



International Agreement Report

Assessment of RELAP5/MOD3 With the LOFT L9-1/L3-3 Experiment Simulating an Anticipated Transient With Multiple Failures

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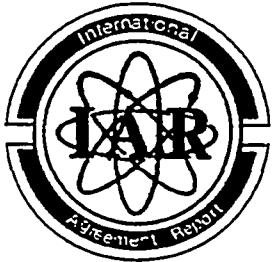
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Assessment of RELAP5/MOD3 with the LOFT L9-1/L3-3 Experiment
Simulating an Anticipated Transient with Multiple Failures

Abstract

The RELAP5/MOD3 5m5 code is assessed using the L9-1/L3-3 test carried out in the LOFT facility, a 1/60-scaled experimental reactor, simulating a loss of feedwater accident with multiple failures and the sequentially-induced small break loss-of-coolant accident. The code predictability is evaluated for the four separated sub-periods with respect to the system response; initial heatup phase, spray and power operated relief valve(PORV) cycling phase, blowdown phase and recovery phase. Based on the comparisons of the results from the calculation with the experiment data, it is shown that the overall thermal-hydraulic behavior important to the scenario such as a heat removal between the primary side and the secondary side and a system depressurization can be well-predicted and that the code could be applied to the full-scale nuclear power plant for an anticipated transient with multiple failures within a reasonable accuracy. The minor discrepancies between the prediction and the experiment are identified in reactor scram time, post-scram behavior in the initial heatup phase, excessive heatup rate in the cycling phase, insufficient energy convected out the PORV under the hot leg stratified condition in the saturated blowdown phase and void distribution in secondary side in the recovery phase. This may come from the code uncertainties in predicting the spray mass flow rate, the associated condensation in pressurizer and junction fluid density under stratified condition.

Executive Summary

This report presents the RELAP5/MOD3 code assessment calculation using the test L9-1/L3-3 conducted in the loss of fluid test(LOFT) facility. The LOFT facility was a 1/60-scaled experimental reactor. The experiment L9-1/L3-3 simulated a loss of feedwater accident(LOFA) with multiple failures and a consequentially-induced small break loss of coolant accident(LOCA).

The full period of the test was separated with four sub-periods according to the thermal-hydraulic characteristics ; the initial heatup phase, the spray and power operated relief valve(PORV) cycling phase, the blowdown phase and the recovery phase.

RELAP5/MOD3 calculation successfully simulated the complex sequence of events associated with a LOFA and a consequential LOCA. Based on the comparisons between the calculation results and the experiment data, the overall behavior such as a subcooled heatup and a depressurization in the primary coolant system, and a heat removal after the dryout in steam generator secondary side was well-predicted throughout the four sub-periods. However, the calculation results show the reactor scram earlier than the experiment, resulting in the overestimation of the post-scram cooling, which may due to a code uncertainty in the spray mass flow rate and the associated condensation in the pressurizer. Due to this difference, the predicted initiation and completion times were somewhat delayed. The excessive heatup rate was also found in the spray cycling phase, which may come from the overprediction of discharged flow rate through the PORV during the blowdown phase. And the RELAP5/MOD3 predicted an inaccurate junction fluid density under the hot leg stratified, which resulted in an insufficient energy convected out the PORV. This caused an overprediction in primary system pressure and temperature during the saturated blowdown phase. In the recovery phase, the RELAP5/MOD3 calculation yields an inaccurate void distribution in the SG secondary side. It may be ascribed to the overprediction of the pressure and temperature drop in primary coolant system.

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1. Introduction

The RELAP5/MOD3 code [1] was developed by the Idaho National Engineering Laboratory (INEL) under the sponsorship of US Nuclear Regulatory Commission (NRC), and its frozen version, 5m5 was released at the end of 1990. Through the developmental assessments conducted [2], the code capability was investigated, however, the code predictability for such transients as an anticipated transient with multiple failures was not fully demonstrated. This report summarizes a code assessment using the typical experiment simulating this type of transient, the L9-1/L3-3 [3] conducted in the Loss-of-Fluid-Test (LOFT) facility [4]. The test L9-1/L3-3 composed of two sequential tests; L9-1 and L3-3, which simulated a loss of feedwater accident (LOFA) with multiple failures and a consequentially-induced small break loss of coolant accident (SBLOCA) in pressurized water reactor (PWR), respectively.

The major objective of this study was to identify the code capability of the RELAP5/MOD3 5m5 on the prediction of thermal-hydraulic (TH) behavior in primary coolant system (PCS) and secondary coolant system (SCS) during the LOFA with multiple failures and the consequentially-induced LOCA. To achieve this objective, the full period of the test L9-1/L3-3 was separated with four sub-periods with respect to the system response on the accident ; the initial heatup phase, the spray and power operated relief valve(PORV) cycling phase, the blowdown phase and the recovery phase. The programmatic objectives of this study are :

1. to provide RELAP5/MOD3 simulation of the test L9-1/L3-3 for demonstrating the code applicability to this kind of transient in full-scale PWR,
2. to evaluate the accuracy and the discrepancy of the code in predicting the following TH phenomena during the four sub-periods based on the comparison with the experiment,
 - Steam generator (SG) secondary side dry out after a LOFA
 - Post-scram PCS cooling

- PCS heatup in subcooled state and pressurizer liquid level swell
 - Pressurizer spray valve actuation and pressure control
 - Pressurizer PORV cycling and pressure control
 - PCS depressurization due to PCS mass depletion through PORV
 - Two-phase break flow through PORV and hot leg stratification
 - PCS depressurization due to the secondary side refill and secondary side feed and bleed
3. to identify reasons for the discrepancy evaluated in item 2.

The descriptions of the LOFT system and the test L9-1/L3-3 are given in Chapter 2. The code description, the input modeling and the initial and boundary conditions are given in Chapter 3. The results of the calculation are discussed in Chapter 4 and the run statistics given in Chapter 5. The conclusions obtained throughout the assessment are summarized in Chapter 6.

2. Facility and Test Description

2.1 Facility Description

The LOFT facility is an experimental 50 MWt PWR designed to simulate LOCA's and anticipated transients and to provide data on the thermal-hydraulic phenomena occurring throughout the system [4]. It is a scaled representation of a commercial PWR of Westinghouse type having 4 loops with a volume ratio of 1/60. The LOFT system consists of five major systems : reactor system, primary coolant system, blowdown suppression system, emergency core cooling system and secondary coolant system, and also includes instrumentations. The lengths of the core and reactor vessel are 1.68 and 7 m, respectively. The overall configuration is shown in Fig.1.

The break location for the test L9-1/L3-3 was the experiment PORV located in the pressurizer relief line at the top of the pressurizer. The experiment PORV was geometrically similar to the commercial PWR PORV's and was steam-scaled by 1.32×10^{-2} kg/s/MW. The detailed description was provided in reference [10].

2.2 Test Description

The experiment L9-1/L3-3 composed of two sequential tests. The test L9-1 simulated a LOFA with delayed scram and no auxiliary feedwater injection in PWR. The test L3-3 described the LOFA recovery modes initiated by tripping the PCP and depressurizing the PCS through the PORV in pressurizer. The experiment objectives were as follows [5];

1. For L9-1:

- a. To evaluate uncertainties in predicted primary and secondary thermal hydraulic response associated with steam generator dryout during delayed scram.
- b. To evaluate the adequacy of PORV to provide overpressure protection in a LOFA.

2. For L3-3

- a. To investigate uncertainties in system response during a PORV imposed small break with loss of heat sink.
- b. To assess the adequacy of modelling assumptions which are used in small break performance predictions such as those identified in NUREG-0623 [7].
- c. To assess the effectiveness of steam generator refill on LOFAs following reestablishment of auxiliary feedwater availability.
- d. To assess the relative magnitude of the change in reactor vessel mixture level as a result of primary coolant system shrink during steam generator refill.
- e. To contribute to the NRC relief and safety valve testing program by providing experimental data on PORV performance characteristics over a range of PORV inlet fluid conditions.

Prior to the experiment, the flow rate of the primary system was 479.1 ± 2.6 kg/sec under the pressure of 14.9 ± 0.10 MPa. Temperatures at the hot leg and the cold leg in the intact loop were 578.2 ± 1.8 K and 558.9 ± 1.3 K, respectively. The important initial conditions including pressure, temperature and liquid level in the intact loop steam generator (SG) secondary side were listed in

Table 1.

Experiment L9-1 was initiated by stopping the main feedwater pump. Due to decrease in heat removal capacity of SG secondary side, the PCS pressure increased and the pressurizer spray valve was open at its setpoint (15.338 MPa), which was observed at 30.0 seconds after initiation of LOFA. As the magnitude of the primary-secondary power mismatch grew, the PCS pressurization exceeded the spray cooling, which caused a delayed scram, simulating a failure of the SG low level trip, on the high pressure of hot leg (15.745 MPa) at 65.4 seconds. Auxiliary feedwater was not activated in order to simulate nonavailability of auxiliary feedwater. The main steam control valve (MSCV) started to close on the scram signal and completed to close at 77.2 seconds. The primary system pressure was decreased on reactor scram and then increased due to the decay heat and the complete loss of heat sink in SG secondary, which caused the pressurizer spray valve open and initiate cycling at 208.9 seconds to control PCS pressure. The open/close setpoints of spray valve were 15.338 and 15.05 MPa, respectively. Spray was allowed to cycle for 900 seconds approximately, whereupon it was manually overridden, allowing PCS pressure to rise to the PORV actuation setpoint (16.20 MPa) at 1468 seconds. Thereafter, the pressurizer came into the liquid-full state. The PORV was allowed to cycle relieving single phase liquid primary coolant as the PCS volume continued to heatup and expand at 1468 seconds. The PORV cycling was ended at the time which the PCS hot leg temperature reached 597 K, 3270 seconds. At that time, the PCPs were deenergized, the PORV was held open and the test L3-3 was initiated. The sequence of important events was presented in Table 2.

As the PORV latch open for 1580 seconds from the initiation of L3-3, the PCS pressure dropped rapidly to saturation and the hot regions of the core and upper plenum flashed. ECCS actuation was inhibited. The depressurization stabilized while the upper plenum and upper head voided whereupon the hot leg stratified. As hot leg voided a higher quality fluid was convected up the surge line, and the pressurizer liquid level receded as the cooler pressurizer fluid was entrained out the PORV. A transition to higher quality PORV mass flow decreased fluid density

flowing pressurizer relief line shortly after latching open PORV. This transition resulted in a higher specific energy fluid being discharged out the PORV and resulted in increased energy removal out the break. As break energy removal exceeded decay heat addition, PCS pressure declined steadily. PCS pressure stabilized as the PORV was closed. A steam generator refill was initiated 265 seconds after the PORV-closure. PCS pressure dropped rapidly as the secondary heat sink was restored. When the normal steam generator liquid level was regained at 5746.4 seconds, the SG refill was completed and then a 966 seconds equilibration period was observed to allow the primary and secondary to reach an equilibrium. Subsequently, a secondary steam and makeup operation was initiated at 6712.2 seconds to cool down the primary and recover plant. ECCS injection was not provided throughout the experiment. The experiment was terminated as PCS pressure reached 2.15 MPa. The major sequence was summarized in Table 2.

3. Code and Modeling Description

3.1 Code Description

RELAP5/MOD3 Cycle 5m5 version released by USNRC was used in the present assessment calculation of the test L9-1/L3-3. The changed features from the RELAP5/MOD2 were described in references [1, 2].

3.2 Input Modelling

The original RELAP5/MOD1 input data for simulating the LOFT system and the sequence specific to the test L9-1/L3-3 was received from INEL at January 1991. Based on the original RELAP5/MOD1 input data, some modifications was made during the assessment work. Major changes were as follows :

1. All geometric data except the U-tube heat transfer area and separator in the intact loop SG remain unchanged.
2. Modeling options related to volume, junction, heat structure were properly modified to work with RELAP5/MOD3 [1].
3. The options, 'new transnt' were changed to 'new stdy-st' in order to re-initialize the whole plant conditions under RELAP5/MOD3 models and correlations.
4. For steady state run, three steady state control systems were added ;
 - a. PCP speed controllers for controlling a intact loop mass flow rate,
 - b. a pressurizer heater controller and a pressurizer spray controller for controlling the PCS pressure, and
 - c. a main feedwater controller for controlling the S/G secondary side liquid level.
5. For steady state run, the test specific trips were set not to be activated.
6. A new transient input data was developed with deleting steady state controllers and changing the test specific trips to be activated.
7. The moderator density feedback table in a reactor kinetics input data was appropriately changed from the original one, based on the reference [8].

In the present calculation, the LOFT system was discretized by 125 volumes, 135 junctions and 136 heat structures after implementing the items stated above. Figure 2 shows a RELAP5 nodalization diagram for simulating the test L9-1/L3-3. Table 3 summarizes the nodalization and input modelling. A steady state input deck and a transient input deck were provided in Appendix A and B.

3.2.1 Primary Coolant System Modelling

The PCS composed of an intact loop and a broken loop, the former included a hot leg, a crossover leg, a pump suction tee, two PCPs and a cold leg. The intact loop was modelled by 25 hydrodynamic volumes. All piping metal structures exposed to environmental atmosphere were simulated by the heat structure to consider the associated heat loss. An overall information for the all heat structures was provided in table 4. The broken loop composed of a hot leg, a SG-pump simulator, a reflood assist bypass system (RABS), a cold leg and pipings front of the quick opening blowdown valves (QOBVs). The detailed information can be found in Fig.2, table 3 and table 4. The volume and junction modelling options were set with default options.

3.2.2 Reactor Vessel Modeling

The LOFT reactor vessel was modelled by a downcomer annulus, a lower plenum, an active core, a core-bypass flow path, an upper plenum, an upper head and a filler gap flow path. The filler gap flow path was especially modeled for simulating an upward flow during a natural circulation phase. The active core, the downcomer and the filler gap were modeled by 3 volumes, 6 volumes and 7 volumes stacked vertically, respectively. Totally 26 volumes and 50 heat structures were used. The rod bundle interphase friction model option was selected for the active core volumes. The fuel rods were modeled by 3 heat structures representing the central fuel assembly and 3 heat structures representing the peripheral fuel assemblies of LOFT core. The axial power shape was described according to the reference[8]. The reactor kinetics was used for simulating the moderator density and doppler temperature feedback and a scram curve was provided, which was

used in the posttest calculation [8]. The ANS-79 model was used for a decay heat simulation, which was changed from ANS-73 model in the posttest calculation [8].

3.2.3 Pressurizer Modeling

The pressurizer system was modeled by a surgeline, a pressurizer vessel, a spray line from cold leg, a spray valve and a experiment PORV. Two volumes for the surge line, nine volumes for the vessel and one volume for the spray line were used, respectively. The spray valve and the PORV were simulated by two trip valves. The associated trip logics were prepared according to the experimental specification [6]. To consider the environmental heat loss from the pressurizer vessel wall, the vessel wall was modeled by nine heat structures.

3.2.4 Steam Generator Modeling

The steam generator consisted of a SG inlet plenum, U-tubes, a outlet plenum, a main feedwater tank and feed line, a auxiliary feedwater tank and feed line, a feedwater inlet annulus, a SG secondary side downcomer, a boiler section, a separator inlet annulus, a separator, a steam dome, a steimeline, a MSCV, a MSCV bypass flow path, a MSCV downstream piping and a air-cooled condenser. The numbers of volumes used for each flow path were provided in Table 3 and Fig.2. All of the SG metal wall and U-tubes were described by the proper heat structures. The detailed description can be found in Table 4. The rod bundle interphacial friction option was used for the volumes contacted with the U-tubes heat structures (Volumes 515-4, -5, -6). The separator section in SG was modeled by a branch component (Volume 520) and a SEPARATR component (Volume 500). The separator inlet junction was connected to the bottom of the volume 520, as show in Fig.2.

The heat transfer area of U-tube heat structure in the intact loop SG generally has an impact on the initial conditions in SG secondary side. According to the previous LOFT calculations using RELAP5/MOD2 [9, 10], the predicted pressure in SG secondary side were generally underpredicted by 0.3-0.4 MPa. This discrepancy was considered as a result of underestimation of heat transfer area

in the SG U-tube. In the present input data, an increase of heat transfer area by 110 % of the original heat transfer area [8] was made. The whole listing of steady state input data were provided in Appendix A.

3.2.5 Others

The emergency core cooling system (ECCS) in LOFT was also modeled, however, it is not used in the transient calculation. Table 3, Fig 2 and Appendix A provided a detailed information of it. And the containment was also modeled by time-dependent volume with a constant pressure.

3.3 Initial and Boundary conditions

To provide all initial conditions of the whole system prior to transient, a steady state run was carried out with three steady state controllers as stated above. The result obtained from the steady state run was compared with the measured initial conditions in Table 1. The RELAP5 calculated results generally agree with the experiment initial conditions.

Boundary conditions required to simulate the L9-1/L3-3 experiment including the pressures and temperatures at air-cooled condenser, makeup feed storage tank and reactor core power history were almost the same as those used in the posttest calculation [8]. The exact values can be found in the steady state input data.

Test specific sequence to be described are as follows: Main feedwater turned off, Reactor scram, SG MCSV closure, Pressurizer spray valve open/closure, Pressurizer PORV cycling, Pressurizer PORV latched open and closure, PCP coastdown initiation, SG secondary refill initiation/completion, and SG secondary bleed initiation/completion.

All of the sequence were as the same as the original input data [8] and were illustrated with some comments in the Figure 3-a through 3-g. The delay time in the trip logic describing the SG refill initiation (Variable trip 561) was corrected to '265 seconds' after PORV closure according to the reference [5]. The whole list of the transient input data was attached in Appendix B.

4. Calculation and Discussion

A transient calculation using the input modelings, initial conditions and boundary conditions stated above was conducted by RELAP5/MOD3 5m5 code. The transient calculation was terminated at 8106 seconds due to water property failure at the SG secondary side volume 515-06. Since the calculational result up to 8100 seconds contains all of the important phenomena in the L9-1/L3-3 experiment, any additional restart transient calculation was not executed. The foregoing description was, therefore, based on the calculational result up to 8100 seconds. This chapter was devoted to address results from the transient calculation, to compare them with the corresponded measurement data and to identify the code predictability. Table 2 shows a comparison of the predicted sequence of event with the measured chronology. The detailed discussion of the comparison was provided in following sub-chapters. From the test description above, it is shown that the full period of the LOFT L9-1/L3-3 experiment can be divided into four distinguishable sub-phases according to the TH characteristics as follows;

- 1) Initial heatup phase before spray cycling,
- 2) Spray and PORV cycling phase until PORV latched open,
- 3) Blowdown phase until PORV closure, and
- 4) Recovery phase

The following discussions contain the prediction and its comparison for the important thermal-hydraulic phenomena during these four period, respectively. Table 5 summarizes the comparison plots and their data channels.

The measurement uncertainties for each parameter were also listed in this table, which were from the reference [5].

4.1 Initial Heatup Phase

Figure 4 shows a comparison of the pressure at the intact loop hot leg in PCS with the measured data up to 300 seconds after the test initiation. Fig.5 shows a comparison of the coolant temperature at the intact loop hot leg with the measured data for the same period as in Fig.4. Due to LOFA the heat removal capacity in SG secondary side was degraded, the PCS pressure and temperature was increased. These figures show good agreements between the calculation and the experiment before reactor scram. The calculated reactor scram time (55.8 seconds) was earlier than the experiment (65.4 seconds). This discrepancy may come from a code uncertainty in predicting the mass flow rate through the spray valve and the associated condensation phenomena in the pressurizer. For an illustration of it, the calculation shows the PCS pressure was still increased inspite of the second spray actuation at 50 seconds approximately, while the experiment indicated the PCS pressure was slightly decreased at the almost same time and then re-increased. It can be also identified in the first activation of spray (30 seconds), in which the predicted slope of pressure decrease was slower than the predicted one. The underprediction of pressure and temperature after scram was due to the difference in scram time. Figure 6 shows a comparison of the calculated reactor power with the power measured by a neutron detector and with the decay heat reported in reference [5]. The difference in power during time period from 56 to 65 seconds lowered the PCS pressure below 14 MPa and delayed a pressure re-increase until 170 seconds, i.e, an excessive post-scram cooling. This discrepancy also delayed the spray valve activation time until 315 seconds, which was later than the experiment, 208 seconds.

Figures 7 and 8 show comparisons of the pressure and temperature in the SG steam dome and the top of the boiler section with the measured data, respectively. Before the reactor scram the predicted behavior was agreed to the measured one. Due to earlier scram in calculation, the starting time and completion time of MCSV closure predicted by RELAP5/MOD3 were earlier than those in experiment as shown in Table 2. According to the experiment, just after a LOFA, the SCS pressure and temperature were both increased from saturated state until

the complete dryout, and then decreased until the MCV began to reduce the discharging steam flow on the response to the reactor scram. This reduction yields a decrease in heat rejection from the SCS, therefore, the SCS pressure and temperature were re-increased. Afterwards, the TH behavior of the SCS was dependent on the energy balance between the heat-rejection due to the MCV leakage flow and the heat addition from the PCS generated by core decay heat. The result from the RELAP5/MOD3 calculation generally shows these TH behavior well, however, shows an overprediction in SCS pressure and temperature after scram. It must due to a difference in the scram time. Inspite of this difference, the slope of increase in pressure after scram was almost the same as that in the experiment. Figure 9 shows a comparison of the collapsed liquid level with the measured data, which indicated a complete dryout in SG secondary side at 60 seconds after a LOFA, approximately and a good agreement between the calculation and the experiment. Figure 10 shows a comparison of the mass flow rate through MCV. From these comparisons, it, therefore, can be stated that the consequent behavior after scram can be well-predicted if the scram time was correctly predicted.

4.2 Spray and PORV Cycling Phase

Figures 11 and 12 show comparisons of the pressure and temperature at the intact loop hot leg in PCS up to 10000 seconds. The starting time of the spray valve cycling predicted was, as previously mentioned, later than the measured. The predicted duration of spray cycling was about 1055 seconds ($= 1370 - 315$), which was similar to the measured duration, 1037 seconds ($= 1246 - 209$). The slope of temperature increase, i.e., heatup rate was larger than the experiment, however, a saw-tooth behavior in pressure was well predicted during the spray cycling period. One of the reasons of higher heatup rate was also considered as an uncertainty in the spray mass flow rate.

The predicted starting time of PORV cycling was 1795 seconds and also later than the experiment, 1468 seconds. The duration of PORV cycling was about 1390 seconds ($= 3185 - 1795$) in calculation, which was shorter than the experiment, 1802 seconds ($= 3270 - 1468$). The heatup rate during the PORV cycling phase was almost same as the experiment. The cycling phase was ended at 3185 sec in calculation. During the spray and PORV cycling period the major contributor to the PCS heatup was considered as the core decay heat and the heat provided by PCP's.

Figures 13 and 14 show comparisons of the pressure and temperature at the same position as in Figures 7 and 8 up to 10000 seconds, respectively. The predicted pressure was monotonously decreased during the spray and PORV cycling phase, which was, however, higher than the experiment throughout the cycling phase. It was due to a difference in scram time, but the slope of pressure decrease was well agreed to the experiment. The secondary coolant temperature was also overpredicted as shown in Fig.14.

4.3 Blowdown Phase

After the PCS hot leg temperature reached 597 K, the PORV was held open for the consequent 1580 seconds. During this period the primary coolant was discharged through the PORV, which caused a rapid depressurization until the onset time of saturation in PCS. As shown in Fig.11, the calculated pressure drop was almost same as the experiment until the PCS saturation. After the saturation, the calculation shows that the PCS pressure was almost constant until the PORV closure time (4769 seconds), which was quite different from the experiment. The difference in the pressurizer liquid level can be regarded as one reason for the pressure increase during the saturated blowdown period as shown in Fig.15. The calculated liquid level in the pressurizer was almost constant until the SG refill initiation, while the measured level was slowly decreased from the PORV open time. It is also shown that the high heatup rate during the spray cycling period yielded an overprediction in the pressurizer liquid level swell and in the PCS pressure. The over-estimated liquid level also contributed to the overprediction of mass flow rate through the PORV during the two-phase blowdown phase as shown Fig.16.

During the same period, the PCS temperature was also overpredicted, which indicated that the insufficient energy convected out the PORV. According to the reference [8], the effective flow area of PORV was correctly chosen, the reason for the insufficient energy discharged out the PORV, therefore, was a code inaccuracy in calculating the fluid density convected from the hot leg to the pressurizer surge line under the hot leg stratified. As shown in Fig.17, the measured fluid density at the intact loop hot leg was different from the calculated one from 3500 seconds, approximately. The experiment indicated that the intact loop hot leg was stratified shortly after holding open PORV, that a higher quality fluid was convected out the break as pressurizer level receded and that the hot leg fluid density significantly decreased. However, RELAP5/MOD3 predicted this phenomena inaccurately, which due to a code weakness in calculating the junction density under the stratified condition.

During the blowdown period, the SCS experienced the similar depressurization

to the previous phase as shown in Figures 13 and 14.

4.4 Recovery Phase

After 265 seconds from the closure of PORV, the SG secondary side refill was initiated through the auxiliary feedwater line. The predicted hot leg pressure and temperature were rapidly decreased during the secondary refill period as shown in Figures 11 and 12. However, the magnitudes of drops in pressure and temperature were overpredicted. One of the reason for this overprediction was considered as an difference in the refill duration (1085 seconds in calculation versus 622 seconds in experiment). It is also shown in Fig.17, which presents a comparison of the SG liquid level in long term. The calculated liquid level indicated no jump which was found in the experiment and the predicted refill duration was longer than the experiment. Since the refill duration was strongly dependent on the SG secondary side liquid level, the inaccuracy of the level prediction may extend the refill duration, consequently increase the cooling effect. The major contributor to their accuracy of level prediction was a void distribution calculated by the code.

After restoring the SCS heat removal capacity, the predicted SCS pressure was increased more rapidly and the predicted peak pressure was higher than the experiment as shown in Fig.13. During the same period the predicted temperature at SG secondary side moved down as shown in Fig.14, which indicates the return from the superheated steam to the saturated state in SG secondary side at 5200 seconds, approximately. The reason for the overprediction of pressure was considered as a propagation from the previous phase. The descending behavior in pressure after saturation was almost similar to the experiment.

During the equilibration period of 966 seconds after the SG refill completion (6119 seconds in prediction), the PCS pressure and temperature were slightly increased. The calculation shows that the SG feed and bleed operation was initiated at 7085 seconds, that the PCS pressure and temperature were both decreased in stepwise manner and that the magnitudes of drops in the pressure and temperature were larger than those measured. It due to the continual feed operation from the auxiliary feedwater valve, which was different from the continous feed operation in the experiment. Since the feed operation is also

strongly dependent on the SG secondary side liquid level, the reason for this larger drops than the experiment can be regarded as the inaccuracy of the SG secondary void distribution.

5. Run Statistics

The main frame computer used in the present calculation was a CRAY-2S in System Engineering Research Institute(SERI) in Taejon, Korea under UNICOS as a operating system. Figure 19 presents the plot of the required CPU time for the transient time in the calculation. And the time step size are also plotted in Fig.20. The user-specified maximum time step was 1.0 second up to 1000 seconds, 0.1 second up to 2000 seconds, 0.5 second up to 4000 seconds, 0.1 second up to 8000 seconds and 0.5 second up to 10000 seconds in real time. The grind time can be calculated as follows.

$$\text{Computer time, } \text{CPU} = 7981.4 - 1.9181 = 7979.48 \text{ (sec)}$$

$$\text{Number of time step, } \text{DT} = 89332 - 220 = 89112$$

$$\text{Number of volume, } \text{C} = 125$$

$$\text{Transient real time, } \text{RT} = 8100 \text{ (sec)}$$

$$\text{Grind time} = \text{CPU} \times 1000 / (\text{C} * \text{DT}) = 0.71635 \text{ CPU m sec/vol/step}$$

6. Conclusions

The RELAP5/MOD3 5m5 code was assessed using the test L9-1/L3-3 simulating a LOFA with multiple failures and the consequentially-induced LOCA. The full period of the test was divided into four sub-periods according to the thermal-hydraulic characteristics ; the initial heatup phase, the spray and PORV cycling phase, the blowdown phase and the recovery phase. The calculation results were compared with the measured data and the evaluation of the code predictability for this type of transient was conducted. The following conclusions are obtained.

- 1) RELAP5/MOD3 code calculation was successfully executed for the L9-1/L3-3 test and the code applicability to an anticipated transient with multiple failures in PWR was demonstrated.
- 2) From the fact that the result from the calculation generally shows a good agreement with the experiment data, the overall predictability of the RELAP5/MOD3 was identified and the minor discrepancies were also identified.
- 3) In the initial heatup phase, the predicted scram time was earlier than the experiment due to a code uncertainty in predicting the spray mass flow rate and the associated condensation phenomena in pressurizer, which caused an excessive heatup rate in the spray cycling phase.
- 4) In the blowdown phase, the overprediction of PORV-discharged flow was found under the over-estimated pressurizer level, which may come from the excessive heatup in the previous phase. And a code inaccuracy was found in calculating the junction fluid density at the hot leg to the pressurizer surge line under the stratified condition.
- 5) In the recovery phase, an excessive cooling was predicted both in the steam generator secondary refill phase and in the secondary feed and bleed operation phase due to a poor prediction on void distribution in the SG secondary side.

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9. Y.S. Bang, et al, *Assessment of RELAP5/MOD2 Cycle 36.04 Using LOFT Large Break Experiment L2-5*, NUREG/IA-0032, April 1990.
10. E.J. Lee et al, *ICAP Assessment of RELAP5/MOD2 Cycle 36.05 Against LOFT Small Break Experiment L3-7*, NUREG/IA-0031, April 1990

Table 1. Initial conditions for L9-1/L3-3

<u>Parameter</u>	<u>Measured</u>	<u>Simulated</u>
Primary Coolant System		
Mass flow rate (kg/s)	479.1 ± 2.6	479.34
Hot leg pressure (MPa)	14.9 ± 0.10	14.8905
Cold leg temperature (K)	558.9 ± 1.3	559.132
Hot leg temperature (K)	578.2 ± 1.8	578.327
Reactor		
Power level (MW)	49.6 ± 0.9	49.6
Maximum linear heat generation rate (kW/m)	50.8 ± 3.6	50.8
Steam Generator Secondary Side		
Water level (m)	0.14 ± 0.08	0.1475
Water temperature (K)	545.0 ± 0.8	542.377
Pressure (MPa)	5.67 ± 0.08	5.72
Mass flow rate (kg/s)	27.0 ± 1.0	26.728
Broken Loop		
Hot leg temperature (K)	563.3 ± 2.6	559.137
Cold leg temperature (K)	557.6 ± 2.6	558.381
Pressurizer		
Steam Volume (m ³)	0.43 ± 0.05	---
Liquid volume (m ³)	0.50 ± 0.05	---
Water temperature (K)	614.9 ± 1.3	610.4
Pressure (MPa)	14.93 ± 0.25	14.901
Liquid level (m)	0.92 ± 0.1	0.96

Table 2. Sequence of events in L9-1/L3-3

<u>Event</u>	<u>Description</u>	<u>Measured</u> (sec)	<u>Calculated</u> (sec)
<u>L9-1</u>			
Main feedwater pump off		0.0	0.0
Pressurizer spray activated	$P_{p_{zr}} > 15.338^*$	30.0 ± 0.1	28.94
Reactor scram (15.67 MPa) t_{SCRAM}	$P_{ILHL} > 15.745$ $T_{ILHL} > 583.16^*$	65.4 ± 0.2	55.8
Steam generator main steam control valve closed	$t_{SCRAM} + \text{delay}^*$	77.2 ± 0.2	69.0
Steam generator liquid level reached bottom of range	$L_{S/G} = 0.25 \text{ m}$	190 ± 20	82.0
Pressurizer spray valve cycling initiated	$P_{p_{zr}} > 15.338$	208.9 ± 0.1	315.0
Pressurizer liquid level reached top of the range	$L_{p_{zr}} = 1.83 \text{ m}$	1089.7 ± 30	1840.0
Pressurizer spray valve cycling ended	$P_{p_{zr}} > 16.2$	1246.0 ± 0.1	1370.0
PORV cycling initiated	$P_{p_{zr}} > 16.2$	1467.9 ± 0.1	1795.0
<u>L3-3</u>			
PORV latched open (t_{LATCH})	$T_{ILHL} > 597$	3269.9 ± 0.1	3189.0
PCPs tripped off	$T_{ILHL} > 597$	3284.8 ± 0.2	3189.0

(continued)

<u>Event</u>	<u>Description</u>	<u>Measured</u> (sec)	<u>Calculated</u> (sec)
PCP coastdown completed		3304.2 ± 0.8	3220.0
Upper plenum fluid reached saturation pressure		3329.4 ± 0.2	3270.0
PORV closed ($t_{PORV-CLOSE}$)	$t_{LATCH} + 1580$	4849.7 ± 0.1	4769.0
Steam generator secondary refill initiated	$t_{PORV-CLOSE} + 265$	5114.6 ± 0.2	5034.0
Natural circulation initiated		5205 ± 10	---
Steam generator secondary refill completed ($t_{REF-COM}$)	$L_{S/G} = 2.9464$	5746.4 ± 0.2	6119.0
Pressurizer liquid level reached bottom of the range	$L_{pzc} = 0.06$	5915 ± 5	5460.0
Steam generator secondary feed and bleed initiated	$t_{REF-COM} + 966$	6712.2 ± 0.2	7822.2
Experiment completed		9517.4 ± 0.2	---

Note --- : not predicted

* : MPa in pressure, K in temperature, and m in level

Table 3. Summary of nodalization

Component	Vol	Jun	H.S
1.Reactor Vessel			
Filler Gap	7	7	14
Downcomer	6	6	18
Lower Plenum	3	5	5
Active Core	3	2	6
Core Bypass	3	2	---
Upper Plenum	3	4	5
Upper Head	1	1	2
2.Primary Coolant System (Intact Loop)			
Hot Leg (included S/G inlet plenum)	6	7	8
S/G U-tube	6	5	6
Loop Seal (included S/G outlet plenum)	4	4	3
Pump Suction Tee	5	6	5
Primary Coolant Pumps	2	4	---
Cold Leg (included pump discharge pipes)	8	12	7
3.Primary Coolant System (Broken Loop)			
Hot Leg	3	4	3
S/G-Pump Simulator	12	12	12
RABS	4	5	4
Cold Leg	5	6	5
QOBV/Line	2	2	---
4.Pressurizer System			
Surge Line/Valve	2	3	---
Pzr Vessel	9	8	10
Spray Line/Valve	1	3	---
Experiment PORV	---	1	---
Heater	---	---	1
5.Secondary Coolant System			
Feedwater Storage	2	2	---
S/G Downcomer	6	6	10
S/G Riser	5	4	12
Separator	1	3	1
Steam Dome/Line	3	2	2
MSCV/Bypass	---	2	---
6.ECCS	6	6	---
7.Others (Letdown/Charging, Containment)	3	1	---
Total	125	135	136

Table 4. Detailed information for heat structure

<u>No</u>	<u>NH</u>	<u>NA</u>	<u>Description</u>	<u>Left Bn.</u>	<u>Right Bn.</u>
60	6	8	SG U-tube	115-4:9	515-4:6
1151	2	4	SG Inlet/Outlet Plenum Wall	115-3,-10	Ambient
1152	2	20	S/G Tube Sheet Periphery Region	115-3,10	515-3
1001	12	11	Intact Loop Piping (Large Pipes)	100, 105, 110, 115-1 115-12,-13 120, 150 150, 175-1, 175-2, 180, 185	Ambient
1002	2	11	S/G Inlet-Cold Leg, Outlet-Hot Leg Connection	115-2, 11	Ambient
1003	7	11	Intact Loop Piping (0.216 m OD)	125, 130, 140, 145, 155, 160, 170	Ambient
1004	2	11	S/G Inlet/Outlet Plena	115-3,10,	Ambient
2000	1	21	Reactor Vessel Filler Block Inlet Annulus Top Volume	200	Insulated
2001	6	11	Core Support Barrel	Insulated 210-1:4	200, 205
2050	1	21	Filler Blocks Inlet Annulus Lower Volume	205-1	223-1
2100	6	21	Downcomer and Lower Plenum	210-1:4, 215, 220	223-2:7

(continued)

<u>No</u>	<u>NH</u>	<u>NA</u>	<u>Description</u>	<u>Left Bn.</u>	<u>Right Bn.</u>
2110	3	11	Reactor Vessel Wall (Mid-Part)	223-1:3	Ambient
2120	5	7	Reactor Vessel Wall (Lower-Part)	223-3:7	Ambient
2200	1	11	Reactor Vessel Bottom Wall	220	Ambient
2250	7	11	Core Flow Skirt-Core Filler Assembly	225, 230-1:3, 240, 245, 246	Insulated
2260	1	7	Lower Core Support Structure, Core Support Barrel Lips, Fuel Module Lower End Box	225	Insulated
2300	3	10	Active Core	230-1:3	Kinetics
2400	1	7	Upper Core Support Stucture	240	Insulated
2460	1	5	Fuel Module Top	245	246
2500	1	11	Core Support Barrel-Upper Plenum Lower Volume	250	Insulated
2510	2	5	Upper Plenum Internals	250	Insulated
2501	1	21	Core Support Barrel-Upper Plenum Upper part	250	Insulated
2550	1	21	Upper Head Top Plate	250	Ambient
3150	2	11	Broken Loop S/G Simulator 1	315-1:2	Ambient
3151	1	11	Broken Loop S/G Simulator 2	315-9	Ambient

(continued)

<u>No</u>	<u>NH</u>	<u>NA</u>	<u>Description</u>	<u>Left Bn.</u>	<u>Right Bn.</u>
3152	1	11	Broken Loop S/G Simulator 3	315-11	Ambient
3153	6	11	Broken Loop S/G Simulator 4	315-3:8	Ambient
3154	1	11	Broken Loop S/G Simulator 5	315-12	Ambient
3155	1	11	Broken Loop S/G Simulator 6	315-10	Ambient
3000	3	11	Broken Loop Hot Leg	300, 305 310	Ambient
2250	3	11	Broken Loop Cold Leg	335, 340, 345	Ambient
3501	1	11	Broken Loop Cold Leg	350-1	Ambient
3502	1	11	Broken Loop Cold Leg	350-2	Ambient
3700	4	11	Reflood Assist Bypass Piping	370, 375, 380, 385	Ambient
4151	1	11	Pressurizer Vessel Bottom	415-1	Ambient
4152	7	11	Pressurizer Vessel (Large Dia.)	415-2:7	Ambient
4162	1	11	Pressurizer Vessel (Small Dia.)	415-8	Ambient
4172	12	9	Pressurizer Backup Heater	415-2	Table 417/8
4201	1	11	Pressurizer Top Wall	420	Ambient
5000	3	4	S/G Shroud Upper Part	500, 505, 510-1	520, 515-8:7
5150	4	4	S/G Shroud Lower Part	510-1:4	515-7:4
5300	8	10	S/G Secondary Vessel Wall	530-1, 525 500, 505 510, 515-1:3	Ambient

Table 5. Summary of data channels and uncertainties in comparison plots

<u>Description</u>	<u>Calculation</u>	<u>Experiment</u>	<u>Uncertainty *</u>	<u>Fig. No</u>
1. Pressure at ILHL	p 100-01	PE-PC-005	0.28 MPa	4, 11
2. Coolant temperature at ILHL	tempf-100-01	TE-PC-02B	3.0 K	5, 12
3. Reactor power	rktpow-0	RE-T-77-A	2.0 MW	6
4. Pressure at SG steam dome	p 530-02	PE-SGS-01	0.12 MPa	7, 13
5. Coolant temperature at SG secondary	tempg 515-06	TE-SGS-04	3.0 K	8, 14
6. Liquid level at SG secondary	cntrlvar-1	LT-P004-08B	0.08 m	9, 18
7. Mass flow rate downstream MSCV	mflowj-550	FT-P004-012	0.8 kg/s	10
8. Liquid level at pressurizer	cntrlvar-2	LE-PdEP139-6	0.06 m	15
9. Mass flow rate through PORV	mflowj-425	FR-PC-S231	0.2 kg/s	16
10. Fluid density at the intact loop hot leg	rho-100	DE-PC-02C	0.17 Mg/m3	17

Note * : Measurement uncertainty referred to the reference [5]

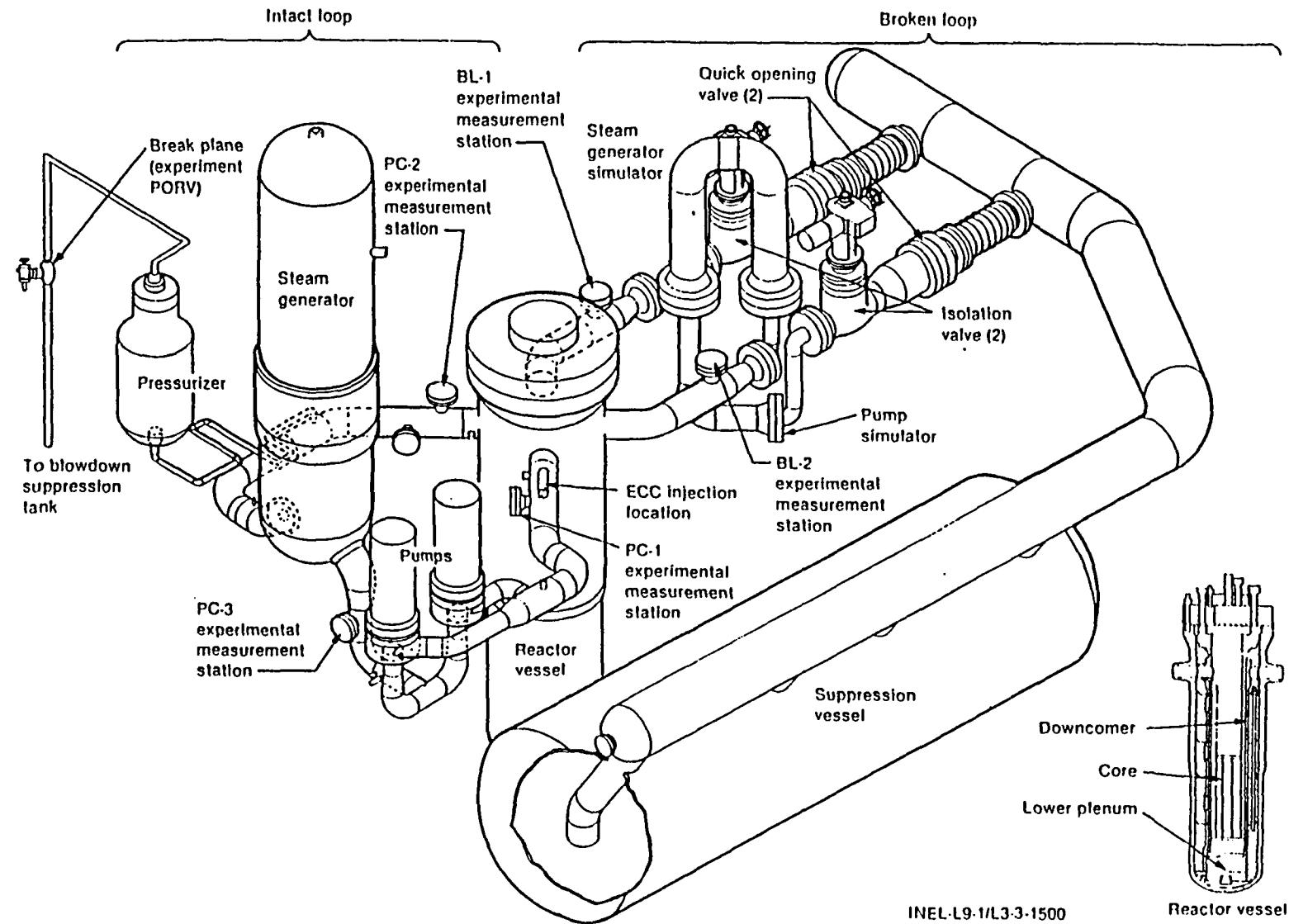


Fig.1, Axonometric configuration of LOFT L9-1/L3-3 test

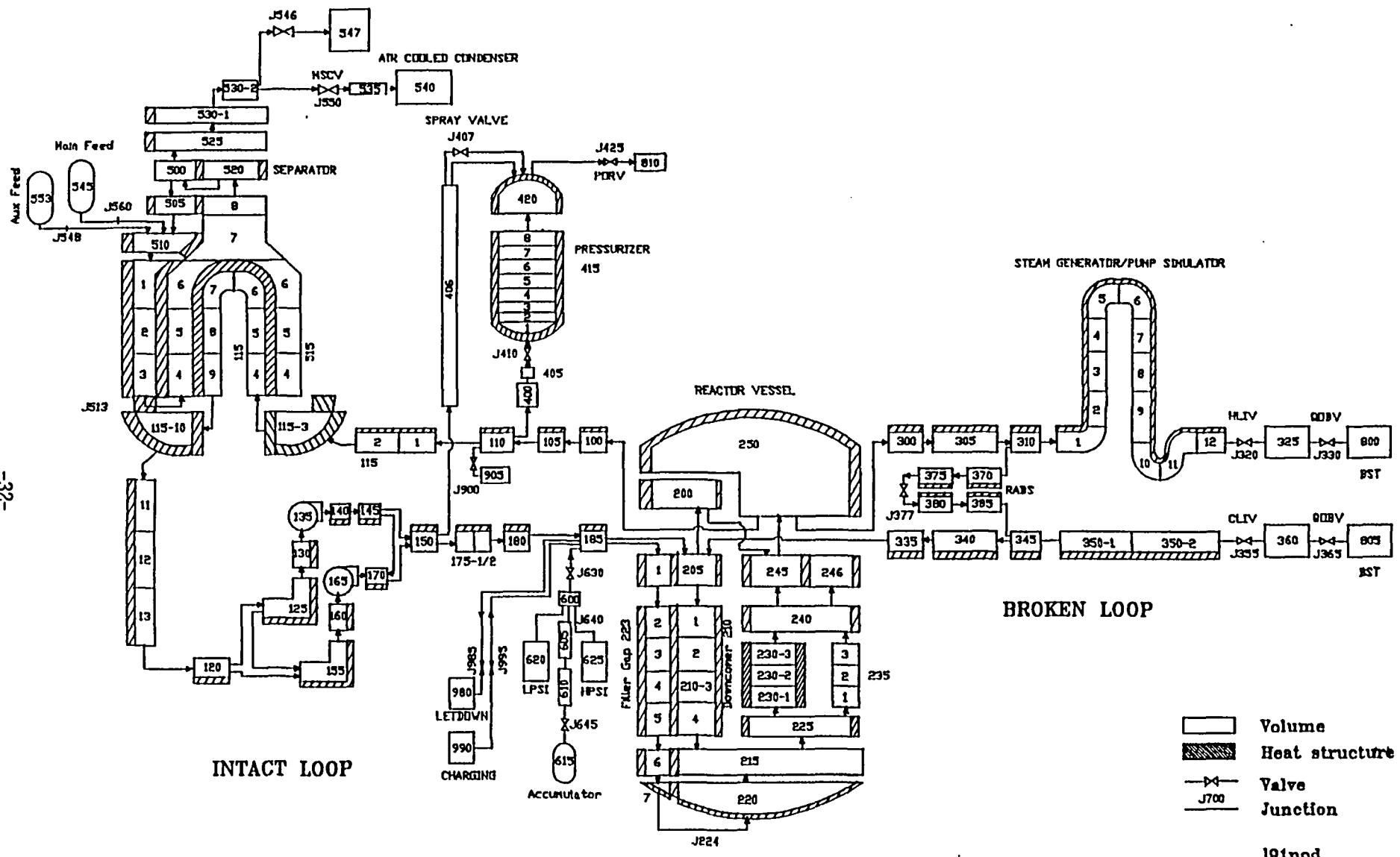


Fig. 2 RELAP5 Nodalization for LOFT Experiment L9-1/L3-3

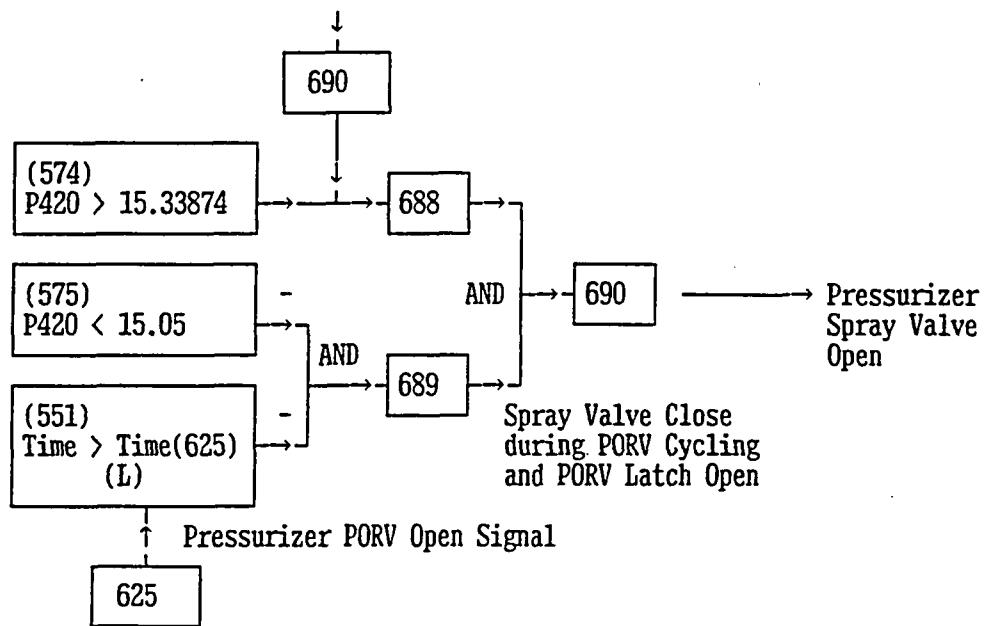


Fig.3-a. Pressurizer spray valve control trip

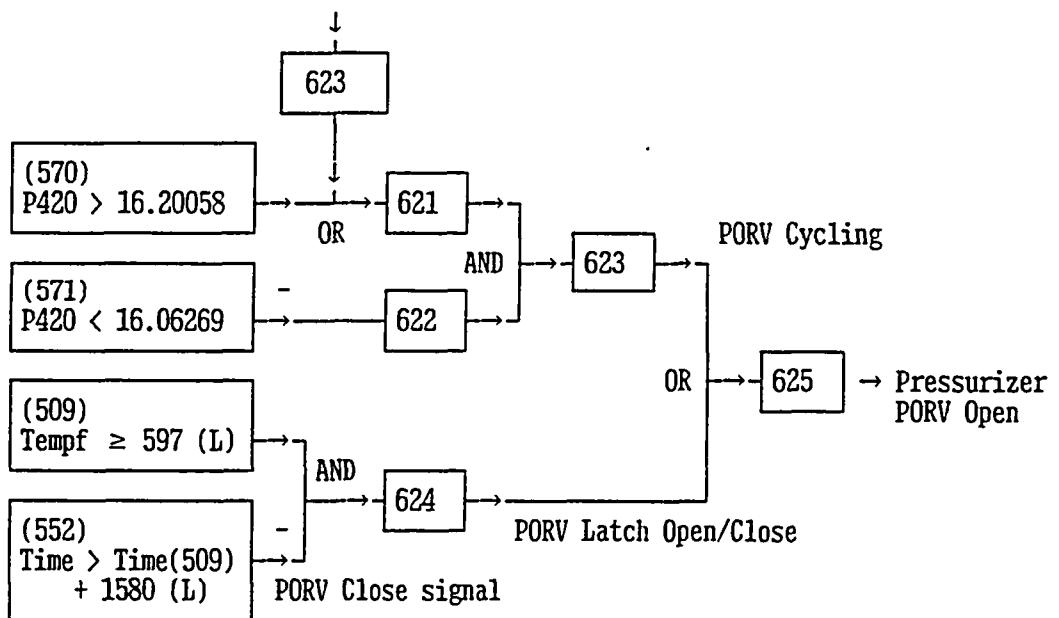


Fig.3-b. Pressurizer PORV control trip

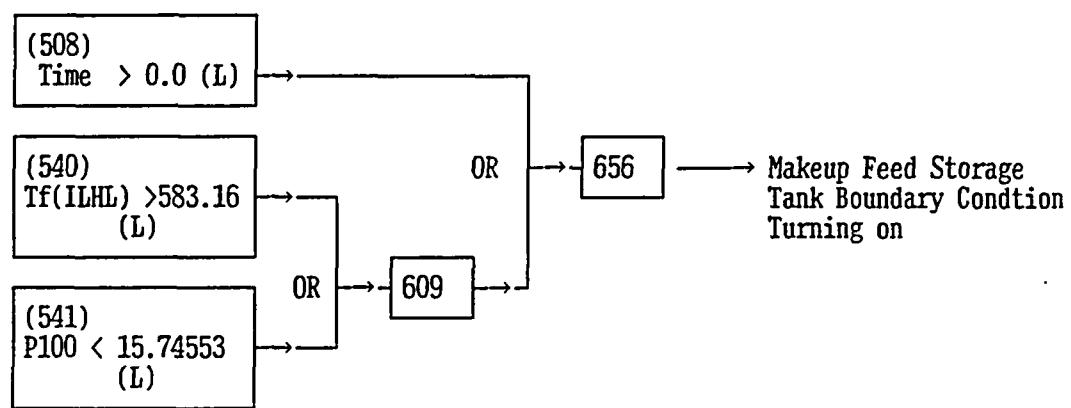


Fig.3-c. Makeup feed storage tank boundary condition trip

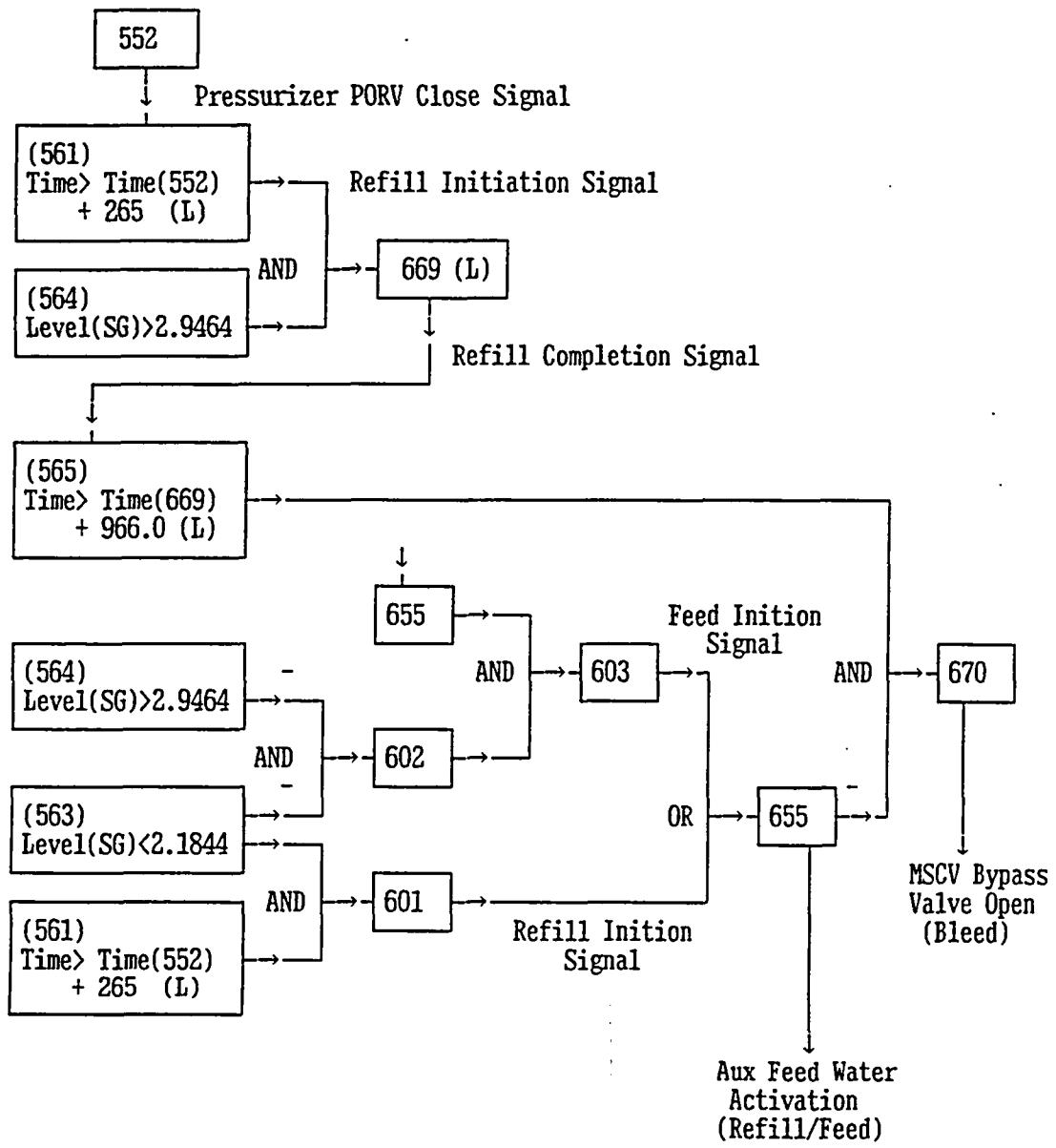


Fig.3-d MSCV byapass valve control trip

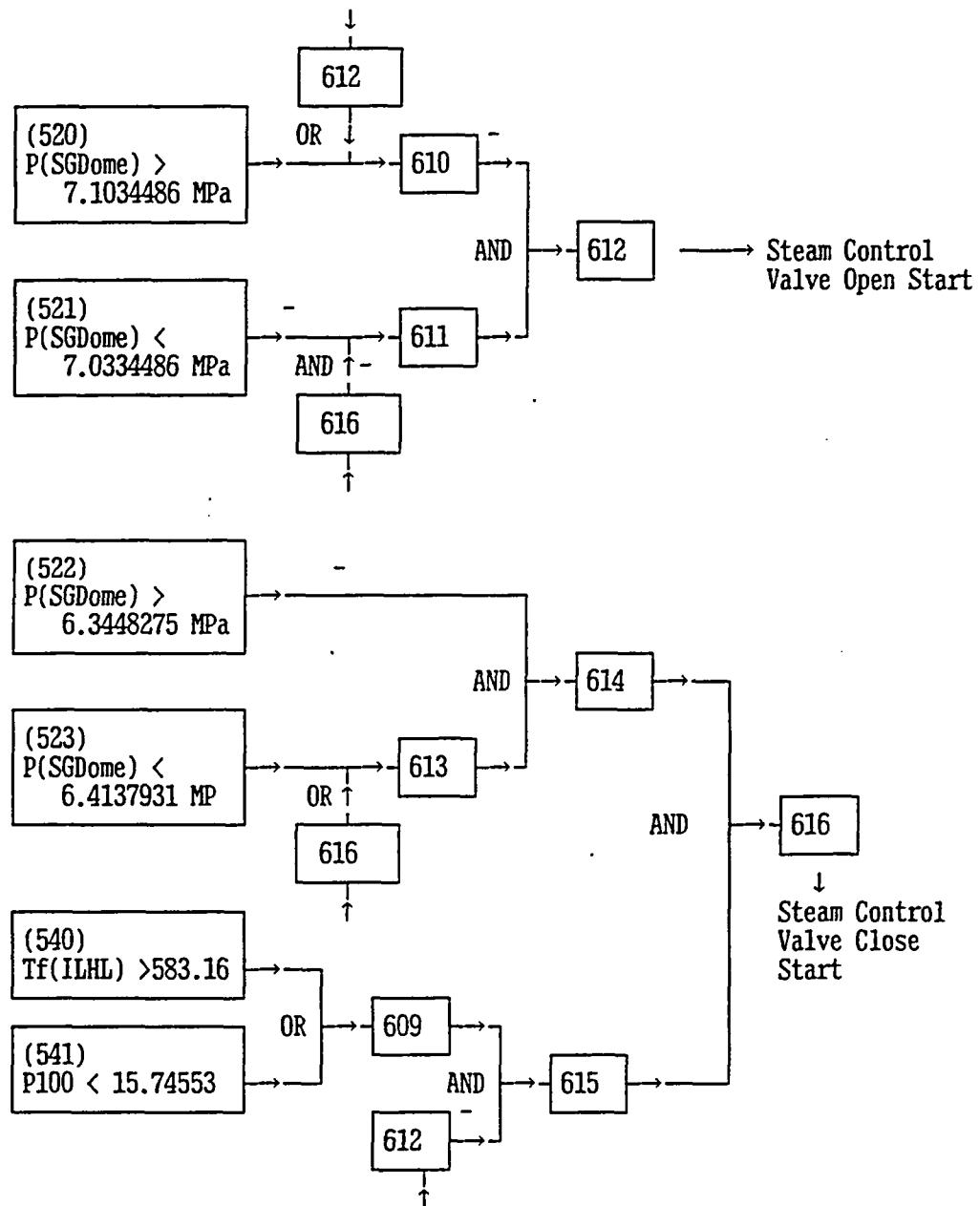


Fig.3-e MCV open/close control trip

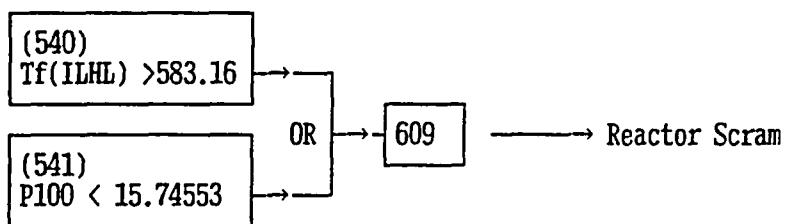


Fig.3-f Reactor scram trip

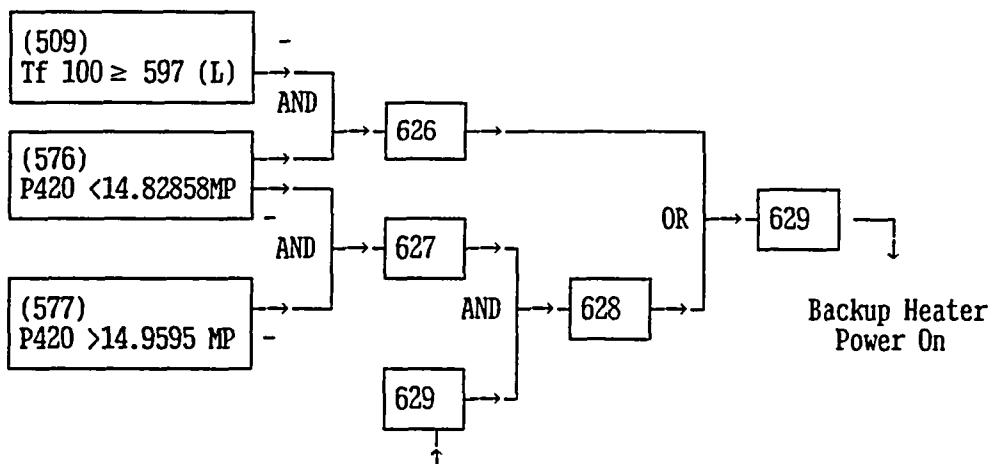
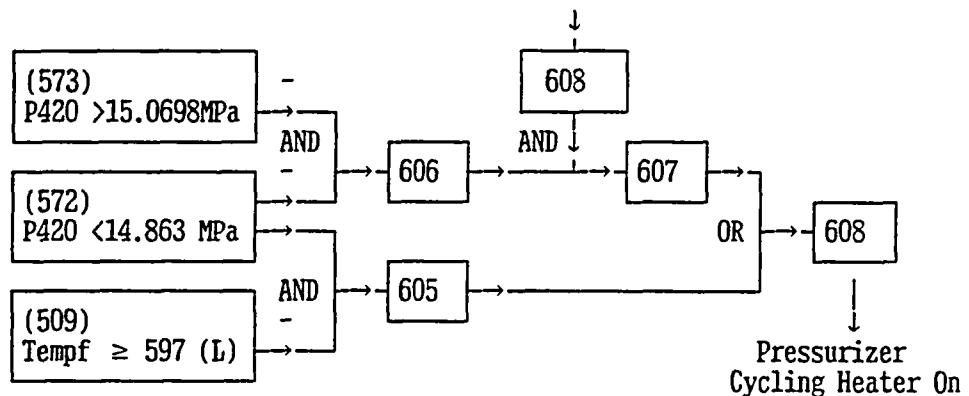


Fig.3-g Pressurizer heater control trip

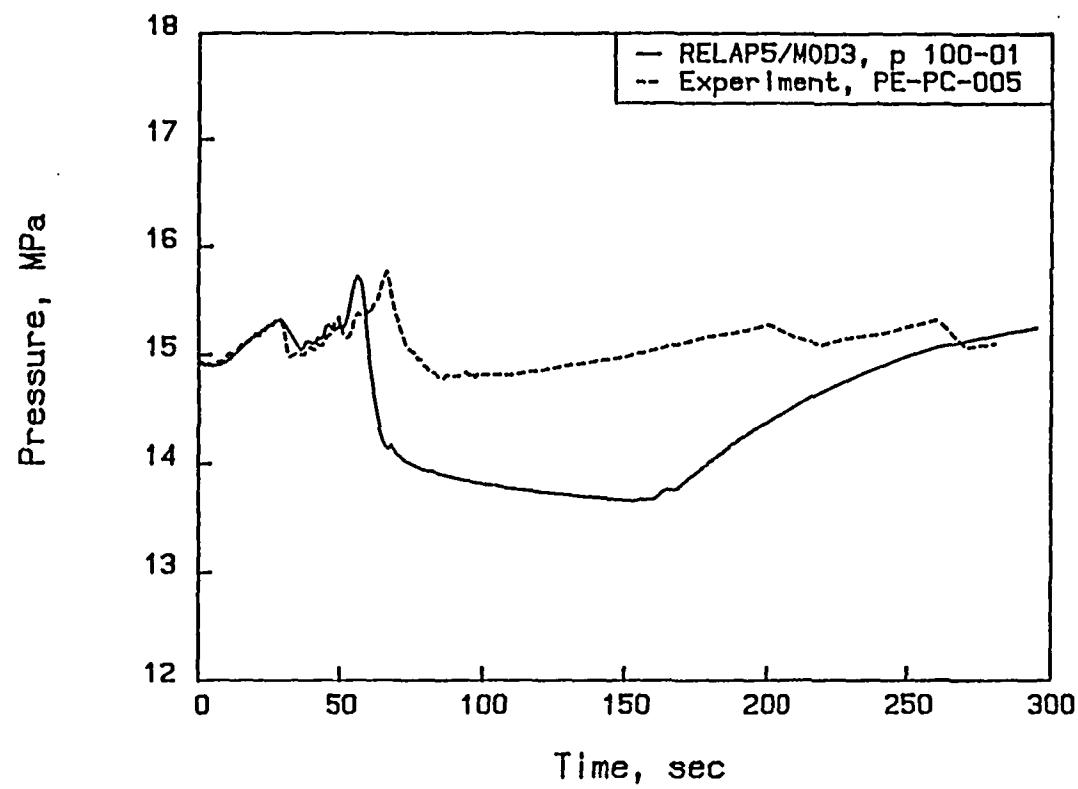


Fig.4 Comparison of pressure at the intact loop hot leg (short term)

-63-

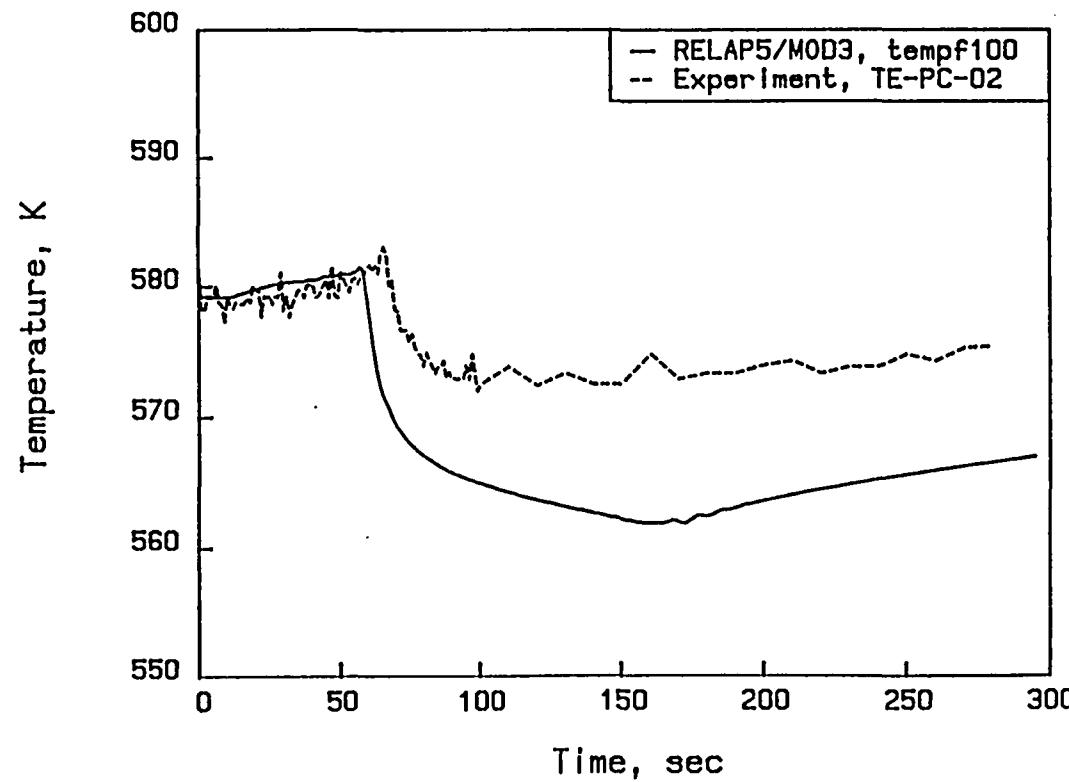


Fig.5 Comparison of coolant temperature at the intact loop hot leg
(short term)

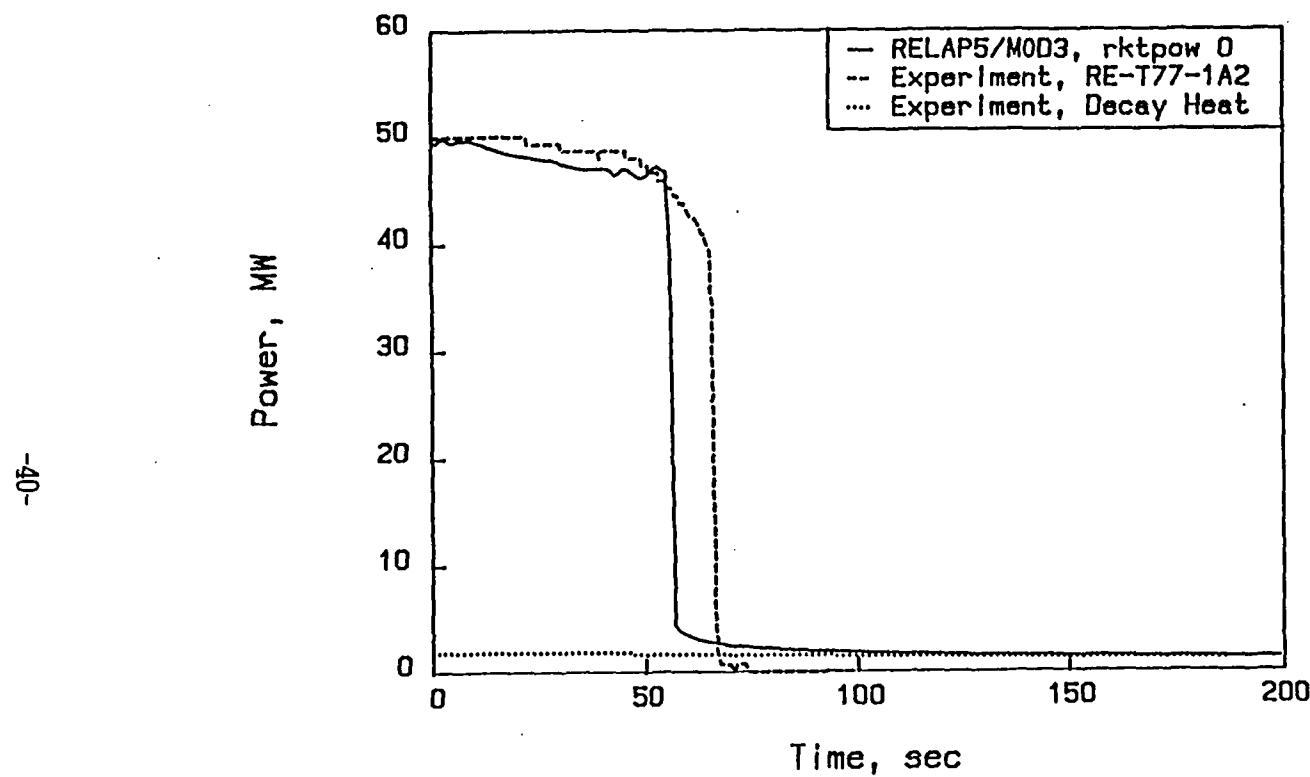


Fig.6 Comparison of reactor power

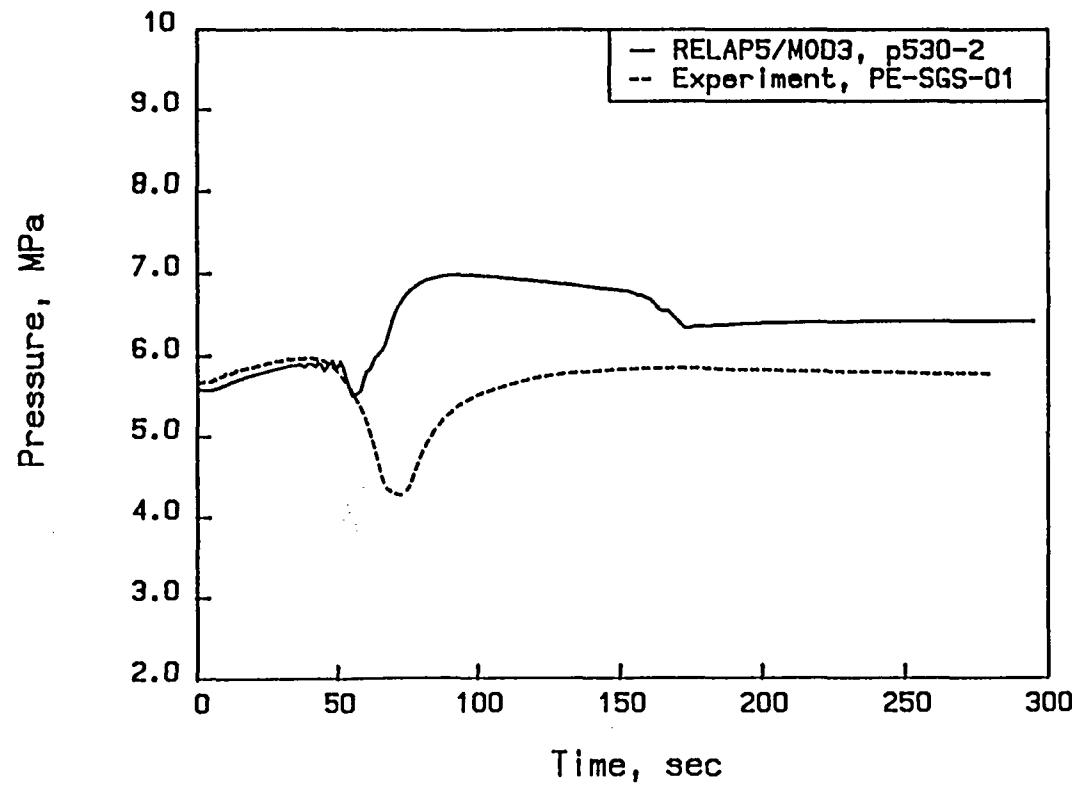


Fig.7 Comparison of pressure at SG steam dome (short term)

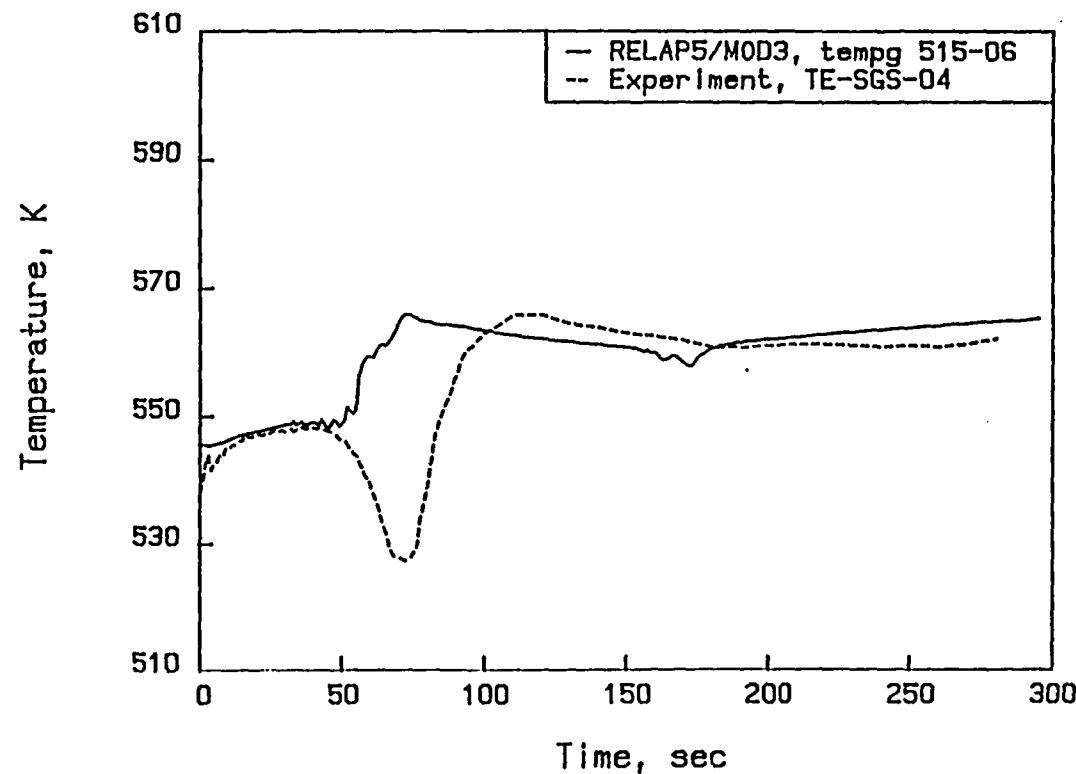


Fig.8 Comparison of coolant temperature at SG secondary side (short term)

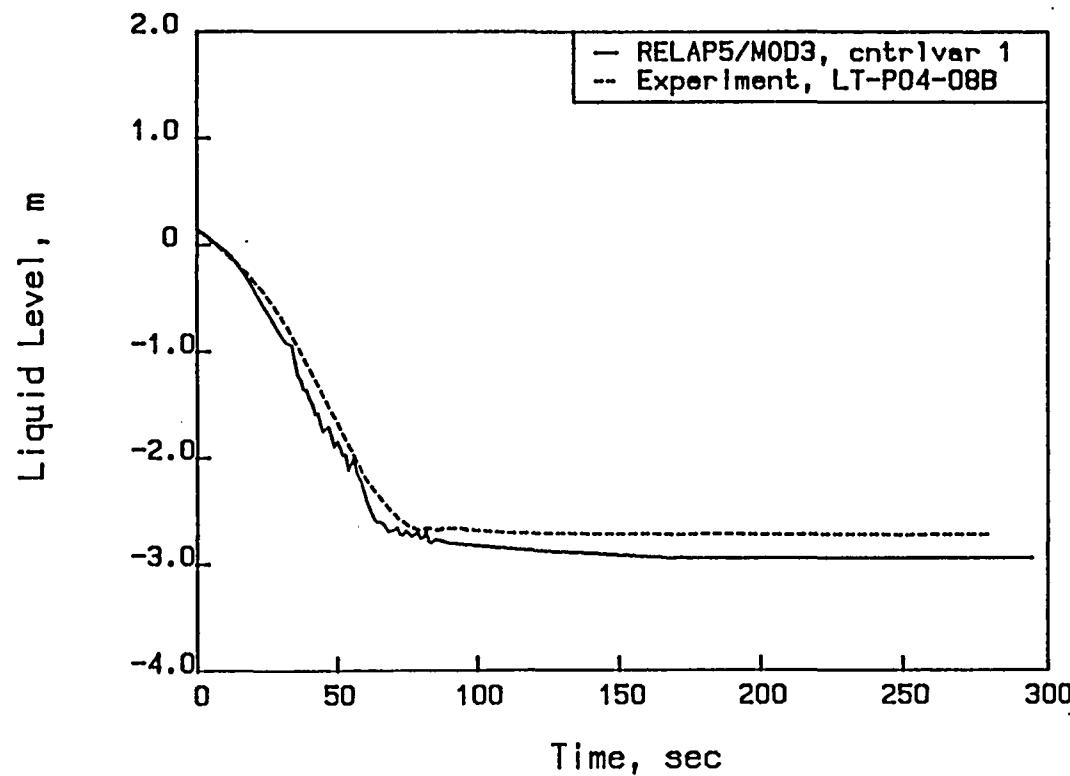


Fig.9 Comparison of SG collapsed liquid level (short term)

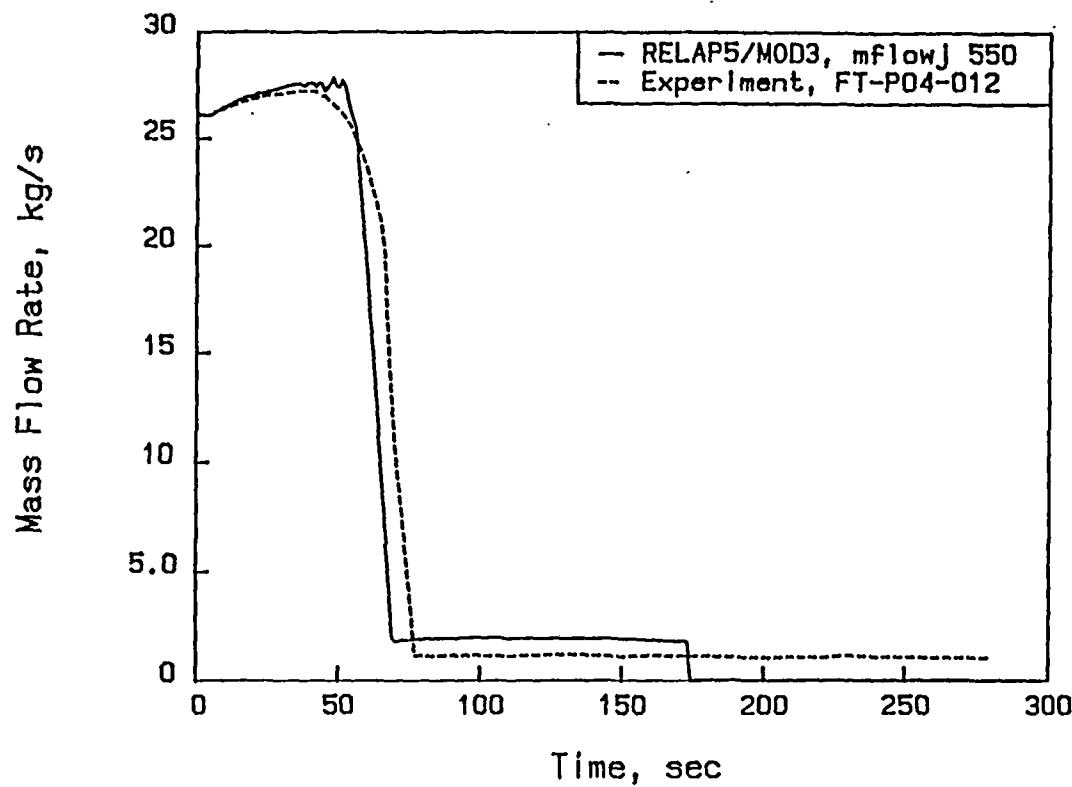


Fig.10 Comparison of mass flow rate through MCV (short term)

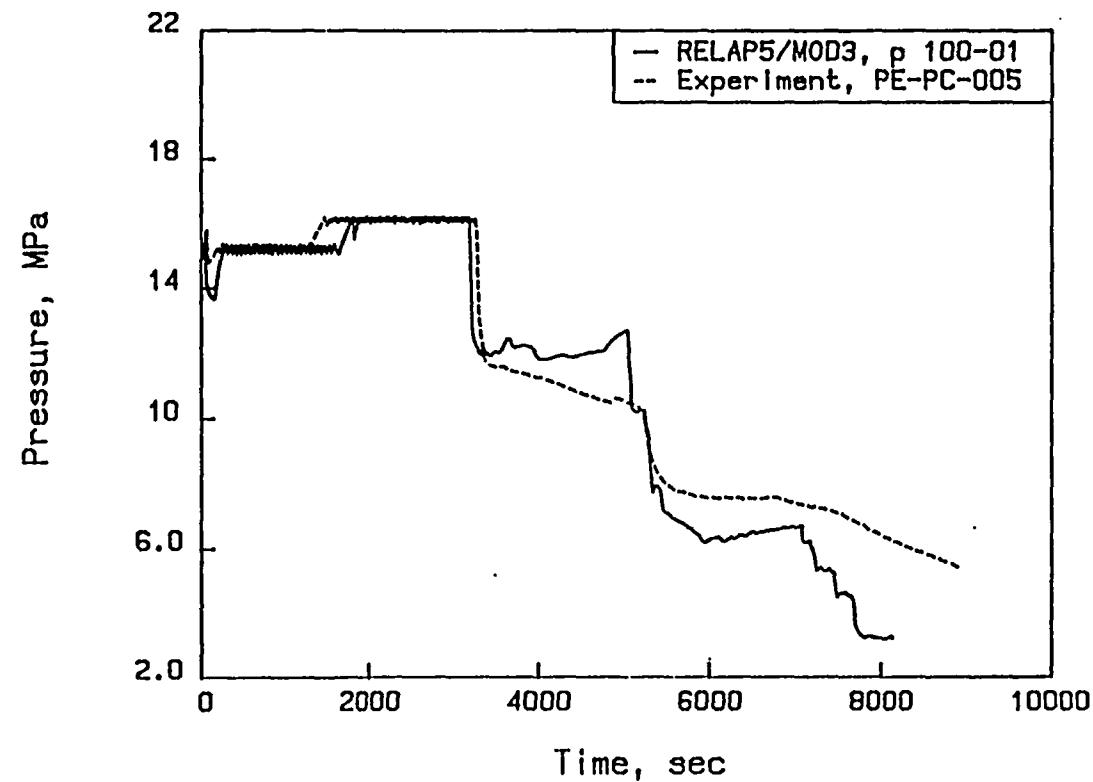


Fig.11 Comparison of pressure at the intact loop hot leg (long term)

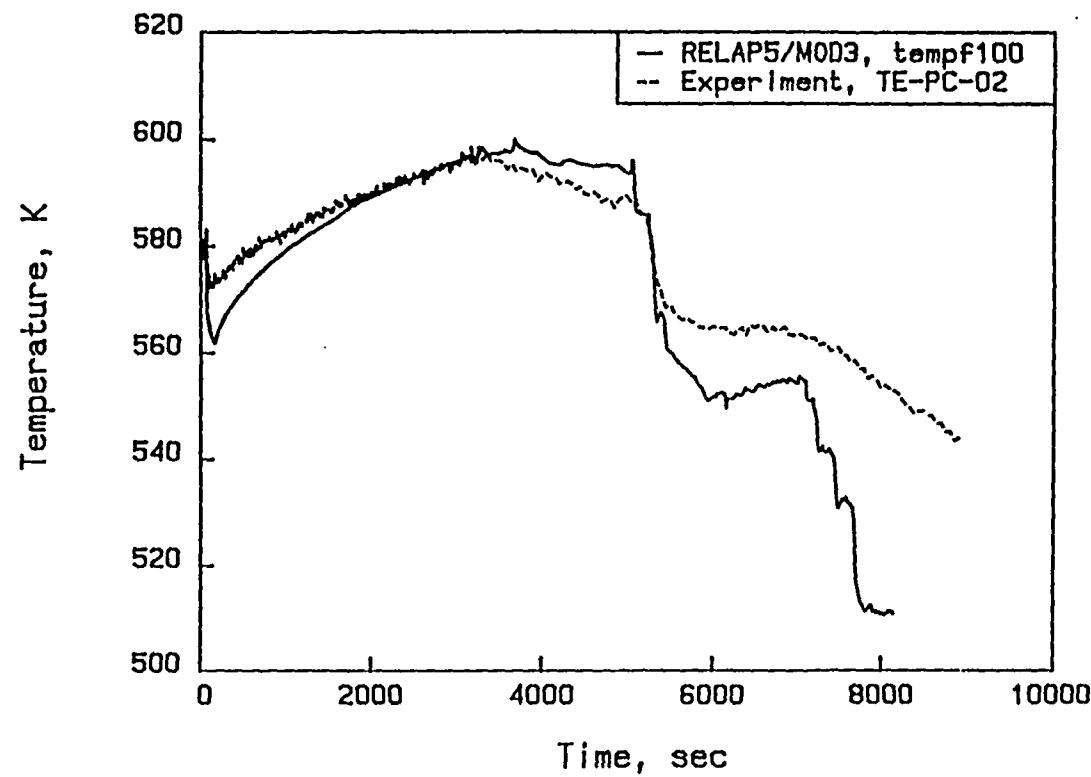


Fig.12 Comparison of coolant temperature at the intact loop hot leg
(long term)

-17-

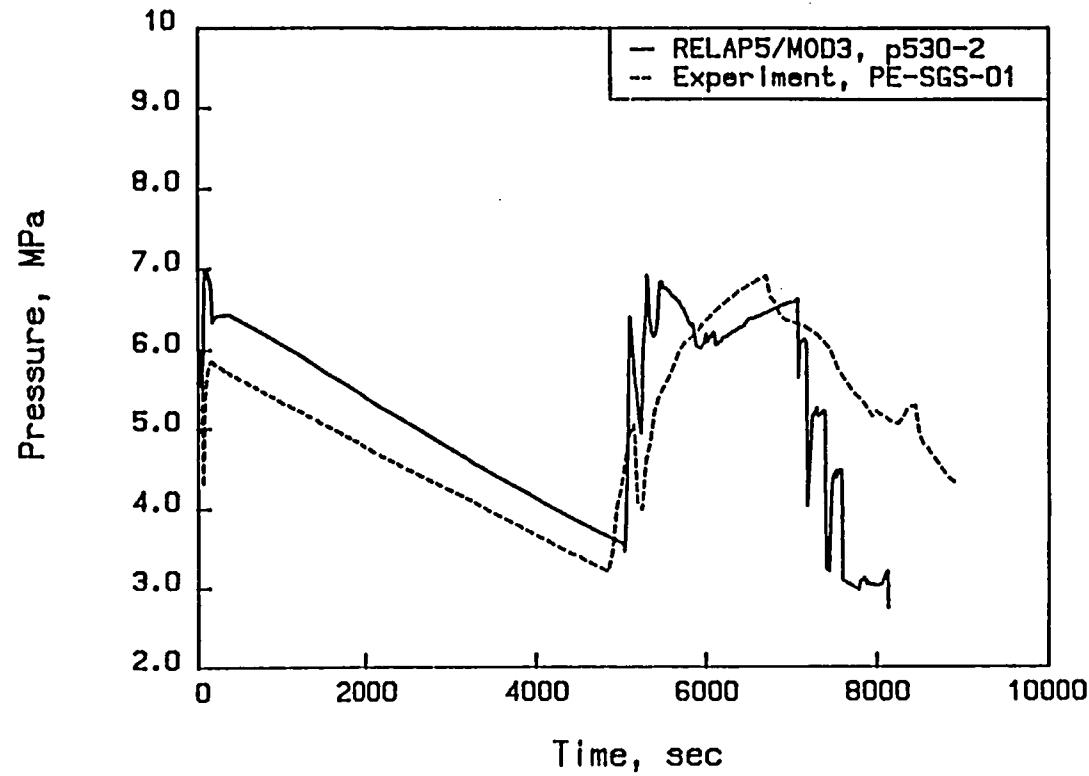


Fig.13 Comparison of pressure at SG steam dome (long term)

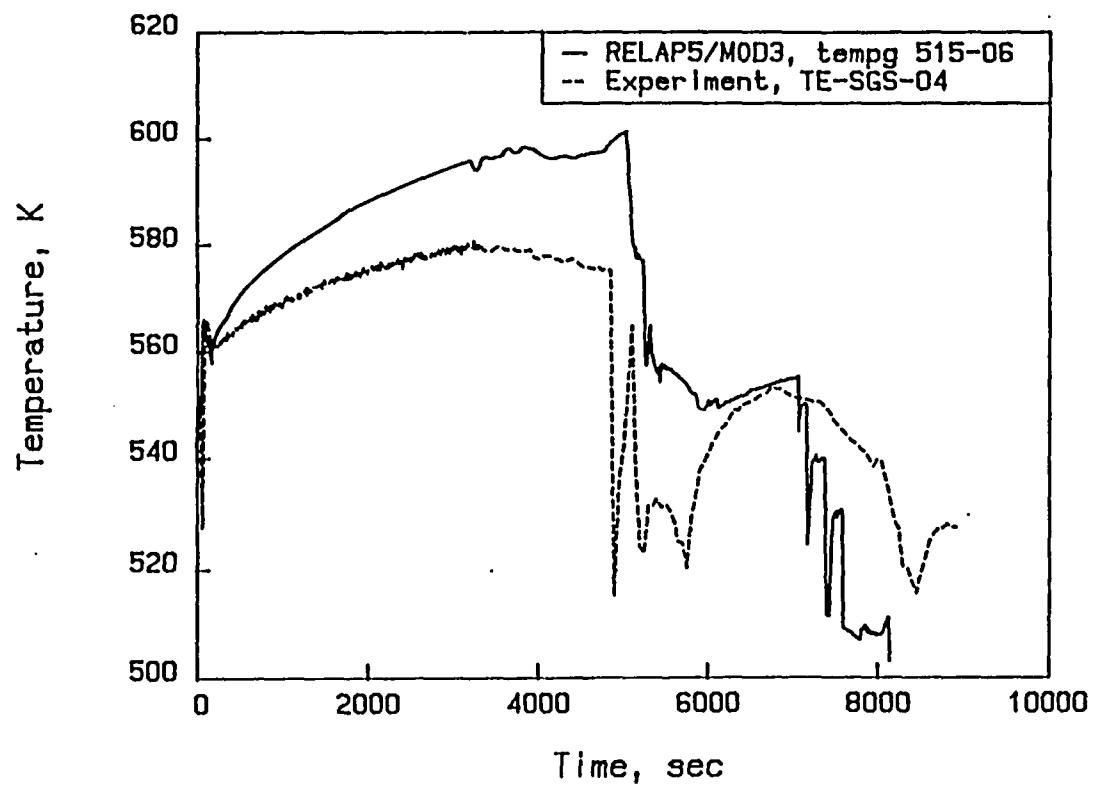


Fig.14 Comparison of coolant temperature at SG secondary side (long term)

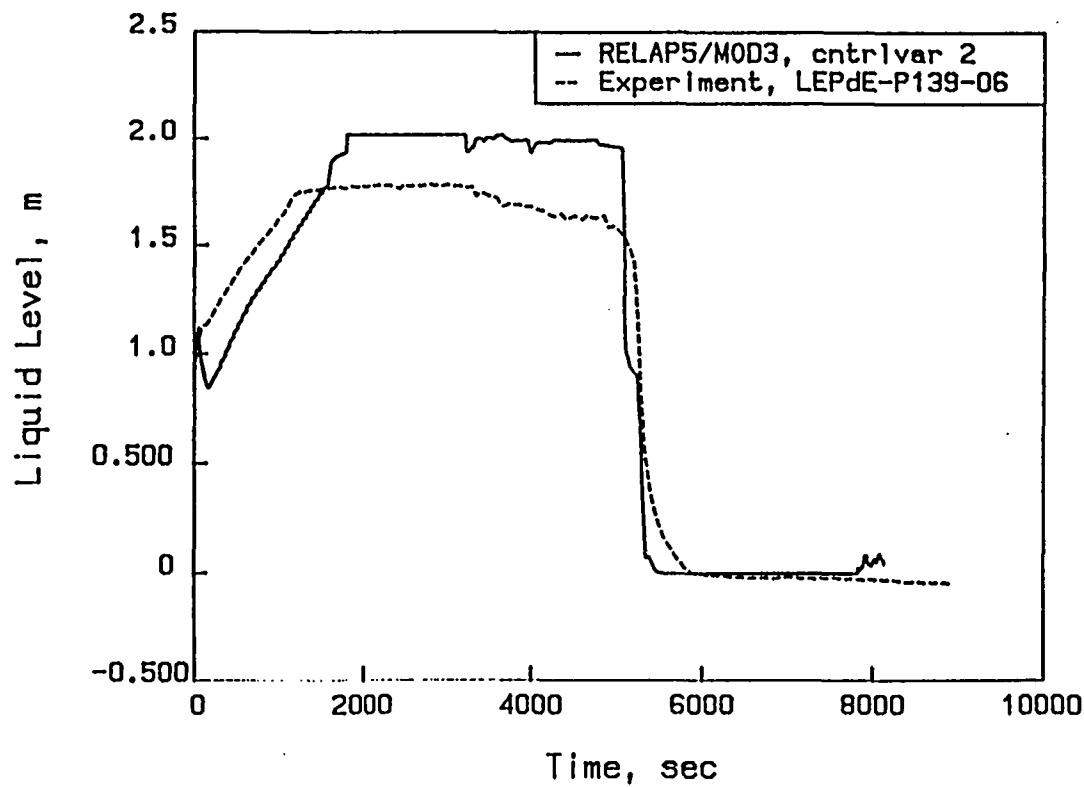


Fig.15 Comparison of pressurizer collapsed liquid level (long term)

-05-

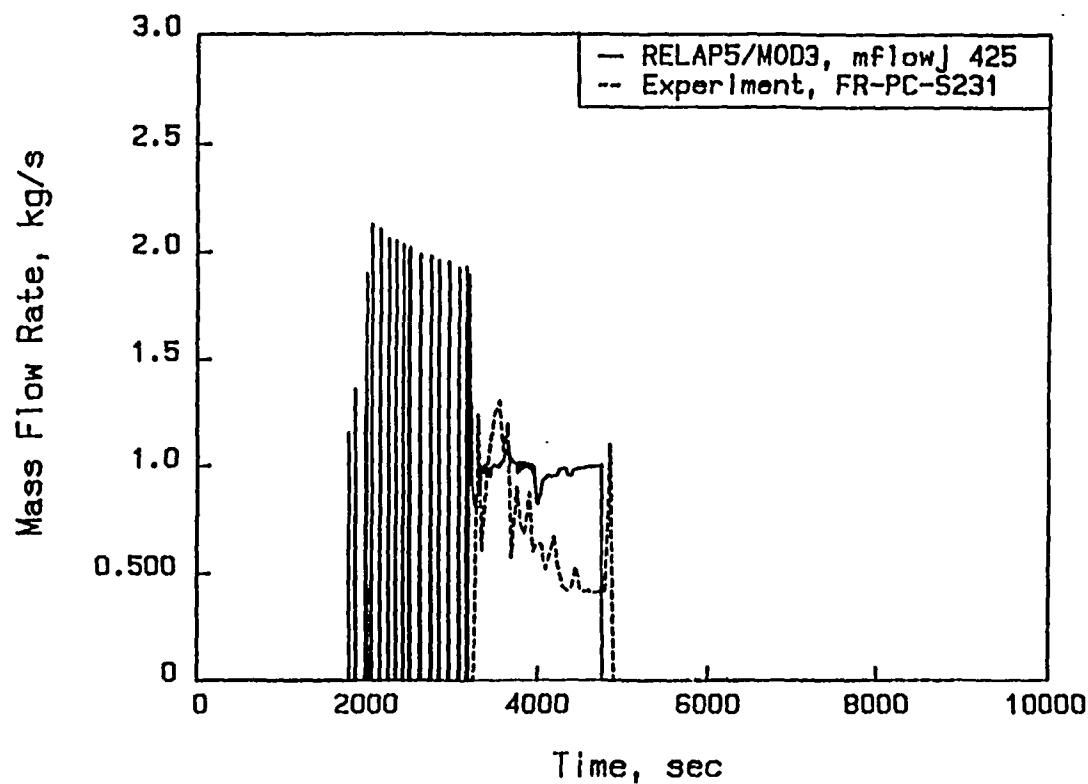


Fig.16 Comparison of mass flow rate through PORV (long term)

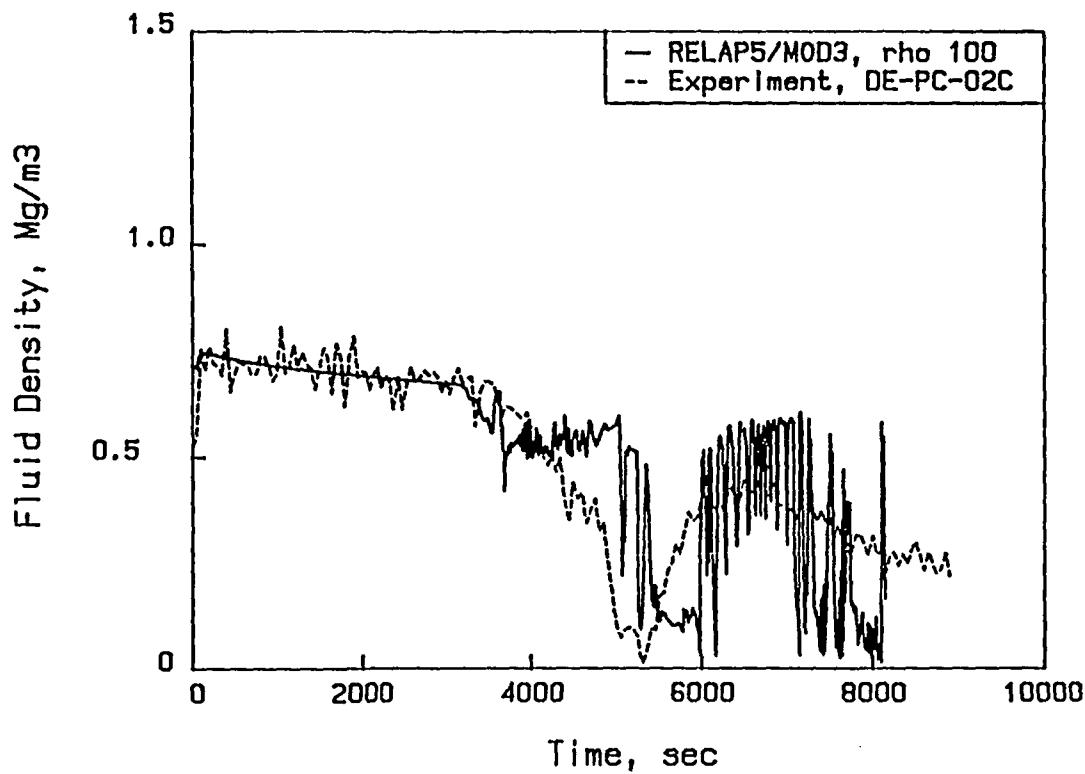


Fig.17 Comparison of fluid density at intact loop hot leg (long term)

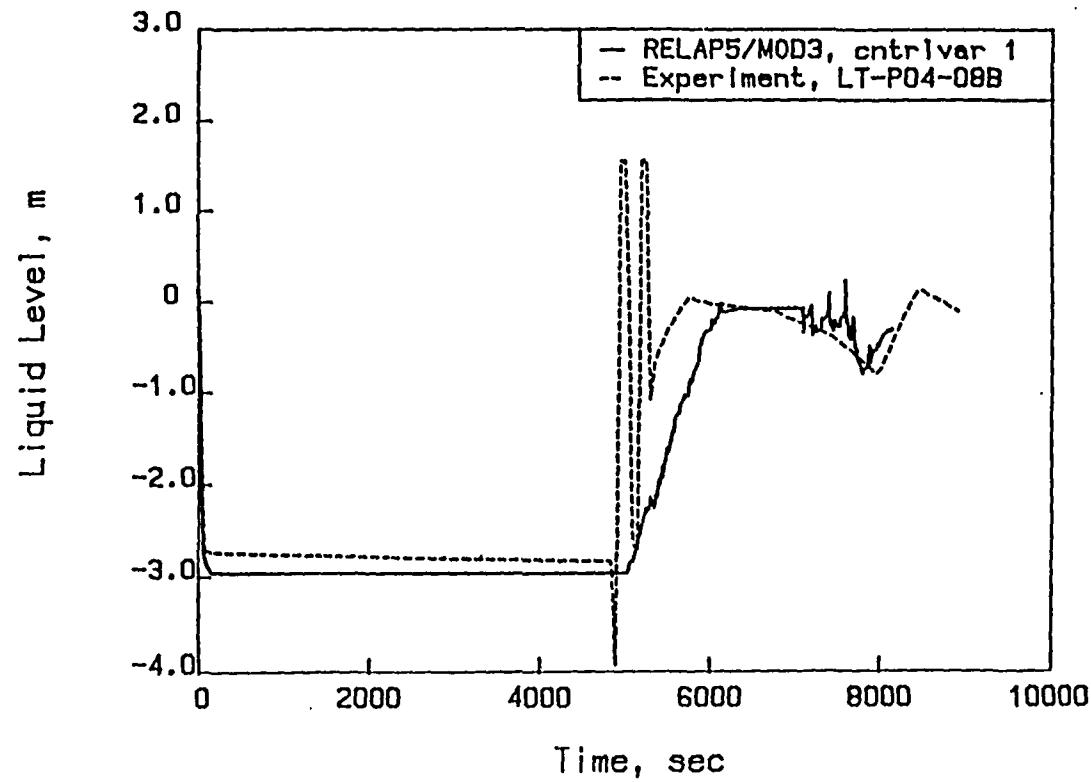


Fig.18 Comparison of SG collapsed liquid level (long term)

-35-

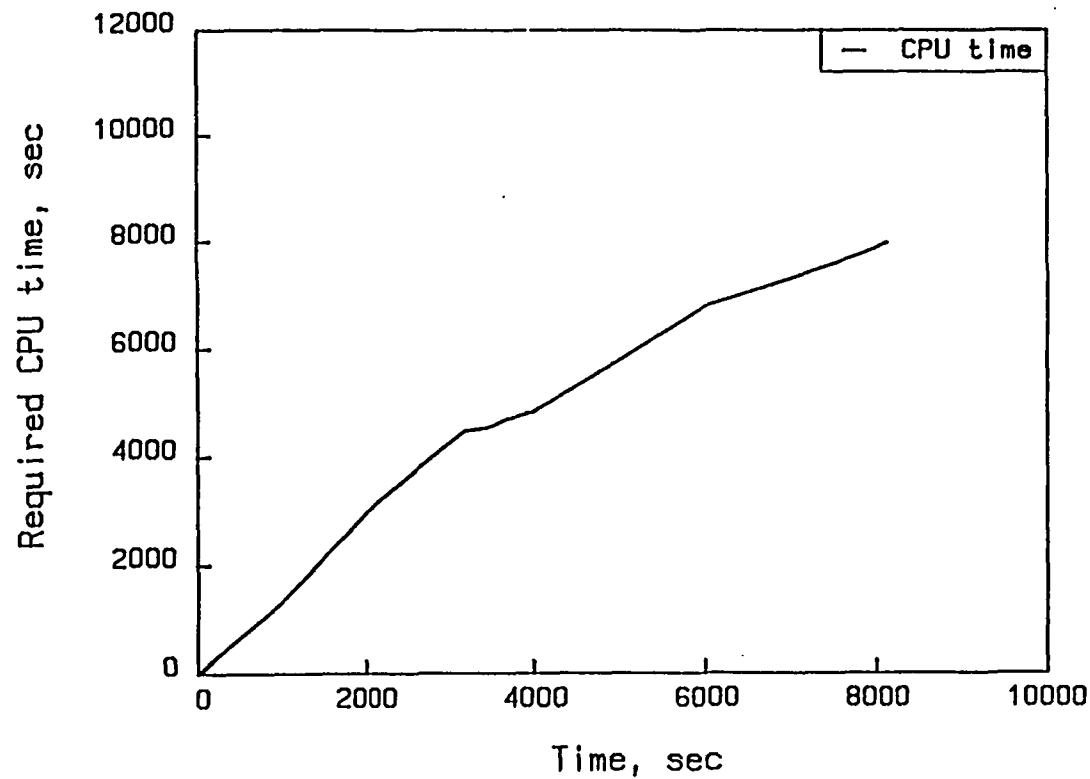


Fig.19 The required CPU time versus the advanced time

-45-

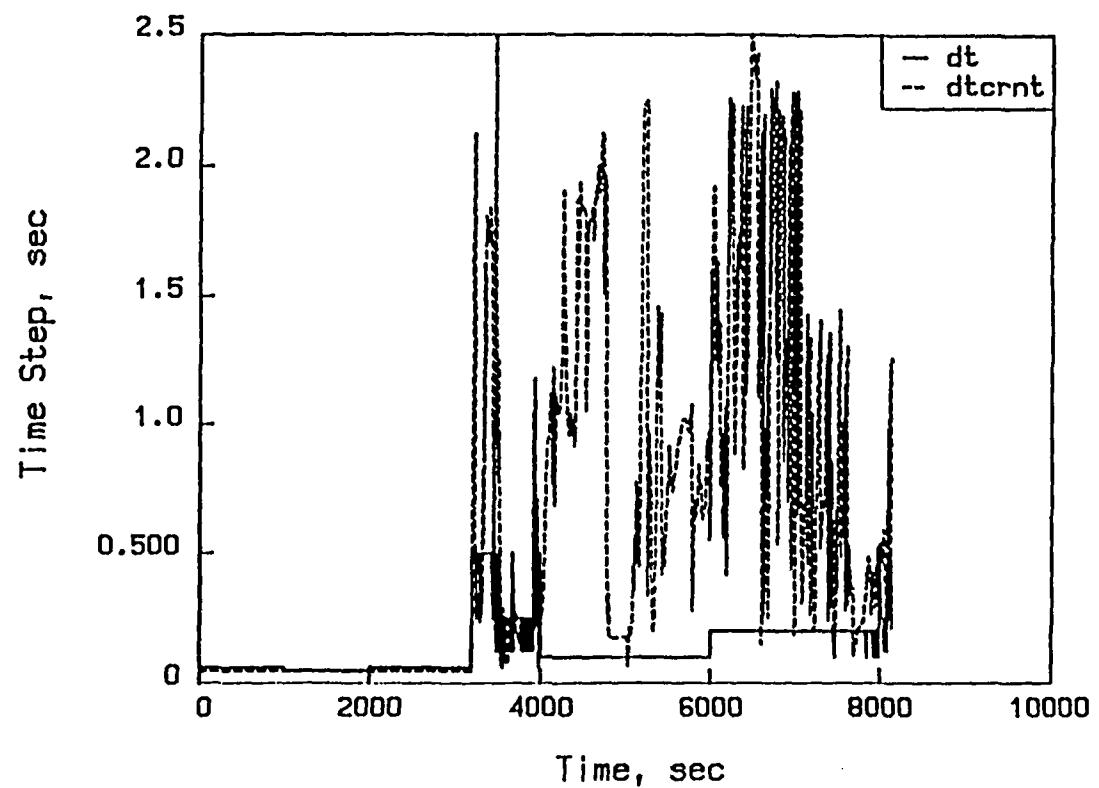


Fig.20 Time step size of base case calculation

Appendix A Input Deck for Steady State Calculation



```

=loft 19-1 post test analysis deck
*-----1-----1-----1-----1-----1-----1-----
* initial conditions
*
* core power = 50. mw
* pcf flow = 479.3 kg/s
* thot = 578. k
* tcold = 559.0 k
*
*-----1-----1-----1-----1-----1-----1-----
0000100 new stdy-st
0000101 run
0000102 si
0000105 5. 10.
0000110 nitrogen
* time step control cards
* end time min dt max dt optn mnr mjr rst
*0000201 5400.0 1.e-6 0.5 2 4 200 200
*-----1-----1-----1-----1-----1-----1-----
* modification for steady state run at 91/2/8
*-----1-----1-----1-----1-----1-----1-----
0000201 1000.0 1.e-6 0.5 2 4 500 200
***** minor edit variables
*****
* pressure
*****
0000301 p 345010000 * pe-bl-1
0000302 p 310010000 * pe-bl-2
0000303 p 315110000 * pe-bl-3
0000304 p 350010000 * pe-bl-4
0000305 p 315090000 * pe-bl-6
0000306 p 350020000 * pe-bl-8
0000307 p 185010000 * pe-pc-1
0000308 p 100010000 * pe-pc-2
0000309 p 420010000 * porv inlet
0000310 p 110010000 * pt-139-2,3,4
0000311 p 245010000 * pe-lup-1a,1b
0000312 p 215010000 * pe-1st-1a,b/pe-2st-1a,b
0000313 p 200010000 * pe-1st-3a,3b
0000314 p 530020000 * pt-p4-10a
0000315 p 535010000 * pt-p4-85
***** temperatures
*****
0000320 tempf 406010000 * spray tempf
0000321 tempf 310010000 * te-bl-2a,2b,2c
0000322 tempf 100010000 * te-pc-2a,2b,2c
0000323 tempf 185010000 * te-pc-1
0000324 tempf 115030000 * te-sg-1
0000325 tempf 115100000 * te-sg-2
0000326 tempf 515040000 * te-sg-3
0000328 tempf 415050000 * pzs volume 5
0000329 tempf 415040000 * te-139-19
0000330 tempf 415030000 * tc-139-20
0000331 tempf 315120000 * te-p138-171
0000332 tempf 350020000 * te-p138-170
0000333 tempf 205010000 * te-1st-1/te-2st-1
0000334 tempf 210010000 * te-1st-2/te-2st-2
0000335 tempf 345010000 * te-bl-1
0000336 tempf 210030000 * te-1st-14/te-2st-14
0000337 tempf 210040000 * te-3up-2
0000338 tempf 245010000 * te-1up-6
0000339 tempf 246010000 * te-2up-4
0000340 tempf 250010000 * te-1up-3
***** densities
*****
0000341 rho 345010000 * de-bl-1
0000342 rho 310010000 * de-bl-2
0000343 rho 185010000 * de-pc-1
0000344 rho 100010000 * de-pc-2
0000345 rho 115120000 * de-pc-3
0000346 voidgj 400010000 * surge line density
0000347 rho 115040000 * s/g tubes
0000348 rho 115050000 * s/g tubes
0000349 rho 115060000 * s/g tubes
0000350 rho 115070000 * s/g tubes
***** velocities
*****
0000351 voidf 100010000 * ilhl nozzle
0000352 velf 100010000 * ilhl nozzle
0000353 velf 115030000 * s/g inlet
0000354 velf 400010000 * surge line
0000355 velfj 425000000 * porv liq vel
0000356 velg 100010000 * ilhl nozzle
0000357 velg 115030000 * s/g inlet
0000358 velg 400010000 * surge line
0000359 velgj 425000000 * porv vap vel
***** mass flow rates
*****
0000360 mflowj 100010000 * ilhl nozzle
0000361 mflowj 150010000 * pump outlet
0000362 mflowj 185020000 * dtt-rake ilcl
0000363 mflowj 400010000 * pres. surge line flow
0000364 mflowj 407000000 * pzs spray flow
0000366 mflowj 425000000 * pres. relief valve flow
0000367 mflowj 550000000 * steam flow control valve
0000368 mflowj 548000000 * aux feed
0000369 mflowj 560000000 * main feed
0000370 cntrivar 1 * s/g level
***** cladding temperatures center module
*****
0000371 httemp 230000110 * te-5h5-015
0000372 httemp 230000210 * te-5h5-034
0000373 httemp 230000310 * te-5h5-049
*****
```

* peak centerline temperatures	*													

0000374	htemp	230000101	* core lower region	0000522	p	530020000	gt null	0	6.3448275e6	n				
0000375	htemp	230000201	* core middle region	0000523	p	530020000	lt null	0	6.4137931e6	n				
0000376	htemp	230000301	* core upper region	0000530	time	0	ge null	0	3600.0	n				

* reactor kinetic parameters				0000531	p	530020000	gt p	547010000	0.0	n				

0000377	rktppow	0	* total reactor power	0000536	time	0	ge null	0	10000.0	n				
0000378	rkfipow	0	* fission decay power	0000540	tempf	100010000	gt null	0	583.16	l				
0000379	rkgapow	0	* gamma decay power	0000541	p	100010000	gt null	0	1.574553e7	l				
0000380	rkreac	0	* reactivity	0000550	time	0	ge null	0	10000.0	l				
0000381	pmphead	135	* pcp1 head	0000551	time	0	ge timeof	625	0.0	l				
0000382	pmphead	165	* pcp2 head	0000552	time	0	ge timeof	509	1580.	l				
0000384	cntrivar	2	* pzc level	0000560	p	100010000	le null	0	13.15862e6	n				
0000385	cntrivar	3	* rx vessel level	0000561	time	0	ge timeof	552	265.0	l				
0000386	mflowj	185010000		0000562	time	0	gt null	0	5400.0	n				
0000387	mflowj	185030000		0000563	cntrivar	1	lt null	0	2.1844	n				
0000388	mflowj	200020000		0000564	cntrivar	1	gt null	0	2.9464	n				
0000389	pmpvel	135		0000565	time	0	ge timeof	669	966.	l				
0000390	pmpvel	165		0000570	p	420010000	gt null	0	1.620058e7	n				

*				0000571	p	420010000	lt null	0	1.606269e7	n				
* trips				0000572	p	420010000	lt null	0	1.486300e7	n				
*				0000573	p	420010000	gt null	0	1.506980e7	n				
* variable trips				0000574	p	420010000	gt null	0	1.533874e7	n				

0000501	p	100010000	le null	0	14.193103e6	l	0000575	p	420010000	lt null	0	1.505000e7	n	
* ecc check valve				0000576	p	420010000	lt null	0	1.482853e7	n				
0000502	p	600010000	ge p		185010000	20.e6	0000577	p	420010000	gt null	0	1.495950e7	n	
* accumulator check valve				*****										
0000503	p	615010000	ge p		185010000	20.e6	* logical trips							
* isolation valve hot leg				*****										
0000504	time	0	lt null	0	0.0	1	0000600	670						
* isolation valve cold leg				0000601	563	and	561	n						
0000505	time	0	lt null	0	0.0	1	0000602	-563	and	-564	n			
* qobv hot leg				0000603	655	and	602	n						
0000506	time	0	lt null	0	0.0	1	0000604	609	or	609	l			
* qobv cold leg				0000605	572	and	-509	n						
0000507	time	0	lt null	0	0.0	1	0000606	-572	and	-573	n			
* check valve surge line pressurizer				0000607	608	and	606	n						
0000508	time	0	ge null	0	0.0	1	0000608	605	or	607	n			
* pressurizer relief valve				*0000609	540	or	541	l						
0000509	tempf	100010000	ge null	0	597.0	1	* modification for steady state run at 91/2/8							
* steam control valve				0000609	504	or	504	l						
0000510	time	0	lt null	0	0.0	1	0000610	612	or	520	n			
* boundary system valve				0000611	-521	and	-616	n						
0000511	time	0	lt null	0	0.0	1	0000612	611	and	610	n			
* lpis trip				0000613	616	or	523	n						
0000512	time	0	ge null	0	10000.0	1	0000614	-522	and	613	n			
* hpis trip				0000615	-612	and	609	n						
0000513	time	0	ge null	0	10000.0	1	0000616	615	and	614	n			
*				0000617	612	or	616	n						
0000520	p	530020000	gt null	0	7.103448e6	n	0000618	605	or	607	n			
0000521	p	530020000	lt null	0	7.0344827e6	n	0000621	623	or	570	n			
				0000622	-571	and	-571	n						
				0000623	621	and	622	n						
				0000624	509	and	-552	n						
				0000625	623	or	624	n						
				0000626	576	and	-509	n						


```

1150907 0.0   0.0   9
1150908 0.05  0.05  11
1150909 0.1   0.1   12
1151001 000000 13
1151101 000100  3
1151102 000000  8
1151103 000100 12
1151201 0 14871600. 1346350. 2462710.0 0.0 0.001
1151202 0 14877200. 1346350. 2462600.0 0.0 0.002
1151203 0 14793300. 1346370. 2464340.0 0.0 0.003
1151204 0 14770000. 1321980. 2464840.0 0.0 0.004
1151205 0 14746400. 1301720. 2465340.0 0.0 0.005
1151206 0 14729700. 1283950. 2465690.0 0.0 0.006
1151207 0 14721700. 1268380. 2465870.0 0.0 0.007
1151208 0 14715000. 1254890. 2466020.0 0.0 0.008
1151209 0 14707300. 1242570. 2466180.0 0.0 0.009
1151210 0 14707600. 1242600. 2466180.0 0.0 0.010
1151211 0 14631100. 1242600. 2467720.0 0.0 0.011
1151212 0 14621800. 1242600. 2467980.0 0.0 0.012
1151213 0 14616700. 1242600. 2468100.0 0.0 0.013
1151300 0
1151301 10.728000 10.670000 0.0 01
1151302 8.3370000 8.4284000 0.0 02
1151303 4.4456000 4.7693000 0.0 03
1151304 4.3865000 4.2164000 0.0 04
1151305 4.3407000 4.6700000 0.0 05
1151306 4.3009000 4.6296000 0.0 06
1151307 4.2676000 4.5954000 0.0 07
1151308 4.2398000 4.5671000 0.0 08
1151309 4.2249000 4.5338000 0.0 09
1151310 7.9665000 8.1922000 0.0 10
1151311 9.4925000 9.9460000 0.0 11
1151312 10.040000 10.505000 0.0 12
*****
* pump data
*****
* pump suction tee
*****
1200000 pmpscrt branch
1200001 3 0
1200101 0.0634 0.76 0.0 0.0 0.0 0.0
1200102 4.0e-5 0.0 00000
1200200 0 14613100. 1242600. 2468180.0 0.0
1201101 115010000 120000000 0.0 0.1 0.1 000000
1202101 120010000 125000000 0.0317 0.2 0.2 000100
1203101 120010000 155000000 0.0317 0.2 0.2 000100
1201201 10.040000 10.505000 0.0
1202201 5.2077000 5.2983000 0.0
1203201 5.2071000 5.2944000 0.0
*****
* pmp1 suction tee outlet
*****
1250000 pmp1scrt branch
1250001 2 0
1250101 0.0 1.003 0.0613 0.0 90.0 0.521
1250102 4.0e-5 0.0 00000
1250200 0 14600300. 1242600. 2468180.0 0.0
1251101 125010000 130000000 0.0 0.1 0.1 000100
1252101 125000000 155000000 0.0 0.0 0.0 000100
1251201 7.8711000 8.2528000 0.0
1252201 -11855000 -1.3539000 0.0
*****
* pump 1 inlet
*****
1300000 pmp1inlet snglvol
1300101 0.0 0.457 0.0189 0.0 90.0 0.457
1300102 4.0e-5 0.0 00000
1300200 0 14578200. 1242600. 2468900.0 0.0
*****
* primary coolant pump 1
*****
1350000 pcpump1 pump
1350101 0.0366 0.0 0.099 0.0 90.0 0.319
1350102 00000
1350108 130010000 0.0 0.0 0.0 0.0 000100
1350109 140000000 0.0 0.05 0.05 0.05 000100
1350200 0 14818100. 1242890. 2463900.0 0.0
1350201 0 8.8943000 9.2942000 0.0
1350202 0 8.8928000 8.1177000 0.0
*1350301 0 0 0 -1 0 509 0
* -----
* modification for steady state run at 91/28
* -----
1350301 0 0 0 -1 -1 504 0
1350302 369.00 .90178860 .31550 96.00 500.600 1.4310000
1350303 613.6 0.0 207.0000 0.00400 19.598000 0.0
1350310 0.0 0.0 0.0
* -----
* -----
* single phase head curves
*****
* head curve no. 1
* -----
1351100 1 1
1351101 0.000000e+00 1.403600e+00
1351102 1.906100e-01 1.363600e+00
1351103 3.896300e-01 1.318600e+00
1351104 5.939600e-01 1.232800e+00
1351105 7.902000e-01 1.133600e+00
1351106 1.000000e+00 1.000000e+00
* -----
* head curve no. 2
* -----
1351200 1 2
1351201 0.000000e+00 -6.700000e-01
1351202 2.000000e-01 -5.000000e-01
1351203 4.000000e-01 -2.500000e-01
1351204 5.755400e-01 0.000000e+00
1351205 7.443200e-01 2.583000e-01
1351206 7.734800e-01 3.778000e-01

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1351704 -4.000000e-01 -5.000000e-02
1351705 -2.000000e-01 1.500000e-01
1351706 0.000000e+00 2.500000e-01
*----1----1----1----1----1----1----1----1
* head curve no. 8
*----1----1----1----1----1----1----1----1
1351800 1 8
1351801 -1.000000e+00 -1.000000e+00
1351802 -8.000000e-01 -9.700000e-01
1351803 -6.000000e-01 -9.500000e-01
1351804 -4.000000e-01 -8.800000e-01
1351805 -2.000000e-01 -8.000000e-01
1351806 0.000000e+00 -6.700000e-01
*****single phase torque data*****
*****single phase torque data*****
* torque curve no. 1
*----1----1----1----1----1----1----1----1
1351900 2 1
1351901 0.000000e+00 6.032000e-01
1351902 1.930000e-01 6.325000e-01
1351903 3.930000e-01 7.369000e-01
1351904 5.955200e-01 8.331000e-01
1351905 7.978200e-01 9.229000e-01
1351906 1.000000e+00 1.000000e+00
*----1----1----1----1----1----1----1----1
* torque curve no. 2
*----1----1----1----1----1----1----1----1
1352000 2 2
1352001 0.000000e+00 -6.700000e-01
1352002 4.000000e-01 -2.500000e-01
1352003 5.000000e-01 1.500000e-01
1352004 7.372550e-01 5.265860e-01
1352005 7.680490e-01 6.065940e-01
1352006 8.672300e-01 7.436600e-01
1352007 1.000000e+00 1.000000e+00
*----1----1----1----1----1----1----1----1
* torque curve no. 3
*----1----1----1----1----1----1----1----1
1352100 2 3
1352101 -1.000000e+00 1.984300e+00
1352102 -8.009600e-01 1.394000e+00
1352103 -6.063800e-01 1.097500e+00
1352104 -4.068600e-01 8.220000e-01
1352105 -1.992800e-01 6.648000e-01
1352106 0.000000e+00 6.032000e-01
*----1----1----1----1----1----1----1----1
* torque curve no. 4
*----1----1----1----1----1----1----1----1
1352200 2 4
1352201 -1.000000e+00 1.984300e+00
1352202 -8.223400e-01 1.830800e+00
1352203 -6.337100e-01 1.682400e+00
1352204 -4.585300e-01 1.557000e+00
1352205 -2.670230e-01 1.436200e+00
1352206 -1.761070e-01 1.387900e+00

```

1352207	-8.931000e-02	1.348100e+00	1353011	9.000000e-01	8.000000e-01
1352208	0.000000e+00	1.233610e+00	1353012	9.600000e-01	5.000000e-01
*----1-----1-----1-----1-----1-----1-----			1353013	1.000000e+00	0.000000e+00
* torque curve no. 5			*----1-----1-----1-----1-----1-----1-----		
*----1-----1-----1-----1-----1-----1-----			* torque curve		
1352300	2	5	*----1-----1-----1-----1-----1-----1-----		
1352301	0.000000e+00	-4.500000e-01	1353100	0	
1352302	4.000000e-01	-2.500000e-01	1353101	0.000000e+00	0.000000e+00
1352303	5.000000e-01	0.000000e+00	1353102	1.250000e-01	7.000000e-02
1352304	1.000000e+00	3.569000e-01	1353103	1.650000e-01	1.250000e-01
*----1-----1-----1-----1-----1-----1-----			1353104	2.400000e-01	5.600000e-01
* torque curve no. 6			1353105	8.000000e-01	5.600000e-01
*----1-----1-----1-----1-----1-----1-----			1353106	9.600000e-01	4.500000e-01
1352400	2	6	1353107	1.000000e+00	0.000000e+00
1352401	0.000000e+00	1.233610e+00	******	******	******
1352402	9.064300e-02	1.196500e+00	pump 2-phase difference data		
1352403	1.885690e-01	1.109600e+00	******	******	******
1352404	2.734700e-01	1.041600e+00	* head curve no. 1		
1352405	4.586690e-01	8.958000e-01	*----1-----1-----1-----1-----1-----1-----		
1352406	5.744800e-01	7.807000e-01	1354100	1	1
1352407	7.381600e-01	6.134000e-01	1354101	0.000000e+00	0.000000e+00
1352408	7.685200e-01	5.849000e-01	1354102	1.000000e-01	8.300000e-01
1352409	8.700570e-01	4.877000e-01	1354103	2.000000e-01	1.090000e+00
1352410	1.000000e+00	3.569000e-01	1354104	5.000000e-01	1.020000e+00
*----1-----1-----1-----1-----1-----1-----			1354105	7.000000e-01	1.010000e+00
* torque curve no. 7			1354106	9.000000e-01	9.400000e-01
*----1-----1-----1-----1-----1-----1-----			1354107	1.000000e+00	1.000000e+00
1352500	2	7	*----1-----1-----1-----1-----1-----1-----		
1352501	-1.000000e+00	-1.000000e+00	* head curve no. 2		
1352502	-3.000000e-01	-9.000000e-01	*----1-----1-----1-----1-----1-----1-----		
1352503	-1.000000e-01	-5.000000e-01	1354200	1	2
1352504	0.000000e+00	-4.500000e-01	1354201	0.000000e+00	0.000000e+00
*----1-----1-----1-----1-----1-----1-----			1354202	1.000000e-01	-4.000000e-02
* torque curve no. 8			1354203	2.000000e-01	0.000000e+00
*----1-----1-----1-----1-----1-----1-----			1354204	3.000000e-01	1.000000e-01
1352600	2	8	1354205	4.000000e-01	2.100000e-01
1352601	-1.000000e+00	-1.000000e+00	1354206	8.000000e-01	6.700000e-01
1352602	-2.500000e-01	-9.000000e-01	1354207	9.000000e-01	8.000000e-01
1352603	-8.000000e-02	-8.000000e-01	1354208	1.000000e+00	1.000000e+00
1352604	0.000000e+00	-6.700000e-01	*----1-----1-----1-----1-----1-----1-----		
******			* head curve no. 3		
two - phase multiplier data from 19-1 test data			*----1-----1-----1-----1-----1-----1-----		
******			1354300	1	3
* head curve			1354301	-1.000000e+00	-1.160000e+00
*----1-----1-----1-----1-----1-----1-----			1354302	-9.000000e-01	-1.240000e+00
1353000	0		1354303	-8.000000e-01	-1.770000e+00
1353001	0.000000e+00	0.000000e+00	1354304	-7.000000e-01	-2.360000e+00
1353002	2.000000e-02	2.000000e-02	1354305	-6.000000e-01	-2.790000e+00
1353003	6.000000e-02	5.000000e-02	1354306	-5.000000e-01	-2.910000e+00
1353004	1.000000e-01	1.000000e-01	1354307	-4.000000e-01	-2.670000e+00
1353005	2.000000e-01	4.600000e-01	1354308	-2.500000e-01	-1.690000e+00
1353006	2.400000e-01	8.000000e-01	1354309	-1.000000e-01	-5.000000e-01
1353007	3.000000e-01	9.600000e-01	1354310	0.000000e+00	0.000000e+00
1353008	4.000000e-01	9.800000e-01	*----1-----1-----1-----1-----1-----1-----		
1353009	6.000000e-01	9.700000e-01	* head curve no. 4		
1353010	8.000000e-01	9.000000e-01	*----1-----1-----1-----1-----1-----1-----		

1354400	1	4
1354401	-1.000000e+00	-1.160000e+00
1354402	-9.000000e-01	-7.800000e-01
1354403	-8.000000e-01	-5.000000e-01
1354404	-7.000000e-01	-3.100000e-01
1354405	-6.000000e-01	-1.700000e-01
1354406	-5.000000e-01	-8.000000e-02
1354407	-3.500000e-01	0.000000e+00
1354408	-2.000000e-01	5.000000e-02
1354409	-1.000000e-01	8.000000e-02
1354410	0.000000e+00	1.100000e-01
*----1----1----1----1----1----1----		
* head curve no. 5		
*----1----1----1----1----1----1----		
1354500	1	5
1354501	0.000000e+00	0.000000e+00
1354502	2.000000e-01	-3.400000e-01
1354503	4.000000e-01	-6.500000e-01
1354504	6.000000e-01	-9.300000e-01
1354505	8.000000e-01	-1.190000e+00
1354506	1.000000e+00	-1.470000e+00
*----1----1----1----1----1----1----		
* head curve no. 6		
*----1----1----1----1----1----1----		
1354600	1	6
1354601	0.000000e+00	1.100000e-01
1354602	1.000000e-01	1.300000e-01
1354603	2.500000e-01	1.500000e-01
1354604	4.000000e-01	1.300000e-01
1354605	5.000000e-01	7.000000e-02
1354606	6.000000e-01	-4.000000e-02
1354607	7.000000e-01	-2.300000e-01
1354608	8.000000e-01	-5.100000e-01
1354609	9.000000e-01	-9.100000e-01
1354610	1.000000e+00	-1.470000e+00
*----1----1----1----1----1----1----		
* head curve no. 7		
*----1----1----1----1----1----1----		
1354700	1	7
1354701	-1.000000e+00	0.000000e+00
1354702	0.000000e+00	0.000000e+00
*----1----1----1----1----1----1----		
* head curve no. 8		
*----1----1----1----1----1----1----		
1354800	1	8
1354801	-1.000000e+00	0.000000e+00
1354802	0.000000e+00	0.000000e+00
*----1----1----1----1----1----1----		
* torque curve no. 1		
*----1----1----1----1----1----1----		
1354900	2	1
1354901	0.000000e+00	6.032000e-01
1354902	1.930000e-01	6.325000e-01
1354903	3.930000e-01	7.369000e-01
1354904	5.955200e-01	8.331000e-01
1354905	7.978200e-01	9.229000e-01

1354906	1.000000e+00	1.000000e+00
*----1----1----1----1----1----1----		
* torque curve no. 2		
*----1----1----1----1----1----1----		
1355000	2	2
1355001	0.000000e+00	-6.700000e-01
1355002	4.000000e-01	-2.500000e-01
1355003	5.000000e-01	1.500000e-01
1355004	7.372550e-01	5.265860e-01
1355005	7.680490e-01	6.065940e-01
1355006	8.672300e-01	7.436600e-01
1355007	1.000000e+00	1.000000e+00
*----1----1----1----1----1----1----		
* torque curve no. 3		
*----1----1----1----1----1----1----		
1355100	2	3
1355101	-1.000000e+00	1.984300e+00
1355102	-8.009600e-01	1.394000e+00
1355103	-6.063800e-01	1.097500e+00
1355104	-4.068600e-01	8.220000e-01
1355105	-1.992800e-01	6.648000e-01
1355106	0.000000e+00	6.032000e-01
*----1----1----1----1----1----1----		
* torque curve no. 4		
*----1----1----1----1----1----1----		
1355200	2	4
1355201	-1.000000e+00	1.984300e+00
1355202	-8.223400e-01	1.830800e+00
1355203	-6.337100e-01	1.682400e+00
1355204	-4.585300e-01	1.557000e+00
1355205	-2.670230e-01	1.436200e+00
1355206	-1.761070e-01	1.387900e+00
1355207	-8.931000e-02	1.348100e+00
1355208	0.000000e+00	1.233610e+00
*----1----1----1----1----1----1----		
* torque curve no. 5		
*----1----1----1----1----1----1----		
1355300	2	5
1355301	0.000000e+00	-4.500000e-01
1355302	4.000000e-01	-2.500000e-01
1355303	5.000000e-01	0.000000e+00
1355304	1.000000e+00	3.569000e-01
*----1----1----1----1----1----1----		
* torque curve no. 6		
*----1----1----1----1----1----1----		
1355400	2	6
1355401	0.000000e+00	1.233610e+00
1355402	9.064300e-02	1.196500e+00
1355403	1.885690e-01	1.109600e+00
1355404	2.734700e-01	1.041600e+00
1355405	4.586690e-01	8.958000e-01
1355406	5.744800e-01	7.807000e-01
1355407	7.381600e-01	6.134000e-01
1355408	7.685200e-01	5.849000e-01
1355409	8.700570e-01	4.877000e-01
1355410	1.000000e+00	3.569000e-01

1750301 0.559 1
 1750302 0.613 2
 1750401 0.0 2
 1750501 0.0 2
 1750601 0.0 2
 1750701 0.0 2
 1750801 4.0e-5 0.0 2
 1750901 0.15 0.15 1
 1751001 00000 2
 1751101 000100 1
 1751201 0 15044100. 1242900. 2458830.0 0.0 0.0 01
 1751202 0 15037400. 1242900. 2458990.0 0.0 0.0 02
 1751300 0
 1751301 10.035000 10.106000 0.0 01

 * ecc connection tee pump side

 1800000 ecct branch
 1800001 1 0
 1800101 0.0634 1.152 0.0 0.0 0.0 0.0
 1800102 4.0e-5 0.0 00000
 1800200 0 15034000. 1242910. 2259090.0 0.0
 1801101 175010000 180000000 0.0 0.05 0.05 000100
 1801201 10.035000 10.083000 0.0

 * cold leg pipe from ecc connection to reactor vessel

 1850000 rvnilcl branch
 1850001 3 0
 1850101 0.0634 1.01 0.0 0.0 0.0 0.0
 1850102 4.0e-5 0.0 00000
 1850200 0 15032100. 1242910. 2459140.0 0.0
 1851101 185010000 205000000 0.0634 1.0 1.0 000100
 1852101 180010000 185000000 0.0 0.0 0.0 000100
 1853101 185010000 223000000 0.0 45.0 45.0 000100
 1851201 9.2743000 9.3795000 0.0
 1852201 10.035000 10.064000 0.0
 1853201 1.6570000 1.7271000 0.0

 *
 * reactor vessel
 *

 * inlet annulus top volume

 2000000 inanbot branch
 2000001 2 0
 2000101 0.0 0.33 0.0855 0.0 90.0 0.33
 2000102 4.0e-5 0.178 00000
 2000200 0 15044100. 1242880. 2458850.0 0.0
 2001101 200000000 205000000 0.0 0.0 0.0 000100
 2002101 200000000 245010000 0.001 1800. 1800. 000100
 2001201 -0.0306700 -0.03023076 .0
 2002201 .06975000 .07019300 0.0

 * inlet annulus bottom volume

 2050000 inanbot branch
 2050001 1 0
 2050101 0.0 0.424 0.11 0.0 -90.0 -0.424
 2050102 4.0e-5 0.172 00000
 2050200 0 15018400. 1242920. 2459460.0 0.0
 2051101 205010000 210000000 0.0 0.0 0.0 000100
 2051201 4.0266000 4.3312000 0.0

 * downcomer

 2100000 downcomr annulus
 2100001 4
 2100101 0.142 4
 2100201 0.0 3
 2100301 0.958 4
 2100401 0.0 4
 2100501 0.0 4
 2100601 -90.0 4
 2100801 4.0e-5 0.102 4
 2100901 0.0 0.0 3
 2101001 00000 4
 2101101 000000 3
 2101201 0 15017400. 1242940. 2459500.0 0.0 0.0 01
 2101202 0 15023500. 1242960. 2459350.0 0.0 0.0 02
 2101203 0 15029700. 1242980. 2459200.0 0.0 0.0 03
 2101204 0 15035800. 1243000. 2459050.0 0.0 0.0 04
 2101300 0
 2101301 4.0266000 4.3398000 0.0 01
 2101302 4.0266000 4.3397000 0.0 02
 2101303 4.0266000 4.3396000 0.0 03

 * lower plenum top volume

 2150000 lwrplop branch
 2150001 3 0
 2150101 0.74 0.360 0.0 0.0 -90.0 -0.36
 2150102 4.0e-5 0.0 00000
 2150200 0 15044100. 1242880. 2458850.0 0.0
 2151101 210010000 215000000 0.0 0.00 0.00 000100
 2152101 215010000 220000000 0.0 0.00 0.00 000100
 2153101 215000000 225000000 0.15 0.0 0.0 000100
 2151201 4.0265000 4.3184000 0.0
 2152201 -0.0651070 -0.0771765 0.0
 2153201 2.4798000 2.5728000 0.0

 * lower plenum bottom volume

 2200000 lwrplot snglvol
 2200101 0.79 0.37 0.0 0.0 -90.0 -0.37
 2200102 4.0e-5 0.0 00000
 2200200 0 15046800. 1241150. 2458780.0 0.0

 * core filler bypass

 2230000 fillegap annulus

3501201 0 15018600. 1067100. 2459470.0 0.0 0.0 01
 3501202 0 15018600. 1173730. 2459470.0 0.0 0.0 02
 3501300 0
 3501301 .0 .0 0.0 01
 * isolation valve cold leg
 *----1----1----1----1----1----1----1----1----
 3550000 isvcl valve
 3550101 350010000 360000000 0.0 0.0 0.0 000100
 3550201 1 0.0 0.0 0.0
 3550300 trpvlv
 3550301 505
 *----1----1----1----1----1----1----1----1----
 * pipe section between isolation valve and qobv cold leg
 *----1----1----1----1----1----1----1----1----
 3600000 vvolcl snglvol
 3600101 0.0525 0.813 0.0 0.0 0.0 0.0
 3600102 4.0e-5 0.0 00000
 3600200 3 14.74e6 558.
 *----1----1----1----1----1----1----1----1----
 * quick opening blowdown cold leg
 *----1----1----1----1----1----1----1----1----
 3650000 qobvcl valve
 3650101 360010000 805000000 0.0466 0.0 0.0 000100
 3650201 1 0.0 0.0 0.0
 3650300 trpvlv
 3650301 507
 *----1----1----1----1----1----1----1----1----
 * reflood assist bypass piping - cold leg side
 *----1----1----1----1----1----1----1----1----
 3700000 rabsphl branch
 3700001 1 0
 3700101 0.0388 2.203 0.0 0.0 90.0 0.653
 3700102 4.0e-5 0.0 00000
 3700200 0 14755500. 1239680.0 2460930.0 0.0
 3701101 375010000 370000000 0.0 0.0 0.0 000100
 3701201 .21294000. 24585000.0
 *----1----1----1----1----1----1----1----1----
 * reflood assist bypass parrel pipes hot leg side
 *----1----1----1----1----1----1----1----1----
 3750000 rabphl snglvol
 3750101 0.0776 0.0 0.0858 0.0 0.0 0.0
 3750102 4.0e-5 0.0 00000
 3750200 0 14957900. 1239760.0 2460880.0 0.0
 *----1----1----1----1----1----1----1----1----
 * reflood assist bypass valves
 *----1----1----1----1----1----1----1----1----
 3770000 rabsvlv sngljun
 3770101 380010000 375000000 0.0 1.4e+4 1.4e+4 000000
 3770201 0 .106460 .25646 0.0
 *----1----1----1----1----1----1----1----1----
 * reflood assist bypass parrel pipes cold leg side
 *----1----1----1----1----1----1----1----1----
 3800000 rabppcl snglvol
 3800101 0.0776 0.0 0.0855 0.0 0.0 0.0
 3800102 4.0e-5 0.0 00000
 3800200 0 15023400. 1240020.0 2459350.0 0.0
 *----1----1----1----1----1----1----1----1----
 * reflood assist bypass single pipe cold leg side
 *----1----1----1----1----1----1----1----1----
 3850000 rabspcl branch
 3850001 1 0
 3850101 0.0388 0.0 0.11802 0.0 -90.0 -0.653
 3850102 4.0e-5 0.0 00000
 3850200 0 15021000. 1240850.0 2459410.0 0.0
 3851101 385010000 380000000 0.0 0.0 0.0 000100
 3851201 .212920 .260740 0.0

 *
 * pressurizer
 *

 * surge line pcs side
 *----1----1----1----1----1----1----1----1----
 4000000 slpcs branch
 4000001 2 0
 4000101 0.00145 3.45 0.0 0.0 90.0 0.54
 4000102 4.0e-5 0.0 00000
 4000200 0 14923700. 1458370. 2461610.0 0.0
 4001101 110000000 400000000 0.0 0.93 0.93 000100
 4002101 400010000 405000000 0.0 0.93 0.93 000000
 4001201 -.17675e-4 -.17772e-4 0.0
 4002201 -.17696e-5 -.17696e-5 0.0
 *----1----1----1----1----1----1----1----1----
 * surge line pressurizer vessel
 *----1----1----1----1----1----1----1----1----
 4050000 slprv snglvol
 4050101 0.00145 3.45 0.0 0.0 90.0 0.60
 4050102 4.0e-5 0.0 00000
 4050200 0 14920000. 1494210.0 2461690.0 0.0
 *----1----1----1----1----1----1----1----1----
 * spray line
 *----1----1----1----1----1----1----1----1----
 4060000 spray branch
 4060001 1 0
 4060101 0.0003363 6.322 0.0 0.0 90.0
 4060102 3.161 4.0e-5 0.0 00000
 4060200 0 15075000. 1244040.0 2458090.0 0.0
 4061101 406010000 420010000 2.4e-6 1.0392 1.0392 000100
 4061201 .08890000. 08890000 0.0
 *----1----1----1----1----1----1----1----1----
 * spray valve
 *----1----1----1----1----1----1----1----1----
 4070000 sprvlv valve
 4070101 406010000 420010000 3.34e-4 1.54e01 1.54e01
 + 000100
 4070201 0 .000000 .000000 0.0
 4070300 trpvlv
 4070301 690
 *----1----1----1----1----1----1----1----1----
 * pressurizer surge line valve
 *----1----1----1----1----1----1----1----1----

4100000 svalv valve
 4100101 405010000 415000000 0.0 0.93 0.93 000100
 4100201 0 -17704000 -1770400 0.0
 4100300 trpvlv
 4100301 508
 *----1----1----1----1----1----1----1----1----1----1----
 * pressurizer vessel
 *----1----1----1----1----1----1----1----1----1----
 4150000 pzrve pipe
 4150001 8
 4150101 0.362 1
 4150102 0.565 5
 4150103 0.466 7
 4150104 0.13 8
 4150201 0.0 7
 4150301 0.224 1
 4150302 0.403 3
 4150303 0.207 5
 4150304 0.1705 7
 4150305 0.118 8
 4150401 0.0 8
 4150501 0.0 8
 4150601 90.0 8
 4150801 4.0e-5 0.0 8
 4151001 00000 8
 4151101 000000 7
 4151201 0 14917400. 1511010. 2461750.0 .0 0.001
 4151202 0 14915500. 1568180. 2461790.0 .1839e-3 0.002
 4151203 0 14913200. 1558810. 2463620.0 .15145 0.003
 4151204 0 14912100. 1582630. 2461930.0 .9996500 0.004
 4151205 0 14911900. 1582620. 2461840.0 .9996400 0.005
 4151206 0 14911700. 1582560. 2461840.0 .9996000 0.006
 4151207 0 14911500. 1582300. 2461840.0 .9995300 0.007
 4151208 0 14911400. 1575760. 2461840.0 1.0 0.008
 4151300 0
 4151301 -.716473e-3 .05388 0.0 01
 4151302 -.62376e-3 .3445 0.0 02
 4151303 -.27965 .12293e-2 0.0 03
 4151304 -.27030 .17636e-3 0.0 04
 4151305 -.30526 .20283e-3 0.0 05
 4151306 -.28127 .19339e-3 0.0 06
 4151307 -.58439 .64379e-3 0.0 07
 *----1----1----1----1----1----1----1----1----1----
 * pressurizer top hat and relief connection
 *----1----1----1----1----1----1----1----1----
 4200000 toppre branch
 4200001 1 0
 4200101 0.13 0.118 0.0 0.0 90.0 0.118
 4200102 4.0e-5 0.0 00000
 4200200 0 14911300. 1541380. 2461830.0 .99907000
 4201101 415010000 420000000 0.0 0.0 0.0 000000
 4201201 -.38729 5.44472e-4 0.0
 *----1----1----1----1----1----1----1----1----
 * porv
 *----1----1----1----1----1----1----1----1----
 4250000 porv valve
 4250101 420010000 810000000 2.4784-5 0.0 0.0 000100
 4250201 0 .000000 .000000 0.0
 4250300 trpvlv
 4250301 625

 *
 * steam generator secondary side
 *

 * primary separator
 *----1----1----1----1----1----1----1----1----
 5000000 sepaout separatr
 5000001 3 0
 5000101 1.273 0.718 0.0 0.0 +90.0 +0.718
 5000102 4.e-5 0.7874 00010
 5000200 0 5670640.0 1444230. 3000000.0 .19415000
 5001101 500010000 525000000 1.272800 0.0 0.0 001100 0.5
 5002101 500000000 505000000 0.000000 0.0 0.0 001100 +
 + 0.15
 5003101 520000000 500000000 0.19600 0.4 0.4 001100
 5001201 -0.4175 .75723 0.0
 5002201 0.8006 -9.39768e-2 0.0
 5003201 1.9086 4.4093 0.0
 *----1----1----1----1----1----1----1----1----
 * separator outlet region
 *----1----1----1----1----1----1----1----
 5050000 lwrsep branch
 5050001 1
 5050101 1.273 0.718 0.0 0.0 -90.0 -0.718
 5050102 4.e-5 0.7874 00000
 5050200 0 5672780.0 1183350. 2400000.0 .01138160
 5051101 505010000 510000000 0.0 0.0 0.0 000100
 5051201 0.21828 -.30041 0.0
 *----1----1----1----1----1----1----1----
 * feed inlet volume
 *----1----1----1----1----1----1----1----
 5100000 feedinl branch
 5100001 1 0
 5100101 0.7525 0.518 0.0 0.0 -90.0 -0.518
 5100102 4.e-5 0.10796 00000
 5100200 0 5676840.0 1109810. 2400000.0 .408589e-5
 5101101 510010000 515000000 0.0 0.0 0.0 000100
 5101201 0.6328700 0.632870 0.0
 *----1----1----1----1----1----1----1----
 * steam generator downcomer
 *----1----1----1----1----1----1----1----
 5150000 dwncmr annulus
 5150001 8
 5150101 0.23226 3
 5150102 0.27871 8
 5150201 0.0 7
 5150301 0.7102 3
 5150302 1.85075 7
 5150303 0.718 8
 5150401 0.0 8
 5150601 -.90.0 3

12100604	223050000	0	1	1	0.958	4	12200000	1	11	1	1	0.0	
12100605	223060000	0	1	1	0.36	5	12200100	0	1				
12100606	223070000	0	1	1	0.37	6	12200101	10	0.092				
12100701	0	0.0	0.0	0.0	6		12200201	5	10				
12100801	0.0	11.0	11.0	0.0	0.0	0.0	1.0	4 * mod 3					
12100802	0.0	11.0	11.0	0.0	0.0	0.0	1.0	5 * mod 3					
12100803	0.0	11.0	11.0	0.0	0.0	0.0	1.0	6 * mod 3					
12100901	0.0	11.0	11.0	0.0	0.0	0.0	1.0	4 * mod 3					
12100902	0.0	11.0	11.0	0.0	0.0	0.0	1.0	5 * mod 3					
12100903	0.0	11.0	11.0	0.0	0.0	0.0	1.0	6 * mod 3					

* reactor vessel wall above station 178 - 5.50 inches thick													
* station 178 to 258 rv not modelled above bottom of nozzles													

12110000	3	11	2	1	0.7328		12250000	7	11	2	1	0.3	
12110100	0	1					12250100	0	1				
12110101	10	0.8725					12250101	10	0.38				
12110201	5	10					12250201	4	10				
12110301	0.0	10					12250301	0.0	10				
12110401	558.0	11					12250401	558.0	11				
12110501	223010000	0	1	1	0.424	1	12250501	225010000	0	1	1	0.52	1
12110502	223020000	0	1	1	0.958	2	12250502	230010000	0	1	1	0.559	2
12110503	223030000	0	1	1	0.6500	3	12250503	230020000	0	1	1	0.559	3
12110601	-939	0	3949	1	0.424	1	12250504	230030000	0	1	1	0.657	4
12110602	-939	0	3949	1	0.958	2	12250505	240010000	0	1	1	1.118	5
12110603	-939	0	3949	1	0.6500	3	12250506	245010000	0	1	1	0.42	6
12110701	0	0.0	0.0	0.0	3		12250507	246010000	0	1	1	0.35	7
12110801	0.0	11.0	11.0	0.0	0.0	0.0	1.0	1 * mod 3					
12110802	0.0	11.0	11.0	0.0	0.0	0.0	1.0	2 * mod 3					
12110803	0.0	11.0	11.0	0.0	0.0	0.0	1.0	3 * mod 3					

* reactor vessel wall bellow station 178 - 3.62 inches thick													
* station 67.7 to 178													

12120000	5	7	2	1	0.7328		12250601	0	0	0	1	0.52	1
12120100	0	1					12250602	0	0	0	1	0.559	2
12120101	6	0.8247					12250603	0	0	0	1	0.559	3
12120201	5	6					12250604	0	0	0	1	0.657	4
12120301	0.0	6					12250605	0	0	0	1	1.118	5
12120401	558.0	7					12250606	0	0	0	1	0.42	6
12120501	223030000	0	1	1	0.308	1	12250607	0	0	0	1	0.35	7
12120502	223040000	10000	1	1	0.958	3	12250701	0	0.0	0.0	0.0	7	
12120503	223060000	0	1	1	0.3600	4	12250801	0.0	11.0	11.0	0.0	0.0	0.0
12120504	223070000	0	1	1	0.37	5	12250802	0.0	11.0	11.0	0.0	0.0	0.0
12120601	-939	0	3949	1	0.308	1	12250803	0.0	11.0	11.0	0.0	0.0	0.0
12120602	-939	0	3949	1	0.958	3	12250804	0.0	11.0	11.0	0.0	0.0	0.0
12120603	-939	0	3949	1	0.36	4	12250805	0.0	11.0	11.0	0.0	0.0	0.0
12120604	-939	0	3949	1	0.37	5	12250806	0.0	11.0	11.0	0.0	0.0	0.0
12120701	0	0.0	0.0	0.0	5		12250807	0	0	0	0	7 * mod 3	
12120801	0.0	11.0	11.0	0.0	0.0	0.0	1.0	1 * mod 3					
12120802	0.0	11.0	11.0	0.0	0.0	0.0	1.0	3 * mod 3					
12120803	0.0	11.0	11.0	0.0	0.0	0.0	1.0	4 * mod 3					
12120804	0.0	11.0	11.0	0.0	0.0	0.0	1.0	5 * mod 3					

* reactor vessel bottom station 67.7													

12260000	1	7	2	1	0.282		12260100	0	1				
12260100	0	1					12260101	6	0.3				
12260101	6	0.3					12260201	4	6				
12260301	0.0	6					12260301	0.0	6				
12260401	558.0	7					12260401	558.0	7				
12260501	225010000	0	1	1	0.52	1	12260501	225010000	0	1	1	0.52	1
12260601	0	0	0	1	0.52	1	12260701	0	0.0	0.0	0.0	1	
12260701	0	0.0	0.0	0.0	1		12260801	0.0	11.0	11.0	0.0	0.0	0.0
12260801	0.0	11.0	11.0	0.0	0.0	0.0	1.0	1 * mod 3					

* active core station 116.91 to 182.94

12300000	3	10	2	1	0.0
12300100	0	1			
12300101	5	4.647e-3			
12300102	1	4.742e-3			
12300103	3	5.359e-3			
12300201	1	5			
12300202	2	6			
12300203	3	9			
12300301	1.0	5			
12300302	0.0	9			
12300401	558.0	10			
12300501	0	0	0	1	725.1 3
12300601	230010000 0	1	1	725.1	1
12300602	230020000 0	1	1	725.1	2
12300603	230030000 0	1	1	725.1	3
12300701	1000	0.41209	0.0	0.0	1
12300702	1000	0.44565	0.0	0.0	2
12300703	1000	0.14226	0.0	0.0	3
12300901	0.0124	11.0	11.0	0.0	0.0
					0.0 0.0 1.0 3 *mod 3

* upper core support structure station 190.5 to 234.5

12400000	1	7	2	1	0.282
12400100	0	1			
12400101	6	0.31			
12400201	4	6			
12400301	0.0	6			
12400401	558.0	7			
12400501	240010000 0	1	1	1.118	1
12400601	0	0	0	1	1.118 1
12400701	0	0.0	0.0	0.0	1
12400801	0.0	11.0	11.0	0.0	0.0
					0.0 0.0 1.0 1 * mod 3

* fuel modules station 187.6 to 258.4

12460000	1	5	1	1	0.0
12460100	0	1			
12460101	4	0.01			
12460201	4	4			
12460301	0.0	4			
12460401	558.0	5			
12460501	245010000 0	1	1	1.8	1
12460601	246010000 0	1	1	1.8	1
12460701	0	0.0	0.0	1.8	1
12460801	0.0	11.0	11.0	0.0	0.0
					0.0 0.0 1.0 1 * mod 3
12460901	0.0	11.0	11.0	0.0	0.0
					0.0 0.0 1.0 1 * mod 3

* core support barrel - upper plenum lower volume
* station 264 to 297.6
* reactor vessel not modelled above bottom of nozzles
* the vessel to filler gap is assumed to insulate the vessel
* from the fillers. the vessel to filler gap is not modelled
* at this elevation.

12500000 1 11 2 1 0.381
12500100 0 1
12500101 10 0.419
12500201 5 10
12500301 0.0 10
12500401 558.0 11
12500501 250010000 0 1 1 0.854 1
12500601 0 0 0 1 0.854 1
12500701 0 0.0 0.0 0.0 1
12500801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3

* internals upper plenum

12510000	2	5	1	1	0.0
12510100	0	1			
12510101	4	0.005			
12510201	4	4			
12510301	0.0	4			
12510401	558.0	5			
12510501	250010000 0	1	1	1.0	1
12510502	250010000 0	1	1	1.0	2
12510601	0	0	0	1	1.0 2
12510701	0	0.0	0.0	0.0	2
12510801	0.0	11.0	11.0	0.0	0.0 0.0 0.0 1.0 2 * mod 3

* core support barrel - upper plenum top volume
* station 297.6 to 325
* reactor vessel not modelled above bottom of nozzles
* the vessel to filler gap is assumed to insulate the vessel
* from the fillers. the vessel to filler gap is not modelled
* at this elevation.

12501000 1 21 2 1 0.381
12501100 0 1
12501101 20 0.728
12501201 5 20
12501301 0.0 20
12501401 558.0 21
12501501 250010000 0 1 1 0.712 1
12501601 0 0 0 1 0.712 1
12501701 0 0.0 0.0 0.0 1
12501801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3

* upper head top plate station 325

12550000	1	21	1	1	0.0
12550100	0	1			
12550101	20	0.474			
12550201	5	20			
12550301	0.0	20			
12550401	558.0	21			
12550501	250010000 0	1	1	0.712	1
12550601	-939	0	3949	1	0.712 1
12550701	0	0.0	0.0	0.0	1

12550801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	1 * mod 3

* broken loop hot leg piping heat structures									

13150000	2	11	2	1	0.0515				
13150100	0	1							
13150101	10	0.0705							
13150201	4	10							
13150301	0.0	10							
13150401	540.0	11							
13150501	315010000	0	1	1	0.4054	1			
13150502	315020000	0	1	1	0.5265	2			
13150601	-939	0	3979	1	0.4054	1			
13150602	-939	0	3979	1	0.5265	2			
13150701	0	0	0	0	2				
13150801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	1 * mod 3
13150802	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	2 * mod 3

13151000	1	11	2	1					
0.0550									
13151100	0	1							
13151101	10	0.0705							
13151201	4	10							
13151301	0.0	10							
13151401	540.0	11							
13151501	315090000	0	1	1	0.0120357	1			
13151601	-939	0	3979	1	0.0120357	1			
13151701	0	0	0	0	1				
13151801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	1 * mod 3

13152000	1	11	2	1	0.0660				
13152100	0	1							
13152101	10	0.0840							
13152201	4	10							
13152301	0.0	10							
13152401	540.0	11							
13152501	315110000	0	1	1	0.00836	1			
13152601	-939	0	3979	1	0.00836	1			
13152701	0	0	0	0	1				
13152801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	1 * mod 3

13153000	6	11	2	1	0.1835				
13153100	0	1							
13153101	10	0.2285							
13153201	4	10							
13153301	0.0	10							
13153401	540.0	11							
13153501	315030000	10000	1	1	0.108	6			
13153601	-939	0	3979	1	0.108	6			
13153701	0	0	0	0	6				
13153801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	6 * mod 3

13154000	1	11	2	1	0.1285				
13154100	0	1							
13154101	10	0.1620							
13154201	4	10							
13154301	0.0	10							
13154401	540.0	11							
13154501	315120000	0	1	1	0.0525	1			
13154601	-939	0	3979	1	0.0525	1			
13154701	0	0	0	0	1				
13154801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	1 * mod 3

13155000	1	11	2	1	0.1420				
13155100	0	1							
13155101	10	0.1780							
13155201	4	10							
13155301	0.0	10							
13155401	540.0	11							
13155501	315100000	0	1	1	0.0489057	1			
13155601	-939	0	3979	1	0.0489057	1			
13155701	0	0	0	0	1				
13155801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	1 * mod 3

* nozzle piping									

13000000	3	11	2	1	0.1420				
13000100	0	1							
13000101	10	0.1780							
13000201	4	10							
13000301	0.0	10							
13000401	540.0	11							
13000501	300010000	0	1	1	0.876	1			
13000502	305010000	0	1	1	0.698	2			
13000503	310010000	0	1	1	1.424	3			
13000601	-939	0	3979	1	0.876	1			
13000602	-939	0	3979	1	0.698	2			
13000603	-939	0	3979	1	1.424	3			
13000701	0	0	0	0	3				
13000801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	1 * mod 3
13000802	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	2 * mod 3
13000803	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	3 * mod 3

* broken loop cold leg									

* nozzle piping									

13350000	3	11	2	1	0.1420				
13350100	0	1							
13350101	10	0.1780							
13350201	4	10							
13350301	0.0	10							
13350401	540.0	11							
13350501	335010000	0	1	1	0.7495	1			
13350502	340010000	0	1	1	0.698	2			
13350503	345010000	0	1	1	0.974	3			
13350601	-939	0	3949	1	0.7495	1			
13350602	-939	0	3949	1	0.698	2			
13350603	-939	0	3949	1	0.974	3			
13350701	0	0	0	0	3				
13350801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	1 * mod 3
13350802	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	2 * mod 3
13350803	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	3 * mod 3

```

*****
13501000 1 11 2 1 0.0550
13501100 0 1
13501101 10 0.1780
13501201 4 10
13501301 0.0 10
13501401 540.0 11
13501501 350010000 0 1 1 0.488 1
13501601 -939 0 3949 1 0.488 1
13501701 0 0 0 0 1
13501801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
*****
13502000 1 11 2 1 0.0865
13502100 0 1
13502101 10 0.1095
13502201 4 10
13502301 0.0 10
13502401 540.0 11
13502501 350020000 0 1 1 1.6085 1
13502601 -939 0 3949 1 1.6085 1
13502701 0 0 0 0 1
13502801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
*****
* reflood assist piping and valves [rabv]
*****
13700000 4 11 2 1 0.111
13700100 0 1
13700101 10 0.1365
13700201 4 10
13700301 0.0 10
13700401 540.0 11
13700501 370010000 0 1 1 2.00 1
13700502 375010000 0 1 1 1.10567 2
13700503 380010000 0 1 1 1.101804 3
13700504 385010000 0 1 1 3.04201 4
13700601 -939 0 3979 1 2.00 1
13700602 -939 0 3979 1 1.10567 2
13700603 -939 0 3949 1 1.101804 3
13700604 -939 0 3949 1 3.04201 4
13700701 0 0 0 0 4
13700801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
13700802 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 2 * mod 3
13700803 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 3 * mod 3
13700804 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 4 * mod 3
*****
* pressurizer heat structures
*****
* vessel bottom
*****1-----1-----1-----1-----1-----1-----
14151000 1 11 1 1 1 0.0
14151100 0 1
14151101 10 0.0762
14151201 5 10
14151301 0.0 10
14151401 617.0 11
14151501 415010000 0 1 1 0.362 1
14151601 -939 0 3969 1 1 0.362 1
14151701 0 0 0 0 0 1
14151801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
*****1-----1-----1-----1-----1-----1-----1-----
* vessel sides - large diameter section
*****1-----1-----1-----1-----1-----1-----1-----
14152000 7 11 2 1 1 0.42291
14152100 0 1
14152101 10 0.49911
14152201 5 10
14152301 0.0 10
14152401 617.0 11
14152501 415010000 0 1 1 0.224 1
14152502 415020000 10000 1 1 0.403 3
14152503 415040000 10000 1 1 0.207 5
14152504 415060000 10000 1 1 0.1705 7
14152601 -939 0 3969 1 0.224 1
14152602 -939 0 3969 1 0.403 3
14152603 -939 0 3969 1 0.207 5
14152604 -939 0 3969 1 0.1705 7
14152701 0 0 0 0 0 7
14152801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
*****1-----1-----1-----1-----1-----1-----1-----
* vessel sides - small diameter section
*****1-----1-----1-----1-----1-----1-----1-----
14162000 1 11 2 1 1 0.2032
14162100 0 1
14162101 10 0.3683
14162201 5 10
14162301 0.0 10
14162401 617.0 11
14162501 415080000 0 1 1 0.118 1
14162601 -939 0 3969 1 0.118 1
14162701 0 0 0 0 0 1
14162801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
*****
* pressurizer heaters
*****
14172000 12 9 2 1 0.0
14172100 0 1
14172101 3 4.0132e-3
14172102 2 4.3942e-3
14172103 1 5.6642e-3
14172104 2 8.3820e-3
14172201 7 3
14172202 8 5
14172203 7 6
14172204 4 8
14172301 0.0 3
14172302 1.0 5
14172303 0.0 8
14172401 617.6 9
14172501 0 0 0 1 0.6096 12
14172601 415020000 0 1 1 0.6096 12
14172701 417 1.0 0.0 0.0 9 *cycli
14172702 418 1.0 0.0 0.0 12 *backu

```


20100710	866.48	0.1987
20100711	922.04	0.1934
20100712	977.59	0.1882
20100713	1033.15	0.1830
20100714	1088.71	0.1777
20100715	1144.26	0.1725
20100716	1199.82	0.1673
20100717	1255.37	0.1621
20100718	1310.93	0.1568
20100719	1366.48	0.1516
20100720	1422.04	0.1464
20100721	1477.59	0.1412
20100722	1533.15	0.1359
20100723	1588.71	0.1307
20100724	1644.26	0.1255
20100725	1699.82	0.1203
20100726	1755.37	0.1150
20100727	1810.93	0.1098
20100728	1866.48	0.1046
20100729	1922.04	0.0993
20100730	5000.00	0.0993
*	-----	-----
*	magnesium oxide - volumetric heat capacity	
*	-----	-----
20100751	373.15	2033.52
20100752	422.04	2004.59
20100753	477.59	1917.74
20100754	533.15	1938.87
20100755	588.71	1906.01
20100756	644.26	1873.15
20100757	699.82	1840.29
20100758	755.37	1807.43
20100759	810.93	1774.56
20100760	866.48	1741.70
20100761	922.04	1708.84
20100762	977.59	1675.96
20100763	1033.15	1643.11
20100764	1088.71	1610.25
20100765	1144.26	1577.39
20100766	1199.82	1544.53
20100767	1255.37	1511.67
20100768	1310.93	1478.80
20100769	1366.48	1445.94
20100770	1422.04	1413.08
20100771	1477.59	1380.22
20100772	1533.15	1347.35
20100773	1588.71	1314.49
20100774	1644.26	1281.63
20100775	1699.82	1248.77
20100776	1755.37	1215.90
20100777	1810.93	1183.04
20100778	1866.48	1150.18
20100779	1922.04	1117.32
20100780	5000.00	1117.32
*	-----	-----
*	nichrome - thermal conductivity	
*	-----	-----

* steam generator environmental loss heat xfer coefficient
 *-----1-----1-----1-----1-----1-----1-----1-----
 20295900 htc-t
 20295901 0.0 3.385
 *-----1-----1-----1-----1-----1-----1-----1-----
 * pressurizer generator environmental loss heat xfer coefficient
 *-----1-----1-----1-----1-----1-----1-----1-----
 20296900 htc-t
 20296901 0.0 3.019
 *-----1-----1-----1-----1-----1-----1-----1-----
 * blhl environmental loss heat xfer coefficient
 *-----1-----1-----1-----1-----1-----1-----1-----
 20297900 htc-t 509
 20297901 -1.0 0.0
 20297902 0.0 13.450
 **** core collapsed liquid level ****
 20255000 normarea 0 1.0 1.0
 20255001 0.0 9.25e-4
 20255002 9.25e-4 9.25e-4
 20255003 1.0 1.0
 20290000 power 609
 20290001 0.0 48.9e+6
 20290002 0.15 43.032e6
 20290003 0.3 37.164e6
 20290004 0.6 28.362e6
 20290005 0.85 8.6064e6
 20290006 1.0 5.99538e6
 20290007 1.3 4.89e6
 20290008 2.0 4.274e6
 20290009 4.0 3.7060332e6
 20290010 7.0 3.1296e6
 20290011 10.0 2.93458e6
 20290012 25.0 2.28548e6
 20290013 65.0 1.7115e6
 20290014 100.0 1.5425994e6
 20290015 250.0 1.232769e6
 20290016 650.0 0.91932e6
 20290017 1000.0 0.80196e6
 20290018 1500.0 0.6846e6
 20290019 3000.0 0.5379e6
 20290020 5000.0 0.44988e6
 **** reactor kinetics data ****
 *-----
 30000000 point
 30000001 gamma-ac 49.6e+6 0.0 348.43 1.0
 0.556
 30000002 ans79-1
 * shoud not be changed for transient
 **** delayed neutron constants ****
 30000101 0.0349 0.01275

30000102	0.2035	0.03177
30000103	0.1848	0.1181
30000104	0.4046	0.3160
30000105	0.1401	1.402
30000106	0.0321	3.914

power history		

30000401	4.96e+7	70. hr
* ----- should be changer for transient as 4.89e+7		

* reactivity curve numbers		

30000011	609	

moderator density reactivity table		

*30000501	0.818	-4.428
*30000502	0.905	-2.249
*30000503	0.955	-1.032
*30000504	1.000	0.000
*30000505	1.044	0.926
*30000506	1.095	1.853
*30000507	1.139	2.589
*30000508	1.213	3.689
*30000509	1.270	4.489
*30000510	1.316	5.212

doppler reactivity table		

*30000601	293.16	1.375
*30000602	338.72	1.125
*30000603	422.05	0.682
*30000604	477.60	0.419
*30000605	505.38	0.274
*30000606	570.72	0.000
*30000607	588.72	-0.075
*30000608	695.83	-0.526
*30000609	922.05	-1.386
*30000610	1310.94	-2.543
*30000611	1810.94	-3.865
*30000612	2088.72	-4.502
*30000613	2499.83	-5.392
*30000614	3027.60	-6.417

* moderator density reactivity table		

30000501	0.818	0.0
30000502	0.905	0.0
30000503	0.955	0.0
30000504	1.000	0.0
30000505	1.044	0.0
30000506	1.095	0.0
30000507	1.139	0.0
30000508	1.213	0.0
30000509	1.270	0.0

20512308		0.453056	htrnr	415200700
20512309		0.150656	htrnr	416200100
20512310		0.130000	htrnr	420100100
20512311		0.150656	htrnr	420200100
*	-	-	-	-
* metal heating in reactor vessel (1st part)				
*	-	-	-	-
20525100	rv1	sum	1.0	0.0 1
20525101	0.0	1.05331	htrnr	200000100
20525102		0.79000	htrnr	200100101
20525103		1.01501	htrnr	200100201
20525104		2.29335	htrnr	200100301
20525105		2.29335	htrnr	200100401
20525106		2.29335	htrnr	200100501
20525107		2.29335	htrnr	200100601
20525108		1.33475	htrnr	205000100
20525109		1.93518	htrnr	205000101
20525110		2.82907	htrnr	210000100
20525111		2.82907	htrnr	210000200
20525112		2.82907	htrnr	210000300
20525113		2.82907	htrnr	210000400
20525114		1.06311	htrnr	210000500
20525115		1.09265	htrnr	210000600
20525116		4.37241	htrnr	210000101
20525117		4.37241	htrnr	210000201
20525118		4.37241	htrnr	210000301
20525119		4.37241	htrnr	210000401
20525120		1.64308	htrnr	210000501
*				
20525200	rv2	sum	1.0	0.0 1
20525201	0.0	1.68872	htrnr	210000601
20525202		1.95223	htrnr	211000100
20525203		4.41094	htrnr	211000200
20525204		2.99281	htrnr	211000300
20525205		1.41813	htrnr	212000100
20525206		4.41094	htrnr	212000200
20525207		4.41094	htrnr	212000300
20525208		1.65755	htrnr	212000400
20525209		1.70360	htrnr	212000500
20525210		1.6800	htrnr	220000100
*				
20525300	rv3	sum	1.0	0.0 1
20525301	0.0	0.695734	htrnr	225000700
20525302		0.921366	htrnr	226000100
20525303		1.98094	htrnr	240000100
20525304		1.80000	htrnr	246000100
20525305		1.80000	htrnr	246000101
20525306		2.04439	htrnr	250000100
20525307		1.00000	htrnr	251000100
20525308		1.00000	htrnr	251000200
20525309		1.70445	htrnr	250100100
20525310		0.71200	htrnr	255000100
20525311		1.68000	htrnr	220000101
20525312		0.980177	htrnr	225000100
20525313		1.05369	htrnr	225000200
20525314		1.05369	htrnr	225000300

```

* metal heating in broken loop simulators
*-----1-----1-----1-----1-----1-----1-----1-----
20513000 blhlsm sum 1.0 0.0 1
20513001 0.0 0.1312 htrnr 315000100
20513002 0.1703 htrnr 315000200
20513003 0.0042 htrnr 315100100
20513004 0.00347 htrnr 315200100
20513005 0.12452 htrnr 315300100
20513006 0.12452 htrnr 315300200
20513007 0.12452 htrnr 315300300
20513008 0.12452 htrnr 315300400
20513009 0.12452 htrnr 315300500
20513010 0.12452 htrnr 315300600
20513011 0.04239 htrnr 315400100
20513012 0.04363 htrnr 315500100
*-----1-----1-----1-----1-----1-----1-----1-----
* metal heating in steam generator
*-----1-----1-----1-----1-----1-----1-----1-----
20555100 sgmth1 sum 1.0 0.0 1
20555101 0.0 1.47943 htrnr 500000100
20555102 1.47943 htrnr 500000200
20555103 0.291097 htrnr 500000300
20555104 1.52566 htrnr 500000101
20555105 1.52566 htrnr 500000201
20555106 0.300194 htrnr 500000301
20555107 0.615526 htrnr 515000100
20555108 2.88042 htrnr 515000200
20555109 2.88042 htrnr 515000300
20555110 2.88042 htrnr 515000400
20555111 0.627655 htrnr 515000101
20555112 2.93718 htrnr 515000201
20555113 2.93718 htrnr 515000301
20555114 2.93718 htrnr 515000401
*
20555200 sgmth2 sum 1.0 0.0 1
20555201 0.0 3.40507 htrnr 530000100
20555202 3.40507 htrnr 530000200
20555203 3.20846 htrnr 530000300
20555204 3.30846 htrnr 530000400
20555205 2.31474 htrnr 530000500
20555206 3.17360 htrnr 530000600
20555207 3.17360 htrnr 530000700
20555208 3.17360 htrnr 530000800
*-----1-----1-----1-----1-----1-----1-----1-----
* pcs-tubesheet heat transfer
*-----1-----1-----1-----1-----1-----1-----1-----
20513200 pcstub sum 1.0 0.0 1
20513201 0.0 56.4226 htrnr 115100100
20513202 56.4226 htrnr 115100200
20513203 0.157962 htrnr 115200100
20513204 0.157962 htrnr 115200200
*-----1-----1-----1-----1-----1-----1-----1-----
* tubesheet-scs heat transfer
*-----1-----1-----1-----1-----1-----1-----1-----
20513300 tushscs sum 1.0 0.0 1
20513301 0.0 0.157962 htrnr 115200101

```

```

20513302          0.157962 htrnr   115200201
*--- ---1---1---1---1---1---1---1---1---
* metal hx in rabs
*--- ---1---1---1---1---1---1---1---1---
20517000 rabs     sum      1.0    0.0    1
20517001 0.0      1.39487 htrnr   370000100
20517002          0.77113 htrnr   370000200
20517003          0.77278 htrnr   370000300
20517004          2.12160 htrnr   370000400
*****
bl total metal hx
*****
20517100 qbtotal sum      1.0    0.0    1
20517101 0.0      1.0      cntrlvar 127
*20517102          1.0      cntrlvar 170
20517103          1.0      cntrlvar 130 * only for simula
*****
* pcs stored energy excluding pressurizer
*****
20557000 pcsqre sum      1.0    0.0    1
20557001 0.0      1.0      cntrlvar 253 * rv metal heat
20557002          1.0      cntrlvar 113 * rv ambloss
20557003          1.0      cntrlvar 171 * only for simula
20557004          1.0      cntrlvar 117 * blhl ambloss
20557005          1.0      cntrlvar 118 * blcl ambloss
20557006          1.0      cntrlvar 119 * rabv ambloss
20557007          1.0      cntrlvar 128 * ilhl heat
20557008          1.0      cntrlvar 120 * ilhl ambloss
20557009          1.0      cntrlvar 129 * ilcl heat
20557010          1.0      cntrlvar 121 * ilcl ambloss
20557011          1.0      cntrlvar 132 * pcs-tubesheet
20557012          1.0      cntrlvar 133 * tubesheet-scs
*****
scs stored energy
*****
20557300 scsqse sum      1.0    0.0    1
20557301 0.0      1.0      cntrlvar 552 * sg heat
20557302          1.0      cntrlvar 115 * sg ambloss
*****
* heat flow calculations
*****
ecc energy flow
*****
20515300 pvecc  div      1.0    0.0    1
20515301          rhofj  630000000 p      600010000
20515400 hecc  sum      1.0    0.0    1
20515401 0.0      1.0      ufj    630000000
20515402          1.0      cntrlvar 153
20515500 mdothecc mult    1.0    0.0    1
20515501          mflowj 630000000
20515502          cntrlvar 154
20515600 qcce/v mult    0.126646 0.0    1
20515601          cntrlvar 155
20515700 mdotev mult    0.126646 0.0    1
20515701          mflowj 630000000
*****

```

sg hx per unit pcs volume

20516000	qsg/v	mult	0.126646	0.0	1
20516001		cntrlvar	112		

* core hx per unit pcs volume

20516100	qcore/v	mult	0.126646	0.0	1
20516101		cntrlvar	111		

pump power

20516200	pledotv	mult	0.04136	0.0	1
20516201		voidgj	135020000		
20516202		velgj	135020000		
20516203		pmphead	135		
20516300	pledotl	mult	0.04136	0.0	1
20516301		voidfj	135020000		
20516302		velfj	135020000		
20516303		pmphead	135		
20516400	p2edotv	mult	0.04136	0.0	1
20516401		voidgj	165020000		
20516402		velgj	165020000		
20516403		pmphead	165		
20516500	p2edotl	mult	0.04136	0.0	1
20516501		voidfj	165020000		
20516502		velfj	165020000		
20516503		pmphead	165		
20516600	qpmp	sum	1.0	0.0	1
20516601	0.0		1.0	cntrlvar	162
20516602			1.0	cntrlvar	163
20516603			1.0	cntrlvar	164
20516604			1.0	cntrlvar	165
20516700	qpmp/v	mult	0.126646	0.0	1
20516701		cntrlvar	166		

energy to fluid in vessel from structures

20562000	rvhx	sum	6.2832	0.0	1
20562001	0.0	0.3080	htnr	205000101	
20562002		0.6959	htnr	210000101	
20562003		0.6959	htnr	210000201	
20562004		0.6959	htnr	210000301	
20562005		0.6959	htnr	210000401	
20562006		0.2615	htnr	210000501	
20562007		0.2688	htnr	210000601	
20562008		0.3107	htnr	211000100	
20562009		0.7020	htnr	211000200	
20562010		0.7020	htnr	212000100	
20562011		0.7020	htnr	212000200	
20562012		0.7030	htnr	212000300	
20562013		0.6	htnr	212000400	
20562014		0.2	htnr	212000500	
20562015		1.0	cntrlvar	253	

*-----1-----1-----1-----1-----1-----1-----1-----1-----

* total vessel hx/v

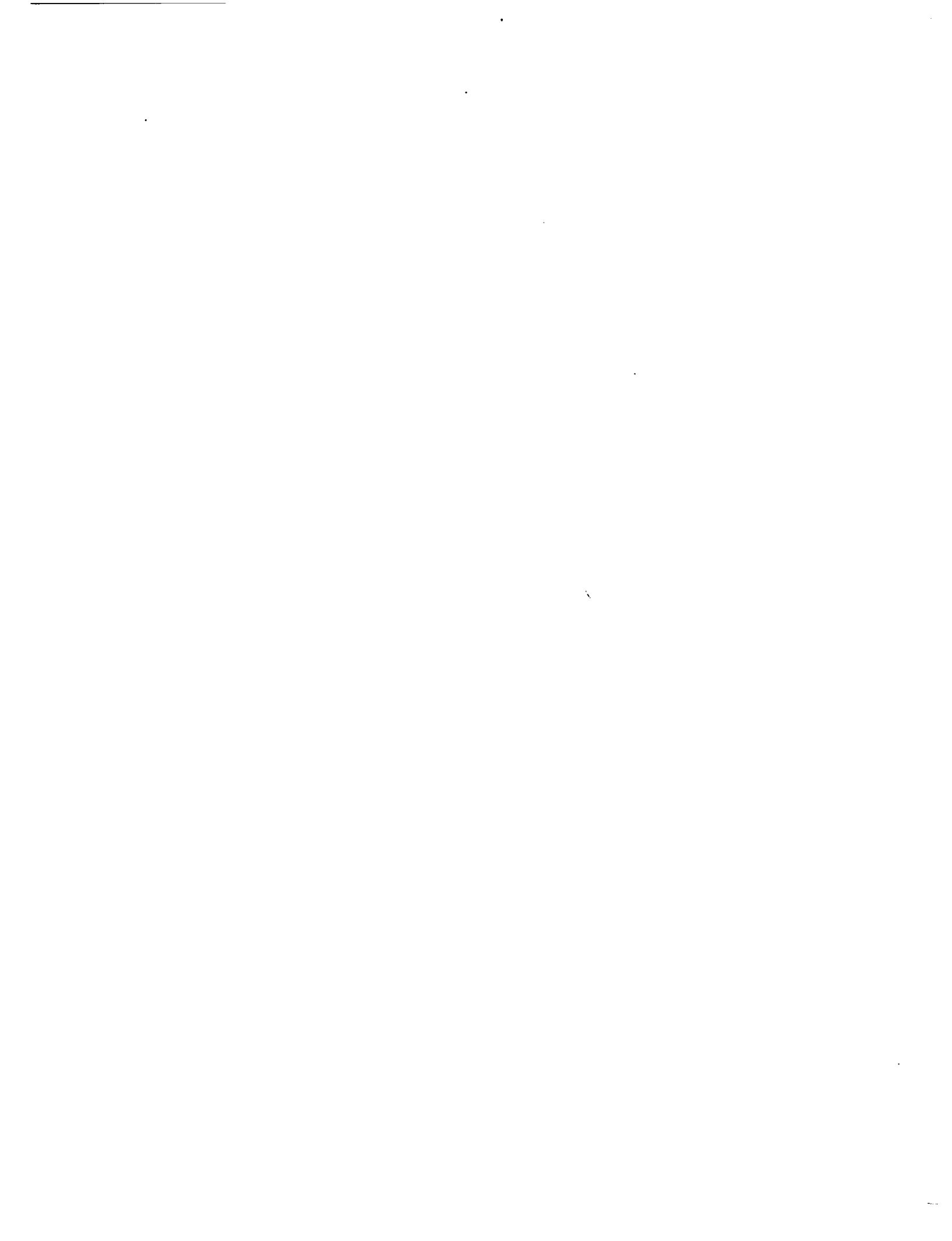

```

*9850201 0 .00000000 .00000000 0.0
*9850300 srvvlv
*9850301 905 999
*---1---1---1---1---
* charging valve position calculator
*---1---1---1---1---
*20590500 charge sum 7.7 0.0 1 *contin
*+ 3 0.0 1.0
*20590501 0.92 -1.0 cntrivar 2
*---1---1---1---1---
* letdown sink
*---1---1---1---1---
*9900000 ltdwn tmddpvol
*9900101 1.0 1.0 0.0 0.0 0.0 0.0
*9900102 4.0-5 0.0 00000
*9900200 3
*9900201 0.0 1.4+7 558.9
*---1---1---1---1---
* letdown valve
*---1---1---1---1---
*9950000 ltdwn valve
*9950101 185000000 990000000 2.5-5 0.0 0.0
000100
*9950201 0 .00000000 .00000000 0.0
*9950300 srvvlv
*9950301 906 999
*---1---1---1---1---
* letdown valve position calculator
*---1---1---1---1---
*20590600 letdown sum -7.7 0.0 1 *contin
*+ 3 0.0 1.0
*20590601 1.10 -1.0 cntrivar 2
*---1---1---1---1---1---1---1---
* steam valve controller
*---1---1---1---1---1---1---1---
* changes to steam valve
*---1---1---1---1---
*5500201 0 19.758 22.082 0.0
*5500300 srvvlv
*5500301 910 540
*20254000 normarea
*20254001 0.0 0.0
*20254002 0.0001 0.0
*20254003 1.0 1.0
*---1---1---1---1---
* compute delta t error
*---1---1---1---1---
*20590700 delta sum 1.0 0.0 1
*20590701 559.0 -1. tempf 185010000
*---1---1---1---1---
* filter delta t thru deadband
*---1---1---1---1---
*20590800 deadband function 1.0 0.0 1
*20590801 cntrivar 907 908
*20290800 reac-t
*20290801 -100. -100.

```



Appendix B Input Deck for Transient Calculation



```

=loft 19-1 post test analysis deck
*-----1-----1-----1-----1-----1-----1-----
* initial conditions
* pcp pressure = 14.901 mpa
* core power = 50. mw
* pcs flow = 479.3 kg/s
* thot = 578. k
* tcold = 559.0 k
*
*-----1-----1-----1-----1-----1-----1-----
0000100 restart transnt
0000101 run
0000102 si
*0000103 16006
0000103 6934
0000105 5. 10.
* time step control cards
*   end time min dt  max dt optn mnr mjr rst
0000201 200.00 1.e-6 1.0 2 1 30 100
0000202 1000.0 1.e-6 1.0 2 5 300 500
0000203 2000.0 1.e-6 0.1 2 50 3000 5000
0000204 4000.0 1.e-6 0.5 2 10 1000 2000
0000205 8000.0 1.e-6 0.1 2 50 4000 5000
0000206 10000. 1.e-6 0.5 2 10 2000 2000
***** minor edit variables
*****
* pressure
*****
*0000301 p 345010000 * pe-bl-1
0000301 p 310010000 * pe-bl-2
*0000303 p 315110000 * pe-bl-3
*0000304 p 350010000 * pe-bl-4
*0000305 p 315090000 * pe-bl-6
*0000306 p 350020000 * pe-bl-8
0000302 p 185010000 * pe-pc-1
0000303 p 100010000 * pe-pc-2
0000304 p 420010000 * porv inlet
*0000310 p 110010000 * pt-139-2,3,4
0000305 p 245010000 * pe-lup-1a,1b
0000306 p 215010000 * pe-1st-1a,b/pe-2st-1a,b
*0000313 p 200010000 * pe-1st-3a,3b
0000307 p 530010000 * pe-sgs-01
0000308 p 535010000 * pt-p4-85
*****
* temperatures
*****
0000309 tempf 406010000 * spray tempf
0000310 tempf 310010000 * te-bl-2a,2b,2c
0000311 tempf 100010000 * te-pc-2a,2b,2c
0000312 tempf 185010000 * te-pc-1
0000313 tempf 115030000 * te-sg-1
0000314 tempf 115100000 * te-sg-2
0000315 tempf 515070000 * te-sg-4
***** temperatures center module
*****
*0000328 tempf 415050000 * pqr volume 5
0000316 tempf 415040000 * te-139-19
*0000330 tempf 415030000 * te-139-20
*0000331 tempf 315120000 * te-p138-171
*0000332 tempf 350020000 * te-p138-170
*0000333 tempf 205010000 * te-1st-1/te-2st-1
0000317 tempf 210010000 * te-1st-2/te-2st-2
*0000335 tempf 345010000 * te-bl-1
*0000336 tempf 210030000 * te-1st-14/te-2st-14
*0000337 tempf 210040000 * te-3up-2
*0000338 tempf 245010000 * te-lup-6
*0000339 tempf 246010000 * te-2up-4
*0000340 tempf 250010000 * te-lup-3
*****
* densities
*****
***** rho
*0000341 rho 345010000 * de-bl-1
0000318 rho 310010000 * de-bl-2
0000319 rho 185010000 * de-pc-1
0000320 rho 100010000 * de-pc-2
*0000345 rho 115120000 * de-pc-3
0000321 voidgj 400010000 * surge line density
*0000347 rho 115040000 * s/g tubes
*0000348 rho 115050000 * s/g tubes
*0000349 rho 115060000 * s/g tubes
*0000350 rho 115070000 * s/g tubes
*****
* velocities
*****
***** velf
*0000351 voidf 100010000 * ilhl nozzle
*0000352 velf 100010000 * ilhl nozzle
*0000353 velf 115030000 * s/g inlet
*0000354 velf 400010000 * surge line
*0000355 velfj 425000000 * porv liq vel
*0000356 velg 100010000 * ilhl nozzle
*0000357 velg 115030000 * s/g inlet
*0000358 velg 400010000 * surge line
*0000359 velgj 425000000 * porv vap vel
*****
* mass flow rates
*****
***** mflowj
0000322 mflowj 100010000 * ilhl nozzle
*0000361 mflowj 150010000 * pump outlet
*0000362 mflowj 185020000 * dtr-rake ilcl
0000323 mflowj 400010000 * pres. surge line flow
0000324 mflowj 407000000 * pqr spray flow
0000325 mflowj 425000000 * pres. relief valve flow
0000326 mflowj 550000000 * steam flow control valve
0000327 mflowj 548000000 * aux feed
*0000369 mflowj 560000000 * main feed
*****
* cladding temperatures center module
*****
*0000371 httemp 230000110 * te-5h-015
*0000372 httemp 230000210 * te-5h-034

```

*0000373	htemp	230000310	* te-5h5-049	0000365	cntrlvar	128					
*****				0000366	cntrlvar	129					
* peak centerline temperatures				0000367	cntrlvar	130					
*****				0000368	cntrlvar	551					
*0000374	htemp	230000101	* core lower region	0000369	cntrlvar	552					
*0000375	htemp	230000201	* core middle region	0000370	cntrlvar	132					
*0000376	htemp	230000301	* core upper region	0000371	cntrlvar	133					
*****				0000372	cntrlvar	170					
* reactor kinetic parameters				0000373	cntrlvar	171					
*****				0000374	cntrlvar	570					
0000328	rktppow	0	* total reactor power	0000375	cntrlvar	573					
*0000378	rkfipow	0	* fission decay power	0000376	cntrlvar	153					
*0000379	rkgapow	0	* gamma decay power	0000377	cntrlvar	154					
*0000380	rkreac	0	* reactivity	0000378	cntrlvar	155					
*0000381	pmphead	135	* pcp1 head	0000379	cntrlvar	156					
*0000382	pmphead	165	* pcp2 head	0000380	cntrlvar	157					
0000329	mflowj	185010000		0000381	cntrlvar	160					
0000330	mflowj	185030000		0000382	cntrlvar	161					
*0000388	mflowj	200020000		0000383	cntrlvar	166					
0000331	pmpvel	135		0000384	cntrlvar	167					
*****				0000385	cntrlvar	620					
* control variable requests				0000386	cntrlvar	621					
*****				0000387	cntrlvar	622					
0000332	cntrlvar	001		0000388	cntrlvar	623					
0000333	cntrlvar	002		0000389	cntrlvar	624					
0000334	cntrlvar	003		0000390	cntrlvar	625					
0000335	cntrlvar	041		0000391	cntrlvar	626					
0000336	cntrlvar	042		0000392	cntrlvar	627					
0000337	cntrlvar	043		0000393	tempg	515070000					
0000338	cntrlvar	004		0000394	rho	420010000					
0000339	cntrlvar	005		0000395	cputime	0					
0000340	cntrlvar	006		20800095	dt	0					
0000341	cntrlvar	007		20800096	dtrnrt	0					
0000342	cntrlvar	008		*****							
0000343	cntrlvar	009		*							
0000344	cntrlvar	010		*							
0000345	cntrlvar	433		*	trips						
0000346	cntrlvar	434		*							
0000347	cntrlvar	111		*****							
0000348	cntrlvar	112		*	variable trips						
0000349	cntrlvar	113		*****							
0000350	cntrlvar	114		0000501	p	100010000	le null	0	14.193103e6	1	
0000351	cntrlvar	115		*	ecc check valve						
0000352	cntrlvar	116		0000502	p	600010000	ge p		185010000	20.e6	n
0000353	cntrlvar	117		*	accumulator check valve						
0000354	cntrlvar	118		0000503	p	615010000	ge p		185010000	20.e6	n
0000355	cntrlvar	119		*	isolation valve hot leg						
0000356	cntrlvar	120		0000504	time	0	lt null	0	0.0		1
0000357	cntrlvar	121		*	isolation valve cold leg						
0000358	cntrlvar	122		0000505	time	0	lt null	0	0.0		1
0000359	cntrlvar	123		*	qobv hot leg						
0000360	cntrlvar	251		0000506	time	0	lt null	0	0.0		1
0000361	cntrlvar	252		*	qobv cold leg						
0000362	cntrlvar	253		0000507	time	0	lt null	0	0.0		1
0000363	cntrlvar	126		*	check valve surge line pressurizer						
0000364	cntrlvar	127		0000508	time	0	ge null	0	0.0		1

* pressurizer relief valve
 0000509 tempf 100010000 ge null 0 597.0 1 0000615 -612 and 609 n
 * steam control valve
 0000510 time 0 lt null 0 0.0 1 0000616 615 and 614 n
 0000617 612 or 616 n
 * boundary system valve
 0000511 time 0 lt null 0 0.0 1 0000621 623 or 570 n
 0000622 -571 and -571 n
 * lpis trip
 0000512 time 0 ge null 0 10000.0 1 0000623 621 and 622 n
 * hpis trip
 0000513 time 0 ge null 0 10000.0 1 0000624 509 and -552 n
 0000625 623 or 624 n
 0000626 576 and -509 n
 * 0000627 -576 and -577 n
 0000520 p 530020000 gt null 0 7.103448e6 n 0000628 629 and 627 n
 0000521 p 530020000 lt null 0 7.0344827e6 n 0000629 626 or 628 n
 0000522 p 530020000 gt null 0 6.3448275e6 n 0000635 504 and 504 n
 0000523 p 530020000 lt null 0 6.4137931e6 n 0000636 509 and -536 n
 0000530 time 0 ge null 0 3600.0 n 0000650 -652 and 550 n
 0000531 p 530020000 gt p 547010000 0.0 n 0000651 650 or 652 n
 0000536 time 0 ge null 0 10000.0 n 0000652 -509 and 651 n
 0000540 tempf 100010000 gt null 0 583.16 1 0000655 601 or 603 n
 0000541 p 100010000 gt null 0 1.574553e7 1 0000656 508 or 609 n
 0000550 time 0 ge null 0 10000.0 1 0000659 561 or 562 n
 0000551 time 0 ge timeof 625 0.0 1 0000660 504 or 504 n
 0000552 time 0 ge timeof 509 1580. 1 0000669 561 and 564 1
 0000560 p 100010000 le null 0 13.15862e6 n 0000670 565 and -655 n
 0000561 time 0 ge timeof 552 265.0 1 0000680 530 or 530 n
 0000562 time 0 gt null 0 5400.0 n 0000688 690 or 574 n
 0000563 cntrlvar 1 lt null 0 2.1844 n 0000689 -575 and -551 n
 0000564 cntrlvar 1 gt null 0 2.9464 n 0000690 688 and 689 n
 0000565 time 0 ge timeof 669 966. 1 **** pqr heater delete
 0000570 p 420010000 gt null 0 1.620058e7 n 14201000 delete
 0000571 p 420010000 lt null 0 1.606269e7 n 14202000 delete
 0000572 p 420010000 lt null 0 1.486300e7 n *----1----1----1
 0000573 p 420010000 gt null 0 1.506980e7 n * control variable 114 re-define
 0000574 p 420010000 gt null 0 1.533874e7 n *----1----1----1
 0000575 p 420010000 lt null 0 1.505000e7 n 20511400 pqrheat sum 1.0 0.0 1
 0000576 p 420010000 lt null 0 1.482853e7 n 20511401 0.0 0.362 htrnr 415100101
 0000577 p 420010000 gt null 0 1.495950e7 n 20511402 0.702464 htrnr 415200101

 * logical trips

 0000600 536
 * modify from 670 in original input
 0000601 563 and 561 n 20511403 1.26381 htrnr 415200201
 0000602 -563 and -564 n 20511404 1.26381 htrnr 415200301
 0000603 655 and 602 n 20511405 0.649152 htrnr 415200401
 0000604 609 or 609 1 20511406 0.649152 htrnr 415200501
 0000605 572 and -509 n 20511407 0.534688 htrnr 415200601
 0000606 -572 and -573 n 20511408 0.534688 htrnr 415200701
 0000607 608 and 606 n 20511409 0.273063 htrnr 416200101
 *----1----1----1
 * control variable 123 redefine
 *----1----1----1
 20512300 pqr sum 1.0 0. 1
 0000608 605 or 607 n 20512301 0.0 0.362 htrnr 415100100
 0000609 540 or 541 1 20512302 0.59522 htrnr 415200100
 0000610 612 or 520 n 20512303 1.07086 htrnr 415200200
 0000611 -521 and -616 n 20512304 1.07086 htrnr 415200300
 0000612 611 and 610 n 20512305 0.550045 htrnr 415200400
 0000613 616 or 523 n 20512306 0.550045 htrnr 415200500
 0000614 -522 and 613 n 20512307 0.453056 htrnr 415200600
 20512308 0.453056 htrnr 415200700

20512309	0.150656	htrnr	416200100					

* primary coolant pump 1								

1350000	pcpump1	pump						
1350101	0.0366	0.0	0.099	0.0	90.0	0.319		
1350102	00000							
1350108	130010000	0.0	0.0	0.0	000100			
1350109	140000000	0.0	0.05	0.05	000100			
1350200	0	14818100.	1242890.	2463900.0	0.0			
1350201	0	8.8943000	9.2942000	0.0				
1350202	0	8.8928000	8.1177000	0.0				
1350301	0	0	0	-1	0	509	0	
1350302	369.00	.90178860	.31550	96.00	500.60	1.4310		
1350303	613.6	0.0	207.0000	0.0040000	19.598000	0.0		
1350310	0.0	0.0	0.0					
*								

* single phase head curves								

* head curve no. 1								

1351100	1	1						
1351101	0.000000e+00		1.403600e+00					
1351102	1.906100e-01		1.363600e+00					
1351103	3.896300e-01		1.318600e+00					
1351104	5.939600e-01		1.2232800e+00					
1351105	7.902000e-01		1.133600e+00					
1351106	1.000000e+00		1.000000e+00					

* head curve no. 2								

1351200	1	2						
1351201	0.000000e+00		-6.700000e-01					
1351202	2.000000e-01		-5.000000e-01					
1351203	4.000000e-01		-2.500000e-01					
1351204	5.755400e-01		0.000000e+00					
1351205	7.443200e-01		2.583000e-01					
1351206	7.734800e-01		3.778000e-01					
1351207	8.631300e-01		6.326000e-01					
1351208	1.000000e+00		1.000000e+00					

* head curve no. 3								

1351300	1	3						
1351301	-1.000000e+00		2.472200e+00					
1351302	-8.057400e-01		2.047400e+00					
1351303	-6.069000e-01		1.831000e+00					
1351304	-4.068300e-01		1.624000e+00					
1351305	-2.001710e-01		1.470500e+00					
1351306	0.000000e+00		1.403600e+00					

* head curve no. 4								

1351400	1	4						
1351401	-1.000000e+00		2.472200e+00					

* single phase torque data								

* torque curve no. 1								


```

* head curve no. 1
*-----1-----1-----1-----1-----1-----
1354100 1 1
1354101 0.000000e+00 0.000000e+00
1354102 1.000000e-01 8.300000e-01
1354103 2.000000e-01 1.090000e+00
1354104 5.000000e-01 1.020000e+00
1354105 7.000000e-01 1.010000e+00
1354106 9.000000e-01 9.400000e-01
1354107 1.000000e+00 1.000000e+00
*-----1-----1-----1-----1-----1-----
* head curve no. 2
*-----1-----1-----1-----1-----1-----
1354200 1 2
1354201 0.000000e+00 0.000000e+00
1354202 1.000000e-01 -4.000000e-02
1354203 2.000000e-01 0.000000e+00
1354204 3.000000e-01 1.000000e-01
1354205 4.000000e-01 2.100000e-01
1354206 8.000000e-01 6.700000e-01
1354207 9.000000e-01 8.000000e-01
1354208 1.000000e+00 1.000000e+00
*-----1-----1-----1-----1-----1-----
* head curve no. 3
*-----1-----1-----1-----1-----1-----
1354300 1 3
1354301 -1.000000e+00 -1.160000e+00
1354302 -9.000000e-01 -1.240000e+00
1354303 -8.000000e-01 -1.770000e+00
1354304 -7.000000e-01 -2.360000e+00
1354305 -6.000000e-01 -2.790000e+00
1354306 -5.000000e-01 -2.910000e+00
1354307 -4.000000e-01 -2.670000e+00
1354308 -2.500000e-01 -1.690000e+00
1354309 -1.000000e-01 -5.000000e-01
1354310 0.000000e+00 0.000000e+00
*-----1-----1-----1-----1-----1-----
* head curve no. 4
*-----1-----1-----1-----1-----1-----
1354400 1 4
1354401 -1.000000e+00 -1.160000e+00
1354402 -9.000000e-01 -7.800000e-01
1354403 -8.000000e-01 -5.000000e-01
1354404 -7.000000e-01 -3.100000e-01
1354405 -6.000000e-01 -1.700000e-01
1354406 -5.000000e-01 -8.000000e-02
1354407 -3.500000e-01 0.000000e+00
1354408 -2.000000e-01 5.000000e-02
1354409 -1.000000e-01 8.000000e-02
1354410 0.000000e+00 1.100000e-01
*-----1-----1-----1-----1-----1-----
* head curve no. 5
*-----1-----1-----1-----1-----1-----
1354500 1 5
1354501 0.000000e+00 0.000000e+00
1354502 2.000000e-01 -3.400000e-01
1354503 4.000000e-01 -6.500000e-01
1354504 6.000000e-01 -9.300000e-01
1354505 8.000000e-01 -1.190000e+00
1354506 1.000000e+00 -1.470000e+00
*-----1-----1-----1-----1-----1-----
* head curve no. 6
*-----1-----1-----1-----1-----1-----
1354600 1 6
1354601 0.000000e+00 1.100000e-01
1354602 1.000000e-01 1.300000e-01
1354603 2.500000e-01 1.500000e-01
1354604 4.000000e-01 1.300000e-01
1354605 5.000000e-01 7.000000e-02
1354606 6.000000e-01 -4.000000e-02
1354607 7.000000e-01 -2.300000e-01
1354608 8.000000e-01 -5.100000e-01
1354609 9.000000e-01 -9.100000e-01
1354610 1.000000e+00 -1.470000e+00
*-----1-----1-----1-----1-----1-----
* head curve no. 7
*-----1-----1-----1-----1-----1-----
1354700 1 7
1354701 -1.000000e+00 0.000000e+00
1354702 0.000000e+00 0.000000e+00
*-----1-----1-----1-----1-----1-----
* head curve no. 8
*-----1-----1-----1-----1-----1-----
1354800 1 8
1354801 -1.000000e+00 0.000000e+00
1354802 0.000000e+00 0.000000e+00
*-----1-----1-----1-----1-----1-----
* torque curve no. 1
*-----1-----1-----1-----1-----1-----
1354900 2 1
1354901 0.000000e+00 6.032000e-01
1354902 1.930000e-01 6.325000e-01
1354903 3.930000e-01 7.369000e-01
1354904 5.955200e-01 8.331000e-01
1354905 7.978200e-01 9.229000e-01
1354906 1.000000e+00 1.000000e+00
*-----1-----1-----1-----1-----1-----
* torque curve no. 2
*-----1-----1-----1-----1-----1-----
1355000 2 2
1355001 0.000000e+00 -6.700000e-01
1355002 4.000000e-01 -2.500000e-01
1355003 5.000000e-01 1.500000e-01
1355004 7.372550e-01 5.265860e-01
1355005 7.680490e-01 6.065940e-01
1355006 8.672300e-01 7.436600e-01
1355007 1.000000e+00 1.000000e+00
*-----1-----1-----1-----1-----1-----
* torque curve no. 3
*-----1-----1-----1-----1-----1-----
1355100 2 3
1355101 -1.000000e+00 1.984300e+00

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1355102 -8.009600e-01 1.394000e+00
1355103 -6.063800e-01 1.097500e+00
1355104 -4.068600e-01 8.220000e-01
1355105 -1.992800e-01 6.648000e-01
1355106 0.000000e+00 6.032000e-01
*****1-----1-----1-----1-----1-----
* torque curve no. 4
*****1-----1-----1-----1-----1-----
1355200 2 4
1355201 -1.000000e+00 1.984300e+00
1355202 -8.223400e-01 1.830800e+00
1355203 -6.337100e-01 1.682400e+00
1355204 -4.585300e-01 1.557000e+00
1355205 -2.670230e-01 1.436200e+00
1355206 -1.761070e-01 1.387900e+00
1355207 -8.931000e-02 1.348100e+00
1355208 0.000000e+00 1.233610e+00
*****1-----1-----1-----1-----1-----
* torque curve no. 5
*****1-----1-----1-----1-----1-----
1355300 2 5
1355301 0.000000e+00 -4.500000e-01
1355302 4.000000e-01 -2.500000e-01
1355303 5.000000e-01 0.000000e+00
1355304 1.000000e+00 3.569000e-01
*****1-----1-----1-----1-----1-----
* torque curve no. 6
*****1-----1-----1-----1-----1-----
1355400 2 6
1355401 0.000000e+00 1.233610e+00
1355402 9.064300e-02 1.196500e+00
1355403 1.885690e-01 1.109600e+00
1355404 2.734700e-01 1.041600e+00
1355405 4.586690e-01 8.958000e-01
1355406 5.744800e-01 7.807000e-01
1355407 7.381600e-01 6.134000e-01
1355408 7.685200e-01 5.849000e-01
1355409 8.700570e-01 4.877000e-01
1355410 1.000000e+00 3.569000e-01
*****1-----1-----1-----1-----1-----
* torque curve no. 7
*****1-----1-----1-----1-----1-----
1355500 2 7
1355501 -1.000000e+00 -1.000000e+00
1355502 -3.000000e-01 -9.000000e-01
1355503 -1.000000e-01 -5.000000e-01
1355504 0.000000e+00 -4.500000e-01
*****1-----1-----1-----1-----1-----
* torque curve no. 8
*****1-----1-----1-----1-----1-----
1355600 2 8
1355601 -1.000000e+00 -1.000000e+00
1355602 -2.500000e-01 -9.000000e-01
1355603 -8.000000e-02 -8.000000e-01
1355604 0.000000e+00 -6.700000e-01
*****1-----1-----1-----1-----1-----

```

```

* pcp1 pump velocity table
*****
1356100 536
1356101 0.0 0.0
1356102 1.0 220.
*****
* primary coolant pump 2
*****
1650000 pcpump2 pump
1650101 0.0366 0.0 0.099 0.0 90.0 0.319
1650102 00000
1650108 160010000 0.0 0.0 0.0 000100
1650109 170000000 0.0 0.1 0.1 000100
1650200 0 14832700. 1242890. 2463590.0 0.0
1650201 0 8.4974000 8.8872000 0.0
1650202 0 8.4959000 6.6507000 0.0
1650301 135 135 135 -1 135 509 0
1650302 369.0 .89699187 .31550 96.000 500.60000 1.431
1650303 613.6 0.0 207.433 0.004 19.5980 0.0
1650310 0.0 0.0 0.0
*****1-----1-----1-----1-----1-----
* spray valve
*****1-----1-----1-----1-----1-----
4070000 sprv1v valve
4070101 406010000 420010000 3.3451e-4 15.432 15.432
000100
4070201 0 .000000 .000000 0.0
4070300 trpv1v
4070301 690
*****1-----1-----1-----1-----1-----
* air cooled condenser
*****1-----1-----1-----1-----1-----
5470000 condens tmdpvol
5470101 0.21677 17.67 0.0 0.0 0.0 0.0
5470102 4.e-5 0.0 00000
5470200 1 680
5470201 0.0 559.15 0.999
5470202 18000. 334.15 0.999
*****1-----1-----1-----1-----1-----
* aux feed water
*****1-----1-----1-----1-----1-----
5480000 auxfeed tmdpjun
5480101 553000000 510000000 0.10
5480200 1 655
5480201 -1.0 0.0 0.0 0.0
5480202 0.0 0.0 0.0 0.0
5480203 0.0 2.5207 0.0 0.0
*****1-----1-----1-----1-----1-----
* steam flow control valve
*****1-----1-----1-----1-----1-----
*5500000 cv-p4-1 valve
*5500101 530010000 535000000 0.0043266 0.0 0.0 000100
*5500201 0 18.276 20.246 0.0
* initial velocity modified from 21.268, 21.599 in original
one
*5500300 mtrvlv

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*5500301 612   616   0.05   0.7279808   550
* initial valve position modified from 0.67 in original one
*----1---1---1---1---1---1---1---1---1---
* main feed water valve
*----1---1---1---1---1---1---1---1---1---
5600000 mnfeed      tmdpjun
5600101 545000000 510000000 0.05
5600200 1       656
5600201 0.0     26.533  26.533  0.0
5600202 0.0     0.0     0.0     0.0
*****core collapsed liquid level*****
*20255000 normarea 0 1.0 1.0
*20255001 0.0    9.25e-3
*20255002 9.25e-3 9.25e-3
*20255003 1.0    1.0
*****reactor kinetics data*****
*
*      reactor kinetics data
*
*****point separabl*****
30000000 point separabl
30000001 gamma-ac 49.6e+6 0.0 348.43  1.0  0.556
30000002 ans79-1
*****delayed neutron constants*****
30000101 0.0349  0.01275
30000102 0.2035  0.03177
30000103 0.1848  0.1181
30000104 0.4046  0.3160
30000105 0.1401  1.402
30000106 0.0321  3.914
*****
* power history
*****
30000401 4.89e+7 70. hr
*****reactivity curve numbers*****
30000011 609
*****moderator density reactivity table*****
30000501 0.62626e+3 -4.4769
30000502 0.66396e+3 -3.2923
30000503 0.71617e+3 -1.5692
30000504 0.76112e+3 -0.1692
30000505 0.76837e+3  0.04615
30000506 0.79157e+3  0.6923
30000507 0.81188e+3  1.2398
30000508 0.86263e+3  2.2415
30000509 0.93804e+3  3.9231
30000510 0.99749e+3  5.1077
*****doppler reactivity table*****

```

```

* doppler reactivity table
*****
30000601 293.16  1.375
30000602 338.72  1.125
30000603 422.05  0.682
30000604 477.60  0.419
30000605 505.38  0.274
30000606 570.72  0.000
30000607 588.72  -0.075
30000608 695.83  -0.526
30000609 922.05  -1.386
30000610 1310.94 -2.543
30000611 1810.94 -3.865
30000612 2088.72 -4.502
30000613 2499.83 -5.392
30000614 3027.60 -6.417
*****volume weighting factors*****
* moderator temperature feedback
*****
30000701 230010000 0  0.31493  0.0
30000702 230020000 0  0.31493  0.0
30000703 230030000 0  0.37014  0.0
*****doppler feedback*****
30000801 2300001  0  0.43153  0.0
30000802 2300002  0  0.51686  0.0
30000803 2300003  0  0.05161  0.0
*----1---1---1---1---1---1---1---1---1---
* scram reactivity data
*----1---1---1---1---1---1---1---1---1---
20260900 "reac-t" 609
20260901 0.0    0.0
20260902 0.5    -0.5
20260903 0.59   -3.13
20260904 0.65   -3.95
20260905 0.75   -6.27
20260906 0.83   -8.72
20260907 0.90   -12.00
20260908 0.97   -17.12
20260909 1.125  -20.67
20260910 1.213  -22.10
20260911 1.3    -22.78
20260912 1.4    -23.17
20260913 1.6    -23.32
20260914 60.0   -23.32
.
```

BIBLIOGRAPHIC DATA SHEET

(See instructions on the reverse)

2. TITLE AND SUBTITLE

Assessment of RELAP5/MOD3 with the LOFT L9-1/L3-3 Experiment
Simulating an Anticipated Transient with Multiple Failures

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Young Seok Bang, Kwang Won Seul and Hho Jung Kim

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10. SUPPLEMENTARY NOTES

11. ABSTRACT (200 words or less)

The RELAP5/MOD3 5m5 code was assessed using the L9-1/L3-3 test carried out in the LOFT facility, a 1/60-scaled experimental reactor, simulating a loss of feedwater accident with multiple failures and the sequentially-induced small break loss-of-coolant accident. The code predictability was evaluated for the four separated sub-periods with respect to the system response; initial heatup phase, spray and PORV cycling phase, blowdown phase and recovery phase. Based on the comparisons of the results from the calculation with the experiment data, it is shown that the overall thermal-hydraulic behavior important to the scenario such as a heat removal between the primary side and the secondary side and a system depressurization was well-predicted and that the code could be applied to the full-scale nuclear power plant for an anticipated transient with multiple failures within a reasonable accuracy. The minor discrepancies between the prediction and the experiment were identified in reactor scram time, post-scram behavior in the initial heatup phase, excessive heatup rate in the cycling phase, insufficient energy convected out the PORV under the hot leg stratified condition in the saturated blowdown phase and void distribution in secondary side in the recovery phase. This may come from the code uncertainties in predicting the spray mass flow rate, the associated condensation in pressurizer and junction fluid density under stratified condition.

12. KEY WORDS/DESCRIPTORS (List words or phrases that will assist researchers in locating the report.)

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RELAPS/MOD3
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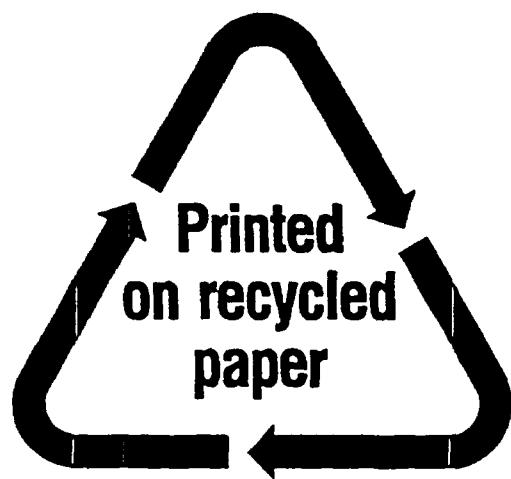
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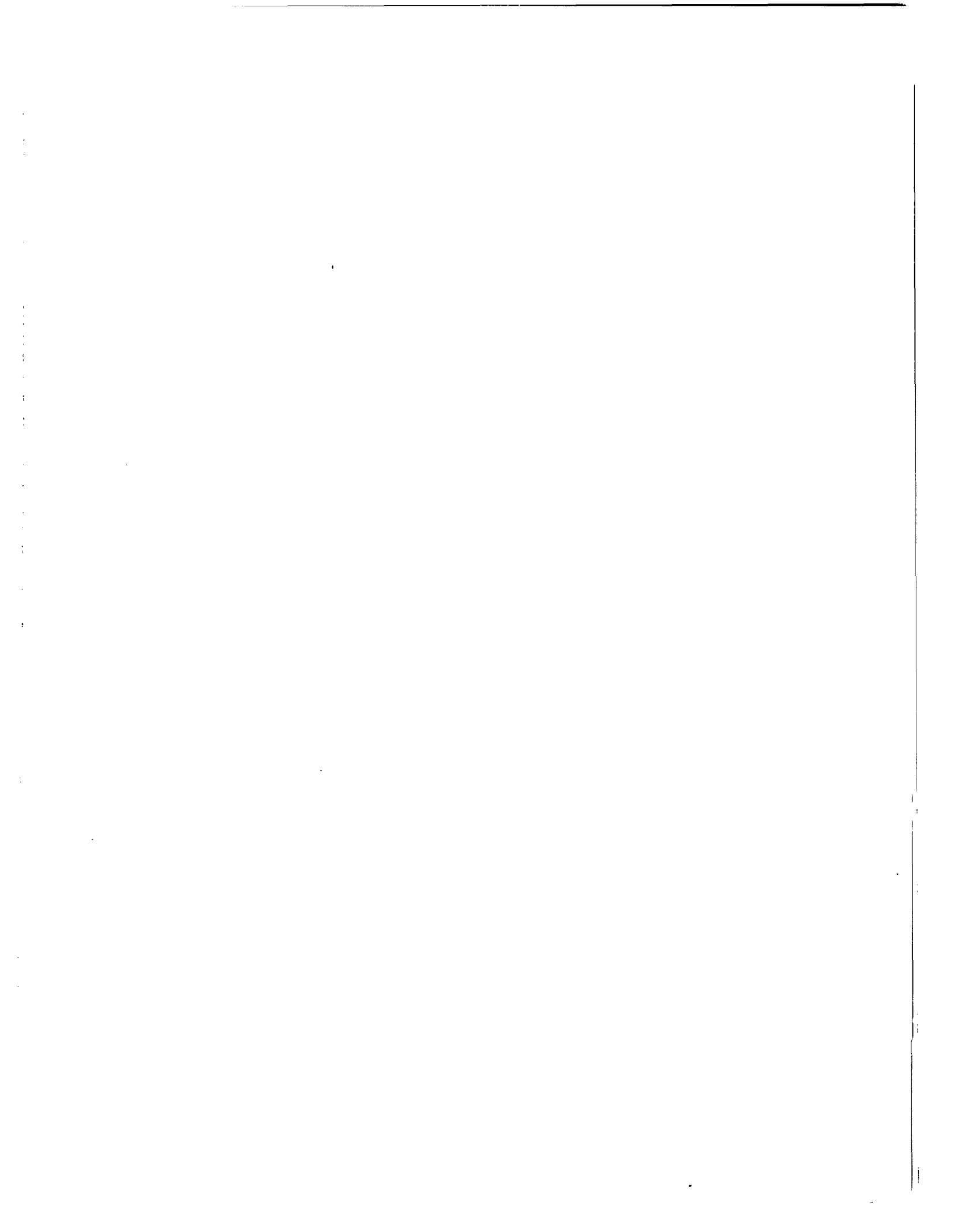
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