

Entergy Nuclear Operations, Inc. Pilgrim Station 600 Rocky Hill Road Plymouth, MA 02360

Stephen J. Bethay Director, Nuclear Assessment

June 29, 2006

U.S. Nuclear Regulatory Commission Attn: Document Control Desk Washington, D.C. 20555-0001

SUBJECT: Entergy Nuclear Operations, Inc. Pilgrim Nuclear Power Station Docket No. 50-293 License No. DPR-35

Pilgrim Fourth Ten-Year In-service Testing (IST) Program, IST Relief Request PR-03, Rev. 3

LETTER NUMBER: 2.06.008

- REFERENCES: 1. NRC Letter, Pilgrim Nuclear Power Station-Entergy Relief Request PR-03, High Pressure Coolant Injection Pump (TAC NO. MB8773) dated August 29, 2005
  - Entergy Letter No. 2.05.012, Pilgrim Fourth Ten-Year In-service Testing (IST) Program, IST Relief Request PR-03, dated February 24, 2005

Dear Sir or Madam:

By this letter Entergy submits the HPCI Pump Relief Request PR-03, Revision 3 for NRC approval to continue for the remaining duration of the IST interval the alternative testing previously approved by the NRC in Reference 1. The PR-03 Rev. 3 includes updated information based on the results of NRC approved alternative comprehensive test and additional information concerning the alternative testing.

Entergy submitted Relief Request, PR-03, Rev. 2 by Reference 2 for the fourth IST interval and NRC approved the alternative testing for use until August 29, 2008. The fourth IST interval began on December 7, 2002 and ends on December 6, 2012.

The scope of this relief applies to ASME OMa-1996, ISTB 5.2.3, Comprehensive Test for HPCI pumps and includes confirmation of operational readiness of HPCI pumps based on the NRC approved alternative comprehensive test results and historical pump test data.

Pursuant to 10 CFR 50.55 a(a)(3)(i), Entergy proposes to continue to use the alternative testing to comply with ISTB 5.2.3. The proposed alternative provides an acceptable level of quality and safety because it verifies the operational readiness of the as-built configuration of the HPCI pump, and the historical data has shown no signs of degradation in the HPCI pump.

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Pilgrim intends to continue to perform the alternative comprehensive HPCI surveillance test as approved for the remaining duration of the Fourth IST interval.

This letter contains no new commitments.

If you have any questions or require additional information, please contact Mr. Bryan Ford, Licensing Manager, at (508) 830-8403.

Sincerely,

Stephen J. Bethav

WGL/dm

Attachment: HPCI Pump Relief Request, PR-03, Revision 3 (86 pages)

cc: Mr. James J. Shea, Project Manager Office of Nuclear Reactor Regulation Mail Stop: 0-8B-1 U.S. Nuclear Regulatory Commission 1 White Flint North 11555 Rockville Pike Rockville, MD 20852

> U.S. Nuclear Regulatory Commission Region 1 475 Allendale Road King of Prussia, PA 19406

Senior Resident Inspector Pilgrim Nuclear Power Station

## **ATTACHMENT**

## HPCI Pump Relief Request, PR-03, Revision 3, (8 pages)

Enclosure 1 to PR-03, Rev. 3 (11 pages) Enclosure 2 to PR-03, Rev. 3 (66 pages)

(Total 86 pages)

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## PUMP RELIEF REQUEST PR-03, Revision 3

PUMP: P-205 (Main/Booster)

**<u>SYSTEM</u>:** High Pressure Coolant Injection (HPCI)

**<u>CLASS</u>**: 2

**FUNCTION:** Provides emergency core cooling subsequent to a small break LOCA.

## **TEST REQUIREMENTS:**

ASME OM Code OMa-1996, ISTB 5.2.3, Comprehensive Test

ISTB 5.2.3(d): Vibration (displacement or velocity) shall be determined and compared with corresponding reference values. Vibration measurements are to be broad band (unfiltered). If velocity measurements are used, they shall be peak. If displacement amplitudes are used, they shall be peak-to-peak.

ISTB 5.2.3(e): All deviations from the reference values shall be compared with the ranges of Tables ISTB 5.2.1-1 and ISTB 5.2.3-1 and corrective action taken as specified in paragraph ISTB 6.2. The vibration measurements shall be compared to the relative and absolute criteria shown in the Alert and Required Action Ranges of Table ISTB 5.2.1-1. For example, if vibration exceeds either 6 V<sub>r</sub> or 0.7 in./sec, the pump is in the Required Action Range.

### **RELIEF REQUESTED:**

Relief is requested from the ASME OMa-1996, ISTB 5.2.3(d) required method of determining the vibration velocity ( $V_v$ ) overall value for surveillance test use and for establishing reference values for the HPCI Main pump inboard (turbine side) bearing horizontal point (P3H) and the Main pump outboard (gearbox side) bearing horizontal point (P4H). PNPS proposes that the vibration occurring at the discrete frequency component that is at exactly 4x Booster pump RPM not be included as part of the vibration spectrum vector summing process to obtain the Main pump overall value for these points during comprehensive pump testing. This method is equivalent to extracting the discrete frequency component that is at exactly 4x Booster pump RPM from the broad band vibration spectrum. Since ISTB 5.2.3(d) requires broad band vibration measurements, NRC approved alternative testing is required to demonstrate the operational readiness of the HPCI pump taking into account the as-built configuration of the HPCI pump as specified in ISTB 4.3(g) and associated footnote.

Pilgrim requests relief from the Code requirements of paragraph ISTB 5.2.3(e) for the HPCI Main and Booster Pumps specifically from the vibration velocity ( $V_v$ ) acceptance criteria specified in Table ISTB 5.2.1-1 for all Main pump and Booster pump vibration points except for the Booster pump outboard horizontal axial vibration point (P8A). Pilgrim proposes to expand the Acceptable Range identified in Table ISTB 5.2.1-1, for pump Quarterly and Biennial Comprehensive vibration monitoring.

## **BASIS FOR RELIEF:**

Relief from the referenced Code requirements is based on the determination that the proposed alternative testing would provide an acceptable level of quality and safety in accordance with 10 CFR 50.55 a(a)(3)(i), as evidenced by the results of recent pump tests performed in November 2005 and February 2006, and historical vibration test data.

Historic testing and analysis performed on the HPCI System by PNPS (and the pump manufacturer) have consistently revealed characteristic pump vibration levels that exceed the acceptance criteria stated in Table ISTB 5.2.1-1. High vibration appears on the Main pump bearing housings at approximately 2x RPM in the horizontal direction, which is caused by Booster pump excitation (at 4x RPM of the booster pump). Under normal circumstances at 4000 rpm, the vibration amplitude at the Main pump bearings in the horizontal direction exceeds the OM Code absolute vibration Required Action Range of > 0.7 in./sec. Additionally, under the same conditions, all of the remaining HPCI Main and Booster pump vibration monitoring points, except for two, typically exceed the OM Code absolute acceptable range upper value of 0.325 in./sec.

The vibration characteristics of the HPCI pump are predominantly a function of the pump design and should be identified as such rather than attributed to pump degradation. The high vibration has been present to the same order of magnitude since the pump was new. Although existing vibration levels of the HPCI pump are higher than the acceptance criteria provided in Table ISTB 5.2.1-1, they reflect the unique operating characteristics of the HPCI pump design configuration. There are no major vibrational concerns that would result in pump degradation or would prevent the HPCI pump from performing its design safety function for an extended period of operation.

The purpose of the Code required testing is to demonstrate the operational readiness of the HPCI pump by monitoring pump vibrations for degradation and taking corrective actions when those vibration levels exceed the Code specified values. The Code specifies in ISTB 4.3(g) footnote that the reference vibration measurements should be representative of the pump and that the measured vibration will not prevent the pump from fulfilling its function. Accordingly, Pilgrim is proposing an alternative testing to demonstrate the operational readiness by taking into consideration the vibration measurements representative of the as-built configuration of the HPCI pump.

## Alternate Testing to the ASME OMa-1996 Code:

Pilgrim proposes alternative testing as follows.

- 1. The alternative testing proposes to remove the 4x Booster pump RPM frequency component (discrete peak) from the vibration spectrum of the Main pump since its amplitude is not related to the physical condition or rotating dynamics of the Main pump rotor or bearing system. The Main pump vibration spectrum, with this single 4x Booster pump RPM frequency component removed, has been shown to be stable and more useful for monitoring actual pump condition. When this vibration frequency component at 4x Booster pump RPM is subtracted from the Main pump vibration spectrum the remaining vibration, which is attributed to the Main pump, is below the OM Code Required Action Range. This corrected vibration level provides a more representative measurement of the pump condition to be used for trending.
- 2. All other discrete vibration peaks observed at the Main pump horizontal vibration points will be evaluated during each pump vibration test, and will have an Acceptable Range upper limit of 1.05 V<sub>r</sub> and an Alert Range upper limit 1.3 V<sub>r</sub>. The reviews of the frequency spectrum data ensure that any significant change in the vibration signature will be noted regardless of whether the severity causes the overall level to exceed its criteria. For example, if the overall vibration level is acceptable but the 1x RPM component has increased to greater than 1.3 times the reference value overall level (Vr), then the pump will be placed in the vibration Required Action Range (>0.7in./sec).

- 3. PNPS will increase the ASME OMa-1996, ISTB 5.2.3 required frequency for vibration monitoring (that is part of the comprehensive testing) from once/2 years to once/year. The Code required comprehensive test for flow rates would continue to be once/2 years. Given that the HPCI vibration will normally exceed the OM Code limiting Alert Range of >0.325 in./sec, the once/year frequency will be doubled to twice/year. The twice/year frequency will be the commitment frequency. However, the normal PNPS practice will be to monitor vibration in the same manner during each of the Quarterly Group B Hydraulic Tests, whenever practicable. Thus, vibration monitoring will be performed up to 8 times in two years as part of the Group B Hydraulic Tests; instead of once/2 years as part of the Comprehensive pump tests.
- 4. As normal practice, Pilgrim will continue to monitor vibration of HPCI pump during each of the Quarterly Group B Hydraulic Tests in the same manner as required by the OM Code. The preventive maintenance (PM) procedure will also typically be performed, which provides for vibration monitoring of specific pumps for preventive maintenance and balancing, and includes vibration monitoring and trending of the HPCI pump to detect and monitor changes in equipment conditions. As shown in the HPCI pump configuration figure, vibration monitoring is performed at locations required by the OM Code and at additional locations within the scope of the PM procedure (perpendicular to the shaft in the horizontal and vertical positions at each bearing locations and at axial direction to the shaft). Vibration monitoring is thereby routinely performed for the Main pump, Booster pump, Speed Reduction Gearbox, and Steam Turbine. Using the vibration data collected at these points, an accurate diagnosis is made by analyzing the vibration spectrum and planned maintenance is determined to prevent failures. Thus, HPCI pump vibration monitoring will be performed up to 8 times in 2 years as part of Group B Hydraulic Tests and preventive or corrective maintenance will be implemented as necessary to prevent failures. Enclosures 1 and 2 provide HPCI pump vibration spectrum at locations required by the OM Code procedure.
- 5. Pilgrim will continue current HPCI pump and turbine monitoring and maintenance activities, with changes as conditions warrant, as follows:
  - Quarterly pump and valve operability tests will be performed to ensure the HPCI pump and turbine function for the intended safety function.
  - Quarterly lubrication oil sampling and periodic laboratory analysis as appropriate for the pressure-fed bearings on the Turbine, Main pump, and Gear Reducer and once/cycle (2 years) sampling and analysis for the non-pressure fed Booster pump will be performed. Lubrication oil analysis currently performed includes viscosity, acidity, residue, water content, metals by A.E. spectrometry, and ferrogram readings. This type of monitoring will detect degradation of the turbine or pump bearings due to accelerated wear, fretting, surface fatigue, or oil contamination.
  - HPCI pump and Turbine lube oil system is serviced as-needed weekly. HPCI gland seal condenser hot well pump and motor bearings and HPCI auxiliary lube oil pump and motor bearings are serviced semiannually for lubrication.
  - HPCI Turbine/Main pump, Main pump/Reducer, and Reducer/Booster pump geartype shaft couplings are cleaned, examined, and grease-lubricated every 2 years. These examinations detect excessive wear, fretting, heating, or fatigue due to any unusual loading conditions.

Past monitoring and maintenance activities have shown no evidence or observations of degradation in the HPCI Turbine, Main pump, Gear Reducer, or Booster pump. The

attached HPCI and Booster pump historical vibration spectrum (Attachment 4) supports this conclusion. Thus, the continuation of the above periodic monitoring and maintenance activities will ensure that the HPCI pump remains in a high level of operational readiness and that degradation of HPCI pump mechanical condition, reliability, or performance will be detected and corrected in a timely manner.

### **Technical Justification:**

PNPS has conducted an evaluation of the HPCI pump vibration characteristics. An important conclusion of this evaluation is that the mechanical condition of the Main pump can be monitored satisfactorily by disregarding the single frequency component caused by the excitation at 4x Booster pump RPM. The four-vane impeller of the Booster pump generates the excitation force hydraulically. This small pressure pulsation force exists at the vane passing frequency (number of vanes times RPM) for all centrifugal pumps and is usually seen as a significant but not particularly troublesome component on the frequency spectrum for vibration measurements taken at the bearing housings. For the HPCI pump, this vane passing frequency is a problem because it coincides with a hydraulic standing wave resonance in the cross-over piping from the Booster pump to the Main pump when the machine is operating at the rated speed of 4000 RPM. There is an acoustic pressure standing wave pattern, at the 4x RPM frequency, whose wavelength in water is equal to an even fraction (1/4 or 1/2) of the dimensional length inside the cross-over pipe. This is the same principle on which an organ pipe generates a pure tone pneumatic pressure standing wave.

In addition, and exacerbating the vibration resonance condition, the Main pump pedestal experiences a horizontal structural primary rocking mode of the pump pedestal at this same frequency when the Main pump is operating at the rated speed of 4000 RPM. The vibration mode is the second fundamental rocking mode, which is a torsional or twisting mode where the two end bearings move 180 degrees out of phase horizontally. The result of these coincident acoustic and structural resonances is that the Main pump exhibits high vibration in the horizontal direction at the 4x Booster pump RPM frequency. This is solely due to the excitation from the Booster pump being amplified by the coincident resonances. This level of vibration at 4x Booster pump RPM would be seen on the Main pump bearing housings even if the Main pump was not actually running (which is not possible as both pumps are on the same drive train).

The resonant vibration condition at the 4000 RPM operating speed is not detrimental and will not prevent the HPCI pump from fulfilling its function. At the 134 Hz frequency of the resonant vibration on the Main pump, caused by the excitation at 4x Booster pump RPM, the actual displacement amplitude at 0.7 in/sec peak velocity amplitude is 0.0017 inches peak-to-peak. This displacement imposes negligible alternating stresses on the pump pedestal, housings, and connected piping. The peak-to-peak displacement is also less than the Main pump fluid film journal bearing clearances and would impose negligible loading to these bearings.

The purpose of the ASME OM Code for pump testing is to monitor pumps for degradation. The concept of vibration monitoring is to establish baseline values for vibration when the pump is known to be in good working condition, such as after a maintenance overhaul. From that reference point, trending is performed to monitor for degradation based on the ratio of subsequent vibration levels relative to the reference values. The OM Code also establishes absolute vibration level criteria for Alert (>0.325 in/sec) and Required Action (>0.7 in/sec). In doing so, it was recognized that absolute vibration level limits (as opposed to relative change or ratio limits) are not always quantitatively linked directly with pump physical condition and the following remarks are stated in the ASME OMa Code 1996:

<sup>&</sup>quot;Vibration measurements of pumps may be foundation, driver, and piping dependent. Therefore, if initial vibration readings are high and have no obvious relationship to the

pump, then vibration measurements should be taken at the driver, at the foundation, and on the piping and analyzed to ensure that the reference vibration measurements are representative of the pump and that the measured vibration levels will not prevent the pump from fulfilling its function. "

An important conclusion of the PNPS HPCI pump vibration evaluation is that the mechanical condition of the Main pump can be monitored satisfactorily by disregarding the single frequency component caused by the excitation at 4x Booster pump RPM. A single peak frequency component can be effectively isolated and deleted from a vibration spectrum using the mean-squared subtraction method, that is, the discrete component amplitude (in/sec peak) is squared and subtracted from the spectrum overall level squared, then the square root of that difference represents the overall vibration level that exists without the energy contributed by the deleted component. It has been found that when this method is used, the remaining vibration overall level is much more consistent, stable, and trendable.

This method of vibration level correction has been applied to historical spectrums. The 4x Booster pump RPM component was taken out of the calculation for the main pump overall vibration level. This data shows that when the 4x Booster pump RPM component is deleted from the Main pump vibration, the level is below the Required Action Range (> 0.7 in./sec) but still within the Alert Range (> 0.325 in./sec). It was also shown that the potential effects from the dynamic alignment of pump shaft couplings (at 2X Main pump RPM) can still be monitored effectively.

The vibration spectra derived from the NRC approved alternative test conducted in November 2005 conforms to the historical vibration spectra documented since 1994. Enclosure 1 provides the November 2005 test results and Enclosure 2 provides the historical tests results. Since the observed vibration spectra have not changed, no degradation in the established operational readiness of the HPCI pump has taken place. Also, the alternative test verifies the operational readiness of the HPCI pump in its as-built configuration as stipulated by ISTB 4.3(g) with corresponding footnote.

### Impact of Potential Modifications:

For the HPCI Main and Booster pumps, it has been determined that the vibration is foundation and piping dependent. To reduce the HPCI Main and Booster pump vibration down to levels that meet acceptable OM Code vibration criteria requires modifications to the HPCI pump, mounting components, foundation and/or cross-over (interconnecting) piping.

As suggested in a Byron Jackson Tech Note, this vibration may be improved by modifying the interconnecting piping and the Main pump mounting pedestal. The alternative modification changes the Booster pump impeller from four to five vanes to alter the forcing function of the standing wave resonance.

The proposed Byron Jackson modifications, other than replacing the Booster pump impeller, are generally very difficult to implement successfully. Altering the natural frequency of a large pump installation requires either considerable additions of stiffening components or substantial additions of mass. Often the results of such design changes are unsuccessful or unfavorable due to the variable speed operation requirements.

Modification of the HPCI Booster pump would require replacing the current four-vane impeller with an upgraded five-vane impeller. The impeller modification, although yielding predictable results, requires extensive work to the HPCI pump at a time when such a major rebuild of this pump is not otherwise necessary or desired. The expected result would be a modest decrease in the vibration caused on the Main pump at 4000 RPM, although the vibration would remain

above the 0.325 inch/sec Alert Range criteria. A small decrease in hydraulic performance is also expected when changing from a four to five-vane impeller. The proposed major modification would cost approximately \$500,000 without a compensating improvement in the pump vibration. Most HPCI pump vibration points would remain above the 0.325 in./sec Alert Criteria. Accordingly, the proposed modification would not achieve the underlying objective of performing the Code required testing without the need for Code relief.

PNPS has also concluded that none of the possible modifications that could be performed on the HPCI pump, mounting pedestal, or cross-over piping are necessary. This is primarily due to the nature of the HPCI pump service profile. The Byron Jackson Tech Note describes the following consideration in the Technical Discussion:

" Pumping systems in which the vane passing pressure pulsations form standing waves in the attached piping are not unusual, especially if the pumps have a variable speed driver. Standing waves are highly dependent upon water temperature. Thus, measured vibration amplitudes often vary from test to test. "

The HPCI pump service is such that the pump runs for short periods of time at highly variable speeds. The pump inservice testing at PNPS is performed with the pump operating at or close to its rated speed (4000 RPM) and flow conditions (4250 GPM) that are unique to PNPS. For this particular pump configuration, this pump speed corresponds to the point where the acoustic resonant vibration is typically most pronounced. In actual service for high pressure coolant injection to the reactor, the pump will operate at the speed that the flow controller requires to maintain reactor water level. The flow rate of 4250 GPM is the maximum makeup flow rate for which the HPCI System was intended to be capable of maintaining reactor water level. This flow rate is far in excess of the decay heat makeup water requirements for the reactor in the isolated condition in the absence of a major leak. The pump speed required is also dependent on reactor pressure with the required speed decreasing along with reactor pressure.

The same general HPCI pump configuration is used at other plants but often with different pump impellers, rated speeds and plant design flow rates. For these plants the vibration characteristics at the inservice testing points are markedly different for that reason. The vibration monitoring performed (including a frequency spectral review) to date under the IST program and the PNPS Pump Vibration Monitoring Program has shown that there has not been degradation of these HPCI pump components.

Inservice Testing can be successfully performed for the PNPS HPCI pump using the methods proposed in this relief request, along with monitoring and maintenance activities currently in practice. Any significant degradation of the HPCI pump components will be readily identified using the vibration spectral analysis methods and other preventive monitoring activities described in this relief request. Therefore, Entergy believes that the proposed alternative testing and monitoring for the PNPS HPCI pump will provide an acceptable level of quality and safety in accordance with 10 CFR 50.55 a(a)(3)(i).

## **ALTERNATE TESTING:**

To allow for practicable monitoring of vibration levels on the HPCI pump, alternate vibration acceptance criteria are necessary. A full spectrum review will be performed for all IST vibration points during each proposed comprehensive test, utilizing the following criteria.

The table below provides the acceptance criteria that are applied to the overall vibration level for the Main pump. The note explains that for the horizontal Main pump points, the discrete frequency component at 4x Booster pump RPM will be extracted from the overall value using the mean-squared subtraction. The two extracted discrete peaks (points P3H and P4H) will be

evaluated separately, and will have an Acceptance Range upper limit of 1.05Vr and Alert Range upper limit of 1.3Vr (where Vr equals the vibration reference overall value).

The table boxes in **bold italics** have values that have been modified from the OM Code vibration criteria. The **Alert vibration range of 1.5Vr to 6Vr** (in lieu of the OM Code range of 2.5Vr to 6Vr) has been applied as the modified OM vibration criteria. The absolute limiting upper Alert Values (i.e. 0.375, 0.450, 0.500, 0.550, and 0.600) are based upon existing pump reference values, and fall between the values of 1.25Vr and 1.5Vr. All of the modified Alert Values have been compared to historical pump vibration data.

The Table row for P8A is in compliance with the OM Code vibration criteria, and has been placed into this relief request for information only.

<u>Test</u> <u>Parameter</u>	Vibration Point	Acceptable Range	Alert Range	Required Action Range
Vv	Main pump** Horizontal Inboard (P3H)	≤ 1.5 V <sub>r</sub> but not > 0.550 in./sec	> 1.5 V, to 6 V, or > 0.550 to 0.70 in./sec	> 6 V <sub>r</sub> or > 0.70 in./sec
V <sub>v</sub>	Main pump** Horizontal Outboard (P4H)	≤ 1.5 V <sub>r</sub> but not > 0.600 in./sec	> 1.5 V <sub>r</sub> to 6 V <sub>r</sub> or > 0.600 to 0.70 in./sec	> 6 V <sub>r</sub> or > 0.70 in./sec
V <sub>v</sub>	Main pump Vertical Inboard (P3V)	≤ 1.5 V, but not > 0.450 in./sec	> 1.5 V <sub>r</sub> to 6 V <sub>r</sub> or > 0.450 to 0.70 in./sec	> 6 V <sub>r</sub> or > 0.70 in./sec
V <sub>v</sub>	Main pump Vertical Outboard (P4V)	≤ 1.5 V <sub>r</sub> but not > 0.375 in./sec	> 1.5 V <sub>r</sub> to 6 V <sub>r</sub> or > 0.375 to 0.70 in./sec	> 6 V <sub>r</sub> or > 0.70 in./sec
V <sub>v</sub>	Main pump Axial Inboard (P3A))	≤ 1.5 V <sub>r</sub> but not > 0.500 in./sec	> 1.5 V <sub>r</sub> to 6 V <sub>r</sub> or > 0.500 to 0.70 in./sec	> 6 V <sub>r</sub> or > 0.70 in./sec

MAIN PUMP\*\*

\*\*Note: For Main pump Horizontal vibration points P3H and P4H, a frequency spectrum analysis will be performed for each pump vibration operability test and the discrete peak at 4x Booster pump RPM will be extracted (using mean-squared subtraction method) from the vibration spectrum overall value. In addition, all other vibration spectrum discrete peaks (including the extracted discrete peak) will be evaluated during each test, and will have an Acceptable Range upper limit of 1.05 V<sub>r</sub> and an Alert Range upper limit 1.3 V<sub>r</sub>.

Test	Vibration Point	Acceptable Range	Alert Range	Required Action
Parameter				<u>Range</u>
V <sub>v</sub>	Booster pump	≤ 1.5 V <sub>r</sub>	> 1.5 V <sub>r</sub> to 6 V <sub>r</sub>	> 6 V <sub>r</sub>
	Horizontal	but not	or	or
	Inboard (P7H)	> 0.450 in./sec	> 0.450 to 0.70	> 0.70 in./sec
			in./sec	
V <sub>v</sub>	Booster pump	≤1.5 V <sub>r</sub>	> 1.5 V <sub>r</sub> to 6 V <sub>r</sub>	> 6 V <sub>r</sub>
	Horizontal	but not	or	or
	Outboard (P8H)	> 0.500 in./sec	> 0.500 to 0.70	> 0.70 in./sec
			in./sec	
V <sub>v</sub>	Booster pump	≤1.5 V <sub>r</sub>	> 1.5 V <sub>r</sub> to 6 V <sub>r</sub>	> 6 V <sub>r</sub>
	Vertical	but not	or	or
	Inboard (P7V)	> 0.400 in./sec	> 0.400 to 0.70	> 0.70 in./sec
			in./sec	
V <sub>v</sub>	Booster pump	≤ 1.5 V <sub>r</sub>	> 1.5 V, to 6 V,	> 6 V <sub>r</sub>
	Vertical	but not	or	or
	Outboard (P8V)	> 0.500 in./sec	> 0.500 to 0.70	> 0.70 in./sec
			in./sec	
V <sub>v</sub>	Booster pump	≤ 2.5 V <sub>r</sub>	$> 2.5 V_r$ to 6 $V_r$	> 6 V <sub>r</sub>
	Axial	but not	or	or
	Outboard (P8A)	> 0.325 in./sec	> 0.325 to 0.70	> 0.70 in./sec
			in./sec	

## **BOOSTER PUMP**

## **DURATION OF PROPOSED ALTERNATIVE**

The proposed alternative testing shall apply for the remainder of the 4<sup>th</sup> Inservice Testing Interval at Pilgrim.

## REFERENCES

- 1. NRC Letter, Pilgrim Nuclear Power Station- Entergy Relief Request PR-03 High Pressure Coolant Injection Pump (TAC NO. MB8773), dated August 29, 2005
- 2. Entergy Letter No. 02.05.042, Response to NRC Request for Additional Information Related to Pilgrim In-service Testing (IST) Relief Request PR-03 (TAC NO. MB8773), dated May 24, 2005
- 3. Entergy Letter No. 02.05.012, Pilgrim Fourth Ten-year In-Service Testing Program, IST relief Request PR-03, dated February 24, 2005

## ENCLOSURES

Enclosure 1: HPCI pump November 2005 Vibration Test Results (11 pages)

Enclosure 2: HPCI pump Configuration and Historical Vibration Test Results (66 pages)

## ENCLOSURE 1

## HPCI PUMP NOVEMBER 2005 VIBRATION TEST RESULTS (11 pages)

(Pilgrim Seeks Relief for P3H and P4H Points. Data for the remaining point is provided for information)

- 1. Relief Point P3H Data
- 2. Relief Point P4H Data
- 3. Point P3V Data
- 4. Point P3A Data
- 5. Point P4V Data
- 6. Point P7H Data
- 7. Point P7V Data
- 8. Point P8H Data
- 9. Point P8V Data
- 10. Point P8A Data





















Velocity in In/Sec



### ENCLOSURE 2

### HPCI PUMP CONFIGURATION AND HISTORICAL VIBRATION TEST RESULTS (Total 66 pages)

# (Pilgrim seeks Relief for P3H and P4H Points. Data for the remaining point is provided for information)

### HPCI Pump Layout

- 1. HPCI Pump Configuration
- 2. HPCI Pump Configuration
- 3. HPCI Pump Configuration
- 4. HPCI Pump Vibration Monitoring Program

### Relief Point P3H Data

5. P3H HPCI Vibration Spectrum Data, Nov. 24, 2004

6. P3H HPCI Vibration Spectrum Data, Aug. 24, 2004

- 7. P3H HPCI Vibration Spectrum Data, Dec. 17, 1997
- 8. P3H HPCI Vibration Spectrum Data, May 06, 1996
- 9. P3H HPCI Vibration Spectrum Data, Nov. 20, 1995
- 10. P3H HPCI Vibration Spectrum Data, May 25, 1994

### Relief Point P4H Data

P4H HPCI Vibration Spectrum Data, Nov. 24, 2004
P4H HPCI Vibration Spectrum Data, Aug. 24, 2004
P4H HPCI Vibration Spectrum Data, Dec. 17, 1997
P4H HPCI Vibration Spectrum Data, May 06, 1996
P4H HPCI Vibration Spectrum Data, Nov. 20, 1995
P4H HPCI Vibration Spectrum Data, May 25, 1994

#### Point P3V Data

17. P3V HPCI Vibration Spectrum Data, Nov. 24, 2004 18. P3V HPCI Vibration Spectrum Data, Aug. 24, 2004 19. P3V HPCI Vibration Spectrum Data, Dec. 17, 1997 20. P3V HPCI Vibration Spectrum Data, May 06, 1996 21. P3V HPCI Vibration Spectrum Data, Nov. 20, 1995 22. P3V HPCI Vibration Spectrum Data, May 25, 1994

### Point P3A Data

23. P3A HPCI Vibration Spectrum Data, Nov. 24, 2004 24. P3A HPCI Vibration Spectrum Data, Aug. 24, 2004 25. P3A HPCI Vibration Spectrum Data, Dec. 17, 1997 26. P3A HPCI Vibration Spectrum Data, May 06, 1996 27. P3A HPCI Vibration Spectrum Data, Nov. 20, 1995 28. P3A HPCI Vibration Spectrum Data, May 25, 1994

### Point P4V Data

29. P4V HPCI Vibration Spectrum Data, Nov. 24, 2004 30. P4V HPCI Vibration Spectrum Data, Aug. 24, 2004 31. P4V HPCI Vibration Spectrum Data, Dec. 17, 1997 32. P4V HPCI Vibration Spectrum Data, May 06, 1996 33. P4V HPCI Vibration Spectrum Data, Nov. 20, 1995 34. P4V HPCI Vibration Spectrum Data, May 25, 1994

### Point P7H Data

35. P7H HPCI Vibration Spectrum Data, Nov. 24, 2004 36. P7H HPCI Vibration Spectrum Data, Aug. 24, 2004 37. P7H HPCI Vibration Spectrum Data, Dec. 17, 1997 38. P7H HPCI Vibration Spectrum Data, May 06, 1996 39. P7H HPCI Vibration Spectrum Data, Nov. 20, 1995 40. P7H HPCI Vibration Spectrum Data, May 25, 1994

### Point P7V Data

41. P7V HPCI	Vibration	Spectrum	Data,	Nov. 24, 2004
42. P7V HPCI	Vibration	Spectrum	Data,	Aug. 24, 2004
43. P7V HPCI	Vibration	Spectrum	Data,	Dec. 17, 1997
44. P7V HPCI	Vibration	Spectrum	Data,	May 06, 1996
45. P7V HPCI	Vibration	Spectrum	Data,	Nov. 20, 1995
46. P7V HPCI	Vibration	Spectrum	Data,	May 25, 1994

### Point P8H Data

47. P8H HF	2CI Vibration Spectre	um Data, Nov. 24, 2004
48. P8H HF	CI Vibration Spectr	um Data, Aug. 24, 2004
49. P8H HF	CI Vibration Spectr	um Data, Dec. 17, 1997
50. P8H HF	CI Vibration Spectr	um Data, May 06, 1996
51. P8H HF	CI Vibration Spectr	um Data, Nov. 20, 1995
52. P8H HF	CI Vibration Spectr	um Data, May 25, 1994

### Point P8V Data

53. P8V HPCI Vibration Spectrum Data, Nov. 24, 2004 54. P8V HPCI Vibration Spectrum Data, Aug. 24, 2004 55. P8V HPCI Vibration Spectrum Data, Dec. 17, 1997 56. P8V HPCI Vibration Spectrum Data, May 06, 1996 57. P8V HPCI Vibration Spectrum Data, Nov. 20, 1995 58. P8V HPCI Vibration Spectrum Data, May 25, 1994

#### Point P8A Data

59. P8A HPCI Vibration Spectrum Data, Nov. 24, 2004 60. P8A HPCI Vibration Spectrum Data, Aug. 24, 2004 61. P8A HPCI Vibration Spectrum Data, Dec. 17, 1997 62. P8A HPCI Vibration Spectrum Data, July 31, 1996\* 63. P8A HPCI Vibration Spectrum Data, Nov. 20, 1995 64. P8A HPCI Vibration Spectrum Data, May 25, 1994

\*July 31, 1996 data is submitted since May 06, 1996 data is not available for point P8A.



# **HPCI** Pump Configuration



Main Pump

**Booster Pump** 

**HPCI** Pump Configuration



**HPCI Pump Configuration** 



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## HPCI Pump Vibration Monitoring Program

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Other points are monitored as part of Vibration Monitoring for Preventive Maintenance and Balance

## HPCI Data November 24, 2004



## HPCI Data August 24, 2004

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