

# An Abstracted Model for Estimating Temperature and Relative Humidity in the Potential Repository at Yucca Mountain

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# Outline

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- Objective
- Background
- Model Abstraction
- Sample Results
- Conclusions

# Objective

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- Assess temperature and relative humidity at waste package surfaces in a potential high-level waste repository
- Account for parametric uncertainties
- Assess effects of drift-degradation on waste package surface temperature

# Background

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- Heat is generated by the radioactive decay of spent nuclear fuel disposed in waste packages emplaced in underground drifts
- Increased temperatures will potentially affect:
  - Distribution of water in the near-field
  - Initiation of localized corrosion
  - Pore water chemistry
  - Radioactive waste dissolution
  - Mechanical properties of rocks
  - Enhancement of microbial processes

# Model Abstraction

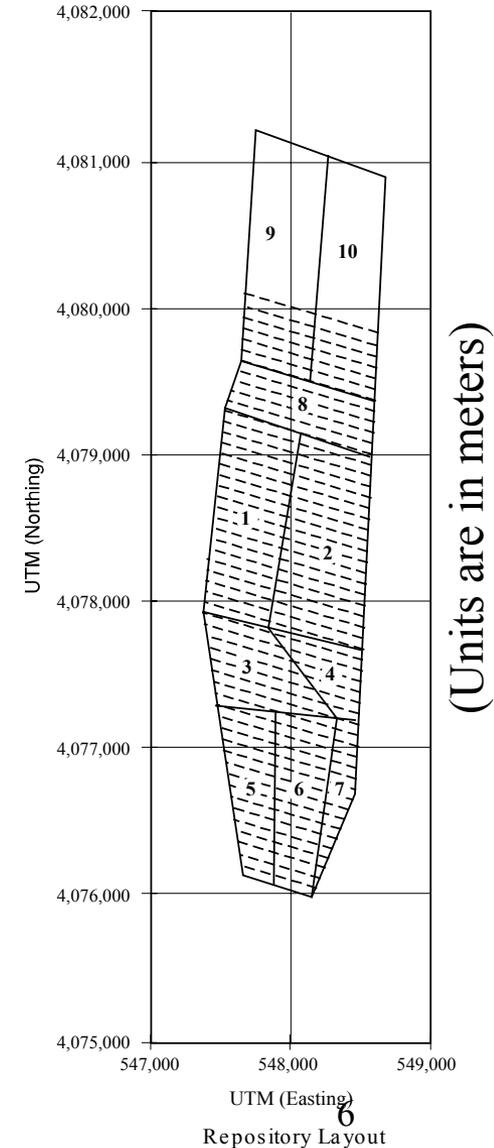
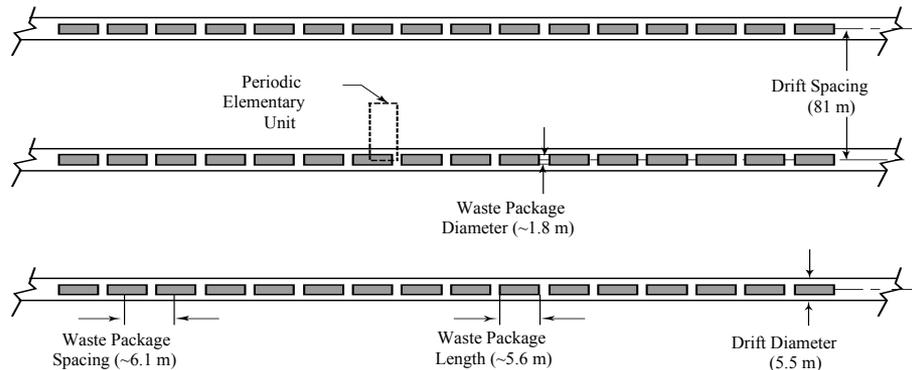
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## Abstracted model

- Needed because estimating temperatures in a probabilistic framework may require a large number of computer runs
- Needs to capture significant features, events and processes
- Usually requires uncoupling of the thermal and hydrological processes

# Abstracted Model - Scales

- Heat transfer model consists of two parts:
  - Mountain scale
  - Drift scale
- Temperature is estimated at the drift wall at the center of each subarea
- Temperatures and relative humidity are estimated at the waste package surface



# Abstracted Model - Mountain Scale

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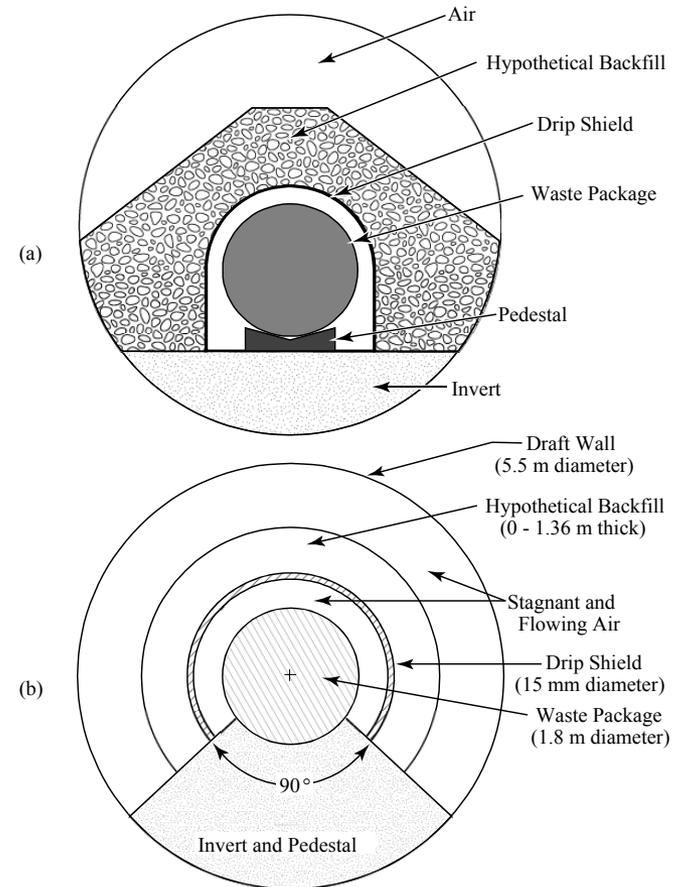
- Estimates the repository-horizon rock temperature
  - Center of each subarea
  - At the drift wall
- Semi-analytic transient heat conduction model
- Drifts are represented as heat sources
- Assumptions
  - Uniform thermal properties and uniform heat loading at the repository level
  - Two-dimensional planar sources to represent the heat output in each drift at the repository level
  - Drifts are considered as heat sources though the model permits considering each waste package as a heat source
  - The ground surface is at a constant temperature and is not affected by climate change
  - No sharp increase in temperature along the drift

# Abstracted Model - Drift Scale

- Estimate the waste package surface temperature from the rock temperature
- Use quasi-steady state assumption
- Represent in-drift heat transfer using a thermal network model that incorporates the details of the drift (drip shield, invert, air gaps, and potential backfill)
- Include heat transfer modes of conduction, convection, and radiation

$$Q_{wp} = G_{tot} (T_{wp} - T_{rock})$$

$$G_{tot} = G_{cond, floor} + \left[ \frac{1}{G_{rad1} + G_{conv1}} + \frac{1}{G_{cond, bdfs}} + \frac{1}{G_{rad2} + G_{conv2}} \right]^{-1}$$



# Abstracted Model- Drift Scale (continued)

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- Relative humidity is defined here as the ratio of the saturated vapor pressure at drift wall to the saturated vapor pressure at the waste package surface
- Saturated vapor pressure is computed using the standard thermodynamic equation relating vapor pressure to temperature

$$RH = \frac{P_V \left[ \min(T_b, T_{rock}) \right]}{P_V(T_{wp})}$$

$P_V$	—	vapor pressure as a function of temperature [Pa]
$\min(T_b, T_{rock})$	—	minimum of $T_b$ or $T_{rock}$
$T_b$	—	boiling point temperature
$T_{rock}$	—	drift wall temperature [K]
$T_{wp}$	—	waste package temperature [K]

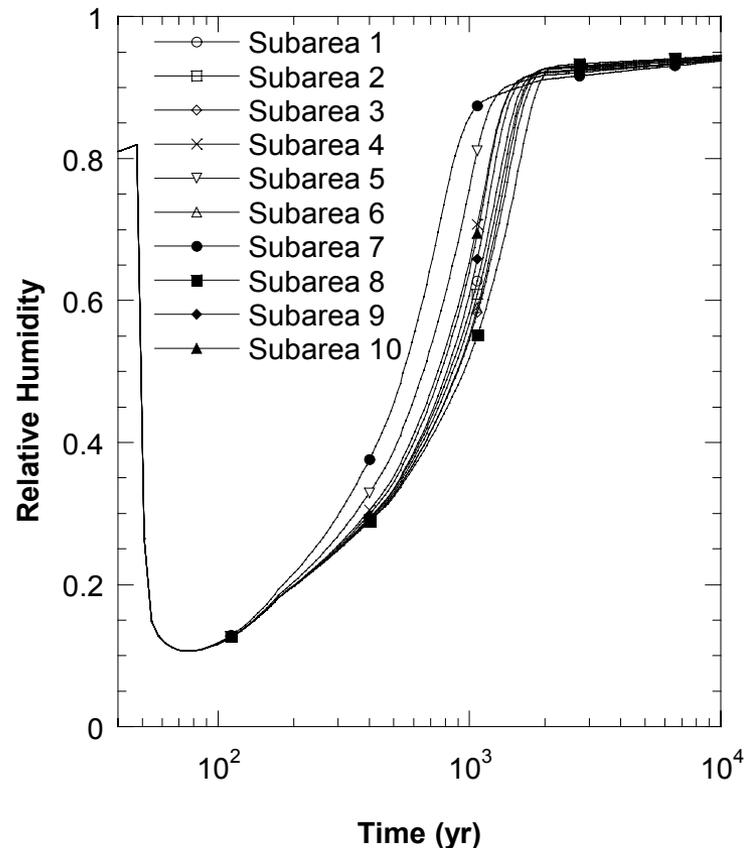
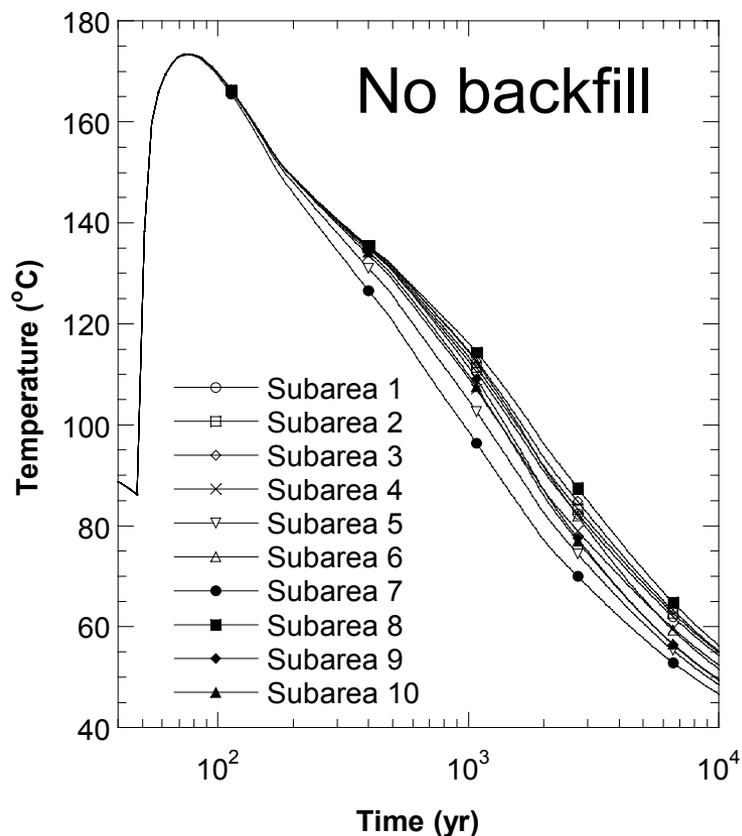
# Parameters for Determining Repository Scale and Drift-scale Heat Transfer

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Parameter	Value
Emplacement drift spacing	81 m
Waste package spacing along emplacement drift	6.14 m
Total waste emplaced in repository	70,040 MTU
Waste package payload	7.89 MTU
Number of equivalent WPs	8,877
Age of waste	26 yr
Ambient repository temperature	20 °C
Mass density of Yucca Mountain rock	2,580 kg/m <sup>3</sup>
Specific heat of Yucca Mountain rock	840 J/(kg-K)
Thermal conductivity of Yucca Mountain rock (sampled)	1.34-1.75 W/(m-°C)
Emissivity of drift wall	0.8
Emissivity of drip shield	0.63
Emissivity of WP	0.87
Thermal conductivity of floor	0.6 W/(m-°C)
Effective thermal conductivity (with natural convection)	0.9 W/(m-°C)
Factor for ventilation heat losses, $f_v$	0.70
Time of repository closure	50 yr
Effective thermal conductivity of the hypothetical backfill	0.27 W/(m-°C)

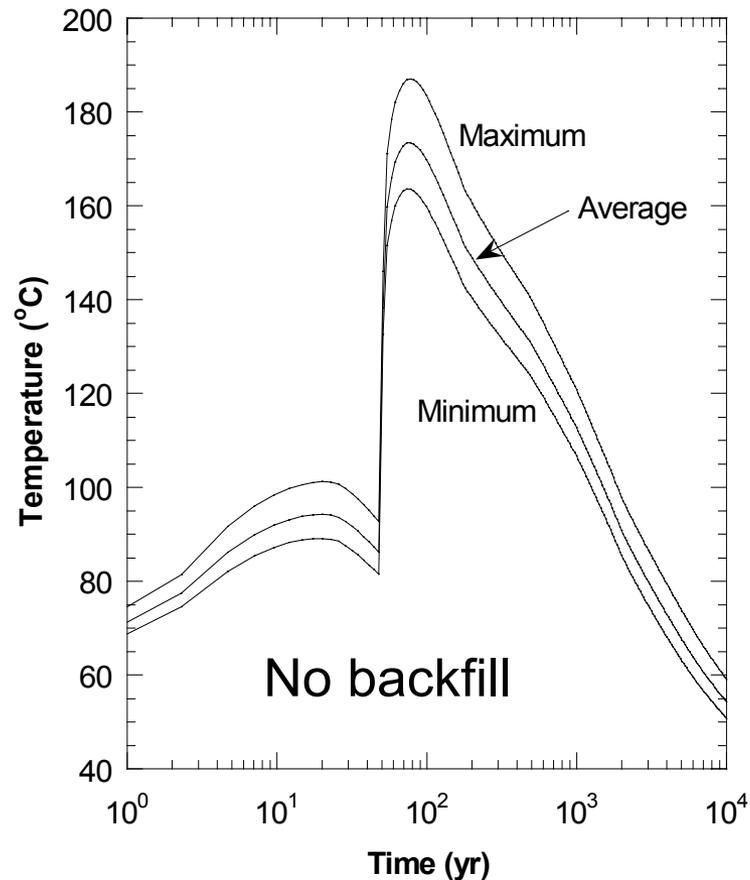
# Example Results

Subarea-to-subarea variation in waste package surface temperature and relative humidity (averaged for 350 Monte Carlo realizations for each subarea)



# Example Results (continued)

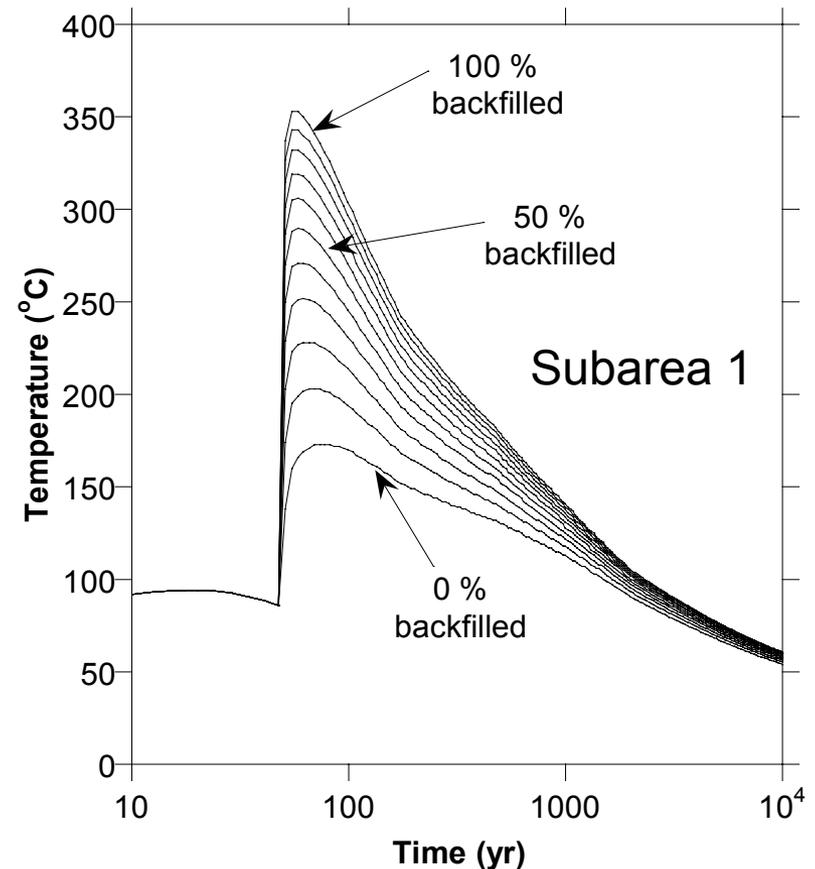
Maximum, minimum, and average waste package surface temperatures in subarea 1 from 350 Monte Carlo realizations



# Example Results (continued)

- Parameter Values
  - Maximum hypothetical thickness: 100 percent backfilled is 1.36 m (the radial distance between the outer wall of the drip shield and the drift wall)
  - Backfill thickness is constant with time
  - All other parameters set to their mean values
- For the 100 percent backfill case, a peak temperature of 353 °C occurs at 54.5 years.

With a hypothetical backfill



# Conclusions

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- Based on an abstracted model for estimating temperatures in a probabilistic system model requiring multiple Monte Carlo realizations.
  - The basecase (i.e., no backfill) waste package temperature near the center of the potential repository is approximately 165 °C on an average.
  - The waste package temperature remains above boiling for nearly 1,000 years even without the hypothetical backfill.

# Conclusions (continued)

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- The presence of a hypothetical backfill results in the peak waste package temperature for the fully backfilled condition approximately double that for the no-backfill condition.
- The time span for which the estimated temperature remains above boiling is much longer than in the no-backfill case.
- Future work will involve
  - A more accurate analysis of backfill on waste package temperature to include natural backfilling
  - Incorporation of cold-trap effect into the abstracted model if detailed calculations show it will have a significant influence on relative humidity along the drifts