

Detroit Edison



June 8, 2006
NRC-06-0043

U. S. Nuclear Regulatory Commission
Attention: Document Control Desk
Washington D C 20555-0001

- References: 1) Fermi 2
NRC Docket No. 50-341
NRC License No. NPF-43
- 2) Detroit Edison Letter NRC-06-0034, Transmittal of Cycle 12
Core Operating Limits Report, dated April 27, 2006

Subject: Transmittal of Cycle 12 Core Operating Limits Report, Revision 1

In accordance with Fermi 2 Technical Specification 5.6.5, Detroit Edison hereby submits a copy of the Core Operating Limits Report (COLR), Cycle 12, Revision 1. This COLR will be used during the Fermi 2 twelfth operating cycle.

Should you have any questions or require additional information, please contact me at (734) 586-5197.

Sincerely,

A handwritten signature in black ink, appearing to read "Ronald W. Gaston".

Ronald W. Gaston
Manager, Nuclear Licensing

Enclosure

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**ENCLOSURE TO
NRC-06-0043**

**CORE OPERATING LIMITS REPORT
[COLR]**

CYCLE 12

REVISION 1

FERMI 2

CORE OPERATING LIMITS REPORT

CYCLE 12

REVISION 1

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May 2006

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1.0 INTRODUCTION AND SUMMARY

This report provides the cycle specific plant operating limits, which are listed below, for Fermi 2, Cycle 12, as required by Technical Specification 5.6.5. The analytical methods used to determine these core operating limits are those previously reviewed and approved by the Nuclear Regulatory Commission in GESTAR II (Reference 9).

The cycle specific limits contained within this report are valid for the full range of the licensed operating domain.

| <u>OPERATING LIMIT</u> | <u>TECHNICAL SPECIFICATION</u> |
|------------------------|--------------------------------|
| APLHGR | 3.2.1 |
| MCPR | 3.2.2 |
| LHGR | 3.2.3 |
| RBM | 3.3.2.1 |
| BSP REGIONS | 3.3.1.1 |

| | | |
|--------|---|--|
| APLHGR | = | AVERAGE PLANAR LINEAR HEAT GENERATION RATE |
| MCPR | = | MINIMUM CRITICAL POWER RATIO |
| LHGR | = | LINEAR HEAT GENERATION RATE |
| RBM | = | ROD BLOCK MONITOR SETPOINTS |
| BSP | = | BACKUP STABILITY PROTECTION |

2.0 AVERAGE PLANAR LINEAR HEAT GENERATION RATE

| TECH SPEC IDENT | OPERATING LIMIT |
|-----------------|-----------------|
| 3.2.1 | APLHGR |

2.1 Definition

The AVERAGE PLANAR LINEAR HEAT GENERATION RATE (APLHGR) shall be applicable to a specific planar height and is equal to the sum of the LINEAR HEAT GENERATION RATEs (LHGRs) for all the fuel rods in the specified bundle at the specified height divided by the number of fuel rods in the fuel bundle at the height.

2.2 Determination of MAPLHGR Limit

The maximum APLHGR (MAPLHGR) limit is a function of reactor power, core flow, fuel type, and average planar exposure. The limit is developed, using NRC approved methodology described in References 9 and 10, to ensure gross cladding failure will not occur following a loss of coolant accident (LOCA). The MAPLHGR limit ensures that the peak clad temperature during a LOCA will not exceed the limits as specified in 10CFR50.46(b)(1) and that the fuel design analysis criteria defined in References 9 and 10 will be met.

The MAPLHGR limit during dual loop operation is calculated by the following equation:

$$MAPLHGR_{LIMIT} = \text{MIN} (MAPLHGR (P), MAPLHGR (F))$$

where:

$$MAPLHGR (P) = MAPFAC (P) \times MAPLHGR_{STD}$$

$$MAPLHGR (F) = MAPFAC (F) \times MAPLHGR_{STD}$$

Within four hours after entering single loop operation, the MAPLHGR limit is calculated by the following equation:

$$MAPLHGR_{LIMIT} = \text{MIN} (MAPLHGR (P), MAPLHGR (F), MAPLHGR (SLO))$$

where:

$$MAPLHGR (SLO) = 1.0 \times MAPLHGR_{STD}$$

The Single Loop multiplier is 1.0 since the offrated ARTS limits bound the single loop MAPLHGR limit.

MAPLHGR_{STD}, the standard MAPLHGR limit, is defined at a power of 3430 MWt and flow of 105 Mlbs/hr for each fuel type as a function of average planar exposure and is presented in Table 1. When hand calculations are required, MAPLHGR_{STD} shall be determined by interpolation from Table 1. MAPFAC(P), the core power-dependent MAPLHGR limit adjustment factor, shall be calculated by using Section 2.2.1. MAPFAC(F), the core flow-dependent MAPLHGR limit adjustment factor, shall be calculated by using Section 2.2.2.

**TABLE 1
FUEL TYPE-DEPENDENT
STANDARD MAPLHGR LIMITS**

| GE11 Exposure <u>GWD/ST</u> | GE11 MAPLHGR <u>KW/FT</u> | GE14 Exposure <u>GWD/ST</u> | GE14 MAPLHGR <u>KW/FT</u> |
|--------------------------------|------------------------------|--------------------------------|------------------------------|
| 0.0 | 13.42 | 0.0 | 12.82 |
| 19.72 | 13.42 | 19.13 | 12.82 |
| 27.22 | 12.29 | 57.61 | 8.00 |
| 63.50 | 8.90 | 63.50 | 5.00 |

Fuel Types

- | | |
|--|---|
| 17 = GE11-P9CUB380-11GZ-100T-146-T6-2542 | 1 = GE14-P10CNAB400-16GZ-100T-150-T6-2787 |
| 18 = GE11-P9CUB404-12GZ-100T-146-T6-2543 | 2 = GE14-P10CNAB399-16GZ-100T-150-T6-2788 |
| 19 = GE11-P9CUB408-12GZ-100T-146-T6-2604 | 3 = GE14-P10CNAB380-10G5/4G4-100T-150-T6-2868 |
| 20 = GE11-P9CUB380-12GZ-100T-146-T6-2605 | 4 = GE14-P10CNAB381-7G5/8G4-100T-150-T6-2869 |
| | 5 = GE14-P10CNAB381-7G6/8G4-100T-150-T6-2877 |

2.2.1 Calculation of MAPFAC(P)

The core power-dependent MAPLHGR limit adjustment factor, MAPFAC(P) (Reference 3), shall be calculated by one of the following equations:

For $0 \leq P < 25$:

No thermal limits monitoring is required.

For $25 \leq P < 30$:

With turbine bypass OPERABLE,

For core flow ≤ 50 Mlbs/hr,

$$MAPFAC(P) = 0.606 + 0.0038(P - 30)$$

For core flow > 50 Mlbs/hr,

$$MAPFAC(P) = 0.586 + 0.0038(P - 30)$$

With turbine bypass INOPERABLE,

For core flow ≤ 50 Mlbs/hr,

$$MAPFAC(P) = 0.490 + 0.0050(P - 30)$$

For core flow > 50 Mlbs/hr,

$$MAPFAC(P) = 0.438 + 0.0050(P - 30)$$

For $30 \leq P \leq 100$:

$$MAPFAC(P) = 1.0 + 0.005224(P - 100)$$

where: P = Core power (fraction of rated power times 100).

2.2.2 Calculation of MAPFAC(F)

The core flow-dependent MAPLHGR limit adjustment factor, MAPFAC(F) (Reference 3), shall be calculated by the following equation:

$$MAPFAC(F) = \text{MIN}(1.0, A_F \times \frac{WT}{100} + B_F)$$

where:

WT = Core flow (Mlbs/hr).

A_F = Given in Table 2.

B_F = Given in Table 2.

TABLE 2 FLOW-DEPENDENT MAPLHGR LIMIT COEFFICIENTS

| Maximum Core Flow* (Mlbs/hr) | A _F | B _F |
|---------------------------------|----------------|----------------|
| 110 | 0.6787 | 0.4358 |

*As limited by the Recirculation System MG Set mechanical scoop tube stop setting.

3.0 MINIMUM CRITICAL POWER RATIO

| TECH SPEC IDENT | OPERATING LIMIT |
|-----------------|-----------------|
| 3.2.2 | MCPR |

3.1 Definition

The MINIMUM CRITICAL POWER RATIO (MCPR) shall be the smallest Critical Power Ratio (CPR) that exists in the core for each type of fuel. The CPR is that power in the assembly that is calculated by application of the appropriate correlation(s) to cause some point in the assembly to experience boiling transition, divided by the actual assembly operating power.

3.2 Determination of Operating Limit MCPR

The required Operating Limit MCPR (OLMCPR) (Reference 2 and 8) at steady-state rated power and flow operating conditions is derived from the established fuel cladding integrity Safety Limit MCPR and an analysis of abnormal operational transients. To ensure that the Safety Limit MCPR is not exceeded during any anticipated abnormal operational transient, the most limiting transients have been analyzed to determine which event will cause the largest reduction in CPR. Three different core average exposure conditions are evaluated. The result is an Operating Limit MCPR which is a function of exposure and τ . τ is a measure of scram speed, and is defined in Section 3.3.2. Cycle 12 operating limits are based on the Dual Loop SLMCPR of 1.08.

The OLMCPR shall be calculated by the following equation:

$$OLMCPR = \text{MAX}(MCPR(P), MCPR(F))$$

MCPR(P), the core power-dependent MCPR operating limit, shall be calculated using Section 3.3.

MCPR(F), the core flow-dependent MCPR operating limit, shall be calculated using Section 3.4.

In case of **Single Loop Operation**, the Safety Limit MCPR (Reference 2 and 8) is increased to account for increased uncertainties in core flow measurement and TIP measurement, but OLMCPR does not change. This is due to the fact that sufficient conservatism exists in the power-dependent MCPR operating limits to allow for the increase in the SLMCPR without requiring a corresponding increase in OLMCPR.

3.3 Calculation of MCPR(P)

MCPR(P) the core power-dependent MCPR operating limit (Reference 3) shall be calculated by _____

3.3.1 Calculation of K_P

The core power-dependent MCPR operating limit adjustment factor, K_P (Reference 3), shall be calculated by using one of the following equations:

For $0 \leq P < 25$:

No thermal limits monitoring is required.

For $25 \leq P < 30$:

When turbine bypass is OPERABLE,

$$K_P = \frac{(K_{BYP} + (0.032 \times (30 - P)))}{OLMCPR_{100/105}}$$

where: $K_{BYP} = 2.16$ for core flow ≤ 50 Mlbs/hr
 $= 2.44$ for core flow > 50 Mlbs/hr

When turbine bypass is INOPERABLE,

$$K_P = \frac{(K_{BYP} + (0.076 \times (30 - P)))}{OLMCPR_{100/105}}$$

where: $K_{BYP} = 2.61$ for core flow ≤ 50 Mlbs/hr
 $= 3.34$ for core flow > 50 Mlbs/hr

For $30 \leq P < 45$:

$$K_P = 1.28 + (0.0134 \times (45 - P))$$

For $45 \leq P < 60$:

$$K_P = 1.15 + (0.00867 \times (60 - P))$$

For $60 \leq P \leq 100$:

$$K_P = 1.0 + (0.00375 \times (100 - P))$$

where: $P =$ Core power (fraction of rated power times 100).

3.3.2 Calculation of τ

The value of τ , which is a measure of the conformance of the actual control rod scram times to the assumed average control rod scram time in the reload licensing analysis, shall be calculated by using the following equation:

$$\tau = \frac{(\tau_{ave} - \tau_B)}{\tau_A - \tau_B}$$

where: $\tau_A = 1.096$ seconds

$$\tau_B = 0.830 + 0.019 \times 1.65 \sqrt{\frac{N_1}{\sum_{i=1}^n N_i}} \text{ seconds}$$

$$\tau_{ave} = \frac{\sum_{i=1}^n N_i \tau_i}{\sum_{i=1}^n N_i}$$

$n =$ number of surveillance tests performed to date in cycle,

$N_i =$ number of active control rods measured in the i^{th} surveillance test,

$\tau_i =$ average scram time to notch 36 of all rods measured in the i^{th} surveillance test, and

$N_1 =$ total number of active rods measured in the initial control rod scram time test for the cycle (Technical Specification Surveillance Requirement 3.1.4.4).

The value of τ shall be calculated and used to determine the applicable OLMCPR_{100/105} value from Table 3 within 72 hours of the conclusion of each control rod scram time surveillance test required by Technical Specification Surveillance Requirements 3.1.4.1, 3.1.4.2, and 3.1.4.4. Prior to performance of the initial scram time measurements for the cycle, a τ value of 1.0 shall be used to determine the applicable OLMCPR_{100/105} value from Table 3.

3.4 Calculation of MCPR(F)

MCPR(F), the core flow-dependent MCPR operating limit (Reference 3), shall be calculated by using the following equation:

$$MCPR(F) = \text{MAX}(1.21, (A_F \times \frac{WT}{100} + B_F))$$

where:

- WT = Core flow (Mlbs/hr).
- A_F = Given in Table 4.
- B_F = Given in Table 4.

TABLE 4 FLOW-DEPENDENT MCPR LIMIT COEFFICIENTS

| Maximum Core Flow* (Mlbs/hr) | A _F | B _F |
|---------------------------------|----------------|----------------|
| 110 | -0.601 | 1.743 |

*As limited by the Recirculation System MG Set mechanical scoop tube stop setting.

4.0 LINEAR HEAT GENERATION RATE

| TECH SPEC IDENT | OPERATING LIMIT |
|-----------------|-----------------|
| 3.2.3 | LHGR |

4.1 Definition

The LINEAR HEAT GENERATION RATE (LHGR) shall be the heat generation rate per unit length of fuel rod. It is the integral of the heat flux over the heat transfer area associated with the unit length. By maintaining the operating LHGR below the applicable LHGR limit, it is assured that all thermal-mechanical design bases and licensing limits for the fuel will be satisfied.

4.2 Determination of LHGR Limit

The maximum LHGR limit is a function of reactor power, core flow, fuel and rod type, and fuel rod nodal exposure. The limit is developed, using NRC approved methodology described in References 9 and 10, to ensure the cladding will not exceed its yield stress and that fuel thermal-mechanical design criteria will not be violated during any postulated transient events. The LHGR limit ensures the fuel mechanical design requirements as defined in References 1 and 8 will be met.

The LHGR limit during dual loop operation is calculated by the following equation:

$$LHGR_{LIMIT} = \text{MIN} (LHGR (P), LHGR (F))$$

where:

$$LHGR (P) = LHGRFAC (P) \times LHGR_{STD}$$

$$LHGR (F) = LHGRFAC (F) \times LHGR_{STD}$$

LHGR_{STD}, the standard LHGR limit, is defined at a power of 3430 MWt and flow of 105 Mlbs/hr for each fuel and rod type as a function of fuel rod nodal exposure and is presented in Table 5. Table 5 contains only the most limiting Gadolinia LHGR limit for the maximum allowed Gadolinia concentration of the applicable fuel product line. When hand calculations are required, LHGR_{STD} shall be determined by interpolation from Table 5. LHGRFAC(P), the core power-dependent LHGR limit adjustment factor, shall be calculated by using Section 4.2.1. LHGRFAC(F), the core flow-dependent LHGR limit adjustment factor, shall be calculated by using Section 4.2.2.

TABLE 5
STANDARD LHGR LIMITS FOR VARIOUS FUEL TYPES

| GE11 Uranium Only Fuel Rods | | GE11 Most Limiting Gadolinia Bearing Fuel Rods | |
|-----------------------------|--------------|---|--------------|
| Exposure | LHGR | Exposure | LHGR |
| <u>GWD/ST</u> | <u>KW/FT</u> | <u>GWD/ST</u> | <u>KW/FT</u> |
| 0.0 | 14.40 | 0.0 | 12.74 |
| 13.24 | 14.40 | 10.59 | 12.74 |
| 27.22 | 12.29 | 23.99 | 10.87 |
| 63.50 | 8.90 | 58.81 | 7.88 |

| GE14 Uranium Only Fuel Rods | | GE14 Most Limiting Gadolinia Bearing Fuel Rods | |
|-----------------------------|--------------|---|--------------|
| Exposure | LHGR | Exposure | LHGR |
| <u>GWD/ST</u> | <u>KW/FT</u> | <u>GWD/ST</u> | <u>KW/FT</u> |
| 0.0 | 13.40 | 0.0 | 12.26 |
| 14.51 | 13.40 | 12.28 | 12.26 |
| 57.61 | 8.00 | 55.00 | 7.32 |
| 63.50 | 5.00 | 60.84 | 4.57 |

Fuel Types

- | | |
|--|---|
| 17 = GE11-P9CUB380-11GZ-100T-146-T6-2542 | 1 = GE14-P10CNAB400-16GZ-100T-150-T6-2787 |
| 18 = GE11-P9CUB404-12GZ-100T-146-T6-2543 | 2 = GE14-P10CNAB399-16GZ-100T-150-T6-2788 |
| 19 = GE11-P9CUB408-12GZ-100T-146-T6-2604 | 3 = GE14-P10CNAB380-10G5/4G4-100T-150-T6-2868 |
| 20 = GE11-P9CUB380-12GZ-100T-146-T6-2605 | 4 = GE14-P10CNAB381-7G5/8G4-100T-150-T6-2869 |
| | 5 = GE14-P10CNAB381-7G6/8G4-100T-150-T6-2877 |

4.2.1 Calculation of LHGRFAC(P)

The core power-dependent LHGR limit adjustment factor, LHGRFAC(P) (Reference 3), shall be calculated by one of the following equations:

For $0 \leq P < 25$:

No thermal limits monitoring is required.

For $25 \leq P < 30$:

With turbine bypass OPERABLE,

For core flow ≤ 50 Mlbs/hr,

$$\text{LHGRFAC}(P) = 0.606 + 0.0038(P - 30)$$

For core flow > 50 Mlbs/hr,

$$\text{LHGRFAC}(P) = 0.586 + 0.0038(P - 30)$$

With turbine bypass INOPERABLE,

For core flow ≤ 50 Mlbs/hr,

$$\text{LHGRFAC}(P) = 0.490 + 0.0050(P - 30)$$

For core flow > 50 Mlbs/hr,

$$\text{LHGRFAC}(P) = 0.438 + 0.0050(P - 30)$$

For $30 \leq P \leq 100$:

$$\text{LHGRFAC}(P) = 1.0 + 0.005224(P - 100)$$

where: P = Core power (fraction of rated power times 100).

4.2.2 Calculation of LHGRFAC(F)

The core flow-dependent LHGR limit adjustment factor, LHGRFAC(F) (Reference 3), shall be calculated by the following equation:

$$LHGRFAC(F) = \text{MIN}(1.0, A_F \times \frac{WT}{100} + B_F)$$

where:

- WT = Core flow (Mlbs/hr).
- A_F = Given in Table 6.
- B_F = Given in Table 6.

TABLE 6 FLOW-DEPENDENT LHGR LIMIT COEFFICIENTS

| Maximum Core Flow* (Mlbs/hr) | A _F | B _F |
|---------------------------------|----------------|----------------|
| 110 | 0.6787 | 0.4358 |

*As limited by the Recirculation System MG Set mechanical scoop tube stop setting.

5.0 CONTROL ROD BLOCK INSTRUMENTATION

| TECH SPEC IDENT | SETPOINT |
|-----------------|----------|
| 3.3.2.1 | RBM |

5.1 Definition

The nominal trip setpoints and allowable values of the control rod withdrawal block instrumentation are shown in Table 7. These values are consistent with the bases of the APRM Rod Block Technical Specification Improvement Program (ARTS) and the MCPR operating limits. (References 2, 6, 7, 8, & 16).

TABLE 7 CONTROL ROD BLOCK INSTRUMENTATION SETPOINTS WITH FILTER

| Setpoint | Trip Setpoint | Allowable Value |
|----------|---------------|-----------------|
| LPSP | 27.0 | 28.4 |
| IPSP | 62.0 | 63.4 |
| HPSP | 82.0 | 83.4 |
| LTSP | 117.0 | 118.9 |
| ITSP | 112.2 | 114.1 |
| HTSP | 107.2 | 109.1 |
| DTSP | 94.0 | 92.3 |

where:

- LPSP Low power setpoint; Rod Block Monitor (RBM) System trip automatically bypassed below this level
- IPSP Intermediate power setpoint
- HPSP High power setpoint
- LTSP Low trip setpoint
- ITSP Intermediate trip setpoint
- HTSP High trip setpoint
- DTSP Downscale trip setpoint

6.0 BACKUP STABILITY PROTECTION REGIONS

| | |
|--|--|
| TECH SPEC REFERENCE 3.3.1.1 Action Condition J | OPERATING LIMIT Alternate method to detect and suppress thermal hydraulic instability oscillations |
| TRM REFERENCE 3.4.1.1 | OPERATING LIMIT Scram, Exit, and Stability Awareness Regions |

6.1 Definition

The Backup Stability Protection (BSP) Regions are an integral part of the Tech Spec required alternative method to detect and suppress thermal hydraulic instability oscillations in that they identify areas of the power/flow map where there is an increased probability that the reactor core could experience a thermal hydraulic instability. Regions are identified (refer to Table 8 and Figure 1) that are either excluded from planned entry (Scram Region), or where specific actions are required to be taken to immediately leave the region (Exit Region). A region is also identified where operation is allowed provided that additional monitoring is performed to verify that the reactor core is not exhibiting signs of core thermal hydraulic instability (Stability Awareness Region). (Reference 5 and 8)

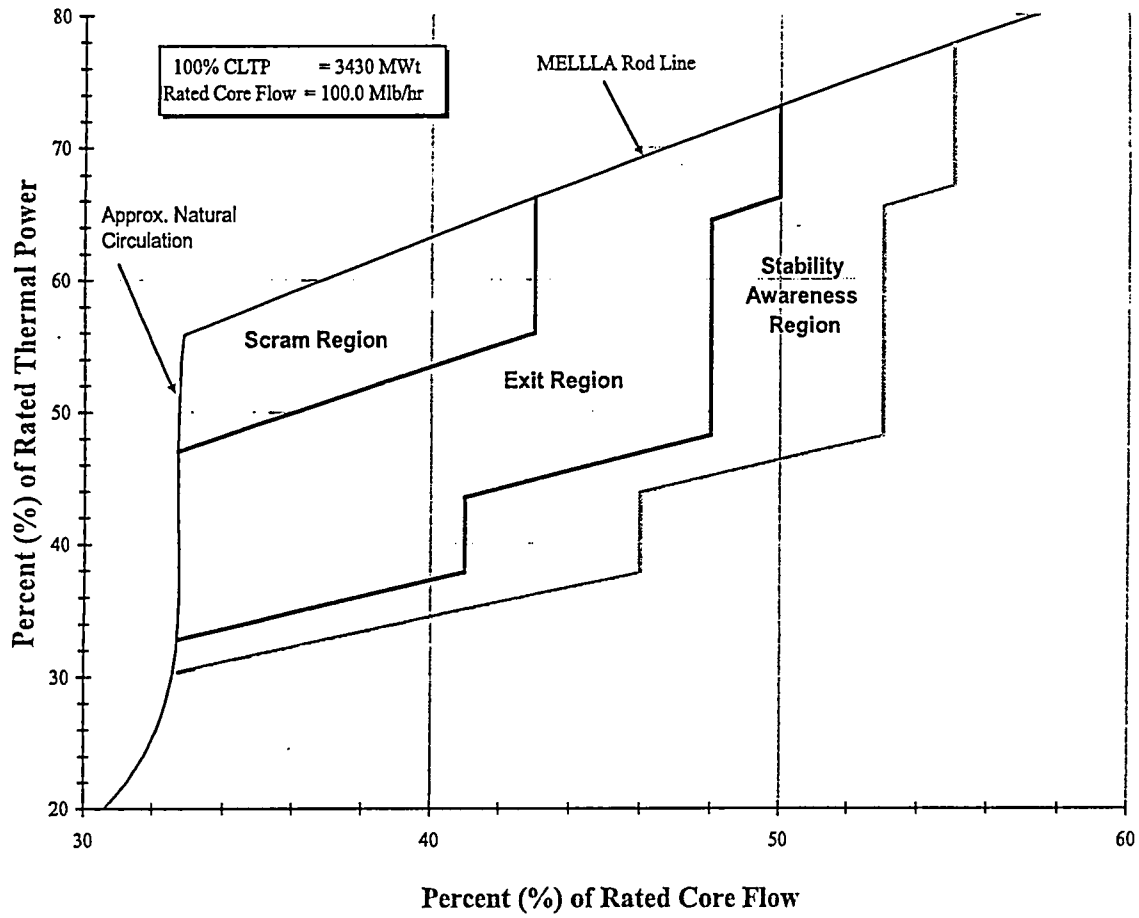
The boundaries of these regions are established on a cycle specific basis based upon core decay ratio calculations performed using NRC approved methodology. The Cycle 12 regions are valid to a cycle exposure of 12,600 MWd/st. (Reference 2 and 8)

These regions are only applicable when the Upscale Trip function of the Oscillation Power Range Monitoring System (OPRM) is inoperable. It must be noted that the Cycle 12 region boundaries defined in Table 8 and illustrated in Figure 1 are not applicable to operation with Feedwater Heaters Out-Of-Service (FWHOOS) or with Final Feedwater Temperature Reduction (FFWTR).

TABLE 8 BSP REGION DESCRIPTIONS

| | |
|-----------------------------|----------------------------------|
| Scram Region: | > 96% Rod Line, < 43% Core Flow |
| Exit Region: | > 67% Rod Line, < 41% Core Flow |
| Not in Scram Region -and- | > 77% Rod Line, < 48% Core Flow |
| Stability Awareness Region | > 103% Rod Line, < 50% Core Flow |
| Not in Scram or Exit Region | > 62% Rod Line, < 46% Core Flow |
| | > 72% Rod Line, < 53% Core Flow |
| | > 98% Rod Line, < 55% Core Flow |

FIGURE 1 - BSP REGIONS FOR NOMINAL FEEDWATER TEMPERATURE



7.0 REFERENCES

7.1 SOURCE REFERENCES

1. "Fuel Bundle Information Report for Enrico Fermi 2 Reload 11 Cycle 12," Global Nuclear Fuel, 0000-0038-3146-FIBR, Revision 0, January 2006 (LHGR Limits)
2. "Supplemental Reload Licensing Report for Enrico Fermi 2 Reload 11 Cycle 12," Global Nuclear Fuel, 0000-0038-3146-SRLR, Revision 0, January 2006 (MAPLHGR Limits, SLO Multiplier, MCPR Limits, SLMCPR)
3. "GE14 Fuel Cycle-Independent Analyses for Fermi Unit 2", GE-NE-0000-0025-3282-00 dated November 2004 (ARTS Limits)
4. Letter from Greg Porter to B. L. Myers, "Scram Times for Improved Tech Specs." GP-99014, October 22, 1999 containing DRF A12-00038-3, Vol. 4 information from G. A. Watford, GE, to Distribution, Subject: Scram Times versus Notch Position (TAU Calculation)
5. Evaluation Report, "BSP Stability Evaluation for Fermi 2 Cycle 12," GENE-0000-0048-1142-R0, January 2006 (BSP Limits)
6. CSCCD-C51 K622/C51 R809C Revision 2, "Programming for Rod Block Monitor (RBM-A) PIS # C51K622 and Operator Display Assembly (ODA) PIS # C51R809C" (RBM A Setpoints)
7. CSCCD-C51 K623/C51 R809D Revision 2, "Programming for Rod Block Monitor (RBM-B) PIS # C51K623 and Operator Display Assembly (ODA) PIS # C51R809D" (RBM B Setpoints)
8. "Fermi Cycle 12B GESTAR II Letter and Stability Report" letter FRL-DTE-KH1-06-012 from F.R. Lindquist, GNF, to P.R. Kiel, DECo, dated May 24, 2006

7.2 BASIS REFERENCES

9. "General Electric Standard Application for Reactor Fuel (GESTAR II)," NEDE-24011-P-A, Revision 14 as amended by Amendment 25
10. "The GESTR-LOCA and SAFER Models for the Evaluation of the Loss-of-Coolant Accident - SAFER/GESTR Application Methodology," NEDE 23785-1-PA, Revision 1, October 1984
11. "Fermi-2 SAFER/GESTR-LOCA, Loss-of-Coolant Accident Analysis," NEDC-31982P, July 1991, and Errata and Addenda No. 1, April 1992
12. "DTE Energy Enrico Fermi 2 SAFER/GESTR Loss of Coolant Accident Analysis for GE14 Fuel" GE-NE-0000-0030-6565 Revision 0 dated September 2004
13. "DTE Energy Enrico Fermi 2 SAFER/GESTR Loss of Coolant Accident Analysis for GE11 Fuel" GE-NE-0000-0047-1716 Revision 0 dated December 2005

7.2 BASIS REFERENCES

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15. Letter from J. F. Stang to W. S. Orser, "Amendment No. 53 to Facility Operating License No. NPF-43: (TAC No. 69074)," July 27, 1990
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