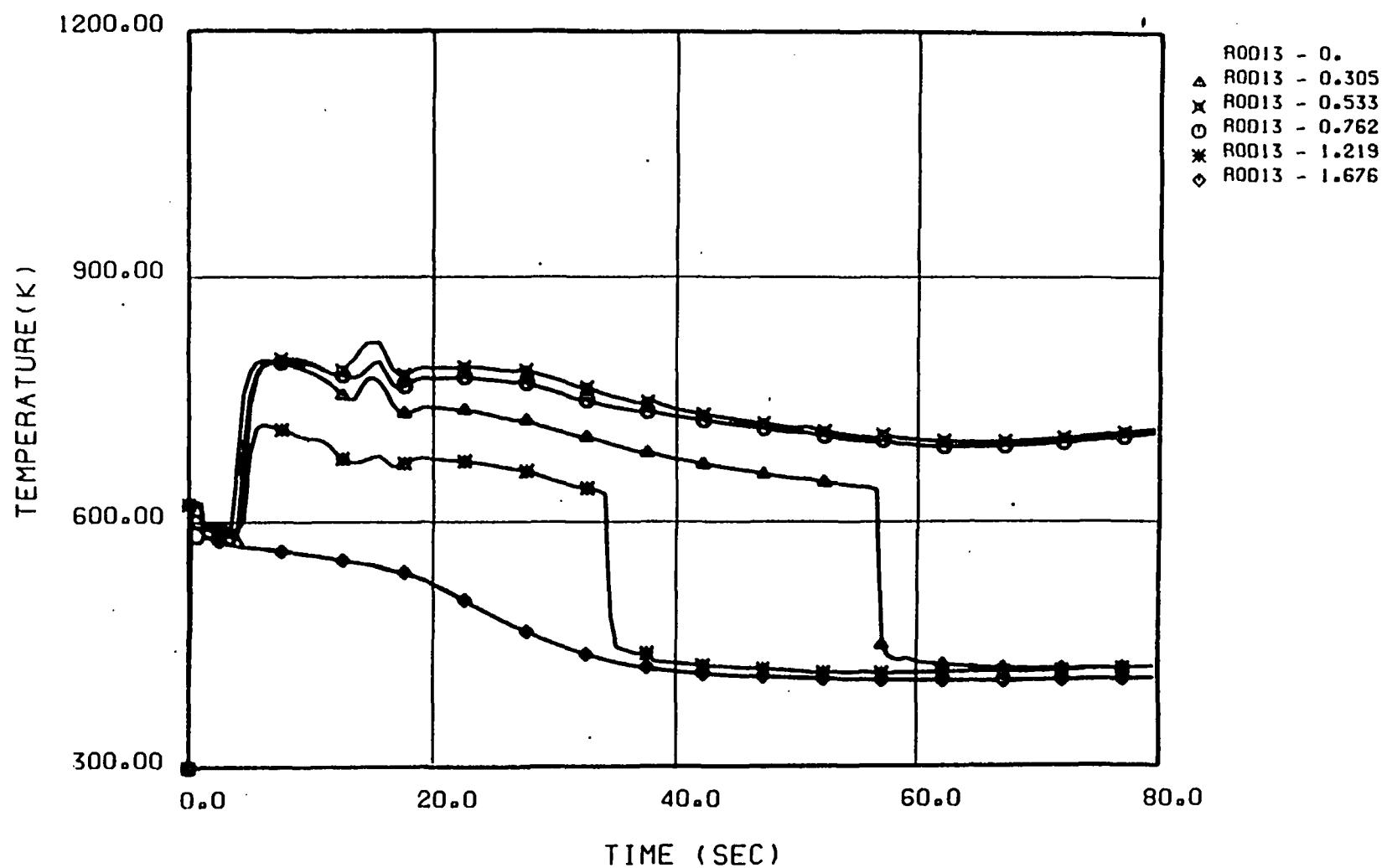


Figure 4.11. Simulated 6 % rod 13 at several heights during blowdown phase

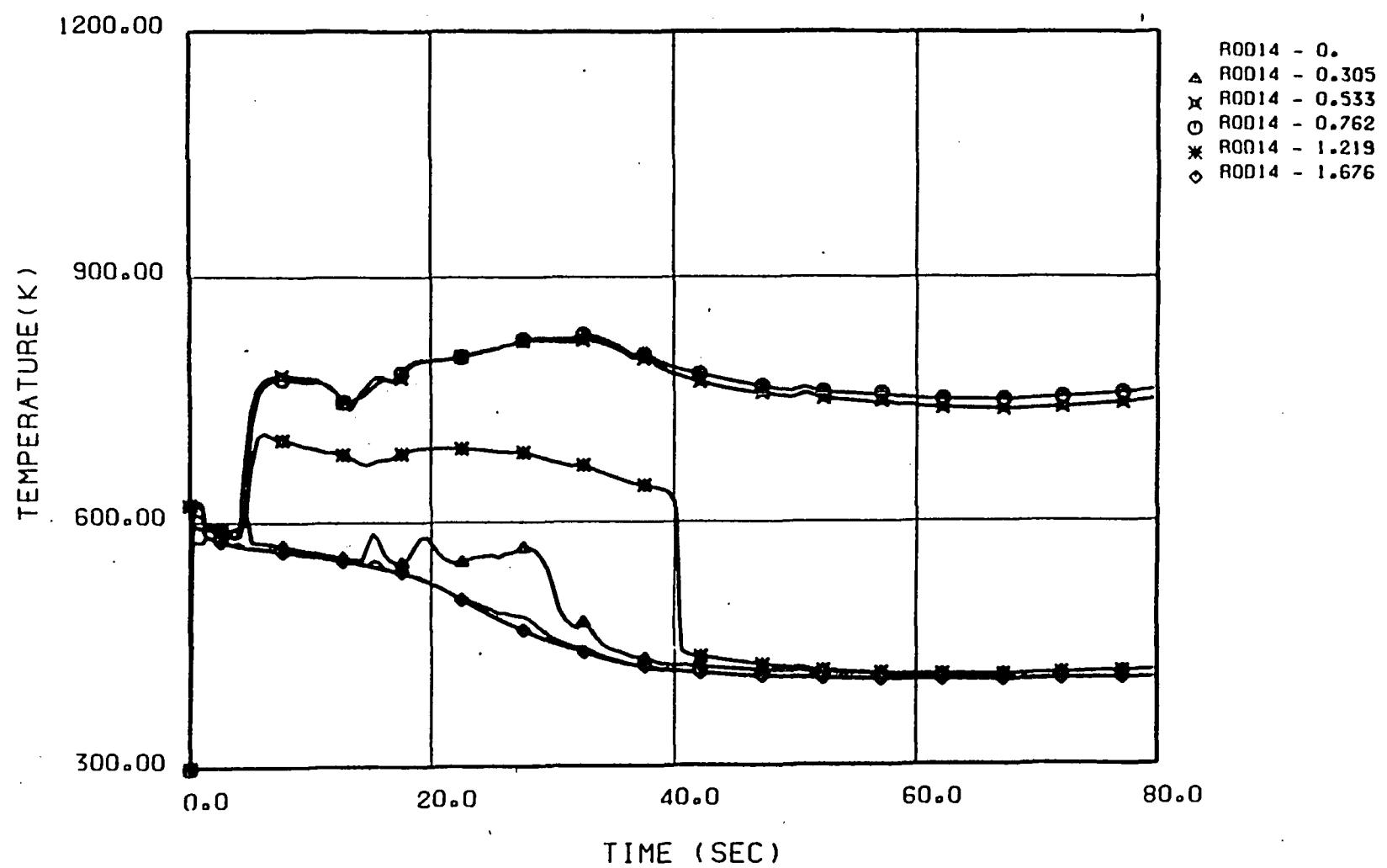


Figure 4.12. Simulated 6 % rod 14 at several heights during blowdown phase

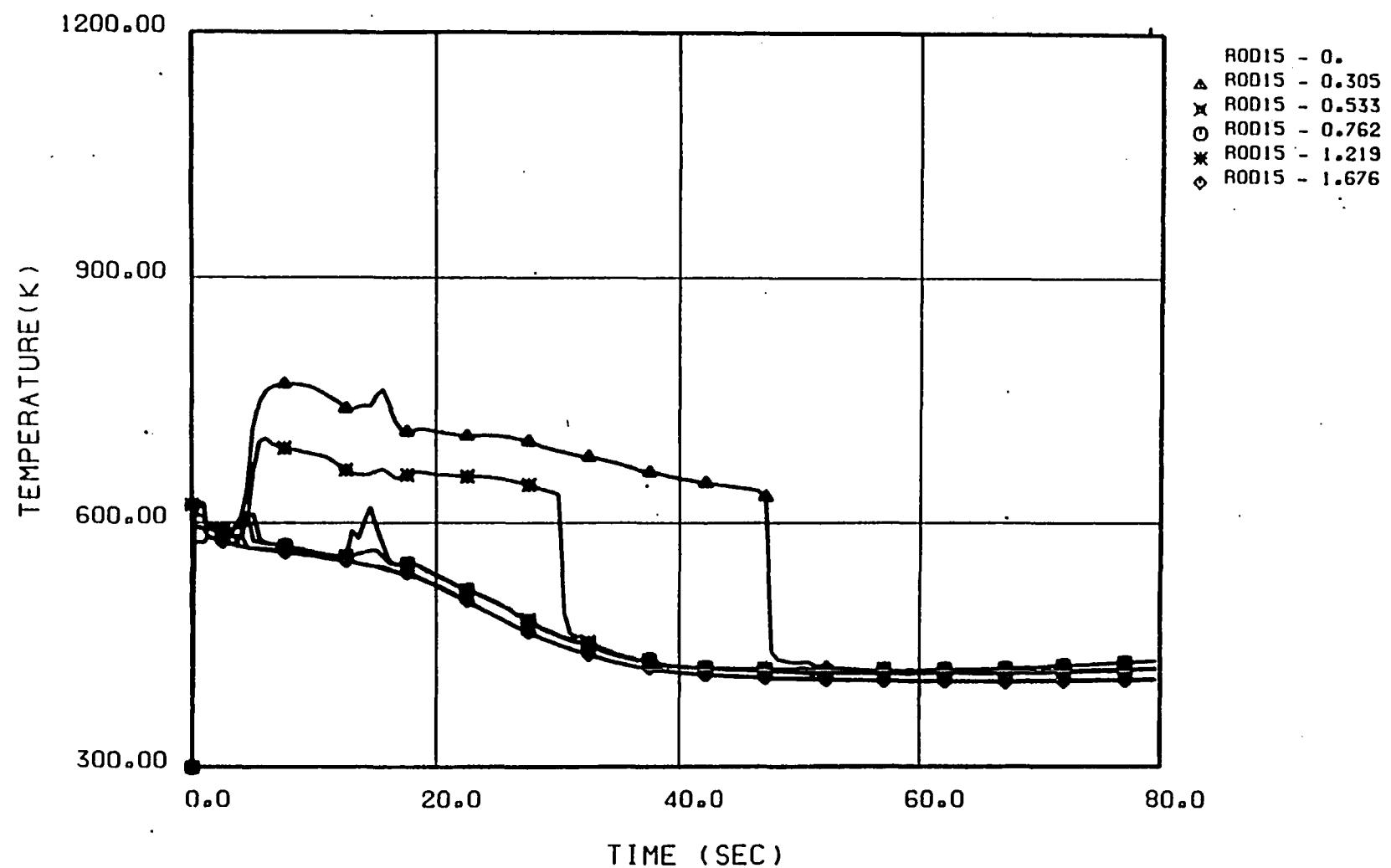


Figure 4.13. Simulated 6 % rod 15 at several heights during blowdown phase

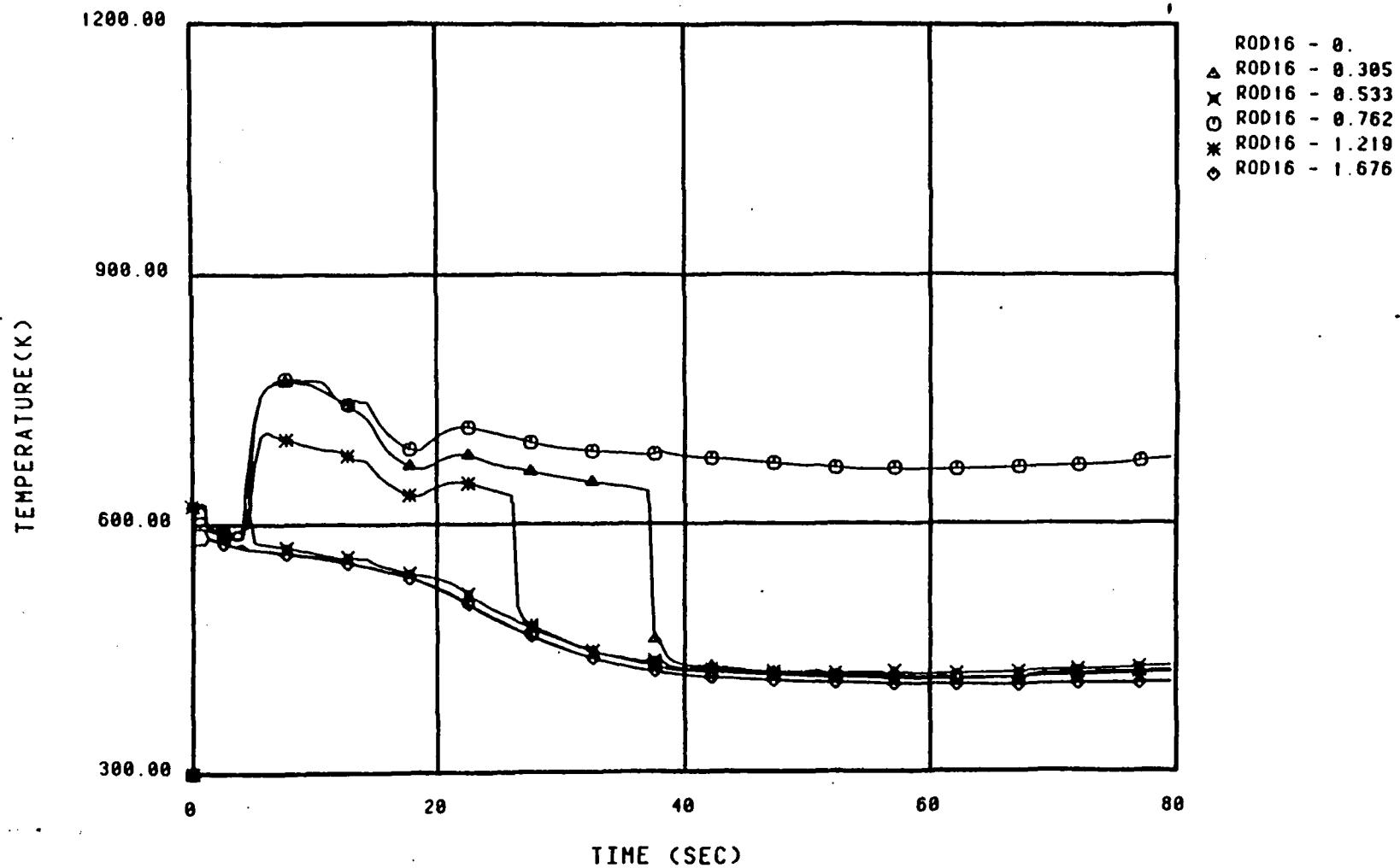


Figure 4.14. Simulated 6 % rod 16 at several heights during blowdown phase

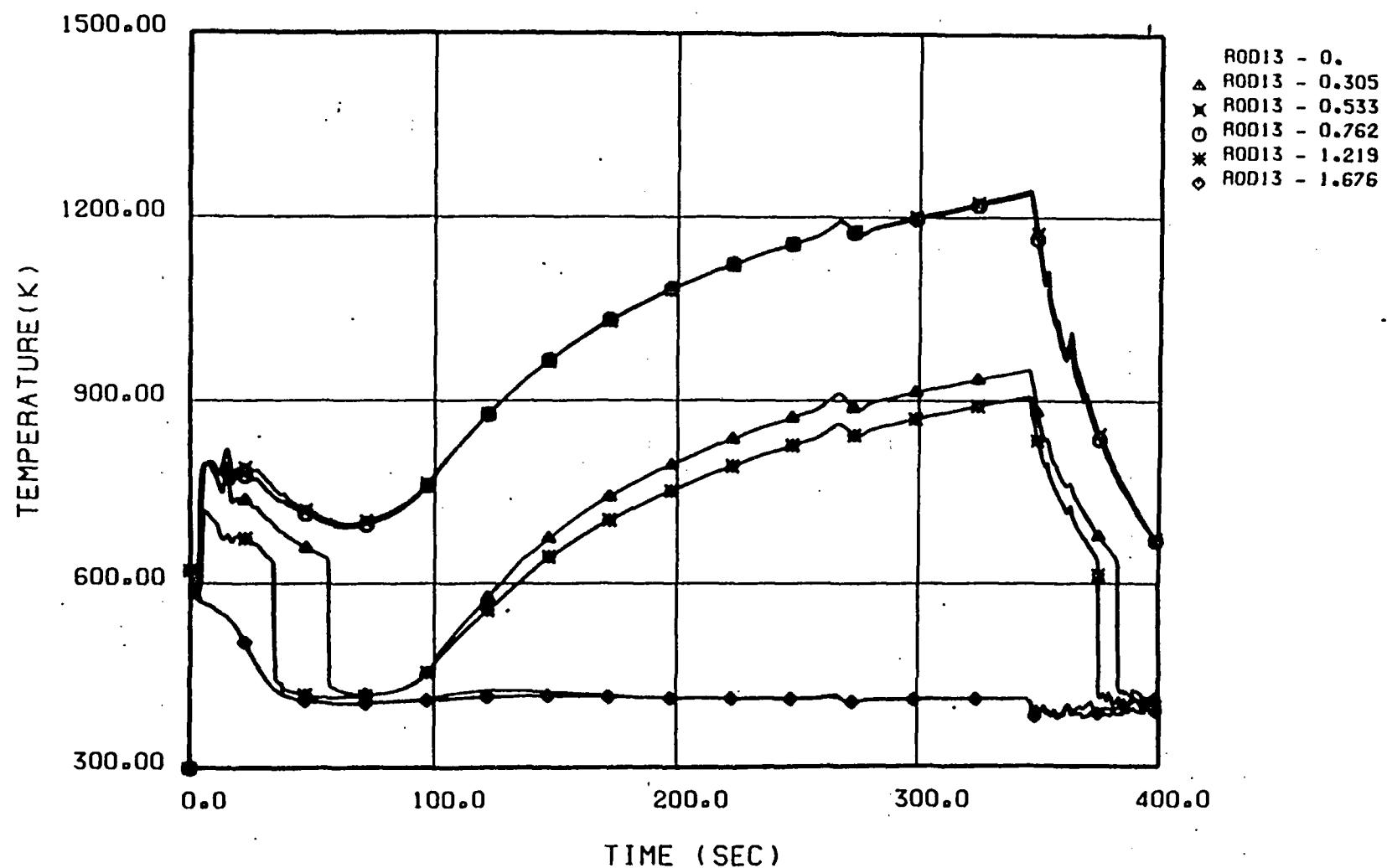


Figure 4.15. Simulated 6 % rod 13 at several heights during the whole transient

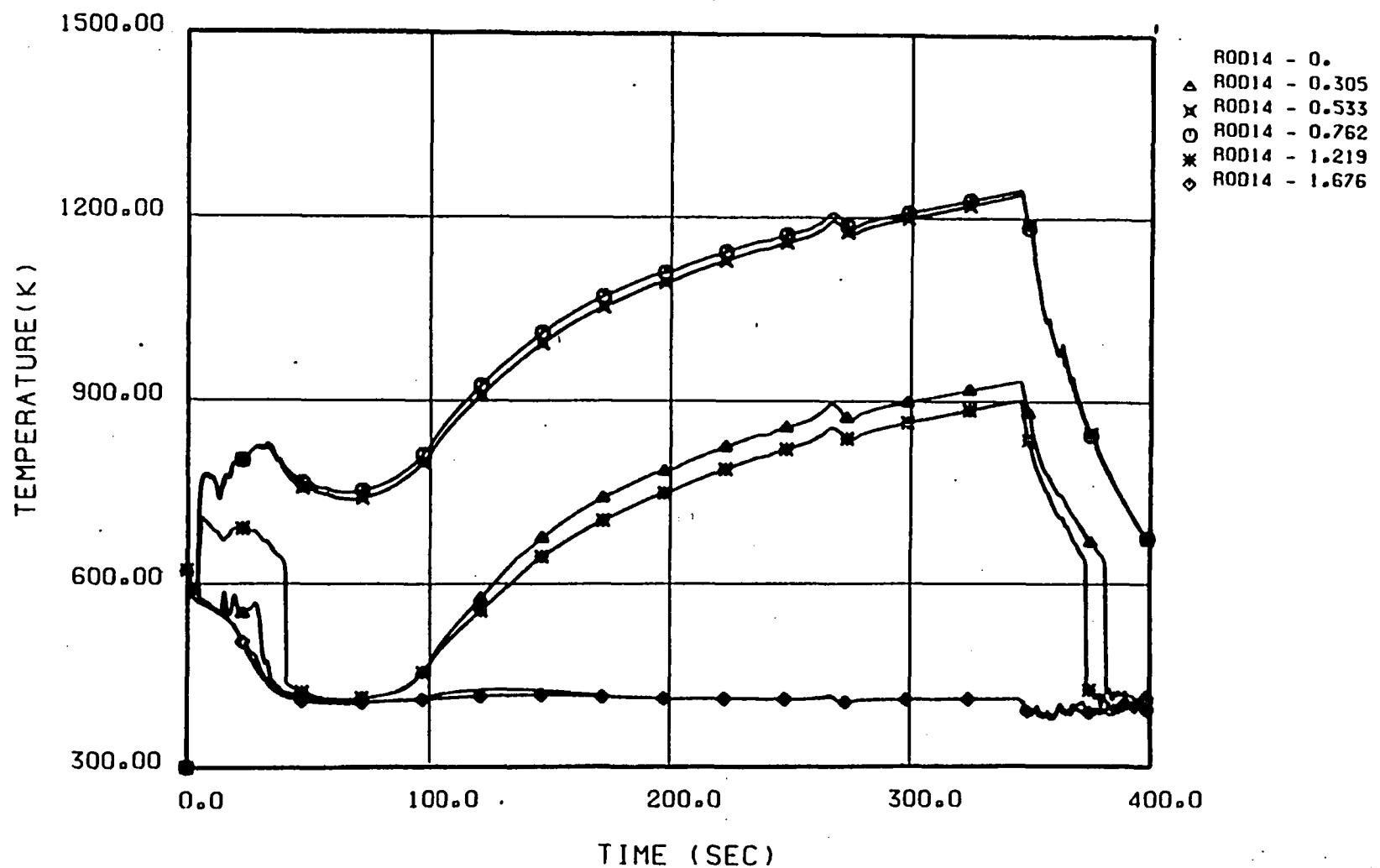


Figure 4.16. Simulated 6 x rod 14 at several heights during the whole transient

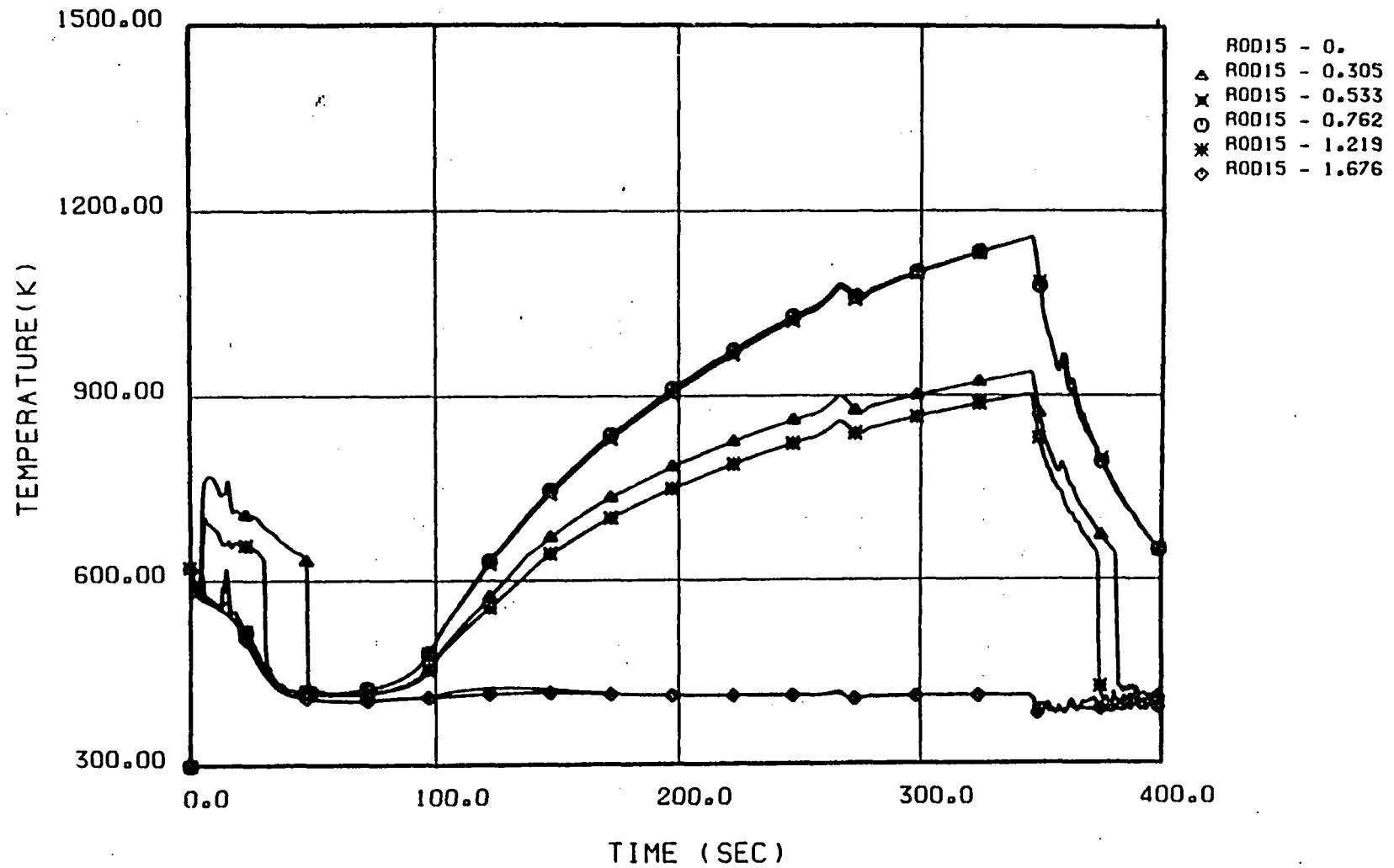


Figure 4.17. Simulated 6 % rod 15 at several heights during the whole transient

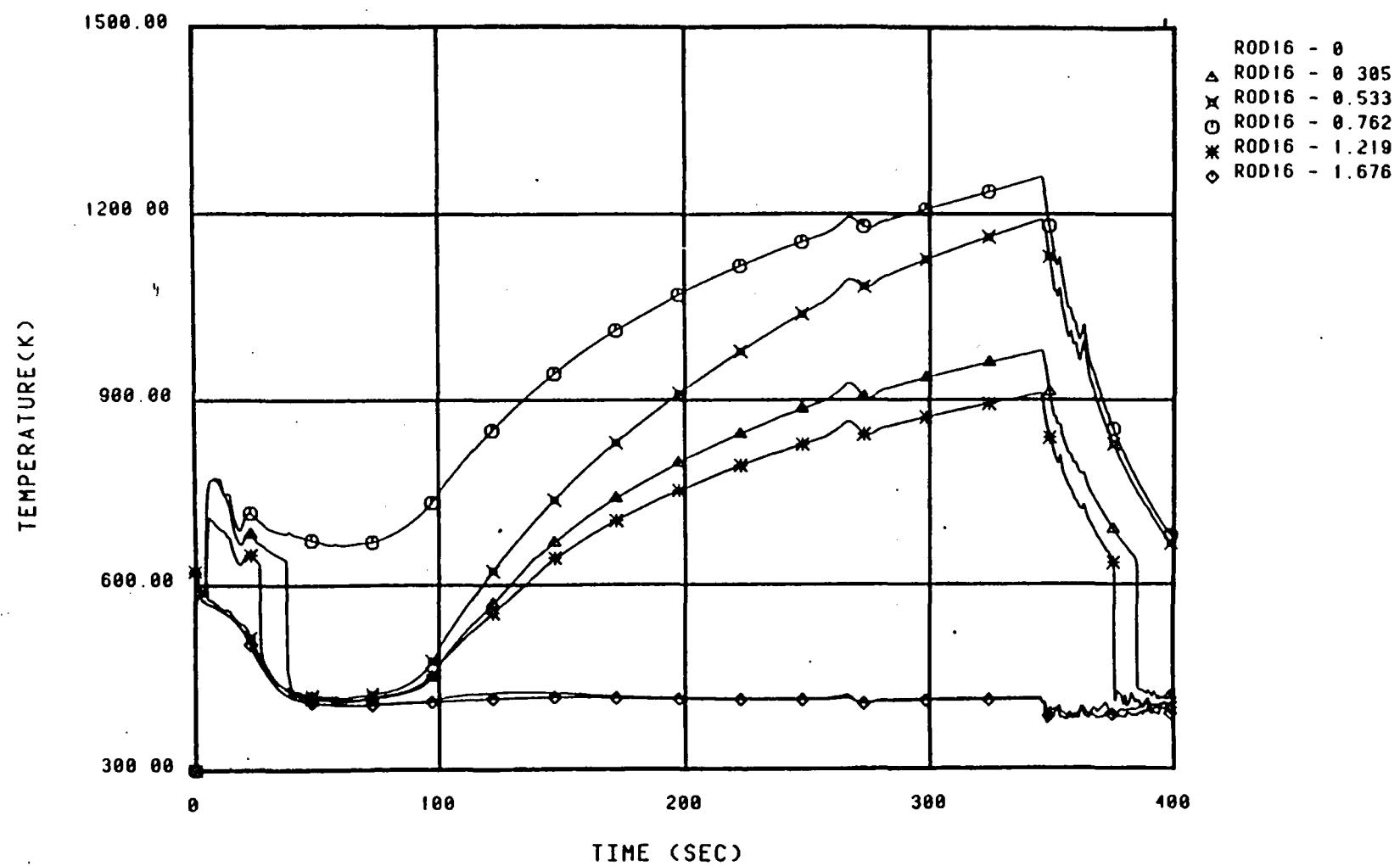


Figure 4.18. Simulated 6 % rod 16 at several heights during the whole transient

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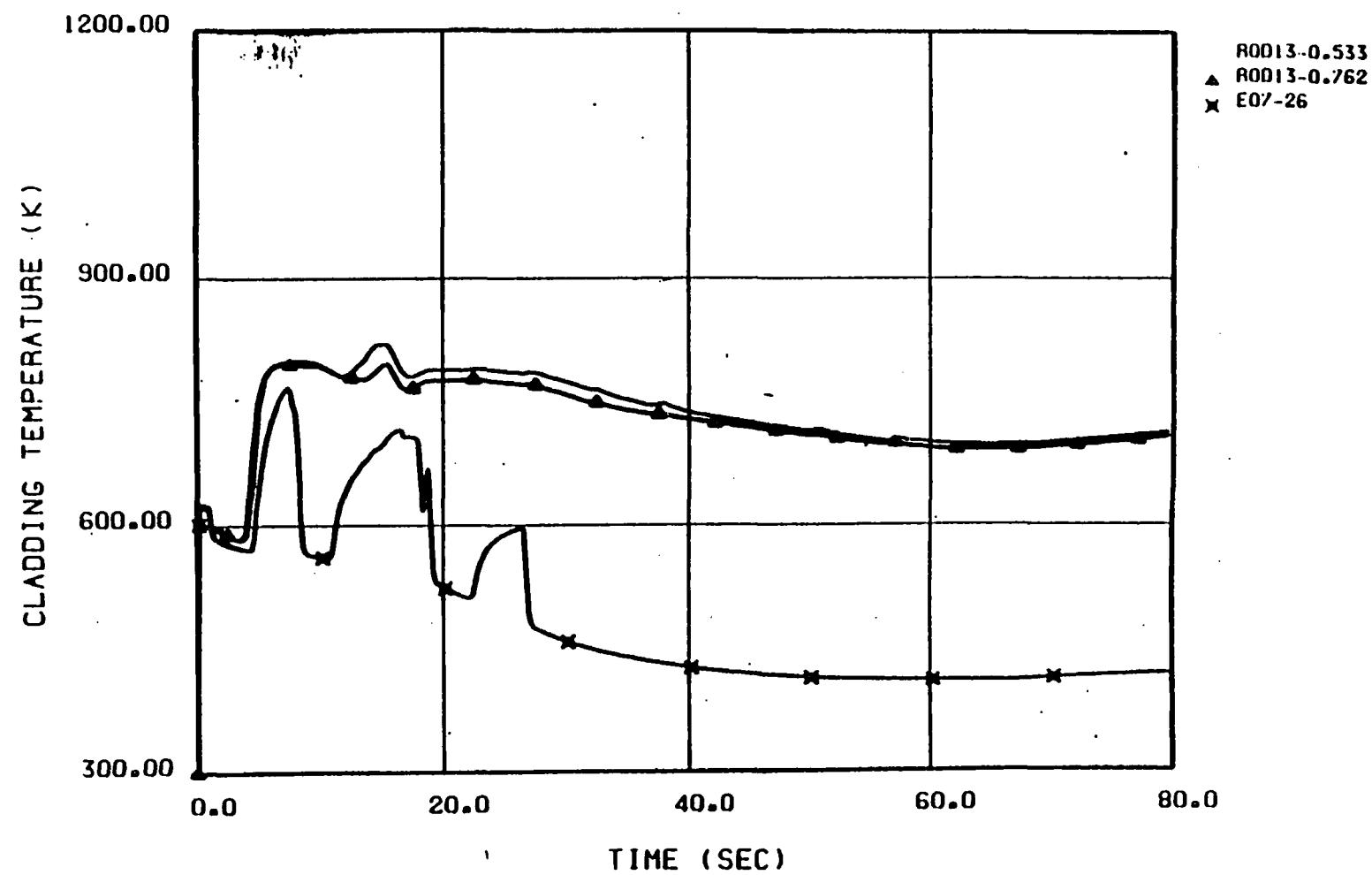


Figure 4.19. Comparison with thermocouple 5E07 (blowdown)

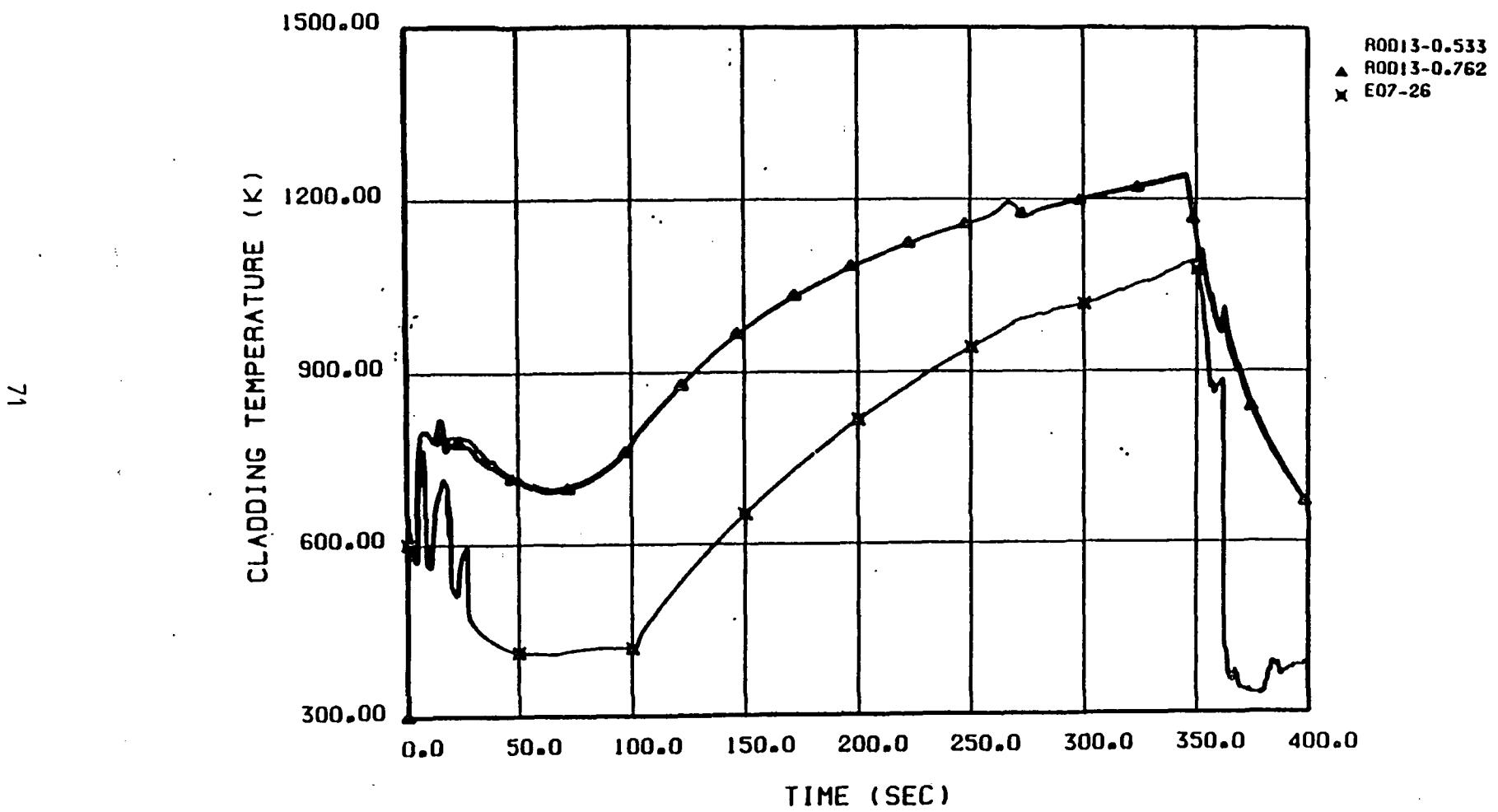


Figure 4.20. Comparison with thermocouple 5E07 (transient)

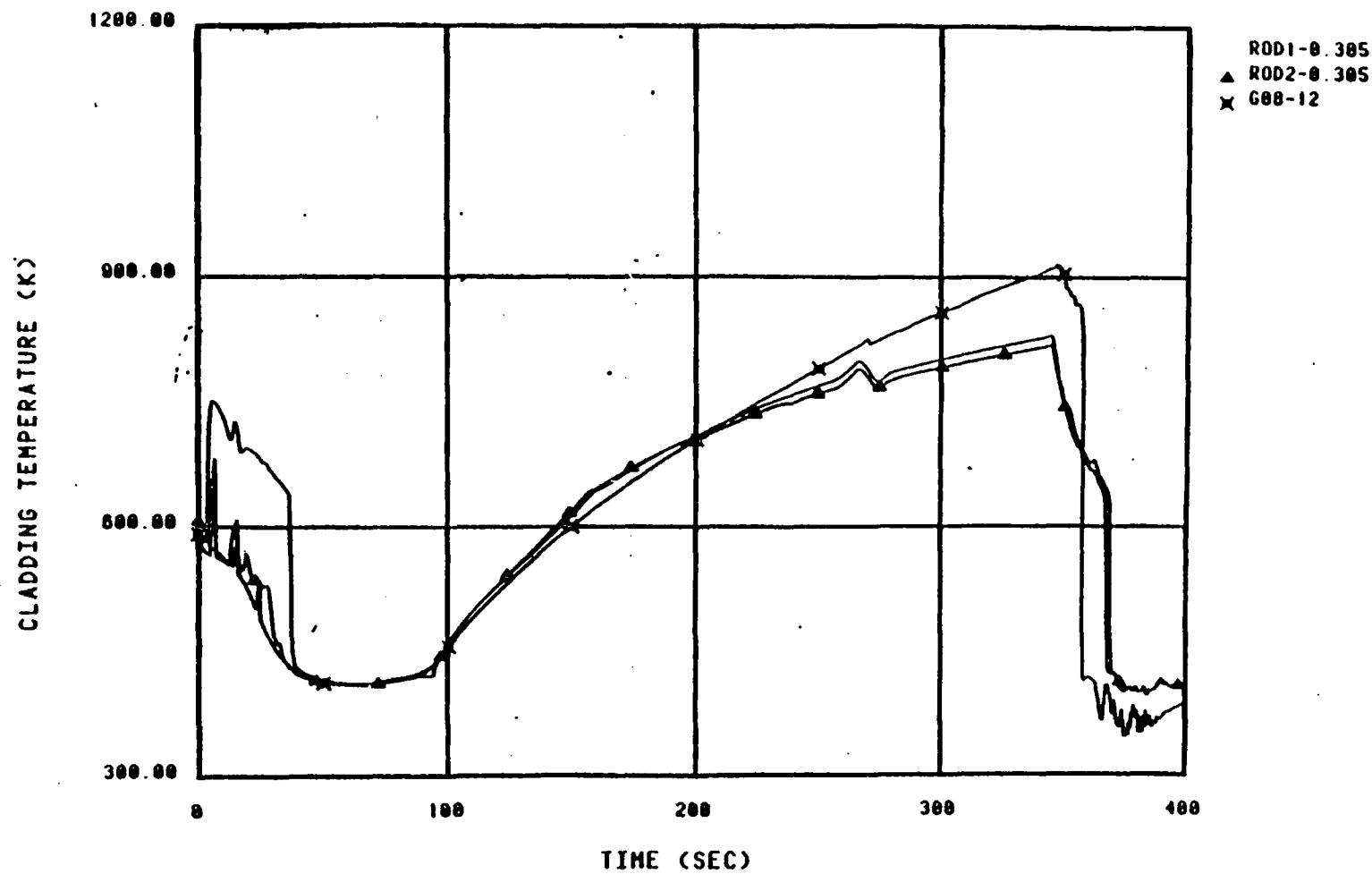


Figure 4.21. Cladding temperatures calculated for 5G08  
(4 % fuel rod in central element)

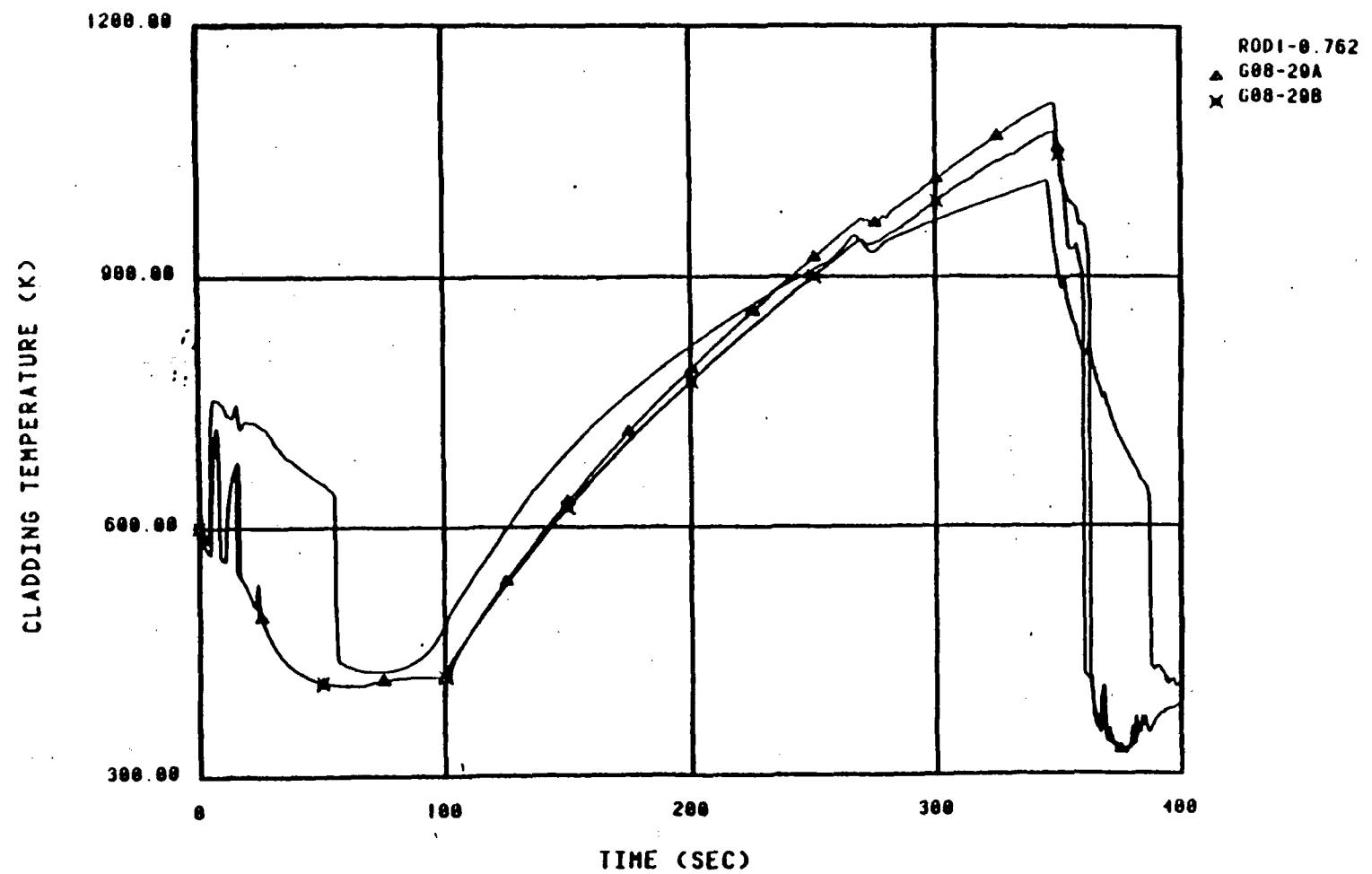


Figure 4.22. Cladding temperatures calculated for 5G08  
(4 % fuel rod in central element)

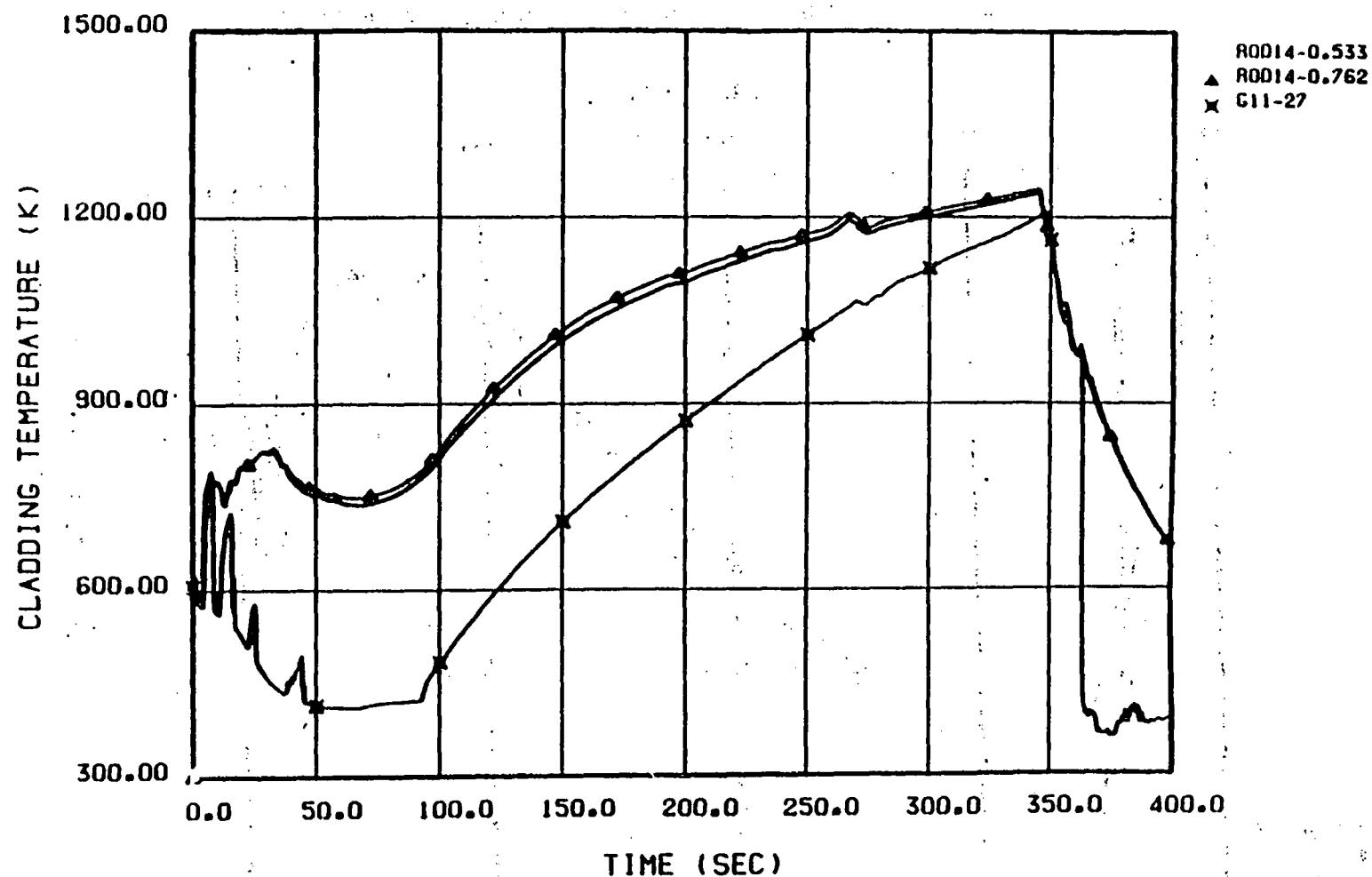


Figure 4.23. Cladding temperatures calculated for 5G11  
(6 % ruptured fuel rod)

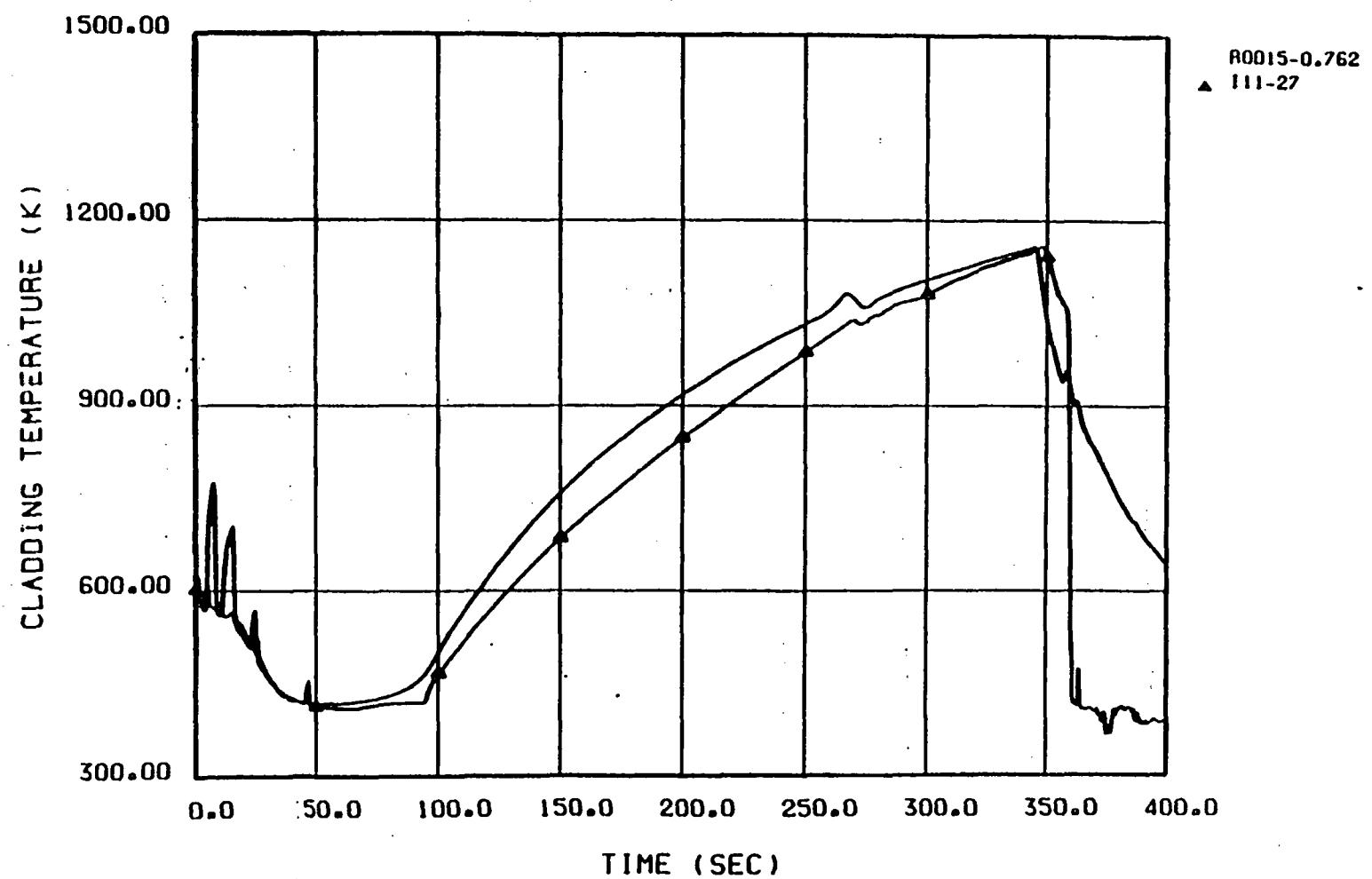


Figure 4.24. Cladding temperatures calculated for 5111  
(6 % ruptured fuel rod)

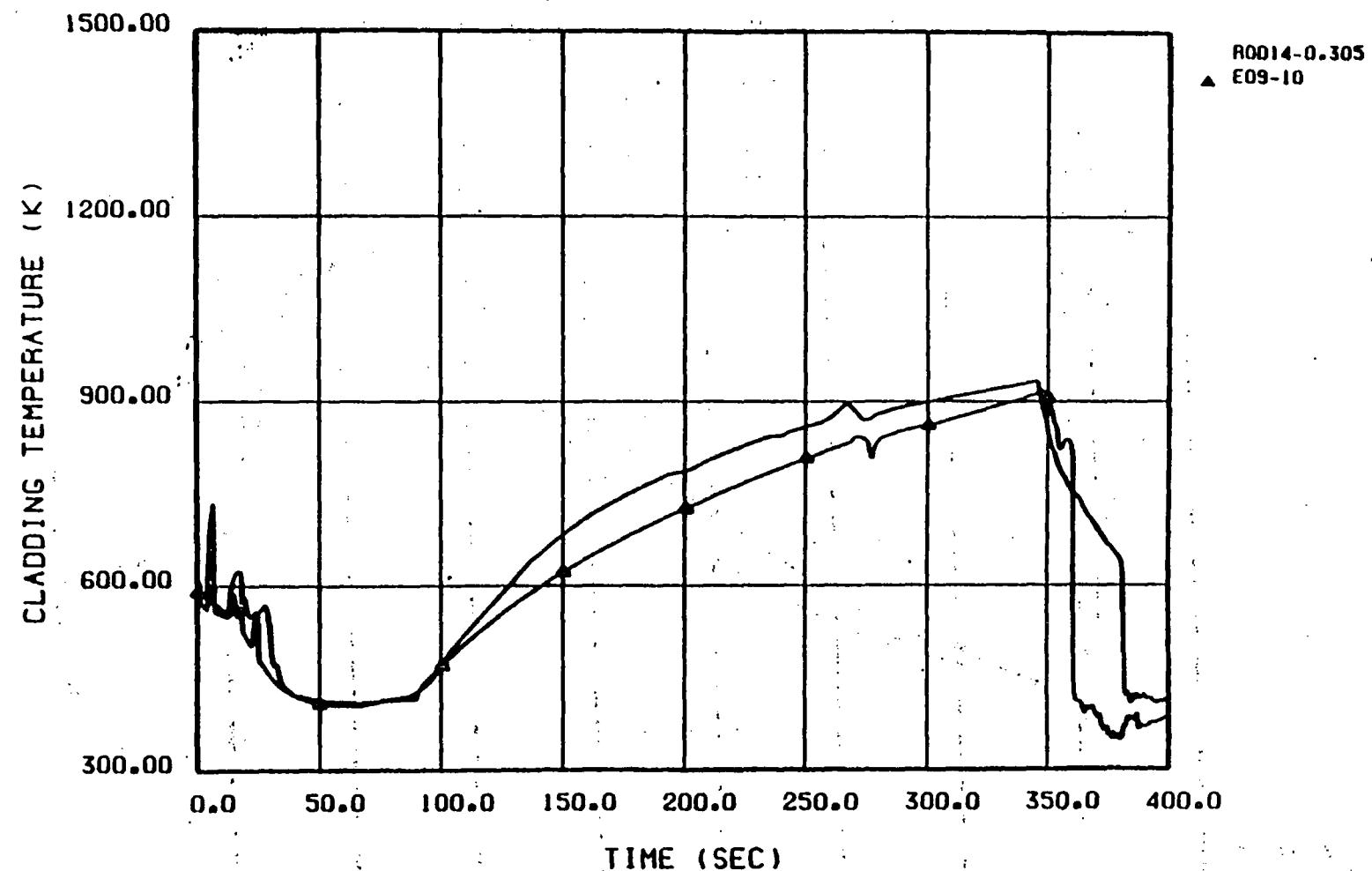


Figure 4.25. Cladding temperatures calculated for 5E09  
(6 % ruptured fuel rod)

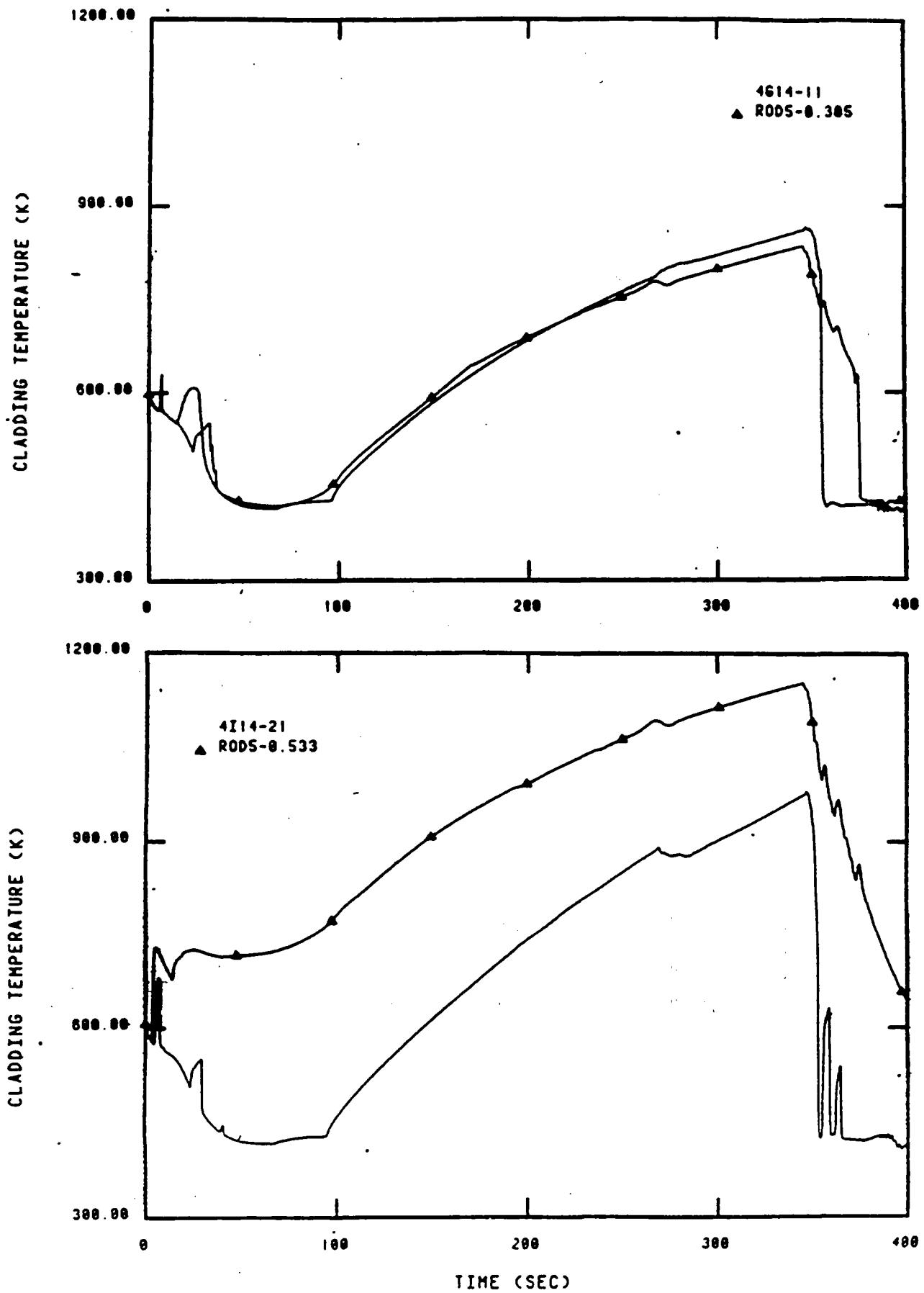


Figure 4.26. Cladding temperatures calculated for fuel rods in peripheral bundles

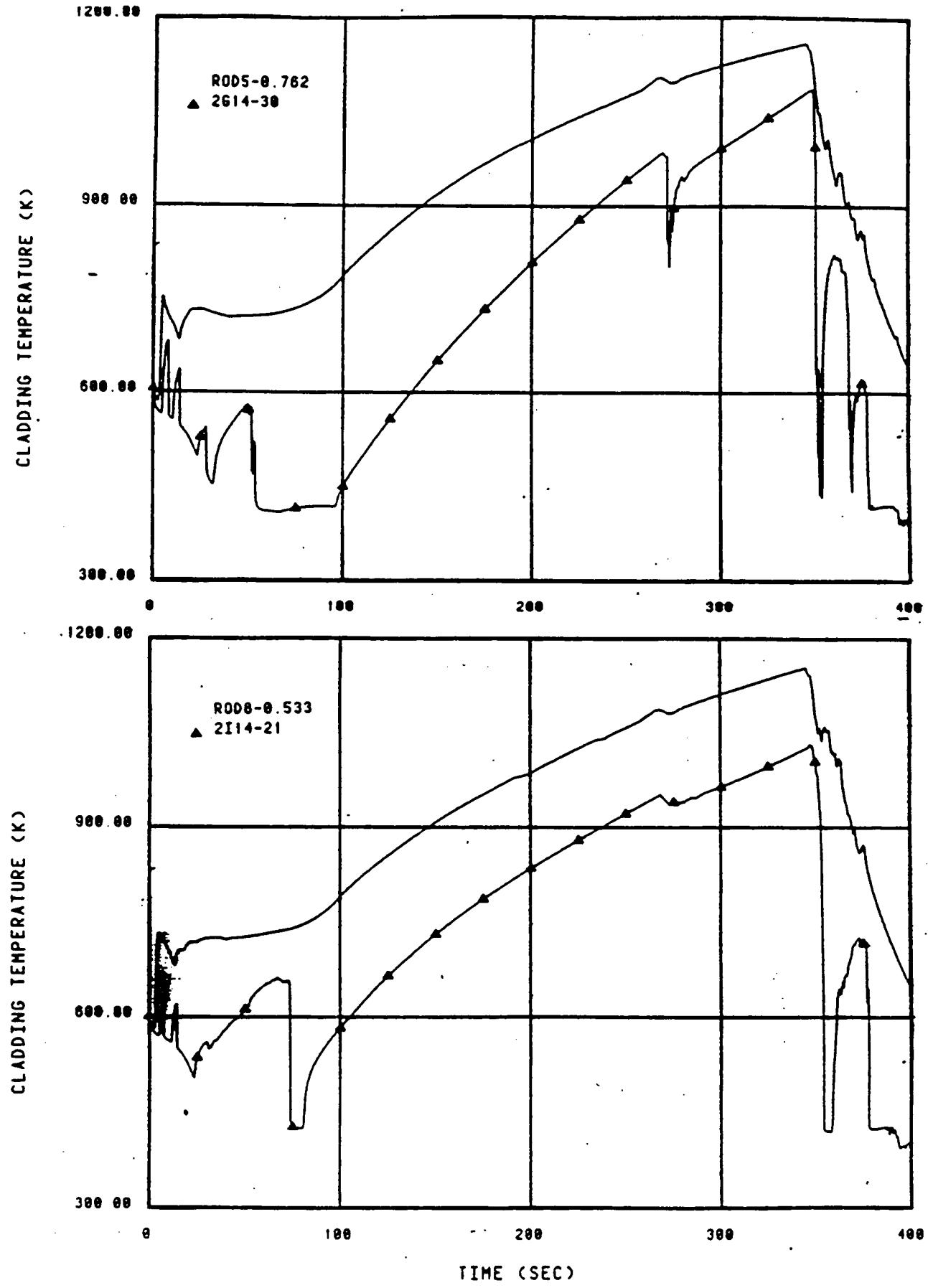


Figure 4.26. Cladding temperatures calculated for fuel rods in peripheral bundle 2

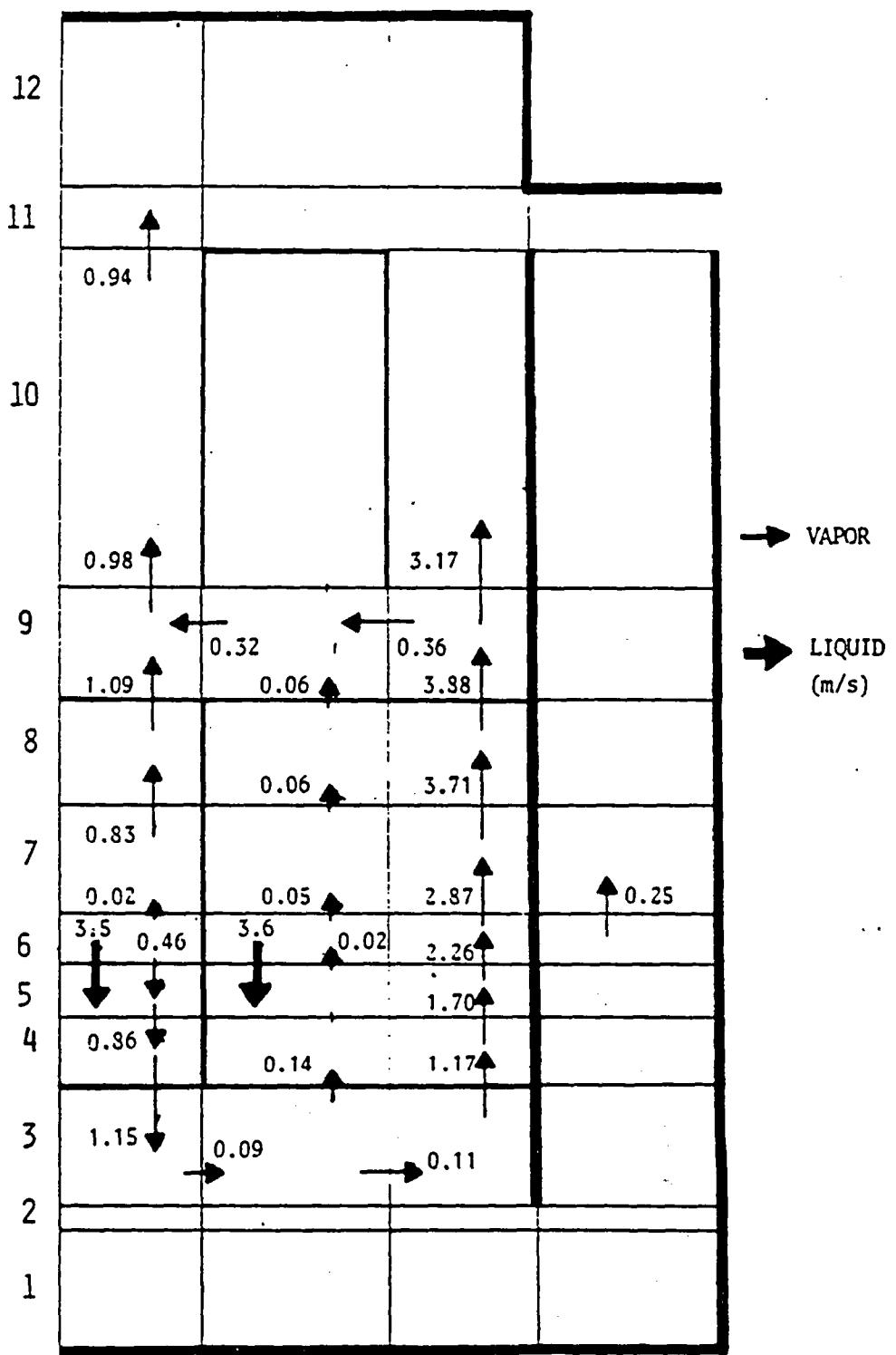
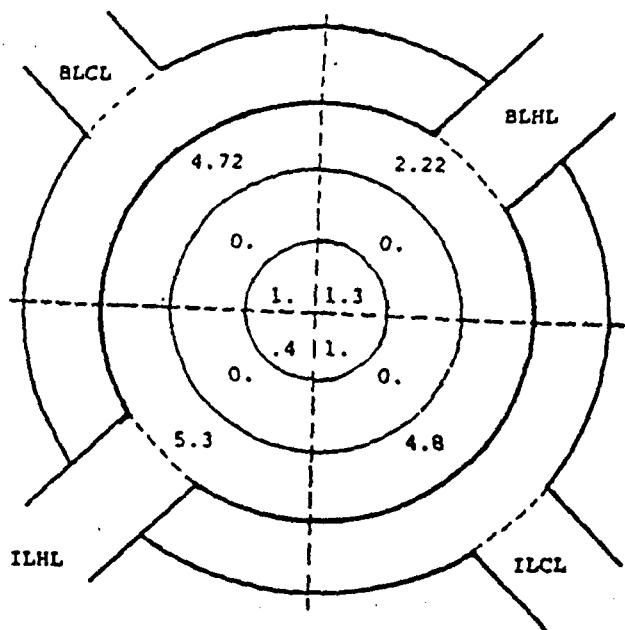
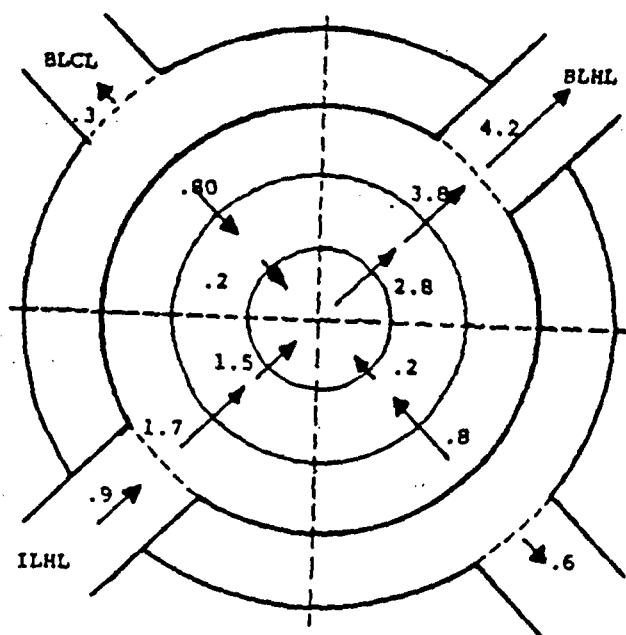


Figure 4.27. Flow patterns in vessel during rupture phase



**Figure 4.28.** Vapor axial velocity (m/s) from level 10 to 11 during rod rupture phase



**Figure 4.29.** Vapor radial velocity (m/s) in level 11 during rod rupture phase

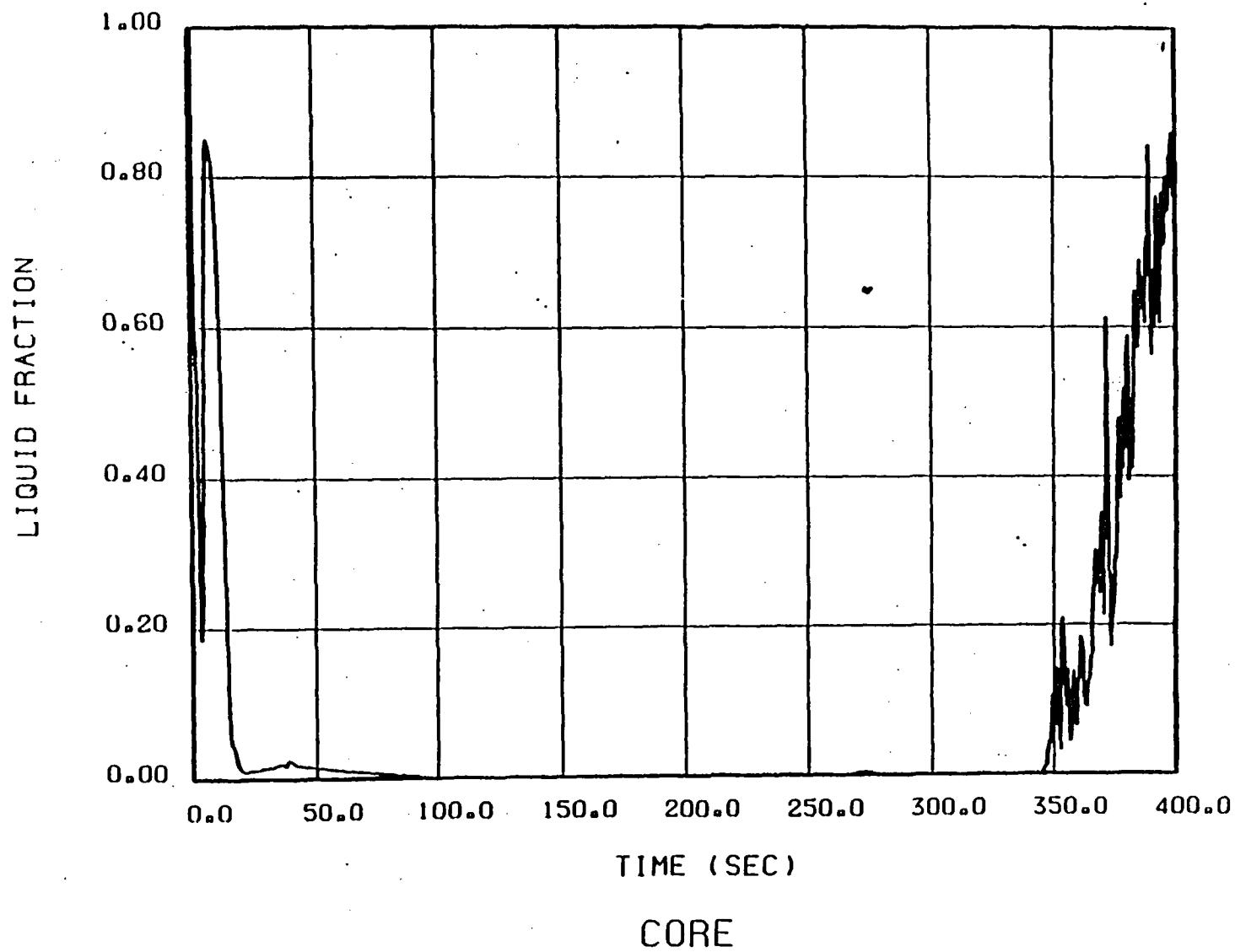


Figure 4.30. Liquid fraction in core

## 5. RUN STATISTICS

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In the nodalization defined we have used the following number of cells:

- Vessel and core ..... 192
  - Intact loop ..... 54
  - Broken loop ..... 37
  - Steam generator  
(secondary side) .... 19
- 

Total number of cells = 302

Minimum and maximum time steps selected were:

Range (s)	DTMIN (s)	DTMAX (s)
0 - 1	1.E-5	1.E-3
1 - 5	1.E-5	1.E-2
5 - 345	1.E-5	1.E-1

---

These maximum values haven't been reached in any phase as may be seen in Fig 5.1, where the time step evolution along the transient is shown.

Figure 5.2 reflects the cumulative CPU time used in calculating the transient. Clearly, we can distinguish two phases according to the time steps selected by the code:

Phase	Range (s)	Number steps	CPU time (s)	RS
Blowdown & Heat-up	0 - 345	21500	624E3	96.1
Reflood	345 - 400	16000	576E3	119.2

---

The last column, named RS, represents the calculated run statistics (CPU time in ms per cell and time step) in units of ms/(cell\*step).

Machine used for this calculation was CDC Cyber (operating system NOS-BE) with reserved Core Memory = 376500 and Extended Memory = 500.

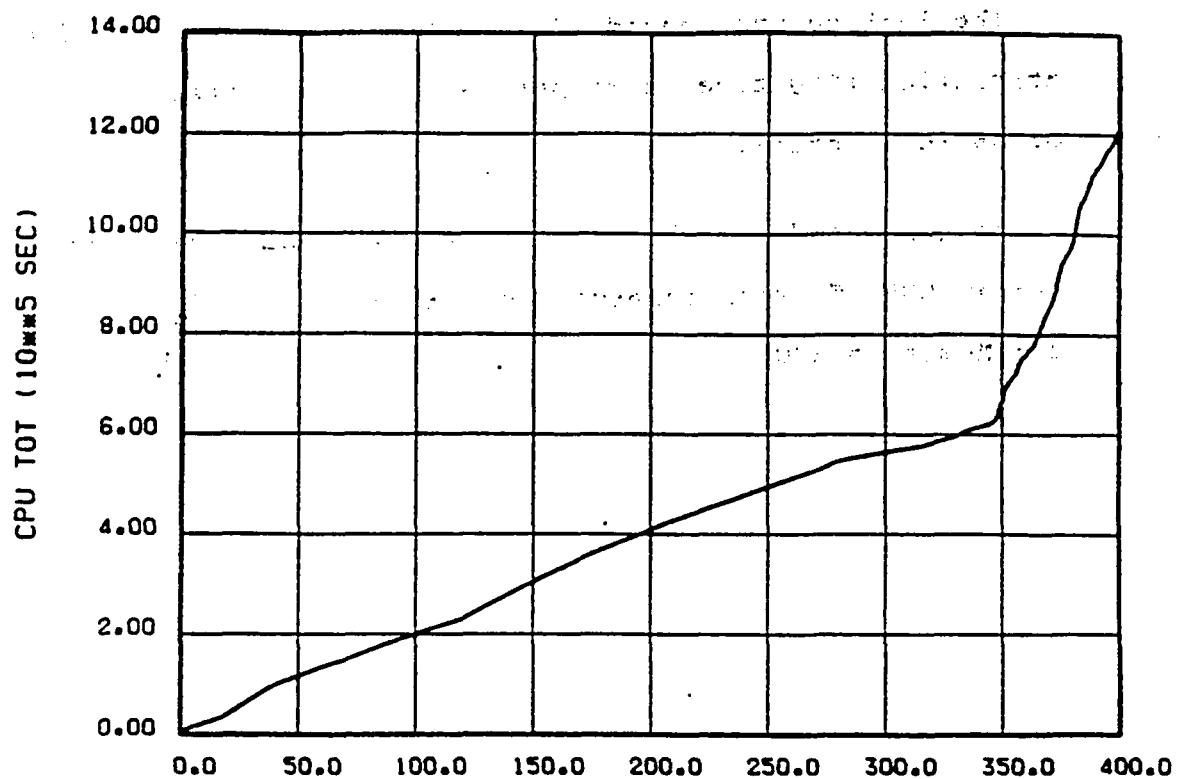


Figure 5.2. Accumulated CPU time

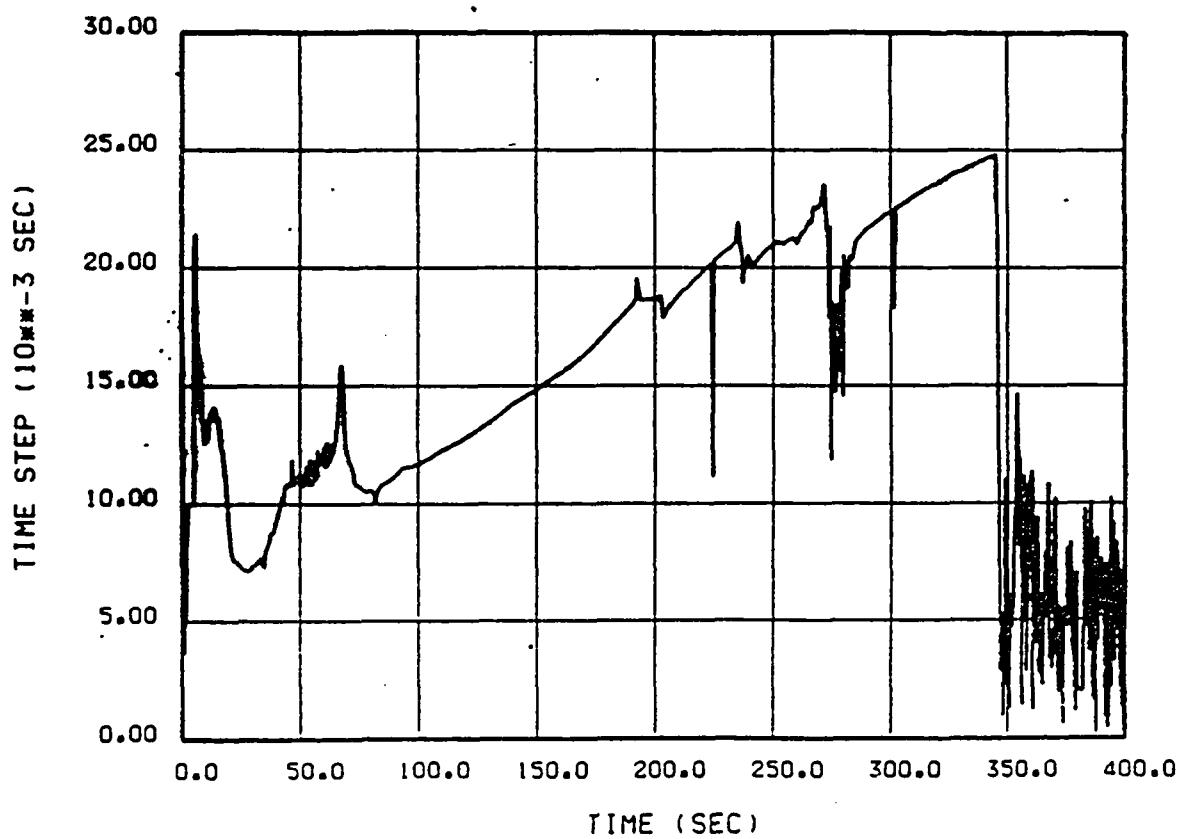


Figure 5.1. Time step evolution

## **6. CONCLUSIONS**

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1. Good agreement exists between calculated and experimental hydraulic variables during the blowdown, like pressure, mass flow rates and densities.
2. TRAC-PF1 cannot simulate observed initial quenches and final quench time. If these delays were consequence of an incorrect value of MSFBT, introducing a multiplicative correcting factor greater than 1.12 in the correlation for MSFBT (only for the FP-1 case), the experimental quench time can be reproduced.
3. Good agreement is found between calculated and measured cladding temperatures for the 4 % enriched rods in central fuel assembly.
4. Those simulated 6 % fuel rods which suffer quench during the blowdown phase (such as rod 15 in TRAC, close to ILCL), show the best fitting with thermocouple data. For the remaining 6 % and peripheral rods, higher temperatures are calculated in film boiling transfer regime.
5. Three-dimensional behaviour is calculated, although unplanned upper plenum injection was defined to be azimuthally symmetric within each ring.
6. Flow patterns during rod rupture period show two possible paths for fission products in a non-dry phase.

## 7. REFERENCES

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## **APENDIX A. LOFT system instrumentation**

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This section resumes the instrumentation nomenclature and location in the LOFT facility, contained in reference [5].

Figures show locations for the main instrumentation used for the FP-1 thermal-hydraulic study.

All experimental data plotted in this document are identified using the instrumentation nomenclature explained in Table A.1, which is also used for the related variables. The DIRC report resumed, shows the qualified and failed data in the experiment, recorded at 50 samples per second, except in the cases which are noted.

TABLE A.1. Nomenclature for LOFT instrumentation

**Designation for the different types of transducers**

RPE - Pump speed	FE - Coolant flow
PE - Pressure transducer	DE - Densitometer
PdE - Differential pressure	ME - Momentum flux
LE - Coolant level	FT - Flow rate
PS - Pressure switch	TC - Fuel centerline
TE - Thermocouple	

**Designation of systems**

PC - Primary coolant intact	LP - Lower plenum
BL - Broken loop	ST - Dowcomer stalk
RV - Reactor vessel	UP - Upper plenum
P120 - Emergency core coolant system	P128 - Primary coolant addition and control

**Designation for Core instrumentation**

Transducer location (inches from bottom) —

Fuel assembly row —

Fuel assembly column —

Fuel assembly number —

Transducer type —

TE-3B11-28

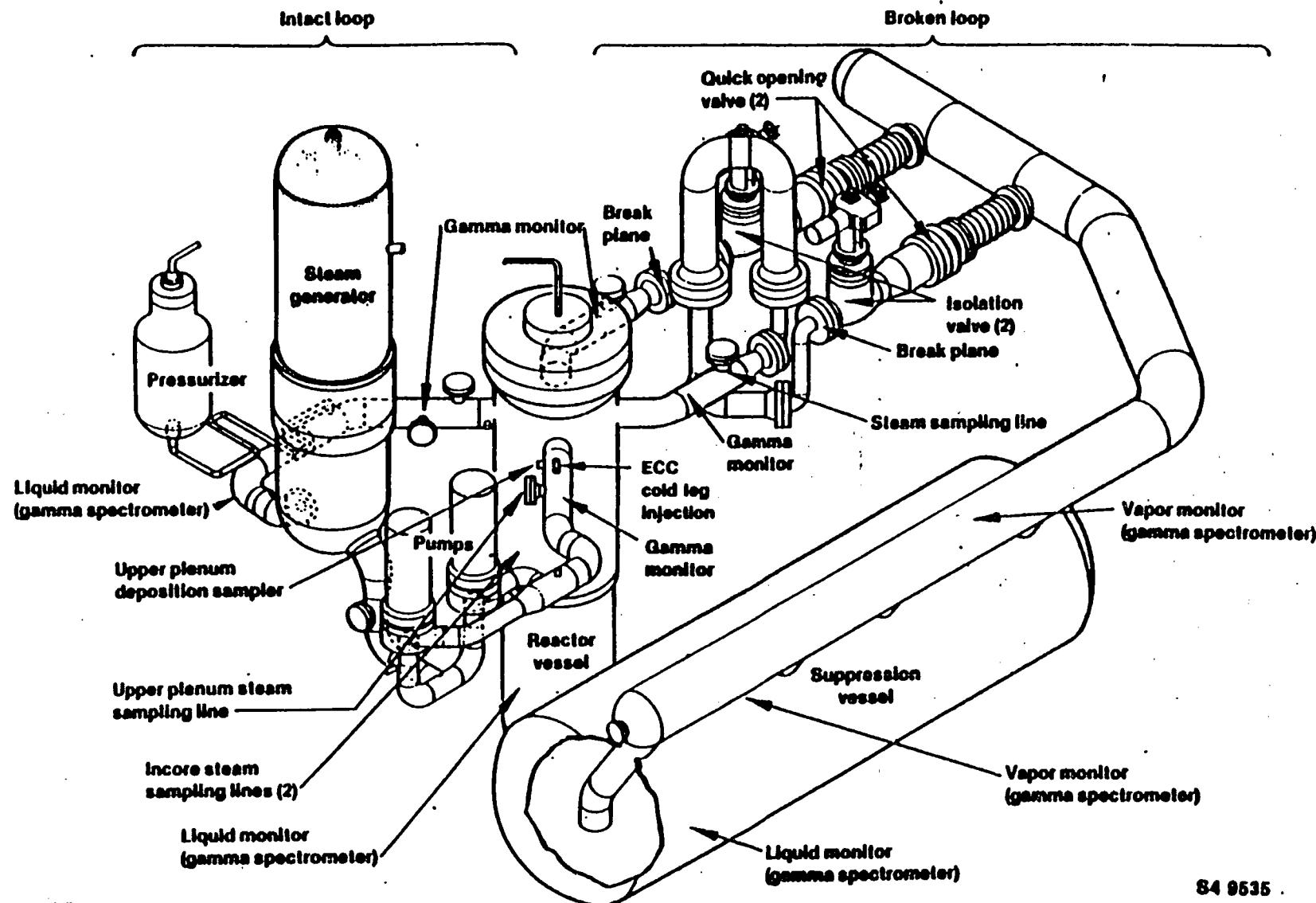


Figure A-1. LOFT Major Components

84 9535

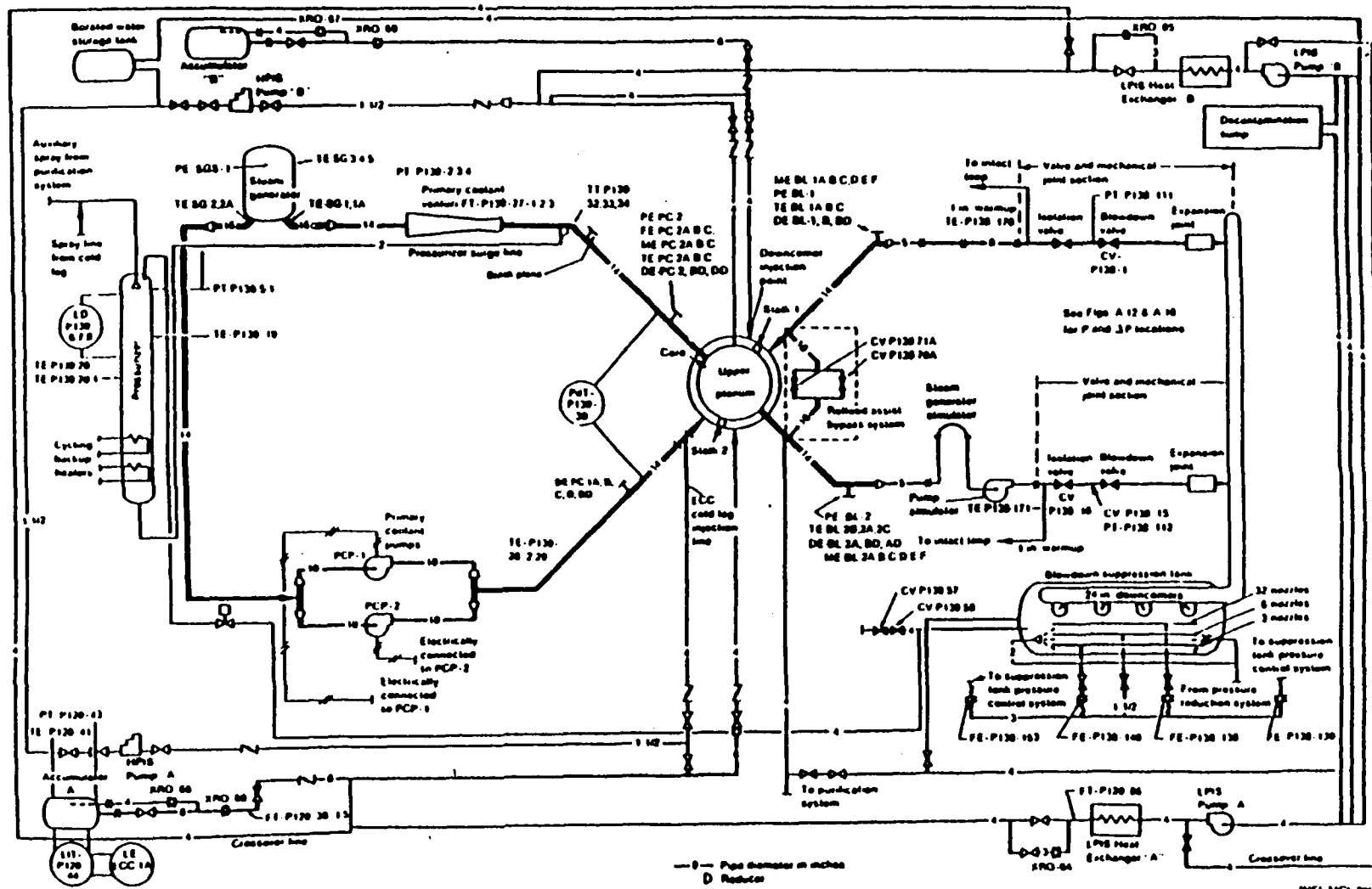


Figure A-2. LOFT Piping Schematic with Instrumentation

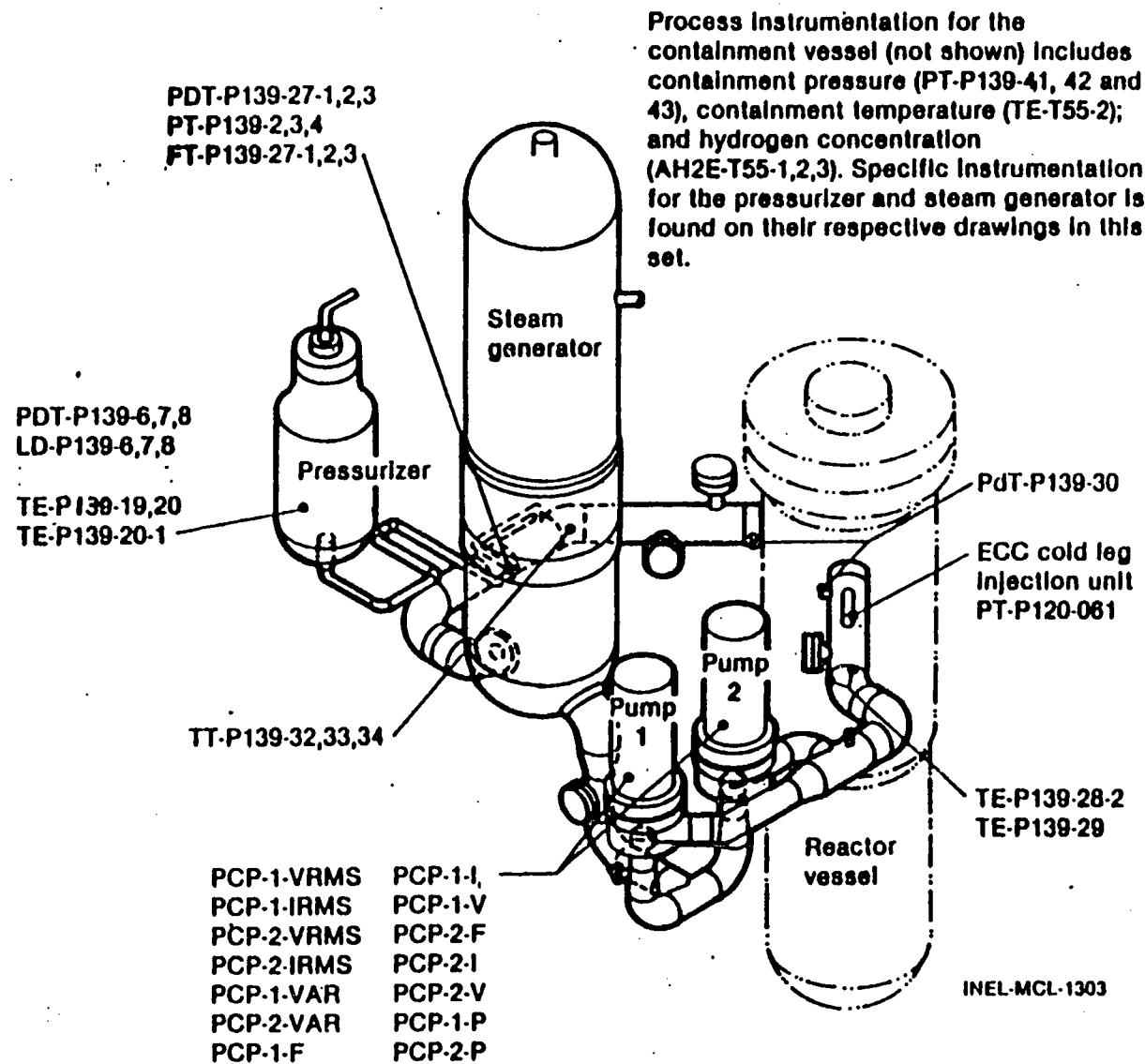


Figure A-3 LOFT Intact Loop Process  
Instrumentation

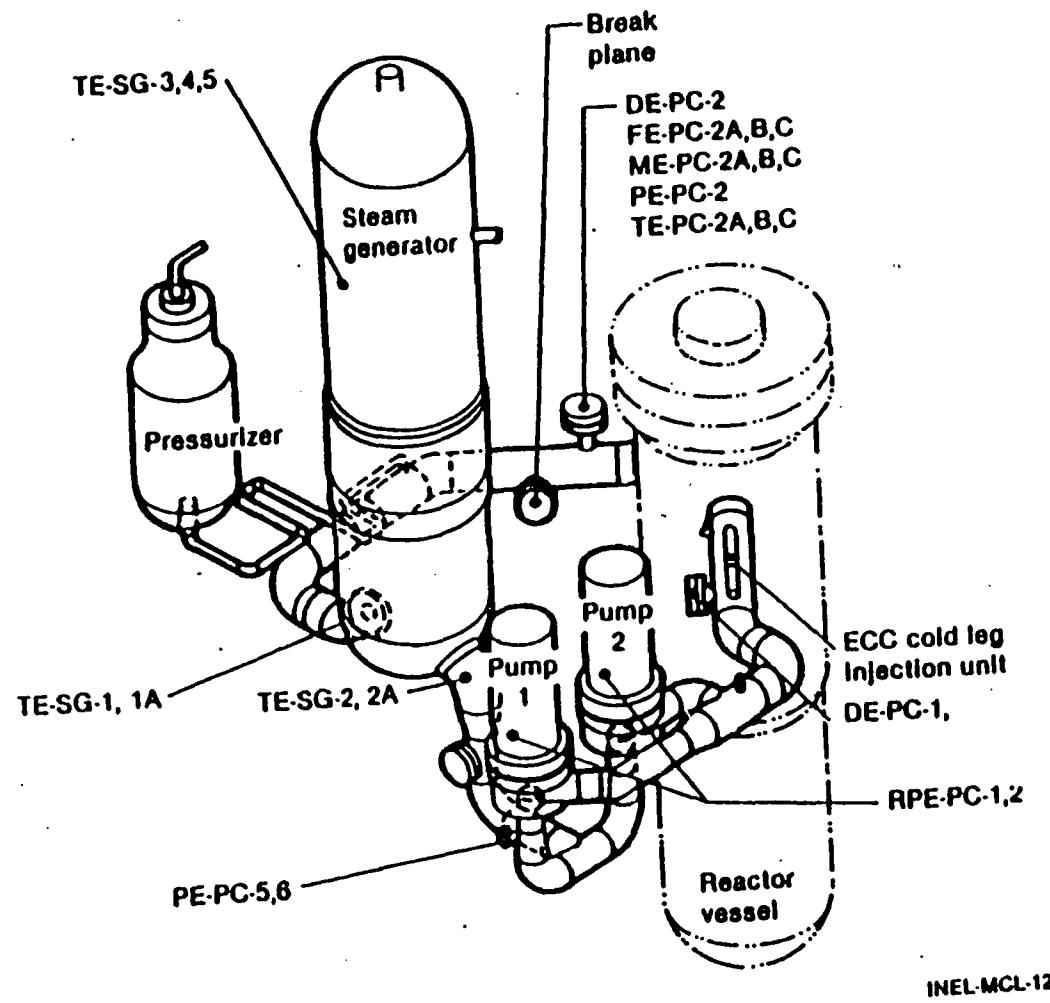


Figure A-4. LOFT Intact Loop Experimental Thermal-Hydraulic Instrumentation

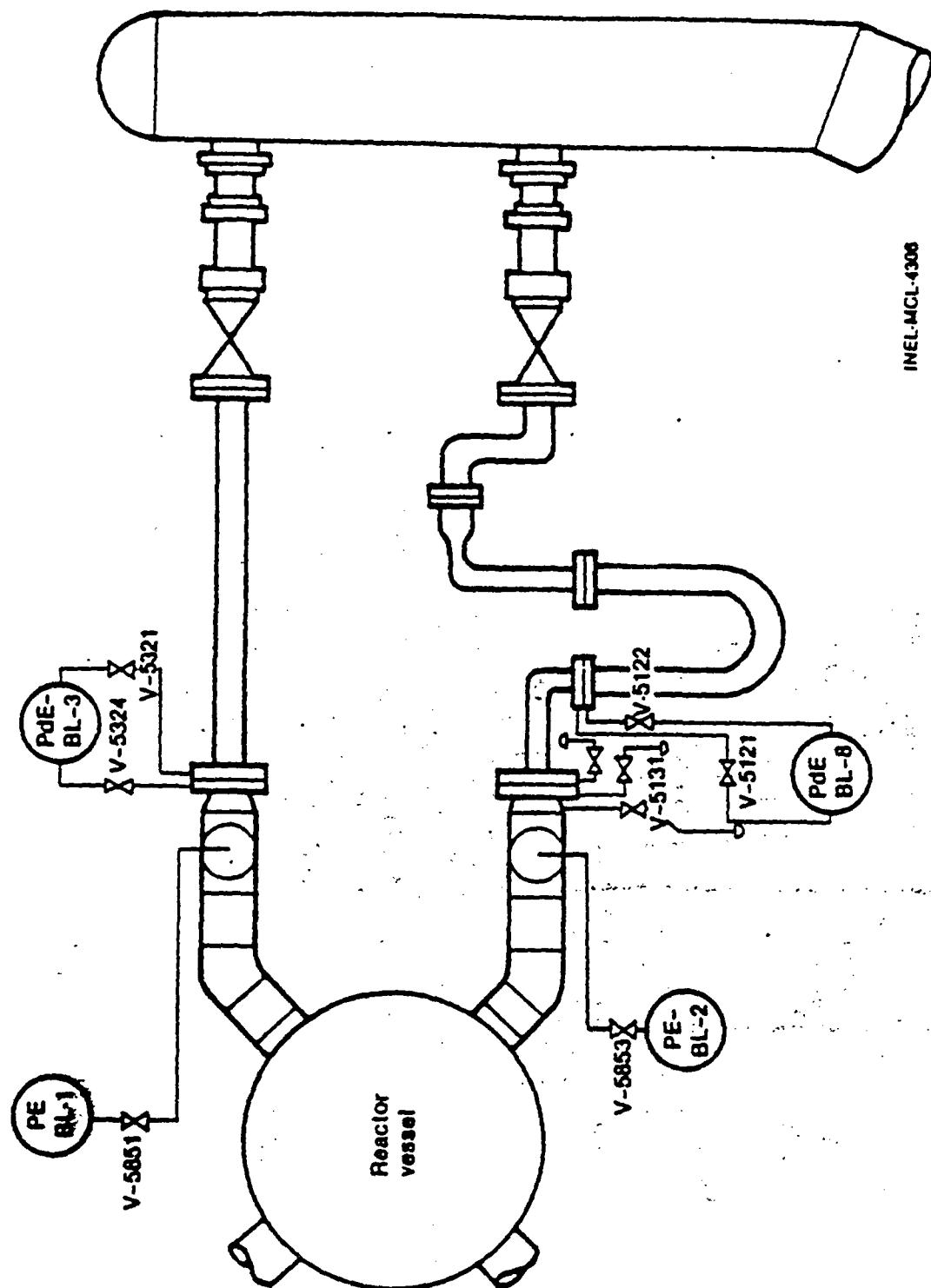


Figure A-5. Instrument Locations - Broken Loop Differential Pressure Measurements

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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
CV-P004-008	VALVE POS-FEEDWATER FLOW CONTROL	01-03-85	QUALIFIED	
CV-P004-010	VALVE POS-SCS STEAM FLOW CONTROL	12-31-84	QUALIFIED	
CV-P004-090	MAIN STEAM BYPASS VALVE	01-03-85	QUALIFIED	
CV-P004-091	MAIN FEED BYPASS VALVE	12-31-84	QUALIFIED	
CV-P138-001	VALVE POS-BROKEN LOOP CL Q0BV	01-03-85	QUALIFIED	
CV-P138-015	VALVE POS-BROKEN LOOP HL Q0BV	12-31-84	QUALIFIED	
CV-P138-070A	VALVE POS-BLOWDOWN SYSTEM RABV CH A	12-31-84	QUALIFIED	
CV-P138-071A	VALVE POS-BLOWDOWN SYSTEM RABV CH B	12-31-84	QUALIFIED	
DE-BL-001A	CHORDAL DENSITY-BROKEN LOOP CL	01-03-85	QUALIFIED	
DE-BL-001B	CHORDAL DENSITY-BROKEN LOOP CL	01-03-85	QUALIFIED	
DE-BL-001C	CHORDAL DENSITY-BROKEN LOOP CL	01-03-85	QUALIFIED	TO 65 SECONDS
DE-BL-002A	CHORDAL DENSITY-BROKEN LOOP HL	01-03-	QUALIFIED	TO 65 SECONDS
DE-BL-002B	CHORDAL DENSITY-BROKEN LOOP HL	01-03	QUALIFIED	TO 65 SECONDS

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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
DE-BL-002C	CHORDAL DENSITY-BROKEN LOOP HL	01-09-85	QUALIFIED	TO 65 SECONDS
DE-BL-002D	GROSS GAMMA BKG/BROKEN LOOP HL	01-29-85	QUALIFIED	TREND DATA ONLY, 80 SAMPLES PER SECOND DATA
DE-BL-105	AVERAGE DENSITY-BROKEN LOOP CL	01-11-85	QUALIFIED	AFTER 13 SECONDS SPURIOUS SPIKES
DE-BL-205	AVERAGE DENSITY-BROKEN LOOP HL	01-11-85	QUALIFIED	TO 65 SECONDS
DE-PC-001A	CHORDAL DENSITY-INTACT LOOP CL	01-08-85	QUALIFIED	SPURIOUS SPIKES
DE-PC-001B	CHORDAL DENSITY-INTACT LOOP CL	01-08-85	QUALIFIED	SPURIOUS SPIKES
DE-PC-001C	CHORDAL DENSITY-INTACT LOOP CL	01-08-85	QUALIFIED	SPURIOUS SPIKES
DE-PC-002A	CHORDAL DENSITY-INTACT LOOP HL	01-09-85	QUALIFIED	DE-PC-001D USED FOR BACKGROUND CORRECTION
DE-PC-002B	CHORDAL DENSITY-INTACT LOOP HL	01-03-85	QUALIFIED	TO 65 SECONDS
DE-PC-002C	CHORDAL DENSITY-INTACT LOOP HL	01-09-85	FAILED	
DE-PC-002D	GROSS GAMMA BKG/INTACT LOOP HL	01-29-85	QUALIFIED	TREND DATA ONLY
DE-PC-105	AVERAGE DENSITY - INTACT LOOP CL	01-11-85	QUALIFIED	
DE-PC-225	WEIGHTED AVG DENSITY IL HL	01-11-85	QUALIFIED	TO 65 SECONDS

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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
FE-PC-002A	VELOCITY-INTACT LOOP HOT LEG BOTTOM	01-09-85	QUALIFIED	UNIDIRECTIONAL
FE-PC-002B	VELOCITY-INTACT LOOP HOT LEG MIDDLE	01-09-85	QUALIFIED	UNIDIRECTIONAL
FE-PC-002C	VELOCITY-INTACT LOOP HOT LEG TOP	01-09-85	QUALIFIED	UNIDIRECTIONAL
FE-PC-002	AVERAGE VELOCITY - INTACT LOOP HL	01-22-85	QUALIFIED	UNIDIRECTIONAL
FE-1ST-001	VELOCITY DOWNCOMER STALK 1	01-09-85	QUALIFIED	UNIDIRECTIONAL
FE-1ST-002	VELOCITY DOWNCOMER STALK 1 LOWER	01-10-85	QUALIFIED	UNIDIRECTIONAL
FE-5UP-002	VELOCITY-FAS ABOVE UPPER END BOX	01-09-85	QUALIFIED	UNIDIRECTIONAL
FR-BL-203	AVERAGE FLOWRATE, BROKEN LOOP CL	01-10-85	QUALIFIED	TO 69 SECONDS
FR-BL-203	AVERAGE FLOWRATE, BROKEN LOOP HL	01-22-85	QUALIFIED	TO 420 SECONDS. MASS FLOW AFTER 69 SECONDS BASED ON STEAM DENSITY
FR-PC-203	MASS FLOW RATE HL DD+DENS	01-22-85	QUALIFIED	TO 22 SECONDS. B DRAG DISC SUBSTITUTED FOR C DRAG DISC IN CALCULATION
FT-P004-012	FLOWRATE-STEAM FLOW CONDENSER IN	01-03-85	QUALIFIED	INITIAL CONDITIONS ONLY
FT-P004-090	VOLUMETRIC FLOW, STEAM ULTRASONIC B	01-03-85	QUALIFIED	
FT-P004-091	VOLUMETRIC FLOW SECONDARY	01-03-85	QUALIFIED	

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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
FT-P004-72A	FLOWRATE-SCS FEEDWATER	01-09-85	QUALIFIED	INITIAL CONDITION ONLY
FT-P004-72-2	FLOWRATE-SCS FEEDWATER	01-09-85	QUALIFIED	INITIAL CONDITIONS ONLY
FT-P120-072	FLOWRATE-LPIS PUMP B DISCHARGE	01-03-85	QUALIFIED	NO OTHER MEASUREMENT FOR DIRECT COMPARISON
FT-P120-085	FLOWRATE-LPIS PUMP A DISCHARGE	01-03-85	QUALIFIED	NO OTHER MEASUREMENT FOR DIRECT COMPARISON
FT-P120-085	FLOWRATE-HPIIS PUMP B DISCHARGE	01-09-85	QUALIFIED	NO OTHER MEASUREMENT FOR DIRECT COMPARISON
FT-P120-104	FLOWRATE-HPIIS PUMP A DISCHARGE	01-10-85	QUALIFIED	NO OTHER MEASUREMENT FOR DIRECT COMPARISON
FT-P139-27-1	FLOWRATE-INTACT LOOP COOLANT	01-08-85	QUALIFIED	INITIAL CONDITION ONLY
FT-P139-27-2	FLOWRATE-INTACT LOOP COOLANT	01-08-85	QUALIFIED	INITIAL CONDITION ONLY
FT-P139-27-3	FLOWRATE-INTACT LOOP COOLANT	01-08-85	QUALIFIED	INITIAL CONDITION ONLY
FT-P141-022	FLOWRATE-TOTAL PCC	01-03-85	QUALIFIED	NO OTHER MEASUREMENT FOR DIRECT COMPARISON
LD-P139-006	LIQUID LEVEL-PRESSURIZER CH A	12-31-84	QUALIFIED	INITIAL CONDITIONS ONLY
LD-P139-007	LIQUID LEVEL-PRESSURIZER CH B	12-31-84	QUALIFIED	INITIAL CONDITIONS ONLY
LD-P139-008	LIQUID LEVEL-PRESSURIZER CH C	12-31-84	FAILED	

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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S) <sup>1</sup>
LEPDE-SV-161	LIQUID LEVEL-BST	01-18-85	QUALIFIED	INITIAL AND FINAL CONDITIONS ONLY
LEPDE-SV-261	LIQUID LEVEL-BST	01-18-85	QUALIFIED	INITIAL AND FINAL CONDITIONS ONLY
LE-ECC-01A	ACCUMULATOR A LIQUID LEVEL	01-11-85	QUALIFIED	NO OTHER MEASUREMENT FOR DIRECT COMPARISON
LE-1F10	COOLANT LEVEL-FUEL ASSY 1 LOC F10	01-03-85	QUALIFIED	FAILED STINGS - 1,4,5,6,7,8,9,11,13,16,18,19
LE-1ST-001	COOLANT LEVEL-INSTR STALK 1 LP	12-27-84	QUALIFIED	
LE-1ST-002	COOLANT LEVEL-INSTR STALK 1 DC	12-27-84	QUALIFIED	FAILED STINGS - 1,2,5
LE-3F10	COOLANT LEVEL-FUEL ASSY 3 LOC F10	12-27-84	QUALIFIED	FAILED STINGS - 2,3,4,5,7,11,16,18,19
LE-3UP-001	COOLANT LEVEL-UPPER PLENUM	01-03-85	QUALIFIED	FAILED STINGS - 1,2,3,4,9,6,7
LE-5E11	COOLANT LEVEL-FUEL ASSY 5 LOC E 11	12-27-84	QUALIFIED	FAILED STRING - 17
LE-5UP-001	COOLANT LEVEL-UPPER PLENUM	12-27-84	QUALIFIED	
LIT-P120-030	LIQUID LEVEL-ACCUMULATOR B	01-11-85	QUALIFIED	NO OTHER MEASUREMENT FOR DIRECT COMPARISON
LTD-P138-033	BST DENS CORR	01-18-85	QUALIFIED	INITIAL AND FINAL CONDITIONS ONLY
LTD-P138-058	BST DENS CORR	01-18-85	QUALIFIED	INITIAL AND FINAL CONDITIONS ONLY

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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S),
LT-P004-008A	STEAM GENERATOR LEVEL NARROW RANGE	01-14-85	QUALIFIED	
LT-P004-042	CONDENSATE RECEIVER LEVEL	12-31-84	QUALIFIED	
LT-P004-08AA	STEAM GEN LEVEL NARROW RANGE	01-14-84	QUALIFIED	
LT-P138-033	LIQUID LEVEL-BST A	01-18-85	QUALIFIED	INITIAL AND FINAL CONDITIONS ONLY
LT-P138-038	LIQUID LEVEL-BST B	01-18-85	QUALIFIED	INITIAL AND FINAL CONDITIONS ONLY
ME-BL-001A	NON FLUX, BL-1, BOT, HIGH RANGE	01-18-85	QUALIFIED	TO 69 SECONDS
ME-BL-001B	NON FLUX, BL-1, MIDDLE, HIGH RANGE	01-18-85	QUALIFIED	TO 69 SECONDS
ME-BL-001C	NON FLUX, BL-1, TOP, HIGH RANGE	01-18-85	QUALIFIED	TO 69 SECONDS
ME-BL-001	AVERAGE NON FLUX BROKEN LOOP CL	01-18-85	QUALIFIED	TO 69 SECONDS
ME-BL-002A	MOMENTUM FLUX-BROKEN LOOP HL BOTTOM	01-18-85	QUALIFIED	
ME-BL-002B	MOMENTUM FLUX-BROKEN LOOP HL MIDDLE	01-18-85	QUALIFIED	
ME-BL-002C	MOMENTUM FLUX-BROKEN LOOP HL TOP	01-18-85	QUALIFIED	
ME-BL-002	AVERAGE MOM FLUX BROKEN LOOP HL	01-18-85	QUALIFIED	

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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
ME-PC-002A	MOMENTUM FLUX-INTACT LOOP HL BOTTOM	01-22-85	QUALIFIED	TO 22 SECONDS
ME-PC-002B	MOMENTUM FLUX-INTACT LOOP HL MIDDLE	01-22-85	QUALIFIED	TO 22 SECONDS
ME-PC-002C	MOMENTUM FLUX-INTACT LOOP HL TOP	01-10-85	FAILED	
ME-PC-002	AVE MOMENTUM FLUX-INTACT LOOP HL	01-22-85	QUALIFIED	TO 22 SECONDS. B DRAG DISC SUBSTITUTED FOR C DRAG DISC IN CALCULATION
ME-1ST-001	MOMENTUM FLUX-INSTR STALK 1 DC	01-22-85	FAILED	
ME-1ST-002	MOMENTUM FLUX-INSTR STALK 1 DC	01-22-85	FAILED	
ME-SUP-002	MOMENTUM FLUX-FAS AB UPPER END BOX	01-22-85	QUALIFIED	UNTIL 10 SECs AND AFTER 70 SECONDS UNCOMPENSATED TEMPERATURE SENSITIVITY BETWEEN 10 & 70 SECs.
ME-2H08-26	NEUTRON DETECTOR IN CORE FA#2	12-31-84	QUALIFIED	
ME-4H08-26	NEUTRON DETECTOR IN CORE FA#4	12-31-84	QUALIFIED	
ME-6H08-26	NEUTRON DETECTOR IN CORE FA#6	12-31-84	QUALIFIED	
PDE-BL-003	DELTA P-BL COLD LEG BRK PLANE	01-03-85	QUALIFIED	
PDE-BL-008	DELTA P-BL ACROSS SG SIM IN FLNG	01-03-85	QUALIFIED	
PDE-SV-001	SUPPRESSION VESSEL LEVEL	01-10-85	QUALIFIED	INITIAL AND FINAL CONDITIONS ONLY

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## FP-1 FINAL DIRC QUALIFICATION REPORT

EFFECTIVE DATE: 01/30/85  
REVISIONS: FINAL  
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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
PDE-SV-002	SUPPRESSION VESSEL LEVEL	01-18-85	QUALIFIED	INITIAL AND FINAL CONDITIONS ONLY
PDT-P139-27-1	INTACT LOOP MASS FLOW DELTA P	01-08-85	QUALIFIED	INITIAL CONDITION ONLY, TREND THEREAFTER
PDT-P139-27-2	INTACT LOOP MASS FLOW DELTA P	01-08-85	QUALIFIED	INITIAL CONDITION ONLY, TREND THEREAFTER
PDT-P139-27-3	INTACT LOOP MASS FLOW DELTA P	01-08-85	QUALIFIED	INITIAL CONDITION ONLY, TREND THEREAFTER
PDT-P004-072	DIFF PRESS FEEDWATER FLOW ORIFICE	01-09-85	QUALIFIED	INITIAL CONDITIONS ONLY
PDT-P139-030A	DELTA P-PRIMARY COOLANT PUMP	01-03-85	QUALIFIED	INITIAL CONDITIONS ONLY
PDT-P139-030B	DELTA P-INTACT LOOP SG	01-08-85	QUALIFIED	INITIAL CONDITION ONLY, TREND THEREAFTER
PDT-P139-030	DELTA P - REACTOR VESSEL	01-03-85	QUALIFIED	UNIDIRECTIONAL
PE-BL-001	PRESSURE-BROKEN LOOP COLD LEG	12-27-84	QUALIFIED	
PE-BL-002	PRESSURE-BROKEN LOOP HOT LEG	12-27-84	QUALIFIED	
PE-PC-002	PRESSURE-INTACT LOOP HOT LEG	12-27-84	QUALIFIED	
PE-PC-003	PRESSURE-INTACT LOOP REF.	12-27-84	QUALIFIED	
PE-PC-006	PRESSURE-INTACT LOOP REF.	12-27-84	QUALIFIED	

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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
PS-5F04-SW	PRESSURE SWITCH, FA 05	01-11-85	QUALIFIED	SWITCH ACTIVATES AT ROD INTERNAL PRESSURE OF 450 +/-20 PSI
PS-5F12-SW	PRESSURE SWITCH, FA 05	01-11-85	QUALIFIED	SWITCH ACTIVATES AT ROD INTERNAL PRESSURE OF 450 +/-20 PSI
PS-5G11-SW	PRESSURE SWITCH, FA 05	01-11-85	QUALIFIED	SWITCH ACTIVATES AT ROD INTERNAL PRESSURE OF 450 +/-20 PSI
PS-5I05-SW	PRESSURE SWITCH, FA 05	01-11-85	QUALIFIED	SWITCH ACTIVATES AT ROD INTERNAL PRESSURE OF 450 +/-20 PSI
PS-5J12-SW	PRESSURE SWITCH, FA 05	01-11-85	QUALIFIED	SWITCH ACTIVATES AT ROD INTERNAL PRESSURE OF 450 +/-20 PSI
PT-P004-010A	PRESSURE-SCS 10 INCH LINE FROM SG	12-27-84	QUALIFIED	
PT-P004-022	CONDENSATE RECEIVER PRESSURE	12-27-84	QUALIFIED	
PT-P004-034	PRESSURE-SCS FEEDWATER	12-27-84	QUALIFIED	
PT-P004-085	PRESSURE-SCS 12 INCH CONDENSOR IN	12-27-84	FAILED	
PT-P120-029	PRESSURE-ECCS ACCUMULATOR B	12-27-84	QUALIFIED	
PT-P120-043	PRESSURE-ECCS ACCUMULATOR A	01-18-85	QUALIFIED	
PT-P128-102	AC-P-4B DISCHARGE PRESS	01-09-85	FAILED	
PT-P128-103	AC-P-4A DISCHARGE PRESS	01-09-85	QUALIFIED	

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## FP-I FINAL DIRC QUALIFICATION REPORT

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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
PT-P138-055	PRESSURE-BST VAPOR SPACE CH A	01-03-85	QUALIFIED	
PT-P138-056	PRESSURE-BST VAPOR SPACE CH B	01-03-84	QUALIFIED	
PT-P138-057	PRESSURE-BST VAPOR SPACE CH C	01-03-85	QUALIFIED	
PT-P139-002	PRESSURE-INTACT LOOP HOT LEG CH A	12-31-84	QUALIFIED	RESPONSE LIMITED DURING THE SUB COOLED BLOWDOWN
PT-P139-003	PRESSURE-INTACT LOOP HOT LEG CH B	12-31-84	QUALIFIED	RESPONSE LIMITED DURING THE SUB COOLED BLOWDOWN
PT-P139-004	PRESSURE-INTACT LOOP HOT LEG CH C	12-31-84	QUALIFIED	RESPONSE LIMITED DURING THE SUB COOLED BLOWDOWN
PT-P139-041	PRESSURE CONTAINMENT CHAN A	12-27-84	FAILED	
PT-P139-042	PRESSURE CONTAINMENT CHAN B	12-27-84	QUALIFIED	
PT-P139-043	PRESSURE CONTAINMENT CHAN C	12-31-84	QUALIFIED	
PT-P139-051	PRESSURE-PRESSURIZER	12-27-84	QUALIFIED	
RE-T-77-1A2	NIS-POWER RANGE CHANNEL A LEVEL	01-11-85	QUALIFIED	
RE-T-77-2A2	NIS-POWER RANGE CHANNEL B LEVEL	01-11-85	QUALIFIED	
RE-T-77-3A2	NIS-POWER RANGE CHANNEL C LEVEL	01-11-85	QUALIFIED	

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## FP-1 FINAL DIRE QUALIFICATION REPORT

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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
RPE-PC-001	PUMP SPEED-PRIMARY COOLANT PUMP 1	12-31-84	QUALIFIED	AFTER 5 SECONDS
RPE-PC-002	PUMP SPEED-PRIMARY COOLANT PUMP 2	12-31-84	QUALIFIED	
RP-CRDm2-TC	ROD POS-ROD 2 TURNS COUNTER	12-31-84	QUALIFIED	FOR SCRAM EVENT TIME ONLY
RP-CRDm4-TC	ROD POS-ROD 4 TURNS COUNTER	12-31-84	QUALIFIED	FOR SCRAM EVENT TIME ONLY
RP-CRDm6-TC	ROD POS-ROD 6 TURNS COUNTER	12-31-84	QUALIFIED	FOR SCRAM EVENT TIME ONLY
RP-CRDm8-TC	ROD POS-ROD 8 TURNS COUNTER	12-31-84	QUALIFIED	FOR SCRAM EVENT TIME ONLY
RTP165-S1-10	GROSS GAMMA S1 SAMPLE SYSTEM	01-22-85	QUALIFIED	TREND DATA ONLY
RTP165-S2-10	GROSS GAMMA S2 SAMPLE SYSTEM	01-22-85	FAILED	
RTP165-S3-10	GROSS GAMMA S3 SAMPLE SYSTEM	01-22-85	QUALIFIED	S-3 SAMPLE SYSTEM BLOCKED
RTP165-S4-10	GROSS GAMMA S4 SAMPLE SYSTEM	01-22-85	QUALIFIED	TREND DATA ONLY
SP-BL-0018	SAT PRESSURE BROKEN LOOP CL	01-08-85	QUALIFIED	
SP-BL-0028	SAT PRESSURE BROKEN LCCP HL	01-08-85	QUALIFIED	
SP-PC-0028	SATURATION PRESS-INTACT LOOP HL	01-08-85	QUALIFIED	

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## FP-1 FINAL DIRC QUALIFICATION REPORT

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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
SP-SG-004	SATURATION PRESSURE, STEAM GEN, MID	01-08-89	QUALIFIED	
SP-1ST-005	SATURATION PRESS-DOWNCOMER STALK 1	01-08-89	QUALIFIED	
SP-1UP-001	SATURATION PRESSURE, UPPER PLENUM	01-08-89	QUALIFIED	
ST-BL-001	SAT TEMPERATURE BROKEN LOOP CL	01-08-89	QUALIFIED	
ST-BL-002	SAT TEMPERATURE BROKEN LOOP HL	01-08-89	QUALIFIED	
ST-PC-002	SATURATION TEMP, INTACT LOOP, HL	01-08-89	QUALIFIED	
ST-PC-005	SATURATION TEMP, INTACT LOOP, CL	01-08-89	QUALIFIED	
ST-P004-010A	SATURATION TEMP - SCS SG 10 IN LINE	01-08-89	QUALIFIED	
TC-5D06-27	TEMP FUEL CENTERLINE/FA5 PIN D6 27"	12-27-84	FAILED	
TC-5D10-27	TEMP FUEL CENTERLINE/FA5 PIN D10 27	01-03-89	QUALIFIED	FAILED PRE-LOCE TEST
TE-BL-001A	COOLANT TEMP-BROKEN LOOP CL BOTTOM	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-BL-001B	COOLANT TEMP-BROKEN LOOP CL MIDDLE	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-BL-001C	COOLANT TEMP-BROKEN LOOP CL TOP	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS

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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
TE-BL-002B	COOLANT TEMP-BROKEN LOOP HL MIDDLE	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-BL-002C	COOLANT TEMP-BROKEN LOOP HL TOP	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-PC-002A	TEMP-INTACT LOOP HL BOTTOM	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-PC-002B	TEMP-INTACT LOOP HL MIDDLE	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-PC-002C	TEMP-INTACT LOOP HL TOP	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-P004-054	CONDENSATE RECEIVER TEMP	12-27-84	QUALIFIED	
TE-P120-001	Liquid TEMP-BWST	12-27-84	QUALIFIED	
TE-P120-041	Liquid TEMP-ECCS ACCUM A	01-03-85	QUALIFIED	INITIAL CONDITIONS ONLY
TE-P120-102	Liquid TEMP-ECCS LPIS HK & OUTLET	12-27-84	QUALIFIED	
TE-P139-019	TEMPERATURE-PRESSURIZER VAPOR	12-31-84	QUALIFIED	INITIAL CONDITIONS ONLY
TE-P139-020	TEMPERATURE-PRESSURIZER LIQUID	12-31-84	QUALIFIED	INITIAL CONDITIONS ONLY
TE-P139-029	COOLANT TEMP-INTACT LOOP COLD LEG	12-27-84	QUALIFIED	INITIAL CONDITIONS ONLY
TE-P139-28-2	TEMPERATURE-INTACT LOOP COLD LEG	12-27-84	QUALIFIED	INITIAL CONDITIONS ONLY

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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
TE-P139-32-1	PRIMARY COOLANT HOT LEG TEMP CHAN A 12-27-84	12-27-84	QUALIFIED	INITIAL CONDITIONS ONLY
TE-P141-094	PCCS HEAT EXCH ML TEMP	12-27-84	QUALIFIED	
TE-P141-095	WATER TEMP-COLD LEG OF PCC LOADS	12-27-84	QUALIFIED	
TE-SG-001A	COOLANT TEMP-IL SG INLET PLENUM	01-03-85	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-SG-001	COOLANT TEMP-IL SG INLET PLENUM	12-31-84	FAILED	
TE-SG-002A	COOLANT TEMP-IL SG OUTLET PLENUM	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-SG-002	COOLANT TEMP-IL SG OUTLET PLENUM	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-SG-003	LIQUID TEMP-SCS SG DOWNCOMER	12-27-84	FAILED	
TE-SG-004	LIQUID TEMP-SCS SG DOWNCOMER	12-27-84	QUALIFIED	
TE-SV-001	LIQUID TEMP-BST STALK 1-107.2	12-27-84	QUALIFIED	
TE-SV-006	LIQUID TEMP-BST STALK 1-14.7	12-27-84	QUALIFIED	
TE-SV-007	LIQUID TEMP-BST STALK 2-107.2	12-27-84	QUALIFIED	
TE-SV-011	LIQUID TEMP-BST STALK 2-39.0	12-27-84	QUALIFIED	

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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
TE-SV-012	LIQUID TEMP-BST STALK 2-14.7	12-27-84	QUALIFIED	
TE-T055-002	TEMPERATURE-CONTAINMENT AMBIENT	12-27-84	QUALIFIED	NO OTHER MEASUREMENT FOR DIRECT COMPARISON
TE-1A11-030	TEMP-CLADDING/FA1 PIN A18 30 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-1B10-037	TEMP-CLADDING/FA1 PIN B10 37 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-1B11-028	TEMP-CLADDING/FA1 PIN B11 28 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-1B11-032	TEMP-CLADDING/FA1 PIN B11 32 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-1C11-021	TEMP-CLADDING/FA1 PIN C11 21 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-1C11-039	TEMP-CLADDING/FA1 PIN C11 39 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-1F07-015	TEMP-CLADDING/FA1 PIN F7 15 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-1F07-026	TEMP-CLADDING/FA3 PIN F7 .26 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-1ST-001	COOLANT TEMP-RV INSTR STALK 1 DC	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1ST-002	COOLANT TEMP-RV INSTR STALK 1 DC	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1ST-003	COOLANT TEMP-RV INSTR STALK 1 DC	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS

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FP-1 FINAL DIRC QUALIFICATION REPORT

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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
TE-1ST-004	COOLANT TEMP-RV INSTR STALK 1 DC	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1ST-005	COOLANT TEMP-RV INSTR STALK 1 DC	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1ST-006	COOLANT TEMP-RV INSTR STALK 1 DC	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1ST-008	COOLANT TEMP-RV INSTR STALK 1 LP	12-27-84	FAILED	
TE-1ST-009	COOLANT TEMP-RV INSTR STALK 2 LP	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1ST-010	COOLANT TEMP-RV INSTR STALK 1 LP	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1ST-011	COOLANT TEMP-RV INSTR STALK 1 LP	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1ST-012	COOLANT TEMP-RV INSTR STALK 1 LP	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1ST-013	COOLANT TEMP-RV INSTR STALK 1 LP	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1ST-014	COOLANT TEMP-RV INSTR STALK 1 LP	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1ST-015	COOLANT TEMP-RV INSTR STALK 1 DC	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1UP-001	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1UP-002	COOLANT TEMP-UPPER END BOX	12-31-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS

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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
TE-IUP-005	COOLANT TEMP-ON DTC FE-IUP-1	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-IUP-006	METAL TEMP-SUPPORT COLUMN FA1	12-27-84	QUALIFIED	
TE-IUP-007	METAL TEMP-SUPPORT COLUMN FA1	12-27-84	QUALIFIED	
TE-2E08-045	TEMP-CLADDING/FAZ PIN E8 45 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-2F07-013	TEMP-CLADDING/FAZ PIN F7 15 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-2F08-032	TEMP-CLADDING/FAZ PIN F8 32 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-2F09-026	TEMP-CLADDING/FAZ PIN F9 26 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-2G14-011	TEMP-CLADDING/FAZ PIN G14 11 IN.	12-27-84	QUALIFIED	
TE-2G14-030	TEMP-CLADDING/FAZ PIN G14 30 IN.	12-27-84	QUALIFIED	
TE-2G14-049	TEMP-CLADDING/FAZ PIN G14 49 IN.	12-27-84	QUALIFIED	
TE-2H02-028	TEMP-CLADDING/FAZ PIN H2 28 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-2H13-021	TEMP-CLADDING/FAZ PIN H13 21 IN.	12-27-84	QUALIFIED	
TE-2H13-049	TEMP-CLADDING/FAZ PIN H13 49 IN.	01-03-84	QUALIFIED	



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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
TE-2H14-028	TEMP-CLADDING/FAZ PIN H14 20 IN.	12-27-84	QUALIFIED	
TE-2H14-032	TEMP-CLADDING/FAZ PIN H14 32 IN.	12-27-84	QUALIFIED	
TE-2H15-026	TEMP-CLADDING/FAZ PIN H15 26 IN.	12-27-84	QUALIFIED	
TE-2H15-041	TEMP-CLADDING/FAZ PIN H15 41 IN.	12-27-84	QUALIFIED	
TE-2I14-021	TEMP-CLADDING/FAZ PIN I14 21 IN.	12-27-84	QUALIFIED	
TE-2I14-039	TEMP-CLADDING/FAZ PIN I14 39 IN.	12-27-84	QUALIFIED	
TE-2LP-001	COOLANT TEMP-LOWER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-2LP-002	COOLANT TEMP-LOWER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-2LP-003	COOLANT TEMP-LOWER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-2UP-001	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-2UP-002	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-2UP-003	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-2UP-004	METAL TEMP-SUPPORT COLUMN FAZ	12-27-84	QUALIFIED	

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## FP-1 FINAL DIRC QUALIFICATION REPORT

EFFECTIVE DATE: 01/30/05  
REVISION: FINAL  
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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
TE-2UP-005	METAL TEMP-SUPPORT COLUMN FA2	12-27-84	QUALIFIED	
TE-3A11-030	TEMP-CLADDING/FA3 PIN A11 30 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-3B11-028	TEMP-CLADDING/FA3 PIN B11 20 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-3B11-032	TEMP-CLADDING/FA3 PIN B11 32 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-3C11-021	TEMP-CLADDING/FA3 PIN C11 21 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-3C11-039	TEMP-CLADDING/FA3 PIN C11 39 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-3F07-026	TEMP-CLADDING/FA3 PIN F7 26 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-3UP-001	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-3UP-006	METAL TEMP-SUPPORT COLUMN FA3	12-27-84	QUALIFIED	
TE-3UP-008	TEMP-COOLANT LLT ABOVE FA3	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-3UP-010	TEMP-COOLANT LLT ABOVE FA3	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-3UP-011	TEMP-COOLANT LLT ABOVE FA3	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-3UP-012	TEMP-COOLANT LLT ABOVE FA3	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS

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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
TE-3UP-013	TEMP-COOLANT LLT ABOVE FA3	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-3UP-014	TEMP-COOLANT LLT ABOVE FA3	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-3UP-015	TEMP-COOLANT LLT ABOVE FA3	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-3UP-016	TEMP-COOLANT LLT ABOVE FA3	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-4E08-045	TEMP-CLADDING/FA4 PIN E8 49 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-4F07-015	TEMP-CLADDING/FA4 PIN F7 15 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-4F08-032	TEMP-CLADDING/FA4 PIN F8 32 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-4G08-021	TEMP-CLADDING/FA4 PIN G8 21 IN.	12-27-84	QUALIFIED	
TE-4G14-011	TEMP-CLADDING/FA4 PIN G14 11 IN.	12-27-84	QUALIFIED	
TE-4G14-030	TEMP-CLADDING/FA4 PIN G14 30 IN	12-27-84	FAILED	
TE-4G14-045	TEMP-CLADDING/FA4 PIN G14 45 IN.	12-27-84	QUALIFIED	
TE-4H13-015	TEMP-CLADDING/FA4 PIN H13 15 IN.	12-27-84	QUALIFIED	
TE-4H13-037	TEMP-CLADDING/FA4 PIN H13 37 IN.	12-27-84	QUALIFIED	

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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
TE-5C10-032	TEMP-GUIDE TUBE FA5 LOC C10 32 IN	12-27-84	QUALIFIED	
TE-5E05-032	TEMP-GUIDE TUBE FA5 LOC E5 32 IN	12-27-84	QUALIFIED	
TE-5E07-026	TEMP-CLADDING/FA5 PIN E7 26 IN	12-27-84	QUALIFIED	
TE-5E07-032	TEMP-CLADDING/FA5 PIN E7 32 IN	12-27-84	QUALIFIED	
TE-5E07-039	TEMP-CLADDING/FA5 PIN E7 39 IN	12-27-84	QUALIFIED	
TE-5E07-043	TEMP-CLADDING/FA5 PIN E7 43 IN	12-27-84	QUALIFIED	
TE-5E09-005	TEMP-CLADDING/FA5 PIN E9 5 IN	12-27-84	QUALIFIED	
TE-5E09-010	TEMP-CLADDING/FA5 PIN E9 10 IN	12-27-84	QUALIFIED	
TE-5E09-016	TEMP-CLADDING/FA5 PIN E9 16 IN	12-27-84	QUALIFIED	
TE-5E09-021	TEMP-CLADDING/FA5 PIN E9 21 IN	12-27-84	QUALIFIED	
TE-5F03-045	TEMP-GUIDE TUBE FA5 LOC F3 45 IN	12-27-84	QUALIFIED	
TE-5F13-068	TEMP-GUIDE TUBE FA5 LOC F13 68 IN	12-27-84	QUALIFIED	
TE-5G05-027	TEMP-CLADDING/FA5 PIN G5 27 IN	01-03-85	QUALIFIED	

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## FP-1 FINAL DIRC QUALIFICATION REPORT

EFFECTIVE DATE: 01/30/85  
REVISION: FINAL  
SYSTEM: LOCE FP-1

MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S) <sup>1</sup>
TE-5608-006	TEMP-CLADDING/FA3 PIN G8 6 IN	12-27-84	QUALIFIED	
TE-5608-012	TEMP-CLADDING/FA3 PIN G8 12 IN	12-27-84	QUALIFIED	
TE-5608-029A	TEMP-CLADDING/FA3 PIN G8 29 IN	12-27-84	QUALIFIED	
TE-5608-029B	TEMP-CLADDING/FA3 PIN G8 29 IN	12-27-84	QUALIFIED	
TE-5G11-027	TEMP-CLADDING/FA3 PIN G11 27 IN	12-27-84	QUALIFIED	
TE-5I05-027	TEMP-CLADDING/FA3 PIN I9 27 IN	12-27-84	QUALIFIED	
TE-5I11-027	TEMP-CLADDING/FA3 PIN I11 27 IN	12-27-84	QUALIFIED	
TE-9J13-043	TEMP-GUIDE TUBE FA3 LOC J13 43 IN	12-27-84	QUALIFIED	
TE-5K07-048	TEMP-CLADDING/FA3 PIN K7 48 IN	12-27-84	FAILED	
TE-5K07-055	TEMP-CLADDING/FA3 PIN K7 55 IN	12-27-84	QUALIFIED	
TE-5K07-060	TEMP-CLADDING/FA3 PIN K7 60 IN	12-27-84	QUALIFIED	
TE-5K07-065	TEMP-CLADDING/FA3 PIN K7 65 IN	12-27-84	QUALIFIED	
TE-5K09-021	TEMP-CLADDING/FA3 PIN K9 21 IN	12-27-84	QUALIFIED	

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## FP-1 FINAL DIRC QUALIFICATION REPORT

EFFECTIVE DATE: 01/30/85  
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SYSTEM: LOCE FP-1

MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
TE-5K09-026	TEMP-CLADDING/FA5 PIN K9 26 IN	12-27-84	QUALIFIED	
TE-5K09-032	TEMP-CLADDING/FA5 PIN K9 32 IN	12-27-84	QUALIFIED	
TE-5K09-039	TEMP-CLADDING/FA5 PIN K9 39 IN	12-27-84	QUALIFIED	
TE-5L08-032	TEMP-GUIDE TUBE FA5 LOC L0 32 IN	12-27-84	QUALIFIED	
TE-5M06-045	TEMP-GUIDE TUBE FA5 LOC M6 45 IN	12-27-84	QUALIFIED	
TE-5M10-066	TEMP-GUIDE TUBE FA5 LOC M10 66 IN	12-27-84	QUALIFIED	
TE-5UP-004	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-5UP-005	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-5UP-006	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-5UP-007	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-5UP-009	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-5UP-011	COOLANT TEMP-UPPER END BOX	12-31-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-5UP-012	COOLANT TEMP-UPPER END BOX	12-31-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS

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## FP-1 FINAL DIRC QUALIFICATION REPORT

EFFECTIVE DATE: 01/30/85  
REVISION: FINAL  
SYSTEM: LOCE FP-1

MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
TE-5UP-021	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-5UP-022	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-5UP-171A	METAL SURFACE TEMPERATURE UPPER END	12-27-84	QUALIFIED	
TE-5UP-171B	METAL SURFACE TEMPERATURE UPPER END	12-27-84	QUALIFIED	
TE-5UP-194	METAL SURFACE TEMPERATURE UPPER END	12-27-84	QUALIFIED	
TE-5UP-212	METAL SURFACE TEMPERATURE UPPER END	12-31-84	QUALIFIED	
TE-5UP-250	METAL SURFACE TEMPERATURE UPPER END	12-27-84	QUALIFIED	
TE-6E08-043	TEMP-CLADDING/FA6 PIN E8 49 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-6F07-037	TEMP-CLADDING/FA6 PIN F7 37 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-6F09-041	TEMP-CLADDING/FA6 PIN F9 41 IN.	01-03-84	QUALIFIED	
TE-6G08-039	TEMP-CLADDING/FA6 PIN G8 39 IN.	12-27-84	QUALIFIED	
TE-6G14-011	TEMP-CLADDING/FA6 PIN G14 11 IN.	12-27-84	QUALIFIED	
TE-6G14-030	TEMP-CLADDING/FA6 PIN G14 30 IN.	12-27-84	QUALIFIED	

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## FP-1 FINAL DIRC QUALIFICATION REPORT

EFFECTIVE DATE: 01/30/85  
REVISION: FINAL  
SYSTEM: LOCE FP-1

MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
TE-6G14-045	TEMP-CLADDING/FA6 PIN G14 45 IN.	01-03-85	QUALIFIED	
TE-6H13-015	TEMP-CLADDING/FA6 PIN H13 15 IN.	12-27-84	QUALIFIED	
TE-6H13-037	TEMP-CLADDING/FA6 PIN H13 37 IN.	12-27-84	QUALIFIED	
TE-6H14-028	TEMP-CLADDING/FA6 PIN H14 28 IN.	12-27-84	QUALIFIED	
TE-6H14-032	TEMP-CLADDING/FA6 PIN H14 32 IN.	12-27-84	QUALIFIED	
TE-6H15-026	TEMP-CLADDING/FA6 PIN H15 26 IN.	01-03-85	QUALIFIED	
TE-6I14-021	TEMP-CLADDING/FA6 PIN I14 21 IN.	12-27-84	QUALIFIED	
TE-6I14-039	TEMP-CLADDING/FA6 PIN I14 39 IN.	12-27-84	QUALIFIED	
TE-6LP-001	COOLANT TEMP-LOWER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-6LP-002	COOLANT TEMP-LOWER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-6LP-003	COOLANT TEMP-LOWER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-6UP-001	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-6UP-002	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS

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15.52.31

## FP-1 FINAL DIRC QUALIFICATION REPORT

EFFECTIVE DATE: 01/30/85  
REVISION: FINAL  
SYSTEM: LOCE FP-1

MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
TE-6UP-003	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-6UP-004	METAL TEMP-SUPPORT COLUMN FA5	12-27-84	QUALIFIED	
TE-6UP-005	METAL TEMP-SUPPORT COLUMN FA5	12-27-84	QUALIFIED	
TT-P004-004	LIQUID TEMP-SCS FEEDWATER	12-27-84	QUALIFIED	
TT-P120-062	LIQUID TEMP-ECCS CL INJECT POINT	01-03-84	QUALIFIED	RESPONSE LIMITED
TT-P139-032	COOLANT TEMP-INTACT LOOP HOT LEG	12-27-84	QUALIFIED	INITIAL CONDITIONS ONLY
TT-P139-033	COOLANT TEMP-INTACT LOOP HOT LEG	12-27-84	QUALIFIED	INITIAL CONDITIONS ONLY
TT-P139-034	COOLANT TEMP-INTACT LOOP HOT LEG	12-27-84	QUALIFIED	INITIAL CONDITIONS ONLY

**TABLE 3.2. Input deck listing for plant steady state**

\*\*\*\*\*  
\* LEFT POST-TEST LP-FP-1 STEADY STATE DECK FOR TRAC-PF1/MOD1  
\* DATA BASED ON L2-3 DECK FROM LANL FOR TRAC-PF1/MOD1 AND ON  
\* L8-1 DECK FROM AEE-WINFRITH, CHANGED TO FP-1, AUGUST 85  
\* CHANGES ALREADY IN TRAC-PF2-DECK: UPPER PLENUM ECOS, INNER CORE  
\* RING FA-R=0.0 (FLOW SHROUND), BLCL VALVE  
\* ADDITIONAL CHANGES: CORE 131 MM LOWER  
\* HOT RDS IN CELL 1,2,3,4,8,12  
\* BYPASS LOWER PLENUM - UPPER PLENUM => 4 TEES (PATH 1,2,6+GUIDE TUBES),  
\* BYPASS UPPER PLENUM - DOWNCOMER => FA-R IN LEVEL 11 (PATH 3,4,5),  
\* BYPASS KADV (INCREASED),  
\* CPJAR, RDX => RING AREAS,  
\* ENVIRONMENTAL HEAT LOSSES, HTC JUT: PCS PIPING = 6.0 W/M²K  
\* PRESSURIZER = 2.0 W/M²K  
\* SG SEC. SIDE = 1.6 W/M²K  
\* CHANGES INCORPORATED 19.9.86:  
\* PCS F-D, RESISTANCE REDUCED, RESISTANCE ADDED FOR LP-CORE,CORE,CORE-UP  
\* TWO-WAY FRICTION FACTORS USED FOR PCS, FPIKCO NOT ALLOWED  
\* CHANGES TO VESSEL FLUID VOLUME AND FLOW AREA FRACTIONS  
\* CHANGES IN VESSEL HEAT SLABS  
\* NFF RESET TO 1  
\* \*\*\*\*\*

\*\*\*\*\*  
\* INVPTS ICFLUX=2, LHM12=1.0, CHM22=0.84, NOAIR=0, ICENDM3=1, NLT=18,  
\* 1\*FP=3, NFCC1=2,  
\* 1\*FP=3  
\* \*\*\*\*\*

\*\*\*\*\*  
\* \*\*\*\*\*MAIN CONTROL CARDS\*\*\*\*\*  
\* 0 0.0 \*NCOMP\* 53 \*NJUN\* 63 1 \*MCC 01  
\* 1 0 \*NCOMP\* 53 \*NJUN\* 63 1 \*MCC 02  
\* 5.0E-4 5.0E-6 1.0E-5 1.0E-1 1 \*MCC 03  
\* 10 50 25 1 \*MCC 04  
\* #NTSV# 3 \*NTCH# 0 \*NTCF# 0 \*NTRP# 10 \*NTCP# 1 \*MCC 05  
\* 1 2 3 4 55 \*COMP  
\* 5 7 8 935 \*COMP  
\* 23 24 255 \*COMP  
\* 11 12 135 \*COMP  
\* 14 15 16 17 315 \*COMP  
\* 32 41 42 50 435 \*CUMP  
\* 31 92 53 84 855 \*CUMP  
\* 95 67 68 89 905 \*COMP  
\* 91 92 61 52 635 \*COMP  
\* 54 55 66 57 685 \*CUMP  
\* 99 70 71 72 1015 \*COMP  
\* 102 103 104E \*COMP  
\* \*\*\*\*\*

\*\*\*\*\*  
\* SIGNAL VARIABLE DATA\*\*\*\*\*  
\* IDSY ISV4 ILCN ILCN1 ILCV2  
\* 1 0 0 0 0 \* PROBLEM TIME SV01  
\* 2 25 50 1005 4006 \* RUD TEMPERATURE SV02  
\* 3 71 12 2 0 \* RPIS PRESSURE SV03  
\* \*\*\*\*\*

\*\*\*\*\*CONTROL BLOCK DATA\*\*\*\*\*

\*\*\*\*\*TRIP DATA\*\*\*\*\*

\* VTSE NTCT NTSF NTDP NTSD  
\* 0 0 0 0 0 \*TRIP DI

\* TRIP 2 - ECC RPIS (16)

\* IOTP ISRT ISET ITST IDSG  
\* 2 2 0 1 1 \*TRIP02  
\* 0.0 517.0 \*TRIP02  
\* 0.0 0.0 \*TRIP02  
\* 0 0 \*TRIP02

\* TRIP 3 - ECC LPIS (17) (COLD LEG ACCUMULATOR)

3	2	0	1	1	*TRIP03 *TRIP03 *TRIP03 *TRIP03	
	0.0	346.0				
	0.0	0.0				
	0	0				
*	TRIP 4 - PJMPS (4 & 5)					
4	2	0	1	1	*TRIP04 *TRIP04 *TRIP04 *TRIP04	
	0.0	2.00				
	0.0	0.0				
	0	0				
*	TRIP 5 - STEAM GENERATOR FEEDWATER (24)					
5	2	0	1	1	*TRIP05 *TRIP05 *TRIP05 *TRIP05	
	0.0	1.0E-5				
	0.0	0.0				
	0	0				
*	TRIP 5 - ECC LINE VALVE (14)					
6	2	0	1	1	*TRIP06 *TRIP06 *TRIP06 *TRIP06	
	0.0	10000.0				
	0.0	0.0				
	0	0				
*	TRIP 7 - STEAM LINE VALVE (23)					
7	2	0	1	1	*TRIP07 *TRIP07 *TRIP07 *TRIP07	
	0.0	0.0				
	0.0	0.0				
	0	0				
*	TRIP 1010 - J. PLENUM INJECTION SYSTEM (61 BIS 72)					
1010	2	0	1	1	*TRIP1010 *TRIP1010 *TRIP1010 *TRIP1010	
	0.0	1.0E-5				
	0.0	0.0				
	0	0				
*	TRIP 100 - REACTOR SCRAM VESSEL (50)					
100	2	0	1	1	*TRIP100 *TRIP100 *TRIP100 *TRIP100	
	0.0	1.0E-5				
	0.0	0.0				
	0	0				
*	TRIP 101 - RELOAD FINE-MESH TRIP FOR VESSEL (50)					
101	2	0	1	1	*TRIP101 *TRIP101 *TRIP101 *TRIP101	
	0.0	1.0E-5				
	0.0	0.0				
	0	0				
*	TRIP 200 - BROKEN LOOP COLD LEG VALVE (43)					
200	2	0	1	1	*TRIP200 *TRIP200 *TRIP200 *TRIP200	
	0.0	63.5				
	0.0	0.0				
	0	0				
*****COMMONENT DATA*****						
*	NOTE THAT COMPONENT , JUNCTION AND TRIP NUMBERS ARE GIVEN.					
*	1. TEE	1	1,2,10	INTACT-LOOP HOT LEG		
*	2. STGEN	2	2,3 - P	STEAM GENERATOR		
*			22,25 - S EXTERNAL			
*			21,23,24 - S INTERNAL			
*	3. VALVE	23	22,26 7	STEAM-LINE VALVE		

*	4.	FILL	24	70		STEAM-GENERATOR FEEDWATER STEAM-GENERATOR VENT
*	5.	BREAK	25	26		
*	6.	TEE	3	4,5,3		PUMP SUCTION
*	7.	PUMP	4	4,6	4	PUMP VO. 2
*	8.	PUMP	5	5,7	4	PUMP VO. 1
*	9.	TEE	5	7,8,6		PUMP DISCHARGE
*	10.	TEE	7	8,9,14		INTACT-LOOP COLD LEG
*	11.	PRIZER	6	10,43		PRESSURIZER
*	12.	FILL	23	93		PRESSURISER OUTLET
*	13.	FILL	11	11		ACCUMULATOR OUTLET
*	14.	TEE	12	15,14,18		ECC LINE - HPIS
*	15.	TEE	13	15,15,19		ECC LINE - LPIS
*	15.	VALVE	14	17,15	6	ECC LINE - CHECK VALVE
*	17.	PIPE	15	17,11		ACCUMULATOR
*	18.	FILL	16	16	2	HPIS INJECTION
*	19.	FILL	17	19	3	LPIS INJECTION
*	20.	TEE	31	31,32,43		BROKEN-LOOP HOT LEG
*	21.	FILL	32	32		BROKEN-HOT-LEG TERMINAL
*	22.	TEE	41	41,44,43		BROKEN-LOOP COLD LEG
*	23.	FILL	42	42		BROKEN-COLD-LEG TERMINAL
*	24.	VESSEL	50	1,9,31,41,81,82, 83,84,85,86,87, 88,89,90,91,92, 101-112		100,101 VESSE-
*	25.	VALVE	43	44,42	200	BROKEN-LOOP COLD LEG VALVE
*	25.	PIPE	91	81,61		U.PLENUM INJECTION SYSTEM
*	27.	FILL	61	61	1010	U.PLENUM INJECTION SYSTEM
*	28.	PIPE	92	82,52		U.PLENUM INJECTION SYSTEM
*	29.	FILL	62	52	1010	U.PLENUM INJECTION SYSTEM
*	30.	PIPE	93	83,63		U.PLENUM INJECTION SYSTEM
*	31.	FILL	63	63	1010	U.PLENUM INJECTION SYSTEM
*	32.	PIPE	94	84,64		U.PLENUM INJECTION SYSTEM
*	33.	FILL	64	64	1010	U.PLENUM INJECTION SYSTEM
*	34.	PIPE	95	85,55		U.PLENUM INJECTION SYSTEM
*	35.	FILL	65	65	1010	U.PLENUM INJECTION SYSTEM
*	36.	PIPE	96	86,66		U.PLENUM INJECTION SYSTEM
*	37.	FILL	66	66	1010	U.PLENUM INJECTION SYSTEM
*	38.	PIPE	97	87,67		U.PLENUM INJECTION SYSTEM
*	39.	FILL	67	67	1010	U.PLENUM INJECTION SYSTEM
*	40.	PIPE	98	88,68		U.PLENUM INJECTION SYSTEM
*	41.	FILL	68	68	1010	U.PLENUM INJECTION SYSTEM
*	42.	PIPE	99	89,69		U.PLENUM INJECTION SYSTEM
*	43.	FILL	69	69	1010	U.PLENUM INJECTION SYSTEM
*	44.	PIPE	90	90,70		U.PLENUM INJECTION SYSTEM
*	45.	FILL	70	70	1010	U.PLENUM INJECTION SYSTEM
*	46.	PIPE	91	91,71		U.PLENUM INJECTION SYSTEM
*	47.	FILL	71	71	1010	U.PLENUM INJECTION SYSTEM
*	48.	PIPE	92	92,72		U.PLENUM INJECTION SYSTEM
*	49.	FILL	72	72	1010	U.PLENUM INJECTION SYSTEM
*	50.	TEE	101	101,105,109		CORE BYPASS
*	51.	TEE	102	102,106,110		CORE BYPASS
*	52.	TEE	103	103,107,111		CORE BYPASS
*	53.	TEE	104	104,108,112		CORE BYPASS

\*\*\*\*\*COMPONENT DATA\*\*\*\*\*

\*\*\*\*\*

TEE	1	1 INTACT-LOOP HOT LEG
4	4	0.0 *ICHF* 1

MAIN TUBE

0	3	1	2	0	*CN03
0	0	0	0	0	*CN04
0.14209	0.03571	6.0	5.0	300.0	*CN05
300.0	0.0	0.0	1.0E20	1.0	*CN06
0.0	0.0	1.0E20	1.0		*CN07
					*CN08
* SIDE TUBE					
"					
0	3	10	0		*CN09
0	0	0	0	0	*CN10
0.0233005	0.0086958	6.0	5.0	300.0	*CN11
300.0	0.0	0.0	1.0E20	1.0	*CN12
0.0	0.0	1.0E20	1.0		*CN13
					*CN14
* MAIN TUBE					
"					
P 2	7.83555E-1	4.92583E-1	7.75839E-1S	*DX	
	1.19914E+0	8.65752E-1	4.17949E-1S		
	4.25924E-1F				
P 2	5.03932E-2	3.20623E-2	5.04912E-2S	*VJL	
	5.05917E-2	5.52799E-2	3.13808E-2S		
	5.21381E-2F				
P 5	5.34253E-2	6.34253E-2	5.34253E-2S	*FA	
	6.34253E-2	5.15000E-2F			
	0.0F 5	0.0	7.52500E-2S	*FRIC VSL-HL FF=-0.28	
	0.0	1.70400E-1E		*FRIC HL-SG FF=0.1704	
	0.0310R 5	0.0	7.52500E-2S	*FRIC REV	
	0.0	1.70400L-1E		*FRIC REV	
P 9	0.0	5.89737E-1E		*GRAV	
Q 7	2.84000E-1	2.84000E-1	2.56300E-1E	*HD	
F	0E			*ICFLG	
F	1E			*NFF	
F	0.0F			*ALP	
F	0.0E			*VL	
F	0.0F			*VV	
F	578.4E			*TL	
F	515.0E			*TV	
F	148.4E+5E			*P	
F	0.0F			*PA	
F	0.0F			*OPPP	
F	7E			*MATID	
F	593.0F			*TD	
				*CJNC	
				*S	
				*PJWTF1	
				*PJWRF1	
				*OP3TBF1	
				*OP3RBF1	
*					
* SIDE TUBE					
"					
P 3	2.14984E+0	2.64277E+0	2.22169E+0E	*DX	
	3.11497E-3	3.59537E-3	5.70588E-3E	*VJL	
F 3	1.44927E-3	5.73212E-3E		*FA	
	1.65249E-1	5.50315E-3P 2	4.66877E-3F	*FRIC	
	1.65298E-1	5.50315E-3R 2	4.66877E-3E	*FRIC REV	
	5.45100E-1R 2	0.0	6.04100E-1E	*GRAV	
P 3	4.29558E-2	8.54304E-2E		*HD	
F	0E			*ICFLG	
F	1F			*NFF	
F	0.0F			*ALP	
F	0.0F			*VL	
F	0.0E			*VV	
F	578.4F			*TL	
F	515.0F			*TV	
F	148.4E+5E			*P	
F	0.0F			*PA	
F	0.0F			*OPPP	

F 7E  
= 173.0F

\*MATERIAL  
\*TA  
\*CJYC  
\*S  
\*P3WTR1  
\*P3ARF1  
\*P3TR1  
\*P3RF1

\*-----  
\* TO MAKE THIS DATA CONSISTENT AT JUNCTION 2  
\* THE FOLLOWING CHANGES HAVE BEEN MADE  
\* FRIIC : CHANGED FROM 0.1183 TO 0.19258  
\* GRAV : CHANGED FROM 0.4237 TO 0.589737  
\* THE NEW VALUES ARE GIVEN IN COMPONENT 1 FROM TRAC-PD2 L31 DECK  
\*

STCEN	C	2 STEAM GENERATOR	9	*CN 02
-	10	4 3		
	0	2 3		*CN 03
	0	25 22		*CN 04
	0	0 0.000000		*CN 05
	0	5		*CN 06
	17	4		*CN 07
	5.10540E-3	1.24460E-3		*CN 08
PIPE	5	0		*SECONDARY PIPE 20
TEE	4	1		*DOWNCOMER TEE 22
TEE	2	1		*STEAM DOME TEE 21
*-----PRIMARY SIDE				
	3.63500E-1F08	5.56950E-1	9.63600E-1E	*DX
	3.79500E-1F08	5.59500E-2	3.79500E-1E	*VOL
	5.15000E-2F09	1.51100L-1	5.16000E-2F	*FA
	0.17040	R04 0.000000	0.136100E	*FRIC
	0.17040	R04 0.000000	0.186100E	*FRIC P RE
	0.589737 R04	1.000000	0.000000R04 -1.000000	-0.711600E *GRAV
	2.55300E-1F09	1.02110L-2	2.56000E-1E	*HD
F	OF			*ICFLG
	1F09	1	1E	*NFF
F	0.000000E			*ALP
F	0.000000F			*VL
F	0.000000F			*VV
IU	567.500000	552.800000E		*TL
IU	567.500000	552.800000E		*TV
F	14.8400E+6F			*P
F	0.000000F			*PA
*-----SECONDARY SIDE				
	24	21 0	20	*PIPE 20
P04	5.56950E-1	1.11150E+0E		*DX
P04	4.43562E-1	9.97863L-1E		*VOL
	2.18898E-1F03	7.79615L-1F02	5.37762E-1E	*FA
	2.000000P05	0.000000E		*FRICF
	2.000000P05	0.000000E		*FRICK
	0.000000P05	1.00000E+0E		*GRAV
P05	5.35000E-3	1.06910L+0E		*HD
F	OF			*ICFLG
F	1E			*NFF
R04	0.000000	0.258500E		*ALP
F	0.000000E			*VL
F	0.000000E			*VV
F	549.000000F			*TL
F	549.000000F			*TV
F	5.4100E+6E			*P
F	0.000000F			*PA
*-----				
	23	24 25	22	*TEE 22
R02	7.41000E-1	1.70685E+0	5.68950E-1E	*DX
F02	3.82965E-1	3.73532E-1	1.24544E-1E	*VOL
F02	5.15342E-1F03	2.18998E-1E		*FA
R04	0.000000	2.000000E		*FRICF
F04	0.000000	2.000000F		*FRICK
	-3.37524E-1F03	-1.000000	0.000000E	*GRAV
F02	2.54200E-1F02	1.01600E-1	6.35000E-3F	*HD

F 1F  
 F 1.000000 0.746734E02 0.000000F  
 F 0.000000F  
 F 0.000000E  
 F 541.571343E  
 F 541.571343E  
 F 6.4100E+6E  
 F 0.000000F  
 F 0.000000  
 F 2.000000F  
 F 1.52146E-2E  
 F 9.10732E-3E  
 F 0.000000E  
 F 0.000000F  
 F 0.000000E  
 F 1.01500E-1F  
 F UF  
 F 1F  
 F 0.000000F  
 F 0.000000E  
 F 0.000000F  
 F 525.000000E  
 F 525.000000E  
 F 6.4100E+6E  
 F 0.000000F  
 F-----  
 21 22 23 21 \*TEE 21  
 F 1.11157E+0F 1.23695E+0E 4.63242E-2E  
 F 9.07867E-1 1.58904E+0 2.44600E-1E  
 F 8.97762E-1 0.000000 2.44600E-1E  
 F 0.000000 1.00000E+30 2.44600E-1E  
 F 1.000000E  
 R02 1.05910E+0 2.44600E-1E  
 F QE  
 F 1F  
 F 1.000000F  
 F 0.000000E  
 F 0.000000F  
 F 541.571343F  
 F 541.571343E  
 F 6.4100E+6F  
 F 0.000000E  
 F 0.000000  
 F 7.4100E-1E  
 F 3.82966E-1E  
 F 5.15342E-1F  
 F 0.000000E  
 F 0.000000F  
 F -3.37525E-1F  
 F 2.54000E-1E  
 F QE  
 F 1E  
 F 1.000000F  
 F 0.000000F  
 F 0.000000E  
 F 541.571343E  
 F 541.571343E  
 F 6.4100E+6E  
 F 0.000000F  
 F-----HFAT STRUCTURES  
 R03 0R05 0R06 20R04 22R02 21E \*ICMP  
 F 2 3 4 5 6 \*ICELL  
 F 7 6 9S \*ICELL  
 R03 1R02 10S 4R02 5 \*ICELL  
 F 1 2 3 4S \*ICELL  
 F 2 3E \*ICELL  
 R04 20R05 0R06 22R04 0R02 0E \*UCMP

	I	Z	3K02	4	J	
202	0	15			*UCELL	
	4P03	10K02	05		*UCELL	
P04	0P02	0E			*UCELL	
R24	12P06	4R03	6R06	95	*MATS	
R18	6P18	9F			*MATS	
P08	5.10540E-3	0.685800	5.10540E-3	10.000000	0.685800	*RADIG
	5.10540E-3R04	0.644525K02	0.57150P06	0.71120E		*RADIG
P08	1.24460E-3	0.0488900	5.18435E-3	0.031750	0.088400	*TH
	6.18435E-3P06	0.01270UR06	0.053975F			*TH
F	0.000000E					*UPPG
R32	541.571343P12	567.500000F04	552.300000R48	541.571343E		*TWGV
F	0.000000F					*HILG
F	0.000000E					*HIVG
F	0.000000E					*TILG
F	0.000000F					*TIVG
P08	33.848952	1.388600	17.287714	0.738780	1.388600	*WAIG
	17.287714R04	2.304050	2.550813	2.848255	2.214599	*WAIG
	3.311234	7.627232	2.542411	4.956850	4.407864E	*WAIG
P08	0.000000R02	1.600000	0.000000R02	1.600000R05	0.000000	*HOLG
R05	1.600000E					*HOLG
R08	0.000000R02	1.600000	0.000000R02	1.600000R05	0.000000	*H0VG
P05	1.600000F					*H0VG
R08	0.000000R02	305.370000	0.000000R02	305.370000R06	0.000000	*TOLG
P05	305.370000F					*TOLG
R08	0.000000F02	305.370000	0.000000R02	305.370000R06	0.000000	*TOVG
P05	305.370000F					*TOVG
F08	42.162876	1.568604	38.228926	0.738780	1.568504	*WAUG
	38.228926R04	2.349460	2.719942	2.911549	2.382671	*WAUG
	3.567533	8.206085	2.735362	5.343799	4.742394E	*WAUG

\* DATA CHANGED TO AGREE WITH CONTROL LOGIC IN FP-1  
 \* VALVE IS OPEN UNTIL TRIP COMES ON  
 \* THEN VALVE IS CLOSED USING A TABLE (TIME,RELATIVE POSITION)  
 \* . TRIP 7 , SV 1

VALVE	23	23 STEAM LINE VALVE		
6	0	22	26	7 *CN 02
1	0	3	5	0 *CN 03
7	1	6	0	0 *CN 04
0	0			*CN 05
1.0E+20	0.0	0.0	1.0	*CN 07
0.1214	0.0151	1.6	1.6	305.37 *CN 08
305.37	4.65292E-2	0.242900	0.451	*CN 09
F	5.01191F			*UX
F	2.3219E-1F			*VOL
F	4.63242E-2F			*FA
	0.2446 P04	0.0	5.49	*FRICF
	0.2445 P04	0.0	6.49	*FRICK
	1.0 R06	0.0E		*GRAV
F	0.7429E			*HD
P05	0	I	OF	*ICFLG
F	1E			*NFF
F	1.0 E			*ALP
F	0.0 E			*VL
F	0.0 E			*VV
F	541.571343E			*TL
F	541.571343F			*TV
R05	6.4900E+6	2.1500E+6E		*P
F	0.0 E			*PA
	0.0	0.451	1.0	*VMTB1
	2.0	0.350	5.0	*VMTB1
	7.5	0.0	1000.0	*VMTB1

\* MODIFIED TO AGREE WITH FP-1 DATA  
 \* CONSTANT MASS FLOW UNTIL TRIP ON  
 \* THEN "MASS FLOW READ FROM A TABLE(TIME,MASS FLOW)

\* TIP 5 . SV 1

FILL		24	24 STEAM GENERATOR FEEDWATER			
25	8	0				*CN 02
5	1	5	0	0		*CN ..
0.0	1.0E20	0.0				*CN ..
2.0	1.62146E-2	0.0	0.0	482.0	*CN 05	
57.E+5	0.0	12.800	0.0	482.0	*CN 06	
1.0	1.0					*CN 09
0.0	12.800	1.0	2.535			*VMTB
2.0	0.8101	2.67	0.005			*VMTB
500.	0.00E					*VMTB
<hr/>						
BREAK		25	25 STM GEN SEC BRK			
26	0	3	1	0	*CN 02	
5.011910	0.232198	1.0	488.0	21.5E5	*CN 04	
- 0.0	0.0	1.0E20	21.5E5	0.0	*CN 05	
<hr/>						
TEE		3	3 PUMP SUCTION			
2	4	7	0.0	*ICHF# 1		*CN02
<hr/>						
* MAIN TUBE						
..	0	3	4	5	0	*CN03
0	0	0	0	0	0	*CN04
0.14209	0.03571	6.0	6.0	300.0		*CN05
300.0	0.0	0.0	1.0E20	1.0		*CN06
0.0	0.0	1.0E20	1.0			*CN07
						*CN08
<hr/>						
* SIDE TUBE						
*	0	3	3	0		*CN09
*	0	0	0	0	0	*CN10
0.14209	0.03571	6.0	6.0	300.0		*CN11
300.0	0.0	0.0	1.0E20	1.0		*CN12
0.0	0.0	1.0E20	1.0			*CN13
*						*CN14
<hr/>						
* MAIN TUBE						
*	6.35000E-1	1.80340E+0	6.35000E-1E			*DX
F	2.74575E-2	1.14380E-1	2.74675E-2E			*VJL
F	3.65131E-2P	2 6.34249E-2	3.65131E-2E			*FA
F	0.0F					*FRICF
F	0.0E					*FRICR
F	-5.25590E-1	-5.52200E-1	5.52200E-1S			*GRAY
F	6.25590E-1F					
F	2.15910E-1P	2 2.94174E-1	2.15910E-1E			*IJ
F	0E					*ICFLG
F	1E					*NFF
F	0.0E					*ALP
F	0.0E					*V
F	0.0E					*VV
F	564.3E					*TL
F	615.0E					*TV
F	148.4E+5E					*P
F	0.0E					*PA
F	0.0E					*OPPP
F	7E					*MATID
F	593.0E					*TJ
						*CJYC
						*S
						*PJWTR1
						*PJWRF1
						*OP3TB1
						*OP3RF1
<hr/>						
* SIDE TUBE						
*						

1.31413E+11	2.02300E-16		*DX	
7.73710E-2	4.00000E-2	5.00481E-2E	*VJL	
2.534249E-2	5.97143E-2	5.16000E-2E	*FA	
2.3	0.0	1.86100E-1E	*FRIC FF=0.1861	
F 3	0.0	1.86100E-1E	*FRIC REV	
	0.0	6.74400E-1	*GRAV	
	7.11500E-1E			
D 2	2.94174E-1	2.95787E-1	2.55000E-1E	*HD
F	0F		*ICFLG	
F	1E		*NFF	
F	0.0E		*A_P	
F	0.0E		*VL	
F	0.0F		*VV	
F	564.3E		*TL	
F	615.0E		*TV	
F	148.4E+5E		*P	
F	0.0E		*PA	
F	-0.0E		*OPPP	
F	7E		*MATID	
F	593.0E		*TA	
			*CJNC	
			*S	
			*P3WTB1	
			*P3WRF1	
			*P3TB1	
			*P3RF1	

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PUMP	4	4	PUMP NU. 2			
2	4	4	6	7	*CN02	
*1CHFE	1	0	2	1	1	*CN03
	4	0	0	0	0	*CN04
	0	0	0	0	0	*CN05
0.107795	0.02858	6.0	6.0	300.0		*CN05
300.0	1.43	163.0	0.0			*CN07
941.54	500.0	0.315	614.0	369.561		*CN08
363.50	0.0	1.0E20	1.0	0		*CN09
0.0	0.0	1.0E20	1.0			*CN10

\* OPTION FOR LOFT PUMP DATA

\*  
2 \*CN11

\* ARPAY DATA CARDS

F	1.35213E+0E		*DX
F	4.95548E-2E		*VJL
F	3.65131E-2E		*FA
F	0.0E		*FRICF
F	0.0E		*FRICR
F	5.25590E-1R 2	0.0E	*GRAV
F	2.15910E-1E		*HD
F	0E		*ICFLG
F	1	0	*NFF
F	0.0F		*A_P
	0.0	6.77	*VL
	0.0	6.77	*VV
F	564.3E		*TL
F	615.0E		*TV
F	148.4E+5E		*P
F	0.0E		*PA
F	0.0E		*OPPP
F	7E		*MATID
F	593.0E		*TA
			*CJNC
			*S
			*PMPTR
			*PMPRF
			*P3TB
			*P3RF

\*\*\*\*\*

\* TEE JUNCTIONS 1 TO 5 THE SAME AS COMPONENT 4  
\* EXCEPT FOR THE JUNCTION NUMBERS IN CN02

PUMP	2	4	5	7	8	5 PUMP NO. 1	
*ICHF* 1	0	0	2	1	1		*CN02
	0	0	0	0	0		*CN03
	0	0	0	0	0		*CN04
	0	0	0	0	0		*CN05
0.10795	0.02858	6.0	6.0	300.0			*CN06
300.0	1.43	193.0	0.0				*CN07
941.54	500.0	0.315	614.0	369.551			*CN08
343.50	0.0	1.0E20	1.0	0			*CN09
0.0	0.0	1.0E20	1.0				*CN10

\* OPTION FOR LEFT PUMP DATA

-	2					*CN11
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\* A KRAY DATA CARDS

F	1.35213E+0E					*DX
F	4.75548E-2E					*VJL
F	3.66131E-2F					*FA
F	0.0E					*FRICF
F	0.0E					*FRICR
F	5.25590E-19	2	0.0E			*GRAV
F	2.15910E-1E					*HD
F	0F					*ICFLG
F	1	0	1E			*NFF
F	0.0E					*ALP
	0.0	6.77	0.0E			*V-
	0.0	5.77	0.0E			*VV
F	564.3E					*TL
F	515.0E					*TV
F	148.4E+5E					*P
F	0.0E					*PA
F	0.0F					*OPPP
F	7F					*MATID
F	573.0E					*TM
						*CNC
						*S
						*PYPTA
						*PYPRF
						*OP3TP
						*OP3RF

\*\*\*\*\*

TEE	2	4	6	7	8	6 PUMP DISCHARGE	
						0.0 *ICHF* 1	*CN02

\* MAIN TUBE

	0	2	7	8	0		*CN03
	0	0	0	0	0		*CN04
0.10795	0.02858	6.0	6.0	300.0			*CN05
300.0	0.0	0.0	1.0E20	1.0			*CN06
0.0	0.0	1.0E20	1.0				*CN07
							*CN08

\* SIDE TUBE

	0	1	6	0			*CN09
	0	0	0	0	0		*CN10
0.10795	0.02858	6.0	6.0	300.0			*CN11
300.0	0.0	0.0	1.0E20	1.0			*CN12
0.0	0.0	1.0E20	1.0				*CN13
							*CN14

\* MAIN TUBE

	1.30817E+0	1.11763E+0E					*DX
--	------------	-------------	--	--	--	--	-----

	4.73527E-2	6.53107E-2E		*VJL
R	2	3.65131E-2E	1	*FA
F	2	0.0	0.0E	*FRIC PS-CL FF=-0.12
R	2	0.0	0.0E	*FRIC REV FF=-0.12 ?
F		0.0F		*GRAV
F	2	2.15910E-1	2.84174E-1E	*H0
F		0E		*ICFLG
F		1E		*NFF
F		0.0F		*ALP
F		0.0F		*VL
F		0.0F		*VV
F		544.3E		*TL
F		615.0E		*TV
F		148.4E+5E		*P
F		0.0E		*PA
F		0.0E		*OPPP
F	-	7F		*MATID
F		593.0E		*TW
				*CJNC
				*S
				*POWTR1
				*PJWRF1
				*OP3TB1
				*OP3RF1

\* SIDE TUBE

	5.42920E-1E			*PX
F	2.54394E-2F			*VJL
F	3.65131E-2E			*FA
F	0.0E			*FRICF
F	0.0E			*FRICR
F	0.0E			*GRAV
F	2.15910E-1E			*H0
F	0E			*ICFLG
F	1F			*NFF
F	0.0E			*ALP
F	0.0E			*VL
F	0.0E			*VV
F	544.3E			*TL
F	615.0E			*TV
F	148.4E+5E			*P
F	0.0E			*PA
F	0.0F			*OPPP
F	7F			*MATID
F	593.0E			*TW
				*CJNC
				*S
				*PJWTF1
				*PJWRF1
				*OP3TB1
				*OP3RF1

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\*\*\*\*\*  
TEE 5 4 7 7 0.0 \*ICHF\* 1 \*CN02

\* MAIN TUBE

*	0	9	8	9	0	*CN03
*	0	0	0	0	0	*CN04
0.14209	0.03571	6.0	6.0	300.0		*CN05
300.0	0.0	0.0	1.0E20	1.0		*CN06
0.0	0.0	1.0E20	1.0			*CN07
						*CN08

\* SIDE TUBE

*	0	1	14	0		*CN09
*	0	0	0	0		*CN10
						*CN11

1.3416875	1.3116875	6.0	5.0	1.000		*CN12
1.000	0.0	0.0	1.0E20	1.0		*CN13
0.0	0.0	1.0E20	1.0			*CN14

\* MAIN TUBE

R3	0.192457	R3	0.236245	R3	0.455667	F	*DX
S3	0.324772	R3	0.3149136	R3	0.1295343	E	*VJL
F	0.0534240	E					*FA
	0.0	P8	0.0		0.20225	E	*FRIC CL-VSL FF=0.202
	0.0	R8	0.0		0.0	F	*FRIC VSL-CL FF=-0.266
F	0.0	E					*GRAV
F	0.234174	E					*HJ
F		UF					*ICFLG
C		1E					*NFF
S		0.0E					*ALP
F	-	0.0E					*VL
F		0.0E					*VV
F		5E4.3E					*TL
F		515.0E					*TV
F		148.9E+5F					*P
F		0.0E					*PA
F		0.0E					*OPPP
C		7E					*MATID
F		593.0E					*TD
							*CONC
							*S
							*PWTB1
							*POWRF1
							*QP3TBI
							*QP3RF1

\* SIDE TUBE

	1.50000E+0E						*DX
F	4.93381E-3F						*VJL
F	5.93320E-3E						*FA
	0.0	0.4441	E				*FRICF
	0.0	0.4441	E				*FRICR
	-1.00007E+0		0.0E				*GRAV
S	8.73252E-2E						*HJ
F		UF					*ICFLG
S		1E					*NFF
F		0.0E					*ALP
F		0.0E					*VL
F		0.0E					*VV
F		500.0E					*TL
F		515.0E					*TV
F		148.9E+5F					*P
F		0.0E					*PA
F		0.0E					*OPPP
F		7E					*MATID
F		500.0E					*TD
							*CONC
							*S
							*PWTB1
							*POWRF1
							*QP3TBI
							*QP3RF1

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\* NOTE THAT NODES=4 , CHANGED FOR FP-1 DECK (HEAT TRANSF. WALL-FIJID)

PRIZER		3		8 PRESSPRIZER		
	3	4	93	10	7	*CN02
PRIZER	1	0	0.0			*CN03
0.4262	0.075	2.0		2.0	300.0	*CN04
300.0	0.0	0.0		0.0	0.0	*CN05

\* EQUAY DATA

R	3.73717E-1	1.15790E+0	2.00000E-1F	*DX		
R	3.24860E-1	5.00000L-1	1.27700E-2E	*VJL		
R	3.555253E-1	5.73212E-3F		*FA		
R	3.0.0	4.56877E-3E		*FRICF		
R	3.0.0	4.66877E-3E		*FRICR		
R	3.-1.00000E+0	-5.0410L-1E		*GRAY		
R	3.4.48362E-1	0.54304E-2E		*HJ		
F	OF			*ICFLG		
F	1E			*NFF		
F	0.7174	0.0000	0.0E	*ALP		
F	0.0E			*VL		
F	0.0E			*VV		
F	614.3F			*TL		
F	614.3F			*TV		
F	148.4E+5	148.361E+5	148.223E+5E	*P		
F	0.0F			*PA		
F	0.0E			*OPPP		
F	7F			*MATID		
F	614.3F			*TA		
				*CJNC		
				*S		
*****						
* CONSTANT VELOCITY - SET TO ZERO						
*						
FILL	93	93	PRESSURISER OUTLET			
	93	1	0		*CN02	
	0.0	1.0E20	0.0	0.0	*CN03	
	4.609E-1	2.4414E-2	0.0	0.0	*CN04	
	148.4F+5	0.0	0.0	550.3	*CN05	
				550.3	*CN06	
					*CN07	
					*CN08	
					*CN09	
					*CN10	
*****						
* CONSTANT VELOCITY - SET TO ZERO						
*						
FILL	11	11	ACCUMULATOR TOP			
	11	1	0		*CN02	
	0.0	-1.0E20	0.0	0.0	*CN03	
	0.555	0.707	0.0	0.0	*CN04	
	43.0E5	43.0E5	0.0	0.0	*CN05	
				300.0	*CN06	
				300.0	*CN07	
					*CN08	
					*CN09	
					*CN10	
*****						
* NOTE THAT MODES=0 GIVING NO WALL-FLUID HEAT TRANSFER						
*						
TEE		12	12	ECC LINE - HPIS		
	1	0	7	0.0	0	*CN02
*						
* MAIN TUBE						
*						
	0	1	15	14	0	*CN03
	0.0436625	0.0134874	0.0	6.0	300.0	*CN04
	300.0	0.0	0.0	1.0E20	1.0	*CN05
						*CN06
						*CN07
						*CN08
*						
* SIDE TUBE						
*						
	0	1	18	0		*CN09
	0.0436625	0.0134874	0.0	6.0	300.0	*CN10
	300.0	0.0	0.0	1.0E20	1.0	*CN11
						*CN12
						*CN13
						*CN14

\* MAIN TUBE  
 \*  
 F 1.00000E+0F \*DX  
 F 5.93920E-3E \*VJL  
 F 5.99920E-3F \*FA  
 0.0 0.4941 E \*FRICF  
 0.0 0.4941 E \*FRICR  
 F 0.0E \*GRAY  
 F 8.73252E-2F \*HD  
 F 0E \*ICFLG  
 F 1E \*NFF  
 F 0.0F \*ALP  
 F 0.0F \*VL  
 F 0.0E \*VV  
 F 450.0F \*TL  
 F 615.0E \*TV  
 F 148.4E+5F \*P  
 F 0.0F \*PA  
 \*OPPP  
 \*MATID  
 \*TA  
 \*CJNC  
 \*S  
 \*PJWTR1  
 \*PJWRF1  
 \*QP3TB1  
 \*QP3RF1

\* SIDE TUBE

F 5.00000E+0E \*DX  
 F 4.53555E-3E \*VJL  
 F 9.07132E-4E \*FA  
 F 0.0E \*FRICF  
 F 0.0E \*FRICR  
 F 0.0E \*GRAY  
 F 3.39952E-2E \*HD  
 F 0F \*ICFLG  
 F 1E \*NFF  
 F 0.0E \*ALP  
 F 0.0E \*VL  
 F 0.0F \*VV  
 F 450.0F \*TL  
 F 615.0E \*TV  
 F 148.4E+5F \*P  
 F 0.0E \*PA  
 \*OPPP  
 \*MATID  
 \*TA  
 \*CJNC  
 \*S  
 \*PJWTR1  
 \*PJWRF1  
 \*QP3TB1  
 \*QP3RF1

\*\*\*\*\*  
\* NOTE THAT NODES=0 GIVING NO WALL-FLUID HEAT TRANSFER

TEE		13	13	ECC LINE - LPIS	
	1	0	7	0.0	0

\* MAIN TUBE

0	1	15	15	0	*CN03
0.0435625	0.0134874	6.0	5.0	300.0	*CN04
300.0	0.0	0.0	1.0E20	1.0	*CN05
					*CN06
					*CN07
					*CN08

3	J	J	Z	0		*CN03
5	L	Z	0	0		*CN04
2	0	0.0	0.0	0.0		*CN05
20.0	0.0	0.0	0.0	0.0		*CN06
4.36625E-2	1.34874E-2	6.0	6.0	300.0		*CN07
300.0	5.547E-2	2.636E-1	0.0	0.0		*CN08
						*CN09
						*CN10

\* ARRAY DATA

F	1.09220E+0E				*DX
F	2.61555E-2E				*VJL
F	3.29522E-2P	2	5.54700E-2E		*FA
0.013521	0.006551	44.5155	E	*FRICF	
0.013521	0.006551	44.5155	E	*FRICR	
-1.0E	2	0.0E		*GRAV	
2.04520E-1P	2	2.63600E-1E		*HJ	
F	0E			*ICFLG	
F	1E			*NFF	
F	0.0E			*ALP	
F	0.0E			*VL	
F	0.0F			*VV	
307.2	400.0E			*TL	
525.6	615.0E			*TV	
43.0E+5	148.4E+5E			*P	
F	0.0E			*PA	

0.0 1.0 10000.0 1.0 E

\*QPPP  
\*MATID  
\*TW  
\*CDNC  
\*S  
\*VTR1  
\*VTR2  
\*VRF  
\*OP3TR  
\*OP3RF

\*\*\*\*\*  
\* NOTE THAT VALUES=0 GIVING NO HALL-FLUID HEAT TRANSFER  
\* UNKNOWN VALUES FOR RADIJS AND THICKNESS OF PIPE

PIPE		15		15 ACCUMULATOR	
3	0	11	17	0	
1	0	1	0		
1.0	0.1	0.0	0.0	300.0	
300.0	0.0	0.0	1.0E20	1.0	

\*CN02  
\*CN03  
\*CN04  
\*CN05  
\*CN06  
\*CN07  
\*CN08

\* ARRAY DATA  

0.565	0.9316	1.12500E-2E		*DX
0.707	1.166	1.40777E-2E		*VJL
F 3 1.25135E+0	3.26522E-2E			*FA
R 3 0.0	0.013521	E		*FRICF
R 3 0.0	0.013521	E		*FRICR
F -1.0E				*GRAV
R 3 1.25954E+0	2.04520E-1E			*HJ
F 0F				*ICFLG
F 1E				*NFF
F 1.0	0.0	0.0E		*ALP
F 0.0E				*VL
F 0.0E				*VV
F 307.2E				*TL
F 307.2E				*TV
F 43.0E5		E		*P
F 43.0E5 R2 0.0	E			*PA
				*QPPP

\*MATERIAL  
 \*TA  
 \*CUNG  
 \*S  
 \*PDATA1  
 \*PWRF1  
 \*OP3TR1  
 \*OP3RF1

\* USES TRIP 2 AND SIGNAL VARIABLE 3  
 \* CONSTANT VELOCITY UNTIL TRIP ON THE PRESSURE-VELOCITY TABLE  
 \*

FILL 15 16 API5 INJECTION

18	7	0		*CN02
2	3	4	0	*CN03
0.0	1.0E20	0.0	0.0	*CN04
5.0	4.53556E-3	0.0	0.0	*CN05
1.0F+5	0.0	0.0	0.0	*CN06
			307.2	*CN07
			307.2	*CN08
1.0	1.0			*CN09
				*CN10

\* FILL TABLE - (PRESSURE,VELOCITY)  
 \* THIS IS FOR L2-3,LB-1 AND FP-1  
 \*

1.0000E+0	1.76554	0.85013E+5	1.76554S	*VMTB
83.589E+5	0.73564	1000.0E+5	0.73564E	

\* USES TRIP 3 AND SIGNAL VARIABLE 1  
 \* CONSTANT MASS FLOW UNTIL TRIP ON THE TIME-MASS FLOW TABLE  
 \*

FILL 17 17 ILCL ACCUMULATOR A INJECTION

19	8	0		*CN02
3	1	-13	0	*CN03
0.0	1.0E20	0.0	0.0	*CN04
1.0	5.98920E-3	0.0	0.0	*CN05
41.4F+5	0.0	0.0	0.0	*CN06
			303.0	*CN07
			303.0	*CN08
1.0	1.0			*CN09
				*CN10

\* FILL TABLE - (TIME,MASS FLOW)  
 \* FOR FP-1  
 \*

0.0	0.0	0.2	3.0 S	*VMTB
2.0	10.8	4.0	13.8 S	
6.0	15.6	8.0	15.8 S	
12.0	15.3	15.0	14.5 S	
28.0	13.6	52.0	11.0 S	
69.0	3.4	70.0	0.0 S	
1000.0E	0.0E			
78.0	9.6	100.0	8.5 S	
135.0	7.6	145.0	7.4 S	
1920.0	7.4E			

\* RENDERED AS USED IN L2/3 DECK FOR TRAC-PF1(MOD1)  
 \* IC4F=1  
 \*

TEE 31 31 BRUKEY-LJOP HOT LEG

2	4	7	0.0	1	*CN02
---	---	---	-----	---	-------

\*  
 \* MAIN TUBE  
 \*

0	26	31	32	0	*CN03
0	0	0	0	0	*CN04
0.14207	0.03571	6.0	6.0	300.0	*CN05
					*CN06

100.0	0.0	0.0	1.0E20	1.0	1.0	*CV07 *CV08
*						
* SIDE TYPE						
*						
0	3	43	0			*CV09 *CV10
0	0	0	0	0		*CV11
0.10795	0.02858	6.0	5.0	300.0		*CV12
300.0	0.0	0.0	1.0E20	1.0		*CV13
0.0	0.0	1.0E20	1.0			*CV14
*						
* MAIN TYPE						
*						
R 3 5.5998E-1	5.25780E-1	4.67490E-1	5.58510E-1	1.98750E+0S	*DX	
R 2 1.07720E+0	1.98750E+0	5.10290E-1	5.46290E-1	4.86280E-1S	*UX	
2.54000E-1	1.71450E-1	3.00000E-1	2.79400E-1R	2.11840E-1S	*UX	
R 4 0.19717	0.29922	0.244476	0.815976 E		*UX	
*						
R 3 4.24600E-2	4.72800E-3	3.75790E-3	4.55030E-3	1.96860E-1S	*VOL	
R 2 1.13330E-1	1.96860E-1	4.07280E-3	4.06350E-3	3.17150E-3S	*VOL	
2.75000E-2	1.85000E-2	1.89000E-2	5.85060E-3R	2.176670E-3S	*VOL	
R 4 0.0015574	0.002472	0.00204496	0.0423948 E		*VOL	
*						
R 3 5.34250E-2	1.39130E-2R	3 8.36470E-3P	3 1.91410E-2R	3 8.36470E-3S	*FA	
5.34250E-2R	2 7.46240E-3	5.34250E-2S			*FA	
R 9 P.35470E-3P1	5.19560E-2E				*FA	
*						
0.0 R 2 2.20351E-1	2.39561E-1	2.54000E-1		0.0S	*FRICF	
7.72000E-3P 3 1.40000E-2	1.93000E-2R	3 0.0	1.40000E-1S		*FRICF	
1.70000E-1 1.12000L-1R	2 0.0	4.39700E-2R4	0.0S		*FRICF	
0.019973R 0.347932 0.0 E					*FRICF	
0.035 R 2 2.20351E-1	2.39561E-1	2.54000E-1		0.0S	*FRICK	
7.72000L-3R 3 1.40000E-2	1.93000E-2R	3 0.0	1.40000E-1S		*FRICK	
1.70000E-1 1.12000E-1R	2 0.0	4.39700E-2R4	0.0S		*FRICKR	
0.018903R 0.347932 0.0 E					*FRICKR	
*						
P 5 0.0 6.21372L-1R	2 1.00000E+0		0.0R 5-1.00000E+0S		*GRAV	
-6.63354E-1P 2 0.0	2.9152RE-1S				*GRAV	
R 5 1.00000E+0 0.592407 P3	0.0E				*GRAV	
*						
R 3 2.84000L-1	1.33000E-1R	3 1.03000E-1R	3 1.75000E-2R	3 1.03000E-1S	*HD	
2.84000E-1P 2 1.14000E-2	2.84000E-1S				*HD	
R 9 1.03200E-1P1	2.57200E-1E				*HD	
*						
P25 U 2 OF						*ICFLG
F 1F						*NFF
F 0.0F						*ALP
F 0.0E						*VL
F 0.0E						*VV
*						
R 2 5.65500E+2	5.55120E+2	5.64770E+2	5.54450E+2	5.64070E+2S	*TL	
5.62730E+2	5.62000E+2	5.61280E+2	5.59930E+2	5.59590E+2S	*TL	
5.53220E+2	5.56890E+2	5.58720E+2	5.58600E+2	5.58400E+2S	*TL	
5.58210E+2	5.58070E+2	5.57920E+2	5.57800E+2	5.57670E+2S	*TL	
5.57550E+2	5.57420E+2S				*TL	
5.57270E+2	5.57100E+2	5.56760E+2E			*TL	
*						
F 615.0F						*TV
F 148.4E+5F						*P
F 0.0E						*PA
F 0.0E						*QPPP
= 7E						*MATID
*						
R 9 5.65500E+2P 4 5.65120L+2R	4 5.64770E+2P	4 5.64450E+2R	4 5.64070E+2S		*TW	
R 4 5.62730E+2P 4 5.62000E+2R	4 5.61280E+2R	4 5.59930E+2R	4 5.59590E+2S		*TW	
R 4 5.53220L+2P 4 5.56890E+2P	4 5.58720E+2R	4 5.58600E+2R	4 5.58400E+2S		*TW	
R 4 5.58210E+2P 4 5.58070L+2R	4 5.57920E+2R	4 5.57800E+2R	4 5.57670E+2S		*TW	
R 4 5.57550E+2P 4 5.57420E+2S					*TW	
R 4 5.57270E+2P 4 5.57100E+2R	4 5.56760E+2E				*TW	

\*CONC  
\*S  
\*POWTB1  
\*POWRF1  
\*OP3TB1  
\*QP3RF

\* SIDE TUBE

1.38700E+0	8.14000E-1	5.10440E+0E	*DX
5.40000E-2	3.14000E-2	1.98600E-1F	*VOL
3 3.8800E-2	3.3300E-03E		*FA
F 3 0.0	0.0E		*FRICF
D 3 0.0	0.0E		*FRICR
	2.24200E-1	1.91200E-1S	*GRAV
	0.0E		
F 3 2.22300E-1	65.200E-3E		*HD
F 0E			*ISFLG
F 1E			*NFF
F 0.0E			*ALP
F 0.0E			*VL
F 0.0E			*VV
F 565.5E			*TL
F 515.0E			*TV
F 148.4E+5F			*P
F 0.0E			*PA
F 0.0E			*OPPP
F 7E			*MATID
F 565.5E			*TA
			*CONE
			*S
			*POWTB1
			*POWRF1
			*OP3TB1
			*QP3RF1

\*-----  
\* CONSTANT VELOCITY - SET TO ZERO

\* FILL 32 32 BROKEN-HOT-LEG TERMINAL

32	1	0		*CN02
				*CN03
0.0	1.0E20	0.0	0.0	*CN04
0.815975	0.0423948	0.0	0.0	*CN05
148.4E+5	0.0	0.0	0.0	*CN06
				-*CN07
				*CN08
				*CN09
				*CN10

\*-----  
\* REMOVED AS USED IN L2/3 DECK FOR TRAC-PF1(MDD1)

\* ICHF=1

\* TEE 41 41 BROKEN-LOOP COLD LEG TEE

2	4	7	0.0	1	*CN02
---	---	---	-----	---	-------

\* MAIN TUBE

0	2	41	44	0	*CN03
0	0	0	0	0	*CN04
0.14209	0.03571	6.0	6.0	300.0	*CN05
300.0	0.0	0.0	1.0E20	1.0	*CN06
0.0	0.0	1.0E20	1.0		*CN07
					*CN08

\* SIDE TUBE

0	2	43	0		*CN09
0	0	0	0	0	*CN10
0.10725	0.02655	6.0	5.0	300.0	*CN11
					*CN12

\* SIDE TUBE

0	1	19	0		*CN09
0.0149925	0.0071374	6.0	5.0	300.0	*CN10
300.0	0.0	0.0	1.0E20	1.0	*CN11
					*CN12
					*CN13
					*CN14

\* MAIN TUBE

4.35230E+0E		*DX
1.04552E-1F		*VJL
5.54700E-2	5.98920E-3E	*FA
49.5155	0.0E	*FRICF
49.5155	0.0E	*FRICR
F 0.0E		*GRAV
2.63500E-1	8.73252E-2E	*HD
F UF		*ICFLG
F 1E		*NFF
F 0.0E		*A_P
F 0.0F		*V_
F 0.0E		*VV
F 400.0E		*T_
F 615.0E		*TV
F 148.4E+5F		*P
F 0.0E		*PA
		*QPPP
		*MATID
		*TA
		*CONC
		*S
		*PDWTB1
		*POWRF1
		*OP3TR1
		*OP3RF1

\* SIDE TUBE

1.0E		*DX
5.93920E-3E		*VJL
F 5.93920E-3E		*FA
F 0.0F		*FRICF
F 0.0E		*FRICR
F 0.0E		*GRAV
F 8.73252E-2E		*HD
F UF		*ICFLG
F 1E		*V=F
F 0.0F		*A_P
F 0.0F		*VL
F 0.0E		*VV
F 400.0E		*T_
F 615.0E		*TV
F 148.4E+5F		*P
F 0.0F		*PA
		*QPPP
		*MATID
		*TA
		*CONC
		*S
		*PDWTB1
		*POWRF1
		*OP3TR1
		*OP3RF1

\*\*\*\*\*

\* VALVE IS CONTROLLED BY TRIP 5.

VALVE= 14 14 ECG LINE - CHECK VALVE  
? 0 17 16 ?

\*CN02

700.0	0.0	0.0	1.0E20	1.0	*CN13	
0.0	0.0	1.0E20	1.0		*CN14	
* MAIN TUBE						
R2	0.80774			E	*DX	
F2	0.0512676			E	*VJL	
Q3	0.053425			E	*FA	
	0.0	1.0E47	0.030579	E	*FRIC VSL-BLCL -0.17	
	0.1291	1.0E47	0.030579	E	*FRIC BLCL-VSL 0.129	
F	0.0	F			*GRAV	
R3	0.234			E	*HD	
D3	0		E		*ICFLG	
F	1E				*NFF	
F	0.0E				*ALP	
F	0.0E				*VL	
=	-	0.0E			*VV	
	560.95	562.40		E	*TL	
F	516.38E				*TV	
F	148.4E+5E				*P	
F	0.0E				*PA	
F	0.0E				*OPPP	
F	7E				*MATID	
	560.9	561.01	R2 561.03.	562.53S	*TW	
	562.5E	R2 562.58E			*TW	
* SIDE TUBE						
	8.85000E-1	7.28340E+0E			*DX	
	3.03300E-2	2.76800E-1E			*VJL	
F 2	0.0388	3.3300E-03E			*FA	
R ?	0.0	0.0E			*FRICF	
R ?	0.0	0.0E			*FRICP	
	0.0	1.09000E-1	0.0E		*GRAV	
F 2	2.22300E-1	55.200E-3E			*HD	
F	0E	"			*ICFLG	
F	1E				*VFF	
F	0.0E				*ALP	
F	0.0E				*VL	
F	0.0E				*VV	
	563.30	562.88 E			*T-	
F	615.0E				*TV	
F	148.4E+5E				*P	
F	0.0E				*PA	
F	0.0E				*OPPP	
F	7E				*MATID	
F	563.3E				*TW	
*****						
* -- TRIP 200						
* VALVE 43 43 BROKEN-LOOP COLD LEG VALVE						
	4	4	44	42	7	*CN02
	0	0	3	2	0	*CN03
200		1	-4	0	0	*CN04
3		0	0	0	0	*CN05
0		0				*CN06
	1.0E+20	0.0	0.0	0.0		*CN07
	1.4209E-01	3.5710E-02		6.0	5.0	3.00E+02 *CN08

370.0 1.30750E-02 1.327200E-01 1.0 1.0 \*J102  
 0.0 0.0 0.0 0.0 \*CN10

\* ARRAY DATA

F 0.0	E *DX
0.80774 0.513051 1.145039 1.02234	E *VOL
0.0512576 0.00505142 0.02623801 0.0472489	E *FA
0.053425 0.013875 0.0083647 0.02352 0.051955	E *FRICF
0.030579 0.0 0.01515 0.0460103 0.01717	E *FRICR
0.030579 0.0 0.01515 0.0460103 0.01717	E *GRAV
F 0.0	E *HD
0.284 0.13292 0.1032 0.17305 0.2572	E *ICFLG
F2 0 2 R2 0	E *NFF
F 1	E *ALP
E 0.0	E *VL
F 0.0	E *VV
554.53 553.72 551.91 550.35	E *TL
F 616.38	E *TV
F 148.4E+5	E *P
F 0.0	E *PA
F 0.0	E *OPPP
F 7	E *MATID
R4 554.47 F4 554.0 R4 552.5 P4 551.0	E *TW
	E *CONC
	E *S
0.0 1.0 2.5 0.55	E *VTB1
5.0 0.0 1000.0 0.0	E *VTB1
	E *VTB2
	E *VRF
	E *OP3TB
	E *OP3RF

\*\*\*\*\*  
 \* CONSTANT VELOCITY - SET TO ZERO  
 \*

FILL 42 42 BROKEN-COLD-LEG TERMINAL

42	1	0			*CN02
					*CN03
0.0	1.0E20	0.0	0.0		*CN04
1.02235	0.0472489	0.0	0.0	550.3	*CN05
148.4E+5	0.0	0.0	0.0	550.3	*CN06
					*CN07
					*CN08
					*CN09
					*CN10

\*\*\*\*\*

\*

PIPE 81 81 UPPER PLENUM INJECTION PIPE

1	0	51	81	7	*CN02
0	0	0	0		*CN03
3.505200E-02	3.555000E-03	0.	0.		*CN04
3.072000E+02	0.0	0.0	1.0E20	1.0	*CN05
					*CN07
					*CN08

\*

\* ARRAY DATA

F 2.5000E+00E					* DX
F 2.4124E-03F					* VDL
F 0.6497E-04F					* FA
F 0. E					* FRIC
F 0. E					* FRIC
F 1.0000E+00E					* GRAV
F 3.5052E-02F					* HD
F 0 E					* ICFLG
F 1F					* NFF
F 5.0503E-06F					* ALP
7.	-2.9327E-05F				* VL

0. -7.7327E-05E \* VV  
 F 5.9792E+02E \* TL  
 F 6.1531E+02E \* TV  
 F 1.5190E+07E \* P  
 F 0.0 E \* PA  
 \* OPPP  
 \* MATID  
 \* TW  
 \* CONC  
 \* S  
 \* POWTB1  
 \* POWRF1  
 \* OP3TB1  
 \* UP3RF1

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\*  
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 \*  
**FILL** 61 51 UPPER PLENUM INJECTION  
 41 8 0 \* CN02  
 1010 1 21 0 0 \* CN03  
 0.0 1.0E20 0.0 \* CN04  
 2.500000E+00 2.412430E-03 0. 0. 3.080000E+02 \* CN05  
 41.40000E+05 0. 0. \* CN06  
 . .  
 . .  
 0.0825 \* CN07  
 \* CN08  
 \* CN09  
 \* CN10

0.0	0.0	1.0	0.05	* VMTB
38.0	7.2	40.0	5.95	
78.0	0.0	100.0	0.05	
200.0	0.67	255.0	0.705	
260.0	0.0	266.0	1.805	
272.0	0.50	345.0	0.505	
347.0	31.0	352.0	30.05	
358.0	20.0	363.0	18.25	
375.0	16.9	400.0	10.05	
445.0	4.0	450.0	0.05	
1000.0	0.0E			

---

\*  
 \*-----  
 \*  
**PIPE** 82 82 UPPER PLENUM INJECTION PIPE  
 1 0 62 82 7 \* CN02  
 0 0 0 0 \* CN03  
 . .  
 . .  
 3.505200E-02 3.555000E-03 0. 0. 3.072000E+02 \* CN05  
 3.072000E+02 0.0 0.0 1.0E20 1.0 \* CN06  
 \* CN07  
 \* CN08

---

\*  
 \* ARRAY DATA:  
 \*  
 F 2.5000E+00E \* DX  
 F 2.4124E-03E \* VOL  
 F 9.6497E-04E \* FA  
 F 0. E \* FRIC  
 F 0. E \* FRIC  
 F 1.0000E+00E \* GRAV  
 F 3.5052E-02E \* HD  
 F 0. E \* ICFLG  
 F 1E \* NFF  
 F 1.8330E-06E \* ALP  
 F 0. -1.2684E-05E \* VL  
 F 0. -1.2684E-05E \* VV  
 F 5.9792E+02E \* TL  
 F 6.1535E+02E \* TV  
 F 1.5200E+07E \* P  
 F 0.0 E \* PA  
 \* OPPP  
 \* MATID

\* T<sub>n</sub>  
 \* CUVL  
 \* S  
 \* POWTBI  
 \* POWRF1  
 \* CP3TBI  
 \* CP3RF1

```

*
=====
* FILL          62          52 UPPER PLENUM INJECTION
*               6           0
*               1010        21      0       0
*               0.0         1.0E20   0.0
*               2.50000E+00  2.412430E-03 0.
*               41.4000E+05  0.       0.

* 0.0825

*               0.0       1.0       0.05     * VMTB
*               79.0      7.2       40.0      5.95
*               78.0      0.0       100.0     0.05
*               200.0      0.67      255.0     0.705
*               250.0      0.0       266.0     1.805
*               272.0      0.50      345.0     0.505
*               347.0      31.0      352.0     30.05
*               358.0      20.0      363.0     18.25
*               375.0      16.9      400.0     10.05
*               445.0      4.0       450.0     0.05
*               1000.0     0.0E      0.0E      * CN02
*               0.0       1.0       0.05     * CN03
*               0.0       0.0       0.0      * CN04
*               0.0       1.0E20   0.0      * CN05
*               3.505200E-02 3.555000E-03 0.       0.      * CN06
*               3.072000E+02 0.0       0.0      1.0E20   1.0      * CN07
*               0.0       0.0      * CN08

* PIPE          83          83 UPPER PLENUM INJECTION PIPE
*               1           0       63       83       7
*               0           0       0       0       * CN02
*               0.0       1.0       0.0      * CN03
*               0.0       0.0      * CN04
*               0.0       1.0E20   0.0      * CN05
*               3.505200E-02 3.555000E-03 0.       0.      * CN06
*               3.072000E+02 0.0       0.0      1.0E20   1.0      * CN07
*               0.0       0.0      * CN08

* ARRAY DATA
* F               2.5000E+00F     * DX
* F               2.4124E-03F     * VUL
* F               9.5497E-04E     * FA
* F               0.0       E     * FRIC
* F               0.0       E     * FRIC
* F               1.0000E+00E     * GRAV
* F               3.5052E-02F     * HD
* F               0.0       E     * ICFLG
* F               1E       E     * MFF
* F               2.6250E-06F     * ALP
* F               0.0       -1.2657E-05E * VL
* F               0.0       -1.2657E-05E * VV
* F               5.0791E+02E     * TL
* F               6.1535E+02E     * TV
* F               1.5200E+07F     * P
* F               0.0       E     * PA
* F               0.0       E     * QPPP
* F               0.0       E     * MATIU
* F               0.0       E     * TW
* F               0.0       E     * CONC
* F               0.0       E     * S
* F               0.0       E     * POWTBI
* F               0.0       E     * POWRF1
* F               0.0       E     * CP3TBI
* F               0.0       E     * CP3RF1

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FILL                    63                    53 JPPFR PLENUM INJECTION  
 63                    8                    0                    \*CN02  
 1010                1                    21                    0                    \*CN03  
 0.0                    1.0E20            0.0                    \*CN04  
 2.500000E+00      2.412430E-03    0.                    0.                    3.080000E+02    \*CN05  
 41.40000E+05      0.                    0.                    \*CN06  
 \*CN07  
 \*CN08  
 \*CN09  
 \*CN10

0.0825

0.0	0.0	1.0	0.05	* V4TB
28.0	7.2	40.0	5.95	
78.0	0.0	100.0	0.05	
- 200.0	0.67	255.0	0.705	
250.0	0.0	256.0	1.805	
272.0	0.50	345.0	0.505	
347.0	31.0	352.0	30.05	
358.0	20.0	363.0	18.25	
375.0	16.9	400.0	10.05	
445.0	4.0	450.0	0.05	
1000.0	0.0E			

PIPE                    84                    84 UPPER PLENUM INJECTION PIPE  
 1                    0                    64                    84                    7    \*CN02  
 0                    0                    0                    0                    \*CN03  
 \*CN04  
 \*CN05  
 3.505200E-02    3.555000E-03    0.                    0.                    3.072000E+02    \*CN06  
 3.072000E+02    0.0                0.0                1.0E20    1.0                    \*CN07  
 \*CN08

\*  
 \* ARRAY DATA  
 \*  
 F 2.5000E+00F                            \* DX  
 F 2.4124F-03E                            \* VUL  
 F 9.6497E-04E                            \* FA  
 F 0.                    E                    \* FRIC  
 F 0.                    F                    \* FRIC  
 F 1.0000E+00E                            \* GRAV  
 F 3.5052E-02E                            \* HD  
 F 0                    E                    \* ICFLG  
 F 1E                                        \* NFF  
 F 2.5303E-05F                            \* ALP  
 F 0.                    -1.2758E-05E                    \* VL  
 F 0.                    -1.2758E-05E                    \* VV  
 F 5.9791E+02E                            \* TL  
 F 5.1536E+02E                            \* TV  
 F 1.5200E+07E                            \* P  
 F 0.0                    E                    \* PA  
 \*QPPP  
 \*MATID  
 \*TW  
 \*CONC  
 \*S  
 \*PONT81  
 \*POURF1  
 \*QP3T81  
 \*QP3RF1

\*  
 \* FILL                    64                    54 UPPER PLENUM INJECTION  
 64                    8                    0                    \*CN02  
 1010                1                    21                    0                    \*CN03  
 0.0                    1.0E20            0.0                    \*CN04

2.50000E+00 2.412430E-03 0. 0. 3.080000E+02 \*CN05  
41.40000E+05 0. 0. \*CN06  
\*CN07  
\*CN08  
\*CN09  
\*CN10

0.0825

	0.0	0.0	1.0	0.05	* VMTB
38.0	7.2	40.0	5.75		
78.0	0.0	100.0	0.05		
200.0	0.67	255.0	0.705		
240.0	0.0	266.0	1.805		
272.0	0.50	345.0	0.505		
347.0	31.0	352.0	30.05		
358.0	20.0	363.0	18.25		
375.0	16.9	400.0	10.05		
445.0	4.0	450.0	0.05		
- 1000.0	0.0E				

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PIPE 85 85 UPPER PLENUM INJECTION PIPE  
1 0 65 85 7 \*CN02  
0 0 0 0 0 \*CN03  
\*CN04  
\*CN05

3.505200F-02 3.5556000E-03 0. 0. 3.072000E+02 \*CN06  
3.072000F+02 0.0 0.0 1.0E20 1.0 \*CN07  
\*CN08

\*

\* ARRAY DATA

F	2.5000E+00F	*DX
F	2.4124F-03F	*VOL
F	0.6497F-04F	*FA
F	0. F	*FRIC
F	0. F	*FRIC
F	1.0000F+00E	*GRAV
F	3.5052F-02F	*HU
F	0 E	*ICFLG
F	1F	*NFF
F	4.7030F-06F	*ALP
F	0. -1.2637E-05E	*VL
F	0. -1.2837E-05E	*VV
F	5.0731F+02F	*TL
F	5.1537E+02F	*TV
F	1.5203E+07F	*P
F	0.0 F	*PA
		*UPPP
		*MATID
		*TW
		*CONC
		*S
		*POWTF1
		*POWRF1
		*QP3TB1
		*QP3RF1

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FILL 65 55 UPPER PLENUM INJECTION

65	8	0		*CN02
1013	1	21	0	*CN03
0.0	1.0E20	0.0	0	*CN04
2.500000E+00	2.412430E-03	0.	0.	3.080000E+02 *CN05
41.40000E+05	0.	0.		*CN06
				*CN07
				*CN08
				*CN09
				*CN10

0.1675

0.0	0.0	1.0	0.05	* VMTB
-----	-----	-----	------	--------

79.0	7.2	69.0	5.95
75.0	0.0	100.0	0.05
220.0	0.67	255.0	0.705
240.0	0.0	266.0	1.805
272.0	0.50	345.0	0.505
347.0	31.0	352.0	30.05
358.0	20.0	363.0	18.25
375.0	16.9	400.0	10.05
445.0	4.0	450.0	0.05
1000.0	0.0E		

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PIPE                  86                  85 UPPER PLENUM INJECTION PIPE

1	0	66	86	7	*CN02
0	0	0	0		*CN03

3.505200E-02	3.555600E-03	0.	0.	3.072000E+02	*CN05
3.072000E+02	0.0	0.0	1.0E20	1.0	*CN06

\*CN07

\*CN08

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#### ARRAY DATA

F 2.5000E+00F \* DX

F 2.4124E-03F \* VUL

F 9.6497E-04E \* FA

F 0. F \* FRIL

F 0. E \* FRIC

F 1.0000E+00E \* GRAV

F 3.5052E-02F \* HD

F 0 E \* ICFLG

F 1E \* NIFF

F 5.3957E-06E \* ALP

0. -1.2615E-05E \* VL

0. -1.2615E-05E \* VV

F 5.9791E+02E \* TL

F 5.1538E+02F \* TV

F 1.5204E+07E \* P

F 0.0 E \* PA

\*OPPP

\*MATI0

\*TW

\*CONC

\*S

\*POWTB1

\*POWRF1

\*UP3TR1

\*OP3R

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FILL                  66                  56 UPPER PLENUM INJECTION

66	8	0		*CN02
----	---	---	--	-------

1010	1	21	0	*CN03
------	---	----	---	-------

0.0	1.0E20	0.0		*CN04
-----	--------	-----	--	-------

2.500000E+00	2.412430E-03	0.	0.	3.080000E+02
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41.4000E+05	0.	0.		*CN05
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\*CN06

\*CN07

\*CN08

\*CN09

\*CN10

0.1575

0.0	0.0	1.0	0.05	* VMTB
-----	-----	-----	------	--------

38.0	7.2	40.0	5.95	
------	-----	------	------	--

78.0	0.0	100.0	0.05	
------	-----	-------	------	--

200.0	0.67	255.0	0.705	
-------	------	-------	-------	--

240.0	0.0	256.0	1.805	
-------	-----	-------	-------	--

272.0	0.50	345.0	0.505	
-------	------	-------	-------	--

347.0	31.0	352.0	30.05	
-------	------	-------	-------	--

358.0	20.0	363.0	18.25	
-------	------	-------	-------	--

175.0	16.0	400.0	19.05
445.0	4.0	450.0	0.05
1000.0	0.0E		

PIPE 87 87 UPPER PLENUM INJECTION PIPE

1	0	67	87	7	*CN02
0	0	0	0		*CN03
					*CN04
					*CN05
3.505200E-02	3.555000E-03	0.	0.		*CN06
1.072000E+02	0.0	0.0	1.0E20	1.0	*CN07
					*CN08

ARRAY DATA

F 2.5000E+00F					* DX
F 2.4124E-03E					* VOL
F 2.6497E-04E					* FA
F 0. E					* FRIC
F 0. F					* FRIC
F 1.0000E+00E					* GRAV
F 3.5052E-02E					* HD
F 0. E					* ICFLG
F 1E					* NFF
F 4.9541F-06F					* ALP
0. -1.2042E-05E					* VL
0. -1.2082E-05E					* VV
F 5.9770E+02E					* TL
F 5.1537E+02F					* TV
F 1.5203E+07E					* P
F 0.0 E					* PA
					* OPPP
					* MATIU
					* TW
					* CONC
					* S
					* POWT81
					* POWRF1
					* OP3TB1
					* UP3RF1

FILL 67 57 UPPER PLENUM INJECTION

67	8	0			*CN02
1010	1	21	0	0	*CN03
0.0	1.0E20	0.0			*CN04
2.500000E+00	2.412430E-03	0.	0.		*CN05
41.40000E+05	0. 0.				*CN06
					*CN07
					*CN08
					*CN09
0.1675					*CN10
0.0	0.0	1.0	0.05		* VMTB
38.0	7.2	40.0	5.95		
78.0	0.0	100.0	0.05		
200.0	0.67	255.0	0.705		
260.0	0.0	266.0	1.805		
272.0	0.50	345.0	0.505		
347.0	31.0	352.0	30.05		
356.0	20.0	363.0	18.25		
375.0	16.9	400.0	10.05		
445.0	4.0	450.0	0.05		
1000.0	0.0E				

PIPE 88 88 UPPER PLENUM INJECTION PIPE

1 0	0 0	58 0	89 0	7	*CN02 *CN03 *CN04 *CN05 *CN06 *CN07 *CN08
3.505200E-02 3.072000E+02	3.555000E-03 0.0	0. 0.0	0. 1.0E20	3.072000E+02	

\* APRAY DATA

F 2.5000E+00E	* DX
F 2.4124E-03E	* VOL
F 9.6497E-04E	* FA
F 0. F	* FRIC
F 0. E	* FRIC
F 1.0000E+00E	* GRAV
F 3.5052E-02F	* HD
F 0 E	* ICFLG
F 1F	* NFF
C 4.6921E-06F	* ALP
0. -1.2745E-05E	* VL
0. -1.2745E-05E	* VV
F 5.9790E+02F	* TL
F 6.1537E+02F	* TY
F 1.5203E+07F	* P
F 0.0 E	* PA
	* QPPP
	* MATIU
	* TW
	* CONC
	* S
	* POWTB1
	* POWRF1
	* QP3TB1
	* UP3RF1

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FILL 68 58 UPPER PLENUM INJECTION

58	8	0			*CN02
1010	1	21	0	0	*CN03
0.0	1.0E20	0.0	0.	3.080000E+02	*CN04
2.500000E+00	2.412430E-03	0.			*CN05
41.40000E+05	0.	0.			*CN06

0.1675

0.0	0.0	1.0	0.05	* VMTB
38.0	7.2	40.0	5.95	
78.0	0.0	100.0	0.05	
200.0	0.67	255.0	0.705	
260.0	0.0	265.0	1.805	
272.0	0.50	345.0	0.505	
347.0	31.0	352.0	30.05	
358.0	20.0	363.0	18.25	
375.0	16.9	400.0	10.05	
445.0	4.0	450.0	0.05	
1000.0	0.0E			

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PIPE 89 89 UPPER PLENUM INJECTION PIPE

1	0	69	89	7	*CN02
0	0	0	0		*CN03
3.505200E-02 3.072000E+02	3.555000E-03 0.0	0. 1.0E20	0. 1.0	3.072000E+02	*CN04
					*CN05
					*CN06
					*CN07
					*CN08

```

*+
*+ ARRAY DATA
*+
F 2.5000E+00E * DX
F 2.4124E-03E * VUL
F 9.5497E-04E * FA
F 0. E * FKIC
F 0. E * FRIC
F 1.0000E+00E * GRAV
F 3.5052E-02E * HD
F 0. E * ICFLG
F 1E * IFF
F 1.2552E-06E * ALP
D. -1.2874E-05E * VL
D. -1.2874E-05E * VV
F 5.9735E+02E * TL
F 5.4537E+02E * TV
F 1.5203E+07F * P
F 0.0 E * PA
*UPPP
*MATID
*TW
*CONC
*S
*POWTB1
*POWRF1
*OP3T01
*UP3RF1

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*+
*+=====
*+
FILE 69 59 UPPER PLENUM INJECTION
      59      3      0      0      0      0      *CN02
      1010     1      21      0      0      0      *CN03
      0.0    1.0E20      0.0      0.      3.080000E+02      *CN04
2.500000E+00 2.412430E-03 0.      0.      3.080000E+02      *CN05
41.40000E+05 0.      0.      0.      0.      0.      *CN06
      0.0000      0.0      1.0      0.05      0.05      *CN07
      0.0      0.0      7.2      5.95      0.05      *CN08
      78.0      0.0      100.0      0.05      0.05      *CN09
200.0      0.67      255.0      0.705      0.05      *CN10
240.0      0.0      266.0      1.805      0.05
272.0      0.50      345.0      0.505
347.0      31.0      352.0      30.05
358.0      20.0      363.0      18.25
375.0      16.9      400.0      10.05
445.0      4.0      450.0      0.05
1000.0      0.0E      0.0E      0.0E      0.0E      * VMTB

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```

*+
*+=====
*+
PIPE 70 90 UPPER PLENUM INJECTION PIPE
      1      0      70      90      7      *CN02
      0      0      0      0      0      *CN03
      0.05200E-02 3.555000E-03 0.      0.      3.072000E+02      *CN04
      3.072000E+02 0.0      0.0      1.0E20      1.0      *CN05
      0.0      0.0      0.0      0.0      0.0      *CN06
      0.0      0.0      0.0      0.0      0.0      *CN07
      0.0      0.0      0.0      0.0      0.0      *CN08

```

```

*+
*+ ARRAY DATA
*+
F 2.5000E+00E * DX
F 2.4124E-03E * VUL
F 9.5497E-04E * FA
F 0. E * FKIC

```

F 0. F  
 F 1.0000E+00F  
 F 3.5052E-02F  
 F 0. F  
 F 1F  
 F 1.7754E-06E  
 0. -1.2585E-05E  
 0. -1.2586E-05E  
 F 5.9734E+02E  
 F 5.1538E+02F  
 F 1.5204E+07F  
 F 0.0 F

\* FFL  
 \* GRAY  
 \* HD  
 \* ICFLG  
 \* NFF  
 \* ALP  
 \* VL  
 \* VV  
 \* TL  
 \* TV  
 \* P  
 \* PA  
 \* UPPP  
 \* MATID  
 \* TW  
 \* CONC  
 \* S  
 \* PONTB1  
 \* POWRF1  
 \* UP3TB1  
 \* UP3RF1

\*  
 \*-----  
 \*  
 FILL 70 70 UPPER PLENUM INJECTION  
 70 8 0 \*CN02  
 1010 1 21 0 0 \*CN03/  
 0.0 1.0E20 0.0 \*CN04  
 2.500000E+00 2.412430E-03 0. 0. 3.080000E+02 \*CN05  
 41.40000F+05 0. 0. \*CN05  
 0.0000 \*CN07  
 0.0 0.0 1.0 0.05 \*CN08  
 78.0 7.2 40.0 5.95 \*CN09  
 78.0 0.0 100.0 0.05 \*CN10  
 200.0 0.67 255.0 0.705  
 250.0 0.0 266.0 1.805  
 272.0 0.50 345.0 0.505  
 347.0 31.0 352.0 30.05  
 358.0 20.0 363.0 18.25  
 375.0 16.9 400.0 10.05  
 445.0 4.0 450.0 0.05

\* VMTB

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 \*-----  
 \*  
 PIPE 91 91 UPPER PLENUM INJECTION PIPE 7  
 1 0 71 91 7 \*CN02  
 0 0 0 0 \*CN03  
 3.505200F-02 3.555000E-03 0. 0. 3.072000E+02 \*CN04  
 3.072000E+02 0.0 0.0 1.0E20 1.0 \*CN05  
 \*CN06  
 \*CN07  
 \*CN08

\*  
 \* ARRAY DATA  
 \*  
 F 2.5000E+00E \*DX  
 F 2.4124E-03E \*VOL  
 F 9.6497E-04F \*FA  
 F 0. F \*FRIC  
 F 0. F \*FRIC  
 F 1.0000E+00F \*GRAY  
 F 3.5052E-02E \*HD  
 F 0. F \*ICFLG  
 F 1F \*NFF  
 F 3.7557E-06F \*ALP  
 0. -1.0007E-05F \*VL

F 5.9734E+02F -1.9607E-05F \* VV  
 F 6.1537E+02F \* TL  
 F 1.5203E+07E \* TV  
 F 0.0 E \* P  
 \* PA  
 \*OPPP  
 \*MATID  
 \*TW  
 \*CONC  
 \*S  
 \*POWTB1  
 \*POWRF1  
 \*UP3TB1  
 \*UP3RF1

---

FILL 71 71 UPPER PLENUM INJECTION \*CN02  
 71 8 0 \*CN03  
 1010 1 21 0 0 \*CN04  
 0.0 1.0E20 0.0 0. 3.080000E+02 \*CN05  
 2.500000E+00 2.412430E-03 0. \*CN06  
 41.40000E+05 0. 0. \*CN07  
 0.0000 0.0E \*CN08  
 0.0 0.0 1.0 0.05 \*CN09  
 28.0 7.2 40.0 5.95 \*CN10  
 79.0 0.0 100.0 0.05  
 200.0 0.67 255.0 0.705  
 260.0 0.0 266.0 1.805  
 272.0 0.50 345.0 0.505  
 347.0 31.0 352.0 30.05  
 358.0 20.0 363.0 18.25  
 375.0 15.9 400.0 10.05  
 445.0 4.0 450.0 0.05  
 1000.0 0.0E \*VMTB

---

PIPE 92 92 UPPER PLENUM INJECTION PIPE \*CN02  
 1 0 72 92 7 \*CN03  
 0 0 0 0 \*CN04  
 3.505200F-02 3.555000E-03 0. 0. 3.072000E+02 \*CN05  
 3.072000E+02 0.0 0.0 1.0E20 1.0 \*CN07  
 0.0000 0.0E \*CN08

---

APRAY DATA \*DX  
 F 2.5000E+00E \*VUL  
 F 2.4124E-03F \*FA  
 F 9.5497E-04E \*FRIC  
 F 0. E \*FRIC  
 F 0. E \*GRAV  
 F 1.0000UF+00F \*HD  
 F 3.5052E-02E \*ICFLG  
 F 0. E \*NFF  
 F 1F \*ALP  
 F 4.1450F-06E \*VL  
 F 0. -1.2557E-05E \*VV  
 F 0. -1.2557E-05E \*TL  
 F 5.9735E+02F \*TV  
 F 6.1537E+02E \*P  
 F 1.5202E+07E \*PA  
 F 0.0 E \*OPPP  
 \*MATID

\*TW  
 \*C0NC  
 \*S  
 \*POWT81  
 \*POWRF1  
 \*QP3T81  
 \*QP3RF1

```

*
*=====
*
FILL          72          72  UPPER PLENUM INJECTION
    72          8          0
    1010         1          21          0          0
    0.0        1.0E20        0.0
2.500000E+00 2.412430E-03 0.          0.          3.080000E+02
41.40000E+05 0.          0.

0.0000
    0.0          0.0          1.0          0.05      * VMTB
    38.0         7.2          40.0          5.95
    78.0         0.0          100.0          0.05
    220.0        0.67          255.0          0.705
    260.0         0.0          266.0          1.805
    272.0        0.50          345.0          0.505
    347.0        31.0          352.0          30.05
    358.0        20.0          363.0          18.25
    375.0        16.9          400.0          10.05
    445.0         4.0          450.0          0.05
    1000.0        0.0F

*
*=====
*
TEE          101          101  CORE BYPASS
*   JCELL       NODES      MAT      CUST      ICHE
*   3           4           7       0.0       1
*                                             *CN02

* MAIN TUBE
* 
*   ICU4C1      NCCELL1     JUN1      JUN2      IPDW1
*   0           5           101      105       0
*   *QPTR1      IQPSV1      NQPTB1    NQPSV1    NQPRF1
*   0           0           0         0         0
*   RADI41      TH1        HOUTL1    HUITV1    TUUTL1
*   0.00174     0.04        0.0        0.0        300.0
*   TOUTV1      PWIN1      PWOFF1    PWPMX1    PWSCL1
*   300.0        0.0        0.0        1.0E20    1.0
*   QPI41      QP0FF1      QUPMX1    OPSCL1
*   0.0        0.0        1.0E20    1.0
*                                             *CN08

* SIDE TUBE
* 
*   ICU4C2      NCCELL2     JUN3      IPW2
*   0           1           109      0
*   *QPTR2      IQPSV2      NQPTB2    NQPSV2    NQPRF2
*   0           0           0         0         0
*   RADI42      TH2        HOUTL2    HUITV2    TUUTL2
*   0.00195     0.04        0.0        0.0        300.0
*   TOUTV2      PWIN2      PWOFF2    PWPMX2    PWSCL2
*   300.0        0.0        0.0        1.0E20    1.0
*   QPI42      QP0FF2      QUPMX2    OPSCL2
*   0.0        0.0        1.0E20    1.0
*                                             *CN14

* MAIN TUBE
* 
R ?          0.6          0.46E 2      0.97E      *DX1
R ? 2.204E-03 1.693E-03E 2 3.570E-03E      *VJL1
          1.295E-03E 4 5.030E-03 1.295E-03E      *FA1
F          0.0F


```

F	0.0F			*FRILIK
F	1.0F			*GRAV1
	3.440E-03	4	1.44E-02	3.480E-03
	10	4	0	1E
F	1E			*H01
F	0.0F			*ICFLG1
F	0.0F			*NFF1
F	0.0F			*ALP1
F	593.0E			*VLL1
F	615.0F			*VV1
F	148.4E+5E			*T_1
F	0.0F			*TV1
F	0.0E			*P1
F	7F			*PA1
F	570.0E			*OPPP1
F				*MATID1
F				*TA1

\* SIDE TUBE

	0.050E			*DX2
	2.742E-04E			*VJL2
F	1.041E-03E			*FA2
F	0.0E			*FRIC2F
F	0.0F			*FRIC2R
F	0.0F			*GRAV2
F	0.00391E			*HD2
	0	1E		*ICFLG2
F	1E			*NFF2
F	0.0F			*ALP2
F	0.0E			*V_2
F	0.0E			*VV2
F	593.0F			*TL2
F	615.0F			*TV2
F	148.4E+5E			*P2
F	0.0E			*PA2
F	0.0E			*OPPP2
F	7F			*MATID2
F	570.0E			*TN2

\*-----

TEE	JCELL	NIDES	MAT	CUST	IC-F	CORE BYPASS
	3	4	7	0.0	1	

\*CN02

\* MAIN TUBE

*	ICUNCL1	NCELL1	JUN1	JUN2	IPCH1	
*	0	5	102	106	0	*CN03
*	IOPTR1	IOPSV1	NOPTB1	NOPSV1	NOPRF1	
*	0	0	0	0	0	*CN05
*	RADIV1	T-1	HOUTL1	HOUTV1	TOUTL1	
*	0.00174	0.04	0.0	0.0	300.0	*CN06
*	TOUTV1	PWIN1	PWOFF1	PPWMX1	PWSCL1	
*	300.0	0.0	0.0	1.0E20	1.0	*CN07
*	DPIV1	DPUFF1	RUPMX1	DPSC1		
*	0.0	0.0	1.0E20	1.0		*CN08

\* SIDE TUBE

*	IC04C2	NCELL2	JUN3	IPUW2		*CN09
*	0	1	110	0		
*	IOPTR2	IOPSV2	NOPTB2	NOPSV2	NOPRF2	
*	0	0	0	0	0	*CN11
*	RADIV2	T-2	HOUTL2	HOUTV2	TOUTL2	
*	0.00196	0.04	0.0	0.0	300.0	*CN12
*	TOUTV2	PWIN2	PWOFF2	PPWMX2	PWSCL2	
*	300.0	0.0	0.0	1.0E20	1.0	*CN13
*	DPIV2	DPUFF2	RUPMX2	DPSC2		
*	0.0	0.0	1.0E20	1.0		*CN14

\* MAIN TUBE

\* ? 0.6 0.46E 2 0.97E \*0X1  
 \* ? 2.20E-03 1.693E-03R 2 3.570E-03E \*VJL1  
 \* 1.275E-03 4 6.030E-03 1.295E-03F \*FA1  
 \* F 0.0E \*FRIC1  
 \* F 0.0F \*FRIC1  
 \* F 1.0E \*GRAVI  
 \* 3.480F-03 4 1.44E-02 3.480F-03E \*HJ1  
 \* 1R 4 0 1E \*ICFLG1  
 \* 1E \*NFF1  
 \* F 0.0E \*A\_PI  
 \* F 0.0F \*VL1  
 \* F 0.0E \*VV1  
 \* F 533.0E \*T\_1  
 \* F 615.0E \*TV1  
 \* F 148.4E+5E \*P1  
 \* F 0.0E \*PA1  
 \* F 0.0E \*QPPP1  
 \* F 7E \*MATID1  
 \* F 570.0E \*TA1

\* SIDE TUBE

\* U.050E \*DX2  
 \* 2.742F-04E \*VJL2  
 \* 1.041F-03F \*FA2  
 \* F 0.0E \*FRIC2  
 \* F 0.0E \*FRIC2  
 \* F 0.0E \*GRAVI  
 \* F 0.00391F \*HJ2  
 \* 0 1E \*ICFLG2  
 \* F 1E \*NFF2  
 \* F 0.0E \*ALP2  
 \* F 0.0E \*VL2  
 \* F 0.0E \*VV2  
 \* F 593.0E \*TL2  
 \* F 615.0F \*TV2  
 \* F 148.4E+5F \*P2  
 \* F 0.0F \*PA2  
 \* F 0.0E \*QPPP2  
 \* F 7E \*MATID2  
 \* F 570.0E \*TA2

\*\*\*\*\*  
 \* TEE 103 103 CORE BYPASS  
 \* JCELL NODES MAT CUST ICHF  
 \* 3 4 7 0.0 1 \*CN02

\* MAIN TUBE

\* ICUN01 NCELL1 JUN1 JUV2 IPUN1 \*CN03  
 \* 0 5 103 107 0  
 \* ICPTR1 ICPSV1 NUPTB1 VQPSV1 VQPRF1 \*CN05  
 \* 0 0 0 0 0  
 \* RADIV1 TH1 HUUTL1 HOUTV1 TOUTL1  
 \* 0.00174 0.04 0.0 0.0 300.0 \*CN06  
 \* TOJTV1 PWIN1 PHUFF1 RPWMX1 PWSCL1 \*CN07  
 \* 300.0 0.0 0.0 1.0E20 1.0  
 \* QPIN1 QPQFF1 ROPMX1 QPSCL1 \*CN08  
 \* 0.0 0.0 1.0E20 1.0

\* SIDE TUBE

\* ICUN02 NCELL2 JUN3 IPOW2 \*CN09  
 \* 0 1 111 0  
 \* ICPTR2 ICPSV2 NUPTB2 VQPSV2 VQPRF2 \*CN11  
 \* 0 0 0 0 0  
 \* RADIV2 TH2 HOUTL2 HOUTV2 TOUTL2

0.70145	0.04	0.0	0.0	300.0	*CV12
* 17JTV2	PWFF2	RWFF2	RPMY2	PASC2	
300.0	0.0	0.0	1.0E20	1.0	*CV13
* QFIV2	QDFF2	RUPMX2	QPSCL2		
0.0	0.0	1.0E20	1.0		*CV14

\* MAIN TUBE

P 2	0.6	0.46R 2	0.97E	*DX1
P 2	2.20HF-23	1.693E-03R 2	3.570E-03E	*VOL1
F	1.295E-03R 4	6.030E-03	1.295E-03E	*FA1
F	0.0E			*FRIC1
F	0.0E			*FRIC1
F	1.0E			*GRAV1
F	3.490E-03R 4	1.44E-02	3.480E-03E	*HD1
F	1R 4	0	1E	*ICFLG1
F	-	1E		*NFF1
F	0.0E			*ALP1
F	0.0E			*VLL1
F	0.0E			*VV1
F	593.0E			*TL1
F	615.0E			*TV1
F	148.4E+5F			*P1
F	0.0E			*PA1
F	0.0E			*OPPP1
F	7F			*MATID1
F	570.0E			*TW1

\* SIDE TUBE

F	0.050E			*DX2
F	2.742E-04F			*VOL2
F	1.041E-03E			*FA2
F	0.0E			*FRIC2
F	0.0E			*FRIC2
F	0.0E			*GRAV2
F	0.00391E			*HD2
F	0	1E		*ICFLG2
F	-	1E		*NFF2
F	0.0E			*ALP2
F	0.0E			*V-2
F	0.0E			*VV2
F	593.0E			*TL2
F	615.0E			*TV2
F	148.4E+5F			*P2
F	0.0E			*PA2
F	0.0E			*OPPP2
F	7F			*MATID2
F	570.0E			*TW2

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TEE		104	104	CORE BYPASS	
* JCELL	VODES	MAT	CUST	ICHF	
3	4	7	0.0	1	*CN02

\* MAIN TUBE

* ICUN1	NCELL1	JUN1	JUN2	IPDW1	*CN03
0	5	104	108	0	
* IOPTR1	IOPSV1	NQPTB1	NQPSV1	NQPRF1	
0	0	0	0	0	*CN05
* RADIV1	T41	HOUTL1	HOUTY1	TOURL1	
0.00174	0.04	0.0	0.0	300.0	*CV06
* TDUTV1	PWIV1	PWOFF1	RPWMX1	PWSCL1	
300.0	0.0	0.0	1.0E20	1.0	*CN07
* QPIV1	QDFF1	RUPMX1	QPSCL1		
0.0	0.0	1.0E20	1.0		*CN08

\* SIDE TUBE

* ICPV2	"CELL2	JUNS	IPWK2		
0	1	112	0		*CN09
* ICPT2	ICPSV2	NQPTB2	NQPSV2	NOPRF2	
0	0	0	0	0	*CN11
* RADIV2	T42	HOUTL2	HOUTV2	TOUTL2	
0.00195	0.04	0.0	0.0	300.0	*CN12
* TOUTV2	PWIN2	PWOFF2	PWMX2	PNSCL2	
300.0	0.0	0.0	1.0E20	1.0	*CN13
* CPIN2	CPOFF2	KOPMX2	OPSCL2		
0.0	0.0	1.0E20	1.0		*CN14

\* MAIN TUBE

R 2	0.0	0.46R 2	0.97E	*DX1
R 2	2.208E-03	1.693E-03R 2	3.570E-03E	*VOL1
F	1.295E-03R 4	5.030E-03	1.295E-03E	*FA1
F	0.0F			*FRIC1
F	0.0E			*FRIC1
F	1.0F			*GRAV1
F	3.480E-03P 4	1.44E-02	3.480E-03E	*HD1
F	1R 4	0	1E	*ICFLG1
F	1E			*NFF1
F	0.0F			*A_P1
F	0.0F			*VL1
F	0.0E			*VV1
F	503.0F			*T_1
F	615.0F			*TV1
F	148.4E+5E			*P1
F	0.0E			*PA1
F	0.0F			*OPPP1
F	7F			*MATID1
F	570.0E			*TW1

\* SIDE TUBE

F	0.050F			*DX2
F	2.742E-04E			*VOL2
F	1.041E-03E			*FA2
F	0.0E			*FRIC2
F	0.0E			*FRIC2
F	0.0F			*GRAV2
F	0.0391E			*HD2
F	0	1E		*ICFLG2
F	1F			*NFF2
F	0.0E			*ALP2
F	0.0E			*VL2
F	0.0E			*VV2
F	503.0F			*TL2
F	615.0E			*TV2
F	148.4E+5E			*P2
F	0.0E			*PA2
F	0.0E			*OPPP2
F	7E			*MATID2
F	570.0E			*TW2

\*\*\*\*\*

\* - VZMAX SET TO 60 FROM 50

\* THE FOLLOWING ARRAYS HAVE BEEN REPLACED BY FP-1 VALUES  
\* TAKEN FROM TRAC-PDZ(MOD1) ANALYSIS

- \* - CPDWR
- \* - R3KF
- \* - ZPHTR
- \* - RADRD
- \* - PPHTP
- \* - VFAAX
- \* - PGAPT

\*\*\*\*\*

VESSEL	50	50 VESSEL
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\* BASED ON /PD2IA/LUF1/L2-3/RJW1/L2-3IND WITH FOLLOWING MODIFICATIONS:

\* OCT/NOV 1982, PTG  
\* - INCORPORATE DISTRIBUTED HEAT SLABS  
\* - CHANGE INITIAL HSTN'S FRUM 593 K TO 570 K TO HELP INHIBIT  
\* - FILM BOILING AT START OF STEADY STATE RUN  
\* - MINOR CHANGE TO LEVEL 3 DOWNCOMER FA-T AND Z (TO .375)

\* UCI 1983, PTG  
\* - REVISE AXIAL POWER SHAPE PEP PC & TC

\* AUG 1985, GLS  
\* - REVISE ELEVATION OF CORE, 0.13 M LOWER

\* SEP 1985, J.BIRCHLEY  
\* - INCLUDE FRICTION FACTOR VALUES FOR ENTRY INTO, THROUGH  
\* AND EXIT FROM CORE  
\* REVISE FLUID VOLUME AND AREA FRACTIONS

\* NAXS\* 12 \*NRSX\* 4 \*NTSX\* 4 \*NCSR\* 28 \*IVSSBF\* 0 \*CARD 2  
\* IDCU\* 12 \*IDCL\* 2 \*IUCK\* 3 \*ICRU\* 0 \*ICRL\* 3 \*CARD 3  
\* ICPR\* 3 \*ILCSP\* 0 \*IJCSP\* 0 \*IUHP\* 0 \*ICONC\* 0 \*CARD 4  
\* VFFA\* 0 \*VFFK\* 0 \*NFET\* 0 \*NVENT\* 0 \*CARD 5  
\* IRPNTY\* 7 \*NDGX\* 0 \*NUOIX\* 0 \*NRTS\* 0 \*CARD 6

\* TIPPAUTR\* 100 \*IRPNSV\* 1 \*NKPATB\* 25 \*NRPNSV\* 0 \*NRPWRF\* 0 \*CARD 7  
\* IZPNTR\* 0 \*IZPNSV\* 1 \*NZPATB\* 1 \*NZPNSV\* 0 \*NZPWRF\* 0 \*CARD 8  
\* IRFTTR\* 101 \*NMWRX\* 1 \*NFCI\* 1 \*NFCIL\* 1 \*NZMAX\* 60 \*CARD 9

\* VRDUS\* 16 \*NUDES\* 10 \*NUDHS\* 4 \*INHSX\* 1 \*CARD 10  
\* DEACT\* 0. \*TNEUT\* 0.\*KPWDF\*-1.E20 \*RRPWGX\*1.E30 \*RPHSCL\* 1.0 \*CARD 11  
\* PZPRI\*37.0E5\*ZPWHY\* 0. \*ZPWOFF\* 0. \*NZPWHX\* 0. \*CARD 12  
\* SHELV\* 0. \*PLDR\* 0. \*PURAT\* 1.336 \*FUCRAC\* 0.7 \*HGAPO\*1.0E+3 \*CARD 13  
\* DTXHT(1)\*4.0 \*DTXHT(2)\*50. \*DLNHT\*1.0E-3 \*CARD 14

\*  
\* \*SKIPPED\*\* \*CARD 15  
\* \*SKIPPED\*\* \*CARD 16  
\* \*SKIPPED\*\* \*CARD 17

0.527	0.727	1.2485	*Z
1.553	1.7815		*Z
2.010	2.467	2.9245	*Z
3.400	4.8465		*Z
5.130	5.900E		*Z
0.105	0.231	0.329	0.470E *RADIUS
1.570796327	3.141592654	4.712388981	6.283185308E *THETA

\* VESSEL SOURCE CARDS

11	10	3	1 *ILHL
11	15	3	9 *ILCL
11	12	3	31 *BLHL
11	13	3	41 *BLCL
11	9	-2	105 *BYP5
11	6	-2	105 *BYP5
11	11	-2	107 *BYP5
11	8	-2	108 *BYP5
9	1	2	81 *UPINJ
9	2	2	82 *UPINJ
9	3	2	83 *UPINJ
9	4	2	84 *UPIVJ
9	5	2	85 *UPINJ
9	6	2	86 *UPINJ
9	7	2	87 *UPINJ
9	8	2	88 *UPINJ
9	9	2	89 *UPINJ
9	10	2	90 *UPINJ
9	11	2	91 *UPINJ
9	12	2	92 *UPINJ
8	9	3	109 *BYP5
8	10	3	110 *BYP5

8	11	3	111	*BYPS
8	12	3	112	*BYPS
3	4	2	101	*BYPS
3	10	2	102	*BYPS
3	11	2	103	*BYPS
3	12	2	104	*BYPS
0.955	0.9460	0.9655		*RDPWR
0.975	0.9905			*RDPWR
1.016	1.060R 3	0.000E		*RDPWR

\* THE FOLLOWING DATA IS FOR FP-1

R 4	1.4556E 4	1.2039 R 4	0.7245E	*CPJWR	
	1	2	3		
	8	12E			
R 4	1.2F03	1.0939	1.2365E	*IDROD	
*(DUMMY)*	1.05			*IDROD	
	0.1500	1.2541	1.4586 S	*ZPWTB	
	1.4995	1.0337	0.0477 E	*ZPWTB	
R 4	33.102 4	127.1R 4	154.8E	*RDX	
	0.0	7.7449E-4	1.5484E-3S	*RADRD	
	2.3235E-3	3.0479E-3S		*RADRD	
	3.9725E-3	4.6470E-3	4.7420E-3S	*RADRD	
	5.0508E-3	5.3590E-3E		*RADRD	
R 5	1	3R 2	2E	*MATRD	
	0.0	37.0E6	0.3	32.425E6 S	*RPWTB
	0.9	9.8748E6	1.28	5.5142E6 S	*RPWTB
	1.38	3.9596E6	1.40	3.2985E5 S	*RPWTB
	1.46	2.9456E5	1.52	2.6480E6 S	*RPWTB
	1.59	2.3320E5	1.61	2.2712E6 S	*RPWTB
	2.0	2.1547E6	3.0	2.0515E5 S	*KPWTB
	4.0	1.9873E6	6.0	1.8751E6 S	*KPWTB
	8.0	1.7919E6	10.0	1.7251E5 S	*KPWTB
	15.0	1.6047E6	20.0	1.5183E6 S	*KPWTB
	30.0	1.3962E6	40.0	1.3038E6 S	*RPWTB
	60.0	1.1357E5	100.0	1.0700E5 S	*RPWTB
	200.0	0.9500E6	300.0	0.8400E6 S	*RPWTB
	1000.0	5.2560E4 E		*RPWTB	

	0.0F			*PLVUL
	0.0F			*PSLEV
	0.0E			*CLENV
* LEVEL 1				
R 4	0.0077 S			*HSA
R 4	0.0333 S			*HSA
R 4	0.0431 S			*HSA
R 4	1.096 E			*HSA
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
F	0.0E			*CFZL-T
F	0.0E			*CFZL-Z
F	0.0F			*CFZL-R
F	0.0F			*CFZV-T
F	0.0F			*CFZV-Z
F	0.0E			*CFZV-R
F	1.118E			*VOL
F	1.0E			*FA-T
F	1.0F			*FA-Z
F	1.0E			*FA-R
F8	1.0 R4 1.0 F4 0.0 E			*HD-T
F	0.1F			*HD-Z
F	0.1E			*HD-R
F	0.1E			*HSTN
F	570.0E			*MATHS
F	6E			*ALPN
F	0.0F			*VVN-T
F	0.0E			*VVV-Z
F	0.0F			*VVN-R
F	0.0F			*VLN-T
F	0.0F			*VLV-Z
F	0.0E			*VLN-R
F	615.0E			*TVN
F	593.0E			*TLN
F	148.4E5E			*PN
F	0.0E			*PAN
* LEVEL 2				
R 4	0.0 S			*HSA
R 4	0.0 S			*HSA
P 4	0.0 S			*HSA
R 4	0.3024 E			*HSA
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX
	0.0	0.075	0.085	*HSX

	0.0	0.075	0.085	0.0925	*HSX
	0.0	0.075	0.085	0.0925	*HSX
	0.0	0.075	0.085	0.0925	*HSX
	0.0	0.075	0.085	0.0925	*HSX
	0.0	0.075	0.085	0.092E	*HSX
F	0.0F				*CFZL-T
F	0.0E				*CFZL-Z
F	0.0E				*CFZL-R
F	0.0E				*CFZV-T
F	0.0E				*CFZV-Z
F	0.0F				*CFZV-R
S	1.118F				*VOL
F	1.0E				*FA-T
R12	.409R 4	.582E			*FA-Z
R8	1.0 R4 1.0 P4 0.0 E				*FA-R
F	.1E				*HD-T
F	.1E				*HD-Z
F	.1E				*HD-R
F	570.0F				*HSTN
F	6E				*MATHS
F	0.0F				*ALPN
S	0.0E				*VVN-T
F	0.0E				*VVN-Z
F.	0.0E				*VVN-R
F	0.0E				*VLN-T
F	0.0E				*VLN-Z
F	0.0F				*VLN-R
F	615.0F				*TVN
F	573.0E				*TLN
F	148.4E5E				*PV
F	0.0F				*PAN
*					

\* LEVEL 3

R 4	0.1341 S				*HSA
R 4	0.5150 S				*HSA
R 4	0.6676 S				*HSA
R 4	2.1207 E				*HSA
	0.0	0.005	0.010	0.0153S	*HSX
	0.0	0.005	0.010	0.0153S	*HSX
	0.0	0.005	0.010	0.0153S	*HSX
	0.0	0.005	0.010	0.0153S	*HSX
	0.0	0.005	0.010	0.0153S	*HSX
	0.0	0.005	0.010	0.0153S	*HSX
	0.0	0.005	0.010	0.0153S	*HSX
	0.0	0.005	0.010	0.0153S	*HSX
	0.0	0.005	0.010	0.0153S	*HSX
	0.0	0.005	0.010	0.0153S	*HSX
	0.0	0.005	0.010	0.0153S	*HSX
	0.0	0.005	0.010	0.0153S	*HSX
	0.0	0.005	0.010	0.0153S	*HSX
	0.0	0.005	0.010	0.0153S	*HSX
	0.0	0.005	0.010	0.0153S	*HSX
	0.0	0.005	0.010	0.0153S	*HSX
	0.0	0.025	0.035	0.040S	*HSX
	0.0	0.025	0.035	0.040S	*HSX
	0.0	0.025	0.035	0.040S	*HSX
	0.0	0.025	0.035	0.040S	*HSX
	0.0	0.025	0.035	0.040E	*HSX
F	0.0F				*CFZL-T
R12	5.5P 4	0.0E			*CFZL-Z
F	0.0E				*CFZL-R
F	0.0E				*CFZV-T
R12	5.5R 4	0.0E			*CFZV-Z
F	0.0E				*CFZV-R
R12	.656R 4	0.582E			*VOL
R12	.7P 4	.582E			*FA-T
R12	0.448R 4	.582E			*FA-Z
R8	0.7 R4 0.0 P4 0.0 E				*FA-R
R12	1.22E-2R 4	0.100E			*HD-T
R12	1.22E-2P 4	0.100E			*HD-Z
R12	1.22E-2P 4	0.100E			*HD-R
F	570.0F				*HSTN
F	6E				*MATHS
F	0.0F				*ALPN

F	0.0E			*VVV-T	
F	0.0E			*VVV-Z	
F	0.0E			*VVV-R	
F	0.0E			*VLN-T	
F	0.0E			*VLN-Z	
F	0.0E			*VLN-R	
F	515.0E			*TVN	
F	593.0E			*TLN	
F	148.4F5E			*PN	
F	0.0E			*PAN	
*	LEVEL 4				
R 4	0.0 S			*HSA	
R 4	0.0 S			*HSA	
R 4	0.1703 S			*HSA	
R 4	- 1.2410 E			*HSA	
	0.0	0.050	0.050	0.0665S	
	0.0	0.050	0.060	0.0665S	
	0.0	0.050	0.060	0.0665S	
	0.0	0.050	0.050	0.0665S	
	0.0	0.050	0.060	0.0665S	
	0.0	0.050	0.050	0.0665S	
	0.0	0.050	0.050	0.0665S	
	0.0	0.050	0.050	0.0665S	
	0.0	0.050	0.060	0.0665S	
	0.0	0.050	0.050	0.0665S	
	0.0	0.050	0.050	0.0665S	
	0.0	0.050	0.060	0.0665S	
	0.0	0.050	0.050	0.0665S	
	0.0	0.025	0.035	0.040S	
	0.0	0.025	0.035	0.040S	
	0.0	0.025	0.035	0.040S	
	0.0	0.025	0.035	0.040E	
F	0.0E			*CFZL-T	
R12	0.0F	0.0E		*CFZL-Z	
F	0.0E			*CFZL-R	
F	0.0F			*CFZY-T	
R12	0.6E	0.0E		*CFZY-Z	
E	0.0E			*CFZY-R	
R12	.478E 4	.582E		*VOL	
R12	0.251R 4	.5H2E		*FA-T	
R12	0.448R 4	.5K2E		*FA-Z	
R4	0.0R4	0.251R4	0.0R4	0.0E	*FA-R
R12	1.22E-2P 4	0.100E		*HD-T	
R12	1.22E-2P 4	0.100E		*HD-Z	
R12	1.22E-2R 4	0.100E		*HD-R	
F	570.0E			*HSTN	
F	6F			*MATHS	
F	0.0E			*ALPN	
E	0.0E			*VVV-T	
F	0.0F			*VVV-Z	
F	0.0E			*VVV-R	
E	0.0E			*VLN-T	
F	0.0E			*VLN-Z	
E	0.0F			*VLN-R	
F	515.0E			*TVN	
F	593.0E			*TLN	
F	148.4F5E			*PN	
F	0.0E			*PAN	
*	LEVEL 5				
R 4	0.0 S			*HSA	
R 4	0.0 S			*HSA	
R 4	0.1273 S			*HSA	
P 4	0.9277 E			*HSA	
	0.0	0.050	0.060	0.0665S	
	0.0	0.050	0.060	0.0665S	
	0.0	0.050	0.050	0.0665S	
	0.0	0.050	0.060	0.0665S	

0.0	0.050	0.050	0.0655S	*HSX
0.0	0.050	0.050	0.0655S	*HSX
0.0	0.050	0.050	0.0655S	*HSX
0.0	0.050	0.050	0.0655S	*HSX
0.0	0.050	0.050	0.0655S	*HSX
0.0	0.050	0.050	0.0655S	*HSX
0.0	0.050	0.050	0.0655S	*HSX
0.0	0.050	0.050	0.0655S	*HSX
0.0	0.025	0.035	0.040S	*HSX
0.0	0.025	0.035	0.040S	*HSX
0.0	0.025	0.035	0.040S	*HSX
0.0	0.025	0.035	0.040E	*HSX
=	0.0F			*CFZL-T
P12	0.6F	0.0E		*CFZL-Z
F	0.0F			*CFZL-R
F	0.0E			*CFZV-T
R12	0.6F	0.0E		*CFZV-Z
F	0.0E			*CFZV-R
Z4	.478P 4	.582E		*VOL
R12	0.251R 4	.582E		*FA-T
P12	0.448P 4	.582E		*FA-Z
Z4	0.0P4	0.251R4	0.0E	*FA-R
R12	1.22E-2P 4	0.100E		*HD-T
R12	1.22E-2P 4	0.100E		*HD-Z
R12	1.22E-2R 4	0.100E		*HD-R
F	570.0E			*HSTN
F	6F			*MATHS
F	0.0E			*ALPN
F	0.0E			*VVV-T
F	0.0F			*VVN-Z
F	0.0F			*VVN-R
F	0.0F			*VLN-T
F	0.0F			*VLN-Z
F	0.0E			*VLN-R
F	615.0E			*TVN
=	593.0E			*TLN
F	145.4E5E			*PV
F	0.0F			*PAN

\* LEVEL 6

R 4	0.0 S			*HSA
R 4	0.0 S			*HSA
R 4	0.1279 S			*HSA
R 4	0.9281 E			*HSA
	0.0	0.050	0.060	*HSX
	0.0	0.050	0.050	*HSX
	0.0	0.050	0.050	*HSX
	0.0	0.050	0.060	*HSX
	0.0	0.050	0.050	*HSX
	0.0	0.050	0.060	*HSX
	0.0	0.050	0.060	*HSX
	0.0	0.050	0.060	*HSX
	0.0	0.050	0.060	*HSX
	0.0	0.050	0.060	*HSX
	0.0	0.050	0.060	*HSX
	0.0	0.050	0.060	*HSX
	0.0	0.050	0.060	*HSX
	0.0	0.050	0.060	*HSX
	0.0	0.025	0.035	*HSX
	0.0	0.025	0.035	*HSX
	0.0	0.025	0.035	*HSX
	0.0	0.025	0.035	*HSX
	0.0	0.025	0.035	*HSX
F	0.0E			*CFZL-T
R12	0.6F	0.0E		*CFZL-Z
F	0.0F			*CFZL-R
F	0.0E			*CFZV-T
R12	0.6F	0.0E		*CFZV-Z
F	0.0E			*CFZV-R
Z4	.478P 4	.582E		*VOL
R12	0.251R 4	.582E		*FA-T
R12	0.448P 4	.582E		*FA-Z

F4	0.0E4	0.0E4	0.0E4	0.0E	*FA-Z
R12	1.22E-2R 4	0.100E			*HD-T
R12	1.22E-2R 4	0.100E			*HD-Z
R12	1.22E-2R 4	0.100E			*HD-R
F	570.0E				*HSTN
F	6E				*MATHS
F	0.0F				*ALPN
F	0.0E				*VVN-T
F	0.0E				*VVN-Z
F	0.0F				*VNL-R
F	0.0F				*VNL-T
F	0.0E				*VNL-Z
F	0.0E				*VNL-K
F	615.0E				*TVN
F	593.0E				*TLN
F	148.4E5E				*PN
F	0.0F				*PAN

\* LEVEL 7

R 4	0.0 S				*HSA
R 4	0.0 S				*HSA
R 4	0.2552 S				*HSA
R 4	1.9518 E				*HSA
	0.0	0.050	0.050	0.06655	*HSX
	0.0	0.050	0.060	0.06655	*HSX
	0.0	0.050	0.050	0.06655	*HSX
	0.0	0.050	0.060	0.06655	*HSX
	0.0	0.050	0.050	0.06655	*HSX
	0.0	0.050	0.060	0.06655	*HSX
	0.0	0.050	0.050	0.06655	*HSX
	0.0	0.050	0.050	0.06655	*HSX
	0.0	0.050	0.050	0.06655	*HSX
	0.0	0.050	0.060	0.06655	*HSX
	0.0	0.050	0.050	0.06655	*HSX
	0.0	0.050	0.050	0.06655	*HSX
	0.0	0.025	0.035	0.040S	*HSX
	0.0	0.025	0.035	0.040S	*HSX
	0.0	0.025	0.035	0.040S	*HSX
	0.0	0.025	0.035	0.040S	*HSX
F	0.0F				*CFZL-T
R12	0.6F	0.0E			*CFZL-Z
F	0.0E				*CFZL-R
F	0.0E				*CFZV-T
R12	0.6F	0.0E			*CFZV-Z
F	0.0F				*CFZV-R
R12	4.78R 4	.582E			*VOL
R12	0.251R 4	.582E			*FA-T
R12	0.448R 4	.582E			*FA-Z
R4	0.0R4	0.251R4	0.0P4	0.0E	*FA-R
R12	1.22E-2R 4	0.100E			*HD-T
R12	1.22E-2R 4	0.100E			*HD-Z
R12	1.22E-2R 4	0.100E			*HD-R
F	570.0E				*HSTN
F	6E				*MATHS
F	0.0F				*ALPN
F	0.0E				*VVN-T
F	0.0E				*VVN-Z
F	0.0E				*VVN-R
F	0.0E				*VNL-T
F	0.0E				*VNL-Z
F	0.0E				*VNL-R
F	615.0E				*TVN
F	593.0F				*TLN
F	148.4E5E				*PN
F	0.0E				*PAN

\* LEVEL 8

R 4	0.0 S				*HSA
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F 4	0.0 S			*HSA	
R 4	0.7552 S			*HSA	
R 4	1.0516 E			*HSA	
	0.0	0.050	0.050	*HSX	
	0.0	0.050	0.050	*HSX	
	0.0	0.050	0.060	*HSX	
	0.0	0.050	0.050	*HSX	
	0.0	0.050	0.060	*HSX	
	0.0	0.050	0.050	*HSX	
	0.0	0.050	0.050	*HSX	
	0.0	0.050	0.050	*HSX	
	0.0	0.050	0.050	*HSX	
	0.0	0.050	0.050	*HSX	
	0.0	0.050	0.050	*HSX	
	0.0	0.050	0.050	*HSX	
	0.0	0.050	0.050	*HSX	
	0.0	0.050	0.050	*HSX	
	0.0	0.025	0.035	0.040 S	
	0.0	0.025	0.035	0.040 S	
	0.0	0.025	0.035	0.040 S	
	0.0	0.025	0.035	0.040 S	
				*HSX	
F	0.0E			*CFZL-T	
P1?	0.6F	0.0E		*CFZL-Z	
F	0.0E			*CFZL-R	
F	0.0E			*CFZV-T	
Q12	0.6F	0.0E		*CFZV-Z	
F	0.0F			*CFZV-R	
R12	.478P 4	.582E		*VOL	
R12	0.251P 4	.582E		*FA-T	
R12	0.448P 4	.582E		*FA-Z	
D4	0.0P4	0.251R4	0.0R4	0.0E	*FA-R
P1?	1.22E-2P 4	0.100E		*HD-T	
P1?	1.22E-2P 4	0.100E		*HD-Z	
P1?	1.22E-2P 4	0.100E		*HO-R	
F	570.0F			*HSTN	
F	0F			*MATHS	
F	0.0E			*ALPV	
E	0.0F			*VVN-T	
F	0.0E			*VVN-Z	
F	0.0E			*VVN-R	
F	0.0F			*VLN-T	
F	0.0F			*VLN-Z	
E	0.0F			*VLN-R	
F	515.0E			*TVN	
F	503.0F			*TLN	
F	148.4E5F			*PN	
F	0.0E			*PAN	
*					
*	LEVEL 3				
*					
R 4	0.2100 S			*HSA	
F 4	0.8060 S			*HSA	
R 4	0.5172 S			*HSA	
F 4	1.9370 E			*HSA	
	0.0	0.0250	0.00500	.0071S	*HSX
	0.0	0.0250	0.00503	.0071S	*HSX
	0.0	0.0250	0.00500	.0071S	*HSX
	0.0	0.0250	0.00500	.0071S	*HSX
	0.0	0.0250	0.00500	.0071S	*HSX
	0.0	0.0250	0.00500	.0071S	*HSX
	0.0	0.0250	0.00500	.0071S	*HSX
	0.0	0.0250	0.00500	.0071S	*HSX
	0.0	0.0200	0.03000	.0341S	*HSX
	0.0	0.0200	0.03000	.0341S	*HSX
	0.0	0.0200	0.03000	.0341S	*HSX
	0.0	0.0200	0.03000	.0341S	*HSX
	0.0	0.025	0.035	.040 S	*HSX
	0.0	0.025	0.035	.040 S	*HSX
	0.0	0.025	0.035	.040 S	*HSX
	0.0	0.025	0.035	.040 E	*HSX
F	0.0E			*CFZL-T	
R 4	0.0F 4	1.2K 4	0.5R 4	0.0E	*CFZL-Z

F	0.0E				*CFZL-T
F	0.0E				*CFZV-T
R 4	0.0E 4	1.2R 4	0.5R 4	0.0E	*CFZV-Z
F	0.0E				*CFZV-R
P12	0.885P 4	.582E			*VOL
R12	0.366P 4	.582E			*FA-T
R 4	0.85P E	0.366R 4	0.5820E		*FA-Z
R 3	0.365 R4 0.0	0.0 E			*FA-P
R12	1.22E-2R 4	0.100E			*HD-T
R12	1.22E-2P 4	0.100E			*HD-Z
R12	1.22E-2P 4	0.100E			*HD-R
F	570.0E				*HSTN
F	6E				*MATHS
F	0.0E				*ALPN
F	0.0E				*VVN-T
F	0.0E				*VVN-Z
F	- 0.0F				*VVN-R
F	0.0E				*VLN-T
F	0.0F				*VLN-Z
F	0.0F				*VLN-R
F	515.0E				*TVN
=	503.0E				*TLN
F	148.4E5E				*PN
F	0.0F				*PAN
F	.				
LEVEL 10					
F	1.0940 S				*HSA
R 4	4.2018 S				*HSA
R 4	1.3944 S				*HSA
R 4	5.2840 E				*HSA
	0.0	.0010	.002	.003045	*HSX
	0.0	.0010	.002	.003045	*HSX
	0.0	.0010	.002	.003045	*HSX
	0.0	.0010	.002	.003045	*HSX
	0.0	.0010	.002	.003045	*HSX
	0.0	.0010	.002	.003045	*HSX
	0.0	.0010	.002	.003045	*HSX
	0.0	.0010	.002	.003045	*HSX
	0.0	.0010	.002	.003045	*HSX
	0.0	.0010	.002	.003045	*HSX
	0.0	.0010	.002	.003045	*HSX
	0.0	.0010	.002	.003045	*HSX
	0.0	.0010	.002	.003045	*HSX
	0.0	.0010	.002	.003045	*HSX
	0.0	.0200	.030	.03410S	*HSX
	0.0	.0200	.030	.03410S	*HSX
	0.0	.0200	.030	.03410S	*HSX
	0.0	.0200	.030	.03410S	*HSX
	0.0	.0200	.030	.03410S	*HSX
	0.0	.0200	.030	.03410S	*HSX
	0.0	.0250	.035	.0400S	*HSX
	0.0	.0250	.035	.0400S	*HSX
	0.0	.0250	.035	.0400S	*HSX
	0.0	.0250	.035	.0400E	*HSX
F	0.0E				*CFZL-T
F	0.0E				*CFZL-Z
F	0.0F				*CFZL-R
F	0.0F				*CFZV-T
F	0.0E				*CFZV-Z
F	0.0E				*CFZV-R
R12	0.885P 4	.715E			*VOL
R 4	1.0P 3	0.0R 4	.7150F		*FA-T
R 4	0.85P 4	0.0R 4	.250S		*FA-Z
	0.981	0.449	0.981	0.449E	*FA-Z
R8 0.0	R4 0.0 R4 0.0	E			*FA-R
R12	1.22E-2R 4	0.100E			*HD-T
R12	1.22E-2P 4	0.100E			*HD-Z
R12	1.22E-2P 4	0.100E			*HD-R
F	570.0E				*HSTN
F	6E				*MATHS
F	0.0E				*ALPN
F	0.0E				*VVN-T
F	0.0F				*VVN-Z
F	0.0F				*VVN-R
F	0.0E				*VLN-T
F	0.0F				*VLN-Z
F	0.0E				*VLN-R

F .15.0F \*TVN  
 F 523.0F \*TLN  
 F 148.4E5E \*PN  
 F 0.0F \*PAN  
 ♦  
 ♦ LEVEL 11  
 ♦  
 R 4 .2149 S \*HSA  
 P 4 0.9251 S \*HSA  
 Q 4 1.0677 S \*HSA  
 R 4 1.1556 E \*HSA  
 0.0 .0010 .002 .00304S \*HSX  
 0.0 .0200 .030 .03410S \*HSX  
 0.0 .0200 .030 .03410S \*HSX  
 0.0 .0200 .030 .03410S \*HSX  
 0.0 .0250 .035 .0400S \*HSX  
 F 0.0E \*CFZL-T  
 F 0.0F \*CFZL-Z  
 ♦ 0.0P4 159.00R4 0.0E \*CFZL-R  
 F 0.0E \*CFZV-T  
 F 0.0F \*CFZV-Z  
 P 8 0.0P4 159.00R4 0.0E \*CFZV-R  
 R 12 0.951P 4 1.25E \*VOL  
 R 12 0.366P 4 .362E \*FA-T  
 R 12 0.365P 4 .000E \*FA-Z  
 R 8 0.366P4 0.045R4 0.0E \*FA-R  
 P 12 1.22E-2P 4 0.100E \*HD-T  
 P 12 1.22E-2P 4 0.100E \*HD-Z  
 R 8 1.22E-2P 4 0.00276R 4 0.100E \*HD-R  
 F 570.0E \*HSTN  
 F 6F \*MATHS  
 F 0.0F \*ALPN  
 F 0.0E \*VVV-T  
 F 0.0F \*VVN-Z  
 F 0.0F \*VYN-R  
 F 0.0E \*VLN-T  
 F 0.0E \*VLN-Z  
 F 615.0F \*VLY-R  
 F 523.0F \*TVN  
 F 148.4E5E \*TLN  
 F 0.0F \*PN  
 ♦  
 ♦ LEVEL 12  
 ♦  
 R 4 0.5827 S \*HSA  
 R 4 2.2371 S \*HSA  
 R 4 0.7426 S \*HSA  
 R 4 0.0 E \*HSA  
 0.0 .0010 .002 .00304S \*HSX  
 0.0 .0200 .030 .03410S \*HSX  
 0.0 .0200 .030 .03410S \*HSX

F	0.0	.0200	.030	.034105	*HSX
F	0.0	.0200	.030	.034105	*HSX
F	0.0	.0250	.035	.04005	*HSX
F	0.0	.0250	.035	.04005	*HSX
F	0.0	.0250	.035	.04005	*HSX
F	0.0	.0250	.035	.0400E	*HSX
F	0.0F				*CFZL-T
F	0.0F				*CFZL-Z
F	0.0F				*CFZL-R
F	0.0E				*CFZV-T
F	0.0E				*CFZV-Z
F	0.0F				*CFZV-R
P12	0.885P 4	0.000E			*VOL
R12	0.346P 4	0.000E			*FA-T
R12	0.346P 4	0.000E			*FA-Z
P9	0.345 K4 0.0	P4 0.0 E			*FA-R
R12	1.22E-2P 4	0.100E			*HD-T
R12	1.22E-2R 4	0.100E			*HD-Z
R12	1.22E-2P 4	0.100E			*HD-R
F	570.0E				*HSTN
F	6F				*MATHS
F	0.0E				*ALPN
F	0.0F				*VVN-T
F	0.0F				*VVN-Z
F	0.0F				*VVN-R
F	0.0E				*VLN-T
F	0.0F				*VLV-Z
F	0.0E				*VLN-R
F	615.0F				*TVN
F	593.0F				*TLN
F	149.4F5F				*PN
E	0.0F				*PAN

\* PUN DATA

F	0.0E				*BURN 1
F	559.0F				*RDTV 1
F	0.0F				*BURN 2
F	559.0F				*RDTV 2
F	0.0F				*BURN 3
F	559.0F				*RDTN 3
F	0.0F				*BURN 4
F	559.0F				*RDTN 4
F	0.0E				*BURN 5
F	559.0E				*RDTN 5
F	0.0E				*BURN 6
F	559.0E				*RDTV 6
F	0.0E				*BURN 7
F	559.0E				*RDTV 7
F	0.0E				*BURN 8
F	559.0F				*RDTN 8
F	0.0F				*BURN 9
F	559.0F				*RDTN 9
F	0.0F				*BURN10
F	559.0F				*RDTN10
F	0.0E				*BURN11
F	559.0E				*RDTN11
F	0.0E				*BURN12
F	559.0E				*RDTN12
F	0.0E				*BURN13
F	559.0E				*RDTV13
F	0.0E				*BURN14
F	559.0E				*RDTN14
F	0.0F				*BURN15
F	559.0E				*RDTN15
F	0.0F				*BURN16
F	559.0E				*RDTN16
F	0.0F				*BURN17
F	559.0F				*RDTN17
F	0.0E				*BURN18

2 1.0E-5  
\*\*\*\*\* TIME STEP DATA \*\*\*\*\*  
\* 1.0E-5 1.0E+0 3.0E+1 1.0E+1  
\* 1.0E-5 1.0E+0 0.1E-1 1.0E+1  
\* 5.0E+0 1.0E-1 1.0E+0 1.0E+0  
\* -1.0

**TABLE 3.5. Input deck listing for transient**

\*\*\*\*  
 1 9 1 6  
 \*  
 \*\*\*\*\*  
 LUFT POST-TEST LP-FP-1 TRANSIENT DECK FOR TRAC-PF1/MOD1  
 \* RESTART FROM TRACST LAST RECORD OF STEADY STATE RJV  
 \* BREAKS AND ACCUMULATOR & ACTIVES.  
 \* BREAK CONDITIONS TAKEN FROM STEADY STATE.  
 \*\*\*\*\*  
 \*  
 \*\*\*\*\* NAMELIST DATA \*\*\*\*\*  
 SINPUTS ICFLW=2, CHM12=1.0, CHM22=0.84, NUAI=0, IGENDM3=1, NLT=18,  
 1\*FP=3, NFRCL=2  
 SEND  
 \*\*\*\*\* MAIN CONTROL CARDS\*\*\*\*\*  
 -1 0.000000 \*MCC 01  
 0 1 \*NCOMP\* 53 \*NJUN\* 53 1 \*MCC 02  
 5.0E-4 5.0E-6 1.0E-5 1.0E-1 \*MCC 03  
 10 50 25 \*MCC 04  
 \*NTSV# 3 \*NTCH# 0 \*NTCP# 0 \*NTRP# 10 \*NTCP# 1 \*MCC 05  
 \*  
 1 2 3 4 55 \*COMP  
 5 7 8 93S \*COMP  
 23 24 25S \*COMP  
 11 12 13S \*COMP  
 14 15 16 17 31S \*COMP  
 32 41 42 50 43S \*COMP  
 81 82 83 84 85S \*CUMP  
 85 87 88 89 90S \*COMP  
 91 92 61 62 63S \*CUMP  
 54 55 56 57 68S \*CD4P  
 59 70 71 72 101S \*CU4P  
 102 103 104E \*COMP  
 \*\*\*\*\* SIGNAL VARIABLE DATA \*\*\*\*\*  
 0  
 \*\*\*\*\* CONTROL BLOCK DATA \*\*\*\*\*  
 \*\*\*\*\* TRIP DATA \*\*\*\*\*  
 0 0 0 0 0 \*TRIP DI  
 0  
 \*\*\*\*\* COMPONENT DATA \*\*\*\*\*  
 \*  
 \*\*\*\*\*  
 BREAK 32 32 BROKEN-HOT-LEG TERMINAL  
 32 1 3 1 0 \*CN02  
 0 1 17 0 0 \*CN03  
 0.815975 0.042348 0.0 615.3 150.1E5 \*CN04  
 0.0 0.0 1.0E20 0.0 0.0 \*CV05  
 \*CN06  
 1.0 1.0 1.0 1.0 1.0 \*CN07  
 0.0 150.1E5 1.0 150.1E5 S \*PTB  
 1.0191 1.0E5S  
 2.0 1.61E5 3.0 1.61E5 S  
 7.0 1.71E5 21.3 2.79E5 S  
 24.4 2.88E5 74.8 2.50E5 S  
 140.0 2.61E5 269.0 2.60E5 S  
 285.0 2.65E5 357.0 2.645E5 S  
 381.0 2.694E5 401.0 2.86E5 S  
 457.0 3.08E5 500.0 3.08E5 E  
 \* 2.0 3.5E5 6.0 2.3E5 S  
 \* 33.0 3.6E5 53.0 3.34E5 S  
 \* 70.0 3.17E5 100.0 3.0E5 S  
 \* 310.0 2.7E5 500.0 2.7E5 E  
 \*\*\*\*\*  
 BREAK 42 42 BROKEN-COLD-LEG TERMINAL  
 42 1 3 1 0 \*CN02  
 0 1 17 0 0 \*CN03  
 1.0222350 0.0472484 0.0 615.5 150.4E5 \*CN04  
 0.0 0.0 1.0E20 0.0 0.0 \*CN05  
 \*CN06  
 1.0 1.0 1.0 1.0 1.0 \*CN07

0.0	1.00E5	1.0	1.00E5	S	DATA
1.0131	1.01E5				
2.0	1.61E3	3.0	1.61E5	S	
7.0	1.71E5	21.3	2.79E5	S	
24.4	2.88E5	74.8	2.60E5	S	
140.0	2.61E5	269.0	2.60E5	S	
285.0	2.65E5	357.0	2.64E5	S	
391.0	2.684E5	401.0	2.56E5	S	
457.0	3.08E5	500.0	3.08E5	E	
* 2.0	3.5E5	6.0	2.3E5	S	
* 33.0	3.6E5	53.0	3.34E5	S	
* 70.0	3.17E5	100.0	3.0E5	S	
* 210.0	2.7E5	500.0	2.7E5	E	
*****TIME STEP DATA*****					
1.0E-5	5.0E-3	1.0	10.0		
1.0	0.2	2.0	0.5		
1.0E-5	1.0E-2	5.0	10.0		
1.0	0.5	2.0	1.0		
1.0E-5	0.1	345.0	10.0		
5.0	0.5	5.0	5.0		
* 1.0E-5	1.0E-2	500.0	10.0		
* 5.0	0.5	5.0	5.0		
-1.0					

EVD



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*(See instructions on the reverse)*

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This report assesses thermal-hydraulic aspects of LOFT LP-FP-1 experiment making use of TRAC-PF1/MOD1. LP-FP-1 experiment studies the system thermal-hydraulic and core thermal response for initial and boundary conditions similar to a large-break design basis LOCA leading to fission product release from the fuel cladding gap region. It also assesses the fission product retention effectiveness of the PWR-ECCS in best estimate conditions.

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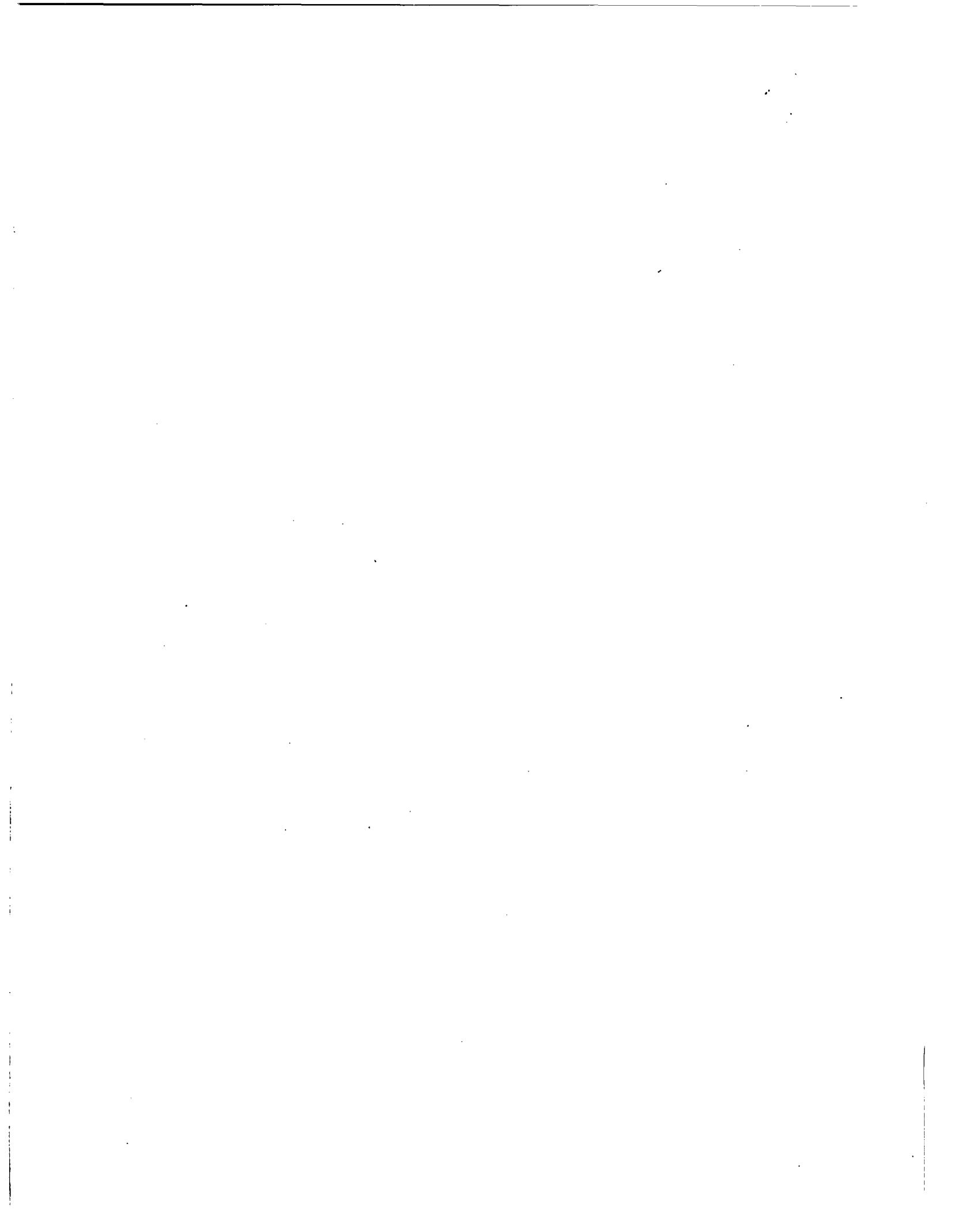
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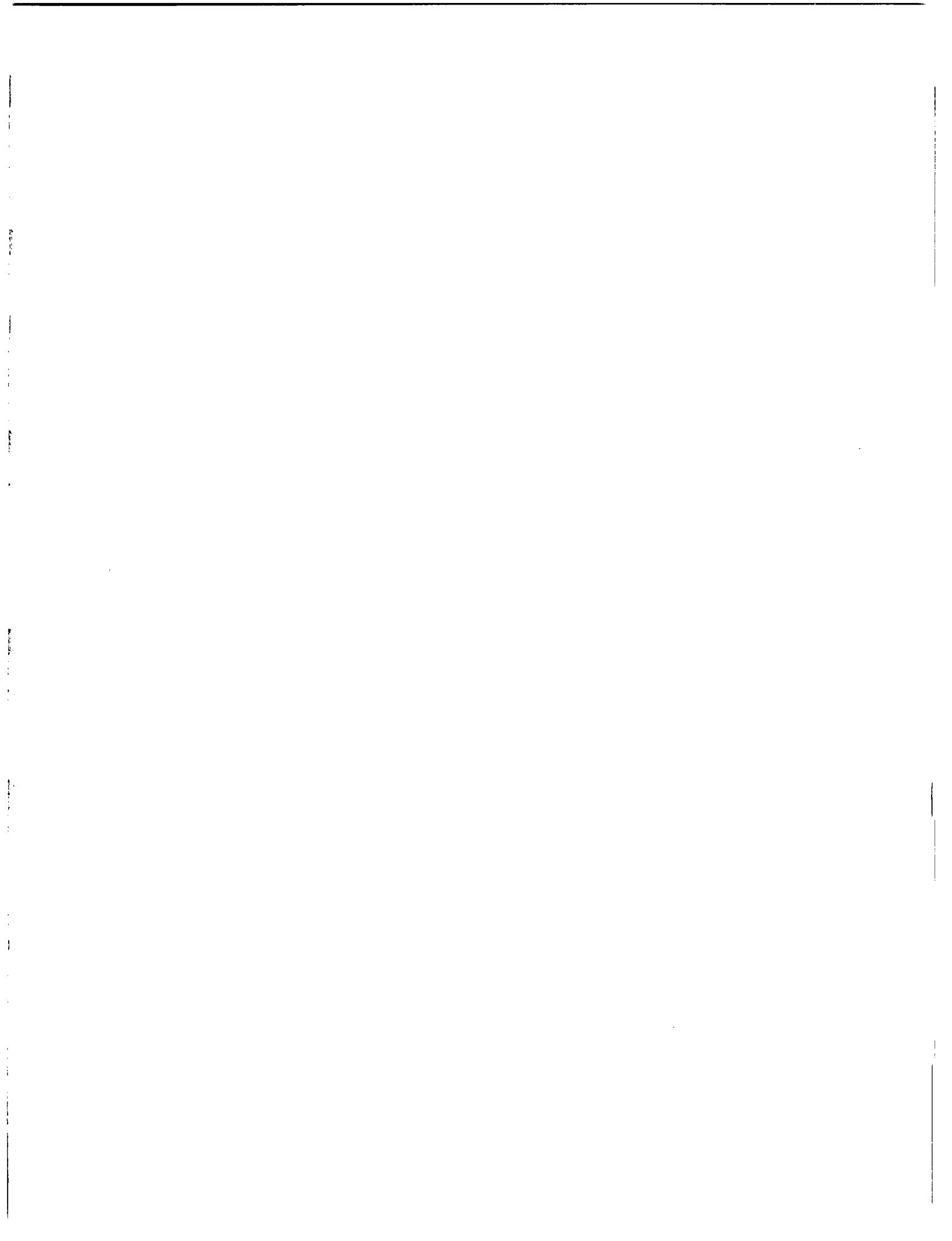
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