

August 1, 2006 JAFP-06-0119 Entergy Nuclear Northeast Entergy Nuclear Operations, Inc. James A. Fitzpatrick NPP P.O. Box 110 Lycoming, NY 13093 Tel 315 349 6024 Fax 315 349 6480

Pete Dietrich Site Vice President - JAF

U.S. Nuclear Regulatory Commission ATTN: Document Control Desk Washington, D. C. 20555

Subject: James A. FitzPatrick Nuclear Power Plant Docket No. 50-333 <u>Response to Request for Additional Information (RAI) Regarding</u> <u>Amendment Application to Revise Technical Specifications on DC</u> <u>Electrical System Requirements (TAC No. MC7204)</u>

References:

- 1. Entergy Nuclear Operations, Inc. letter to USNRC (JAFP-05-0082), Proposed Technical Specification Amendment to DC Electrical System Requirements, dated April 27, 2005.
- 2. USNRC letter to Entergy Nuclear Operations, Inc., Request for Additional Information Regarding Amendment Application to Revise Technical Specifications on DC Electrical System Requirements, dated March 30, 2006 (TAC No. MC7204).

Dear Sir/Madam:

By letter dated April 27, 2005 (Reference 1), Entergy Nuclear Operations, Inc. (ENO) proposed to amend the Technical Specifications (TS) for the James A. FitzPatrick Nuclear Power Plant (JAFNPP) by revising TS 3.8.4, 3.8.5, 3.8.6 and 5.5.14, all of which deal with the DC electrical system. These proposed changes were based on TS Task Force (TSTF) Change Traveler TSTF-360 (Revision 1) that was approved generically for the boiling water reactor (BWR) Standard TS, NUREG-1433 (BWR/4).

ENO received a request for additional information (RAI) from the NRC (Reference 2). Attachment 1 to this letter provides the response to the RAI questions. As stated in the attached RAI response ENO no longer requests changes to TS sections 3.8.5, 3.8.6 and 5.5.14, due to generic industry issues associated with those proposed changes. The proposed changes are now limited to TS section 3.8.4.

This response only reduces the scope of the original application and does not change the conclusions of the No Significant Hazards Consideration or the Environmental Assessment, contained in Reference 1. There are no commitments made by the Licensee in this letter.

Attachment 2 provides existing TS pages marked-up to show the proposed changes. Attachment 3 provides typed TS pages with the proposed changes incorporated. Attachment 4 provides a draft copy of the associated TS Bases pages marked-up to show the proposed

changes. These marked-up and retyped pages replace all of the marked-up and retyped pages in the original proposed amendment (Reference 1).

Should you have any questions or comments concerning this submittal, please contact Mr. James Costedio at (315) 349-6358.

I declare under penalty of perjury that the foregoing is true and correct.

Executed on this the 1^{4} day of <u>Aucus</u> 2006. Sinceret Pete Dietrich Site Vice President

Attachments:

- 1. Response to Request for Additional Information
- 2. Proposed TS Pages (Mark-up)
- 3. Proposed TS Pages (Retyped)
- 4. Proposed TS Bases Changes (Mark-up)
- cc: Regional Administrator, Region I U. S. Nuclear Regulatory Commission 475 Allendale Road King of Prussia, PA 19406-1415

Office of the Resident Inspector U. S. Nuclear Regulatory Commission P. O. Box 136 Lycoming, NY 13093

Mr. John P. Boska Plant Licensing Branch I-1 Division of Operating Reactor Licensing Office of Nuclear Reactor Regulation U. S. Nuclear Regulatory Commission Mail Stop O-8-C2 Washington, DC 20555-0001

Mr. Peter R. Smith, President NYSERDA 17 Columbia Circle Albany, NY 12203-6399 Mr. Paul Eddy New York State Department of Public Service 3 Empire State Plaza, 10th Floor Albany, New York 12223

Attachment 1 to JAFP-06-0119

Entergy Nuclear Operations, Inc. – FitzPatrick Docket No. 50-333

RAI 1

"Specific gravity monitoring is used to measure the strength of a battery cell's electrolyte, which is an important component of the battery's chemical reaction, and provides an indication of the battery's state-of-charge. Whereas, float current monitoring may or may not provide an accurate indication of the battery's state-of-charge. Float current monitoring is based on a calculation that is dependent on several variables. The staff has a concern with two variables of this calculation: the applied charging voltage and cell resistance. A change in either of these variables may provide a false indication of the battery's state-of-charge. Provide assurance that float current monitoring will provide an accurate indication of the battery's state-of-charge."

RESPONSE

The proposed amendment (Reference 1) changes to TS sections 3.8.5, 3.8.6 and 5.5.14 are no longer requested. The proposed changes are limited to TS section 3.8.4. Specific gravity monitoring is still being performed and will continue to provide indication of the battery state of charge.

RAI 2

"The battery pilot cell is representative of the average battery cell in the battery. Provide assurance that a battery with a battery pilot cell with a voltage of 2.07 volts or slightly greater will remain capable of performing its minimum designed function."

RESPONSE

The proposed amendment (Reference 1) changes to TS sections 3.8.5, 3.8.6 and 5.5.14 are no longer requested. The proposed changes are limited to TS section 3.8.4. The current TS associated with the battery pilot cell voltage will remain unchanged.

RAI 3

"As mentioned in question 2, the battery pilot cell is representative of the average battery cell in the battery. Provide assurance that a battery with a battery pilot cell electrolyte temperature slightly greater than or equal to the minimum established design limit will remain capable of performing its minimum designed function."

RESPONSE

The proposed amendment (Reference 1) changes to TS sections 3.8.5, 3.8.6 and 5.5.14 are no longer requested. The proposed changes are limited to TS section 3.8.4. The current TS associated with the pilot cell electrolyte temperature will remain unchanged.

Attachment 1 to JAFP-06-0119 Entergy Nuclear Operations, Inc. – FitzPatrick Docket No. 50-333

RAI 4

"Consistency with the Institute of Electrical and Electronics Engineers (IEEE) Standard 450-1995, "IEEE Recommended Practice for Maintenance, Testing, and Replacement of Vented Lead-Acid Batteries for Stationary Applications," was used throughout your submittal as the justification for approval. The most recent version of IEEE Standard 450 that has been endorsed by the NRC through Regulatory Guides (RGs) is IEEE Standard 450-1975. The RGs of mention are: RG 1.128, "Installation, Design, and Installation of Large Lead Storage Batteries for Nuclear Power Plants," and RG 1.129, "Maintenance, Testing, and Replacement of Large Lead Storage Batteries for Nuclear Power Plants.

- a. Provide a plant specific technical justification for each proposed change in lieu of referencing consistency with the IEEE Standard 450-1995.
- b. Provide a copy of the proposed battery monitoring and maintenance program identified in TS 5.5.14."

RESPONSE

The proposed amendment (Reference 1) changes to TS sections 3.8.5, 3.8.6 and 5.5.14 are no longer requested. The proposed changes are limited to TS section 3.8.4. As such, reference to IEEE 450-1995 (Reference 2) is no longer made, and a battery monitoring and maintenance program is no longer identified, in TS 5.5.14.

REFERENCES

- 1. Entergy Nuclear Operations, Inc. letter to USNRC (JAFP-05-0082), Proposed Technical Specification Amendment to DC Electrical System Requirements, dated April 27, 2005.
- 2. Institute of Electrical and Electronics Engineers (IEEE) Standard 450-1995, "IEEE Recommended Practice for Maintenance, Testing, and Replacement of Vented Lead-Acid Batteries for Stationary Applications"

Attachment 2 to JAFP-06-0119

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Entergy Nuclear Operations, Inc. – FitzPatrick Docket No. 50-333

PROPOSED TECHNICAL SPECIFICATION CHANGES (MARK-UP)

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3.8 ELECTRICAL POWER SYSTEMS

3.8.4 DC Sources – Operating

- LCO 3.8.4 The following DC electrical power subsystems shall be OPERABLE:
 - a. Two 125 VDC subsystems; and
 - b. Two 419 VDC low pressure coolant injection (LPCI) MOV independent power supply subsystems.

APPLICABILITY: MODES 1, 2, and 3.

ACTIONS

[INSERT]	<u> </u>	CONDITION		REQUIRED ACTION	COMPLETION TIME	-
(B)	, к. (One 125 VDC electrical power subsystem inoperable for reasons other than Condition A.	B .1	Restore 125 VDC electrical power subsystem to OPERABLE status.	8 hours	-
Ć	ø.	Required Action and associated Completion Time of Condition A not met.	() 2.1 AND 2.2 ()	Be in MODE 3. Be in MODE 4.	12 hours 36 hours	•
(b	£.	One or both 419 VDC LPCI MOV independent power supply subsystems inoperable.	K .1	Declare associated LPCI subsystem(s) inoperable.	Immediately	· - · · · · · · · · · · · · · · · · · ·

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Amendment -274

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SURVEILLANCE REQUIREMENTS

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		SURVEILLANCE	FREQUENCY
SR	3.8.4.1	<pre>Verify battery terminal voltage on float charge is: a. ≥ 127.8 VDC for 125 VDC batteries, and b. ≥ 396.2 VDC for 419 VDC LPCI MOV independent power supply batteries.</pre>	7 days
SR INS	3.8.4.2 Eret 2	Verify each 125 VDC battery charger supplies \ge 270 amps at \ge 128 VDC for \ge 4 hours.	24 months
SR	3.8.4.3		24 months

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(continued)

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TSTF-360 Inserts for Technical Specifications Pages Mark-Up

Insert 1

Α.	One battery charger on one 125 VDC power subsystem inoperable.	A.1	Restore battery terminal voltage to greater than or equal to the minimum established float voltage (127.8 VDC).	2 hours
		AND		
		A.2	Verify battery float current \leq 2 amps.	Once per 12 hours
		<u>AND</u>	Ĩ	
		A.3	Restore battery charger to OPERABLE status.	7 days

Insert 2

<u>OR</u>

Verify each 125 VDC battery charger can recharge the battery to the fully charged state within 24 hours while supplying the largest combined demands of the various continuous steady state loads, after a battery discharge to the bounding design basis event discharge state.

Attachment 3 to JAFP-06-0119

Entergy Nuclear Operations, Inc. – FitzPatrick Docket No. 50-333

PROPOSED TECHNICAL SPECIFICATION PAGES (RETYPED)

3.8 ELECTRICAL POWER SYSTEMS

3.8.4 DC Sources - Operating

- LCO 3.8.4 The following DC electrical power subsystems shall be OPERABLE:
 - a. Two 125 VDC subsystems; and
 - b. Two 419 VDC low pressure coolant injection (LPCI) MOV independent power supply subsystems.

APPLICABILITY: MODES 1, 2, and 3.

ACTIONS

	CONDITION		REQUIRED ACTION	COMPLETION TIME
Α.	One battery charger on One 125 VDC power subsystem inoperable.	A.1	Restore battery terminal voltage to greater than or equal to the minimum established float voltage (127.8 VDC).	2 hours
		AND		
		A.2	Verify battery float current <a> <	Once per 12 hours
		AND		
		A.3	Restore battery charger to OPERABLE status.	7 days
		L		

(continued)

ACTIONS (continued)

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CONDITION		REQUIRED ACTION		COMPLETION TIME
В.	One 125 VDC electrical power subsystem inoperable for reasons other than Condition A.	B.1	Restore 125 VDC electrical power subsystem to OPERABLE status.	8 hours
C.	Required Action and associated Completion Time of Condition A or B not met.	C.1 <u>AND</u> C.2	Be in MODE 3. Be in MODE 4.	12 hours 36 hours
D.	One or both 419 VDC LPCI MOV independent power supply subsystems inoperable.	D.1	Declare associated LPCI subsystem(s) inoperable.	Immediately

SURVEILLANCE REQUIREMENTS

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	SURVEILLANCE	FREQUENCY
SR 3.8.4.1	 Verify battery terminal voltage on float charge is: a. ≥ 127.8 VDC for 125 VDC batteries, and b. ≥ 396.2 VDC for 419 VDC LPCI MOV 	7 days
<u> </u>	independent power supply batteries.	
SR 3.8.4.2	Verify each 125 VDC battery charger supplies \ge 270 amps at \ge 128 VDC for \ge 4 hours.	24 months
	<u>OR</u>	
	Verify each battery charger can recharge the battery to the fully charged state within 24 hours while supplying the largest combined demands of the various continuous steady state loads, after a battery discharge to the bounding design basis event discharge state.	
SR 3.8.4.3	This Surveillance shall not normally be performed in MODE 1, 2, or 3 for the 125 VDC batteries. However, portions of the Surveillance may be performed to reestablish OPERABILITY provided an assessment determines the safety of the plant is maintained or enhanced. Credit may be taken for unplanned events that satisfy this SR.	
	Verify battery capacity is adequate to supply, and maintain in OPERABLE status, the required emergency loads for the design duty cycle when subjected to a battery service test or a modified performance discharge test.	24 months

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Attachment 4 to JAFP-06-0119

Entergy Nuclear Operations, Inc. – FitzPatrick Docket No. 50-333

PROPOSED TECHNICAL SPECIFICATION BASES CHANGES (MARKUP)

DC Sources - Operating B 3.8.4

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BASES	
BACKGROUND (continued)	Each 419 VDC LPCI MOV independent power supply subsystem is energized by the associated 419 VDC battery or the associated 419 VDC rectifier/charger. Each battery and rectifier/charger is exclusively associated with a 419 VDC LPCI MOV independent power supply subsystem and cannot be interconnected with the other 419 VDC LPCI MOV independent power supply subsystem.
	During normal operation, the DC loads are powered from the battery chargers with the batteries floating on the system. In cases where momentary loads are greater than the charger capability, or battery charger output voltage is low, or on loss of normal power to the battery charger, the DC loads are automatically powered from the batteries. Also, on a LPCI automatic actuation signal, the 419 VDC rectifier/ charger AC input breakers will open and the 600 VAC LPCI independent power supply inverters will be powered from the 419 VDC LPCI MOV independent power supply batteries.
	The DC power distribution system is described in more detail in Bases for LCO 3.8.7, "Distribution System-Operating," and LCO 3.8.8, "Distribution System-Shutdown."
INSERT 1)-	Each 125 VDC battery has adequate storage capacity to Parry the required load continuous votor approximately 2 hours (Ref. 4). Each 419 VDC LPCI MOV independent power supply battery has adequate storage capacity for one repositioning of the LPCI subsystem motor operated valves (MOVs) on its respective MOV bus.
	Each 125 VDC and 419 VDC battery is separately housed in a ventilated room apart from its charger and distribution centers. Each subsystem is located in an area separated physically and electrically from its redundant subsystem to ensure that a single failure in one subsystem does not cause. a failure in the redundant subsystem. There is no sharing between redundant subsystems such as batteries, battery chargers, or distribution panels.
	The 125 VDC batteries are sized to supply associated DC loads required for safe shutdown of the plant, following abnormal operational transients and postulated accidents, until AC power sources are restored (Ref. 4). The 419 VDC batteries are sized to produce required capacity at 80% of nameplate rating, corresponding to warranted capacity at end of life cycles and the 100% design demand. The minimum
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B 3.8.4-2

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Revision 3

DC Sources - Operating B 3.8.4

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BASES	· •		
BACKGROUND (continued)	design voltage limit f established in Referen voltage limit of each supply battery is esta	for each 125 VDC battery is lees 10 and 11. The minimum design 419 VDC LPCI MOV independent power blished in Reference 12.	
(INSERT 3)	Each 125 VDC and 419 V output capacity for th loads required during time maintaining its b 125 VDC battery charge the battery after disc fully charged state wh (Ref. 4).	DC battery charger has ample power e steady state operation of connected normal operation, while at the same attery bank fully charged. Each r has sufficient capacity to restore harging through its duty cycle to its ile supplying normal control loads	ercess
APPLICABLE SAFETY ANALYSES	The initial conditions transient analyses in a Chapter 14 (Ref. 6), as systems are OPERABLE. normal and emergency DO emergency auxiliaries, MODES of operation. Th supplies provide normal during all MODES of operation subsystems is consistent accident analyses and a of the plant. This into during accident condition	of Design Basis Accident (DBA) and the UFSAR, Chapter 6 (Ref. 5) and ssume that Engineered Safeguards The 125 VDC Power System provides C electrical power for the EDGs, and control and switching during all he 419 VDC LPCI MOV independent power 1 and emergency power for LPCI MOVs eration. The OPERABILITY of the DC nt with the initial assumptions of th is based upon meeting the design basis cludes maintaining DC sources OPERABL ions in the event of:	e S
	a. An assumed loss of all onsite AC powe	f all normal and reserve AC power or er; and	
	b. A worst case singl	le failure.	
	The DC sources satisfy (Ref. 7).	Criterion 3 of 10 CFR 50.36(c)(2)(ii))
LCO	The 125 VDC and 419 VDC subsystems - with each s one battery charger, an and interconnecting cab associated bus- are requ availability of the req and maintain it in a sa operational transient o electrical power subsys safety function from be	C LPCI MOV independent power supply subsystem consisting of one battery, ad the corresponding control equipment bling supplying power to the uired to be OPERABLE to ensure the uired power to shut down the reactor offe condition after an abnormal or a postulated DBA. Loss of any DC stem does not prevent the minimum eing performed (Ref S).	- - -
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Revision 3

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BASES	
APPLICABILITY	The DC electrical power sources are required to be OPERABLE in MODES 1, 2, and 3 to ensure safe plant operation and to ensure that:
	a. Acceptable fuel design limits and reactor coolant pressure boundary limits are not exceeded as a result of abnormal operational transients; and
	b. Adequate core cooling is provided, and containment integrity and other vital functions are maintained in the event of a postulated DBA.
	The DC electrical power requirements for MODES 4 and 5 and other specified conditions in which the DC electrical power sources are required are addressed in LCO 3.8.5, "DC Sources- Shutdown."
ACTIONS B	X .1
(INSERT 4)	Condition A represents one division of the 125 VDC Power System with a loss of ability to completely respond to an event, and a potential loss of ability to remain energized during normal operation. It is therefore imperative that the operator's attention focus on stabilizing the plant, minimizing the potential for complete loss of 125 VDC power to the affected division. The 8 hour limit is consistent with the allowed time for an inoperable DC Distribution System division.
for reasons other than Condition A (has	If one of the required 125 VDC power subsystems is inoperable (e.g., inoperable battery, inoperable battery) charger or inoperable battery charger and associated inoperable battery), the remaining 125 VDC power subsystem have the capacity to support a safe shutdown and to mitigate an accident condition. Since a subsequent worst case single failure could, however, result in the loss of minimum necessary 125 VDC power subsystems to mitigate a worst case accident, continued power operation should not exceed 8 hours. The 8 hour Completion Time reflects a reasonable time to assess plant status as a function of the inoperable 125 VDC power subsystem and, if the 125 VDC power subsystem is not restored to OPERABLE status, to prepare to effect an orderly and safe plant shutdown.

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DC Sources - Operating B 3.8.4



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B 3.8.4-5

Revision 3

BASES			
SURVEILLANCE REQUIREMENTS (continued)	<u>SR 3.8.4.2</u> <u>Battery charger capabi</u> design capacity of the UFSAR, Section 8.7 (Re restore the battery af to the fully charged s control loads. The min ensures that these requ	This SR verifies <u>lity-requirements are based on</u> the chargers (Ref. 3). According to f. 4), the battery charger is sized to the discharging through its duty cycle tate, while supplying the normal nimum required amperes and duration mirements can be satisfied.	
INSERTO	The Frequency is accept required to perform the controls existing to end during these 24 month Frequency is intended to cycle lengths.	able, given the plant conditions e test and the other administrative asure adequate charger performance intervals. In addition, this to be consistent with expected fuel	
	<u>SR 3.8.4.3</u>		
	A battery service test capability, as found, t (battery duty cycle) of discharge rate and test duty cycle requirements	is a special test of the battery's to satisfy the design requirements the DC electrical power system. The clength corresponds to the design (Ref. 10, 11, and 12).	Ð
	The Frequency of 24 mor conditions required to requirements existing t during this 24 month ir is intended to be consi lengths.	ths is acceptable, given plant perform the test and the other o ensure adequate battery performance iterval. In addition, this Frequency stent with expected fuel cycle	シ
	A modified performance lieu of a service test because a modified perf more severe test of bat	discharge test may be performed in This substitution is acceptable ormance discharge test represents a tery capacity than the service test.	
	The modified performance which envelopes both the discharge test requirem discharge test discharge cycle loads of the serve discharge current (temp performance discharge to by peak duty cycle load the battery capacity, to for the performance test the performance discharge	e discharge test is a complete test e service test and the performance ents. The modified performance e current envelopes the peak duty ice test followed by a constant erature corrected) for the est. Since the ampere-hours removed s represents a very small portion of he test rate can be changed to that t without compromising the results of ge test. The battery terminal voltage	

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Revision 3

TSTF-360 Inserts for TS Bases Pages Mark-Up

Insert 1

...meet the duty cycle(s) discussed in the UFSAR, Chapter 8 (Ref 4). The battery is designed with additional capacity above that required by the design duty cycle to allow for temperature variations and other factors.

Insert 2

The battery cells are of flooded lead acid construction with a nominal specific gravity of 1.215. This specific gravity corresponds to an open circuit battery voltage of approximately 124V for a 60 cell battery (i.e., cell voltage of 2.065 volts per cell (Vpc)). The open circuit voltage is the voltage maintained when there is no charging or discharging. Once fully charged with its open circuit voltage ≥ 2.07 Vpc, the battery cell will maintain its capacity for 30 days without further charging per manufacturer's instructions. Optimal long term performance however, is obtained by maintaining a float voltage of 2.17 to 2.25 Vpc for the 125 VDC batteries and 2.17 to 2.26 Vpc for the LPCI MOV independent power supply batteries. This provides adequate overpotential, which limits the formation of lead sulfate and self discharge. The nominal float voltage for the 125 VDC batteries is 2.20 Vpc, which corresponds to a total float voltage output of 132 V for a 60 cell battery. The nominal float voltage for the LPCI MOV independent power supply batteries.

Insert 3

The battery charger is normally in the float-charge mode. Float-charge is the condition in which the charger is supplying the connected loads and the battery cells are receiving adequate current to optimally charge the battery. This assures the internal losses of a battery are overcome and the battery is maintained in a fully charged state.

When desired, the charger can be placed in the equalize mode. The equalize mode is at a higher voltage than the float mode and charging current is correspondingly higher. The battery charger is operated in the equalize mode after a battery discharge or for routine maintenance. Following a battery discharge, the battery recharge characteristic accepts current at the current limit of the battery charger (if the discharge was significant, e.g., following a battery service test) until the battery terminal voltage approaches the charger voltage setpoint. Charging current then reduces exponentially during the remainder of the recharge cycle. Lead-calcium batteries have recharge efficiencies of greater than 95%, so once at least 105% of the ampere-hours discharged have been returned, the battery capacity would be restored to the same condition as it was prior to the discharge. This can be monitored by direct observation of the exponentially decaying charging current or by evaluating the amp-hours discharged from the battery and amp-hours returned to the battery.

Insert 4

A.1, A.2, and A.3

 $\mu = \frac{1}{2} \left(\frac{1}{2} \right)_{ij}$ Condition A represents one division of the 125 VDC Power System with one battery charger inoperable (e.g., the voltage limit of SR 3.8.4.1 is not maintained). The ACTIONS provide a tiered response that focuses on returning the battery to the fully charged state and restoring a fully qualified charger to OPERABLE status in a reasonable time period. Required Action A.1 requires that the battery terminal voltage be restored to greater than or equal to the minimum established float voltage within 2 hours. This time provides for returning the inoperable charger to OPERABLE status or providing an alternate means of restoring battery terminal voltage to greater than or equal to the minimum established float voltage. Restoring the battery terminal voltage to greater than or equal to the minimum established float voltage provides good assurance that, within 12 hours, the battery will be restored to its fully charge condition (Required Action A.2) from any discharge that might have occurred due to the charger inoperability. A discharged battery having terminal voltage of at least the minimum established float voltage indicates that the battery is on the exponential charging current portion (the second part) of its recharge cycle. The time to return a battery to its fully charged state under this condition is simply a function of the amount of the previous discharge and the recharge characteristic of the battery. Thus there is good assurance of fully recharging the battery within 12 hours, avoiding a premature shutdown with its own attendant risk.

If established battery terminal float voltage cannot be restored to greater than or equal to the minimum established float voltage within 2 hours, and the charger is not operating in the currentlimiting mode, a faulty charger is indicated. A faulty charger that is incapable of maintaining established battery terminal float voltage does not provide assurance that it can revert to and operate properly in the current limit mode that is necessary during the recovery period following a battery discharge event that the DC system is designed for.

If the charger is operating in the current limit mode after 2 hours, that is an indication that the battery is partially discharged and its capability margins will be reduced. The time to return the battery to its fully charged condition in this case is a function of the battery charger capacity, the amount of loads on the associated DC system, the amount of the previous discharge, and the recharge characteristic of the battery. The charge time can be extensive, and there is not adequate assurance that it can be recharged within 12 hours (Required Action A.2).

Required Action A.2 requires that the battery float current be verified as less than or equal to 2 amps. This indicates that, if the battery had been discharged as the result of the inoperable battery charger, it has now been fully recharged. If at the expiration of the initial 12 hour period the battery float current is not less than or equal to 2 amps, this indicates there may be additional battery problems and the battery must be declared inoperable.

Required Action A.3 limits the restoration time for the inoperable battery charger to 7 days. This action is applicable if an alternate means of restoring battery terminal voltage to greater than or equal to the minimum established float voltage has been used (e.g., balance of plant non-Class 1E battery charger). The 7 day Completion Time reflects a reasonable time to effect restoration of the qualified battery charger to Operable status.

Insert 5

..., while supplying the continuous steady state loads of the associated DC subsystem. On float charge, battery cells will receive adequate current to optimally charge the battery. The voltage requirements are based on the nominal design voltage of the battery and are consistent with the minimum float voltage established by the battery manufacturer (2.17 Vpc or 130.2 V at the 125 VDC battery terminals or 403.6 VDC for 419 VDC LPCI MOV independent power supply battery terminals). This voltage maintains the battery plates in a condition that supports maintaining the grid life (expected to be approximately 20 years).

Insert 6

This SR provides two options. One option requires that each battery charger be capable of supplying 270 amps at the minimum established float voltage for 4 hours. The ampere requirements are based on the output rating of the chargers. The voltage requirements are based on the charger voltage level after a response to a loss of AC power. The time period is sufficient for the charger temperature to have stabilized and to have been maintained for at least 2 hours.

The other option requires that each battery charger be capable of recharging the battery after a service test coincident with supplying the largest coincident demands of the various continuous steady state loads (irrespective of the status of the plant during which these demands occur). This level of loading may not normally be available following the battery service test and will need to be supplemented with additional loads. The duration for this test may be longer than the charger sizing criteria since the battery recharge is affected by float voltage, temperature, and the exponential decay in charging current. The battery is recharged when the measured charging current is ≤ 2 amps.