



International Agreement Report

Assessment of RELAP5/MOD2, Cycle 36.04 Against LOFT Small Break Experiment L3-6

Prepared by
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Swedish Nuclear Power Inspectorate
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Office of Nuclear Regulatory Research
U.S. Nuclear Regulatory Commission
Washington, DC 20555

July 1990

Prepared as part of
The Agreement on Research Participation and Technical Exchange
under the International Thermal-Hydraulic Code Assessment
and Application Program (ICAP)

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John Eriksson

ICAP
ASSESSMENT OF RELAP5/MOD2, CYCLE 36.04,
AGAINST LOFT SMALL BREAK EXPERIMENT L3-6

ABSTRACT

The LOFT small break experiment L3-6 has been analyzed as part of Sweden's contribution to the International Thermal-Hydraulic Code Assessment and Applications Program (ICAP).

Three calculations, of which two were sensitivity studies, were carried out. The following quantities were varied:

- the content of secondary side fluid and the feed water valve closure
- the two-phase characteristics of the main pumps

All three predictions agreed reasonably well with most of the measured data. The sensitivity calculations resulted only in marginal improvements.

The predicted and measured data are compared on plots and their differences are quantified over intervals in real time.

Approved by *Eric Kellebrand*



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1 INTRODUCTION

An International Thermal-Hydraulic Code Assessment and Applications Program (ICAP) is at present being conducted by several countries under the auspices of the USNRC (Ref 1). The goal of the program is to make quantitative statements regarding the prediction capabilities of current best-estimate thermal-hydraulic computer codes. Such codes have been used for many years as state-of-the-art instruments to study and verify numerical and correlative computational models with experimental results. Some of these codes have reached a high degree of sophistication. They include models for all processes which are essential to thermal-hydraulic scenarios in the nuclear power reactor application. So far, however, these codes have not achieved status as reactor licensing tools, i.e. they do not fulfil the Appendix K rules (Ref 2), although they are often applied to other calculations. The present ICAP aims to quantify uncertainties in the codes so that the codes may be used for licensing purposes.

Sweden's contributions to ICAP encompass assessment calculations using the two thermal-hydraulic codes TRAC-PF1/MOD1 (Ref 3) and RELAP5/MOD2 (Ref 4). The work is conducted by Studsvik Energiteknik AB and is sponsored by the Swedish Nuclear Power Inspectorate.

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A brief description of the LOFT test facility and the L3-6 experiment is given in Chapter 2. In Chapter 3 the model and procedures used in the calculations are discussed. The base case and sensitivity predictions are discussed and compared in Chapters 4 and 5 and in the plots, Appendix B. The run statistics is presented in Chapter 6 and Appendix C. Chapter 7 gives some conclusions from the code assessment. The input listings of the calculations are collected in Appendix A.

A data package on tape containing input files and predicted data has been produced. The content is described in Appendix D. A copy of this tape is submitted to USNRC as a part of the ICAP agreement.

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2 FACILITY AND TEST DESCRIPTION

The LOFT-experiment series L3 was intended to provide large-scale blowdown system data for PWR small break transients. To the Swedish ICAP contribution two experiments of the L3 series were assigned. In the experiment LOFT L3-5, treated earlier in Ref 15, the main circulation pumps were stopped shortly after the break had been opened. In the experiment, LOFT L3-6, treated in this report, the pumps were allowed to operate at normal speed throughout the test in order to provide data for analyzing the differences in the two-phase scenarios between the two tests. Apart from the difference in pump operational mode the two experiments were nominally identical.

This chapter shall briefly describe the test facility, the L3-6 experiment, the assessment parameters used and some aspects of the measurement uncertainties.

2.1 Test Facility

The objective of the LOFT experiments was to demonstrate thermal-hydraulic phenomena which might occur in commercial PWR systems during abnormal situations. The facility is capable of performing a variety of operational transients and LOCAs. Brief descriptions of LOFT are given in a number of experiment reports such as Ref 5. The most thorough description is provided by Reeder (Ref 6). Only particular design features and characteristics relevant to the L3-6 experiment will be discussed in the following sections.

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A general view of LOFT is shown in Figure 1. In the L3-6 small break experiment the two isolation valves on the broken loop legs were closed so as to prevent the passage of fluid via the header to the suppression vessel.

The break was simulated by a 205.9 mm^2 orifice in a T-branch line from the intact loop cold leg near the reactor vessel. The aim of the break configuration was to simulate an equally placed 4-in diameter small break on a four-loop 1000 MW(e) PWR.

During the L3-6 experiment the only primary coolant injection was carried out by the HPIS into the reactor vessel downcomer. The experiment was terminated before the LPIS pressure set point was reached.

2.2 The Experiment

After approximately 99 h of nuclear heating the initial conditions listed in Table 1 were obtained. The sequence of events which occurred during this experiment is listed in Table 2. Main imposed actions during the experiment were:

- a. At the time of reactor scram (which for safety reasons had to be verified before the break) the steam generator feed water and steam line valves started to close.
- b. LOCA initiated 5.8 s after the scram.
- c. The HPIS injection started at 13.2 MPa.
- d. The steam generator auxiliary feed was initiated and terminated manually.

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2.3 Assessment Parameters

The selection of the appropriate assessment parameters for the LOFT L3-6 experiment, Table 3, followed the recommendations of the ICAP Guidelines (Ref 1). The selection was made during the input preparation since a number of expanded Edit/Plot variables from RELAP5/MOD2 calculations are not available from the restart file but must be collected as control variables.

In some cases liquid level data are compared as pressure differences. For the upper plenum and downcomer levels only bubble plot data shown in Ref 5 were available. These plots were converted into slightly smoothed elevation histories. Due to ambiguous plot data the resulting level behaviour is rather uncertain (Plots B.15 and B.16).

The early break flow was not qualified by the experiment until 50 s after the break, and showed rather large errors during the remainder of the transient. Predictions of mass inventory obtained through flow integration were therefore not carried out. For the energy balance, the steam generator heat transfer was not known, and could not be estimated by the steam produced.

2.4 Measurement Uncertainty

The experiment instrumentation involves a variety of transducers which may have different accuracies for the same kinds of quantities (Refs 5, 6). Table 4 is a summary of the accuracies of the measured quantities.

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2.5 Experimental Data Preparation

The preparation of the experimental data for plotting and uncertainty analysis required several steps of manipulation of the information. First of all, the data were copied from the original blocked tape files to the CDC standard display code.

A program, LOFTDEC, was developed to sort out the keyword and channel information to be used in the assessment work. The program also decimated the channel data by averaging over time intervals so that information was copied to an intermediate channel information file only every 2nd second up to 200 s after the break, and then every 5th second.

A program, R5SILFT, was developed to select data for desired channels from the intermediate data file. These data were transformed into a new file with the same format as a RELAP5 restart file. Experimental and predicted data could later on be similarly used in plotting and assessment.

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3 CODE AND MODEL DESCRIPTION

The assessment calculations with RELAP5/MOD2 for the LOFT L3-6 experiment were carried out using the cycle 36.04 code version. The code was implemented in June 1986 on a CDC 170-810 computer. The calculational model was based on available LOFT input files and listings, among those the L3-5 input (Ref 15). A number of geometrical model features were introduced as a result of findings in the L3-6 experiment.

3.1 Code Features

The descriptive document available for the RELAP5/MOD2 code is a rather detailed code manual (Ref 4). The main characteristics of the code are summarised in Table 5. A new feature of RELAP5/MOD2 is the cross junction which, according to code manual recommendations, was applied at the steam separator upstream volume and at the hot leg and cold leg vessel junctions.

3.2 Input Model

The preparation of the LOFT L3-6 input proceeded from an input of the closely similar L3-5 experiment which had earlier been assessed for ICAP (Ref 15). In its turn this input had been set up from a LOFT fast transient input and with additional updates from other available input listings (Refs 7, 8, 9).

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Changes introduced for the L3-6 calculations, compared with those of the L3-5 case, include new initial conditions, other trip times and a continuous operation of the main recirculation pumps. However, some changes in the calculation model are due to experiences gained during the L3-5 assessment. Reasons for particular approaches used in the calculation model are presented below. Figure 2 shows the nodalization used. The input files are given in Appendix A.

3.2.1-----Initial system pressure

To avoid an explicit steady-state pressurizer pressure and level control, the surge line junction was modeled as a trip valve which was closed until scram. The pressurizer initial conditions were satisfied with the correct fluid content and saturated water. Pressurizer heat structures were modeled with the outer surface at saturation temperature until scram and then at room temperature.

A time dependent volume was connected to the pressurizer surge line by a trip valve adjacent to the pressurizer bottom in order to maintain the initial primary pressure constant during the steady state calculation. During steady state the pressurizer was isolated from the surge line. The pressure of the time dependent volume was equal that of the pressurizer bottom volume. At scram the trip valve closed at the same time as the pressurizer isolation ceased.

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3.2.2 Primary fluid temperatures

The measured temperatures of the coolant circulating through the core and the steam generator show considerable variations from the standpoint of heat balance. This is particularly the case in the vessel downstream of the core. The same situation was also noticed during the L3-5 assessment (Ref 5). However, the L3-6 measurements of 577.1 K in the hot leg and 557.9 K in the cold leg fulfil the conservation of energy and are consequently accepted for the steady state. In the calculation the primary fluid temperatures are controlled through the steam generator operation and feed water temperature, see Section 3.2.7.

3.2.3 Core flow bypass

Several core bypass flows exist. Two of these (Ref 7) were modelled by servo valves adjusted for the correct flows until scram:

- the inlet annulus to upper plenum with 6.6 % of primary loop flow
- the lower plenum to upper plenum with 3.6 % of primary loop flow
- the reflood assist bypass valve leakage with 1.3 % of primary loop flows.

The leakage from the vessel cold leg inlet annulus to the upper plenum is caused by a flow path in the narrow gap between the filler blocks and the vessel wall. This leakage has a vertical extension equal to the cold leg nozzle diameter. To achieve a more realistic description in the case of stratification the leakage has been divided into two flow path junctions. One low path

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connects the volumes below the inlet and outlet at their upper ends, junction 297 in Figure 2. Similarly, the higher level volumes are connected at their bottom ends by a second junction, junction 296. This second leakage junction will preferably bypass steam in the case of void thus promoting a reduced leakage pressure difference.

3.2.4 Environmental heat losses

The exchange of heat with structure material is important in small break analysis. Since the initial input had only restricted material included, structures had to be added to the input. The bulk structures of the facility were modeled to represent the correct structural masses.

RELAP5/MOD2 does not facilitate an exterior surface heat transfer control during calculation. An environmental heat transfer coefficient had to be found by test calculations to obtain approximately the total heat loss of 250 kW as found in the experiment (Ref 7).

3.2.5 Break discharge coefficient

Test calculations show a too rapid decrease in the pressurizer inventory when the default subcooled discharge coefficient of unity was used. Applying a coefficient of .85 the rates of emptying the pressurizer and of the early system depressurization turned out close to the experimental values. The assumption that the pressurizer emptying rate is an indicator of the break discharge flow is only applicable for a low flow pressure drop in the surge line as it occurs in small break experiments. The pressurizer level during the emptying period is shown on Plot B.54.

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3.2.6-----Pump_model

The main circulation pumps were allowed to run at the constant initial speed during the L3-6 transient. The pump characteristics applied in the previous L3-5 calculation, which originated from an early LOFT base input (Ref 16), were also applied in the first two calculations, whereas modified two-phase characteristics were applied in the last calculation, Case C.

3.2.7-----Steam_generator

A RELAP5/MOD2 separator component is contained in the steam generator, see Figure 2 volume 520. The vapor outlet space above that volume is divided into two parallel and vertical volumes according to the recommendations of the code manual (Ref 4). Of these the one with the larger cross section area, volume 525, receives the steam from the separator component. This volume is connected by a cross-junction to the parallel volume 526, which has a smaller cross section area and which formally represents the downcomer top.

The steam generator initial conditions were established by using auxiliary components for the control of

- dome pressure
- downcomer water level
- rate of feedwater and steam mass flows
- recirculation ratio
- feedwater internal energy.

The dome pressure was controlled by a time dependent volume at the correct pressure and connected by an open junction to the steam dome. The

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downcomer level was regulated by the direction and flow rate through a time dependent junction connecting a time dependent volume with saturated water.

The initial feedwater mass flow rate, 27.8 kg/s, was obtained by using a time dependent junction. Moreover, the internal energy of the fluid in the time dependent volume, which delivers the feed water, was regulated by the steam flow generation rate which in its turn must be equal to the feedwater flow rate.

The initial main steam mass flow rate being equal to the feedwater mass flow rate is controlled by a time dependent junction. The flow rate during the valve closure, which starts at scram, is obtained from the valve characteristics (Ref 6) and a valve stem closure rate of 5 % per second. The reason for using this model is the simplicity by which the closed valve leakage can be calculated. Condie et al (Ref 7) estimated this leakage to be .120 kg/s at 4.5 MPa in the L3-6 experiment. At other pressures a linear dependence is assumed.

Unintentionally the steam valve partly let steam through from 89 s to 99 s after the break. The flow rate during this time interval was assumed to be correct by adjusting the steam lift so that a pressure drop rate close to the measured one (see Plot B.51) was found. The steam mass flow was during these 10 seconds only a few per cent of that for a fully opened valve.

The junction 516, Figure 2, at the bottom of the downcomer is modelled as a regulated valve to achieve an initial recirculation ratio of 4.7.

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4 THE BASE CASE CALCULATION

The base case (Case A) calculation could be carried without any urgent code problems. Thus a very limited computation mass error, Plot B.62, was saved up by the code. Still, however, the computation CPU time required was very extensive, Plot B.61, as a consequence of time step transport limit caused by the continuous main pump operation. Thus one separate calculation consumed about 18 h CPU time on a Cyber 170-810.

The system heat balance was initially dominated by the reactor power, Plot B.2, which was mainly carried over to the steam generator secondary, Plot B.53. The predicted initial heat loss to the environments, was 260 kW, which is close to the 250 kW estimated in the experiment (Ref 7).

The heat generated in the core after scram was determined by the space independent reactor kinetics option of the code. The predicted decay heat, Plot B.2, compares well with the decay heat curve given in Ref 5.

The mass flow rates predicted in the hot leg, Plot B.25, and at the core inlet, Plot B.11, show a smooth decrease during the transient which is mainly a result of the decrease of the fluid density. Unfortunately no internal flow rates in the experiment are qualified for comparisons after the break opened.

The predicted break mass flow rate, Plot B.39, is within the uncertainty band of the measured flow rate from 100 s on, see Ref 5. The experimental flow rate is qualified from 50 s. In the interval from 50 s to 100 s after the break the

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predicted break mass flow rate is apparently overestimated, however, some doubt may also be put on the experimental flow rate. During this time interval there is good agreement between the predicted break fluid density and the chordal density measurement, Plot B.38. Whereas the break fluid subcooled period ends at 44 s in the experiment, it is predicted to occur much later, at about 200 s, in the calculation, Table 2.

The behaviour of the main recirculation pumps is showing up in the pressure head, Plot B.36. An obvious cavitation in the experiment occurs at 290 s at which time also the loop seal becomes filled with water, Plot B.31, and the steam generator pressure difference, Plot B.46, rapidly diminishes (Ref 12). In addition effects from the cavitation in the experiment can be seen in the pump speed, Plot B.37, in the cold leg fluid density, Plot B.28, and in the break fluid density, Plot B.38. A pump cavitation is not predicted at the time it occurred in the experiment. On the other hand the prediction shows an earlier pump head loss when the two-phase fluid starts to appear in the suction line, Plot B.36.

The primary side depressurization, as in the hot leg, Plot B.27, is slightly underpredicted from 300 s on. Pressures at high elevations, Plots B.21 and B.57, compare similarly. System pressures at low elevations as in the lower plenum, Plot B.22, and also in the cold legs, Plots B.34 and B.35, are still more underpredicted. As seen, there might be a systematic error in the prediction. However, the discrepancies are within the measurement errors, Table 4.

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After the fast depressurization has ceased the primary fluid temperatures remain close to the saturation temperature, Plots B.9, B.17, B.18, B.20, B.26, B.33 and B.44. Minor deviations from this situation are due to errors in the measured temperatures, Table 4, and by the HPIS coolant injection.

As for the pressure, the predicted underestimate of primary temperatures for the rods, Plots B.3 through B.8, and for the fluid, Plots B.9, B.17, B.18, B.20, B.26, B.33, B.41 and B.44, increase in time. A possible reason for that is the uncertainty, 15 % up to 1 435 s, in the measured break flow and consequently also in the primary enthalpy content.

There is one plainly seen inconsistency in the secondary side prediction of Case A. The down-comer collapsed level, Plot B.49, falls about .6 m too low until the level starts to recover due to the injected auxiliary feedwater. This early level error, which corresponds to about 150 kg of fluid mass, then remains during all the transient. Secondly, too fast a depressurization particularly at the end of the transient is predicted, Plot B.51. Similar predicted pressure behaviours were obtained by the participants of the ISP11 (Ref 13) which also dealt with the L3-6 experiment. Consequently there are reasons to assume some inadequacy to be found in the commonly used steam generator models.

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Several causes for the low fluid content may be suggested, including errors in the feedwater valve operation timing and the steam valve leakage. The void distribution in the boiling section may be wrong due to the geometric model used. Moreover, a non-negligible amount of water droplets may initially reside in the dome space above the fluid level of the steam separator volume.

The predicted pressurizer fluid temperatures in the liquid space, Plot B.55, and in the vapor space, Plot B.56, show substantial deviations from the experiment. In the liquid space the computed water temperature, close to the saturation line, was compared with apparently superheated steam sensed in the experiment. The computed steam superheating, Plot B.56, was not large enough. An other possible explanation, would be some direct influence from the pressurizer vessel wall in the experiment.

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5 SENSITIVITY CALCULATIONS

The base case prediction displayed some deviations from the experiment which provide arguments for the sensitivity studies. A fluid temperature and system pressure decrease faster than in the experiment is in the first place assumed to be a consequence of the steam generator behaviour or simply of the choice of break discharge coefficient. In the Case B predictions the steam generator model is changed. The sudden pump cavitation in the experiment was not predicted. Consequently one calculation, Case C, applied other pump characteristics.

5.1 Case B

Steam generators are supposed to act as the dominant heat sinks during small break transients. However, the 4-in. diameter equivalent L3-6 experiment shows a substantial depletion of coolant through the break so the steam generators become less important as heat sinks, ref 5. Actually the steam generator heat transfer rate, Plot B.53, compared with the break energy release, Plot B.40, and the structure heat losses, Plot B.2, confirms that. Thus, the behaviour of the steam generator will be of less importance for the primary side cooling.

The steam generator design, Figure 3, exhibits a package of U-tubes which are supported by horizontal plates at equidistant heights. These plates have possibly been understood to be impenetrable for fluid thus bringing the geometry found in the Case A input. Then the boiler flow is forced to a zigzagged flow path directed by the plates. In reality the tube support plates are ported to permit penetration of steam and water (Ref 6).

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Consequently the boiling section flow was directed vertically in the Case B calculations. A more efficient void rise indeed increased the initial fluid mass by 90 kg. Further division of the boiler flow into two parallel paths, one with the ascending primary flow and one with the descending flow, added another 50 kg initial fluid mass. Although the changes in the boiler geometry increased the amount of initial water a lot, it accounted only for part of the fluid mass missing in the Case A calculation. According to Plot B.49 the discrepancy in liquid level between prediction and experiment increased with time in Case B contrary to Case A.

The transport time from the feedwater inlet to the downcomer bottom is quite short in the initial state. The liquid temperature at the downcomer bottom, Plot B.50, indicates that the feedwater valve closure starts later than at the scram. Consequently in the Case B calculation a feedwater valve closure starting at the HPIS trip signal was additionally applied. As a result another 70 kg of water was added to the fluid mass, Plot B.49.

5.2 Case C

The previous two calculations predicted from 300 s on a slightly faster decrease in primary system pressure and in fluid temperature than measured. On the other hand were fluid densities, Plots B.23, B.24, B.28, B.29, B.30 and B.38, reasonably well predicted. Discrepancies from the experiment starting at 290 s are more evident in the loop seal liquid level, Plot B.31, and in the downcomer liquid level, Plot B.15, as the pumps start to cavitate, Plot B.36. Obviously,

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the accumulation of water in low elevation areas of the loop starts with the cavitation. This is the time at which the discrepancy in the depressurization rate starts off.

The two-phase pump head, Plot B.36, was underpredicted in the Cases A and B. Chen (Ref 12) and Modro and Chen (Ref 14) found less degradation for mainly all void fractions compared with the pump characteristics of the LOFT base case input (Ref 16) so far assumed. Because of that the same pump data as those used by Grush et al. (Ref 8) were applied in the sensitivity calculation Case C. These data had been obtained from Chen's and Modros' works. In Case C also the updates of Case B were included.

The new two-phase pump characteristics resulted in a better prediction of the pump head, Plots B.36 and B.46. At the time of the pump cavitation, at 290 s, a rapid head loss appeared in Case C too. However, as before in the Cases A and B, the pump head turned out underpredicted during almost all the transient. In the same way the liquid levels in the downcomer, Plot B.15, and in the loop seal, Plot B.31, did not show any better agreement with the experiment.

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6 RUN STATISTICS

The input model for the base case RELAP5/MOD2 calculation for LOFT L3-5 encompassed:

113	volumes
122	junctions
99	heat structures

The volumes include two pump components, one separator component and nine time dependent volumes of which three were involved for the steady state. Among the junctions there are totally five valve components and four time dependent junctions which are connected during steady state.

During the transient calculation the following resources were used:

computer time	CPU = 58 675 s
number of time steps	DT = 36 920
number of volumes	C = 113
transient real time	RT = 2 150 s

resulting in the following code efficiency factor (Ref 1)

$$\frac{\text{CPU} * 10^3}{\text{C} * \text{DT}} = 14.06$$

The computer used was a Cyber 170-810.

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7 CONCLUSIONS

The LOFT L3-6 small break experiment has been calculated using the RELAP5/MOD2 code as part of Sweden's contribution to ICAP. The results from the three calculations done compare reasonably well with most of the experimental data. None of the sensitivity calculations has the capacity of considerably increasing the prediction quality. Consequently all three calculations show mostly rather similar curves jointly away from the measurements. Some more calculations had been desirable but could not be afforded.

The steady state calculation was done in the common way of applying auxiliary components and regulators to speed up and stabilize. Acceptance of a steady state followed when all the auxiliaries had lost importance for the subsequent calculations. Of a particular significance was the temperature regulation of the feedwater to achieve the correct steam generation rate.

One sensitivity calculation, Case B, addressed the question of why initial secondary side fluid content had been considerably underestimated in the base case calculation. The two updates of a vertical boiler flow and of a delayed feed water valve closure were not capable to fully rise the low downcomer liquid level up to the measured value. Actually, the reason for the low predicted fluid content of the secondary side was not fully understood.

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The other sensitivity calculation, Case C, focused on the behaviour of the main recirculation pumps which were allowed to run at a constant speed during the experiment. Updates in the two-phase characteristics improved the prediction of the pump head in the crucial degradation region. However, no other substantial improvements obviously turned out from this calculation.

The RELAP5/MOD2 code worked well during the calculations. The computer resources, made available by the Swedish Nuclear Power Inspectorate, were quite extensive for this assessment test case.

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- 16 KEE, E J et al
Base Input for LOFT RELAP5 Calculations.
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Table 1

Initial conditions.

Quantity		Measured	Case A	Predicted Case B	Case C
Primary coolant system					
Mass flow rate	(kg/s)	483.3	483.3	483.3	483.3
Hot leg pressure	(MPa)	14.87	14.88	14.88	14.88
Cold leg temperature	(K)	557.9	559.7	560.4	560.4
Hot leg temperature	(K)	577.1	578.6	579.3	579.4
Reactor vessel					
Power level	(MW)	50.	50.	50.	50.
Pressurizer					
Water temperature	(K)	614.7	614.8	614.8	614.8
Pressure	(MPa)	14.90	14.90	14.90	14.90
Liquid level	(m)	1.18	1.18	1.18	1.18
Broken loop					
Cold leg temperature	(K)	557.6	559.6	560.6	560.6
Hot leg temperature	(K)	561.4	557.8	556.1	556.1
SG secondary side					
Water level	(m)	0.22	0.22	0.22	0.22
Water temperature	(K)	542.8	534.4	536.0	535.9
Pressure	(MPa)	5.57	5.57	5.57	5.57
Mass flow rate	(kg/s)	27.8	27.8	27.8	27.8

Table 2

Sequence of events.

Event	Imposed action	System reaction	Time (s)		
			Case A	Predicted Case B	Case C
Reactor scrammed	-5.8		-5.8	-5.8	-5.8
LOCA initiated	0.		0.	0.	0.
HPIS injection initiated		3.6	2.3	2.6	2.6
Prssurizer emptied		20.2	25.4	25.4	25.4
Upper plenum reached saturation		28.5	40.	40.	40.
Intact loop hot leg voidin begin		29.4	38.7	38.9	39.1
Intact loop cold leg voidin begin		31.4	35.	35.	35.
End of subcooled break flow		44.2	91.6	91.6	91.6
SCS auxiliary feed initiated	73.4		73.4	73.4	73.4
SCS pressure exceeds primary pressure		930.	1925.	1720.	1740.
SCS auxiliary feed terminated	1856.		1856.	1856.	1856.

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Table 3

Parameters plotted and used in assessment comparisons.

COMPONENT	CONTINUOUS PARAMETER *	EXPERIMENT (IDENTIFIER)	PREDICTION (MINOR EDIT)	PLOT IDENTIF. EXP. CALC.	PLOT NO.	
CORE	FLUID DENSITY (INLET)	**	CNTRLVAR 901	C 17	B. 1	
	HEATING POWER	**	RKTPOW 0	C 27	B. 2	
	CLAD TEMPERATURE, VOLUME 1 (BOTTOM)	TE-2G14-011 TE-5G6-011 TE-516-005	CNTRLVAR 903	C 3X C 37	B. 3	
	- " - , VOLUME 2	TE-1F7-015 TE-1F7-021 TE-2G08-021 TE-4I14-021 TE-5F4-015 TE-516-021	CNTRLVAR 903	C 4X C 47	B. 4	
	- " - , VOLUME 3	TE-1F7-026 TE-1F7-030 TE-2G14-030 TE-2H02-032 TE-4H14-028 TE-4H14-032 TE-5H7-026	CNTRLVAR 905	C 5X C 57	B. 5	
	- " - , VOLUME 4	TE-2G08-039 TE-2H01-037 TE-3C11-039 TE-4I14-039 TE-5H6-037	CNTRLVAR 906	C 6X C 67	B. 6	
	- " - , VOLUME 5	TE-2G14-045 TE-4G14-045 TE-5F9-045 TE-5G6-045 TE-5H5-049	CNTRLVAR 907	C 7X C 77	B. 7	
	- " - , VOLUME 6 (TOP)	TE-5H7-058 TE-5G6-062	CNTRLVAR 908	C 8X C 87	B. 8	
	TEMPERATURE (OUTLET)	TE-1UP-001 TE-5UP-001 TE-5UP-003	CNTRLVAR 909	C 9X C 97	B. 9	
	TEMP. DIFF. (OUTLET-INLET)	TE-1UP-001 - TE-1LP-001	CNTRLVAR 910	C AX C A7	B.10	
	CORE FLOW (INLET)	**	MFLOWJ 225.01	C B7	B.11	
	CORE INVENTORY	PDE-RV-002 **	CNTRLVAR 912	C C7	B.12	
	VESSEL	DOWNCOMER MASS INVENTORY	PDE-RV-003 **	CNTRLVAR 913	V 17	B.13
		MASS INVENTORY (TOTAL VESSEL)	**	CNTRLVAR 914	V 27	B.14
		DOWNCOMER LIQUID LEVEL	LE-1ST-001 ***	CNTRLVAR 915	V 3X V 37	B.15
UPPER PLENUM LIQUID LEVEL		LE-3UP-001 ***	CNTRLVAR 916	V 4X V 47	B.16	
DOWNCOMER TEMPERATURE (INLET)		TE-1ST-001 TE-2ST-001	TEMPF 205	V 5X V 57	B.17	
UPPER PLENUM TEMPERATURE		TE-1UP-001 TE-4UP-001 TE-5UP-001	TEMPF 240	V 6X V 67	B.18	
UPPER PLENUM FLUID SUBCOOLING		SC-5UP-102	CNTRLVAR 919	V 7X V 77	B.19	
LOWER PLENUM TEMPERATURE		TE-1LP-001	TEMPF 225	V 8X V 87	B.20	
UPPER PLENUM PRESSURE		PE-1UP-001A1	P 245	V 9X V 97	B.21	
LOWER PLENUM PRESSURE		PE-1ST-001A PE-2ST-001A	P 225	V AX V A7	B.22	
HOT LEG	FLUID DENSITY (I.L.)	DE-PC-205 ** DE-PC-002A ** DE-PC-002B ** DE-PC-002C **	RHO 105	HL1X HL17	B.23	
	FLUID DENSITY (B.L.)	DE-BL-002B	RHO 305	HL2X HL27	B.24	
	MASS FLOW RATE	FT-P139-27-1 ** FT-P139-27-2 ** FT-P139-27-3 **	MFLOWJ 110	HL37	B.25	
	TEMPERATURE (I.L.)	TE-PC-002B	TEMPF 105	HL4X HL47	B.26	
	PRESSURE (I.L.)	PE-PC-002	P 105	HL5X HL57	B.27	

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Table 3 (cont'd)

COLD LEG	FLUID DENSITY (I.L.)	DE-PC-115 DE-PC-001A DE-PC-001B DE-PC-001C	**	RHO 185	CL1X	CL17	B.28	
	FLUID DENSITY (I.L. PUMP SUCTION)	DE-PC-305 /DE-PC-003A/ /DE-PC-003B/ /DE-PC-003C/	**	RHO 115.13	CL2X	CL27	B.29	
	FLUID DENSITY (B.L.)	DE-BL-105 DE-BL-001A DE-BL-001B DE-BL-001C	**	RHO 345	CL3X	CL37	B.30	
	LIQUID LEVEL (I.L. LOOP SEAL)	LEPDE-PC-028		CNTRLVAR 931	CL4X	CL47	B.31	
	- " - (B.L.)	LEPDE-BL-014	**	CNTRLVAR 932		CL57	B.32	
	TEMPERATURE (I.L. NEAR VESSEL)	TE-PC-004		TEMPF 185	CL6X	CL67	B.33	
	PRESSURE (I.L.)	PE-PC-005		P 120	CL7X	CL77	B.34	
	- " - (B.L.)	PE-BL-001		P 345	CL8X	CL87	B.35	
	PRESS. DIFF. (ACROSS THE PUMPS)	PDE-PC-001		CNTRLVAR 936	CL9X	CL97	B.36	
	PUMP SPEED (PUMP 1)	RPE-PC-001		PMPVEL 135	CLAX	CLA7	B.37	
	BREAK	FLUID DENSITY	DE-PC-S02A		RHO 800	BR1X	BR17	B.38
		MASS FLOW RATE	FR-PC-SBRK		MFLOWJ 805	BR2X	BR27	B.39
		ENERGY RELEASE	**		CNTRLVAR 940		BR37	B.40
INLET TEMPERATURE		TE-PC-S01C		TEMPF 800	BR4X	BR47	B.41	
INLET SUBCOOLING		ST-PC-S101 - TE-PC-S01C		CNTRLVAR 942	BR5X	BR57	B.42	
INLET PRESSURE		PE-PC-S01		P 800	BR6X	BR67	B.43	
SG PRI. SIDE		TEMPERATURE (INLET)	TE-SG-001		TEMPF 115.03	SP1X	SP17	B.44
	TEMP. DIFF. (INLET-OUTLET)	TE-SG-001 - TE-SG-002		CNTRLVAR 945	SP2X	SP27	B.45	
	PRESSURE DIFF.	PDE-PC-002		CNTRLVAR 946	SP3X	SP37	B.46	
SG SEC. SIDE	FLUID DENSITY	**		RHO 515.03		SS17	B.47	
	MASS FLOW RATE	**		MFLOWJ 516		SS27	B.48	
	LIQUID LEVEL	LD-P004-008B		CNTRLVAR 949	SS3X	SS37	B.49	
	LIQUID TEMPERATURE	TE-SG-003		TEMPF 515.03	SS4X	SS47	B.50	
	PRESSURE	PE-SGS-001		P 530.01	SS5X	SS57	B.51	
SG	PRIMARY-SECONDARY TEMP.-DIFF. (AT INLET)	TE-SG-001 - TE-SG-003		CNTRLVAR 952	S 1X	S 17	B.52	
	HEAT TRANSFER RATE	**		CNTRLVAR 953		S 27	B.53	
PRESSURIZER	LIQUID LEVEL	LT-P139-006		CNTRLVAR 954	P 1X	P 17	B.54	
	LIQUID TEMPERATURE	TE-P139-020		TEMPF 415.02	P 2X	P 27	B.55	
	STEAM TEMPERATURE	TE-P139-019		TEMPG 415.07	P 3X	P 37	B.56	
	PRESSURE	PE-PC-004		P 415.08	P 4X	P 47	B.57	
ECCS	HPIS VOLYMERIC FLOW RATE	FT-P128-104		CNTRLVAR 958	EC1X	EC17	B.58	
SYSTEM	MASS BALANCE			CNTRLVAR 959		SY17	B.59	
	COOLANT EGY. BALANCE (INTEGR.)	**		CNTRLVAR 960		SY27	B.60	
	PRIM. EXTERNALS HEATFLOW	**		CNTRLVAR 982		SY37	B. 2	
RELAPS	COMPUTATION CPU TIME	**		CPUTIME 0		R 17	B.61	
	COMPUTATION MASS ERROR	**		EMASS 0		R 27	B.62	

* THE COMPARISON PARAMETERS ARE THOSE REPORTED AS DIRECTLY MEASURED OR AS COMPUTED RESULTS FROM THE EXPERIMENT

** NO DATA AVAILABLE FROM THE EXPERIMENT

*** DATA OBTAINED FROM BUBBLE PLOT IN EXPERIMENT REPORT

// EXPERIMENT DATA AVAILABLE BUT NOT USED IN COMPARISONS

? CALCULATION CASE (A, B OR C)

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Table 4

Measurement errors

Quality	Uncertainty	Comment
Pressure	251-282 kPa 120 kPa	Primary side Secondary side
Fluid temp	2.7-3.1 K .5 K 5.9 K 10.4 K	Mostly TE-P139-019, steam TE-SG-001, TE-SG-002 TE-PC-004
Fluid density	78-82 kg/m ³ 129-131 kg/m ³	Many measure DE-BL-001A, DE-BL-001C DE-PC-002B, DE-PC-002C
Cladding temp	3.1-3.2 K	All
Diff Pressure	.49 k Pa 1. kPa 1.3 kPa 1.8 kPa	PDE-RV-003 PDE-PC-002 PDE-RV-002 PDE-PC-001
Mass flow	.02 L/s 6.3 kg/s 17 kg/s 25 percent 1 kg/s	HPIS I.L. init condition I.L. hot leg Break, 40-750 s Break, 750-2100 s
Liq level	.04 m .05 m .099-.137 m Bubble plot	Pressurizer SG secondary Cold legs Upper plen, downcomer
Speed	1.22 rad/s	Main recirc pumps

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Table 5

RELAP5/MOD2 code features.

COMPUTATION PROCESSING FEATURES

- Several problem type and execution control options as
 - a. steady state initialisation using fictitious structure heat capacities for faster convergence
 - b. transient calculation
 - c. strip type execution, to select requested parameters from a restart file
 - d. trip system, to decide on actions during calculation due to reaching specified conditions in calculation parameters.
 - e. ability to delete or add hydrodynamic components, structure components and control variables at a restart of calculation.

CLASSIFICATION OF HYDRODYNAMIC MODEL

- One-dimensional, with provisions for
 - a. choked flow model
 - b. abrupt area change model
 - c. cross flow junctions.
- Two-fluid, six equation, space-time numerical solution scheme.
- flow regime oriented field characteristics depending on mass flux and void fraction for
 - a. horizontal flow with bubbly, slug, mist and stratified fields
 - b. vertical flow with bubbly, slug, annular-mist (and stratified) fields
 - c. high mixing flow with bubbly and mist fields (for pumps).

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Table 5 cont'dHYDRODYNAMIC COMPONENTS (Input systematics)

- Volume type components
 - a. single volume
 - b. pipe and annulus, for condensed input of several similar single volumes
 - c. time dependent volume, for defining a boundary source with a time dependent fluid state
 - d. branch, a volume capable of two or more connecting junctions at either end
 - e. pump, characterized by rated values for flow, head, torque, density and moment of inertia. The single phase homologous curve, two-phase multipliers and phase difference tables to model the dynamic pump behaviour
 - f. special system components for steam separator, jetmixer, turbine and accumulator.
- Junction type components
 - a. single junction
 - b. time dependent junction, for a time dependent junction flow with a time dependent or controlled flow state
 - c. cross-flow junction, to model a small cross flow, a tee branch or a small leak flow
 - d. valve, various operation characteristics available for check valve, trip valve, inertial valve and relief valve.

INTERPHASE CONSTITUTIVE EQUATIONS

- Interphase drag
 - a. steady drag due to viscous shear depending on flow regime. Semi-empirical mechanisms to describe flow regime transitions
 - b. dynamic drag due to virtual mass effect.
- Interphase mass and heat transfer depending on flow regime and the fluid fields to saturation temperature differences

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Table 5 cont'dFLUID TO WALL CONSTITUTIVE EQUATIONS

- Wall friction due to wall shear effects formulated for flow regimes and based on a two-phase multiplier approach.

- Wall heat transfer depending on flow characteristics defined for
 - a. single-phase forced convection (Dittus-Boelter)
 - b. saturated nucleate boiling (Chen)
 - c. subcooled nucleate boiling (modified Chen)
 - d. critical heat flux (Biasi or modified Zuber)
 - e. transition film boiling (Chen)
 - f. film boiling (Bromley-Pomeranz and Dougall-Rohsenow)
 - g. condensation (partly Dittus-Boelter).

- Interfacial mass transfer at the wall depending on wall, fluid and saturation temperatures for
 - a. subcooled and saturated boiling
 - b. transition film and film boiling
 - c. condensation.

HEAT STRUCTURES

These may be rectangular, cylindrical or spherical in shape. The structure position is defined through component numbers of left and right hand side hydraulic components. A structure is physically defined by the geometry and the temperature dependent conductivity and volumetric heat capacity data. The structure model is further specified by the number of internal mesh points in the direction of heat flow.

CONTROL COMPONENTS

By these new (control) variables are defined from calculated parameters using algebra, standard functions, trip type operands or integrals.

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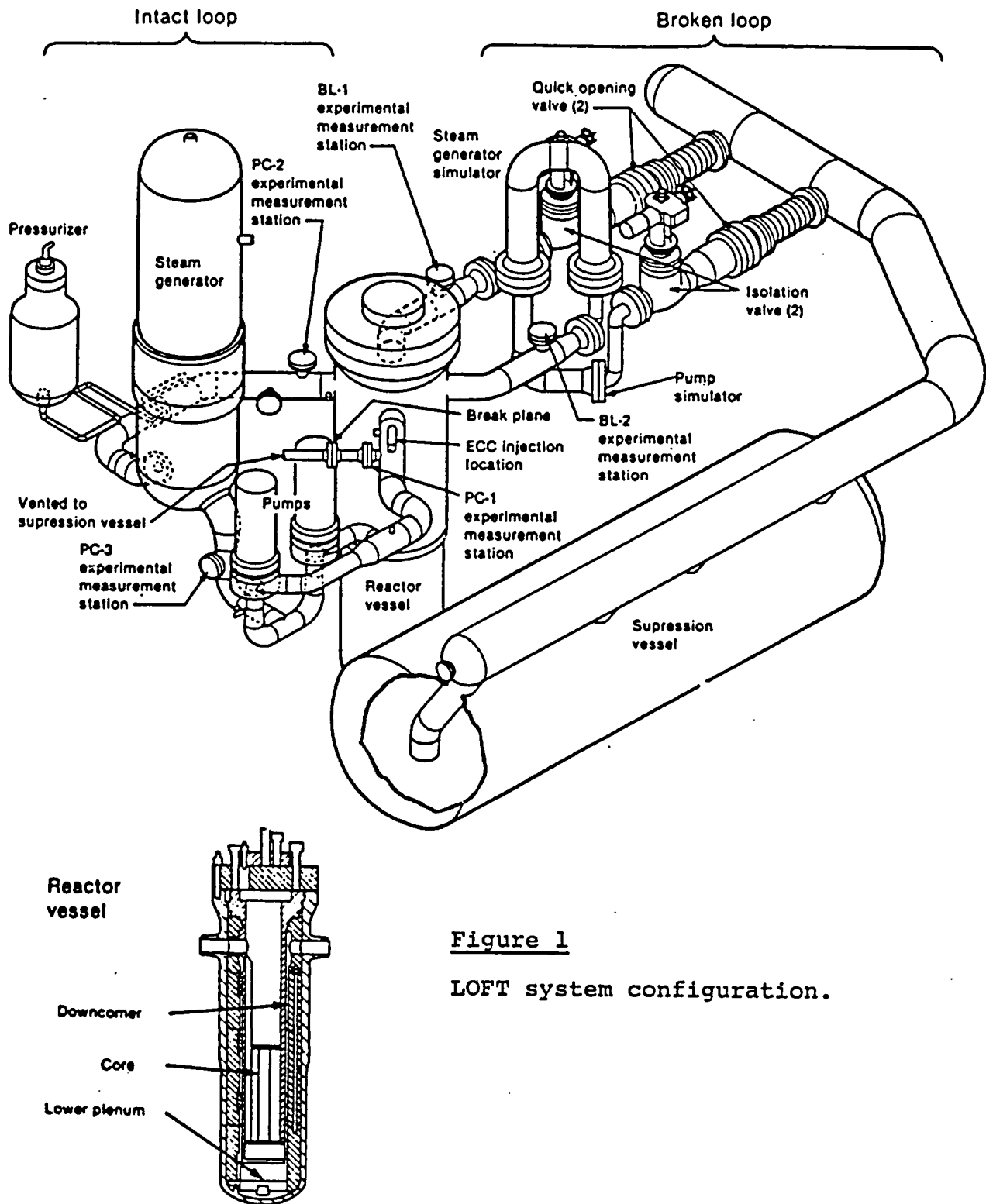


Figure 1

LOFT system configuration.

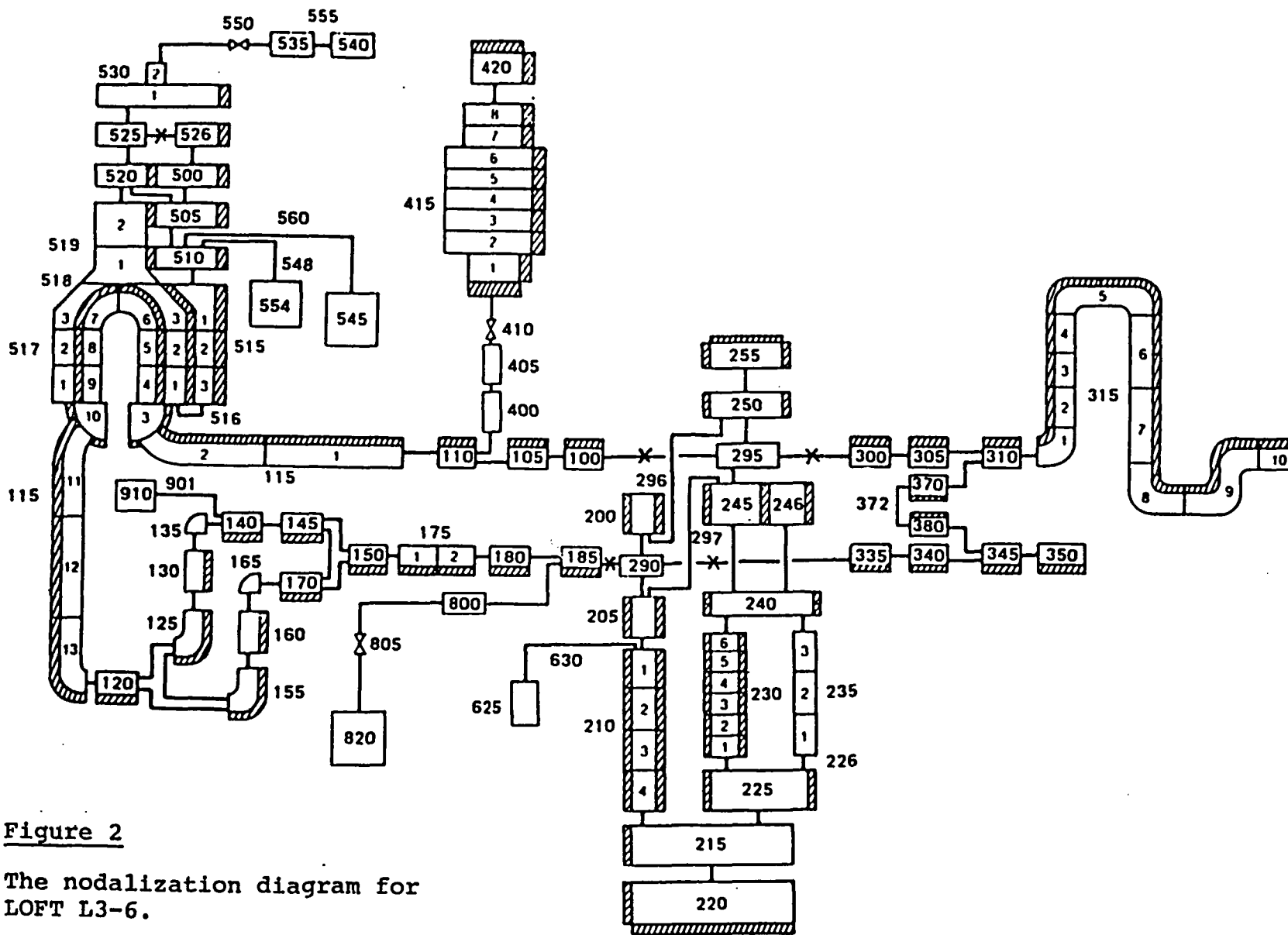


Figure 2

The nodalization diagram for LOFT L3-6.

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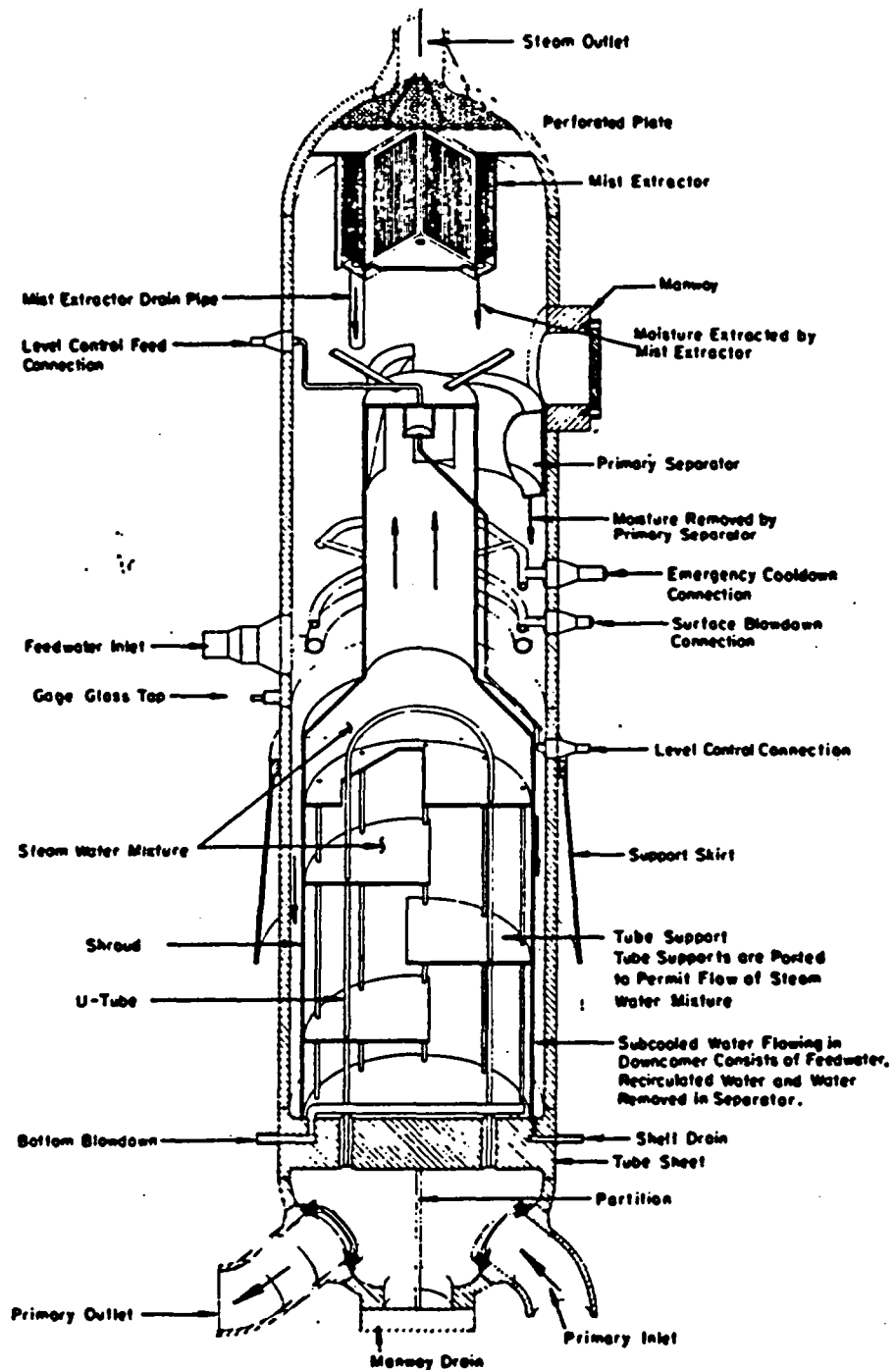


Figure 3'

The LOFT steam generator.

```

* * LOFT L3-S ANALYSIS (PRIMARY-SECONDARY-KINTCS) * *
*****
0000100 NEW      STDY-ST
0000101 RUN
0000102 SI      SI
0000104 NOACTION
0000105 120.    200.0
0000120 100010000 0.0      WATER  PRIMARY
0000121 517010000 0.0      WATER  SECONDARY
0000201 TIME END  MIN STP  MAX STP  EDT OPT  MNOR  MAJR  RST
          144.2    1.0E-5    .20    00001  25    4000  4000
*****
* MINOR EDIT VARIABLES FOR THE ICAP ASSESSMENT
*****
* CORE
0000301 CNTRLVAR 901
0000302 RKTPOW  0
0000303 CNTRLVAR 903
0000304 CNTRLVAR 904
0000305 CNTRLVAR 905
0000306 CNTRLVAR 906
0000307 CNTRLVAR 907
0000308 CNTRLVAR 908
0000309 CNTRLVAR 909
0000310 CNTRLVAR 910
0000311 MFLOWJ  225010000
0000312 CNTRLVAR 912
*****
* VESSEL
0000313 CNTRLVAR 913
0000314 CNTRLVAR 914
0000315 CNTRLVAR 915
0000316 CNTRLVAR 916
0000317 TEMPF  205010000
0000318 TEMPF  240010000
0000319 CNTRLVAR 919
0000320 TEMPF  225010000
0000321 P      245010000
0000322 P      225010000
*****
* HOT LEG
0000323 RHO    105010000
0000324 RHO    305010000
0000325 MFLOWJ 110010000
0000326 TEMPF  105010000
0000327 P      105010000
*****
* COLD LEG
0000328 RHO    185010000

```

```

0000329 RHO    115020000
0000330 RHO    345010000
0000331 CNTRLVAR 931
0000332 CNTRLVAR 932
0000333 TEMPF  185010000
0000334 P      120010000
0000335 P      345010000
0000336 CNTRLVAR 936
0000337 PHVEL   135
*****
* BREAK
0000338 RHO    185010000
0000339 MFLOWJ  805000000
0000340 CNTRLVAR 940
0000341 TEMPF  800010000
0000342 CNTRLVAR 942
0000343 P      185010000
0000344 TEMPF  115030000
*****
* STEAM GENERATOR
0000345 CNTRLVAR 945
0000346 CNTRLVAR 946
0000347 RHO    515030000
0000348 MFLOWJ  516000000
0000349 CNTRLVAR 949
0000350 TEMPF  515030000
0000351 P      530010000
0000352 CNTRLVAR 952
0000353 CNTRLVAR 953
*****
* PRESSURIZER
0000354 CNTRLVAR 954
0000355 TEMPF  415020000
0000356 TEMPG  415070000
0000357 P      415040000
*****
* ECCS
0000358 CNTRLVAR 958
*****
* SYSTEM
0000359 CNTRLVAR 959
0000360 CNTRLVAR 960
0000362 CNTRLVAR 962
*****
* RELAPS
0000361 CPU TIME  0
0000362 EMASS    0
*****
* STEADY STATE CONTROLS
0000370 CNTRLVAR 278
0000371 CNTRLVAR 296
0000372 CNTRLVAR 372
0000373 CNTRLVAR 291
0000374 CNTRLVAR 216
0000375 CNTRLVAR 601
0000376 CNTRLVAR 606
0000360 CNTRLVAR 960
0000382 CNTRLVAR 982

```

```

*****
* TRIP INPUT DATA
0000601 SCRAM REACTIVITY, GEN. TABLE 608
          SS AUX PRESSURIZ, VALVE CLOS 410
          MAIN STEAM VALVE, CLOSE 550
          FEED WATER VALVE, CLOSE 550
0000610 BREAK TIME AUX FEED WATER 548
0000611 TRIP PUMP 1 135
          PUMP 2 165
0000614 BREAK CLOSE 805
0000615 AFTER EXPERIMENT END
0000618 MFLOW DIRECTION OF FLOW FROM CORE 240
0000635 SO S EXP. BREAK FLOW QUALIFIED 805
0000600 STOP ADV. OF CALCULATION
0000645 BREAK OPEN 805
0000646 PRESS. VALVE OPEN, AFTER SS 435
0000661 MPIS INITIATED 640
0000699 PUMP COOLANT INJECTION 901
*****
001 TIME 0 GE NULL 0 144.2 J
008 TIME 0 GE NULL 0 0.0 J
010 TIME 0 GE TIMEOF 501 5.8 J
011 TIME 0 GE TIMEOF 510 10000. J
012 TIME 0 GE NULL 0 10000. J
013 P 100010000 LE NULL 0 13.2E6 J
014 P 100010000 LE NULL 0 2.15E6 J
015 0 GE TIMEOF 514 20. J
018 VELFJ 240010000 GE NULL 0 0.0 J
020 P 530020000 GT NULL 0 5.63E6 J
021 P 530020000 LT NULL 0 5.61E6 J
022 P 530020000 GT NULL 0 5.55E6 J
023 P 530020000 LT NULL 0 5.53E6 J
030 CNTRLVAR 10 LT NULL 0 3.10 J
031 CNTRLVAR 10 GT NULL 0 3.18 J
035 TIME 0 GE TIMEOF 510 50. J
033 TIME 0 GT TIMEOF 510 63. J
061 P 100010000 GT P 530020000 0. J
062 TIME 0 GE TIMEOF 660 1800. J
060 0
060 514 AND 561 N
061 513 AND -514 N
069 -514 AND -514 N
0601 530 OR 602 N
0602 -531 AND 601 N
0603 562 AND 602 N
0610 612 OR 520 N

```

611	-521	AND	-616	N
612	611	AND	610	N
613	616	OR	523	N
614	-522	AND	613	N
615	-612	AND	601	N
616	616	AND	614	N
633	633	AND	-660	N
634	633	OR	603	N
634	610	AND	610	L
645	610	AND	-614	N
546	-601	AND	-601	N

 INTACT LOOP

 REACTOR VESSEL NOZZLE INTACT LOOP HOT LEG

 1000000 RWIIML BRANCH
 1000001 2 1
 1000101 0.0634 1.5373 0.0 0.0 0.0 0.0
 1000102 4.0E-5 0.0 DO
 1001101 295010000 100000000 0.0634 0.1 0.1 0.102
 1002101 100010000 105000000 0.0 0.085 0.085 0.100

 PRESSURIZER CONNECTION TEE REACTOR VESSEL SIDE

 1050000 PACTRVS BRANCH
 1050001 1 1
 1050101 0.0634 1.634 0.0 0.0 0.0 0.0
 1050102 4.0E-5 0.0 DO
 1051101 105010000 110000000 0.0 0.085 0.085 0.100

 STEAM GENERATOR INLET PIPING

 1100000 SGIMLP BRANCH
 1100001 1 1
 1100101 0.0 1.1303 0.06204 0.0 0.0 0.0
 1100102 4.0E-5 0.0 DO
 1101101 110010000 115000000 0.0 0.17 0.17 0.100

 STEAM GENERATOR PLUS PIPING

 1150000 SCAPS PIPE
 1150001 13
 1150101 0.0 3
 1150102 0.151 9
 1150103 0.0 12
 1150104 0.0634 13
 1150201 0.0 1
 1150202 0.0512 2
 1150203 0.0 9
 1150204 0.0512 10
 1150205 0.0 12
 1150301 0.09124 1

1150302	0.708	2
1150303	0.63	3
1150304	1.0022	4
1150305	0.7102	5
1150306	0.8576	6
1150307	-7102	7
1150308	1.0022	8
1150309	0.63	10
1150310	0.647	11
1150311	0.689	12
1150312	0.559	13
1150401	0.05826	1
1150402	0.057	2
1150403	0.223	3
1150404	0.0	9
1150405	0.223	10
1150406	0.0437	11
1150407	0.0462	12
1150408	0.0	13
1150501	0.0	13
1150601	0.0	1
1150602	90.0	6
1150603	-90.0	13
1150701	0.0	1
1150702	0.246	2
1150703	0.613	3
1150704	1.0022	4
1150705	0.498	11
1150706	0.7102	5
1150707	-0.8576	6
1150708	-7102	7
1150709	-1.0022	8
1150710	-0.513	9
1150711	-0.498	11
1150712	-0.689	12
1150713	-0.356	13
1150801	4.0E-5	0.0 2
1150802	4.0E-5	0.0102 3
1150803	1.0E-5	0.0103 9
1150804	4.0E-5	0.0102 10
1150805	4.0E-5	0.0 13
1150901	0.255	0.255 1
1150902	0.048	0.048 2
1150903	0.0	0.0 4
1150904	0.096	0.096 5
1150905	0.192	0.192 6
1150906	0.096	0.096 7
1150907	0.0	0.0 9
1150908	0.048	0.048 11
1150909	0.096	0.096 12
1151001	0.0	13
1151101	0.100	3
1151102	0.000	8
1151103	0.100	12
1151300	1	

 PUMP SUCTION TEE

 1200000 PSTEE BRANCH
 1200001 3 1
 1200101 0.0634 0.76 0.0 0.0 0.0 0.0
 1200102 4.0E-5 0.0 DO
 1201101 115010000 120000000 0.0 0.096 0.096 0.000
 1202101 120010000 125000000 0.0317 0.2 0.2 0.100

1203101	120010000	155000000	0.0317	0.2	0.2	0.100
---------	-----------	-----------	--------	-----	-----	-------

 PUMP1 SUCTION TEE OUTLET

 1250000 PISTOL BRANCH
 1250001 2 1
 1250101 0.0 1.003 0.0613 0.0 90.0 0.521
 1250102 4.0E-5 0.0 DO
 1251101 125010000 130000000 0.0 0.1 0.1 0.100
 1252101 125000000 155000000 .028417 0.0 0.0 0.100

 PUMP 1 INLET

 1300000 P1INL SINGVOL
 1300101 0.0 0.457 0.0189 0.0 90.0 0.457
 1300102 4.0E-5 0.0 DO

 PRIMARY COOLANT PUMP 1 TRIP-611

 1350000 PCP1 PUMP
 1350101 0.0356 0.0 0.099 0.0 90.0 0.319
 1350102 0
 1350108 130010000 0.0 0.0 0.0 0.100
 1350109 140000000 0.0 0.05 0.05 0.100
 1350301 0 0 0 -1 -1 \$11 0
 1350302 369.0 0.911 0.3156 96.0 500.6 1.431
 1350303 613.6 0.0 207.4 0.004 19.598 0.0
 1350308 -212468 0.0 -25. 28.5 6.28
 1350310 0.0 0.0

 PUMP 1 OUTLET PUMP SIDE

 1400000 P1OTLPS SINGVOL
 1400101 0.0356 0.502 0.0 0.0 0.0 0.0
 1400102 4.0E-5 0.0 DO

 COOLANT PUMP INJ. (JOINED ONE PUMP)

 9010000 PCFINJ1 TMOPLUM
 9010101 910000000 140000000 0.0
 9010200 1 699
 9010201 -1 0.0 0.0 0.0
 9010202 0.0 .098 0.0 0.0
 9010203 10000. .098 0.0 0.0

 PCPWATER TMOPLVOL
 9100000
 9100101 7.E-3 1.0 0.0 0.0 0.0 0.0
 9100102 0.0 0.0 DO
 9100200 1
 9100201 0.0 305. 0.0
 9100202 10000. 305. 0.0

 PUMP1 OUTLET PIPE TEE SIDE

 1450000 POPTS BRANCH
 1450001 2 1
 1450101 0.0 1.4084 0.0633 0.0 0.0 0.0
 1450102 4.0E-5 0.0 DO
 1451101 140010000 145000000 0.0 0.0 0.0 0.100

```

1452101 145010000 150000000 .036873 0.0 0.0 0100
*****
* PUMP OUTLET TEE
*****
1500000 POTLTEE BRANCH
1500001 2 1
1500101 0.0634 0.4966 0.0 0.0 0.0 0.0
1500102 4.0E-5 0.0 00
1501101 170010000 150000000 .027528 0.2 0.2 0100
1502101 150010000 175000000 0.0 0.134 0.134 0100
*****
* PUMP 2 SUCTION TEE OUTLET
*****
1550000 P2STOL BRANCH
1550001 1 1
1550101 0.0 1.003 0.0813 0.0 90.0 0.521
1550102 4.0E-5 0.0 00
1551101 155010000 160000000 0.0 0.05 0.05 0100
*****
* PUMP 2 INLET PIPE
*****
1600000 P2INL SINGLVOL
1600101 0.0 0.457 0.0199 0.0 90.0 0.457
1600102 4.0E-5 0.0 00
*****
* PRIMARY COOLANT PUMP 2
*****
1650000 PCP2 PUMP
1650101 0.0368 0.0 0.099 0.0 90.0 0.319
1650102 0
1650108 160010000 0.0 0.0 0.0 0100
1650109 170000000 0.0 0.05 0.05 0100
1650301 135 135 135 -1 -1 511 0
1650302 369.0 0.316 0.3155 96.0 500.6 1.431
1650303 613.6 0.0 207.4 0.004 19.598 0.0
1650308 -212465 0.0 -25. 29.5 6.28 0.0
1650310 0.0 0.0 0.0
*****
* PUMP 2 OUTLET
*****
1700000 P2OUTL BRANCH
1700001 1 1
1700101 0.0366 0.514 0.0 0.0 0.0 0.0
1700102 4.0E-5 0.0 00
1701101 145010000 170010000 0.009073 0.2 0.2 0100
*****
* COLD LEG PIPE TO ECC CONNECTION TEE
*****
1750000 PTECT PIPE
1750001 2 2
1750101 0.0634 2
1750201 0.0 1
1750301 0.559 1
1750302 0.513 2
1750401 0.0 2
1750501 0.0 2
1750601 0.0 2
1750701 0.0 2
1750801 4.0E-5 0.0 2

```

```

1750901 0.15 0.15 1
1751001 00 2
1751101 0100 1
1751300 1
*****
* ECC CONNECTION TEE PUMP SIDE
*****
1800000 ECTPS BRANCH
1800001 1 1
1800101 0.0634 .701 0.0 0.0 0.0 0.0
1800102 4.0E-5 0.0 00
1801101 175010000 180000000 0.0 0.0664 0.0664 0100
*****
* COLD LEG PIPE FROM ECC CONNECTION TO REACTOR VESSEL
*****
1850000 CLPRVS BRANCH
1850001 2 1
1850101 0.0634 1.461 0.0 0.0 0.0 0.0
1850102 4.0E-5 0.0 00
1851101 185010000 290000000 0.0634 1. 1. 0101
1852101 180010000 185000000 0.0 0.0 0.0 0100
*****
* BREAK
*****
* DISCHARGE VOLUME
*****
8200000 BREAKVOL TMDPVOL
8200101 3.E-3 1. 0.0 0.0 0.0 0.0
8200102 0.0 0.0 0.0
8200200 2
8200201 0.0 1.E5 1.
8200202 10000. 1.E5 1.
*****
* BREAK OUTLET LINE
*****
8000000 BRKOUTL BRANCH
8000001 1 1
8000101 .000908 1.8 0.0 0.0 0.0 0.0
8000102 1.E-5 0.0 00
8001101 185010000 800000000 0.0 .5 .5 0102
*****
* BRAKE VALVE (ORIFICE)
*****
8050000 BRVVLV VALVE
8050101 800010000 820000000 205.6E-6 .4 .4 0100 .85 .85
8050300 MTRVLV
8050301 645 514 5. 0.0
*****
* REACTOR VESSEL
*****
* COLD LEG INLET ANNULUS

```

```

2900000 INANLVOL BRANCH
2900001 1 1
2900101 0.0 1 .30 .078 0.0 -90. -30
2900102 4.E-5 172 00
2901101 200010000 290000000 0.0 0.0 0.0 0100
*****
* INLET ANNULUS TOP VOLUME
*****
2000000 IANLTVOL BRANCH
2000001 0
2000101 0.0 0.18 0.0465 0.0 90.0 0.18
2000102 4.0E-5 0.178 00
*****
* INLET ANNULUS LOWER VOLUME
*****
2050000 IANLTVOL BRANCH
2050001 1 1
2050101 0.0 0.274 0.071 0.0 -90.0 -0.274
2050102 4.0E-5 0.172 00
2051101 205010000 210000000 0.0 0.0 0.0 0100
*****
* DOWNCOMER
*****
2100000 DNWCOMR PIPE
2100001 4
2100101 0.142 4
2100201 0.0 3
2100301 0.958 4
2100401 0.0 4
2100501 0.0 4
2100601 -90.0 4
2100801 4.0E-5 0.102 4
2100901 0.0 0.0 3
2101001 00 4
2101101 0000 3
2101300 1
*****
* LOWER PLENUM UPPER VOLUME
*****
2150000 LPUPVOL BRANCH
2150001 3 1
2150101 0.740 0.360 0.0 0.0 -90.0 -0.360
2150102 4.0E-5 0.0 00
2151101 210010000 215000000 0.0 0.0 0.0 0100
2152101 215010000 220000000 0.0 0.0 0.0 0100
2153101 215000000 225000000 0.16 0.0 0.0 0100
*****
* LOWER PLENUM LOWER VOLUME
*****
2200000 LPLOVOL SINGLVOL
2200101 0.790 0.370 0.0 0.0 -90.0 -0.370
2200102 4.0E-5 0.0 00
*****
* LOWER CORE SUPPORT STRUCTURE
*****
2250000 LCOSUST BRANCH
2250001 1 1
2250101 0.25 0.52 0.0 0.0 90.0 0.52
2250102 4.0E-5 0.095 00

```

2251101 22501000 23000000 0.0975 2.4 2.4 0100

* VALVE JUNCTION FOR CORE BYPASS FLOW

*
2260000 CBPVLV VALVE
2260101 22501000 235000000 .015 1. 1. 0100
2260201 1 20. 0.0 0.0
2260300 SRVLV
2260301 226

* ACTIVE CORE

*
2300000 CORE PIPE
2300001 6
2300101 0.1705 6
2300201 0.1705 1
2300202 0.1440 2
2300203 0.1705 3
2300204 0.1440 4
2300205 0.1705 5
2300301 0.2795 6
2300302 0.3776 6
2300401 0.0 6
2300501 0.0 6
2300601 90.0 6
2300801 4.0E-5 0.012 6
2300901 0.0 0.0 1
2300902 .5 .5 2
2300903 0.0 0.0 3
2300904 .5 .5 4
2300905 0.0 0.0 5
2301001 00 6
2301101 0100 6
2301300 1

* BYPASS VOLUME

*
2350000 BYPVOL PIPE
2350001 3
2350101 0.015 3
2350201 0.0 2
2350301 0.559 2
2350302 0.657 3
2350401 0.0 3
2350501 0.0 3
2350601 90.0 3
2350801 4.0E-5 0.003 3
2350901 0.0 0.0 2
2351001 00 3
2351101 0000 2
2351300 1

* UPPER CORE SUPPORT STRUCTURE

*
2400000 UCOSST BRANCH
2400001 2 1
2400101 0.297 1.118 0.0 0.0 90.0 1.118
2400102 4.0E-5 0.145 00
2401101 23001000 240000000 0.12 2.40 2.40 0100
2402101 23501000 240000000 0.0 1.50 1.50 0100

* UPPER FLOW SKIRT REGION

*
2450000 UFOSRE BRANCH
2450001 1 1
2450101 0.114 0.693 0.0 0.0 90.0 0.693
2450102 4.0E-5 0.131 00
2461101 240010000 246000000 0.0 0.0 0.0 0100

* DEAD END OF FUEL MODULES

*
2460000 FUMODL BRANCH
2460001 1 1
2460101 0.183 0.700 0.0 0.0 90.0 0.700
2460102 4.0E-5 0.214 00
2461101 240010000 246000000 0.0 0.0 0.0 0100

* REACTOR VESSEL HOT LEG OUTLET

*
2950000 RWALOUT BRANCH
2950001 1 1
2950101 .201 .30 0.0 0.0 90. .30
2950102 4.E-5 0.0 00
2951101 245010000 295000000 0.0 0.0 0.0 0100

* VALVE JUNCTION INLET ANN. TO UPPER PLENUM

*
2960000 IAUPVLV VALVE
2960101 200010000 250000000 .01 1. 1. 0100
2960201 1 15.9 0.0 0.0
2960300 SRVLV
2960301 296

* VALVE JUNCTION INLET ANN. TO UPPER PLENUM

*
2970000 IAUPVL1 VALVE
2970101 205000000 245010000 .01 1. 1. 0100
2970201 1 15.9 0.0 0.0
2970300 SRVLV
2970301 296

* VALVE JUNCTION INLET ANN. TO DOWNCOMER

*
2910000 IADOWN VALVE
2910101 290010000 205000000 0.259 1. 1. 0100
2910201 1 444.9 0.0 0.0
2910300 SRVLV
2910301 291

* UPPER PLENUM LOWER VOLUME

*
2500000 UPLLVOL BRANCH
2500001 2 1
2500101 0.288 0.704 0.0 0.0 90.0 0.704
2500102 4.0E-5 0.0 00
2501101 295010000 250000000 0.0 0.0 0.0 0100
2502101 250010000 255000000 0.0 0.0 0.0 0100

* UPPER PLENUM UPPER VOLUME

*
2650000 UPLVOL SINGL VOL
2650101 0.244 0.712 0.0 0.0 90.0 0.712
2650102 4.0E-5 0.0 00

* PRESSURIZER

* SURGE LINE PCS SIDE

*
4000000 SLPCS BRANCH
4000001 2 1
4000101 0.00145 3.45 0.0 0.0 90.0 0.54
4000102 4.0E-5 0.0 00
4001101 110000000 400000000 0.0 0.93 0.93 0100
4002101 400010000 405000000 0.0 0.93 0.93 0000

* SURGE LINE PRESSURIZER VESSEL

*
4050000 SLPRV SINGL VOL
4050101 0.00145 3.45 0.0 0.0 90.0 0.60
4050102 4.0E-5 0.0 00

* PRESSURIZER SURGE LINE VALVE

*
4100000 SLVALV VALVE
4100101 405010000 415000000 0.0 0.93 0.93 0100
4100300 TRPVLV
4100301 601

* PRESSURIZER VESSEL

*
4150000 PRESSV PIPE
4150001 8
4150101 0.362 1
4150102 0.565 6
4150103 0.466 7
4150104 0.13 8
4150201 0.0 7
4150301 0.224 7
4150302 0.403 6
4150303 0.207 6
4150304 0.1705 7
4150305 0.118 8
4150401 0.0 8
4150501 0.0 8
4150601 90.0 8
4150801 4.0E-5 0.0 8
4151001 00 8
4151002 01 8
4151101 0100 1
4151102 0000 7
4151300 1

* TOP VOLUME PRESSURIZER

```

4200000 TOPPRE BRANCH
4200001 1 0
4200101 0.13 0.236 0.0 0.0 90.0 0.236
4200102 4.5E-5 0.0 01
4201101 415010000 420000000 0.0 0.0 0.0 0000
    
```

HEAT STRUCTURE INPUT DATA

REACTOR VESSEL HEAT STRUCTURES

FILLER BLOCKS INLET ANNULUS TOP VOLUME

```

12000000 1 5 2 1 0.508
1200100 0 1
1200101 4 0.773
1200201 4 4
1200301 0.0 4
1200401 565.2 5
1200501 200010000 0 1 1 0.33 1
1200501 0 0 1 0.33 1
1200701 0 0.0 0.0 0.0 1
1200801 0 .178 0.0 0.33 1
    
```

FILLER BLOCKS INLET ANNULUS LOWER VOLUME

```

12050000 1 5 2 1 0.501
12050100 0 1
12050101 4 0.766
12050201 4 4
12050301 0.0 4
12050401 565.2 5
12050501 205010000 0 1 1 0.424 1
12050601 0 0 0 1 0.424 1
12050701 0 0.0 0.0 0.0 1
12050801 0 .172 0.0 0.424 1
    
```

FILLER BLOCKS DOWNCOMER AND LOWER PLENUM

```

12100000 5 5 2 1 0.47
12100100 0 1
12100101 4 0.736
12100201 4 4
12100301 0.0 4
12100401 565.2 5
12100501 210010000 0 1 1 0.958 1
12100503 210030000 0 1 1 0.958 3
12100504 210040000 0 1 1 0.958 4
12100505 215010000 0 1 1 0.36 5
12100506 220010000 0 1 1 0.37 6
12100601 0 0 0 1 0.958 4
12100602 0 0 0 1 0.36 5
12100603 0 0 0 1 0.37 5
12100701 0 0.0 0.0 0.0 6
12100801 0 0.102 0.0 0.958 4
12100802 0 0.971 0.0 0.36 5
12100803 0 1.003 0.0 0.37 6
    
```

CORE SUPPORT BARREL

```

12010000 8 5 2 1 0.3810
12010100 0 1
12010101 4 0.4191
12010201 4 4
12010301 0.0 4
12010401 565.2 5
12010501 200010000 0 1 1 0.33 1
12010502 205010000 0 1 1 0.424 2
12010503 210010000 0 1 1 0.958 2
12010504 210020000 0 1 1 0.958 4
12010505 210030000 0 1 1 0.958 8
12010506 210040000 0 1 1 0.958 6
12010601 0 0 0 1 0.33 1
12010602 0 0 0 1 0.424 2
12010603 0 0 0 1 0.958 2
12010604 0 0 0 1 0.958 4
12010605 0 0 0 1 0.958 8
12010606 0 0 0 1 0.958 6
12010701 0 0.0 0.0 0.0 6
12010801 0 0.178 0.0 0.33 1
12010802 0 0.172 0.0 0.424 2
12010803 0 0.102 0.0 0.958 6
    
```

FLOW SKIRT - CORE FILLER ASSEMBLY

```

12250000 10 5 2 1 0.3
12250100 0 1
12250101 4 0.38
12250201 4 4
12250301 0.0 4
12250401 565.2 5
12250501 225010000 0 1 1 0.52 1
12250502 230010000 10000 1 1 0.2795 5
12250503 230060000 0 1 1 0.3775 7
12250504 240010000 0 1 1 1.118 8
12250505 245010000 0 1 1 0.42 9
12250506 246010000 0 1 1 0.35 10
12250601 0 0 0 1 0.52 1
12250602 0 0 0 1 0.2795 6
12250603 0 0 0 1 0.3775 7
12250604 0 0 0 1 1.118 8
12250605 0 0 0 1 0.42 9
12250606 0 0 0 1 0.35 10
12250701 0 0.0 0.0 0.0 10
12250801 0 0.0 0.0 0.52 1
12250802 0 0.012 0.0 0.2795 6
12250803 0 0.012 0.0 0.3775 7
12250804 0 0.145 0.0 1.118 8
12250805 0 0.131 0.0 0.42 9
12250806 0 0.214 0.0 0.35 10
    
```

ACTIVE CORE

```

12300000 6 9 2 1 0.0
12300100 0 1
12300101 8 4.647E-3
12300102 1 4.747E-3
12300103 2 5.359E-3
12300201 1 5
12300202 -2 6
12300203 -3 8
    
```

```

12300301 1.0 5
12300302 0.0 8
12300401 1100. 6
12300402 560. 8
12300501 0 0
12300502 0 0
12300601 230010000 10000 1 1 1 490.75
12300602 230060000 0 1 1 1 490.75
12300701 1000 0.061 0.0 0.0 1
12300702 1000 0.282 0.0 0.0 2
12300703 1000 0.245 0.0 0.0 3
12300704 1000 0.228 0.0 0.0 4
12300705 1000 0.146 0.0 0.0 5
12300706 1000 0.038 0.0 0.0 6
12300901 0 0.01250 0.0 0.2795 6
12300902 0 0.01250 0.0 0.3775 6
    
```

FUEL MODULES

```

12460000 1 5 1 1 0.0
12460100 0 1
12460101 4 0.01
12460201 4 4
12460301 0.0 4
12460401 565.2 5
12460501 245010000 0 1 1 1.8 1
12460601 246010000 0 1 1 1.8 1
12460701 0 0.0 0.0 1.8 1
12460801 0 0.42 0.0 1.8 1
12460901 0 0.214 0.0 1.8 1
    
```

REACTOR VESSEL BOTTOM

```

12200000 1 5 1 1 0.0
12200100 0 1
12200101 4 0.092
12200201 4 4
12200301 0.0 4
12200401 565.2 5
12200501 -999 0 3949 0 1.68 1
12200601 220010000 0 1 1 1.68 1
12200701 0 0.0 0.0 0.0 1
12200901 0 0.0 0.0 0.52 1
    
```

LOWER CORE SUPPORT STRUCTURE

```

12260000 1 5 2 1 0.282
12260100 0 1
12260101 4 0.3
12260201 4 4
12260301 0.0 4
12260401 565.2 5
12260501 225010000 0 1 1 0.52 1
12260601 0 0 0 1 0.52 1
12260701 0 0.0 0.0 0.0 1
12260801 0 0.0 0.0 0.52 1
    
```

UPPER CORE SUPPORT STRUCTURE

```

12400000 1 5 2 1 0.282
12400100 0 1
    
```

12400101	4	0.31				
12400201	4	4				
12400301	0.0	4				
12400401	565.2	5				
12400501	240010000	0	1	1	.559	1
12400601	0	0	0	1	.559	
12400701	0	0.0	0.0	0.0		1
12400801	0	0.145	0.0	.559	1	

* UPPER HEAD TOP PLATE

12550000	1	5	1	1	0.0	
12550100	0	1				
12550101	4	0.474				
12550201	4	4				
12550301	0.0	4				
12550401	565.2	5				
12550501	255010000	0	1	1	0.712	1
12550601	-999	0	3949	1	0.712	1
12550701	0	0.0	0.0	0.0		
12550801	0	0.0	0.0	0.712	1	

* CORE SUPPORT BARREL UPPER PLENUM LOWER VOLUME

12500000	1	5	2	1	0.381	
12500100	0	1				
12500101	4	0.418				
12500201	4	4				
12500301	0.0	4				
12500401	565.2	5				
12500501	250010000	0	1	1	0.854	1
12500601	0	0	1	1	0.854	1
12500701	0	0.0	0.0	0.0		
12500801	0	0.0	0.0	0.854	1	

* CORE SUPPORT BARREL UPPER PLENUM TOP VOLUME

12520000	1	5	2	1	0.381	
12520100	0	1				
12520101	4	0.728				
12520201	4	4				
12520301	0.0	4				
12520401	565.2	5				
12520501	255010000	0	1	1	0.712	1
12520601	-999	0	3949	1	0.712	1
12520701	0	0.0	0.0	0.0		
12520801	0	0.0	0.0	0.712	1	

* INTERNALS UPPER PLENUM

12510000	2	5	1	1	0.0	
12510100	0	1				
12510101	4	0.005				
12510201	4	4				
12510301	0.0	4				
12510401	565.2	5				
12510501	250010000	0	1	1	1.0	1
12510502	255010000	0	1	1	1.0	2
12510601	0	0	1	1	1.0	1
12510602	0	0	1	1	1.0	2
12510701	0	0.0	0.0	0.0	2	

12610801	0	0.0	0.0	1.0	1	
12610802	0	0.0	0.0	1.0	2	

* PRIMARY SYSTEM PIPING

* BROKEN HOT LEG

13150000	2	5	2	1	.0515	
13150100	0	1				
13150101	5	.0705				
13150201	4	5				
13150301	0.0	5				
13150401	540.	5				
13150501	315010000	0	1	1	.4054	1
13150502	315020000	0	1	1	.5265	2
13150601	-997	0	3949	1	.4054	1
13150602	-997	0	3949	1	.5265	2
13150701	0	0	0	0		
13150801	0	0	0	0	.4054	1
13150802	0	0	0	0	.5265	2

13151000	1	5	2	1	.1074	
13151100	0	1				
13151101	5	.1350				
13151201	4	5				
13151301	0.0	5				
13151401	540.	5				
13151501	315060000	0	1	1	2.671	1
13151601	-997	0	3949	1	2.671	1
13151701	0	0	0	0		
13151801	0	0	0	0	2.671	1

13152000	1	5	2	1	.0660	
13152100	0	1				
13152101	5	.0840				
13152201	4	5				
13152301	0.0	5				
13152401	540.	5				
13152501	315090000	0	1	1	1.842	1
13152601	-997	0	3949	1	1.842	1
13152701	0	0	0	0		
13152801	0	0	0	0	1.842	1

13153000	5	5	2	1	.1835	
13153100	0	1				
13153101	5	.2285				
13153201	4	5				
13153301	0.0	5				
13153401	540.	5				
13153501	315030000	10000	1	1	1.699	4
13153502	315070000	0	1	1	.362.	5
13153601	-997	0	3949	1	1.699	4
13153602	-997	0	3949	1	.362	5
13153701	0	0	0	0		
13153801	0	0	0	0	1.699	4
13153802	0	0	0	0	.362	5

13154000	1	5	2	1	.1285	
13154100	0	1				
13154101	5	.1620				

13154201	4	5				
13154301	0.0	5				
13154401	540.	5				
13154501	315100000	0	1	1	.667	1
13154601	-997	0	3949	1	.667	1
13154701	0	0	0	0		
13154801	0	0	0	0	.667	1

13000000	3	5	2	1	.1420	
13000100	0	1				
13000101	5	.1780				
13000201	4	5				
13000301	0.0	5				
13000401	540.	5				
13000501	300010000	0	1	1	.8750	1
13000502	305010000	0	1	1	.6980	2
13000503	310010000	0	1	1	1.424	3
13000601	-999	0	3949	1	.8760	1
13000602	-999	0	3949	1	.6980	2
13000603	-999	0	3949	1	1.424	3
13000701	0	0	0	0		
13000801	0	0	0	0	.8750	1
13000802	0	0	0	0	.6980	2
13000803	0	0	0	0	1.424	3

* REFLOD ASSIST BYPASS

13750000	2	5	2	1	.111	
13750100	0	1				
13750101	5	.1365				
13750201	4	5				
13750301	0.0	5				
13750401	540.	5				
13750501	370010000	0	1	1	4.415	1
13750502	380010000	0	1	1	5.240	2
13750601	-999	0	3949	1	4.415	1
13750602	-999	0	3949	1	5.240	2
13750701	0	0	0	0		
13750801	0	0	0	0	4.415	1
13750802	0	0	0	0	5.240	2

* B.L. COLD LEG

13350000	3	5	2	1	.1420	
13350100	0	1				
13350101	5	.1780				
13350201	4	5				
13350301	0.0	5				
13350401	540.	5				
13350501	315010000	0	1	1	.7495	1
13350502	340010000	0	1	1	.6980	1
13350503	345010000	0	1	1	.9740	3
13350601	-999	0	3949	1	.7495	1
13350602	-999	0	3949	1	.6980	1
13350603	-999	0	3949	1	.9740	3
13350701	0	0	0	0		
13350801	0	0	0	0	.7495	1
13350802	0	0	0	0	.6980	1
13350803	0	0	0	0	.9740	3

13501000	1	5	2	1	.0803	
13501100	0	1				
13501101	5	.1287				

13501201	4	5							
13501301	0.0	5							
13501401	540.	6							
13501501	35001000	0	1	1	2.0965	1			
13501601	-997	0	3949	1	2.0965	1			
13501701	0	0	0	0	0	0			
13501801	0	0	0	2.0965	1				

* INTACT LOOP PIPING

11001000	12	8	2	1	.142				
11001100	0	1							
11001101	5		178						
11001201	4	5							
11001301	0.0	5							
11001401	540.	6							
11001501	100010000	0	1	1	1.5373	1			
11001502	105010000	0	1	1	1.6340	2			
11001503	110010000	0	1	1	1.1303	3			
11001504	115010000	0	1	1	.93124	4			
11001505	115120000	0	1	1	.6890	5			
11001506	115130000	0	1	1	.5590	6			
11001507	120010000	0	1	1	.7600	7			
11001508	150010000	0	1	1	.4966	8			
11001509	175010000	0	1	1	.5590	9			
11001510	175020000	0	1	1	.6130	10			
11001511	180010000	0	1	1	.7010	11			
11001512	185010000	0	1	1	1.4810	12			
11001601	-999	0	3949	1	1.5373	1			
11001602	-999	0	3949	1	1.6340	2			
11001603	-999	0	3949	1	1.1303	3			
11001604	-999	0	3949	1	.93124	4			
11001605	-999	0	3949	1	.6890	5			
11001606	-999	0	3949	1	.5590	6			
11001607	-999	0	3949	1	.7600	7			
11001608	-999	0	3949	1	.4966	8			
11001609	-999	0	3949	1	.5590	9			
11001610	-999	0	3949	1	.6130	10			
11001611	-999	0	3949	1	.7010	11			
11001612	-999	0	3949	1	1.4810	12			
11001701	0	0	0	0	1.5373	12			
11001801	0	0	0	0	1.6340	2			
11001802	0	0	0	0	1.1303	3			
11001803	0	0	0	0	.93124	4			
11001804	0	0	0	0	.6890	5			
11001805	0	0	0	0	.5590	6			
11001806	0	0	0	0	.7600	7			
11001807	0	0	0	0	.4966	8			
11001808	0	0	0	0	.5590	9			
11001810	0	0	0	0	.6130	10			
11001811	0	0	0	0	.7010	11			
11001812	0	0	0	0	1.4810	12			
11002000	2	6	2	1	.1625				
11002100	0	1							
11002101	5		.2030						
11002201	4	5							
11002301	0.0	5							
11002401	540.	6							
11002501	115020000	0	1	1	.708	1			
11002502	115110000	0	1	1	.547	2			
11002601	-999	0	3949	1	.708	1			
11002502	-999	0	3949	1	.547	2			

11002701	0	0	0	0	0	2			
11002801	0	0	0	0	.708	1			
11002802	0	0	0	0	.547	2			
11003000	7	6	2	1	.106				
11003100	0	1							
11003101	5	.1365							
11003201	4	5							
11003301	0.0	5							
11003401	540.	6							
11003501	125010000	0	1	1	1.003	1			
11003502	130010000	0	1	1	.457	2			
11003503	140010000	0	1	1	.502	3			
11003504	145010000	0	1	1	1.4084	4			
11003505	155010000	0	1	1	1.003	5			
11003506	160010000	0	1	1	.457	6			
11003507	170010000	0	1	1	.514	7			
11003601	-999	0	3949	1	1.003	1			
11003602	-999	0	3949	1	.457	2			
11003603	-999	0	3949	1	.502	3			
11003604	-999	0	3949	1	1.4084	4			
11003605	-999	0	3949	1	1.003	5			
11003606	-999	0	3949	1	.457	6			
11003607	-999	0	3949	1	.514	7			
11003701	0	0	0	0	0	0			
11003801	0	0	0	0	1.003	1			
11003802	0	0	0	0	.457	2			
11003803	0	0	0	0	.502	3			
11003804	0	0	0	0	1.4084	4			
11003805	0	0	0	0	1.003	5			
11003806	0	0	0	0	.457	6			
11003807	0	0	0	0	.514	7			
11004000	2	6	3	1	.6858				
11004100	0	1							
11004101	5	.7747							
11004201	4	5							
11004301	0.0	5							
11004401	540.	6							
11004501	118030000	0	1	1	.25	1			
11004502	115100000	0	1	1	.25	2			
11004601	-999	0	3949	1	.25	1			
11004602	-999	0	3949	1	.25	2			
11004701	0	0	0	0	0	2			
11004801	0	0	0	0	.630	1			
11004802	0	0	0	0	.630	2			
11004901	0	0	0	0	.630	2			

* PRESSURIZER HEAT STRUCTURES

14151000	1	6	1	1	0.0				
14151100	0	1							
14151101	5	.0762							
14151201	5	5							
14151301	0.0	5							
14151401	518.	6							
14151501	415010000	0	1	1	.362	1			
14151601	-998	0	3949	1	.362	1			
14151701	0	0	0	0	0	0			
14151801	0	0.0	0.0	0.0	1				
14152000	7	6	2	1	.42291				
14152100	0	1							
14152101	5	.49911							
14152201	5	5							

14152301	0.0	5							
14152401	618.	6							
14152501	415010000	0	1	1	.224	1			
14152502	415020000	10000	1	1	.403	1			
14152503	415040000	10000	1	1	.207	1			
14152504	415060000	10000	1	1	.1705	7			
14152601	-998	0	3949	1	.224	1			
14152602	-998	0	3949	1	.403	1			
14152603	-998	0	3949	1	.207	1			
14152604	-998	0	3949	1	.1705	7			
14152701	0	0	0	0	0	0			
14152801	0	0.0	0.0	0.0	7				
14162000	1	6	2	1	.2032				
14162100	0	1							
14162101	5	.3683							
14162201	5	5							
14152301	0.0	5							
14162401	518.	6							
14162501	415080000	0	1	1	.118	1			
14162601	-998	0	3949	1	.118	1			
14162701	0	0	0	0	1				
14162801	0	0.0	0.0	0.0	1				
14202000	1	6	2	1	.2032				
14202100	0	1							
14202101	5	.3683							
14202201	5	5							
14202301	0.0	5							
14202401	518.	6							
14202501	420010000	0	1	1	.118	1			
14202601	-998	0	3949	1	.118	1			
14202701	0	0	0	0	1				
14202801	0	0.0	0.0	0.0	1				
14201000	1	1	1	1	0.0				
14201100	0	1							
14201101	5	.18415							
14201201	5	5							
14201301	0.0	5							
14201401	518.	6							
14201501	420010000	0	1	1	.130	1			
14201601	-998	0	3949	1	.130	1			
14201701	0	0	0	0	1				
14201801	0	0.0	0.0	0.0	1				

* STEAM GENERATOR PRI-SEC HEAT STRUCTURES

* STEAM GENERATOR TUBING (INCL. HALF THE TUBE SHEET)

10060000	5	8	2	1	0.0051054				
10060100	0	1							
10060101	7	0.006348984							
10060201	6	7							
10060301	0.0	7							
10060401	540.0	8							
10060501	517010000	0	1	1	1579.69	1			
10060602	517020000	0	1	1	1310.32	2			
10060603	517030000	0	1	1	1582.27	3			
10060604	517030000	0	1	1	1582.27	4			
10060605	517070000	0	1	1	1310.32	2			

10060503	115060000	0	1	1	1582.27	3
10060504	115070000	0	1	1	1582.27	4
10060505	115080000	0	1	1	1315.32	5
10060506	115090000	0	1	1	1578.69	6
10060701	0	0	0	0	0	6
10060801	0	0	0	0	0	6
10060901	0	0	0	0	0	6

HEAT STRUCTURE THERMAL PROPERTY DATA

20100100	TBL/FCTN	1	1	UO2
20100200	TBL/FCTN	1	1	GAP
20100300	TBL/FCTN	1	1	ZR
20100400	S-STEEL			
20100500	C-STEEL			
20100600	TBL/FCTN	1	1	INCONEL 600

THERMAL CONDUCTIVITY UO2

20100101	366.48	7.7796	449.81	6.6287	533.15	5.7824
20100102	616.48	4.6228	699.82	4.6332	783.15	422.13
20100103	866.48	3.8803	949.82	3.5965	1033.15	9.3576
20100104	1088.71	3.1551	1199.82	2.9838	1283.15	2.8367
20100105	1366.48	2.7138	1449.82	2.6082	1533.32	2.5217
20100106	1616.48	2.4490	1699.82	2.3919	1977.59	2.2898
20100107	2255.37	2.3071	2533.15	2.4334	2810.93	2.6619
20100108	3088.71	2.9942				

VOLVETRIC HEAT CAPACITY UO2

20100151	273.15	2.3104E6	323.15	2.5720E6	373.15	2.7464E6
20100152	473.15	2.9207E6	673.15	3.1387E6	873.15	3.4438E6
20100153	1773.15	3.5310E6	1973.15	3.7926E6	2173.15	4.2285E6
20100154	2373.15	4.8824E6	2673.15	6.0158E6	2773.15	6.3210E6
20100155	2873.15	6.5825E6	2973.15	6.7133E6	3113.15	6.8005E6
20100156	4699.82	6.8005E6				

THERMAL CONDUCTIVITY ZR

20100301	273.15	9.5744	473.15	12.0044	673.15	14.0051
20100302	873.15	17.0079	1073.15	19.0087	1273.15	22.0098
20100303	1473.15	25.0109	1673.15	30.0127	1873.15	35.0149
20100304	2073.15	44.0178	2273.15	55.0235	2473.15	68.0283

VOLVETRIC HEAT CAPACITY ZR

20100351	255.37	1.9041E6	1077.59	2.3122E6	1185.93	5.7124E6
20100352	1248.43	2.3118E6	2199.82	2.3122E6		

THERMAL CONDUCTIVITY GAP

20100201	273.15	0.14
20100202	590.0	0.24
20100203	810.0	0.29
20100204	1090.0	0.36
20100205	1370.0	0.42
20100206	3260.0	0.75

THERMAL CONDUCTIVITY INCONEL 600

20100601	366.5	13.85
20100602	477.6	15.92
20100603	588.7	18.17
20100604	700.0	20.42
20100605	810.9	22.50
20100606	922.0	24.92
20100607	1033.2	26.83
20100608	1144.3	29.42
20100609	1477.6	36.06

VOLVETRIC HEAT CAPACITY GAP

20100251	273.15	5.4
20100252	3260.0	5.4

VOLVETRIC HEAT CAPACITY INCONEL 600

20100651	366.5	3.908E5
20100652	477.6	4.084E5
20100653	588.7	4.260E5
20100654	700.0	4.436E5
20100655	810.9	4.655E5
20100657	922.0	4.929E5
20100658	1033.2	5.105E5
20100659	1477.6	5.727E5

HEAT STRUCTURE GENERAL TABLES.

20299900	TEMP	
20299901	0.0	305.
20299800	TEMP	501
20299801	-1.	514.7
20299802	0.0	305.
20299700	TEMP	501
20299701	-1.	558.
20299702	0.0	305.
20294900	HTC-T	
20294901	0.0	20. # 250 KW SS SURROUNDINGS HEAT LOSS
20290000	POWER	
20290001	0.0	0.0
20290002	1000.0	0.0

PUMP DATA

SINGLE PHASE HEAD CURVES

HEAD CURVE NO. 1

1351100	1	1
1351101	0.000000E+00	1.403600E+00
1351102	1.906100E-01	1.363600E+00
1351103	3.896300E-01	1.314600E+00
1351104	5.939600E-01	1.278000E+00
1351105	7.902000E-01	1.133600E+00
1351106	1.000000E+00	1.000000E+00

HEAD CURVE NO. 2

1351200	1	2
1351201	0.000000E+00	-6.700000E-01
1351202	2.000000E-01	-5.000000E-01
1351203	4.000000E-01	-2.500000E-01
1351204	5.765400E-01	0.000000E+00
1351205	7.443200E-01	2.583000E-01
1351206	7.734800E-01	3.778000E-01
1351207	8.831300E-01	6.326000E-01
1351208	1.000000E+00	1.000000E+00

HEAD CURVE NO. 3

1351300	1	3
1351301	-1.000000E+00	2.472200E+00
1351302	-8.057400E-01	2.047400E+00
1351303	-6.069000E-01	1.831000E+00
1351304	-4.068300E-01	1.624000E+00
1351305	-2.001710E-01	1.470500E+00
1351306	0.000000E+00	1.403600E+00

HEAD CURVE NO. 4

1351400	1	4
1351401	0.000000E+00	2.472200E+00
1351402	-8.229700E-01	1.996800E+00
1351403	-6.333200E-01	1.589700E+00
1351404	-4.553400E-01	1.327900E+00
1351405	-2.710900E-01	1.154900E+00
1351406	-1.771800E-01	1.060500E+00
1351407	-9.073000E-02	1.015600E+00
1351408	0.000000E+00	9.342790E-01

HEAD CURVE NO. 5

1351500	1	5
1351501	0.000000E+00	2.500000E-01
1351502	2.000000E-01	2.800000E-01
1351503	4.000000E-01	3.400000E-01
1351504	4.118000E-01	2.768000E-01
1351505	5.976300E-01	4.584000E-01
1351506	7.834670E-01	6.982000E-01
1351507	1.000000E+00	1.000000E+00

HEAD CURVE NO. 6

1351600	1	6
1351601	0.000000E+00	9.342790E-01
1351602	9.109900E-02	9.229000E-01
1351603	1.865090E-01	8.968000E-01
1351604	2.717620E-01	8.750000E-01
1351605	4.558720E-01	8.433000E-01
1351606	5.744060E-01	8.355000E-01

1351607 7.405760E-01 8.466000E-01
 1351608 7.666190E-01 8.463000E-01
 1351609 8.714710E-01 8.838000E-01
 1351610 1.000000E+00 1.000000E+00

* HEAD CURVE NO. 7

1351700 1 7
 1351701 -1.000000E+00 -1.000000E+00
 1351702 -8.000000E-01 -6.300000E-01
 1351703 -6.000000E-01 -3.000000E-01
 1351704 -4.000000E-01 -5.000000E-02
 1351705 -2.000000E-01 1.500000E-01
 1351706 0.000000E+00 2.500000E-01

* HEAD CURVE NO. 8

1351800 1 8
 1351801 -1.000000E+00 -1.000000E+00
 1351802 -8.000000E-01 -9.700000E-01
 1351803 -6.000000E-01 -9.500000E-01
 1351804 -4.000000E-01 -8.800000E-01
 1351805 -2.000000E-01 -8.000000E-01
 1351806 0.000000E+00 -6.700000E-01

* SINGLE PHASE TORQUE DATA

* TORQUE CURVE NO. 1

1351900 2 1
 1351901 0.000000E+00 6.032000E-01
 1351902 1.930000E-01 6.325000E-01
 1351903 3.930000E-01 7.369000E-01
 1351904 5.955200E-01 8.331000E-01
 1351905 7.978200E-01 9.228000E-01
 1351906 1.000000E+00 1.000000E+00

* TORQUE CURVE NO. 2

1352000 2 2
 1352001 0.000000E+00 -6.700000E-01
 1352002 4.000000E-01 -2.500000E-01
 1352003 5.000000E-01 1.500000E-01
 1352004 7.372500E-01 5.265860E-01
 1352005 7.680490E-01 6.065940E-01
 1352006 8.672300E-01 7.436600E-01
 1352007 1.000000E+00 1.000000E+00

* TORQUE CURVE NO. 3

1352100 2 3
 1352101 -1.000000E+00 1.984300E+00
 1352102 -8.009600E-01 1.394000E+00
 1352103 -6.063800E-01 1.097500E+00
 1352104 -4.068600E-01 8.220000E-01
 1352105 -1.992800E-01 6.648000E-01
 1352106 0.000000E+00 6.032000E-01

* TORQUE CURVE NO. 4

1352200 2 4
 1352201 -1.000000E+00 1.984300E+00
 1352202 -8.223400E-01 1.830800E+00

1352203 -6.337100E-01 1.682400E+00
 1352204 -4.585300E-01 1.557000E+00
 1352205 -2.670230E-01 1.436200E+00
 1352206 -1.761070E-01 1.387900E+00
 1352207 -8.931000E-02 1.348100E+00
 1352208 0.000000E+00 1.233610E+00

* TORQUE CURVE NO. 5

1352300 2 5
 1352301 0.000000E+00 -4.500000E-01
 1352302 4.000000E-01 -2.500000E-01
 1352303 5.000000E-01 0.000000E+00
 1352304 1.000000E+00 3.569000E-01

* TORQUE CURVE NO. 6

1352400 2 6
 1352401 0.000000E+00 1.233610E+00
 1352402 9.064300E-02 1.196500E+00
 1352403 1.885690E-01 1.109600E+00
 1352404 2.734700E-01 1.041600E+00
 1352405 4.586690E-01 8.958000E-01
 1352406 5.744800E-01 7.807000E-01
 1352407 7.381600E-01 6.134000E-01
 1352408 7.685200E-01 5.849000E-01
 1352409 8.700570E-01 4.877000E-01
 1352410 1.000000E+00 3.569000E-01

* TORQUE CURVE NO. 7

1352500 2 7
 1352501 -1.000000E+00 -1.000000E+00
 1352502 -3.000000E-01 -9.000000E-01
 1352503 -1.000000E-01 -8.000000E-01
 1352504 0.000000E+00 -4.500000E-01

* FOR TORQUE CURVE NO. 8

1352600 2 8
 1352601 -1.000000E+00 -1.000000E+00
 1352602 -2.500000E-01 -9.000000E-01
 1352603 -8.000000E-02 -8.000000E-01
 1352604 0.000000E+00 -6.700000E-01

* TWO - PHASE MULTIPLIER DATA

* HEAD CURVE

1353000 0
 1353001 0.000000E+00 0.000000E+00
 1353002 2.000000E-02 2.000000E-02
 1353003 6.000000E-02 5.000000E-02
 1353004 1.000000E-01 1.000000E-01
 1353005 2.000000E-01 4.600000E-01
 1353006 2.400000E-01 8.000000E-01
 1353007 3.000000E-01 9.600000E-01
 1353008 4.000000E-01 9.800000E-01
 1353009 6.000000E-01 9.700000E-01
 1353010 8.000000E-01 9.000000E-01
 1353011 9.000000E-01 8.000000E-01
 1353012 9.600000E-01 5.000000E-01
 1353013 1.000000E+00 0.000000E+00

* TORQUE CURVE

1353100 0
 1353101 0.000000E+00 0.000000E+00
 1353102 1.250000E-01 7.000000E-02
 1353103 1.650000E-01 1.250000E-01
 1353104 2.400000E-01 5.600000E-01
 1353105 8.000000E-01 5.600000E-01
 1353106 9.600000E-01 4.500000E-01
 1353107 1.000000E+00 0.000000E+00

* PUMP 2-PHASE DIFFERENCE DATA

* HEAD CURVE NO. 1

1354100 1 1
 1354101 0.000000E+00 0.000000E+00
 1354102 1.000000E-01 6.300000E-01
 1354103 2.000000E-01 1.090000E+00
 1354104 5.000000E-01 1.020000E+00
 1354105 7.000000E-01 1.010000E+00
 1354106 9.000000E-01 9.400000E-01
 1354107 1.000000E+00 1.000000E+00

* HEAD CURVE NO. 2

1354200 1 2
 1354201 0.000000E+00 0.000000E+00
 1354202 1.000000E-01 -4.000000E-02
 1354203 2.000000E-01 0.000000E+00
 1354204 3.000000E-01 1.000000E-01
 1354205 4.000000E-01 2.100000E-01
 1354206 8.000000E-01 6.700000E-01
 1354207 9.000000E-01 8.000000E-01
 1354208 1.000000E+00 1.000000E+00

* HEAD CURVE NO. 3

1354300 1 3
 1354301 -1.000000E+00 -1.160000E+00
 1354302 -9.000000E-01 -1.240000E+00
 1354303 -8.000000E-01 -1.770000E+00
 1354304 -7.000000E-01 -2.360000E+00
 1354305 -6.000000E-01 -2.790000E+00
 1354306 -5.000000E-01 -2.910000E+00
 1354307 -4.000000E-01 -2.670000E+00
 1354308 -2.500000E-01 -1.690000E+00
 1354309 -1.000000E-01 -5.000000E-01
 1354310 0.000000E+00 0.000000E+00

* HEAD CURVE NO. 4

1354400 1 4
 1354401 -1.000000E+00 -1.160000E+00
 1354402 -9.000000E-01 -7.800000E-01
 1354403 -8.000000E-01 -5.000000E-01
 1354404 -7.000000E-01 -3.100000E-01
 1354405 -6.000000E-01 -1.700000E-01
 1354406 -5.000000E-01 -8.000000E-02
 1354407 -3.500000E-01 0.000000E+00
 1354408 -2.000000E-01 5.000000E-02
 1354409 -1.000000E-01 8.000000E-02

```

1354410 0.00000E+00 1.10000E-01
*****
* HEAD CURVE NO. 5
*****
1354500 1 5
1354501 0.00000E+00 0.00000E+00
1354502 2.00000E-01 -3.40000E-01
1354503 4.00000E-01 -6.60000E-01
1354504 6.00000E-01 -9.30000E-01
1354505 8.00000E-01 -1.19000E+00
1354506 1.00000E+00 -1.47000E+00
*****
* HEAD CURVE NO. 6
*****
1354600 1 6
1354601 0.00000E+00 1.10000E-01
1354602 1.00000E-01 1.30000E-01
1354603 2.50000E-01 1.50000E-01
1354604 4.00000E-01 1.30000E-01
1354605 5.00000E-01 7.00000E-02
1354606 6.00000E-01 -4.00000E-02
1354607 7.00000E-01 -2.30000E-01
1354608 8.00000E-01 -5.10000E-01
1354609 9.00000E-01 -9.10000E-01
1354610 1.00000E+00 -1.47000E+00
*****
* HEAD CURVE NO. 7
*****
1354700 1 7
1354701 -1.00000E+00 0.00000E+00
1354702 0.00000E+00 0.00000E+00
*****
* HEAD CURVE NO. 8
*****
1354800 1 8
1354801 -1.00000E+00 0.00000E+00
1354802 0.00000E+00 0.00000E+00
*****
* TORQUE CURVE NO. 1
*****
1354900 2 1
1354901 0.00000E+00 6.03200E-01
1354902 1.93000E-01 6.32500E-01
1354903 3.93000E-01 7.36900E-01
1354904 5.95520E-01 8.33100E-01
1354905 7.97820E-01 9.22900E-01
1354906 1.00000E+00 1.00000E+00
*****
* TORQUE CURVE NO. 2
*****
1355000 2 2
1355001 0.00000E+00 -6.70000E-01
1355002 4.00000E-01 -2.50000E-01
1355003 5.00000E-01 1.50000E-01
1355004 7.37255E-01 5.26586E-01
1355005 7.68049E-01 6.06594E-01
1355006 8.67230E-01 7.43660E-01
1355007 1.00000E+00 1.00000E+00
*****
* TORQUE CURVE NO. 3
*****
1355100 2 3
1355101 -1.00000E+00 1.98430E+00
1355102 -8.00960E-01 1.39400E+00
1355103 -6.06380E-01 1.09750E+00

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1355104 -4.06860E-01 8.22000E-01
1355105 -1.99280E-01 6.64800E-01
1355106 0.00000E+00 6.03200E-01
*****
* TORQUE CURVE NO. 4
*****
1355200 2 4
1355201 -1.00000E+00 1.98430E+00
1355202 -8.22340E-01 1.83080E+00
1355203 -6.33710E-01 1.68240E+00
1355204 -4.58630E-01 1.55700E+00
1355205 -2.67023E-01 1.43670E+00
1355206 -1.76107E-01 1.38790E+00
1355207 -8.83100E-02 1.34810E+00
1355208 0.00000E+00 1.23361E+00
*****
* TORQUE CURVE NO. 5
*****
1355300 2 5
1355301 0.00000E+00 -4.50000E-01
1355302 4.00000E-01 -2.50000E-01
1355303 5.00000E-01 0.00000E+00
1355304 1.00000E+00 3.56900E-01
*****
* TORQUE CURVE NO. 6
*****
1355400 2 6
1355401 0.00000E+00 1.23361E+00
1355402 9.06430E-02 1.19650E+00
1355403 1.85690E-01 1.10960E+00
1355404 2.73470E-01 1.04160E+00
1355405 4.58690E-01 8.95800E-01
1355406 5.74480E-01 7.80700E-01
1355407 7.38160E-01 6.13400E-01
1355408 7.68520E-01 5.84900E-01
1355409 8.70057E-01 4.87700E-01
1355410 1.00000E+00 3.56800E-01
*****
* TORQUE CURVE NO. 7
*****
1355500 2 7
1355501 -1.00000E+00 -1.00000E+00
1355502 -3.00000E-01 -9.00000E-01
1355503 -1.00000E-01 -5.00000E-01
1355504 0.00000E+00 -4.50000E-01
*****
* TORQUE CURVE NO. 8
*****
1355600 2 8
1355601 -1.00000E+00 -1.00000E+00
1355602 -2.50000E-01 -9.00000E-01
1355603 -8.00000E-02 -8.00000E-01
1355604 0.00000E+00 -6.70000E-01
*****
* REACTOR KINETICS
*****
* POINT KINETICS
*****
30000000 POINT 371.875
30000001 GAMMA-AC 50.0E6 0.

```

```

*****
* DELAYED NEUTRON CONSTANTS
*****
30000101 0.042 3.01
30000102 0.1150 1.14
30000103 0.3950 3.301
30000104 0.1960 0.301
30000105 0.2190 0.305
30000106 0.0330 0.0124
*****
* POWER HISTORY
*****
30000401 25.E+6 30. HR
30000402 50.0E+6 69. HR
*****
* REACTIVITY CURVE
*****
30000011 609
*****
* MODERATOR DENSITY REACTIVITY TABLE
*****
30000501 0.8125 -3.4
30000502 0.875 -1.8
30000503 0.9375 -0.3
30000504 1.0 1.0
30000505 1.0625 2.2
30000506 1.125 3.1
30000507 1.1875 4.0
30000508 1.25 4.9
*****
* DOPPLER REACTIVITY TABLE
*****
30000601 255. 1.5
30000602 500. 0.3
30000603 750. -0.7
30000604 1000. -1.6
30000605 1250. -2.3
30000606 1500. -3.0
30000607 1750. -3.7
30000608 2000. -4.3
30000609 2250. -4.9
30000610 2500. -5.4
30000611 2750. -5.9
30000612 3000. -6.3
*****
* SCRAM ROD WORTH CURVE 609
*****
20260900 REAC-T 601
20260901 0.0 0.0
20260902 0.1 -2.1
20260903 0.2 -4.3
20260904 0.3 -6.8
20260905 0.4 -9.2
20260906 0.5 -11.1
20260907 0.6 -12.2
20260908 0.7 -12.9
20260909 0.8 -13.3
20260910 0.9 -13.6
20260911 1.0 -13.7

```

20260912 1.1 -13.8
 20260913 1.2 -13.9
 20260914 1.8 -14.0
 20260915 1000. -14.0

 * MODERATOR DENS. FEEDBACK *

 30000701 230010000 0 0.15746 0.0
 30000702 230020000 0 0.15746 0.0
 30000703 230030000 0 0.15746 0.0
 30000704 230040000 0 0.15746 0.0
 30000705 230050000 0 0.15746 0.0
 30000706 230060000 0 0.21270 0.0

 * DOPPLER FEEDBACK *

 30000801 2300001 0 0.0170 0.0
 30000802 2300002 0 0.3639 0.0
 30000803 2300003 0 0.2747 0.0
 30000804 2300004 0 0.2379 0.0
 30000805 2300005 0 0.0976 0.0
 30000806 2300006 0 0.0089 0.0

 * STEAM GENERATOR SECONDARY SIDE *

 * TOP OF DOWNCOMER (OUTLET OF PRIMARY SEPARATOR) *

NO	DOWNTOP	BRANCH					
5000000	1	1					
5000101	1.273	0.718	0.0	0.0	-90.0	-0.718	
5000102	4.E-5	0.7874	0.0				
50001101	505010000	505000000	0.0	0.0	0.0	0100	

 * LOWER SEPARATOR SECTION *

 5000000 LWR-SEP SNGLVOL
 5000101 1.273 0.718 0.0 0.0 -90.0 -0.718
 5000102 4.E-5 0.7874 0.0

 * FEED INLET VOLUME *

 5000000 FEED-INLET BRANCH
 5000101 0.7525 0.518 0.0 0.0 -90.0 -0.518
 5000102 4.E-5 0.10796 0.0
 50001101 505010000 510000000 0.0 0.0 0.0 0100
 500012101 510010000 515000000 0.0 0.0 0.0 0100

 * SEPARATOR (INSIDE SHROUD, ABOVE TUBES) *

 52000000 SEPAR SEPARATR
 5200001 3 1
 5200101 0.27871 0.718 0.0 0.0 90.0 0.718
 5200102 4.E-5 0.0
 5201101 520010000 525000000 0.0 2. 2. 1000 .5

5202101 520000000 505000000 0.0 5. 5. 1000 .10
 5203101 519010000 520000000 0.196 0.4 0.4 1000

 * BELOW MIST EXTRACTOR, ABOVE TOP OF SHROUD IN STEAM DOME *

 5250000 BOTSTMDM BRANCH
 5250001 1
 5250101 .90 0.762 0.0 0.0 90.0 0.762
 5250102 4.E-5 0.0 0.0
 5251101 525010000 530000000 0.0 0.8 0.8 0100

 * BELOW MIST EXTRACTOR, PRALLEL VOLUME *

 5260000 BOTSTMDM BRANCH
 5260001 2
 5260101 .2148 0.762 0.0 0.0 -90.0 -0.762
 5260102 4.E-5 0.0 0.0
 5261101 526010000 525000000 0.0 0.8 0.8 0103
 5262101 526010000 500000000 0.0 0.0 0.0 0100

 * MIST EXTRACTOR AND STEAM GEN OUTLET PIPE TO SCV *

53000000 STMDM-PIPE PIPE
 5300001 2
 5300101 0.799008 1
 5300102 0.04635 2
 5300201 0.01365 1
 5300301 0.782 1
 5300302 25.074 2
 5300401 0.0 2
 5300601 90.0 1
 5300602 0.0 2
 5300801 4.E-5 0.0 2
 5300901 0.4 0.4 1
 5301001 0.0 2
 5301101 0100 1
 5301300 0
 5301300 1

 * PIPE DOWNSTREAM OF SCV *

 5350000 CONDNL SNGLVOL
 5350101 0.06557 54.44 0.0 0.0 0.0 0.0
 5350102 4.E-5 0.0

 * AIR COOLED CONDENSER *

 54000000 CONDSE TMDPVOL
 5400101 0.21677 17.67 0.0 0.0 0.0 0.0
 5400102 4.E-5 0.02 0.0
 5400200 2
 5400207 0.0 2.0200E6 1.0
 5400208 1000. 2.0200E6 1.0

 * MAKE UP FEED STORAGE TANK *

 5450000 FEEDTANK TMDPVOL
 5450101 29.81 3.048 0.0 0.0 0.0 0.0
 5450102 4.E-5 0.0

5450700 0 0 CNTRLVAR 606
 5450201 .8540E6 6.0E6 .8540E6 2.785E6 .5
 5450202 1.0378E6 6.0E6 1.0378E6 2.785E6 .5

 * FLOW PATH TO THE AIR COOLED CONDENSER *

 5550000 COACCO SNGLJUM
 5550101 535010000 540000000 0.0 0.0 0.0 0100

 * HEAT STRUCTURE INPUT DATA *

 * STEAM GENERATOR HEAT STRUCTURES *

 * SHROUD SECONDARY SIDE STEAM GENERATOR *

15000000	3	4	2	1	0.3048	
15000100	0					
15000101	3				0.314325	
15000201	6	3				
15000301	0.0	3				
15000401	540.0	4				
15000501	500010000	0	1	1		0.7725 1
15000502	505010000	0	1	1		0.7725 2
15000503	510010000	0	1	1		0.152 3
15000601	520010000	0	1	1		0.7725 1
15000602	519020000	0	1	1		0.7725 2
15000603	519010000	0	1	1		0.152 3
15000701	0	0	0	0		3
15000801	0	0.0	0.0	0.0		3
15000901	0	0.0	0.0	0.0		3
15150000	4	4	2	0		0.6445
15150100	0					
15150101	3					
15150201	5					
15150301	0.0					
15150401	540.0	4				
15150501	510010000	0	1	1		0.152 1
15150502	515010000	10000	1	1		0.7113 4
15150601	519010000	0	1	1		0.152 1
15150602	517030000	0	1	1		0.7113 4
15150701	0	0	10000	1		
15150801	0	0.0	0.0	0.0		4
15150901	0	0.0	0.0	0.0		4

 * SG VESSEL VALL - SURROUNDINGS *

15050000	5	4	2	1	.7112
15050100	0	1			
15050101	3				.73819
15050201	5				
15050301	0.0				
15050401	540.0	4			
15050501	505010000	0	1	1	.718 1
15050502	510010000	0	1	1	.518 2
15050503	515010000	10000	1	1	.7102 1
15050601	-999	0	3949	1	
15050602	-999	0	3949	1	
15050603	-999	0	3949	1	

15050701 0 0.0 0.0 0.0 5
 15050801 0 0.0 0.0 0.0 5
 15050901 0 0.0 0.0 0.0 5

S.G. SECONDARY DNWC-BOIL-RISR

STEAM GENERATOR DOWNCOMER

ID	DNWCNR	PIPE
5150000	DNWCNR	PIPE
5150001	3	
5150101	0.23226	3
5150201	0.0	2
5150301	0.7102	3
5150401	0.0	3
5150501	-90.	3
5150701	-0.7102	3
5150801	4.E-5	0.10796 3
5150901	0.0	0.0 2
5151001	00	3
5151101	0000	2
5151300	1	

STEAM GENERATOR BOILING SECTION

ID	BILSCT	PIPE
5170000	BILSCT	PIPE
5170001	3	
5170101	0.27871	3
5170201	0.0	2
5170301	1.85075	3
5170401	0.0	3
5170501	21.0	3
5170701	0.7102	3
5170801	4.E-5	0.0192 3
5170901	0.0	0.0 1
5170902	0.0	0.0 2
5171001	00	3
5171101	0000	2
5171300	0	

STEAM GENERATOR RISER

ID	RISER	PIPE
5190000	RISER	PIPE
5190001	2	
5190101	0.27871	2
5190201	0.0	1
5190301	1.85075	1
5190302	0.718	2
5190401	0.0	2
5190501	16.0	1
5190602	90.0	2
5190701	0.518	1
5190702	0.718	2
5190801	4.E-5	0.5957 1
5190802	4.E-5	0.0 2
5190901	0.0	0.0 1
5191001	00	2
5191101	0000	1
5191300	0	

SG DOWNCOMER TO BOILING SECTION, VALVE FOR RECIRCULATION RATIO

ID	DNWCBOIL VALVE	VALVE
5160000	DNWCBOIL VALVE	VALVE
5160101	516010000	517000000 .232 1. 1. 0100
5160201	1	130.7 0.0 0.0
5160300	SRVVLV	
5160301	216	

SG BOILING SECTION TO RISER

ID	BOILRSR	BRANCH
5180000	BOILRSR	BRANCH
5180101	517010000	519000000 0.0 0.0 0000

BROKEN LOOP

REACTOR VESSEL BROKEN LOOP HOT LEG

ID	RVBLHL	BRANCH
3000000	RVBLHL	BRANCH
3000001	2	1
3000101	0.0634	0.876 0.0 0.0 0.0 0.0
3000102	4.0E-5	0.0 00
3001101	295010000	300000000 0.0634 0.1 0.1 0102
3002101	300010000	305000000 0.0 0.1 0.1 0000

HOT LEG PIPE TO REFLOOD ASSIST BYPASS TEE

ID	HLPRAS	BRANCH
3050000	HLPRAS	BRANCH
3050001	1	1
3050101	0.0634	0.698 0.0 0.0 0.0 0.0
3050102	4.0E-5	0.0 00
3051101	305010000	310000000 0.0 0.05 0.05 0100

STEAM GENERATOR SIMULATOR INLET

ID	SGSII	BRANCH
3100000	SGSII	BRANCH
3100001	2	1
3100101	0.0	1.424 0.0668 0.0 0.0 0.0
3100102	4.0E-5	0.0 00
3101101	370010000	310000000 0.0 0.0 0.0 0100
3102101	310010000	316000000 0.0 0.05 0.05 0100

S.G. PIPE AND PUMP SIMULATOR

ID	SGPSI	PIPE
3150000	SGPSI	PIPE
3150001	10	
3150101	0.00836	2
3150102	0.108	7
3150103	0.0	8
3150104	0.00836	9
3150105	0.0525	10
3150201	0.0	2
3150202	0.0326	6
3150203	0.0	7
3150204	0.0081	8

3150205	0.0	9
3150301	0.4054	1
3150302	0.5265	2
3150303	0.362	3
3150304	1.692	4
3150305	1.699	6
3150306	1.692	6
3150307	0.362	7
3150308	2.671	8
3150309	1.842	9
3150310	0.667	10
3150401	0.0	7
3150402	0.081	8
3150403	0.0	10
3150601	90.	4
3150602	0.	5
3150603	-90.	8
3150604	90.	9
3150605	0.	10
3150701	0.127	1
3150702	0.488	2
3150703	0.362	3
3150704	1.692	4
3150705	0.0	6
3150706	-1.692	6
3150707	-0.362	7
3150708	-1.829	8
3150709	1.214	9
3150710	0.0	10
3150801	4.0E-5	0.0 3
3150802	4.0E-5	0.124 4
3150803	4.0E-5	0.0 5
3150804	4.0E-5	0.124 6
3150805	4.0E-5	0.0 10
3150901	0.1	0.1 1
3150902	0.1	0.1 2
3150903	93.9	93.9 4
3150904	93.9	93.9 6
3150905	0.0	0.0 7
3150906	4.1	4.1 8
3150907	0.4	0.4 9
3151001	00	10
3151101	0100	9
3151300	1	

BROKEN LOOP COLD LEG REACTOR VESSEL NOZZLE

ID	RVNBL	BRANCH
3350000	RVNBL	BRANCH
3350001	2	1
3350101	0.0634	0.7495 0.0 0.0 0.0 0.0
3350102	4.0E-5	0.0 00
3351101	290000000	335000000 0.0634 1.0 1.0 0102
3352101	335010000	340000000 0.0 0.1 0.1 0000

CONNECTION TEE OF THE BYPASS ASSIST SYSTEM REACTOR VESSEL SIDE

ID	CTBARV	BRANCH
3400000	CTBARV	BRANCH
3400001	1	1
3400101	0.0634	0.698 0.0 0.0 0.0 0.0
3400102	4.0E-5	0.0 00
3401101	340010000	345000000 0.0 0.1 0.1 0000

* BYPASS ASSIST OUTLET ECC TEE COLD LEG
 *
 3450000 BADET BRANCH
 3450001 2 1
 3450101 0.0634 0.974 0.0 0.0 0.0 0.0
 3450102 4.E-5 0.0 0.0
 3451101 380010000 345000000 0.0 0.0 0.0 0100
 3452101 345010000 350000000 0.0 0.0 0.0 0100

 * ECC TEE OF BROKEN LOOP
 *

3500000 ETIVCL SINGVOL
 3500101 0.0 2.0965 0.08311 0.0 0.0 0.0
 3500102 4.E-5 0.0 0.0

 * REFLOOD ASSIST HOT LEG
 *

3700000 RFASHL SINGVOL
 3700101 0.0388 0.0 0.1713 0.0 90. 0.653
 3700102 4.E-5 0.0 0.0

 * VALVE JUNCTION FOR THE RABV
 *

3720000 RABV VALVE
 3720101 380000000 370000000 .01 1. 1. 0100
 3720201 1 2.0965 0.08311 0.0 0.0 0.0
 3720300 SRVVLV 6.28 0.0 0.0
 3720301 372

 * REFLOOD ASSIST BYPASS SINGLE PIPE COLD LEG SIDE
 *

3800000 RFASCL SINGVOL
 3800101 0.0388 0.0 0.20353 0.0 90. 0.653
 3800102 4.E-5 0.0 0.0

 * ECC SYSTEM
 *

 * DWST HPIS
 *

6250000 BwthPI TMDPVOL
 6250101 20.44 5.0 0.0 0.0 90.0 5.0
 6250102 4.E-5 0.0 0.0
 6250200 3
 6250201 0.0 1.0E5 305.0
 6250202 1000.0 1.0E5 305.0

 * HIGH PRESSURE INJECTION SYSTEM - A+B
 *

6300000 HPIS TMDPVOL
 6300101 625000000 210000000 0.009099
 6300200 1 661 P 210010000
 6300201 -1.0 0.0 0.0 0.0
 6300202 0.0 0.0 0.0 0.0
 6300203 0.0 -75687 0.0 0.0
 6300204 .7725E6 -75687 0.0 0.0

6300205 8.3597E6 .31536 0.0 0.0
 6300206 17.2436E6 .31536 0.0 0.0

 * ICAP ASSESSMENT PARAMETERS
 *

 * CORE INLET FLUID DENSITY
 *

20550100 DCOREINF MULT 1. 0.0 1
 20550101 VOIDFJ 225010000
 20550102 RHOFJ 225010000

20550200 DCOREING MULT 1. 0.0 1
 20550201 VOIDGJ 225010000
 20550202 RHOGJ 225010000

20590100 DENSCORIN SUM 1. 0.0 1
 20590101 0.0 1. CNTRLVAR 501
 20590102 1. CNTRLVAR 502

 * ROD CLADDING TEMPERATURE SAVE UP
 *

20590300 CLDTEMP1 MULT 1. 0.0 1
 20590301 HTTEMP 230000109
 20590400 CLDTEMP2 MULT 1. 0.0 1
 20590401 HTTEMP 230000209
 20590500 CLDTEMP3 MULT 1. 0.0 1
 20590501 HTTEMP 230000309
 20590600 CLDTEMP4 MULT 1. 0.0 1
 20590601 HTTEMP 230000409
 20590700 CLDTEMP5 MULT 1. 0.0 1
 20590701 HTTEMP 230000509
 20590800 CLDTEMP6 MULT 1. 0.0 1
 20590801 HTTEMP 230000609

 * FLUID TEMPERATURE AT THE CORE OUTLET
 *

20550400 FLOWDIR TRIPUNIT 1. 0.0 1
 20550401 518
 20550500 TOIRP MULT 1. 0.0 1
 20550501 CNTRLVAR 504
 20550502 TEMPF 230060000
 20550600 FLOWDIRM TRIPUNIT 1. 0.0 1
 20550601 -518

20550700 TDIRM MULT 1. 0.0 1
 20550701 CNTRLVAR 506
 20550702 TEMPF 240010000

20590900 TCOROUT SUM 1. 0.0 1
 20590901 0. 1. CNTRLVAR 505
 20590902 1. CNTRLVAR 507

 * CORE TEMPERATURE DIFFERENCE
 *

20591000 CTDIFF SUM 1. 0.0 1
 20591001 1. TEMPF 240010000
 20591002 0. -1. TEMPF 225010000

 * PRESS. DIFF. OVER THE CORE
 *

20591200 COREIMV SUM 1. 0.0 1
 20591201 0.0 1. 225010000
 20591202 -2.76 RHO 225010000

20591203 -1. P 245010000
 20591204 3.31 RHO 245010000

 * PRESS. DIFF. OVER THE DOWNCOMER
 *

20591300 DOWNINV SUM 1. 0.0 0
 20591301 0.0 1. P 185010000
 20591302 -1. P 215010000
 20591303 -.78 RHO 215010000

 * VESSEL MASS INVENTORY
 *

20551400 VESSMS1 SUM 1. 0.0 1
 20551401 0.0 .0465 RHO 200010000
 20551402 .078 RHO 290010000
 20551403 .071 RHO 205010000
 20551404 .136036 RHO 210010000
 20551405 .136036 RHO 210010000
 20551406 .136036 RHO 210030000
 20551407 .136036 RHO 210040000
 20551408 .2664 RHO 215010000
 20551409 .2923 RHO 220010000
 20551410 .130 RHO 225010000
 20551411 -.047655 RHO 230010000
 20551412 .047655 RHO 230020000
 20551413 .047655 RHO 230030000
 20551414 .047655 RHO 230040000
 20551415 .047655 RHO 230050000
 20551416 .064364 RHO 230060000

 * VESSEMS2 SUM 1. 0.0 1
 20551500 0.0 .008385 RHO 235010000
 20551501 .008385 RHO 235020000
 20551502 .008385 RHO 235030000
 20551503 .008385 RHO 235040000
 20551504 .332046 RHO 240010000
 20551505 .079002 RHO 245010000
 20551506 .1281 RHO 246010000
 20551507 .0603 RHO 295010000
 20551508 .202752 RHO 250010000
 20551509 .173728 RHO 255010000

20591400 VESSMASS SUM 1. 0.0 1
 20591401 0.0 1. CNTRLVAR 514
 20591402 1. CNTRLVAR 515

 * DOWNCOMER LIQUID LEVEL
 *

20591500 DOWNLEV SUM 1. 0.0 1
 20591501 0.162 .1065 VOIDF 200010000 **
 20591502 .300 VOIDF 290010000
 20591503 .274 VOIDF 205010000
 20591504 .958 VOIDF 210010000
 20591505 .958 VOIDF 210020000
 20591506 .958 VOIDF 210030000
 20591507 .958 VOIDF 210040000
 20591508 .360 VOIDF 215010000
 20591509 .208 VOIDF 220010000 **

 * UPPER PLENUM LIQUID LEVEL
 *

20591600 UPLEV SUM 1. 0.0 1
 20591601 3.764 .3084 VOIDF 240010000 **
 20591602 .693 VOIDF 245010000
 20591603 .300 VOIDF 295010000
 20591604 .3251 VOIDF 250010000 **

 * UPPER PLENUM SUBCOOLING
 *

20591900 UPSCOOL SUM 1. 0.0 1
 20591901 0.0 1. SATTEMP 240010000

1987-11-03

20555202	.4988	HTRNR	100100900 * 175.1
20555203	.5469	HTRNR	100101000 * 175.2
20555204	.6254	HTRNR	100101100 * 180
20555205	1.3035	HTRNR	100101200 * 185
20555206	.6687	HTRNR	335000100 * 335
20555207	.6278	HTRNR	335000200 * 340
20555208	.8690	HTRNR	335000300 * 345
20555209	1.0578	HTRNR	350100100 * 350
20555210	3.6545	HTRNR	375000200 * 380
20555211	.1312	HTRNR	315000100 * 315.1
20555212	.1704	HTRNR	315000200 * 315.2
20555213	1.9589	HTRNR	315300100 * 315.3
20555214	1.9589	HTRNR	315300200 * 315.4
20555215	1.9589	HTRNR	315300300 * 315.5
20555216	1.9589	HTRNR	315300400 * 315.6
20555217	.4174	HTRNR	315300500 * 315.7
20555218	1.8025	HTRNR	315100100 * 315.8
20555219	.7639	HTRNR	315200100 * 315.9
20555220	.6385	HTRNR	315400100 * 315.10/ = 21.950

20555300	STR-HTL3	SUM	-1.	0.0	1	300
20555301	0.0		.7816	HTRNR	300000100 * 300	
20555302			.6228	HTRNR	300000200 * 305	
20555303			1.2705	HTRNR	300000300 * 310	
20555304			3.0792	HTRNR	375000100 * 370	
20555305			-1.6800	HTRNR	220000101 * 220	
20555306			1.7045	HTRNR	252000100 * 252 / -9.8506 M2	
20555307			.7120	HTRNR	255000100 * 255	

20598200	STR-HTL	SUM	1.	0.0	1	
20598201	0.0		1.	CNTRLVAR	551	
20598202			1.	CNTRLVAR	552	
20598203			1.	CNTRLVAR	553	* T.AREA =46.1242 M2

 * AUX. FEEDWATER

 * SS VOLUME STATES

 * BOUNDARY CONDITION CONTROL

 * MAIN STEAM CONTROL VALVE

5500000	MSFCV	TMDPJUN	530010000	535000000	0.002573
5500101	1.	501			
5500201	-1.	0.0	27.80	0.0	
5500202	0.0	0.0	27.80	0.0	* FLOW RATE FROM NUREG/CR-0247
5500203	3.	0.0	23.4	0.0	* PRESSURE RISE 5.57 - 6.90 MPA
5500204	6.0	0.0	15.1	0.0	* 5% CHANGE RATE ASSUMED
5500205	9.	0.0	9.3	0.0	
5500206	13.6	0.0	6.2	0.0	
5500207	13.6	0.0	.181	0.0	* LEAKAGE
5500208	94.8	0.0	.181	0.0	
5500209	94.8	0.0	2.85	0.0	* VALVE OPEN AT 99 S
5500210	104.8	0.0	2.85	0.0	* VALVE CLOSE AT 99 S
5500211	104.8	0.0	.181	0.0	* LEAKAGE
5500212	500.	0.0	.173	0.0	* FROM EXP. SECONDARY PRESSURE
5500213	1000.	0.0	.150	0.0	* LINEAR P-DEPENDENCE ASSUMED
5500214	1500.	0.0	.136	0.0	* .120 KG/S AT 4.5 MPA
5500215	2370.	0.0	.113	0.0	

 * FEED WATER VALVE

5500000	FWLV	TMDPJUN	5600101	545000000	510000000	0.05
5600200	1.	501				
5600201	-1.	27.80	0.0	0.0	0.0	
5600202	0.0	27.80	0.0	0.0	0.0	
5600203	7	0.0	0.0	0.0	0.0	
5600208	3000.	0.0	0.0	0.0	0.0	

5540000	AUXFTANK	TMDPVOL	5540101	3.0	10.0	0.0	0.0	0.0	0.0	3.33E-5	1.0
5540200	1	0.0									
5540201	0.0	315.0	0.0								
5480000	AUXFJUN	TMDPJUN	5480101	554000000	510000000	.1					
5480200	1	510									
5480201	-1.	0.0	0.0	0.0	0.0						
5480202	73.3	0.0	0.0	0.0	0.0						
5480203	73.4	.50364	0.0	0.0	0.0						
5480204	1856.	.60364	0.0	0.0	0.0						
5480205	1857.0	0.0	0.0	0.0	0.0						

1000200	3	14.8896E6	577.73								
1050200	3	14.8832E6	577.73								
1100200	3	14.8606E6	577.72								
1151201	3	14.8607E6	577.71	0.0	0.0	0.0	0.0	1			
1151202	3	14.8624E6	577.71	0.0	0.0	0.0	0.0	2			
1151203	3	14.7834E6	577.68	0.0	0.0	0.0	0.0	3			
1151204	3	14.7603E6	575.52	0.0	0.0	0.0	0.0	4			
1151205	3	14.7365E6	569.98	0.0	0.0	0.0	0.0	5			
1151206	3	14.7195E6	566.28	0.0	0.0	0.0	0.0	6			
1151207	3	14.7116E6	563.09	0.0	0.0	0.0	0.0	7			
1151208	3	14.7045E6	560.77	0.0	0.0	0.0	0.0	8			
1151209	3	14.6967E6	558.68	0.0	0.0	0.0	0.0	9			
1151210	3	14.6968E6	558.68	0.0	0.0	0.0	0.0	10			
1151211	3	14.6191E6	558.66	0.0	0.0	0.0	0.0	11			
1151212	3	14.6097E6	558.65	0.0	0.0	0.0	0.0	12			
1151213	3	14.6046E6	558.65	0.0	0.0	0.0	0.0	13			
1200200	3	14.6010E6	558.65								
1250200	3	14.5885E6	558.64								
1300200	3	14.5670E6	558.63								
1350200	3	14.8202E6	558.78								
1400200	3	15.0825E6	558.78								
1450200	3	15.0878E6	558.79								
1500200	3	15.0603E6	558.82								
1550200	3	14.5884E6	558.64								
1600200	3	14.5679E6	558.63								
1650200	3	14.8239E6	558.78								
1700200	3	15.0869E6	558.87	0.0	0.0	0.0	0.0	1			
1751201	3	15.0542E6	558.81	0.0	0.0	0.0	0.0	2			
1751202	3	15.0473E6	558.81								
1800200	3	15.0435E6	558.81								
1850200	3	15.0417E6	558.81								
2000200	3	15.0400E6	558.82								
2050200	3	15.0190E6	558.80								
2101201	3	15.0171E6	558.80	0.0	0.0	0.0	0.0	1			
2101202	3	15.0231E6	558.81	0.0	0.0	0.0	0.0	2			
2101203	3	15.0292E6	558.81	0.0	0.0	0.0	0.0	3			
2101204	3	15.0335E6	558.82	0.0	0.0	0.0	0.0	4			

2150200	3	15.0437E6	558.82								
2200200	3	15.0464E6	558.82								
2250200	3	15.0329E6	558.82								
2301201	3	15.0042E6	559.98	0.0	0.0	0.0	0.0	1			
2301202	3	14.9994E6	566.20	0.0	0.0	0.0	0.0	2			
2301203	3	14.9918E6	571.49	0.0	0.0	0.0	0.0	3			
2301204	3	14.9870E6	576.31	0.0	0.0	0.0	0.0	4			
2301205	3	14.9793E6	579.37	0.0	0.0	0.0	0.0	5			
2301206	3	14.9737E6	580.13	0.0	0.0	0.0	0.0	6			
2351201	3	14.9879E6	558.81	0.0	0.0	0.0	0.0	1			
2351202	3	14.9764E6	558.81	0.0	0.0	0.0	0.0	2			
2351203	3	14.9640E6	558.81	0.0	0.0	0.0	0.0	3			
2400200	3	14.9512E6	579.53								
2450200	3	14.9318E6	578.71								
2460200	3	14.9465E6	578.71								
2500200	3	14.9329E6	557.75								
2550200	3	14.9278E6	557.75								
2900200	3	15.0404E6	558.81								
2950200	3	14.9358E6	577.75								
3000200	3	14.9358E6	558.63								
3050200	3	14.9358E6	558.63								
3100200	3	14.9358E6	558.63								
3151201	3	14.9354E6	558.00	0.0	0.0	0.0	0.0	1			
3151202	3	14.9331E6	558.00	0.0	0.0	0.0	0.0	2			
3151203	3	14.9299E6	558.00	0.0	0.0	0.0	0.0	3			
3151204	3	14.9223E6	558.00	0.0	0.0	0.0	0.0	4			
3151205	3	14.9160E6	558.00	0.0	0.0	0.0	0.0	5			
3151206	3	14.9223E6	558.00	0.0	0.0	0.0	0.0	6			
3151207	3	14.9299E6	558.00	0.0	0.0	0.0	0.0	7			
3151208	3	14.9380E6	558.00	0.0	0.0	0.0	0.0	8			
3151209	3	14.9402E6	558.00	0.0	0.0	0.0	0.0	9			
3151210	3	14.9357E6	558.00	0.0	0.0	0.0	0.0	10			
3350200	3	15.0404E6	558.70								
3400200	3	15.0404E6	558.58								
3450200	3	15.0404E6	558.40								
3500200	3	15.0404E6	558.00								
3700200	3	14.9382E6	557.15								
3800200	3	15.0478E6	557.73								
4000200	3	14.9131E6	577.85								
4050200	3	14.9092E6	577.24								
4151201	2	14.9071E6	0.0	0.0	0.0	0.0	0.0	1			
4151202	2	14.9052E6	0.0	0.0	0.0	0.0	0.0	2			
4151203	2	14.9028E6	0.0	0.0	0.0	0.0	0.0	3			
4151204	2	14.9011E6	.05661	0.0	0.0	0.0	0.0	4			
4151205	2	14.9006E6	1.	0.0	0.0	0.0	0.0	5			
4151206	2	14.9004E6	1.	0.0	0.0	0.0	0.0	6			
4151207	2	14.9002E6	1.	0.0	0.0	0.0	0.0	7			
4151208	2	14.9001E6	1.	0.0	0.0	0.0	0.0	8			
42002											

5350200 2 2.03274E6 1.0
8000200 3 15.0012E6 477.00

* SS JUNCTION STATES

1001201	483.3	0.0	0.0
1002201	483.3	0.0	0.0
1051201	483.3	0.0	0.0
1101201	483.3	0.0	0.0
1151301	483.3	0.0	0.0
1151302	483.3	0.0	0.0
1151303	483.3	0.0	0.0
1151304	483.3	0.0	0.0
1151305	483.3	0.0	0.0
1201201	483.3	0.0	0.0
1202201	241.6	0.0	0.0
1203201	241.6	0.0	0.0
1251201	241.6	0.0	0.0
1252201	0.0	0.0	0.0
1350201	1	241.6	0.0
1350202	1	241.6	0.0
1451201	241.6	0.0	0.0
1452201	241.6	0.0	0.0
1501201	241.6	0.0	0.0
1502201	483.3	0.0	0.0
1551201	241.6	0.0	0.0
1650201	1	241.6	0.0
1650202	1	241.6	0.0
1701201	0.0	0.0	0.0
1751301	483.3	0.0	0.0
1801201	483.3	0.0	0.0
1851201	483.3	0.0	0.0
1852201	483.3	0.0	0.0
2051201	445.1	0.0	0.0
2101301	445.1	0.0	0.0
2101302	445.1	0.0	0.0
2151201	445.1	0.0	0.0
2152201	1.E-5	0.0	0.0
2153201	445.1	0.0	0.0
2251201	427.7	0.0	0.0
2301301	427.7	0.0	0.0
2351301	17.4	0.0	0.0
2401201	427.7	0.0	0.0
2402201	17.4	0.0	0.0
2451201	445.1	0.0	0.0
2461201	1.E-5	0.0	0.0
2501201	-15.95	0.0	0.0
2502201	0.0	0.0	0.0
2901201	-15.95	0.0	0.0
2951201	461.1	0.0	0.0
3001201	-6.28	0.0	0.0
3002201	-6.28	0.0	0.0
3051201	-6.28	0.0	0.0
3101201	-6.28	0.0	0.0
3102201	0.0	0.0	0.0
3151301	0.0	0.0	0.0
3351201	6.28	0.0	0.0
3352201	6.28	0.0	0.0
3401201	6.28	0.0	0.0
3451201	-6.28	0.0	0.0
3452201	0.0	0.0	0.0

372 RABV / 1.3 X
435 SS SYSTEM PRESSURE

5001201	0.0	0.0	0.0
5101201	102.9	0.0	0.0
5102201	130.7	0.0	0.0
5151301	130.7	0.0	0.0
5151302	130.7	0.0	0.0
5160201	1	130.7	0.0
5171301	1.260	1.608	0.0
5171302	2.010	2.829	0.0
5180201	0	3.001	4.176
5191301	3.489	4.073	0.0
5201201	0.0	27.80	0.0
5202201	102.9	0.0	0.0
5203201	102.9	27.80	0.0
5251201	0.0	27.80	0.0
5261201	0.0	0.0	0.0
5262201	0.0	0.0	0.0
5301301	0.0	27.8	0.0
5550201	1	0.0	27.8
8001201	0.0	0.0	0.0
8050201	1	0.0	0.0

548 AUX FEED
550 MAIN STEAM VALVE
560 FEED WATER VALVE
571 SG SS LEVEL
591 SG SS PRESSURE
630 HPIS INJECTION
901 PUMP COOLANT INJECTION

20522400	CBPERR	SUM	1.	0.0	1
20522401	0.	1.	MFLOWJ	226000000	
20522402		-.036	MFLOWJ	185010000	
20522500	CBPREG	MULT	1.	0.0	1
20522501	CNTRLVAR	274			
20522502	CNTRLVAR	512			
20522600	CBPV	INTEGRAL	-.10	.214	0 3 .01 .99
20522601	CNTRLVAR	225			

20529400	IAUPERR	SUM	1.	0.0	0
20529401	0.	1.	MFLOWJ	296000000	
20529402		1.	MFLOWJ	297000000	
20529403		-.066	MFLOWJ	185010000	
20529500	IAUPREG	MULT	1.	0.0	0
20529501	CNTRLVAR	294			
20529502	CNTRLVAR	512			
20529600	IAUPV	INTEGRAL	-.06	.218	0 3 .01 .99
20529601	CNTRLVAR	295			

* SS CONTROL FOR THE RABV LEAKAGE / 1.3 X

20537000	RABVERR	SUM	1.	0.0	0
20537001	0.	1.	MFLOWJ	372000000	
20537002		-.013	MFLOWJ	185010000	
20537100	RABVREG	MULT	1.	0.0	0
20537101	CNTRLVAR	370			
20537102	CNTRLVAR	512			
20537200	RABVV	INTEGRAL	-.03	.079	0 3 .01 .99
20537201	CNTRLVAR	371			

* SS CONTROL FOR INLET ANN. TO DOWNCOMER FLOW

20528900	IADCERR	SUM	1.	0.0	0
20528901	-483.3	1.	MFLOWJ	185010000	
20529000	IADCREG	MULT	1.	0.0	0
20529001	CNTRLVAR	289			
20529002	CNTRLVAR	512			
20529100	IADCV	INTEGRAL	-.06	.384	0 3 .01 .99
20529101	CNTRLVAR	290			

* SS CONTROL FOR VALVE 516, RECIRCULATION RATIO = 4.7

20521400	ERR516	SUM	1.	0.0	0
20521401	0.	1.	MFLOWJ	516000000	
20521402		-4.7	MFLOWJ	560000000	
20521500	REG516	MULT	1.	0.0	0
20521501	CNTRLVAR	214			
20521502	CNTRLVAR	512			
20521600	V516	INTEGRAL	-.1	.739	0 3 .01 .99
20521601	CNTRLVAR	215			

* SS CONTROL FOR FEED WATER ENTHALPHY

20560100	SPRDERR	SUM	1.0	0.0	0
20560101	0.	-1.	MFLOWJ	560000000	
20560102		.914014	VAPGEN	500010000	
20560103		.914014	VAPGEN	505010000	
20560104		.389795	VAPGEN	510010000	
20560105		.164951	VAPGEN	515010000	
20560106		.164951	VAPGEN	515020000	
20560107		.164951	VAPGEN	515030000	
20560108		.515823	VAPGEN	517010000	
20560109		.515823	VAPGEN	517020000	
20560110		.515823	VAPGEN	517030000	
20560111		.515823	VAPGEN	519010000	
20560112		.200114	VAPGEN	519020000	
20560113		.200114	VAPGEN	520010000	
20560114		.685800	VAPGEN	525010000	
20560115		.163678	VAPGEN	526010000	
20560116		.608844	VAPGEN	530010000	
20560117		1.16218	VAPGEN	530020000	
20560200	SENTHD	SUM	1.0	0.0	1
20560201	0.0	1.0	UG	517030000	

```

20560202      -1.    UF      517030000
*
20560300  SSK1    MULT    -1.    0.0    0
20560301  CNTRLVAR 601
20560302  CNTRLVAR 602
20560303  CNTRLVAR 612
*
20560400  SSK2    MULT      1.    1.    1 1 1.
20560401  MFLOWJ  560000000
*
20560500  SSK3    DIV      1.    0.0    0
20560501  CNTRLVAR 604      CNTRLVAR 603
*
20560600  FDWENTH  INTEGRAL .10  .980E6 0 3 .800E6 1.00E6
20560601  CNTRLVAR 605
*****
* STEAM GENERATOR SS PRESSURE
*
5900000  SGSSPR  TMDPVOL
5900101  .1      1.0 0.0 0.0 0.0 0.0
5900102  4.E-5  0.0      00
5900200  2
5900201  0.0    5.57E6  1.
5900202  10000. 5.57E6  1.
*
5910000  SGSSPRJ VALVE
5910101  530000000 0.0 0.0 0.0 0100
5910201  1      0.0      0.0
5910300  TRPVLV
5910301  646
*****
* SG STEADY STATE LEVEL HOLDING
*
5700000  SGLHOLDV TMDPVOL
5700101  .1      1.    0.0 0.0 0.0 0.0
5700102  4.E-5  0.0      00
5700200  2      0      P      505010000
5700201  4.E6  4.E6  .5
5700202  7.E6  7.E6  .5
*
5710000  SGLHOLDJ TMDPJUN
5710101  505010000 570000000 .1
5710200  1      0      CNTRLVAR 513
5710201  -10.   -10.   0.0 0.0
5710202  10.    10.    0.0 0.0
*
20551100  SGLEVER1 SUM      50.    0.0 0
20551101  -.22   1.      CNTRLVAR 949
*
20551200  TRP-501 TRIPUNIT 1.    0.0 1
20551201  -501
*
20551300  SGLEVER2 MULT      1.    0.0 0
20551301  CNTRLVAR 511
20551302  CNTRLVAR 512
*****
* SS SYSTEM PRESSURE
*
4300000  PRVOL  TMDPVOL
4300101  .362   .224   0.0 0.0 0.0 .224
4300102  4.E-5  0.0    11
4300200  3      0      P      415010000

```

```

4300201  .1E6   .1E6   575.
4300202  16.E6  16.E6  575.
*
4350000  PRVALVE VALVE
4350101  405010000 430000000 0.0 .093 .093 0100
4350201  1      0.0      0.0      0.0
4350300  TRPVLV
4350301  646
*****
** END OF FILE
**

```

*** LFBR2 ***
RESTART OF LOFT CALCULATION L3-6 FROM SS RUN

LOBI RESTART
100 RESTART STDY-ST
101 RUN
103 2196
105 100. 120.

0000201 200. 1.0E-6 .20 00001 25 4000 4000
501 TIME 0 GE NULL 0 1000. L

20299700 TEMP 501
20299701 -1. 305.
20299702 0.0 305.
*
* SG HEAT TRANSFER RATE
20595300 SGNHTRANS SUM -1. 0.0 1
20595301 0.0 42.0327 HTRNR 006000100
20595302 42.0327 HTRNR 006000200
20595303 42.0327 HTRNR 006000300
20595304 8.7237 HTRNR 006000400
20595305 8.7237 HTRNR 006000500
20595306 42.0327 HTRNR 006000600
20595307 42.0327 HTRNR 006000700
20595308 42.0327 HTRNR 006000800

* STEAM GENERATOR BOILING SECTION

5170000 BILSCT PIPE
5170001 3
5170101 0.363105 3
5170201 0.0 2
5170301 0.7102 3
5170401 0.0 3
5170601 90.0 3
5170701 0.7102 3
5170801 4.E-5 0.020 3
5170901 0.0 0.0 1
5170902 0.0 0.0 2
5171001 00 3
5171101 0000 2
5171300 0

5370000 BILSCT PIPE
5370001 3
5370101 0.363105 3
5370201 0.0 2
5370301 0.7102 3
5370401 0.0 3
5370601 90.0 3
5370701 0.7102 3
5370801 4.E-5 0.020 3
5370901 0.0 0.0 1
5370902 0.0 0.0 2
5371001 00 3
5371101 0000 2
5371300 0

* STEAM GENERATOR RISER

5190000 RISER PIPE
5190001 2
5190101 0.72531 1
5190102 0.27871 2
5190201 0.0 1
5190301 0.7102 1
5190302 0.718 2
5190401 0.0 2
5190601 90.0 1
5190602 90.0 2
5190701 0.518 1
5190702 0.718 2
5190801 4.E-5 0.5957 1
5190802 4.E-5 0.0 2
5190901 0.0 0.0 1
5191001 00 2
5191101 0000 1
5191300 0

5160000 DNBBOIL VALVE
5160101 515010000 517000000 .116 1. 1. 0100
5160201 1 65.35 0.0 0.0
5160300 SRWLV
5160301 216
5360000 DNBBOIL VALVE
5360101 516010000 537000000 .116 1. 1. 0100
5360201 1 65.35 0.0 0.0
5360300 SRWLV
5360301 216

* SG DOWNCOMER TO BOILING SECTION, VALVE FOR RECIRCULATION RATIO

5171201 2 5.59162E6 .044 0.0 0.0 0.0 1
5171202 2 5.58571E6 .095 0.0 0.0 0.0 2
5171203 2 5.57814E6 .164 0.0 0.0 0.0 3
5191201 2 5.57236E6 .189 0.0 0.0 0.0 1
5371201 2 5.59162E6 .000 0.0 0.0 0.0 1
5371202 2 5.58571E6 .044 0.0 0.0 0.0 1
5371203 2 5.57814E6 .095 0.0 0.0 0.0 3
5191202 2 5.57141E6 .194 0.0 0.0 0.0 2
5171301 0.403 0.822 0.0 1
5171302 0.605 1.257 0.0 2
5180201 0 2.3741 4.1876 0.0
5191301 3.050 4.162 0.0 1
5371301 0.403 0.822 0.0 1
5371302 0.605 1.257 0.0 2
5280201 0 2.3741 4.1876 0.0

* SG BOILING SECTION TO RISER

5180000 BOILRSR SGNLJUN
5180101 517010000 519000000 0.0 0.0 0000
5280000 BOILRSR SGNLJUN
5280101 537010000 519000000 0.0 0.0 0000

* STEAM GENERATOR TUBES

10060000 8 6 2 1 0.0051054
10060100 0 1
10060101 5 0.006346984
10060201 6 5
10060301 0.0 5
10060401 550.0 6
10060601 517010000 0 1 1 1310.32 1
10060602 517020000 0 1 1 1310.32 2
10060603 517030000 0 1 1 1310.32 3
10060604 519010000 0 1 1 271.95 4
10060605 519010000 0 1 1 271.95 5
10060606 537030000 0 1 1 1310.32 6
10060607 537020000 0 1 1 1310.32 7
10060608 537010000 0 1 1 1310.32 8
10060501 115040000 0 1 1 1310.32 1
10060502 115050000 0 1 1 1310.32 2
10060503 115060000 0 1 1 1310.32 3

10060504 115060000 0 1 1 271.95 4
10060505 115070000 0 1 1 271.95 5
10060506 115070000 0 1 1 1310.32 6
10060507 115080000 0 1 1 1310.32 7
10060508 115090000 0 1 1 1310.32 8
10060701 0 0 0 0 0
10060801 0 0 0 0 0
10060901 0 0 0 0 0

5171301 0.403 0.822 0.0 1
5171302 0.605 1.257 0.0 2
5180201 0 2.3741 4.1876 0.0
5191301 3.050 4.162 0.0 1
5371301 0.403 0.822 0.0 1
5371302 0.605 1.257 0.0 2
5280201 0 2.3741 4.1876 0.0

* SS CONTROL FOR VALVE 516, RECIRCULATION RATIO = 4.7

20521400 ERR516 SUM 1. 0.0 0
20521401 0. 1. MFLOWJ 516000000
20521402 1. 1. MFLOWJ 536000000
20521403 -4.7 MFLOWJ 560000000
20521600 V516 INTEGRAL -.01 .187 0 3 .01 .99
20521601 CNTRLVAR 215

* FEED WATER VALVE

5600000 FWLV TMDPJUN
5600101 545000000 510000000 0.05
5600200 1 513
5600201 -1. 27.80 0.0 0.0
5600202 0.0 27.80 0.0 0.0
5600203 .7 0.0 0.0 0.0
5600208 3000. 0.0 0.0 0.0

* SS CONTROL FOR FEED WATER ENTHALPHY

20560100 SPRDERR SUM 1.0 0.0 0
20560101 0. -1. MFLOWJ 560000000
20560102 .914014 VAPGEN 500010000
20560103 .914014 VAPGEN 505010000
20560104 .389795 VAPGEN 510010000
20560105 .164951 VAPGEN 515010000
20560106 .164951 VAPGEN 515020000
20560107 .164951 VAPGEN 515030000
20560108 .257877 VAPGEN 517010000
20560109 .257877 VAPGEN 517020000
20560110 .257877 VAPGEN 517030000
20560111 .515823 VAPGEN 519010000
20560112 .200114 VAPGEN 519020000

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20560113      .200114  VAPGEN  520010000
20560114      .685800  VAPGEN  525010000
20560115      .163678  VAPGEN  526010000
20560116      .608844  VAPGEN  530010000
20560117      .257877  VAPGEN  537010000
20560118      .257877  VAPGEN  537020000
20560119      .257877  VAPGEN  537030000
*
20560600  FDWENTH  INTEGRAL  .05  .980E6  0  3  .880E6  1.10E6
20560601  CNTRLVAR  605
*
* TOTAL SG DOWNCOMER MASS FLOW
20594800  SGDCFLW  SUM      1.0      0.0      0
20594801  0.      1.      MFLOWJ  516000000
20594802  1.      1.      MFLOWJ  536000000
*
* END OF FILE
```

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*** LFCR3 ***
RESTART OF LOFT CALCULATION L3-6 FROM SS RUN
*
* LOG1 RESTART
100 RESTART TRANSNT
101 RUN
103 0
105 100. 120.
0000201 280. 1.0E-5 .20 00001 25 4000 4000
*
*****
* PRIMARY COOLANT PUMP 1 TRIP=511
*
1350000 PCP1 PUMP
1350101 0.0366 0.0 0.099 0.0 90.0 0.319
1350102 0
1350108 130010000 0.0 0.0 0.0 0100
1350109 140000000 0.0 0.05 0.05 0100
1350301 0 0 0 -1 -1 511 0
1350302 369.0 0.911 0.3155 96.0 500.6 1.431
1350303 613.6 0.0 207.4 0.004 19.698 0.0
1350308 .212465 0.0 -25. 29.5 6.28
1350310 0.0 0.0 0.0
*
*****
* SINGLE PHASE HEAD CURVES
*
* HEAD CURVE NO. 1
*
1351100 1 1
1351101 0.000000E+00 1.403600E+00
1351102 1.906100E-01 1.363600E+00
1351103 3.896300E-01 1.318600E+00
1351104 5.939600E-01 1.232800E+00
1351105 7.902000E-01 1.133600E+00
1351106 1.000000E+00 1.000000E+00
*
*****
* HEAD CURVE NO. 2
*
1351200 1 2
1351201 0.000000E+00 -6.700000E-01
1351202 2.000000E-01 -5.000000E-01
1351203 4.000000E-01 -2.600000E-01
1351204 5.755400E-01 0.000000E+00
1351205 7.443200E-01 2.583000E-01
1351206 7.734800E-01 3.778000E-01
1351207 8.631300E-01 6.328000E-01
1351208 1.000000E+00 1.000000E+00
*
*****
* HEAD CURVE NO. 3
*
1351300 1 3
1351301 -1.000000E+00 2.472700E+00
1351302 -8.057400E-01 2.047400E+00
1351303 -6.069000E-01 1.831000E+00
1351304 -4.068300E-01 1.624000E+00
1351305 -2.001710E-01 1.470500E+00
1351306 0.000000E+00 1.403600E+00
*
*****
* HEAD CURVE NO. 4
*

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```

1351400 1 4
1351401 -1.000000E+00 2.472700E+00
1351402 -8.223700E-01 1.996800E+00
1351403 -6.333200E-01 1.689700E+00
1351404 -4.553400E-01 1.327900E+00
1351405 -2.710900E-01 1.184900E+00
1351406 -1.771600E-01 1.060500E+00
1351407 -9.073000E-02 1.015600E+00
1351408 0.000000E+00 9.342790E-01
*
*****
* HEAD CURVE NO. 5
*
1351500 1 5
1351501 0.000000E+00 2.500000E-01
1351502 2.000000E-01 2.800000E-01
1351503 4.000000E-01 3.400000E-01
1351504 4.118000E-01 2.768000E-01
1351505 5.976300E-01 4.584000E-01
1351506 7.934670E-01 6.992000E-01
1351507 1.000000E+00 1.000000E+00
*
*****
* HEAD CURVE NO. 6
*
1351600 1 6
1351601 0.000000E+00 9.342790E-01
1351602 9.109900E-02 9.229000E-01
1351603 1.652900E-01 9.680000E-01
1351604 2.717620E-01 8.750000E-01
1351605 4.558720E-01 8.433000E-01
1351606 5.744060E-01 8.355000E-01
1351607 7.405760E-01 8.466000E-01
1351608 7.666190E-01 8.469000E-01
1351609 8.714710E-01 8.838000E-01
1351610 1.000000E+00 1.000000E+00
*
*****
* HEAD CURVE NO. 7
*
1351700 1 7
1351701 -1.000000E+00 -1.000000E+00
1351702 -8.000000E-01 -6.300000E-01
1351703 -6.000000E-01 -3.000000E-01
1351704 -4.000000E-01 -5.000000E-02
1351705 -2.000000E-01 1.500000E-01
1351706 0.000000E+00 2.500000E-01
*
*****
* HEAD CURVE NO. 8
*
1351800 1 8
1351801 -1.000000E+00 -1.000000E+00
1351802 -8.000000E-01 -9.700000E-01
1351803 -6.000000E-01 -9.500000E-01
1351804 -4.000000E-01 -8.800000E-01
1351805 -2.000000E-01 -8.000000E-01
1351806 0.000000E+00 -6.700000E-01
*
*****
* SINGLE PHASE TORQUE DATA
*
*****
* TORQUE CURVE NO. 1
*
1351900 2 1
1351901 0.000000E+00 6.032000E-01
1351902 1.930000E-01 6.325000E-01
1351903 3.930000E-01 7.369000E-01

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1351904 5.955200E-01 8.331000E-01
1351905 7.978200E-01 9.229000E-01
1351906 1.000000E+00 1.000000E+00
*
*****
* TORQUE CURVE NO. 2
*
1352000 2 2
1352001 0.000000E+00 -6.700000E-01
1352002 4.000000E-01 -2.600000E-01
1352003 5.000000E-01 1.500000E-01
1352004 7.372500E-01 5.265860E-01
1352005 7.680490E-01 6.065940E-01
1352006 8.672300E-01 7.436600E-01
1352007 1.000000E+00 1.000000E+00
*
*****
* TORQUE CURVE NO. 3
*
1352100 2 3
1352101 -1.000000E+00 1.984300E+00
1352102 -8.009600E-01 1.394000E+00
1352103 -6.063800E-01 1.097500E+00
1352104 -4.068500E-01 8.220000E-01
1352105 -1.992800E-01 6.548000E-01
1352106 0.000000E+00 6.032000E-01
*
*****
* TORQUE CURVE NO. 4
*
1352200 2 4
1352201 -1.000000E+00 1.984300E+00
1352202 -8.223400E-01 1.830800E+00
1352203 -6.337100E-01 1.682400E+00
1352204 -4.585300E-01 1.557000E+00
1352205 -2.670230E-01 1.436200E+00
1352206 -1.761070E-01 1.387900E+00
1352207 -8.931000E-02 1.348100E+00
1352208 0.000000E+00 1.233610E+00
*
*****
* TORQUE CURVE NO. 5
*
1352300 2 5
1352301 0.000000E+00 -4.500000E-01
1352302 4.000000E-01 -2.500000E-01
1352303 5.000000E-01 0.000000E+00
1352304 1.000000E+00 3.569000E-01
*
*****
* TORQUE CURVE NO. 6
*
1352400 2 6
1352401 0.000000E+00 1.233610E+00
1352402 9.064300E-02 1.196500E+00
1352403 1.885690E-01 1.109600E+00
1352404 2.734700E-01 1.041600E+00
1352405 4.586690E-01 8.958000E-01
1352406 5.744800E-01 7.807000E-01
1352407 7.981600E-01 6.134000E-01
1352408 7.685200E-01 5.849000E-01
1352409 8.700570E-01 4.877000E-01
1352410 1.000000E+00 3.569000E-01
*
*****
* TORQUE CURVE NO. 7
*
1352500 2 7
1352501 -1.000000E+00 -1.000000E+00
1352502 -3.000000E-01 -9.000000E-01
1352503 -1.000000E-01 -5.000000E-01

```

1352504 0.00000E+00 -4.50000E-01
 * FOR TORQUE CURVE NO. 8
 *
 1352600 2 8
 1352601 -1.00000E+00 -1.00000E+00
 1352602 -2.50000E-01 -9.00000E-01
 1352603 -8.00000E-02 -8.00000E-01
 1352604 0.00000E+00 -6.70000E-01

* TWO - PHASE MULTIPLIER DATA
 *
 * HEAD CURVE

1353000 0 0.00000E+00 0.00000E+00
 1353001 0.00000E+00 7.00000E-02
 1353002 1.00000E-01 1.80000E-01
 1353003 2.00000E-01 3.40000E-01
 1353004 3.00000E-01 5.00000E-01
 1353005 3.50000E-01 6.00000E-01
 1353006 3.70000E-01 7.00000E-01
 1353007 4.00000E-01 7.20000E-01
 1353008 5.00000E-01 7.50000E-01
 1353009 6.00000E-01 7.70000E-01
 1353010 7.00000E-01 7.70000E-01
 1353011 8.00000E-01 7.40000E-01
 1353012 9.00000E-01 6.10000E-01
 1353013 9.50000E-01 4.00000E-01
 1353014 1.00000E+00 0.00000E+00

* TORQUE CURVE

1353100 0 0.00000E+00 0.00000E+00
 1353101 0.00000E+00 0.00000E+00
 1353102 1.00000E-01 1.00000E-01
 1353103 2.00000E-01 3.00000E-01
 1353104 3.00000E-01 5.00000E-01
 1353105 3.50000E-01 7.50000E-01
 1353106 4.00000E-01 7.50000E-01
 1353107 5.00000E-01 7.50000E-01
 1353108 6.00000E-01 7.50000E-01
 1353109 7.00000E-01 7.50000E-01
 1353110 8.00000E-01 7.50000E-01
 1353111 9.00000E-01 5.00000E-01
 1353112 1.00000E+00 0.00000E+00

* PUMP 2-PHASE DIFFERENCE DATA

* HEAD CURVE NO. 1

1354100 1 1
 1354101 0.00000E+00 1.40360E+00
 1354102 1.90610E-01 1.36360E+00
 1354103 3.89630E-01 1.31860E+00
 1354104 5.93950E-01 1.23280E+00
 1354105 7.90200E-01 1.13360E+00
 1354106 1.00000E+00 1.00000E+00

* HEAD CURVE NO. 2

1354200 1 2

1354201 0.00000E+00 -5.70000E-01
 1354202 2.00000E-01 -5.00000E-01
 1354203 4.00000E-01 -2.50000E-01
 1354204 5.75400E-01 0.00000E+00
 1354205 7.44320E-01 2.58300E-01
 1354206 7.73480E-01 3.77800E-01
 1354207 8.63130E-01 6.32600E-01
 1354208 1.00000E+00 1.00000E+00

* HEAD CURVE NO. 3

1354300 1 3
 1354301 -1.00000E+00 -1.16000E+00
 1354302 -9.00000E-01 -1.24000E+00
 1354303 -8.00000E-01 -1.77000E+00
 1354304 -7.00000E-01 -2.36000E+00
 1354305 -6.00000E-01 -2.79000E+00
 1354306 -5.00000E-01 -2.91000E+00
 1354307 -4.00000E-01 -2.67000E+00
 1354308 -2.80000E-01 -1.69000E+00
 1354309 -1.00000E-01 -5.00000E-01
 1354310 0.00000E+00 0.00000E+00

* HEAD CURVE NO. 4

1354400 1 4
 1354401 -1.00000E+00 -1.16000E+00
 1354402 -9.00000E-01 -7.80000E-01
 1354403 -8.00000E-01 -5.00000E-01
 1354404 -7.00000E-01 -3.10000E-01
 1354405 -6.00000E-01 -1.70000E-01
 1354406 -5.00000E-01 -8.00000E-02
 1354407 -3.80000E-01 0.00000E+00
 1354408 -2.00000E-01 5.00000E-02
 1354409 -1.00000E-01 8.00000E-02
 1354410 0.00000E+00 1.10000E-01

* HEAD CURVE NO. 5

1354500 1 5
 1354501 0.00000E+00 0.00000E+00
 1354502 2.00000E-01 -3.40000E-01
 1354503 4.00000E-01 -6.50000E-01
 1354504 6.00000E-01 -9.30000E-01
 1354505 8.00000E-01 -1.19000E+00
 1354506 1.00000E+00 -1.47000E+00

* HEAD CURVE NO. 6

1354600 1 6
 1354601 0.00000E+00 1.10000E-01
 1354602 1.00000E-01 1.30000E-01
 1354603 2.50000E-01 1.50000E-01
 1354604 4.00000E-01 1.30000E-01
 1354605 5.00000E-01 7.00000E-02
 1354606 6.00000E-01 -4.00000E-02
 1354607 7.00000E-01 -2.30000E-01
 1354608 8.00000E-01 -5.10000E-01
 1354609 9.00000E-01 -9.10000E-01
 1354610 1.00000E+00 -1.47000E+00

* HEAD CURVE NO. 7

1354700 1 7

1354701 -1.00000E+00 0.00000E+00

1354702 0.00000E+00 0.00000E+00

* HEAD CURVE NO. 8

1354800 1 8
 1354801 -1.00000E+00 0.00000E+00
 1354802 0.00000E+00 0.00000E+00

* TORQUE CURVE NO. 1

1354900 2 1
 1354901 0.00000E+00 6.03700E-01
 1354902 1.93000E-01 6.32500E-01
 1354903 3.83000E-01 7.36900E-01
 1354904 5.85200E-01 8.33100E-01
 1354905 7.87200E-01 9.22900E-01
 1354906 1.00000E+00 1.00000E+00

* TORQUE CURVE NO. 2

1355000 2 2
 1355001 0.00000E+00 -6.70000E-01
 1355002 4.00000E-01 -2.50000E-01
 1355003 8.00000E-01 1.50000E-01
 1355004 7.37250E-01 6.26580E-01
 1355005 7.680490E-01 6.065940E-01
 1355006 8.672300E-01 7.436600E-01
 1355007 1.00000E+00 1.00000E+00

* TORQUE CURVE NO. 3

1355100 2 3
 1355101 -1.00000E+00 1.98430E+00
 1355102 -8.00960E-01 1.39400E+00
 1355103 -6.06380E-01 1.09750E+00
 1355104 -4.06860E-01 8.22000E-01
 1355105 -1.99280E-01 5.64800E-01
 1355106 0.00000E+00 6.03200E-01

* TORQUE CURVE NO. 4

1355200 2 4
 1355201 -1.00000E+00 1.98430E+00
 1355202 -8.22340E-01 1.83080E+00
 1355203 -6.33710E-01 1.68240E+00
 1355204 -4.58530E-01 1.55700E+00
 1355205 -2.670230E-01 1.43620E+00
 1355206 -1.761070E-01 1.38790E+00
 1355207 -8.93100E-02 1.34810E+00
 1355208 0.00000E+00 1.233610E+00

* TORQUE CURVE NO. 5

1355300 2 5
 1355301 0.00000E+00 -4.50000E-01
 1355302 4.00000E-01 -2.50000E-01
 1355303 5.00000E-01 0.00000E+00
 1355304 1.00000E+00 3.56900E-01

* TORQUE CURVE NO. 6

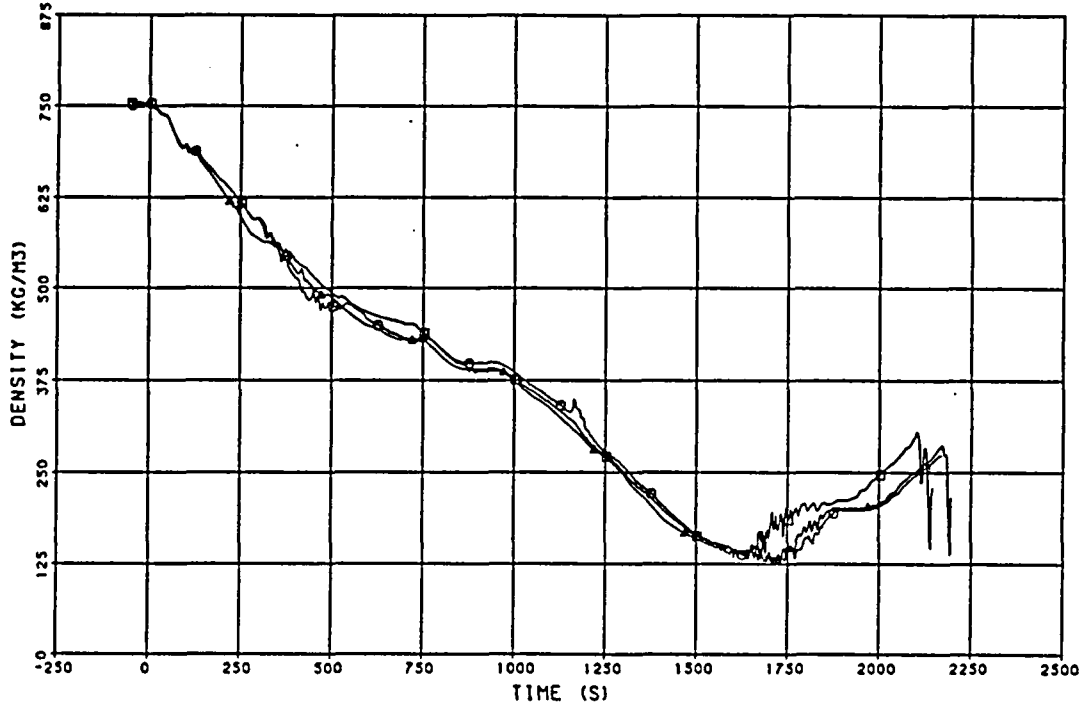
1355400 2 6
 1355401 0.00000E+00 1.233610E+00
 1355402 9.064300E-02 1.19650E+00
 1355403 1.885690E-01 1.10960E+00

```
1355404 2.734700E-01 1.041600E+00
1355405 4.586590E-01 8.958000E-01
1355406 5.744800E-01 7.807000E-01
1355407 7.381600E-01 6.134000E-01
1355408 7.685200E-01 5.849000E-01
1355409 8.700570E-01 4.877000E-01
1355410 1.000000E+00 3.568000E-01
*****
* TORQUE CURVE NO. 7
*
1355500 2 7
1355501 -1.000000E+00 -1.000000E+00
1355502 -3.000000E-01 -9.000000E-01
1355503 -1.000000E-01 -5.000000E-01
1355504 0.000000E+00 -4.500000E-01
*****
* TORQUE CURVE NO. 8
*
1355600 2 8
1355601 -1.000000E+00 -1.000000E+00
1355602 -2.500000E-01 -9.000000E-01
1355603 -8.000000E-02 -8.000000E-01
1355604 0.000000E+00 -6.700000E-01
*
1350200 3 14.8195E6 560.35
1350201 1 241.6 0.0 0.0
1350202 1 241.6 0.0 0.0
. END OF FILE
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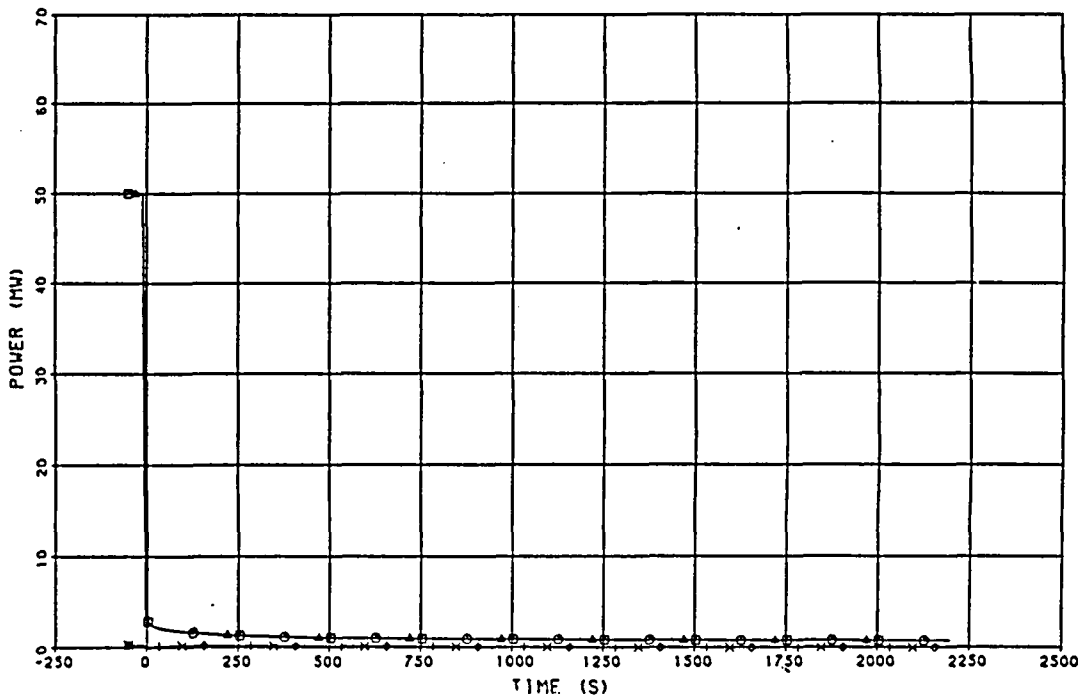
▷○ CORE INLET FLUID DENSITY (CNTRLVAR 901) CASE A
○ CORE INLET FLUID DENSITY (CNTRLVAR 901) CASE B
○ CORE INLET FLUID DENSITY (CNTRLVAR 901) CASE C

Plot B. 1



▷○ REACTOR POWER (RKTPOW 0) CASE A
○ REACTOR POWER (RKTPOW 0) CASE B
○ REACTOR POWER (RKTPOW 0) CASE C
◊x+ PRIM. EXTERNALS HEAT FLOW (CNTRLVAR 982) CASE A
○ PRIM. EXTERNALS HEAT FLOW (CNTRLVAR 982) CASE B
○ PRIM. EXTERNALS HEAT FLOW (CNTRLVAR 982) CASE C

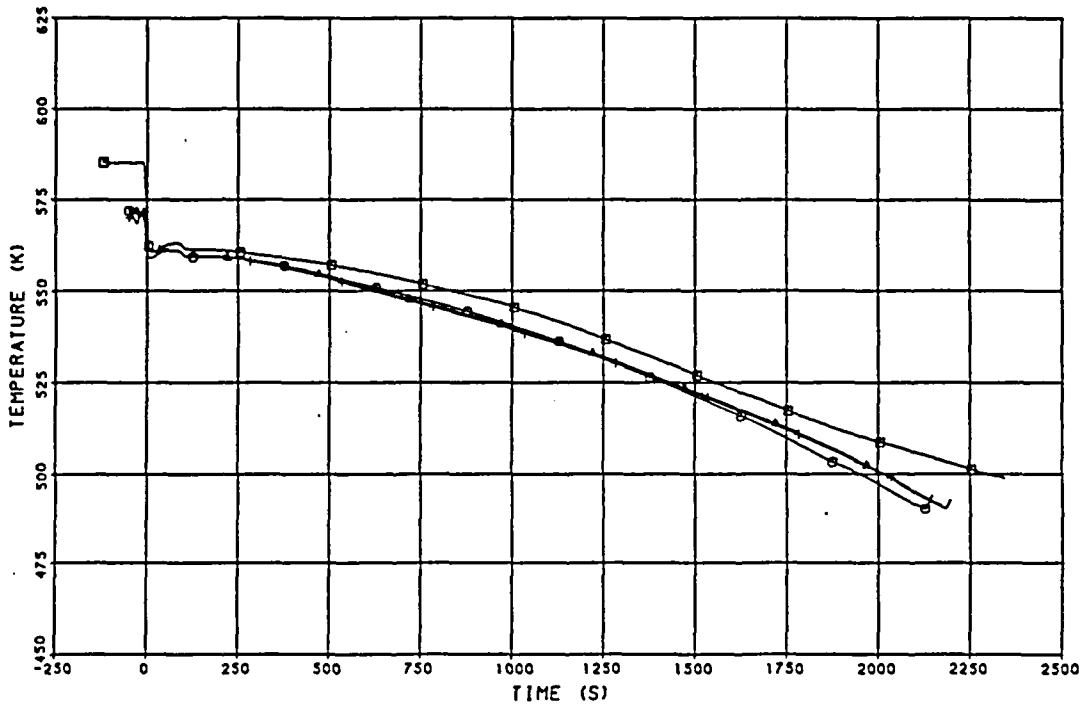
Plot B. 2



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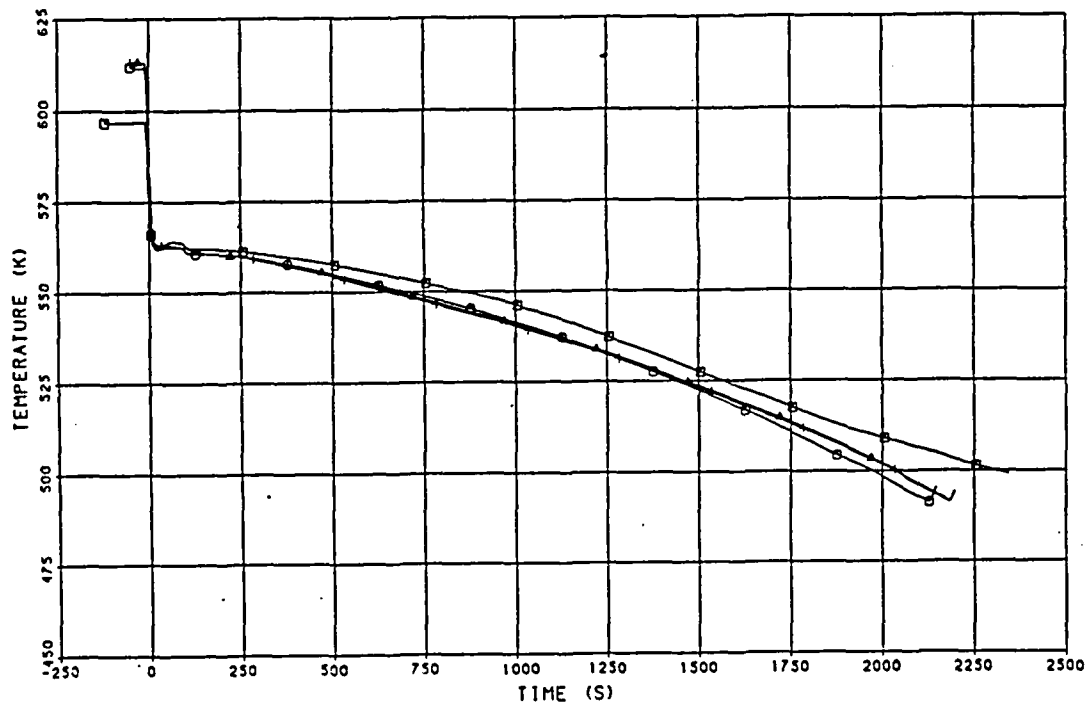
□ CORE CLAD TEMPERATURE VOL. 1 (TE-2014-01) ... 1 EXP.
○ CORE CLAD TEMPERATURE VOL. 1 (CNTRLVAR 903) CASE A
△ CORE CLAD TEMPERATURE VOL. 1 (CNTRLVAR 903) CASE B
+ CORE CLAD TEMPERATURE VOL. 1 (CNTRLVAR 903) CASE C

Plot B. 3



□ CORE CLAD TEMPERATURE VOL. 2 (TE-1F7-01S ... 1 EXP.
○ CORE CLAD TEMPERATURE VOL. 2 (CNTRLVAR 904) CASE A
△ CORE CLAD TEMPERATURE VOL. 2 (CNTRLVAR 904) CASE B
+ CORE CLAD TEMPERATURE VOL. 2 (CNTRLVAR 904) CASE C

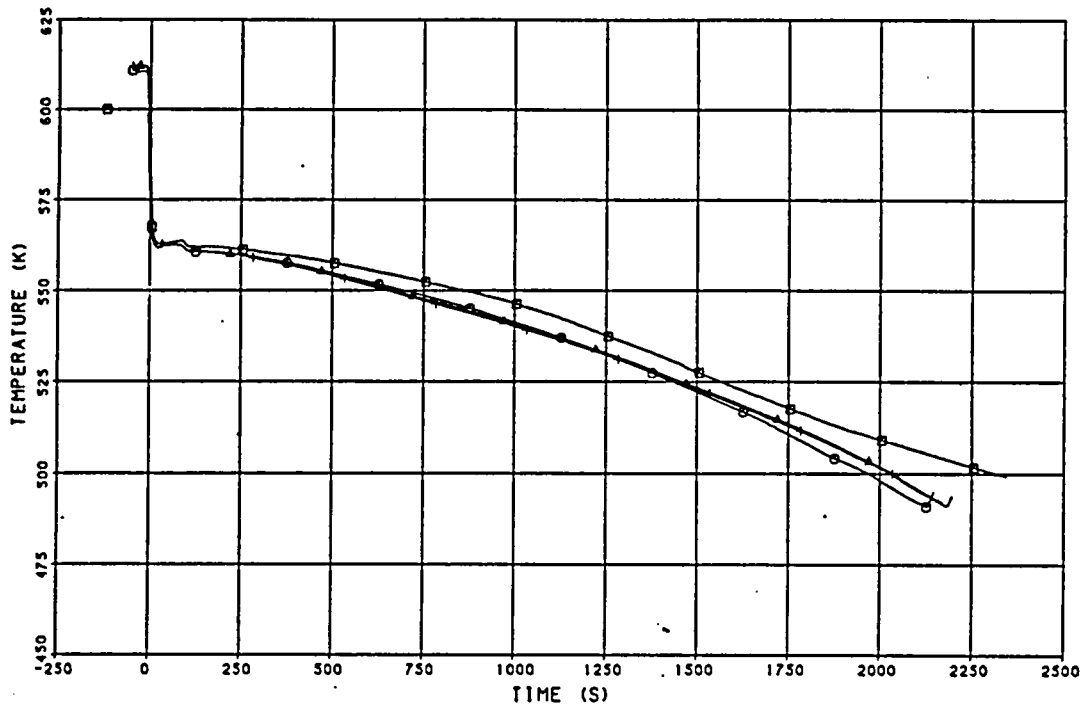
Plot B. 4



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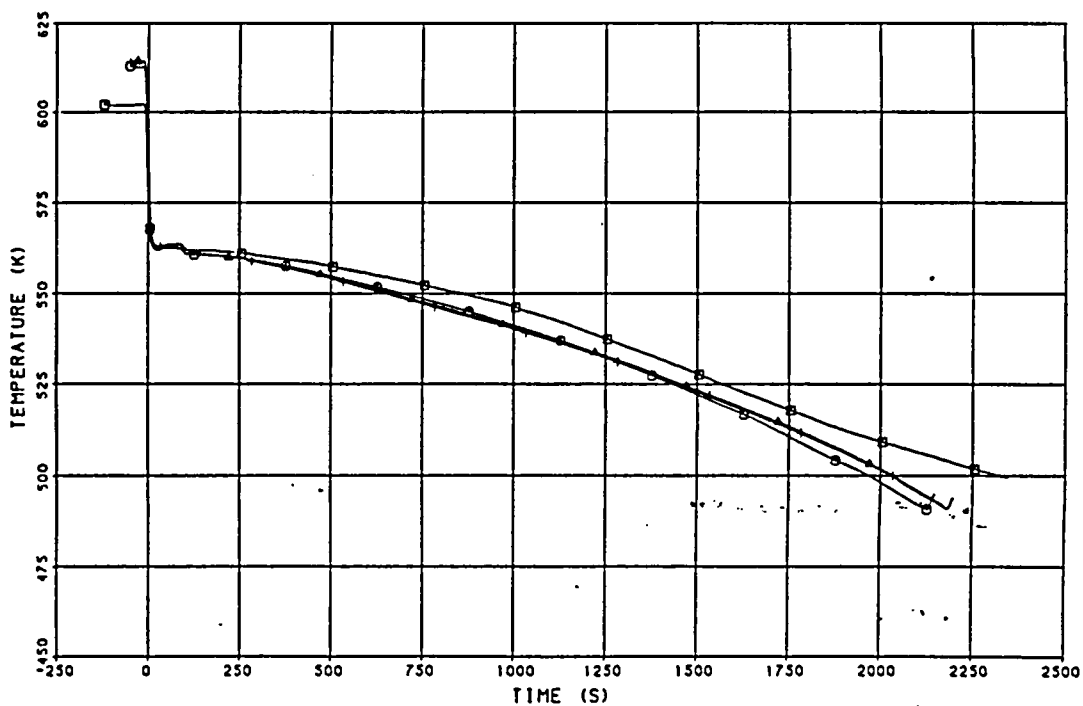
↑ CORE CLAD TEMPERATURE VOL. 3 (TE-177-026 . .) EXP.
CORE CLAD TEMPERATURE VOL. 3 (CNTRLVAR 903) CASE A
CORE CLAD TEMPERATURE VOL. 3 (CNTRLVAR 903) CASE B
CORE CLAD TEMPERATURE VOL. 3 (CNTRLVAR 903) CASE C

Plot B. 5



↑ CORE CLAD TEMPERATURE VOL. 4 (TE-2008-039 . .) EXP.
CORE CLAD TEMPERATURE VOL. 4 (CNTRLVAR 906) CASE A
CORE CLAD TEMPERATURE VOL. 4 (CNTRLVAR 906) CASE B
CORE CLAD TEMPERATURE VOL. 4 (CNTRLVAR 906) CASE C

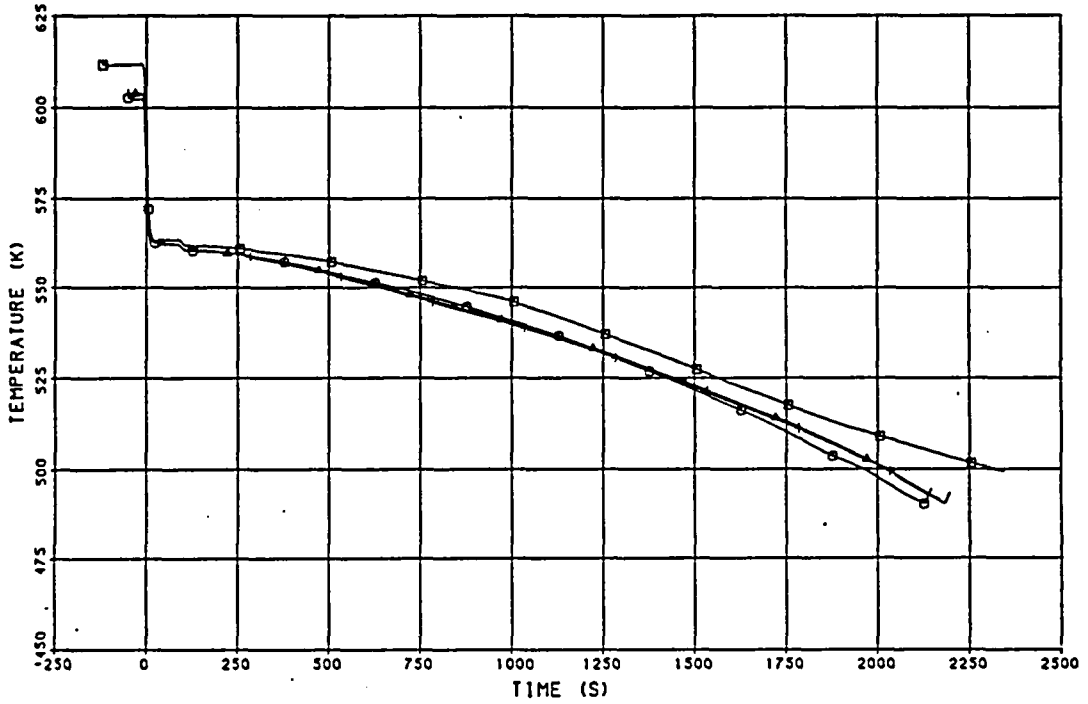
Plot B. 6



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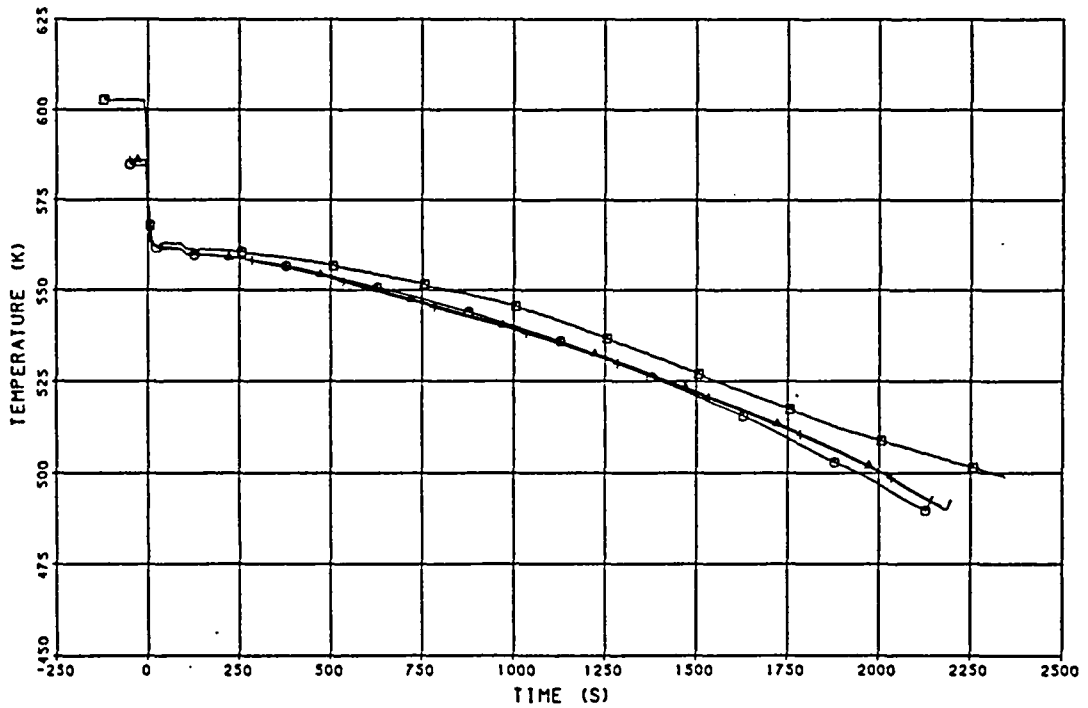
□ CORE CLAD TEMPERATURE VOL. 5 (TE-2014-045 ...) EXP.
+ CORE CLAD TEMPERATURE VOL. 5 (CNTRLVAR 907) CASE A
○ CORE CLAD TEMPERATURE VOL. 5 (CNTRLVAR 907) CASE B
+ CORE CLAD TEMPERATURE VOL. 5 (CNTRLVAR 907) CASE C

Plot B. 7



□ CORE CLAD TEMPERATURE VOL. 6 (TE-3M7-062 ...) EXP.
+ CORE CLAD TEMPERATURE VOL. 6 (CNTRLVAR 908) CASE A
○ CORE CLAD TEMPERATURE VOL. 6 (CNTRLVAR 908) CASE B
+ CORE CLAD TEMPERATURE VOL. 6 (CNTRLVAR 908) CASE C

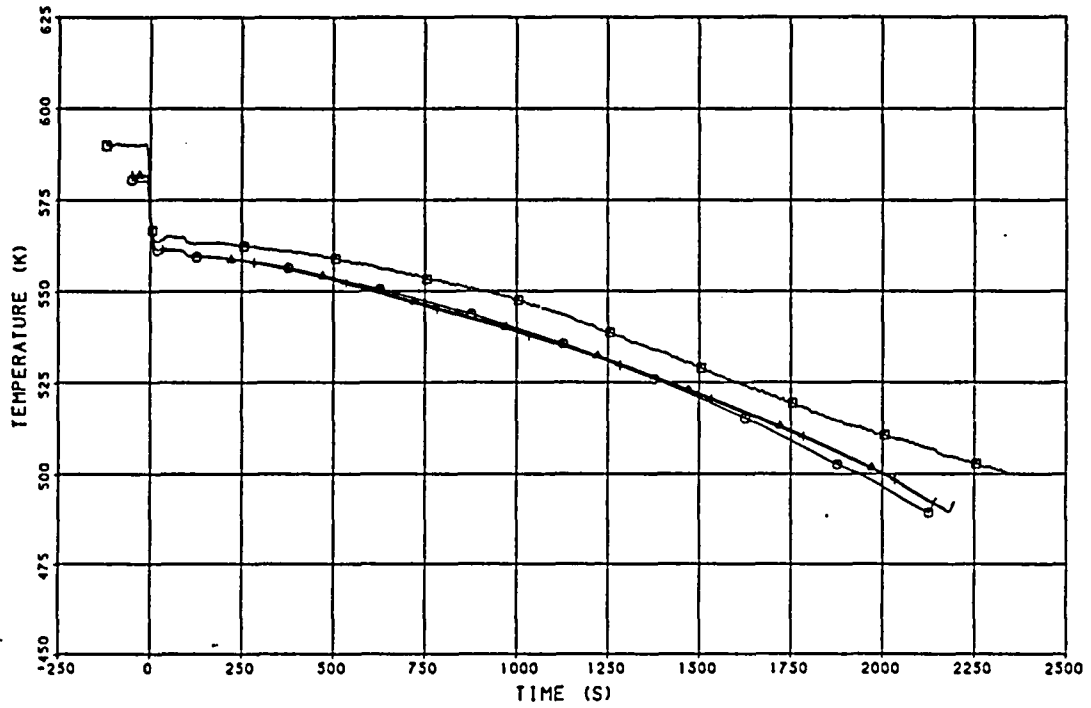
Plot B. 8



1987-11-03

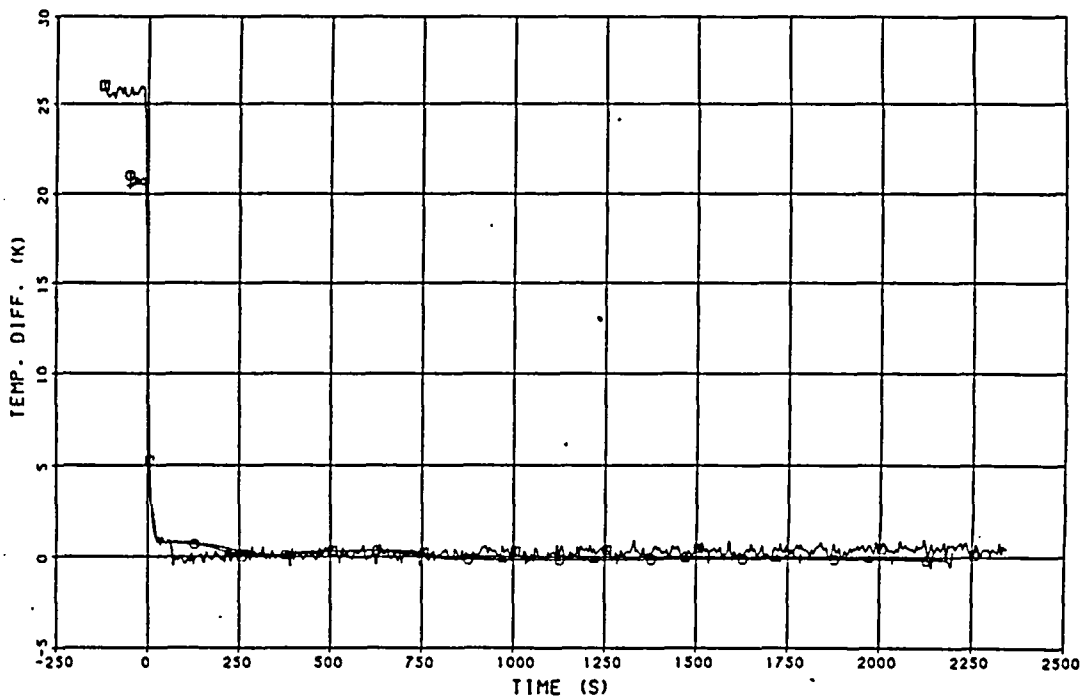
+PQB CORE OUTLET TEMPERATURE (TE-1UP-001 ...) EXP.
CORE OUTLET TEMPERATURE (CNTRLVAR 909) CASE A
CORE OUTLET TEMPERATURE (CNTRLVAR 909) CASE B
CORE OUTLET TEMPERATURE (CNTRLVAR 909) CASE C

Plot B.9



+PQB CORE FLUID TEMPERATURE DIFF. (TE-1UP-001 - TE-1LP-001) EXP.
CORE FLUID TEMPERATURE DIFF. (CNTRLVAR 910) CASE A
CORE FLUID TEMPERATURE DIFF. (CNTRLVAR 910) CASE B
CORE FLUID TEMPERATURE DIFF. (CNTRLVAR 910) CASE C

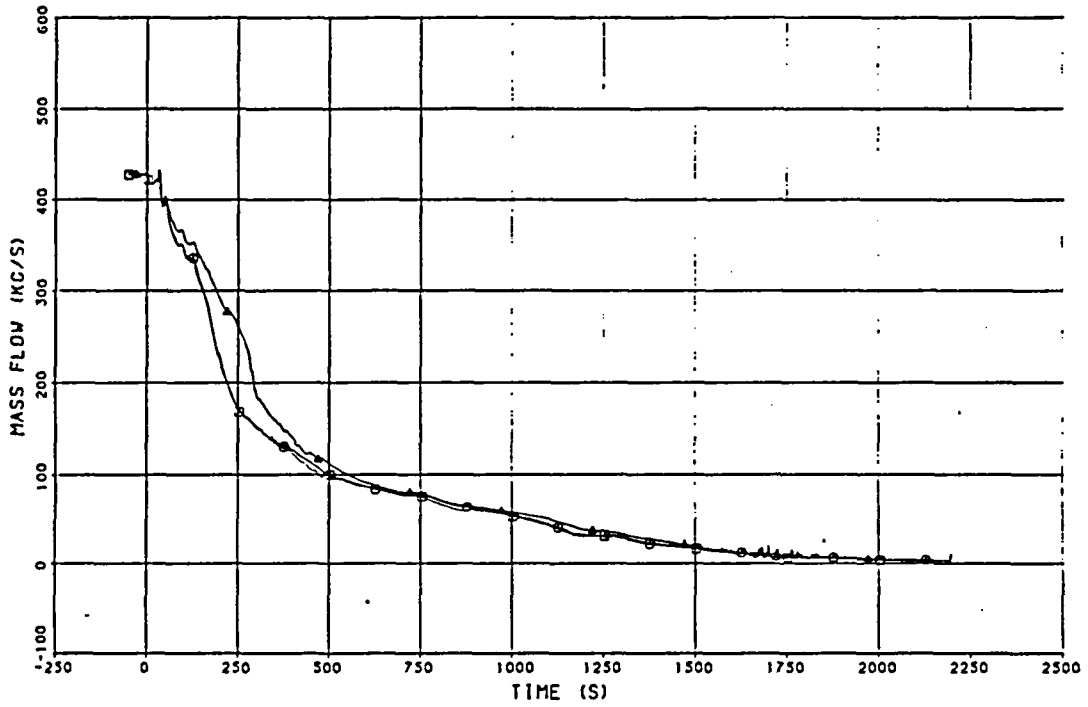
Plot B.10



1987-11-03

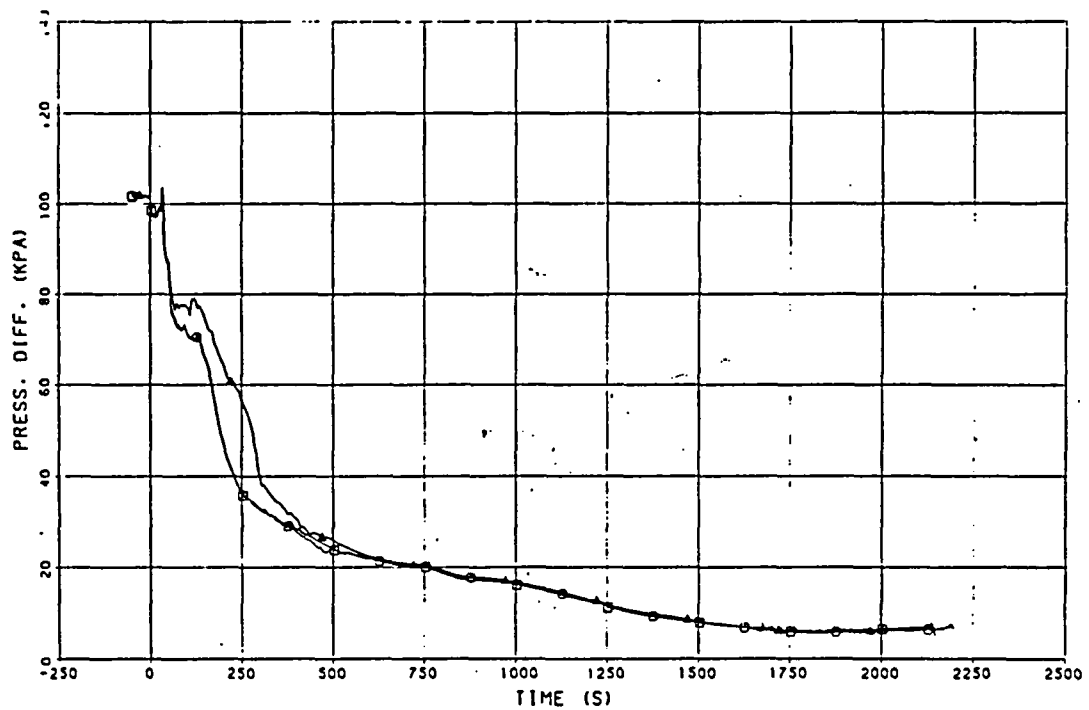
□ CORE INLET MASS FLOW (MFLOWJ 225) CASE A
○ CORE INLET MASS FLOW (MFLOWJ 225) CASE B
▲ CORE INLET MASS FLOW (MFLOWJ 225) CASE C

Plot B.11



□ CORE MASS INVENTORY (CNTRLVAR 912) CASE A
○ CORE MASS INVENTORY (CNTRLVAR 912) CASE B
▲ CORE MASS INVENTORY (CNTRLVAR 912) CASE C

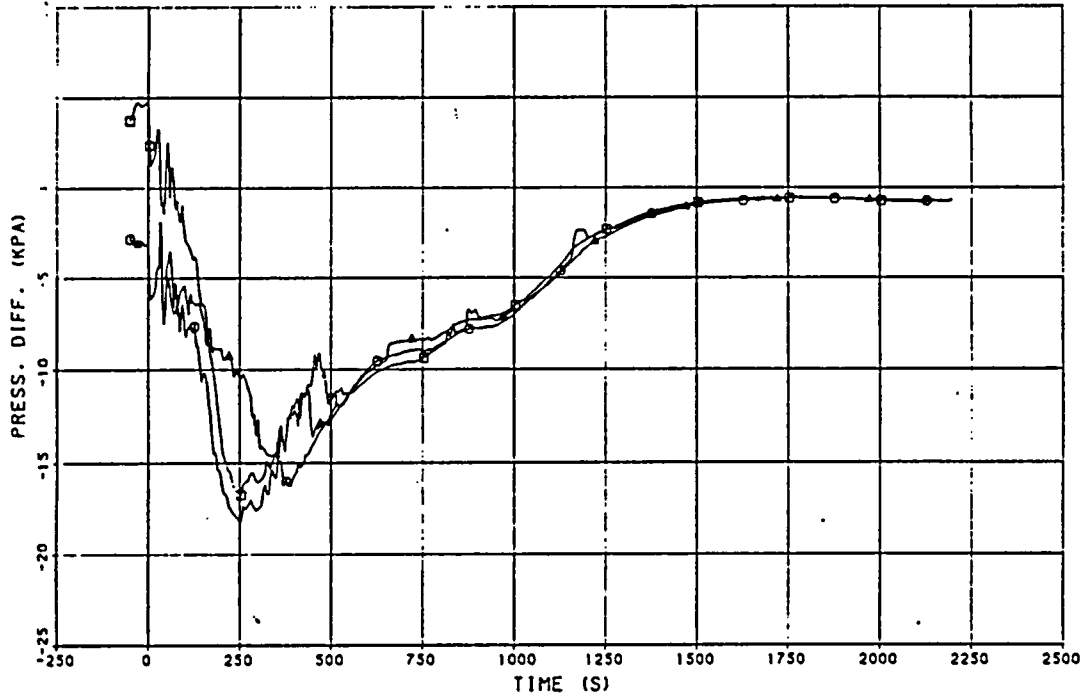
Plot B.12



1987-11-03

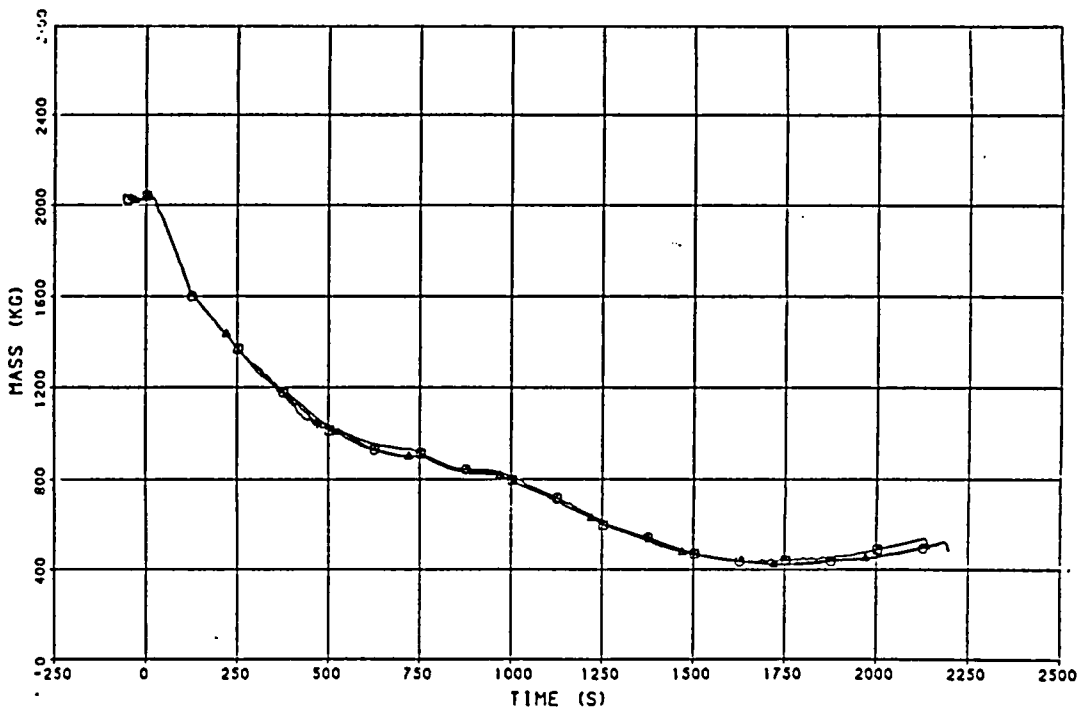
□ DOWNCOMER MASS INVENTORY (CNTRLVAR 913) CASE A
○ DOWNCOMER MASS INVENTORY (CNTRLVAR 913) CASE B
▲ DOWNCOMER MASS INVENTORY (CNTRLVAR 913) CASE C

Plot B.13



□ VESSEL TOTAL MASS INVENTORY (CNTRLVAR 914) CASE A
○ VESSEL TOTAL MASS INVENTORY (CNTRLVAR 914) CASE B
▲ VESSEL TOTAL MASS INVENTORY (CNTRLVAR 914) CASE C

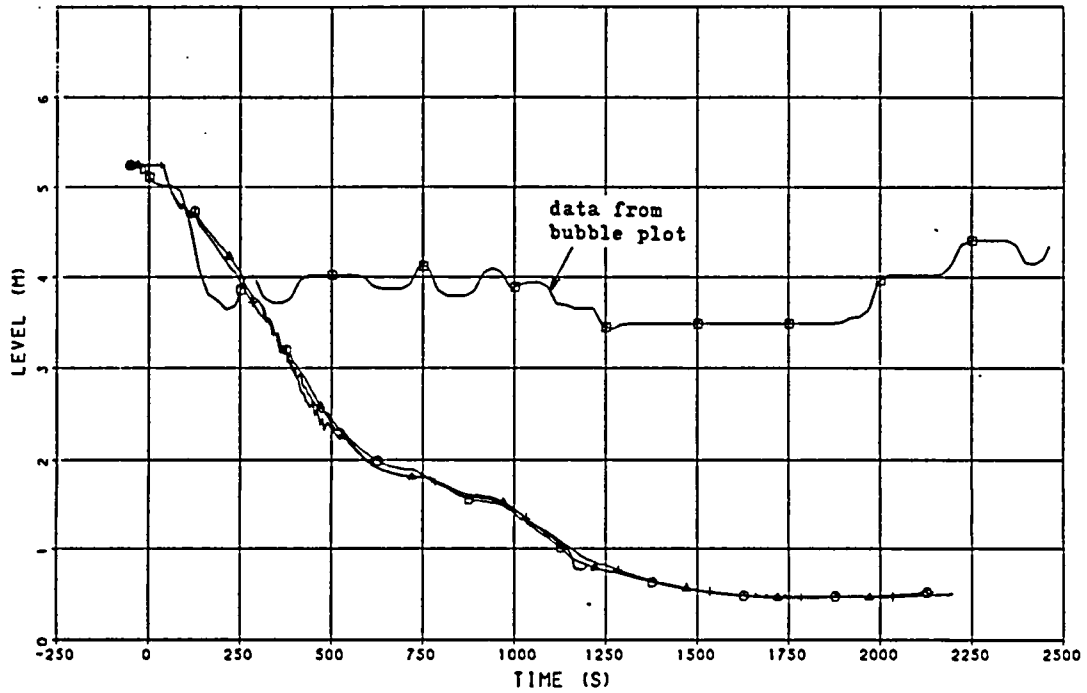
Plot B.14



1987-11-03

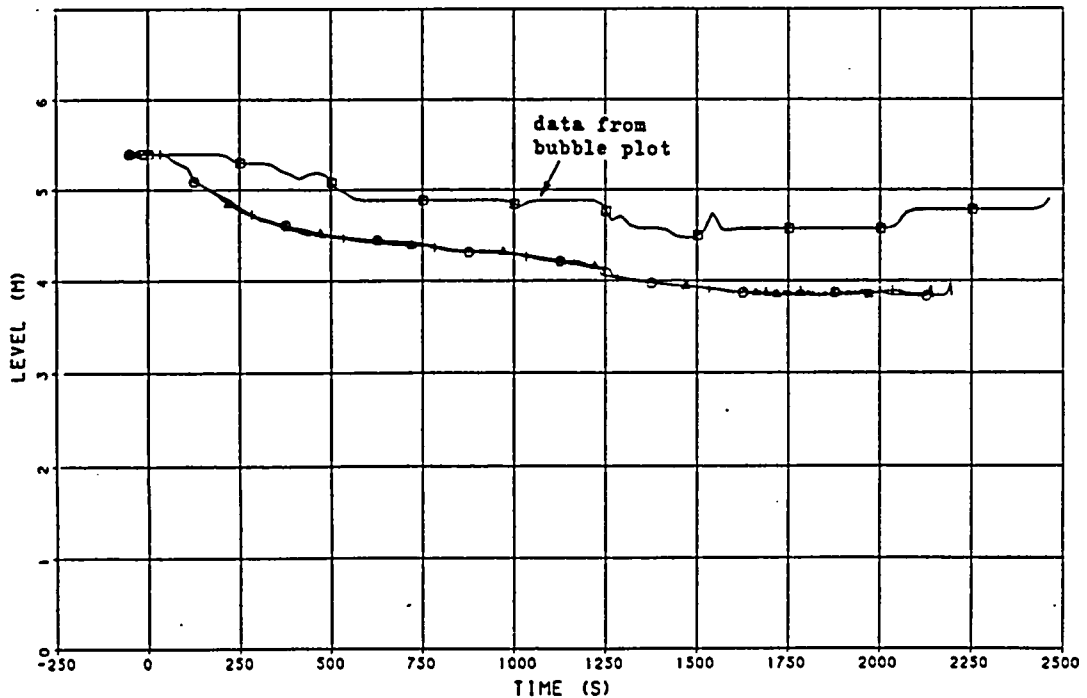
00 DOWNCOMER LIQUID LEVEL (LE-ST-001) EXP.
+ DOWNCOMER LIQUID LEVEL (CNTRLVAR 915) CASE A
+ DOWNCOMER LIQUID LEVEL (CNTRLVAR 915) CASE B
+ DOWNCOMER LIQUID LEVEL (CNTRLVAR 915) CASE C

Plot B.15



00 UPPER PLENUM LIQUID LEVEL (LE-3UP-001) EXP.
+ UPPER PLENUM LIQUID LEVEL (CNTRLVAR 916) CASE A
+ UPPER PLENUM LIQUID LEVEL (CNTRLVAR 916) CASE B
+ UPPER PLENUM LIQUID LEVEL (CNTRLVAR 916) CASE C

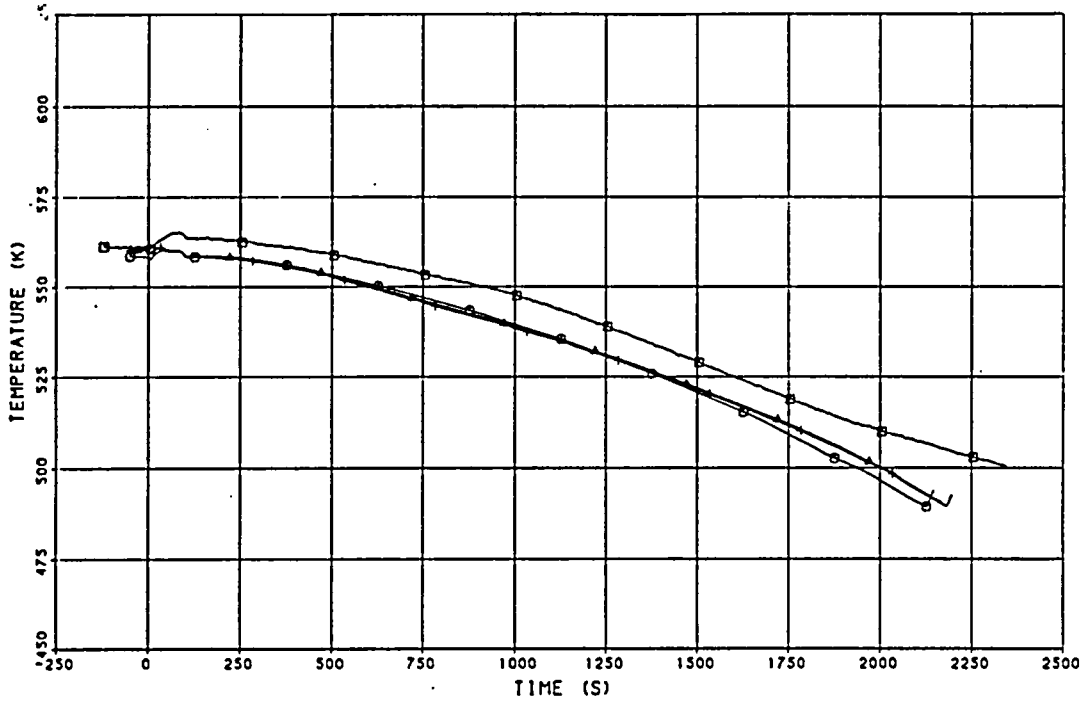
Plot B.16



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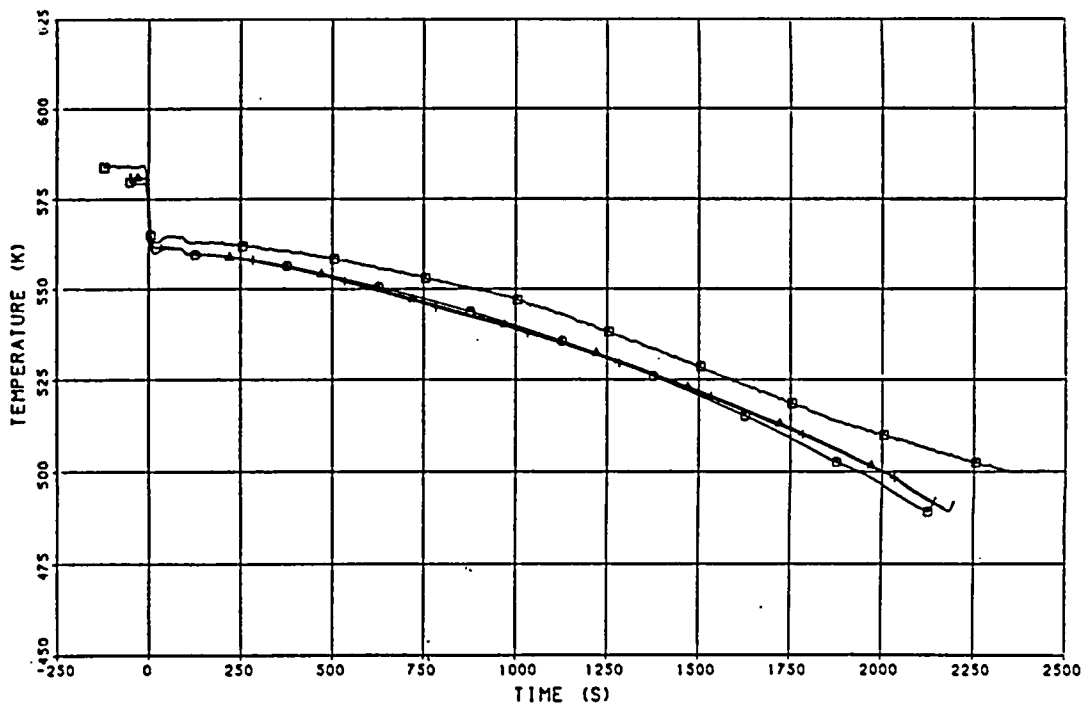
□ DB DOWNCOMER INLET TEMPERATURE (TE-1ST-001 ...) EXP.
○ DOWNCOMER INLET TEMPERATURE (TEMPF 203) CASE A
△ DOWNCOMER INLET TEMPERATURE (TEMPF 203) CASE B
+ DOWNCOMER INLET TEMPERATURE (TEMPF 203) CASE C

Plot B.17



□ DB UPPER PLENUM TEMPERATURE (TE-1UP-001 ...) EXP.
○ UPPER PLENUM TEMPERATURE (TEMPF 240) CASE A
△ UPPER PLENUM TEMPERATURE (TEMPF 240) CASE B
+ UPPER PLENUM TEMPERATURE (TEMPF 240) CASE C

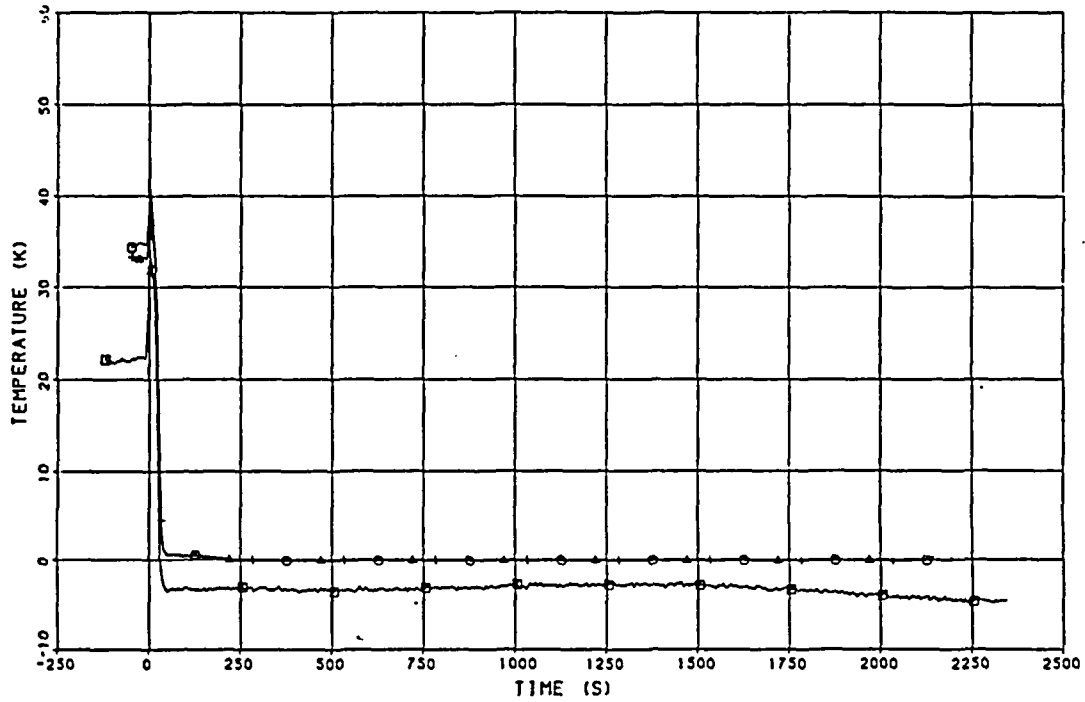
Plot B.18



1987-11-03

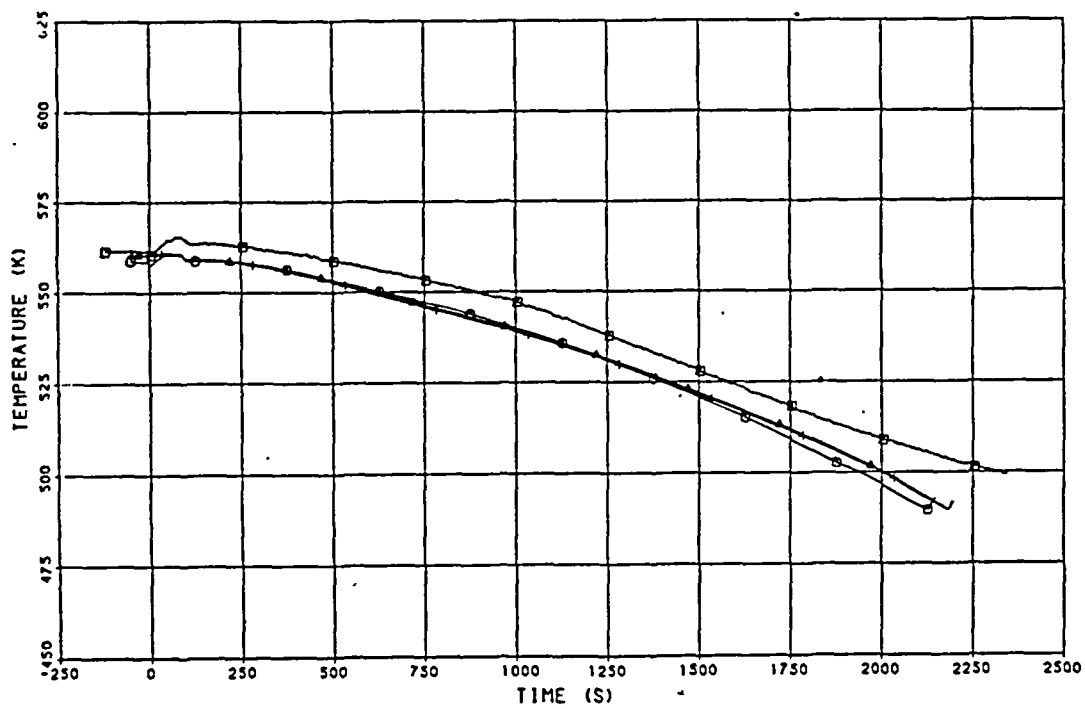
□ □ UPPER PLENUM SUBCOOLING (SC-SUP-102) EXP.
 ▲ □ UPPER PLENUM SUBCOOLING (CNTRLVAR 919) CASE A
 + □ UPPER PLENUM SUBCOOLING (CNTRLVAR 919) CASE B
 + □ UPPER PLENUM SUBCOOLING (CNTRLVAR 919) CASE C

Plot B.19



□ □ LOWER PLENUM TEMPERATURE (TE-1LP-001) EXP.
 ▲ □ LOWER PLENUM TEMPERATURE (TEMPF 225) CASE A
 + □ LOWER PLENUM TEMPERATURE (TEMPF 225) CASE B
 + □ LOWER PLENUM TEMPERATURE (TEMPF 225) CASE C

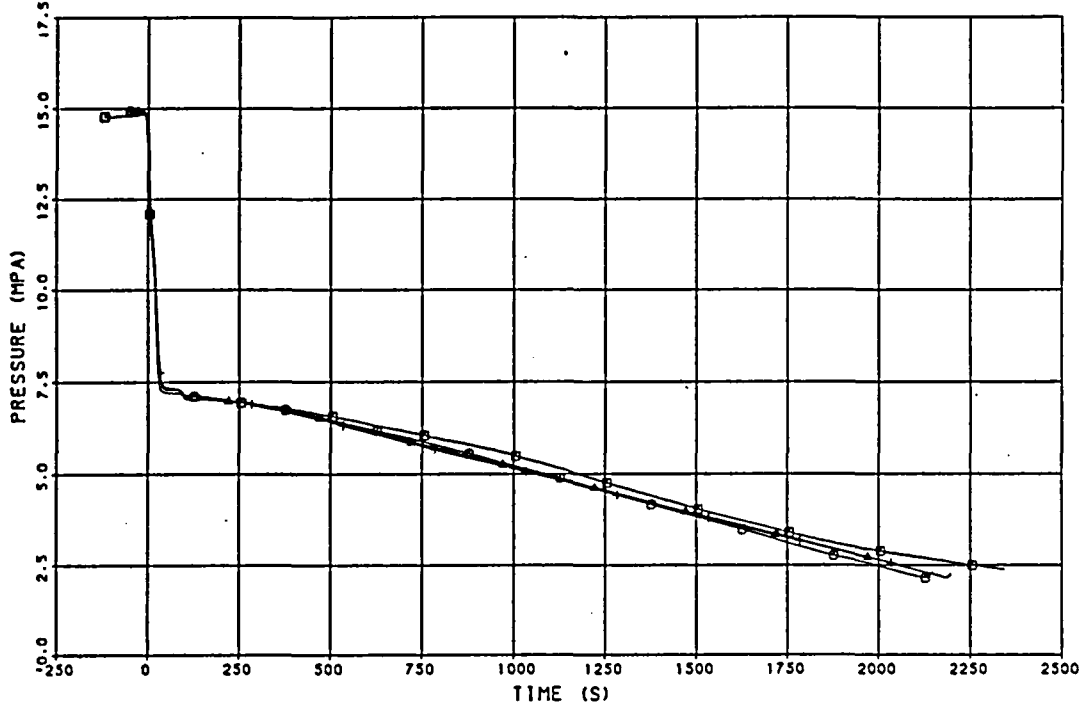
Plot B.20



1987-11-03

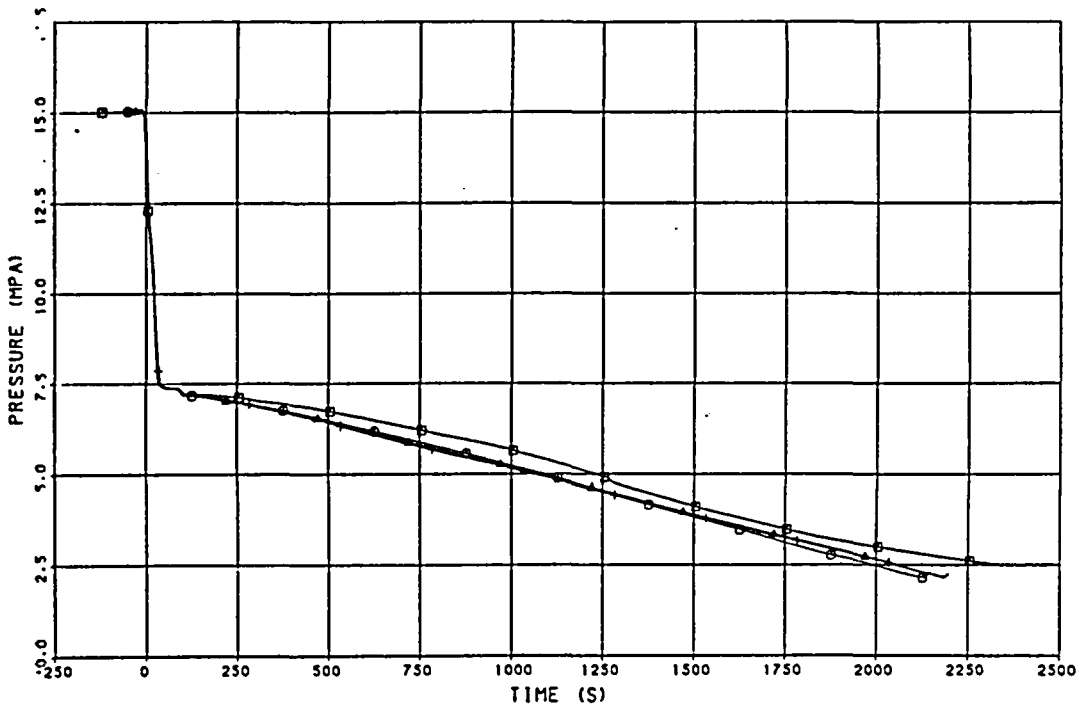
UPPER PLENUM PRESSURE (PE-1UP-001A) EXP.
UPPER PLENUM PRESSURE (P 243) CASE A
UPPER PLENUM PRESSURE (P 243) CASE B
UPPER PLENUM PRESSURE (P 243) CASE C

Plot B.21



LOWER PLENUM PRESSURE (PE-1ST-001A ...) EXP.
LOWER PLENUM PRESSURE (P 225) CASE A
LOWER PLENUM PRESSURE (P 225) CASE B
LOWER PLENUM PRESSURE (P 225) CASE C

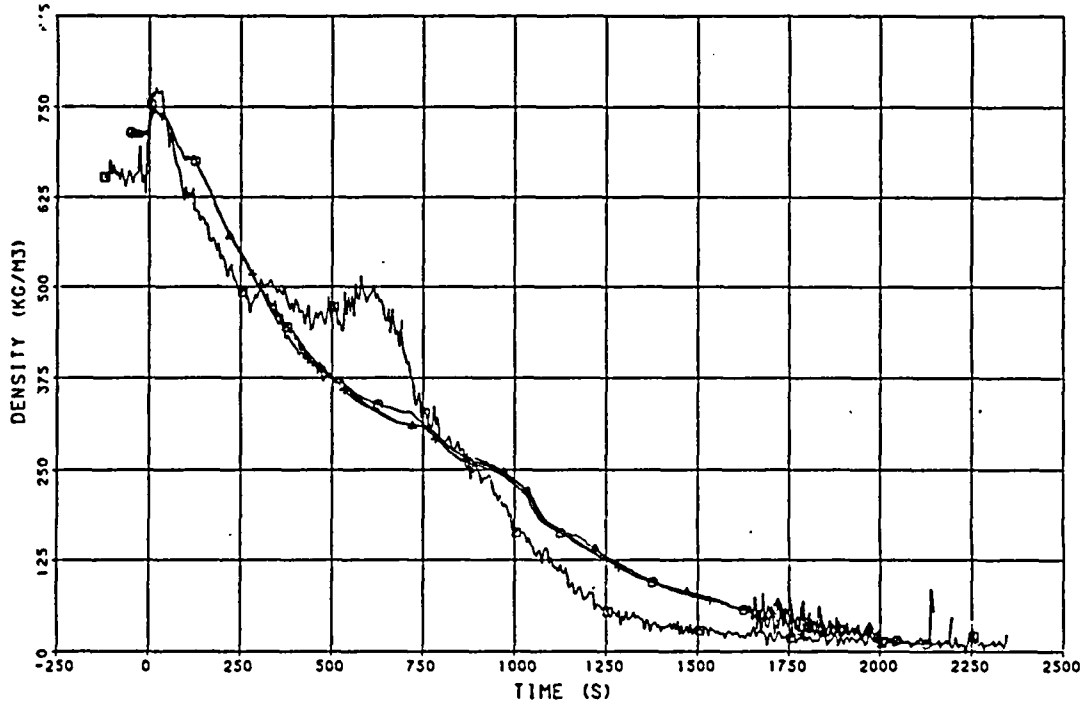
Plot B.22



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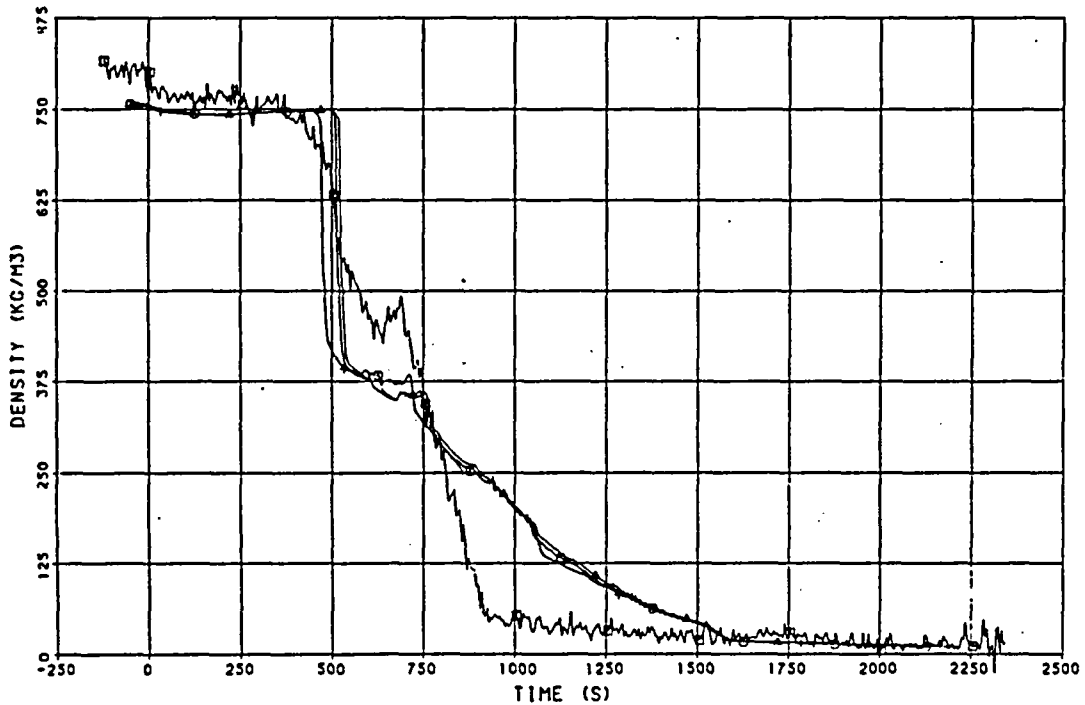
400 I.L. HOT LEG FLUID DENSITY (DE-PC-205) EXP.
I.L. HOT LEG FLUID DENSITY (RHO 103) CASE A
+ I.L. HOT LEG FLUID DENSITY (RHO 103) CASE B
I.L. HOT LEG FLUID DENSITY (RHO 103) CASE C

Plot B.23



400 B.L. HOT LEG FLUID DENSITY (DE-BL-0028) EXP.
B.L. HOT LEG FLUID DENSITY (RHO 303) CASE A
+ B.L. HOT LEG FLUID DENSITY (RHO 303) CASE B
B.L. HOT LEG FLUID DENSITY (RHO 303) CASE C

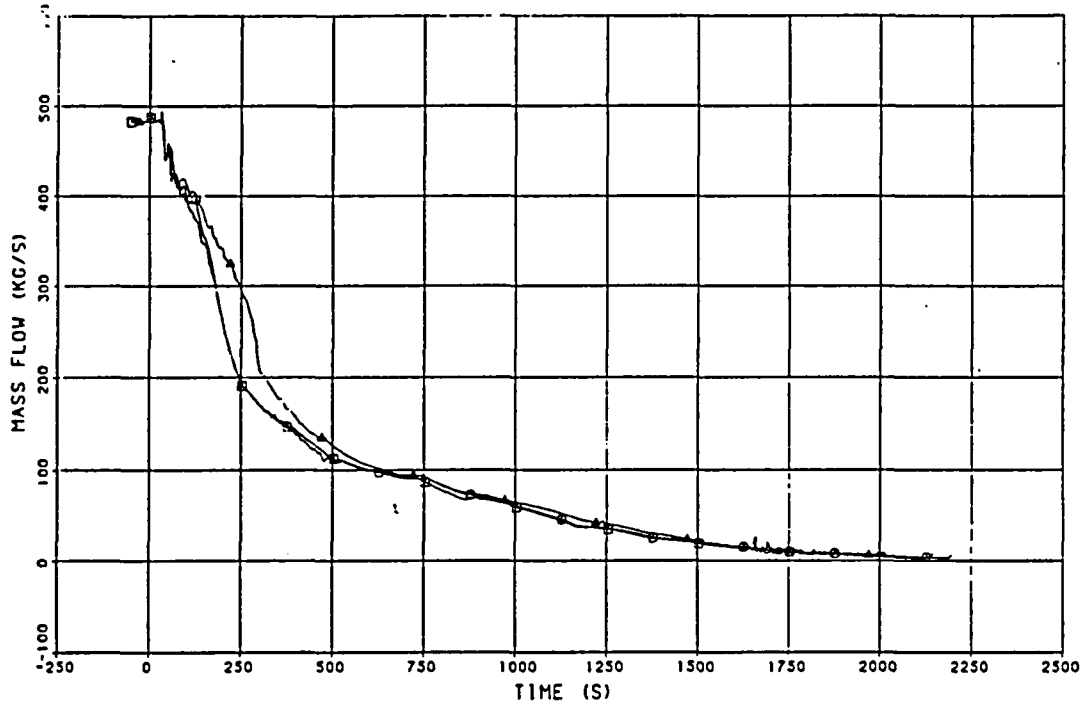
Plot B.24



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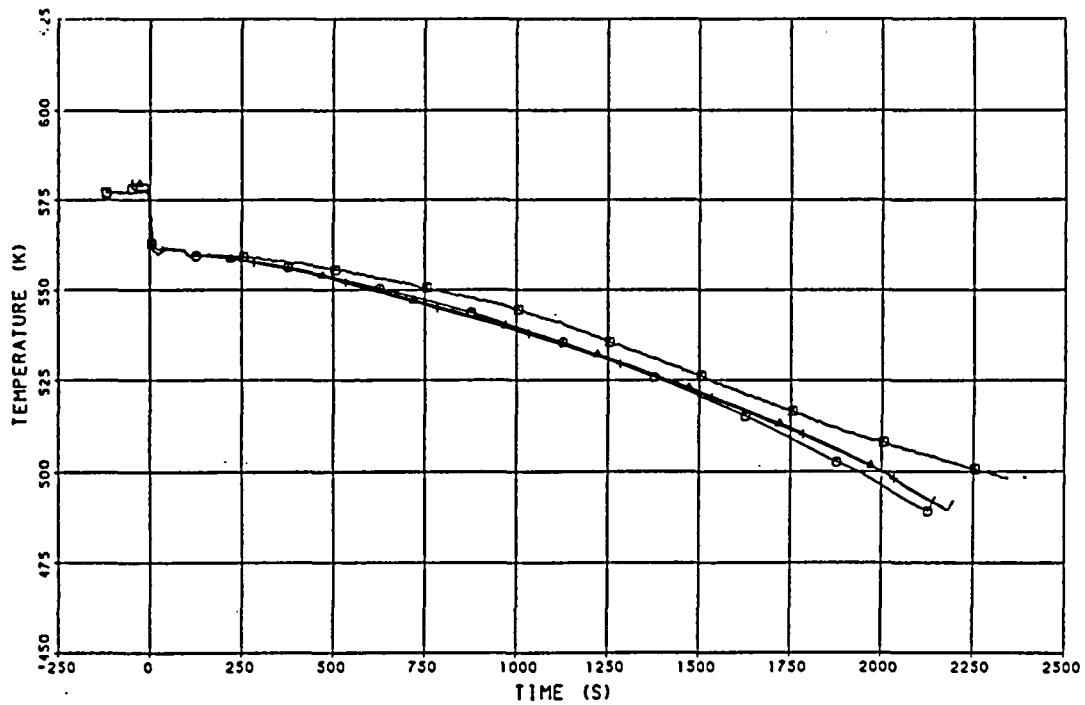
4 GB HOT LEG MASS FLOW RATE (MFLOWJ 110) CASE A
HOT LEG MASS FLOW RATE (MFLOWJ 110) CASE B
HOT LEG MASS FLOW RATE (MFLOWJ 110) CASE C

Plot B.25



4 GB I.L. HOT LEG TEMPERATURE (TE-PC-0028) EXP.
I.L. HOT LEG TEMPERATURE (TEMPF 105) CASE A
I.L. HOT LEG TEMPERATURE (TEMPF 105) CASE B
I.L. HOT LEG TEMPERATURE (TEMPF 105) CASE C

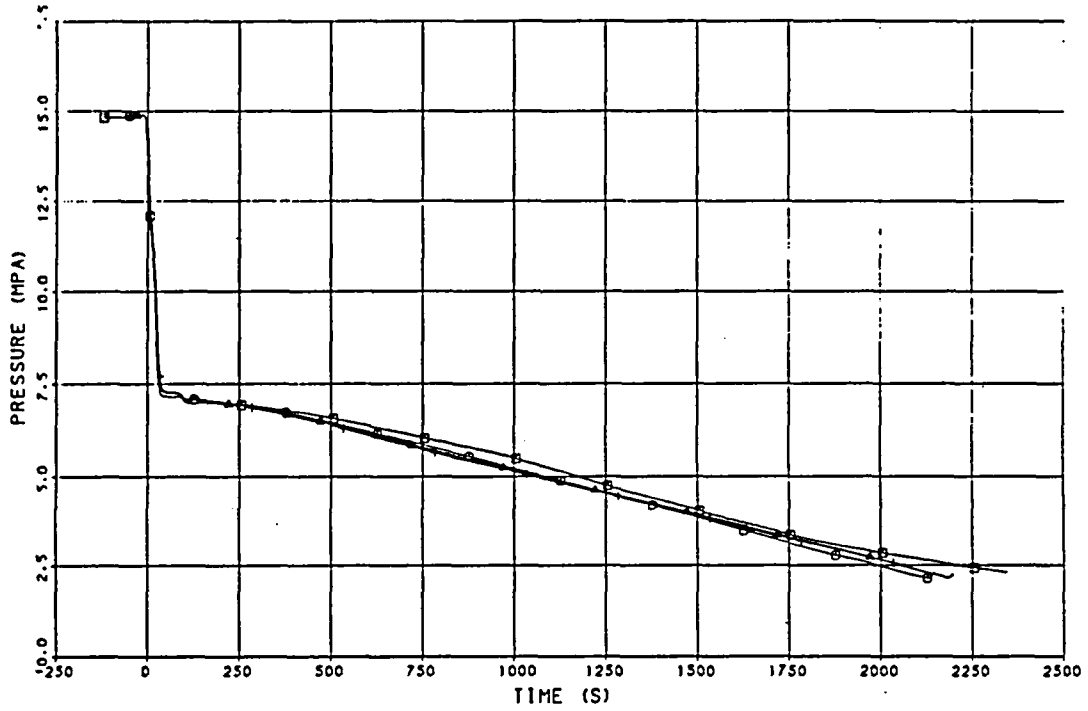
Plot B.26



1987-11-03

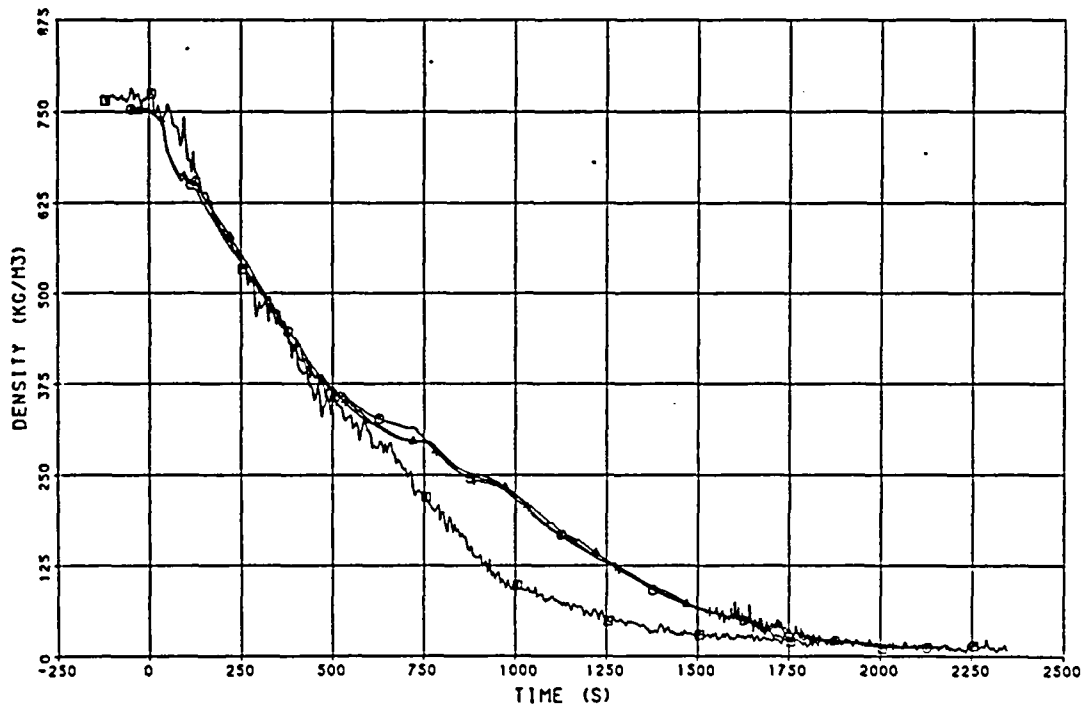
▲dB 1.L. HOT LEG PRESSURE (PE-PC-002) EXP.
1.L. HOT LEG PRESSURE (P 105) CASE A
+ 1.L. HOT LEG PRESSURE (P 105) CASE B
1.L. HOT LEG PRESSURE (P 105) CASE C

Plot B.27



▲dB 1.L. COLD LEG FLUID DENSITY (DE-PC-115) EXP.
1.L. COLD LEG FLUID DENSITY (RHO 185) CASE A
+ 1.L. COLD LEG FLUID DENSITY (RHO 185) CASE B
1.L. COLD LEG FLUID DENSITY (RHO 185) CASE C

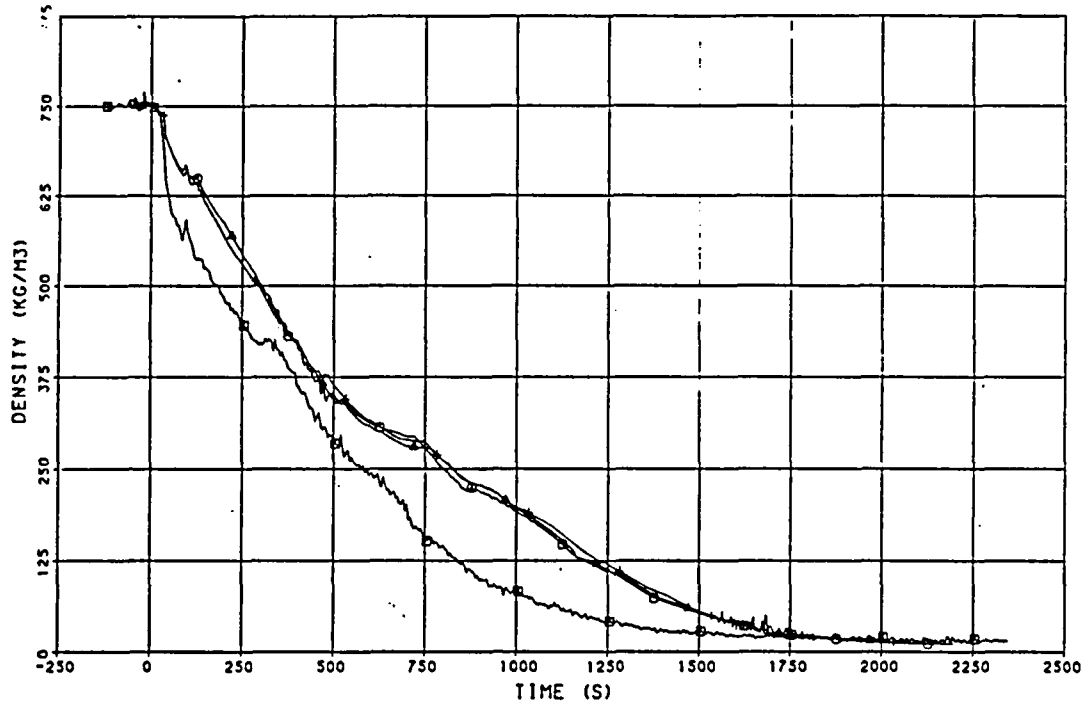
Plot B.28



1987-11-03

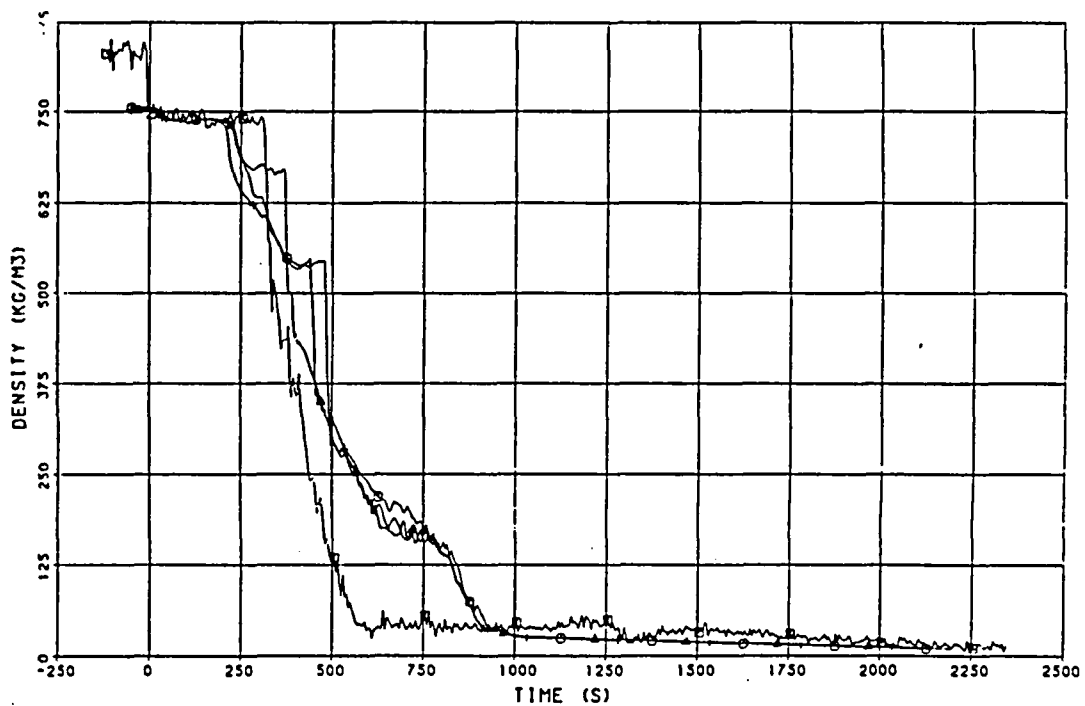
0000 COLD LEG PUMP FLUID DENSITY (DE-PC-305) EXP.
0000 COLD LEG PUMP FLUID DENSITY (RHO 115.13) CASE A
0000 COLD LEG PUMP FLUID DENSITY (RHO 115.13) CASE B
0000 COLD LEG PUMP FLUID DENSITY (RHO 115.13) CASE C

Plot B.29



0000 B.L. COLD LEG FLUID DENSITY (DE-BL-105) EXP.
0000 B.L. COLD LEG FLUID DENSITY (RHO 345) CASE A
0000 B.L. COLD LEG FLUID DENSITY (RHO 345) CASE B
0000 B.L. COLD LEG FLUID DENSITY (RHO 345) CASE C

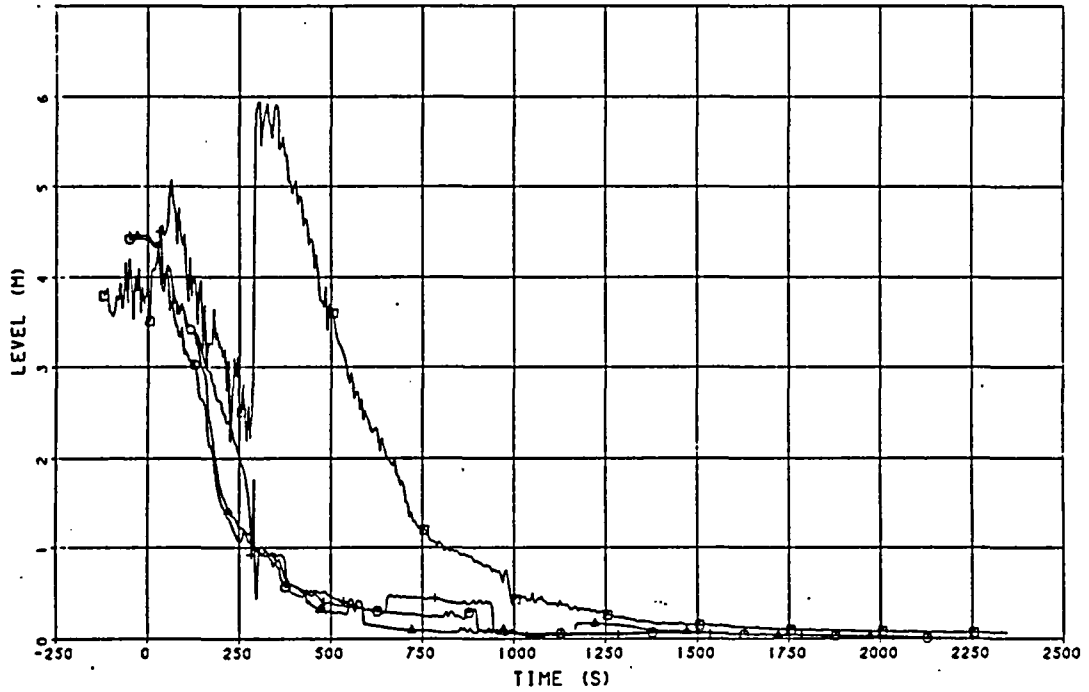
Plot B.30



1987-11-03

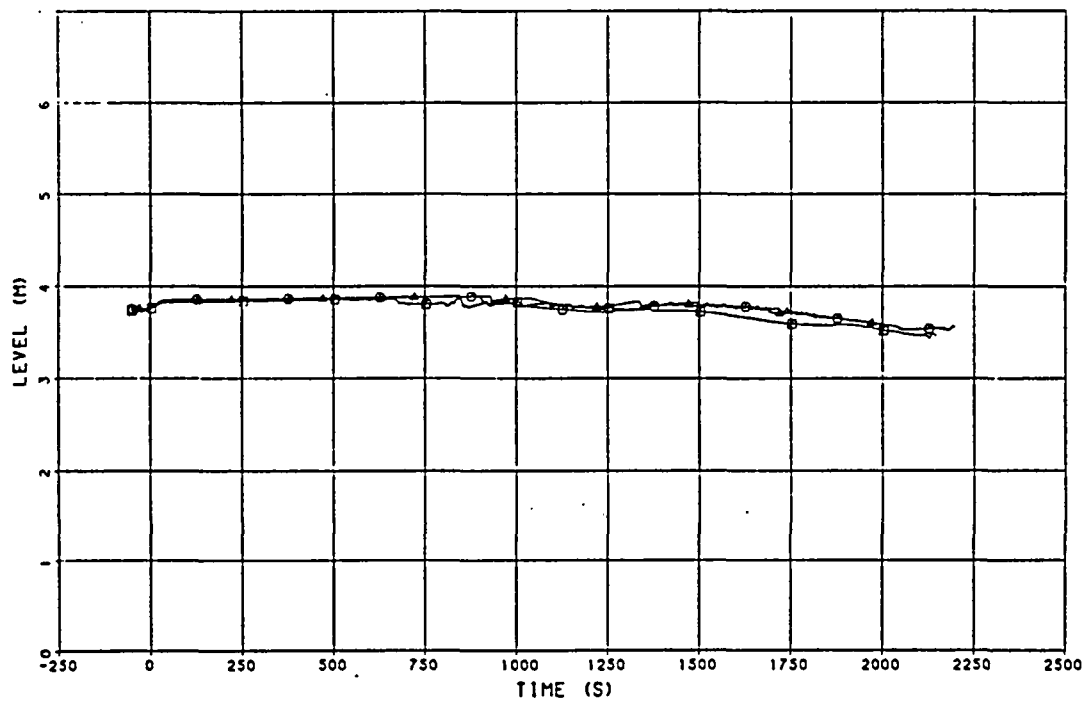
POB I-L. LOOP SEAL LIQUID LEVEL (LEPDE-PC-028) EXP.
 I-L. LOOP SEAL LIQUID LEVEL (CNTRLVAR 931) CASE A
 I-L. LOOP SEAL LIQUID LEVEL (CNTRLVAR 931) CASE B
 I-L. LOOP SEAL LIQUID LEVEL (CNTRLVAR 931) CASE C

Plot B.31



POB B-L. LOOP SEAL LIQUID LEVEL (CNTRLVAR 932) CASE A
 B-L. LOOP SEAL LIQUID LEVEL (CNTRLVAR 932) CASE B
 B-L. LOOP SEAL LIQUID LEVEL (CNTRLVAR 932) CASE C

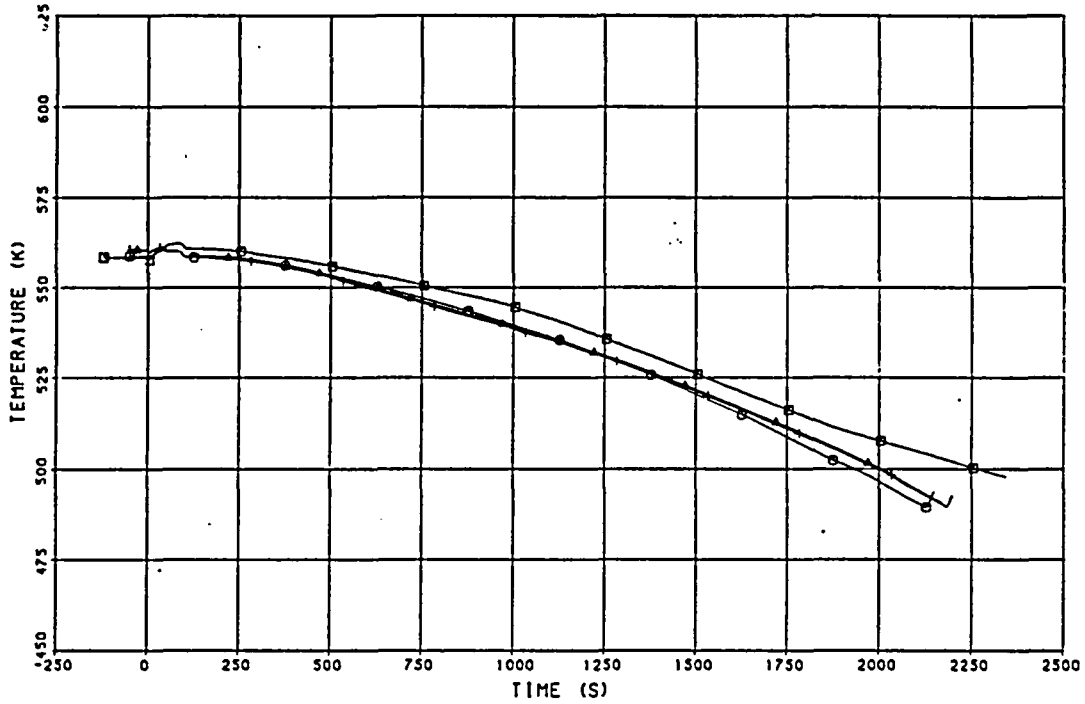
Plot B.32



1987-11-03

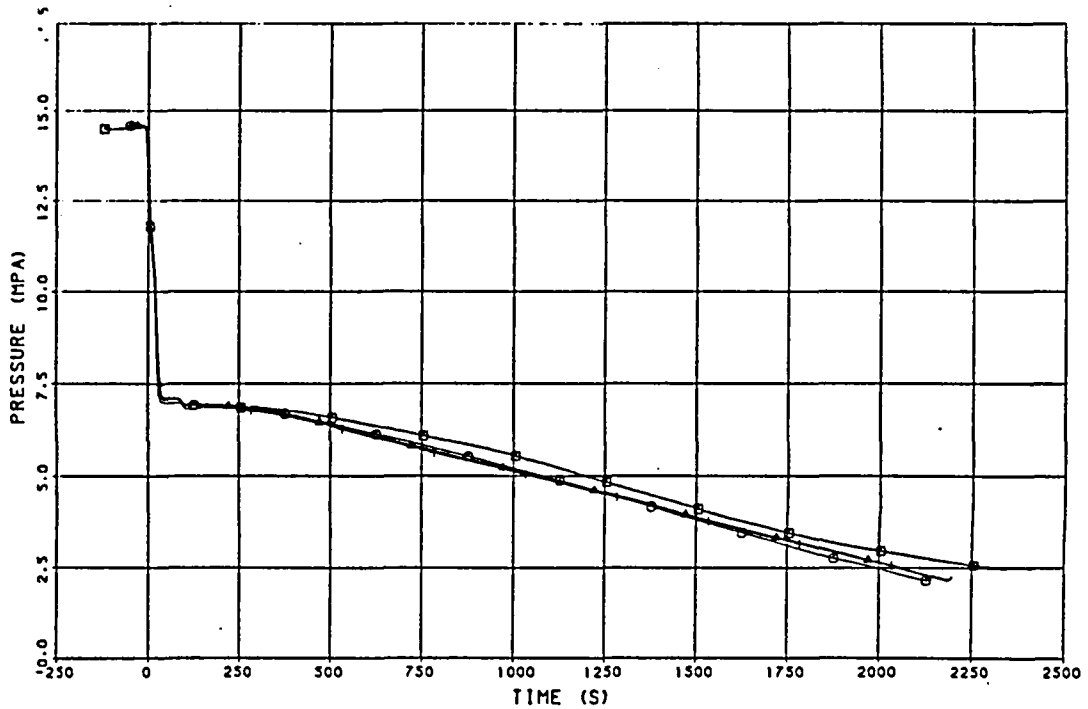
+ P 0 0 I.L. COLD LEG TEMPERATURE (ITE-PC-004) EXP.
I.L. COLD LEG TEMPERATURE (TEMP 183) CASE A
I.L. COLD LEG TEMPERATURE (TEMP 183) CASE B
I.L. COLD LEG TEMPERATURE (TEMP 183) CASE C

Plot B.33



+ P 0 0 I.L. COLD LEG PRESSURE (PE-PC-005) EXP.
I.L. COLD LEG PRESSURE (P 120) CASE A
I.L. COLD LEG PRESSURE (P 120) CASE B
I.L. COLD LEG PRESSURE (P 120) CASE C

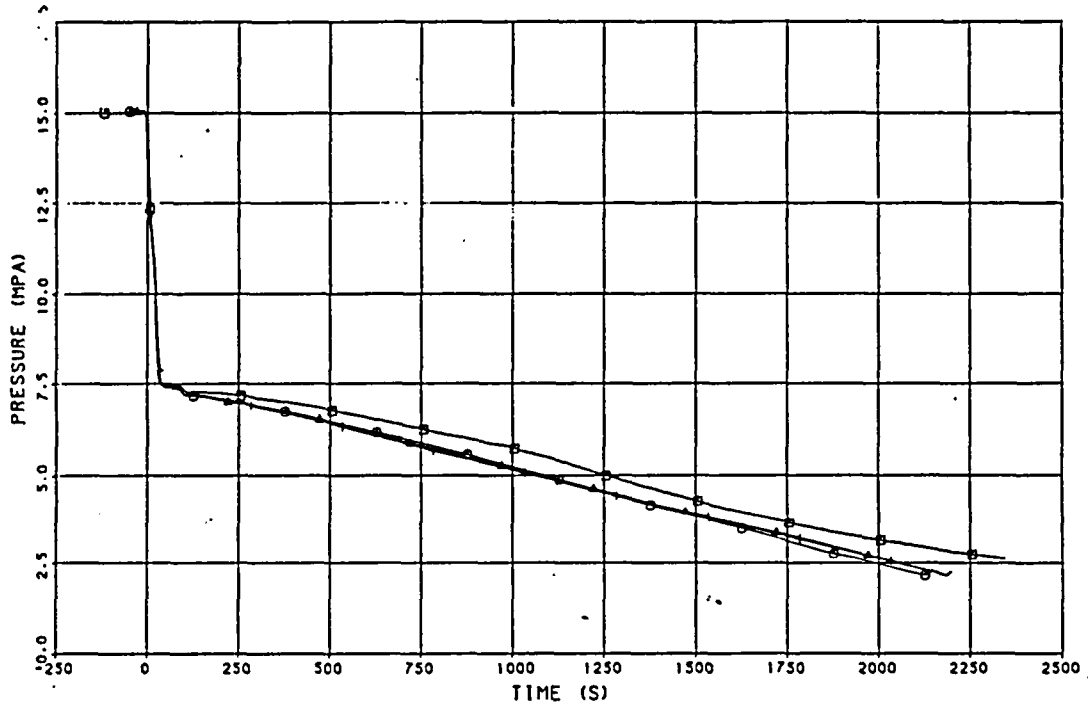
Plot B.34



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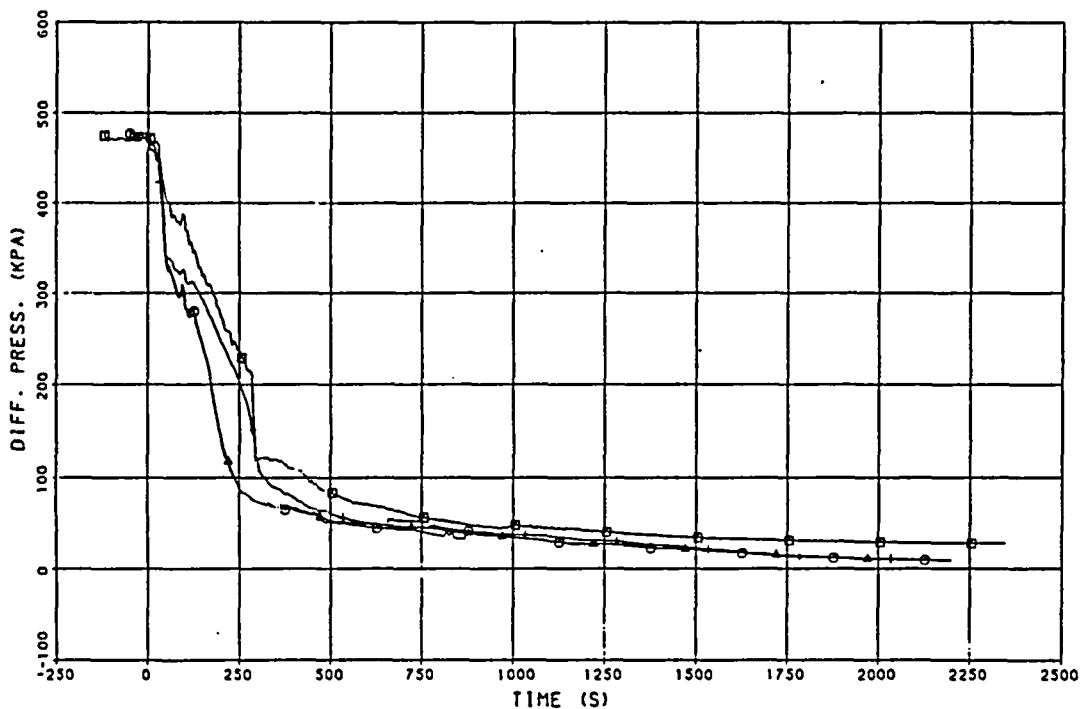
+ B.L. COLD LEG PRESSURE (PE-BL-001) EXP.
 + B.L. COLD LEG PRESSURE (IP 345) CASE A
 + B.L. COLD LEG PRESSURE (IP 345) CASE B
 + B.L. COLD LEG PRESSURE (IP 345) CASE C

Plot B.35



+ PRESS. DIFF. ACROSS PUMPS (PDE-PC-001) EXP.
 + PRESS. DIFF. ACROSS PUMPS (CNTRLVAR 936) CASE A
 + PRESS. DIFF. ACROSS PUMPS (CNTRLVAR 936) CASE B
 + PRESS. DIFF. ACROSS PUMPS (CNTRLVAR 936) CASE C

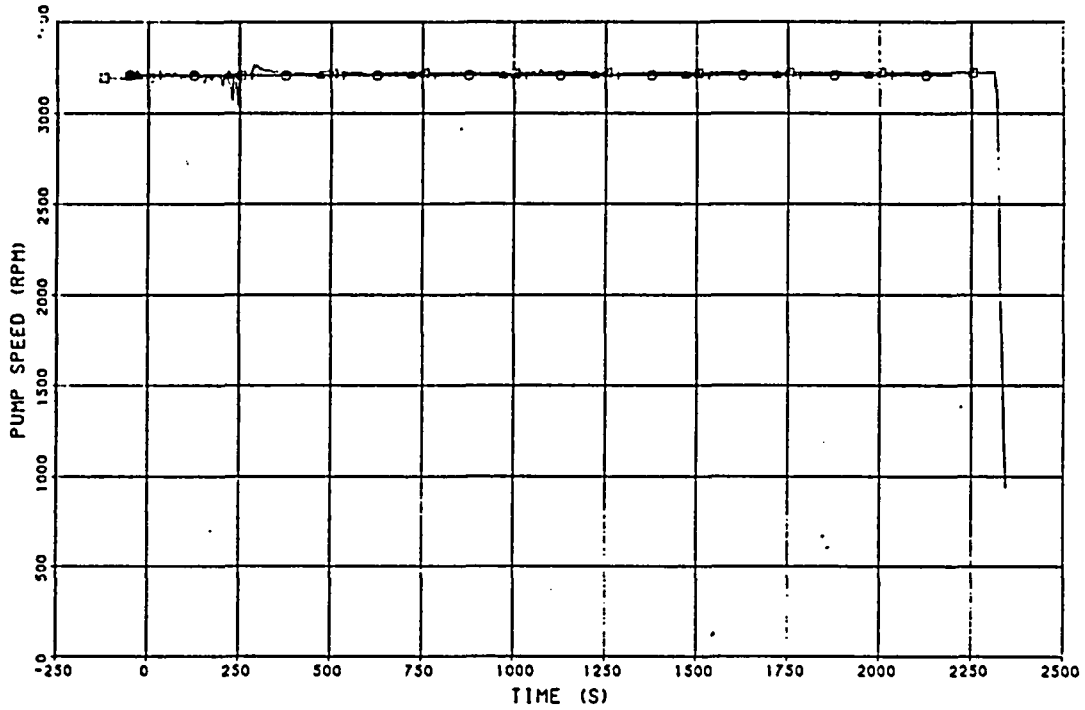
Plot B.36



1987-11-03

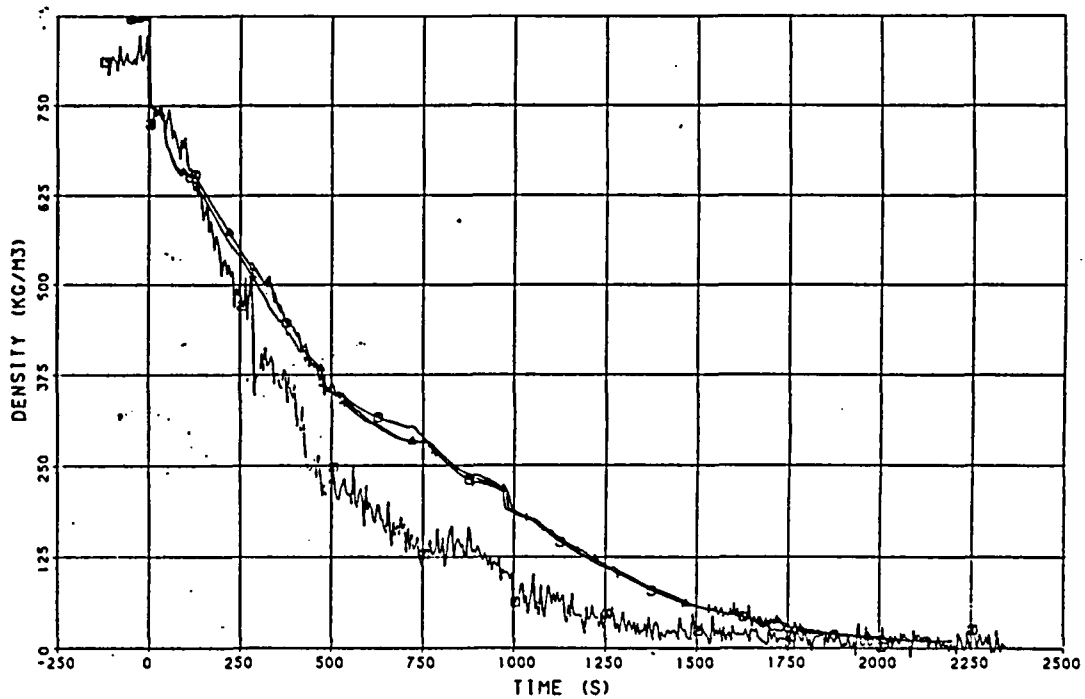
↑&↓&□ SPEED OF PUMP 1 (RPE-PC-001) EXP.
↑&↓&○ SPEED OF PUMP 1 (PUMPVEL 135) CASE A
↑&↓&◇ SPEED OF PUMP 1 (PUMPVEL 135) CASE B
↑&↓&△ SPEED OF PUMP 1 (PUMPVEL 135) CASE C

Plot B.37



↑&↓&□ BREAK FLUID DENSITY (DE-PC-502A) EXP.
↑&↓&○ BREAK FLUID DENSITY (IRHO 800) CASE A
↑&↓&◇ BREAK FLUID DENSITY (IRHO 800) CASE B
↑&↓&△ BREAK FLUID DENSITY (IRHO 800) CASE C

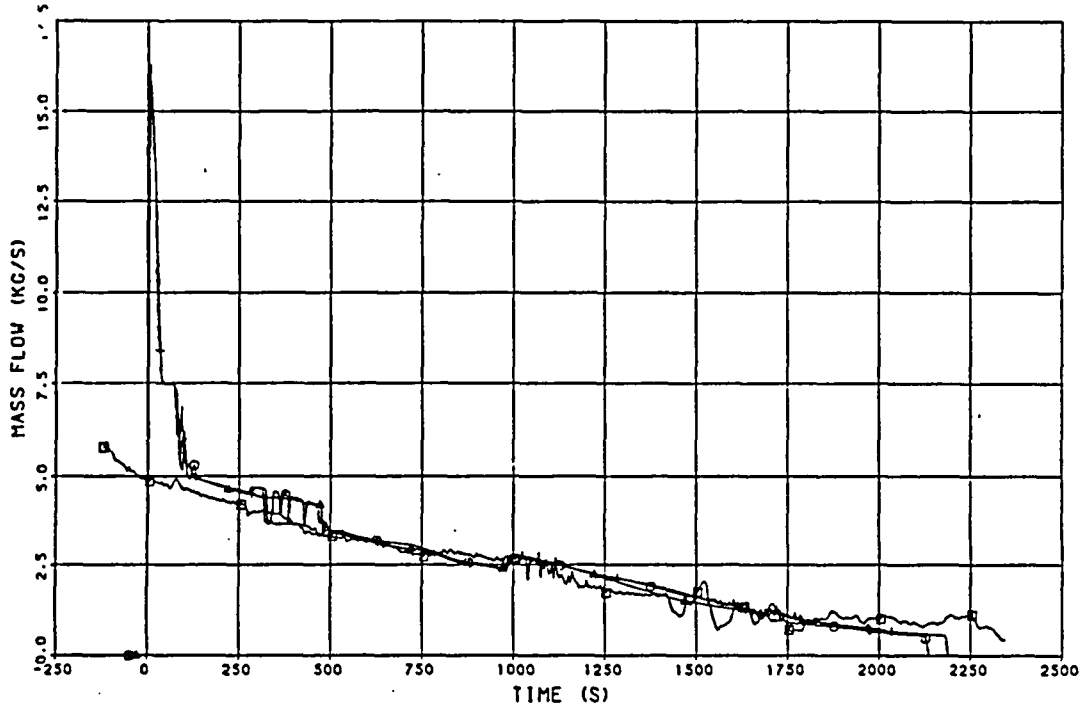
Plot B.38



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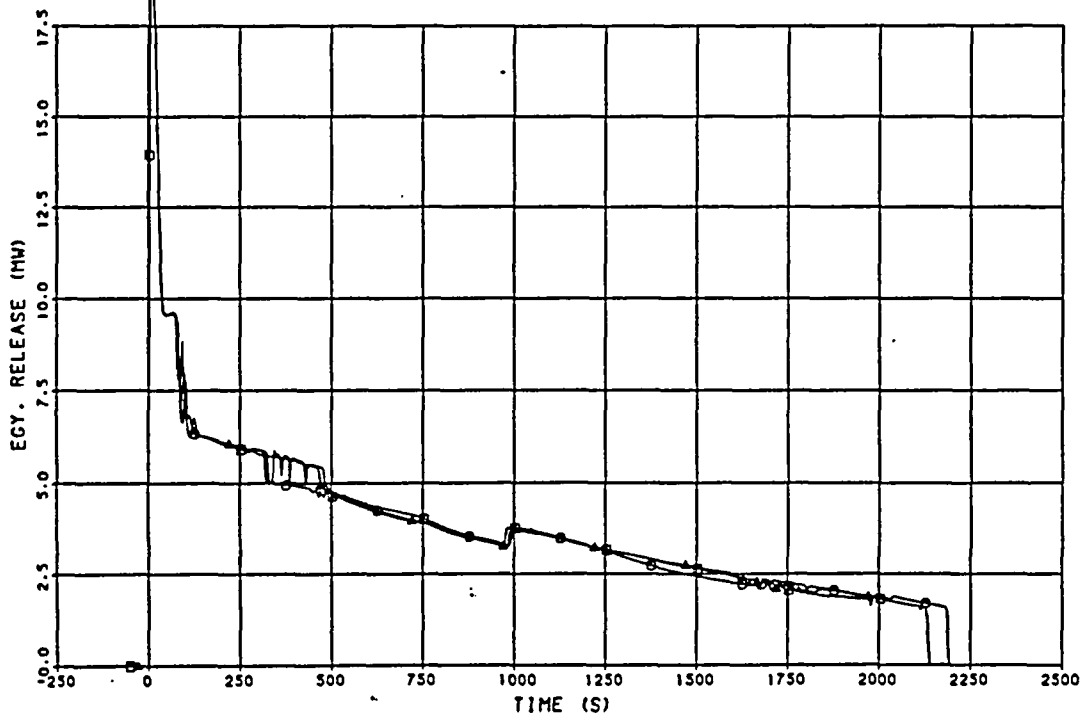
□ BREAK MASS FLOW RATE (FR-PC-S121) EXP.
○ BREAK MASS FLOW RATE (MFLOWJ 803) CASE A
△ BREAK MASS FLOW RATE (MFLOWJ 803) CASE B
+ BREAK MASS FLOW RATE (MFLOWJ 803) CASE C

Plot B.39



□ BREAK ENERGY RELEASE (CNTRLVAR 940) CASE A
○ BREAK ENERGY RELEASE (CNTRLVAR 940) CASE B
△ BREAK ENERGY RELEASE (CNTRLVAR 940) CASE C

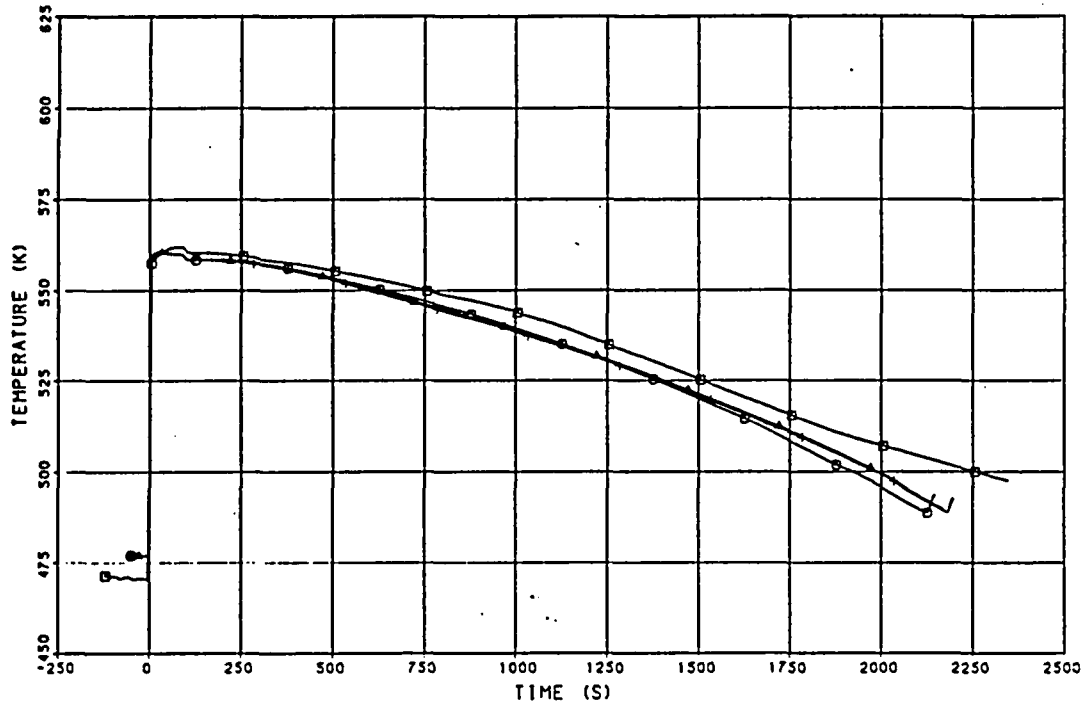
Plot B.40



1987-11-03

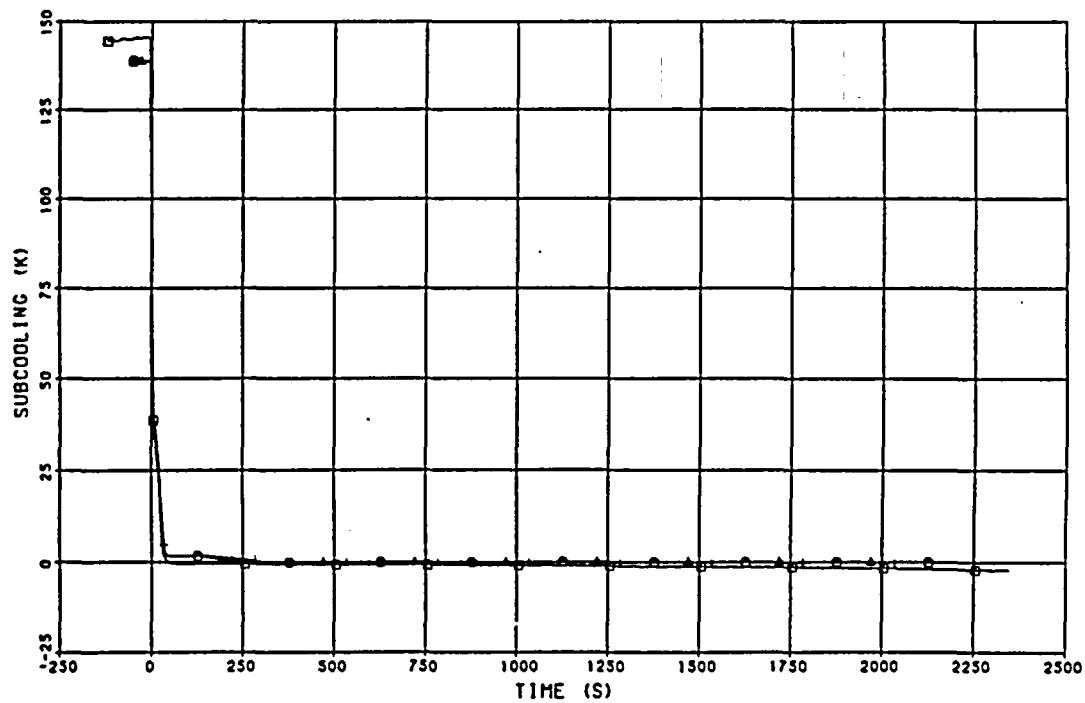
○ BREAK INLET TEMPERATURE (TE-PC-S01C) EXP.
 ▲ BREAK INLET TEMPERATURE (TEMPF 800) CASE A
 + BREAK INLET TEMPERATURE (TEMPF 800) CASE B
 + BREAK INLET TEMPERATURE (TEMPF 800) CASE C

Plot B.41



○ BREAK INLET SUBC. (SI-PC-S101 - TE-PC-S01C) EXP.
 ▲ BREAK INLET SUBC. (CNTRLVAR 942) CASE A
 + BREAK INLET SUBC. (CNTRLVAR 942) CASE B
 + BREAK INLET SUBC. (CNTRLVAR 942) CASE C

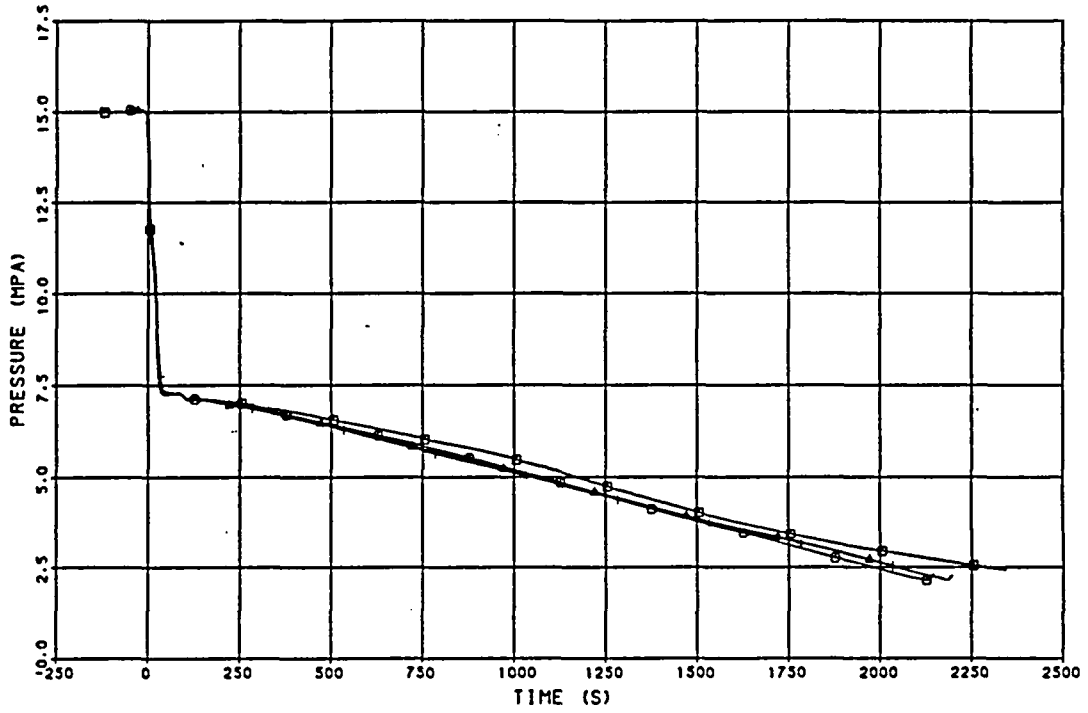
Plot B.42



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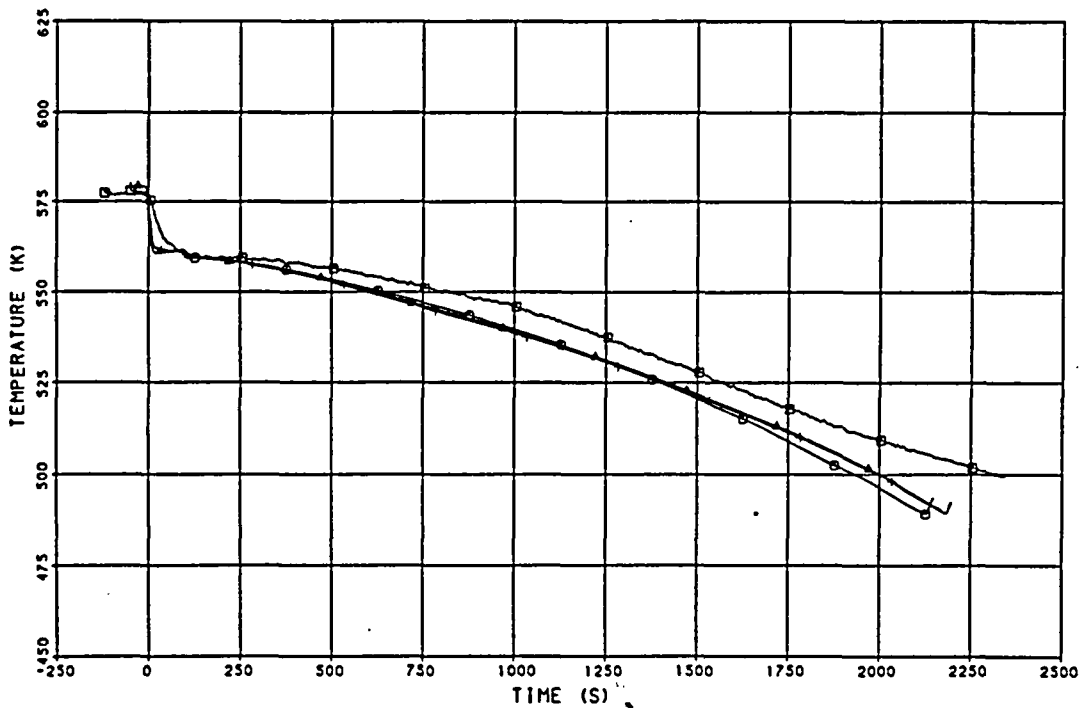
+ 400 BREAK INLET PRESSURE (PE-PC-501) EXP.
BREAK INLET PRESSURE (P 800) CASE A
BREAK INLET PRESSURE (P 800) CASE B
BREAK INLET PRESSURE (P 800) CASE C

Plot B.43



+ 400 SC PRI. SIDE INLET TEMPERATURE (TE-SC-001) EXP.
SC PRI. SIDE INLET TEMPERATURE (TEMPF 115.03) CASE A
SC PRI. SIDE INLET TEMPERATURE (TEMPF 115.03) CASE B
SC PRI. SIDE INLET TEMPERATURE (TEMPF 115.03) CASE C

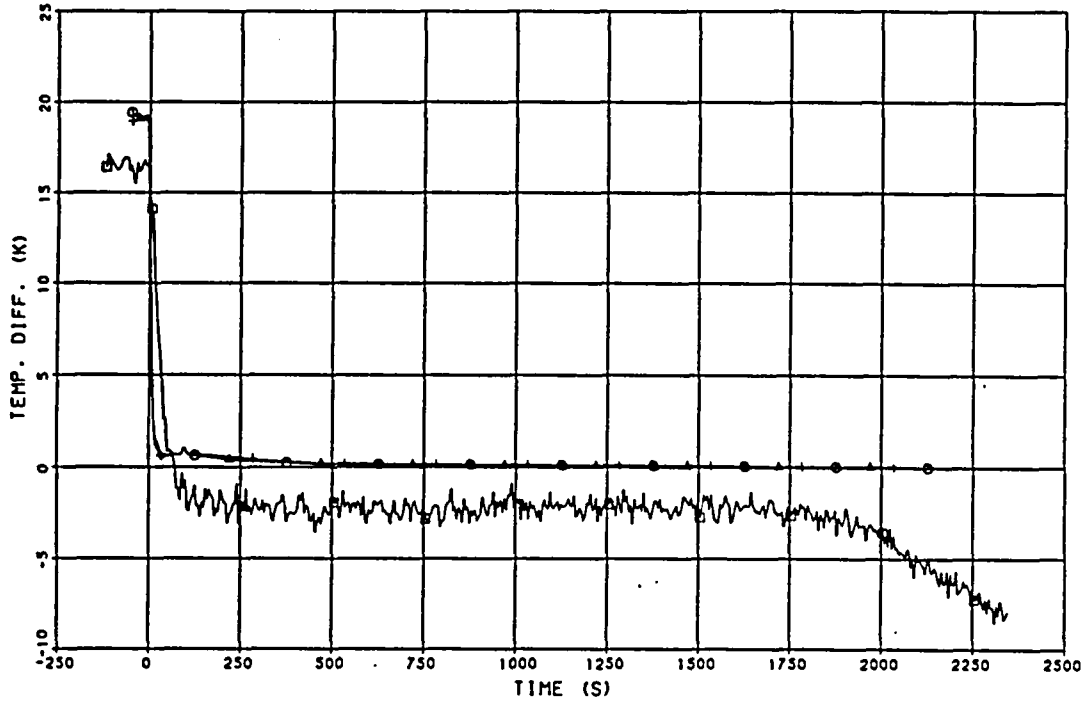
Plot B.44



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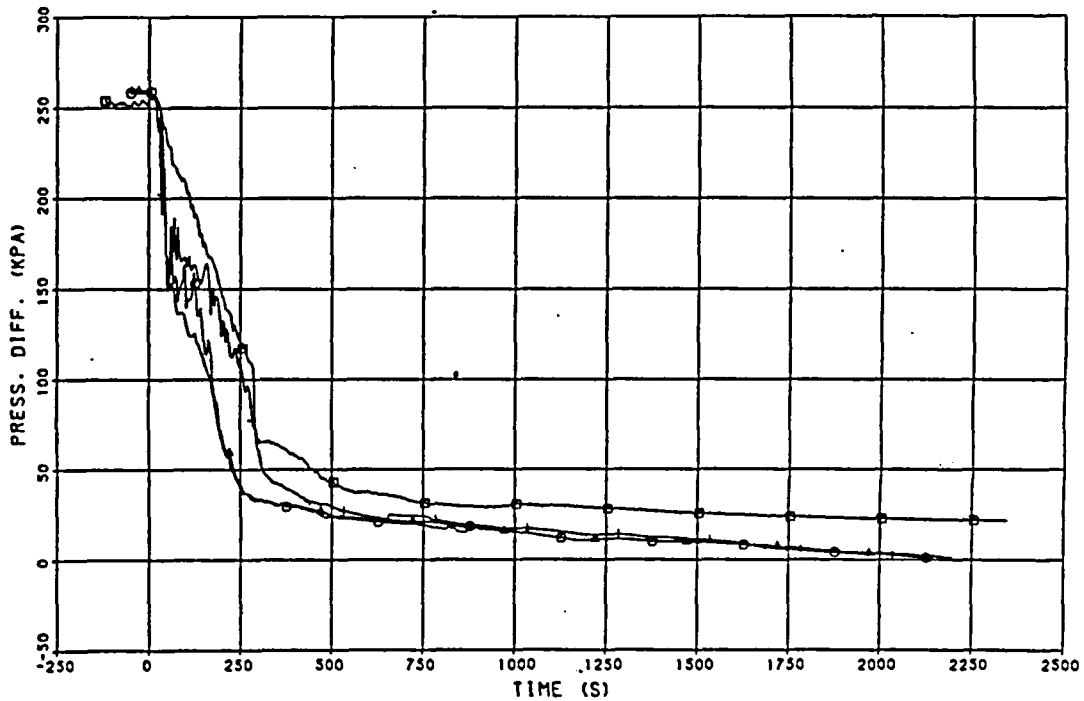
Δ00B SC PRI. TEMP. DIFF. (TE-SC-001 - TE-SC-002) EXP.
SC PRI. TEMP. DIFF. (CNTRLVAR 945) CASE A
+ SC PRI. TEMP. DIFF. (CNTRLVAR 945) CASE B
SC PRI. TEMP. DIFF. (CNTRLVAR 945) CASE C

Plot B.45



Δ00B SC PRI. SIDE PRESSURE DIFF. (PDE-PC-002) EXP.
SC PRI. SIDE PRESSURE DIFF. (CNTRLVAR 946) CASE A
+ SC PRI. SIDE PRESSURE DIFF. (CNTRLVAR 946) CASE B
SC PRI. SIDE PRESSURE DIFF. (CNTRLVAR 946) CASE C

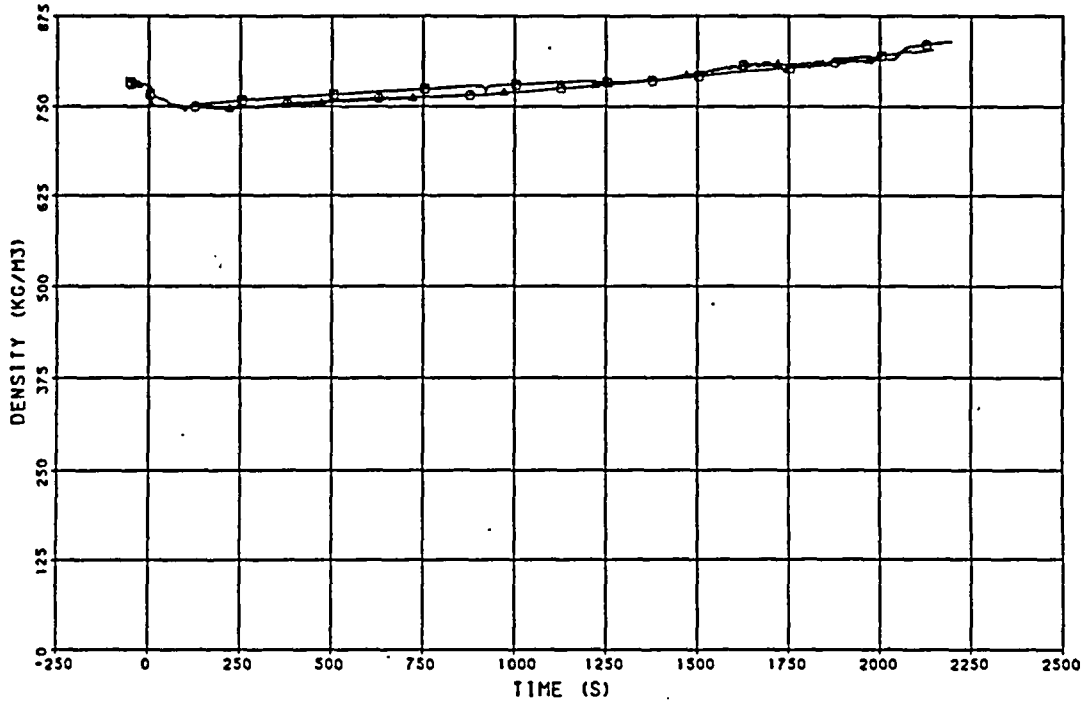
Plot B.46



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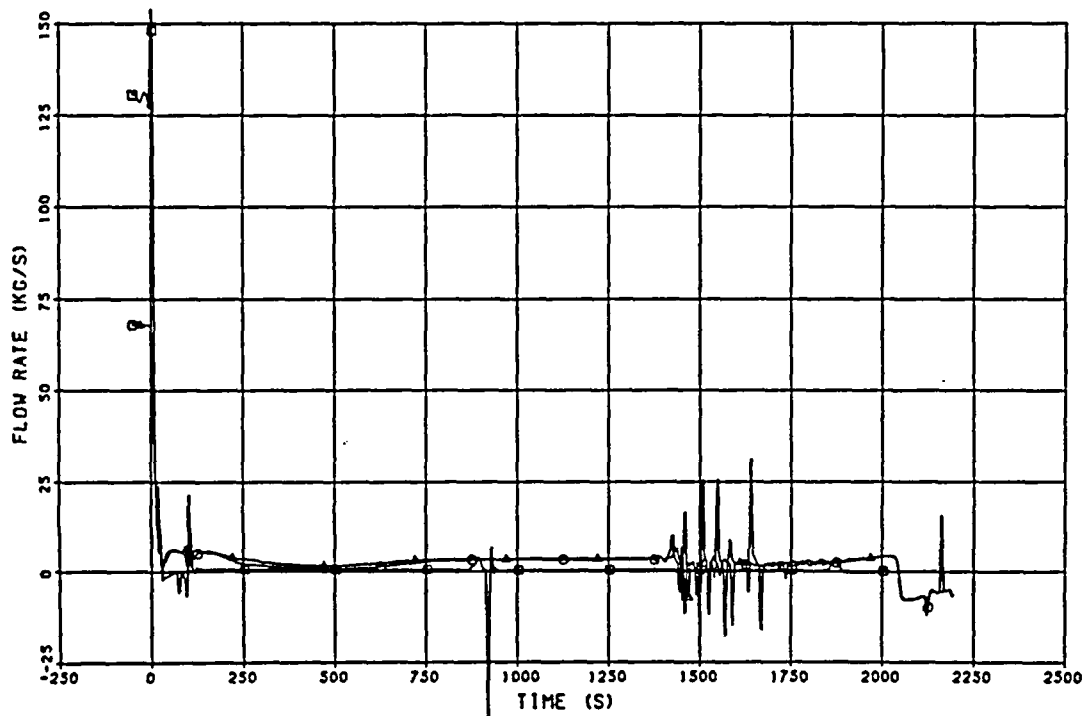
P00 SC FLUID DENSITY (RHO 515.03) CASE A
SC FLUID DENSITY (RHO 515.03) CASE B
SC FLUID DENSITY (RHO 515.03) CASE C

Plot B.47



P00 SC MASS FLOW RATE (MFLOWJ 516) CASE A
SC MASS FLOW RATE (MFLOWJ 516) CASE B
SC MASS FLOW RATE (MFLOWJ 516) CASE C

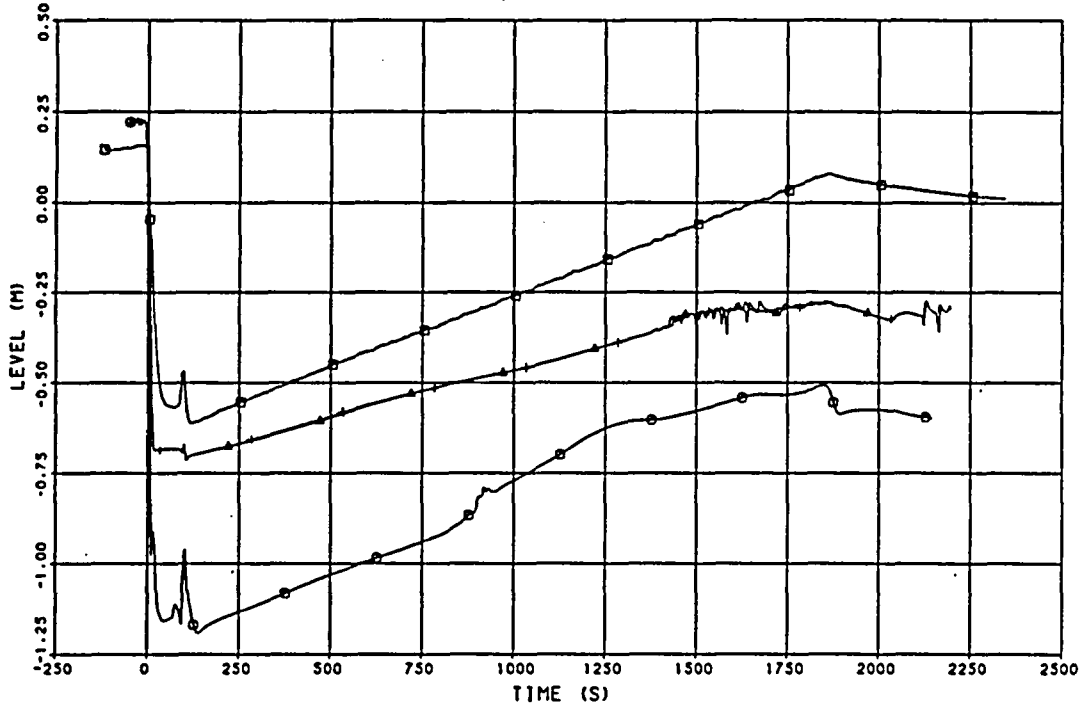
Plot B.48



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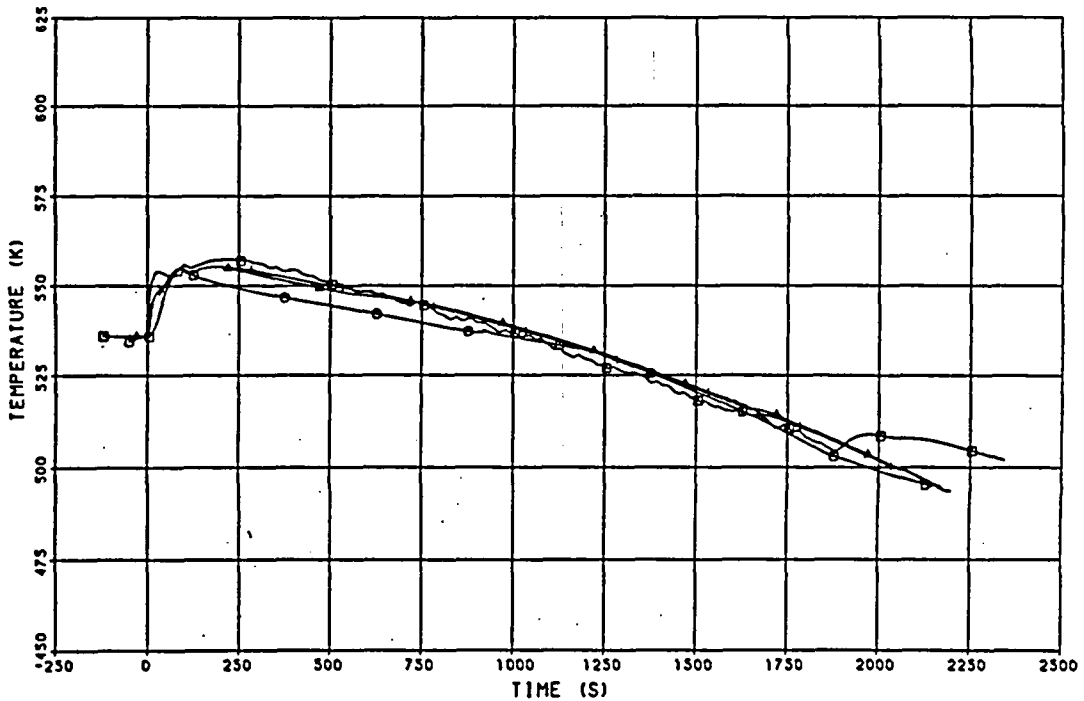
□ SC LIQUID LEVEL (LD-P004-008) EXP.
○ SC LIQUID LEVEL (CNTRLVAR 949) CASE A
△ SC LIQUID LEVEL (CNTRLVAR 949) CASE B
+ SC LIQUID LEVEL (CNTRLVAR 949) CASE C

Plot B.49



□ SC LIQUID TEMPERATURE (TE-SC-003) EXP.
○ SC LIQUID TEMPERATURE (TEMPF 313.03) CASE A
△ SC LIQUID TEMPERATURE (TEMPF 313.03) CASE B
+ SC LIQUID TEMPERATURE (TEMPF 313.03) CASE C

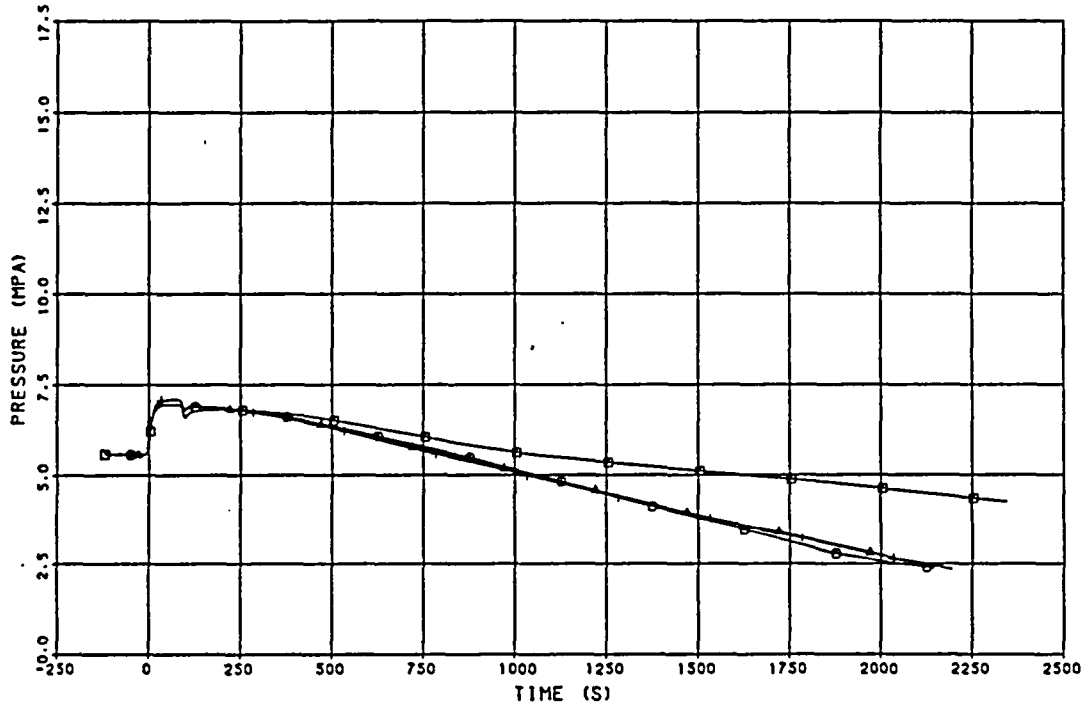
Plot B.50



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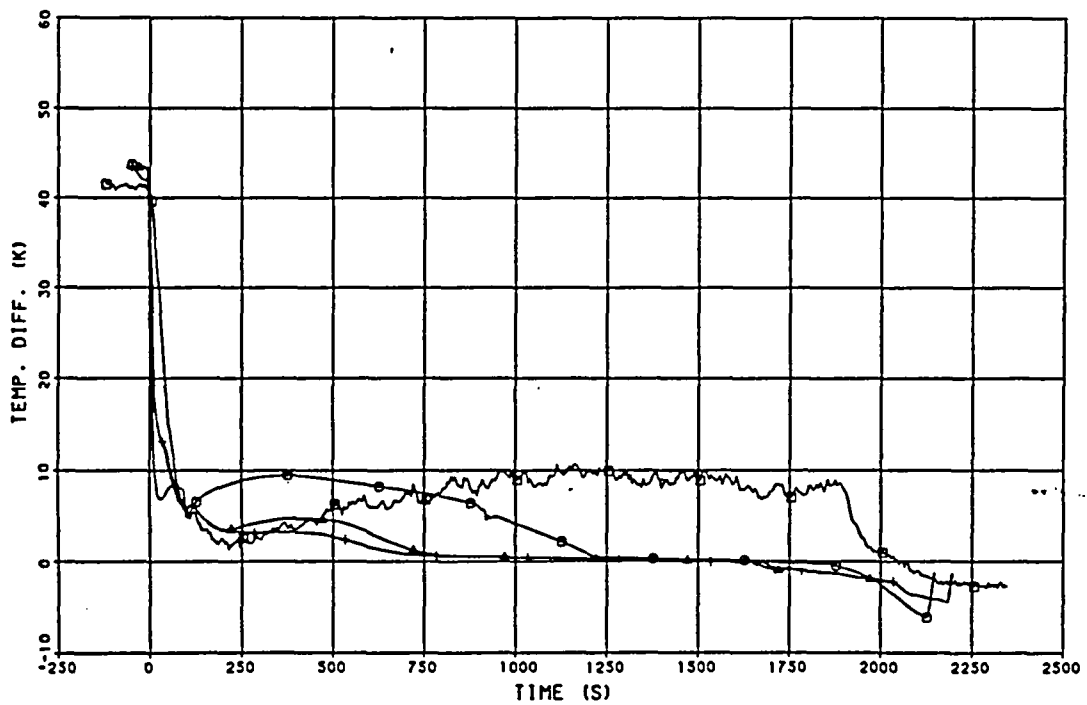
+400 SG PRESSURE (PE-SGS-001) EXP.
 SG PRESSURE (P 330) CASE A
 SG PRESSURE (P 330) CASE B
 SG PRESSURE (P 330) CASE C

Plot B.51



+400 SG PRI.-SEC. TEMP. DIFF. (TE-SG-001 -TE-SG-003) EXP.
 SG PRI.-SEC. TEMP. DIFF. (CNTRLVAR 952) CASE A
 SG PRI.-SEC. TEMP. DIFF. (CNTRLVAR 952) CASE B
 SG PRI.-SEC. TEMP. DIFF. (CNTRLVAR 952) CASE C

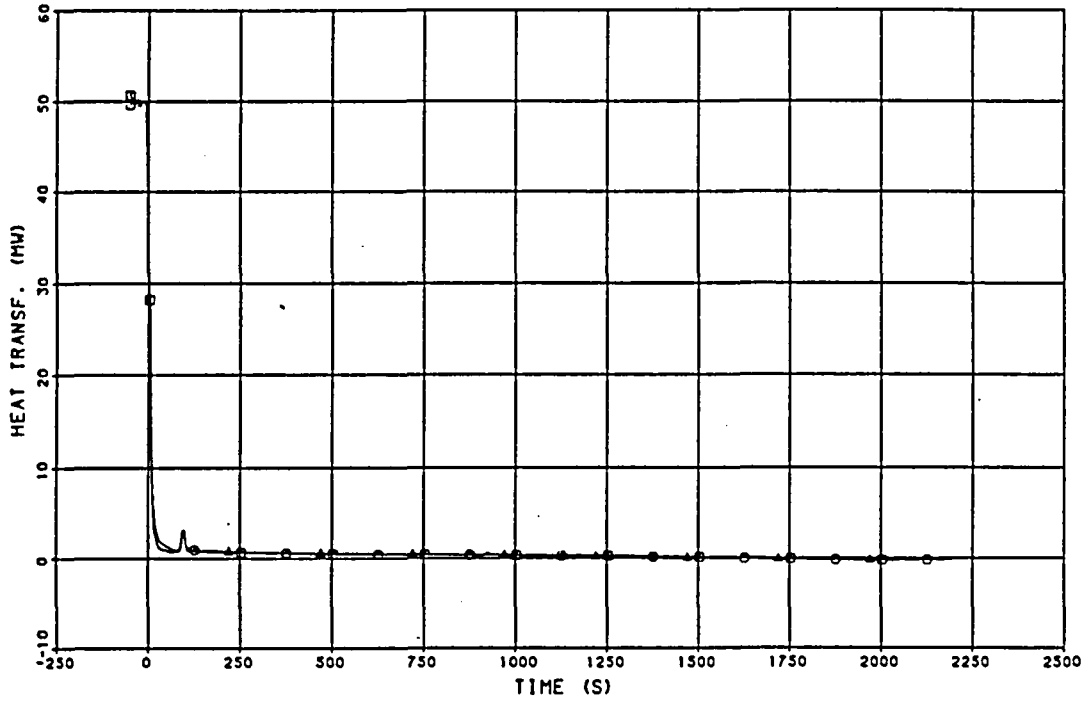
Plot B.52



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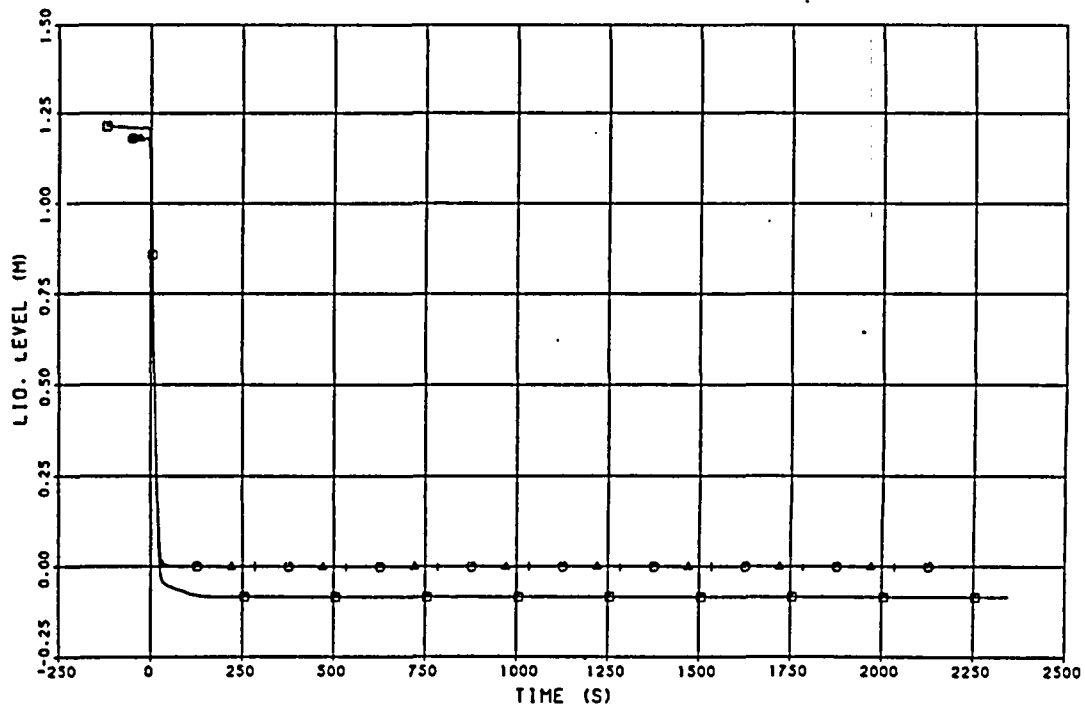
□ SC HEAT TRANSFER RATE (CNTRLVAR 953) CASE A
○ SC HEAT TRANSFER RATE (CNTRLVAR 953) CASE B
△ SC HEAT TRANSFER RATE (CNTRLVAR 953) CASE C

Plot B.53



□ PRESSURIZER LIQUID LEVEL (LI-P139-006) EXP.
○ PRESSURIZER LIQUID LEVEL (CNTRLVAR 954) CASE A
△ PRESSURIZER LIQUID LEVEL (CNTRLVAR 954) CASE B
+ PRESSURIZER LIQUID LEVEL (CNTRLVAR 954) CASE C

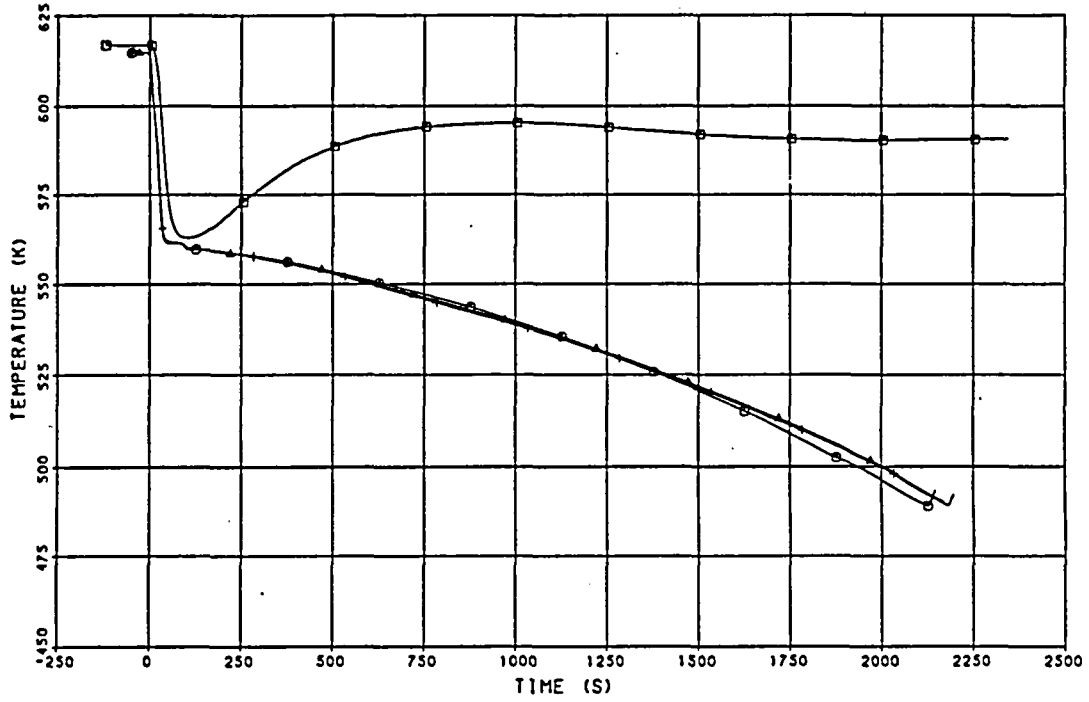
Plot B.54



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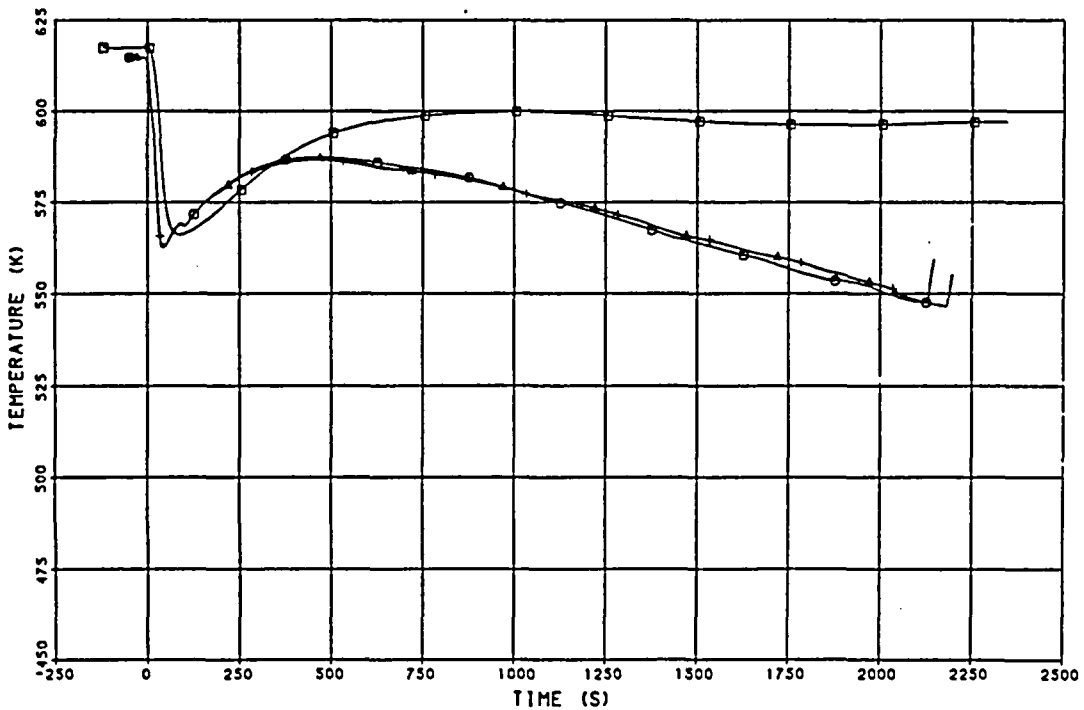
+ ▴ ▽ PRESSURIZER LIQUID TEMP. (TE-P139-020) EXP.
PRESSURIZER LIQUID TEMP. (TEMPF 415.02) CASE A
PRESSURIZER LIQUID TEMP. (TEMPF 415.02) CASE B
PRESSURIZER LIQUID TEMP. (TEMPF 415.02) CASE C

Plot B.55



+ ▴ ▽ PRESSURIZER STEAM TEMP. (TE-P139-018) EXP.
PRESSURIZER STEAM TEMP. (TEMPG 415.07) CASE A
PRESSURIZER STEAM TEMP. (TEMPG 415.07) CASE B
PRESSURIZER STEAM TEMP. (TEMPG 415.07) CASE C

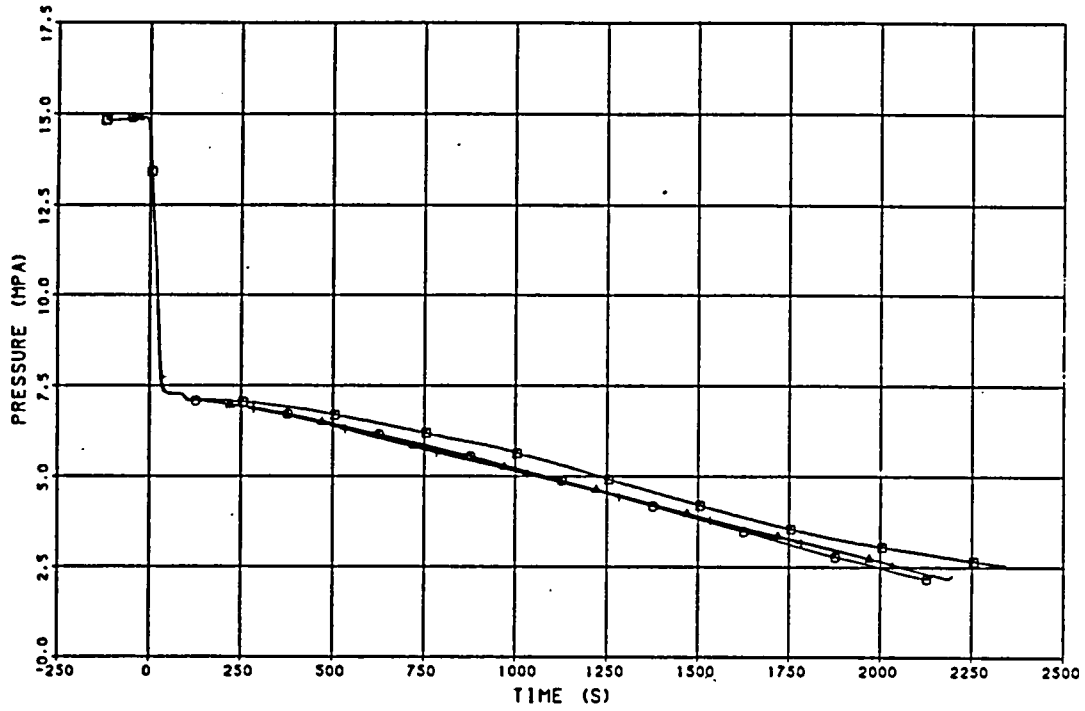
Plot B.56



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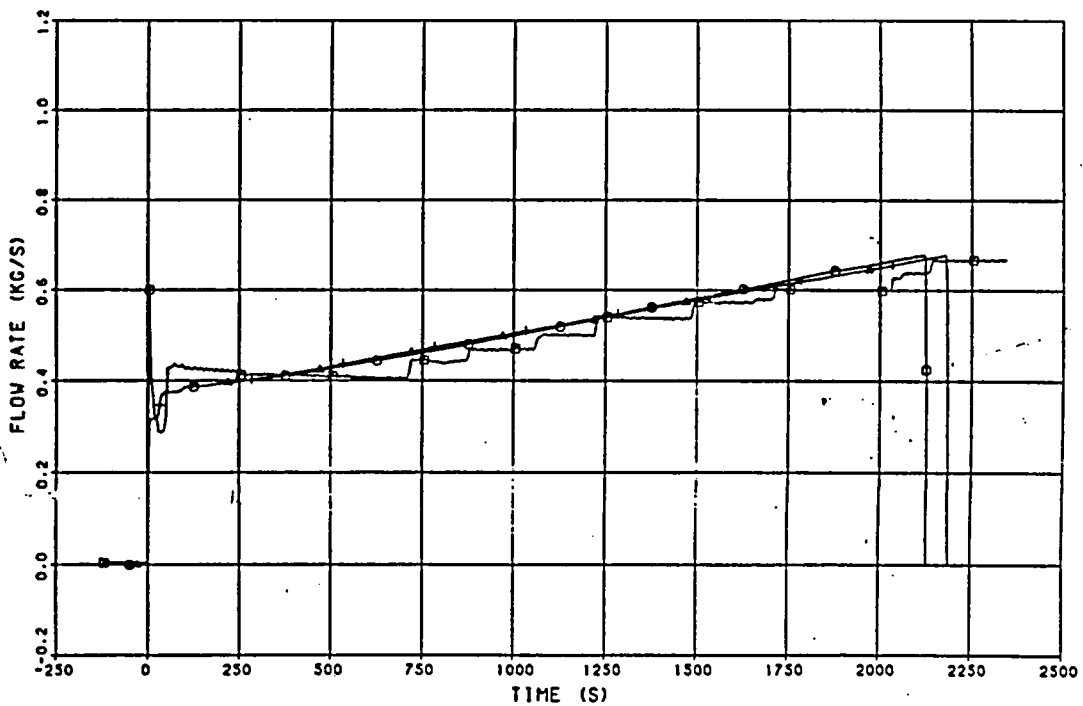
□ PRESSURIZER PRESSURE (PE-PC-004) EXP.
▲ PRESSURIZER PRESSURE (P 413.08) CASE A
△ PRESSURIZER PRESSURE (P 413.08) CASE B
+ PRESSURIZER PRESSURE (P 413.08) CASE C

Plot B.57



□ NP15 VOLUMETRIC FLOW RATE (FT-P128-104) EXP.
▲ NP15 VOLUMETRIC FLOW RATE (CNTRLVAR 958) CASE A
△ NP15 VOLUMETRIC FLOW RATE (CNTRLVAR 958) CASE B
+ NP15 VOLUMETRIC FLOW RATE (CNTRLVAR 958) CASE C

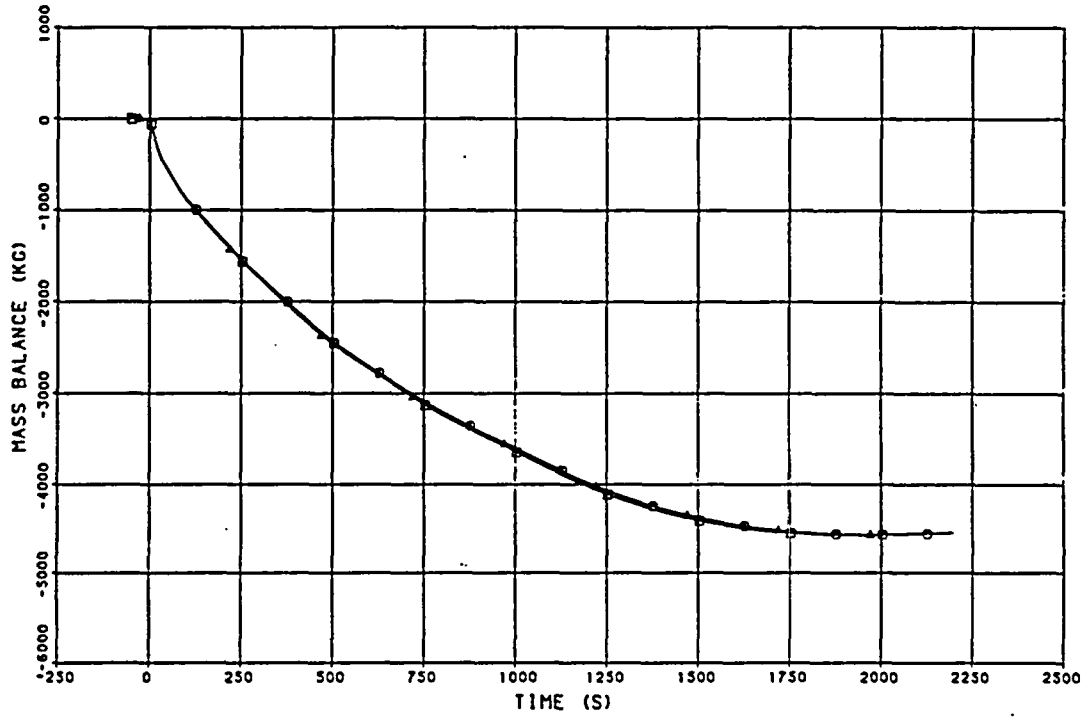
Plot B.58



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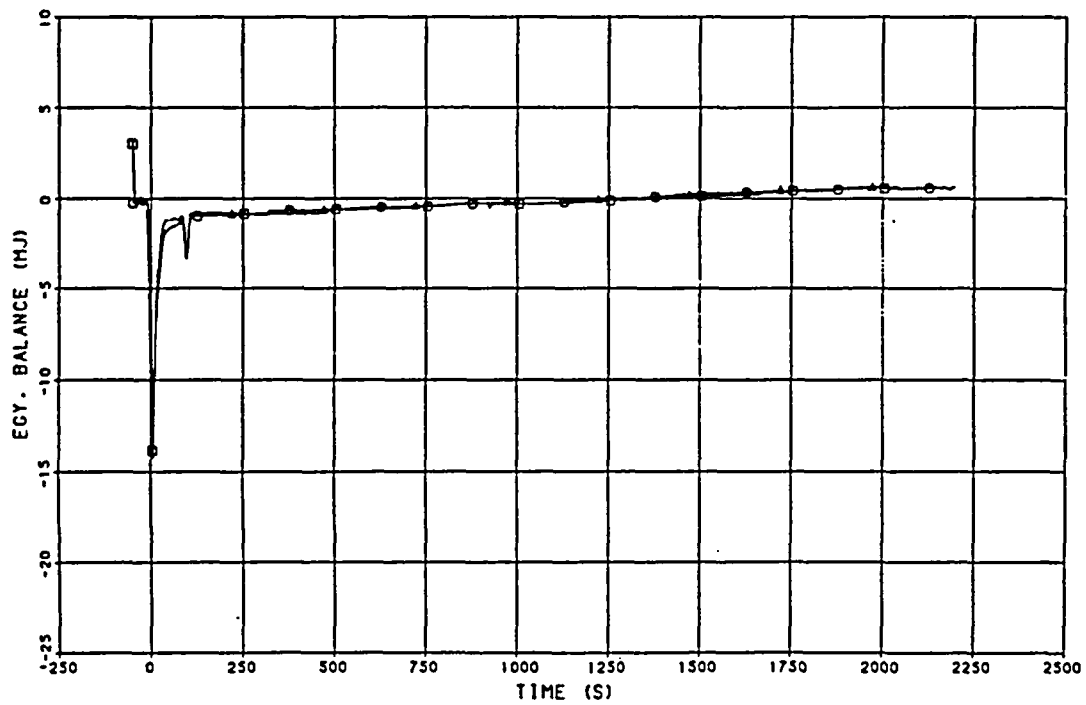
P.00 SYSTEM MASS BALANCE (CNTRLVAR 959) CASE A
SYSTEM MASS BALANCE (CNTRLVAR 959) CASE B
SYSTEM MASS BALANCE (CNTRLVAR 959) CASE C

Plot B.59



P.00 COOLANT ENERGY BALANCE (CNTRLVAR 960) CASE A
COOLANT ENERGY BALANCE (CNTRLVAR 960) CASE B
COOLANT ENERGY BALANCE (CNTRLVAR 960) CASE C

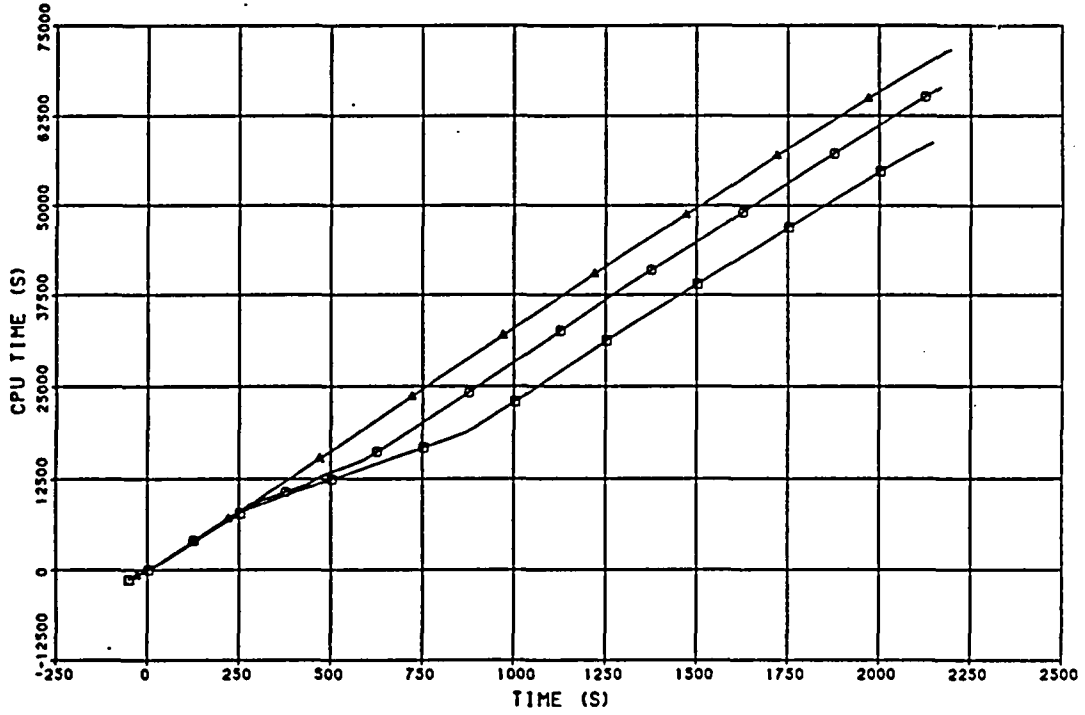
Plot B.60



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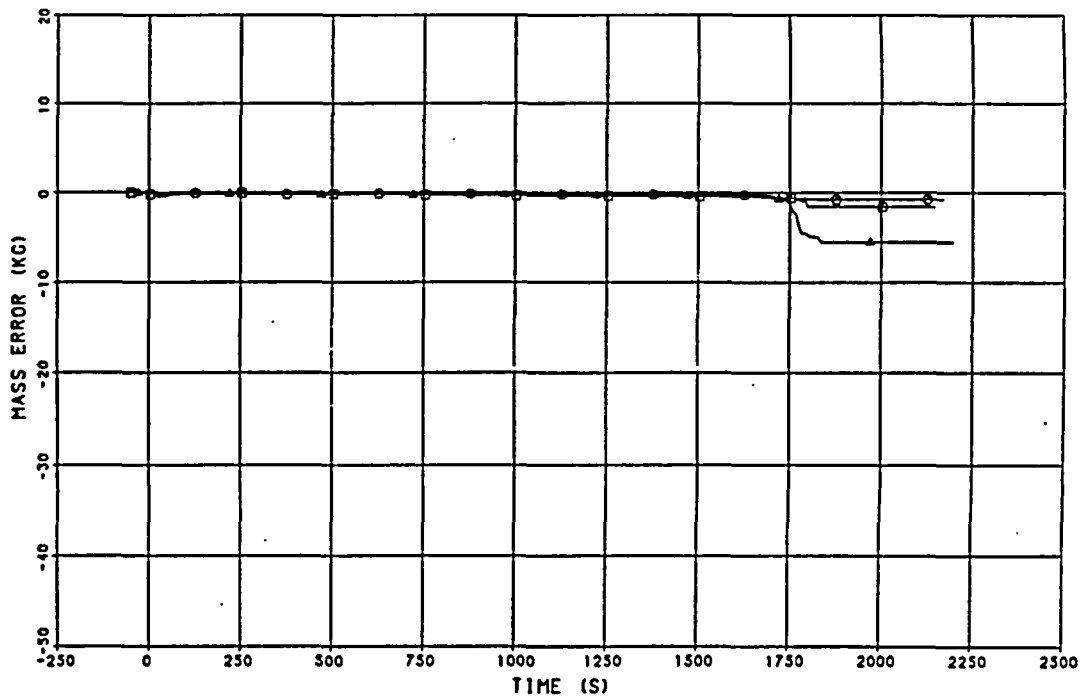
COMPUTATION CPU TIME (CPUTIME 0) CASE A
COMPUTATION CPU TIME (CPUTIME 0) CASE B
COMPUTATION CPU TIME (CPUTIME 0) CASE C

Plot B.61



COMPUTATION MASS ERROR (EMASS 0) CASE A
COMPUTATION MASS ERROR (EMASS 0) CASE B
COMPUTATION MASS ERROR (EMASS 0) CASE C

Plot B.62





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Case A

 CALCULATION-TO-EXPERIMENT DATA UNCERTAINTY ANALYSIS FOR NRC/ICAP.

FIRST LINE : DIFFERENCE BETWEEN CALCULATED AND (AVERAGED) EXPERIMENTAL DATA AT END OF THE INTERVAL
 SECOND LINE : MEAN DIFFERENCE OVER THE INTERVAL
 THIRD LINE : MEAN SIGMA OVER THE INTERVAL (ROOT MEAN SQUARE OF THE DIFFERENCE)

- CODES -	- - - - TIME INTERVAL - - - -							
	CALC. EXP.	0.0 - 20.00	- 80.00	- 200.0	- 500.0	- 1000.	- 1500.	- 2000.
C 3A - C 3X		-1.32 -2.39 2.69	-2.01 -1.47 1.52	-1.82 -1.90 1.90	-3.28 -2.19 2.24	-5.42 -4.20 4.24	-5.90 -5.44 5.44	-11.4 -7.87 8.04
C 4A - C 4X		-0.770 4.44 6.56	-1.27 -1.14 1.18	-1.37 -1.30 1.30	-2.55 -1.83 1.88	-4.96 -3.73 3.79	-5.24 -4.89 4.89	-10.7 -7.15 7.32
C 5A - C 5X		-0.240 2.75 4.24	-1.20 -0.607 .701	-1.55 -1.42 1.42	-2.84 -2.02 2.06	-5.34 -3.99 4.05	-5.39 -5.31 5.31	-10.9 -7.34 7.52
C 6A - C 6X		-0.570 3.76 5.87	-1.09 -0.817 .851	-1.14 -1.18 1.19	-2.60 -1.83 1.88	-5.24 -3.87 3.94	-5.67 -5.22 5.22	-11.1 -7.53 7.69
C 7A - C 7X		-1.98 -2.13 2.18	-1.22 -1.42 1.43	-1.50 -1.38 1.38	-2.91 -2.00 2.05	-5.42 -4.00 4.07	-5.89 -5.44 5.44	-11.4 -7.82 7.98
C 8A - C 8X		-1.90 -2.30 2.36	-1.48 -1.53 1.53	-1.51 -1.49 1.49	-3.05 -2.20 2.25	-5.45 -4.18 4.24	-5.29 -5.74 5.74	-11.9 -8.25 8.41
C 9A - C 9X		-3.60 -3.09 3.15	-3.51 -3.70 3.71	-4.32 -3.84 3.84	-5.82 -4.55 4.58	-8.01 -6.51 6.55	-8.73 -7.98 7.98	-14.1 -10.4 10.5
C AA - C AX		-.431 .647 1.35	.993 .176 .470	.556 .698 .733	.890E-01 .116 .198	-.632E-01 -.238E-01 .310	-.535 -.356 .398	-.437 -.456 .489
V 5A - V 5X		-2.80 -3.08 3.08	-4.93 -3.99 4.07	-4.64 -5.04 5.04	-5.82 -4.90 4.91	-8.28 -6.81 6.85	-8.62 -8.20 8.20	-13.4 -10.1 10.2
V 6A - V 6X		-3.06 -1.64 2.13	-3.03 -3.14 3.15	-3.84 -3.38 3.38	-5.13 -4.03 4.05	-7.44 -5.96 6.00	-9.02 -7.38 7.38	-13.5 -9.78 9.92
V 7A - V 7X		6.59 7.12 7.13	3.61 5.43 5.90	3.25 3.60 3.61	3.45 3.22 3.22	2.79 3.14 3.14	2.76 2.77 2.77	3.99 3.32 3.34
V 8A - V 8X		-3.14 -3.00 3.01	-4.85 -3.90 3.94	-4.47 -4.72 4.73	-5.45 -4.77 4.79	-7.11 -6.25 6.25	-7.23 -7.00 7.00	-12.6 -9.17 9.29
V 9A - V 9X		.601 .740 .763	.960E-01 .292 .425	.135E-01 .626E-01 .658E-01	-.107 -.369E-01 .518E-01	-.285 -.186 .194	-.231 -.247 .247	-.419 -.287 .293
V AA - V AX		.479 .618 .633	-.267E-01 .178 .354	-.107 -.568E-01 .610E-01	-.252 -.176 .182	-.437 -.341 .345	-.301 -.367 .370	-.517 -.378 .384
HL1A - HL1X		-31.5 -18.0 19.2	29.0 2.13 22.6	48.6 55.1 56.6	-72.4 -15.3 49.3	43.7 -48.9 80.2	42.0 58.2 58.8	-2.43 23.8 28.1
HL2A - HL2X		-29.2 -27.5 27.7	-12.0 -21.3 22.0	-31.2 -21.5 22.2	94.1 6.24 31.1	155. 20.0 111.	18.1 68.2 78.2	8.95 -4.46 8.91
HL4A - HL4X		-0.510 .651 1.51	0. -.995E-01 .212	-.570 -.262 .343	-1.93 -1.39 1.48	-5.18 -3.49 3.58	-5.64 -5.09 5.09	-11.6 -7.65 7.84
HL5A - HL5X		.580 .695 .708	.806E-01 .291 .421	.219E-01 .598E-01 .635E-01	-.114 -.558E-01 .705E-01	-.287 -.203 .208	-.201 -.235 .236	-.359 -.244 .249
CL1A - CL1X		-2.62 -13.7 16.3	-60.3 -38.7 45.7	6.02 -16.6 26.4	18.5 17.5 20.2	131. 70.6 79.1	42.7 76.7 79.5	1.18 11.3 15.8
CL2A - CL2X		744. 749. 749.	652. 700. 700.	586. 831. 831.	353. 460. 466.	190. 259. 273.	52.8 114. 121.	12.5 26.5 29.0
CL3A - CL3X		-5.17 -318 2.11	-2.03 -5.87 7.38	4.34 -1.11 7.02	167. 94.9 176.	-7.43 114. 136.	-15.1 -13.7 16.4	-5.18 -11.8 12.4
CL4A - CL4X		.252 .441 .475	-.916 -.655 .825	-1.72 -1.10 1.13	-3.15 -3.47 3.73	-.385 -1.33 1.64	-.837E-01 -.217 .241	-.686E-01 -.675E-01 .685E-01
CL6A - CL6X		-.360 -1.409 .503	-2.37 -1.30 1.54	-1.80 -2.25 2.25	-2.49 -2.00 2.02	-5.23 -3.74 3.82	-5.61 -5.22 5.22	-11.2 -7.64 7.81
CL7A - CL7X		.568 .697 .710	.105 .279 .402	.467E-01 .734E-01 .749E-01	-.164 -.672E-01 .964E-01	-.357 -.265 .271	-.298 -.321 .322	-.490 -.359 .364

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- CODES -		- - - - TIME INTERVAL - - - -						
CALC.	EXP.	0.0 - 20.00	- 80.00	- 200.0	- 500.0	- 1000.	- 1500.	- 2000.
CL8A - CL8X	.468 .617 .631	-.873E-01 .135 .348	-.187 -.122 .125	-.316 -.245 .248	-.534 -.395 .399	-.476 -.489 .489	-.669 -.533 .536	
CL9A - CL9X	-8.48 -1.60 3.03	-76.0 -43.6 51.6	-133. -88.6 90.4	-32.1 -71.8 84.4	-13.3 -17.6 18.8	-13.4 -14.0 14.0	-18.6 -16.7 16.8	
CLAA - CLAX	17.8 14.7 14.8	1.60 -.792 8.93	10.2 7.26 10.3	-14.9 -4.67 33.8	7.60 -11.8 12.3	-13.9 -12.8 13.1	-16.3 -13.6 13.7	
BR1A - BR1X	10.2 44.8 58.3	-32.0 -23.3 30.7	79.3 14.1 32.2	180. 101. 107.	127. 123. 126.	26.3 71.8 75.6	-2.32 13.9 18.0	
BR2A - BR2X	8.81 7.26 8.22	1.17 3.64 3.93	.404 .630 .768	.111E-01 .298 .384	-.236E-01 .204E-01 .179	-.471E-01 .279 .315	-.334 -.596E-01 .306	
BR4A - BR4X	-.370 -10.6 15.3	-1.82 -1.15 1.34	-1.82 -1.85 1.86	-2.02 -1.85 1.87	-4.42 -3.12 3.21	-5.25 -4.77 4.77	-11.3 -7.43 7.63	
BR5A - BR5X	4.43 15.6 19.7	2.14 3.12 3.68	.956 1.82 1.85	.842 .551 .561	.804 .672 .680	1.24 1.05 1.05	1.71 1.37 1.38	
BR6A - BR6X	.551 .781 .809	.344E-01 .232 .384	-.584E-01 -.374E-02 .267E-01	-.127 -.100 .103	-.293 -.213 .219	-.262 -.271 .271	-.474 -.333 .339	
SP1A - SP1X	-9.06 -9.22 9.42	-.510 -3.54 4.34	-.930 -.581 .682	-3.46 -1.83 1.98	-6.33 -4.50 4.60	-6.72 -6.56 6.57	-13.0 -9.20 9.35	
SP2A - SP2X	-7.42 -6.67 7.10	1.82 -1.79 3.22	1.99 2.34 2.38	1.97 2.57 2.60	1.84 2.39 2.42	1.60 2.26 2.27	3.67 2.60 2.65	
SP3A - SP3X	-4.49 -1.64 1.79	-70.5 -41.1 48.9	-77.5 -56.4 57.5	-18.5 -42.9 48.8	-15.7 -14.2 14.3	-16.2 -17.1 17.1	-20.0 -18.2 18.2	
SS3A - SS3X	-.820 -.528 .577	-.548 -.599 .600	-.578 -.562 .564	-.575 -.577 .577	-.513 -.566 .566	-.515 -.489 .489	-.626 -.572 .574	
SS4A - SS4X	15.0 11.4 11.8	-.940 5.88 7.91	-6.73 -3.64 4.09	-6.19 -7.55 7.57	-1.52 -4.17 4.48	2.00 1.53 1.96	-9.52 -1.72 3.63	
SS5A - SS5X	.101 -.210E-01 .647E-01	.130 .125 .128	.433E-01 .103 .112	-.165 -.662E-01 .902E-01	-.476 -.288 .300	-1.33 -.882 .918	-2.06 -1.75 1.77	
S 1A - S 1X	-24.1 -20.6 21.2	.429 -9.41 12.2	5.81 3.06 3.70	3.03 5.75 5.83	-5.19 -2.96 2.55	-9.63 -8.09 8.22	-3.34 -7.57 7.77	
P 1A - P 1X	.816E-01 .446E-01 .550E-01	.675E-01 .619E-01 .626E-01	.840E-01 .801E-01 .803E-01	.836E-01 .839E-01 .839E-01	.844E-01 .838E-01 .838E-01	.839E-01 .840E-01 .840E-01	.839E-01 .842E-01 .842E-01	
P 2A - P 2X	-20.1 -12.0 12.9	-2.15 -14.0 16.8	-9.29 -4.86 5.28	-34.9 -23.1 24.2	-55.6 -46.5 46.8	-71.5 -63.4 63.5	-93.9 -82.0 82.2	
P 3A - P 3X	-19.8 -13.3 14.0	2.07 -12.2 15.9	5.16 4.12 4.29	-6.62 -1.94 3.53	-21.6 -14.4 15.0	-33.5 -27.6 27.8	-45.5 -39.4 39.5	
P 4A - P 4X	.337 .300 .308	-.152E-01 .179 .344	-.985E-01 -.417E-01 .474E-01	-.266 -.178 .185	-.442 -.347 .351	-.387 -.405 .405	-.575 -.442 .446	
EC1A - EC1X	-.870E-03 -.135 .161	-.557E-01 .201E-03 .538E-01	-.259E-01 -.386E-01 .393E-01	-.198E-01 -.454E-02 .134E-01	.284E-01 .282E-01 .299E-01	.718E-02 .215E-01 .245E-01	.606E-01 .322E-01 .348E-01	

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Case B

 CALCULATION-TO-EXPERIMENT DATA UNCERTAINTY ANALYSIS FOR NRC/ICAP.

FIRST LINE : DIFFERENCE BETWEEN CALCULATED AND (AVERAGED) EXPERIMENTAL DATA AT END OF THE INTERVAL
 SECOND LINE : MEAN DIFFERENCE OVER THE INTERVAL
 THIRD LINE : MEAN SIGMA OVER THE INTERVAL (ROOT MEAN SQUARE OF THE DIFFERENCE)

- CODES -	- - - - TIME INTERVAL - - - -								
	CALC.	EXP.	0.0 - 20.00	- 80.00	- 200.0	- 500.0	- 1000.	- 1500.	- 2000.
C 3B - C 3X	.600E-01	-1.98	-1.86	-3.43	-5.95	-4.71	-7.84		
	-.206	-.957	-1.81	-2.29	-4.92	-5.16	-5.33		
	1.22	1.22	1.81	2.34	4.97	5.17	5.40		
C 4B - C 4X	.600	-1.25	-1.42	-2.81	-5.50	-4.05	-7.13		
	6.57	-.639	-1.22	-1.94	-4.46	-4.62	-4.62		
	8.25	.924	1.22	1.99	4.53	4.64	4.70		
C 5B - C 5X	1.12	-1.18	-1.61	-2.99	-5.87	-4.20	-7.34		
	4.85	-.105	-1.34	-2.12	-4.72	-5.03	-4.81		
	5.92	.745	1.34	2.17	4.79	5.05	4.89		
C 6B - C 6X	.790	-1.09	-1.20	-2.77	-5.78	-4.49	-7.51		
	5.82	-.320	-1.11	-1.94	-4.51	-4.95	-4.99		
	7.41	.708	1.11	1.99	4.59	4.96	5.06		
C 7B - C 7X	-.600	-1.22	-1.56	-3.06	-5.95	-4.71	-7.85		
	-.300E-01	-.923	-1.30	-2.11	-4.73	-5.16	-5.29		
	.639	.964	1.31	2.16	4.81	5.17	5.37		
C 8B - C 8X	-.500	-1.45	-1.56	-3.21	-5.98	-5.10	-8.38		
	-.199	-1.01	-1.41	-2.31	-4.91	-5.46	-5.70		
	.684	1.07	1.41	2.35	4.99	5.48	5.77		
C 9B - C 9X	-2.24	-3.50	-4.37	-5.99	-9.54	-7.54	-10.5		
	-.975	-3.21	-3.76	-4.65	-7.24	-7.70	-7.84		
	1.32	3.25	3.77	4.68	7.29	7.71	7.89		
C AB - C AX	-.343	.977	.558	.849E-01	-.641E-01	-.535	-.424		
	.546	.190	.693	.101	-.483E-01	-.357	-.446		
	1.27	.462	.730	.189	.289	.400	.480		
V 5B - V 5X	-1.51	-4.91	-4.72	-5.00	-8.82	-7.43	-9.73		
	-1.22	-3.56	-4.95	-5.01	-7.54	-7.94	-7.55		
	1.25	3.75	4.95	5.03	7.59	7.95	7.59		
V 6B - V 6X	-1.64	-3.02	-3.89	-5.30	-7.98	-6.83	-9.81		
	-.539	-2.63	-3.30	-4.13	-6.69	-7.10	-7.21		
	1.74	2.70	3.30	4.16	6.74	7.12	7.27		
V 7B - V 7X	5.16	3.60	3.24	3.46	2.78	2.76	3.98		
	5.25	5.11	3.59	3.22	3.14	2.77	3.32		
	5.27	5.45	3.60	3.22	3.14	2.77	3.34		
V 8B - V 8X	-1.80	-4.83	-4.52	-5.52	-7.64	-6.04	-8.94		
	-.817	-3.40	-4.54	-4.85	-6.95	-6.73	-6.51		
	.959	3.53	4.54	4.88	6.98	6.75	6.65		
V 9B - V 9X	.592	.954E-01	.750E-02	-.123	-.330	-.154	-.246		
	.781	.310	.698E-01	-.474E-01	-.251	-.230	-.146		
	.798	.433	.745E-01	.617E-01	.259	.236	.149		
V AB - V AX	.459	-.270E-01	-.113	-.258	-.481	-.224	-.345		
	.558	.195	-.494E-01	-.185	-.405	-.349	-.237		
	.578	.359	.574E-01	.192	.410	.350	.240		
HL1B - HL1X	-34.4	28.0	47.4	-76.3	50.2	42.6	13.0		
	-22.0	-246	54.9	-15.5	-50.1	63.0	25.9		
	22.9	22.3	55.5	48.5	86.0	63.6	29.1		
HL2B - HL2X	-32.1	-14.9	-32.1	92.8	159.	19.7	10.2		
	-30.3	-24.3	-23.2	5.79	15.7	73.0	-3.06		
	30.5	24.9	23.8	31.2	116.	83.3	8.51		
HL4B - HL4X	.990	.200E-01	-.520	-2.10	-5.70	-4.45	-7.90		
	2.58	.433	-.181	-1.50	-4.23	-4.81	-5.08		
	3.08	.574	.327	1.59	4.32	4.83	5.17		
HL5B - HL5X	.570	.794E-01	.137E-01	-.130	-.332	-.123	-.185		
	.735	.305	.621E-01	-.666E-01	-.258	-.218	-.103		
	.751	.428	.671E-01	.810E-01	.274	.226	.106		
CL1B - CL1X	-4.95	-51.0	5.69	7.68	137.	44.4	3.77		
	-17.1	-39.5	-17.5	18.0	68.7	79.8	14.7		
	19.4	45.6	27.7	21.8	80.4	83.8	18.8		
CL2B - CL2X	742.	651.	585.	344.	195.	54.8	14.3		
	745.	699.	630.	451.	270.	117.	28.5		
	745.	700.	630.	457.	273.	124.	30.8		
CL3B - CL3X	-9.09	-2.57	3.23	175.	-8.19	-14.7	-5.21		
	-3.95	-7.95	-1.55	68.7	101.	-13.6	-11.1		
	4.55	8.85	7.08	121.	123.	15.3	11.8		
CL4B - CL4X	.285	-.540	-1.57	-3.25	-.370	-.698E-01	-.585E-01		
	.479	-.459	-.805	-3.45	-1.44	-.178	-.618E-01		
	.512	.524	.873	3.73	1.63	.215	.629E-01		
CL5B - CL5X	.820	-2.35	-1.99	-2.67	-5.77	-4.42	-7.63		
	1.43	-.855	-2.17	-2.12	-4.48	-4.95	-5.10		
	1.48	1.45	2.18	2.14	4.57	4.97	5.18		
CL7B - CL7X	.557	.107	.385E-01	-.180	-.402	-.221	-.317		
	.735	.300	.819E-01	-.792E-01	-.332	-.305	-.217		
	.755	.412	.848E-01	.107	.339	.310	.		

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- CODES -		- - - - TIME INTERVAL - - - -						
CALC.	EXP.	0.0 - 20.00	- 80.00	- 200.0	- 500.0	- 1000.	- 1500.	- 2000.
CL8B - CL8X	.451 .650 .669	-.937E-01 .146 .347	-.195 -.120 .124	-.333 -.257 .260	-.579 -.460 .465	-.399 -.471 .474	-.497 -.392 .393	
CL9B - CL9X	-13.6 -7.58 7.86	-81.2 -50.0 55.7	-130. -90.4 91.9	-31.6 -71.6 83.8	-12.9 -14.9 16.2	-12.9 -13.5 13.5	-18.3 -16.2 16.3	
CLAB - CLAX	17.8 14.7 14.8	1.60 -.792 8.93	10.2 7.26 10.3	-14.9 -4.67 33.8	7.60 -11.8 12.3	-13.9 -12.5 13.1	-16.3 -13.6 13.7	
BR1B - BR1X	7.85 42.3 57.0	-33.7 -24.5 31.0	80.3 13.0 32.3	164. 102. 109.	131. 121. 122.	26.7 75.1 79.1	.810 16.6 19.6	
BR2B - BR2X	8.59 7.08 8.02	2.04 3.51 3.86	.398 .572 .688	.232 .353 .506	-.575E-01 -.187E-01 .149	-.187 .206 .254	-.260 -.207E-01 .285	
BR4B - BR4X	.810 -9.29 14.8	-1.83 -7.37 1.25	-1.61 -1.78 1.78	-2.19 -1.68 1.70	-4.94 -3.85 3.95	-4.02 -4.46 4.48	-7.63 -4.86 4.96	
BR5B - BR5X	3.19 14.5 19.3	1.91 2.82 3.25	.975 1.78 1.82	.535 .548 .558	.803 .679 .686	1.24 1.05 1.05	1.72 1.37 1.38	
BR6B - BR6X	.543 .821 .855	.850E-02 .245 .390	-.660E-01 .415E-03 .330E-01	-.143 -.113 .117	-.335 -.277 .283	-.182 -.252 .257	-.300 -.192 .196	
SP1B - SP1X	-7.52 -7.33 7.58	-.480 -3.01 3.66	-.980 -4.89 .602	-3.63 -1.94 2.09	-6.87 -5.24 5.34	-5.52 -6.29 6.30	-9.36 -6.63 6.70	
SP2B - SP2X	-6.99 -6.88 7.13	1.83 -1.66 3.05	2.02 2.35 2.39	1.96 2.58 2.61	1.84 2.40 2.42	1.60 2.25 2.27	3.67 2.60 2.65	
SP3B - SP3X	-3.15 -6.89 .954	-76.9 -51.5 57.6	-80.3 -71.3 71.5	-18.2 -41.9 48.0	-15.5 -13.0 13.2	-15.9 -16.9 16.9	-19.4 -17.5 17.6	
SS3B - SS3X	-.341 -1.177 -.249	-.117 -1.152 .162	-.106 -.111 .115	-.141 -.125 .125	-.207 -.169 .170	-.297 -.234 .235	-.370 -.321 .323	
SS4B - SS4X	8.56 4.93 5.64	.540 3.50 4.37	-2.00 -1.35 1.46	-1.86 -2.84 2.87	1.63 .574 1.65	3.26 2.77 2.84	-6.27 1.33 3.04	
SS5B - SS5X	.147 .815E-01 .837E-01	.128 .131 .131	.306E-01 .108 .121	-.182 -.794E-01 .102	-.517 -.351 .362	-1.24 -.857 .883	-1.90 -1.58 1.60	
S 1B - S 1X	-16.1 -12.3 13.1	-1.02 -6.51 8.02	1.03 .862 1.09	-1.46 .921 1.25	-8.88 -5.78 6.27	-9.70 -9.06 9.08	-2.94 -8.05 8.27	
P 1B - P 1X	.837E-01 .568E-01 .636E-01	.672E-01 .619E-01 .627E-01	.839E-01 .800E-01 .801E-01	.836E-01 .838E-01 .838E-01	.844E-01 .838E-01 .838E-01	.839E-01 .840E-01 .840E-01	.839E-01 .842E-01 .842E-01	
P 2B - P 2X	-20.1 -11.8 12.7	-2.14 -13.8 16.6	-9.35 -4.77 5.22	-35.1 -23.2 24.3	-56.2 -47.2 47.6	-70.3 -63.1 63.2	-90.2 -79.4 79.6	
P 3B - P 3X	-19.7 -13.0 13.7	1.74 -12.1 16.8	4.76 3.96 4.13	-6.88 -4.89 3.52	-21.5 -15.1 15.6	-32.2 -26.7 26.8	-44.0 -37.6 37.8	
P 4B - P 4X	.341 .349 .353	-.144E-01 .200 .349	-.105 -.329E-01 .439E-01	-.281 -.189 .196	-.486 -.412 .417	-.310 -.388 .391	-.402 -.301 .303	
EC1B - EC1X	-.870E-03 -.135 .161	-.558E-01 -.107E-02 .532E-01	-.255E-01 -.392E-01 .399E-01	-.209E-01 -.392E-02 .134E-01	.310E-01 .320E-01 .335E-01	.259E-02 .205E-01 .237E-01	.504E-01 .239E-01 .267E-01	

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Case C

 CALCULATION-TO-EXPERIMENT DATA UNCERTAINTY ANALYSIS FOR NRC/ICAP.

FIRST LINE : DIFFERENCE BETWEEN CALCULATED AND (AVERAGED) EXPERIMENTAL DATA AT END OF THE INTERVAL
 SECOND LINE : MEAN DIFFERENCE OVER THE INTERVAL
 THIRD LINE : MEAN SIGMA OVER THE INTERVAL (ROOT MEAN SQUARE OF THE DIFFERENCE)

- CODES -		- - - - TIME INTERVAL - - - -						
CALC.	EXP.	0.0 - 20.00	- 80.00	- 200.0	- 500.0	- 1000.	- 1500.	- 2000.
C 3C - C 3X		.100E-01 -2.260 1.21	-2.01 -.947 1.21	-1.99 -1.92 1.92	-3.94 -2.89 2.67	-6.62 -5.44 6.48	-5.17 -5.73 5.74	-8.11 -5.80 5.86
C 4C - C 4X		.650 6.51 8.22	-1.27 -.630 .911	-1.49 -1.31 1.31	-3.32 -2.24 2.32	-6.06 -4.98 5.04	-4.62 -5.19 5.21	-7.43 -5.08 5.15
C 5C - C 5X		1.07 4.80 5.89	-1.19 -.908E-01 .733	-1.66 -1.41 1.42	-3.60 -2.42 2.49	-6.44 -5.24 5.30	-4.67 -5.61 5.63	-7.60 -5.27 5.34
C 6C - C 6X		.750 5.77 7.39	-1.08 -.299 .683	-1.23 -1.16 1.17	-3.28 -2.23 2.31	-6.35 -5.13 5.20	-4.96 -5.52 5.54	-7.77 -5.46 5.52
C 7C - C 7X		-.650 -.812E-01 .666	-1.18 -.896 .929	-1.58 -1.36 1.36	-3.57 -2.40 2.47	-6.52 -5.25 5.32	-5.17 -5.74 5.75	-8.11 -5.75 5.82
C 8C - C 8X		-.650 -.247 .699	-1.46 -.986 1.04	-1.47 -1.42 1.43	-3.69 -2.65 2.63	-6.64 -5.42 5.49	-5.66 -6.02 6.03	-8.66 -6.16 6.22
C 9C - C 9X		-2.29 -1.03 1.38	-3.47 -3.17 3.21	-4.31 -3.77 3.78	-6.45 -4.88 4.93	-9.09 -7.76 7.80	-7.98 -8.24 8.25	-10.8 -8.30 8.35
C AC - C AX		-.352 .649 1.27	1.00 .207 .486	.744 .788 .814	.767E-01 .197 .278	-.650E-01 -.554E-01 .295	-.537 -.357 .399	-.425 -.449 .482
V 5C - V 5X		-1.64 -1.19 1.22	-4.96 -3.56 3.75	-5.06 -5.16 5.16	-6.50 -5.41 5.42	-9.37 -8.06 8.11	-7.97 -8.44 8.46	-10.0 -8.02 8.05
V 6C - V 6X		-1.69 .495 1.76	-3.00 -2.60 2.67	-3.81 -3.31 3.31	-5.76 -4.35 4.40	-8.53 -7.20 7.26	-7.27 -7.65 7.66	-10.1 -7.68 7.73
V 7C - V 7X		5.17 5.28 5.31	3.74 5.13 5.47	3.36 3.70 3.70	3.45 3.24 3.24	2.78 3.14 3.14	2.75 2.77 2.77	3.98 3.32 3.34
V 8C - V 8X		-1.85 -.869 1.01	-4.85 -3.39 3.52	-4.63 -4.74 4.74	-6.08 -5.15 5.19	-8.19 -7.46 7.48	-6.48 -7.27 7.29	-9.23 -7.07 7.11
V 9C - V 9X		.587 .779 .798	.113 .316 .434	.232E-01 .777E-01 .812E-01	-.167 -.689E-01 .802E-01	-.375 -.257 .303	-.183 -.270 .276	-.261 -.173 .176
V AC - V AX		.464 .656 .678	-.570E-02 .204 .358	-.805E-01 -.323E-01 .401E-01	-.310 -.200 .213	-.526 -.451 .455	-.253 -.390 .400	-.360 -.264 .266
HL1C - HL1X		-34.3 -21.9 22.8	28.2 .208 22.7	49.1 55.4 56.0	-73.5 -18.6 62.9	47.7 -53.6 87.6	38.2 58.1 58.6	10.5 23.7 27.3
HL2C - HL2X		-32.1 -30.3 30.8	-14.9 -24.3 24.9	-32.3 -23.3 24.0	-239. -19.9 65.0	157. -840 121.	17.0 66.5 76.2	9.98 -3.62 8.36
HL4C - HL4X		.940 2.64 3.05	.600E-01 .464 .675	-.600 -.173 .320	-2.57 -1.75 1.69	-6.25 -4.74 4.82	-4.90 -5.36 5.38	-8.20 -5.55 5.62
HL6C - HL6X		.565 .733 .750	.103 .313 .429	.187E-01 .705E-01 .782E-01	-.176 -.926E-01 .111	-.378 -.314 .319	-.153 -.259 .267	-.201 -.130 .132
CL1C - CL1X		-4.92 -17.2 19.4	-65.0 -41.1 47.7	-8.92 -26.3 32.3	11.0 8.88 16.0	133. 65.2 77.2	43.5 76.2 79.4	4.39 15.2 18.4
CL2C - CL2X		742. 745. 745.	657. 698. 699.	568. 621. 621.	364. 457. 461.	197. 275. 278.	85.7 123. 130.	14.1 28.1 30.4
CL3C - CL3X		-9.04 -3.95 4.55	-2.75 -7.96 8.88	-4.70 -2.07 6.67	202. 67.6 145.	-6.53 104. 126.	-14.8 -13.7 15.4	-5.27 -11.2 11.9
CL4C - CL4X		.285 .479 .513	-.787 -.509 .661	-.605 -.549 .665	-3.08 -3.18 3.61	-.381 -1.22 1.47	-.835E-01 -.228 .254	-.594E-01 -.623E-01 .636E-01
CL6C - CL6X		.790 1.45 1.50	-2.41 -.880 1.46	-2.39 -2.39 2.39	-3.17 -2.54 2.56	-6.32 -4.99 5.07	-4.83 -5.42 5.44	-7.95 -5.58 5.64
CL7C - CL7X		.552 .734 .765	.975E-01 .299 .411	-.170E-01 .526E-01 .627E-01	-.232 -.131 .147	-.449 -.380 .386	-.252 -.348 .353	-.332 -.246 .247

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- CODES -		- - - - TIME INTERVAL - - - -						
CALC.	EXP.	0.0 - 20.00	- 80.00	- 200.0	- 500.0	- 1000.	- 1500.	- 2000.
CL8C - CL8X	.446 .648 .670	-.715E-01 .155 .345	-.153 -.981E-01 .101	-.375 -.266 .275	-.624 -.505 .509	-.428 -.512 .515	-.512 -.419 .420	-.512 -.419 .420
CL9C - CL9X	-13.6 -7.63 7.90	-52.5 -40.5 44.2	-27.4 -38.9 40.7	-23.1 -27.5 28.9	-10.1 -11.5 13.1	-11.1 -9.95 9.97	-18.2 -15.9 15.0	-18.2 -15.9 15.0
CLAC - CLAX	17.8 14.7 14.8	1.60 -.792 8.93	10.2 7.26 10.3	-14.9 -4.67 33.8	7.60 -11.8 12.3	-13.9 -12.5 13.1	-16.3 -13.6 13.7	-16.3 -13.6 13.7
BR1C - BR1X	7.89 42.2 57.0	-38.3 -25.8 32.5	65.8 4.87 27.8	157. 88.4 95.8	128. 117. 119.	27.2 73.2 76.7	1.27 17.1 20.3	1.27 17.1 20.3
BR2C - BR2X	8.59 7.08 8.01	2.31 3.54 3.89	.427 .653 .774	.243 .500 .522	-6.06E-01 -.481E-01 .159	-.245E-01 .286 .325	-.252 -.529E-02 .288	-.252 -.529E-02 .288
BR4C - BR4X	.780 -9.27 14.8	-1.88 -.734 1.25	-1.95 -1.98 1.98	-2.65 -2.02 2.05	-5.49 -4.36 4.45	-4.52 -5.03 5.04	-7.92 -5.33 5.41	-7.92 -5.33 5.41
BR5C - BR5X	3.18 14.5 19.3	2.09 2.89 3.29	1.70 2.15 2.17	.545 .765 .863	.804 .685 .693	1.24 1.05 1.05	1.72 1.37 1.38	1.72 1.37 1.38
BR6C - BR6X	.538 .819 .855	.228E-01 .253 .390	-.263E-01 -.193E-01 -.312E-01	-.185 -.125 .136	-.381 -.322 .327	-.215 -.294 .298	-.314 -.219 .222	-.314 -.219 .222
SP1C - SP1X	-7.55 -7.37 7.62	-.450 -2.98 3.65	-1.01 -.525 .630	-4.12 -2.24 2.41	-7.43 -5.75 5.85	-5.98 -6.84 6.85	-9.65 -7.10 7.15	-9.65 -7.10 7.15
SP2C - SP2X	-6.99 -6.82 7.07	1.83 -1.66 3.06	2.14 2.41 2.45	1.99 2.65 2.67	1.85 2.41 2.43	1.61 2.26 2.29	3.67 2.60 2.65	3.67 2.60 2.65
SP3C - SP3X	-3.18 -.721 -.990	-28.7 -39.9 44.9	-22.4 -25.9 28.1	-12.9 -17.3 17.8	-13.7 -11.0 11.2	-14.5 -14.5 14.5	-19.4 -17.3 17.4	-19.4 -17.3 17.4
SS3C - SS3X	-.341 -.181 .250	-.117 -.153 .162	-.105 -.111 .115	-.138 -.122 .123	-.208 -.169 .170	-.268 -.236 .236	-.369 -.319 .321	-.369 -.319 .321
SS4C - SS4X	8.50 4.91 5.62	.360 3.19 4.18	-1.91 -1.35 1.43	-.590 -1.95 2.00	1.08 .694 1.07	2.83 2.21 2.28	-6.55 .819 2.82	-6.55 .819 2.82
SS5C - SS5X	.145 .635E-01 .680E-01	.132 .134 .134	.223E-01 .101 .115	-.227 -.109 .132	-.563 -.396 .406	-1.27 -.899 .923	-1.92 -1.61 1.63	-1.92 -1.61 1.63
S 1C - S 1X	-16.1 -12.3 13.1	-.806 -6.17 7.82	.912 .821 1.01	-3.23 -2.64 1.24	-8.88 -6.42 6.66	-9.72 -9.05 9.07	-2.86 -8.00 8.22	-2.86 -8.00 8.22
P 1C - P 1X	.826E-01 .559E-01 .626E-01	.671E-01 .618E-01 .625E-01	.839E-01 .800E-01 .801E-01	.835E-01 .835E-01 .838E-01	.844E-01 .838E-01 .838E-01	.839E-01 .840E-01 .840E-01	.839E-01 .842E-01 .842E-01	.839E-01 .842E-01 .842E-01
P 2C - P 2X	-20.1 -11.8 12.8	-2.03 -13.8 16.6	-9.24 -4.73 5.18	-35.6 -23.4 24.6	-55.7 -47.7 48.1	-70.8 -63.7 63.8	-90.5 -79.9 80.1	-90.5 -79.9 80.1
P 3C - P 3X	-19.8 -13.0 13.8	1.90 -12.0 15.7	4.92 3.99 4.15	-7.42 -.836 3.76	-21.7 -15.4 15.8	-32.0 -25.7 25.9	-43.7 -37.6 37.7	-43.7 -37.6 37.7
P 4C - P 4X	.336 .345 .349	-.280E-02 .205 .348	-.931E-01 -.287E-01 .397E-01	-.327 -.212 .223	-.531 -.458 .462	-.339 -.428 .432	-.417 -.328 .329	-.417 -.328 .329
EC1C - EC1X	-.670E-03 -.135 .161	-.665E-01 -.148E-02 .533E-01	-.275E-01 -.400E-01 .407E-01	.234E-01 -.318E-02 .146E-01	.336E-01 .346E-01 .361E-01	.430E-02 .228E-01 .258E-01	.513E-01 .255E-01 .280E-01	.513E-01 .255E-01 .280E-01

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STUDSVIK

THIS TAPE CONTAINS DATA FROM THE ICAP PREDICTION CALCULATION
WITH THE RELAP5/MOD2/36.04 FOR THE LOFT EXPERIMENT NO. L3-6.

CONTENTS, FILE	1.	THIS DESCRIPTIVE TEXT
	2.	INPUT CASE A, STEADY STATE
	3.	- " - B, - " - , UPDATES
	4.	- " - C, - " - , UPDATES TO A + B
	5.	DATA, EXPERIMENT
	6.	-"- , CASE A
	7.	-"- , CASE B
	8.	-"- , CASE C

I. COMPUTER	
NAME	CYBER 170-810
WORD SIZE	60

II. TAPE FORMAT	
NUMBER OF TRACKS	9
PACKING DENSITY	1600 BPI
RECORD SIZE	80
BLOCKING FACTOR	64
CODED	EBCDIC
CONTROL WORDS	NO

III. DATA FORMAT, FOR EACH OF THE FILES 5 THROUGH 8

TITLE RECORD(S), (FORMAT I5,A75)
FIELD 1, THE NUMBER OF DATA CHANNELS ON THE FILE
FIELD 2, PROBLEM IDENTIFICATION
UP TO FIVE ADDITIONAL IDENTIFICATION RECORDS
MAY BE ADDED BY 'C' IN COLUMN 1 OF FIELD 1

DATA SET RECORD 1, (FORMAT 2I5,A60)
FIELD 1, NUMBER OF DATA POINTS
FIELD 2, THE ENGINEERING UNIT CODE (EUC) FOR THE
VARIABLE
FIELD 3, IDENTIFYING TEXT OF THE DATA
REMAINING DATA SET RECORDS FORMAT 5(E16.9)

EACH DATA CHANNEL SUBMITTED IS GIVEN THROUGH TWO DATA
SETS, THE FIRST OF WHICH IS THE TIME DATA SET.
THE TWO SETS HAVE THE SAME NUMBER OF DATA POINTS.
THE TIME DATA SET IS IDENTIFIED BY EUC=77 (FIELD 2)
AND THE IDENTIFYING TEXT 'TIME' (FIELD 3).



BIBLIOGRAPHIC DATA SHEET

(See instructions on the reverse)

1. REPORT NUMBER
(Assigned by NRC, Add Vol., Supp., Rev.,
and Addendum Numbers, if any.)

NUREG/IA-0033

STUDSVIK/NP-87/128

2. TITLE AND SUBTITLE

Assessment of RELAP5/MOD2, Cycle 36.04
Against LOFT Small Break Experiment L3-6

3. DATE REPORT PUBLISHED

MONTH | YEAR
July | 1990

4. FIN OR GRANT NUMBER

N/A

5. AUTHOR(S)

John Eriksson

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Sweden

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Washington, DC 20555

10. SUPPLEMENTARY NOTES

11. ABSTRACT (200 words or less)

The LOFT small break experiment L3-6 has been analyzed as part of Sweden's contribution to the International Thermal-Hydraulic Code Assessment and Applications Program (ICAP).

Three calculations, of which two were sensitivity studies, were carried out. The following quantities were varied:

- the content of secondary side fluid and the feed water valve closure
- the two-phase characteristics of the main pumps

All three predictions agreed reasonably well with most of the measured data. The sensitivity calculations resulted only in marginal improvements.

The predicted and measured data are compared on plots and their differences are quantified over intervals in real time.

12. KEY WORDS/DESCRIPTORS (List words or phrases that will assist researchers in locating the report.)

RELAP5/MOD2/ Cycle 36.04 Against LOFT Small Break
Experiment L3-6

13. AVAILABILITY STATEMENT

Unlimited

14. SECURITY CLASSIFICATION

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Unclassified

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