

# ***Radioactivity Releases From PBMR Fuel***

**Stanley Ritterbusch**



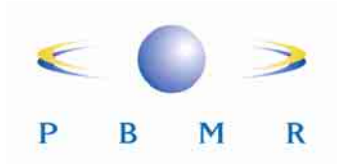
## ***Presentation Contents***

- **Overview of German experience**
  - Manufacturing and testing experience
  - Comparison of PBMR operating conditions to German data
  - Analysis of German data applicable to PBMR
  - Fuel failure fraction vs. temperature correlation
- **Method of predicting releases of radioactive fission products from the fuel for an accident**
  - Fuel burn-up accrued during normal operation
  - Fuel temperature during transients -- failure fraction
  - Fission product release from fuel spheres

- **Manufacturing**
- **Material test reactors**
  - Phase 1 – irradiation and heat-up tests that would be applicable to a variety of reactor designs.
  - Phase 2 – irradiation tests aimed at the HTR-Modul reactor design.
- **AVR test reactor**
  - Fuel design: GLE 4/2
  - Irradiation under in-reactor conditions
  - Accident simulation heat-up



**AVR (1967-88)**  
**15 MWe**



## ***Overview of Sources of Release Data***

- **Releases from PBMR fuel include contributions from**
  - Manufacturing deficiencies
  - Normal operation irradiation
  - Heat-up tests (simulating transients and accidents)



## ***Manufacturing Experience***

- **Post-1985 manufacturing –fuel design and manufacturing process was well-established**
- **Burn-leach tests on 528,200 fresh-fuel coated particles measured the quantity of fissionable isotopes not within intact particles**
  - Detects contamination and defective particles
  - Converted to equivalent “failed” particles
- **Results:**
  - Six equivalent failed particles
  - Nominal, calculated failure fraction:  $1 \times 10^{-5}$
  - 95% one-sided upper limit failure fraction:  $3 \times 10^{-5}$



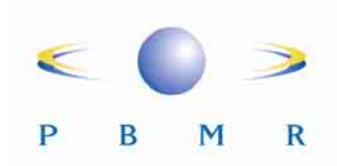
## ***German Test Envelope – Normal Operation***

Phase	Temperature (°C)	Burn-up (%FIMA)	Fast Neutron Dose $E > 0.1$ MeV ( $\times 10^{25} \text{ m}^{-2}$ )	Duration (EFPD)
1	880/1320	7.2/15.3	0.1/8.0	232/682
2	903/1140	7.81/10.88	3.2/5.9	565/634

**Phase 1: 211,936 coated particles**

**Phase 2: 145,320 coated particles**

**Total: 357,256 coated particles  
simulating normal operation irradiation**



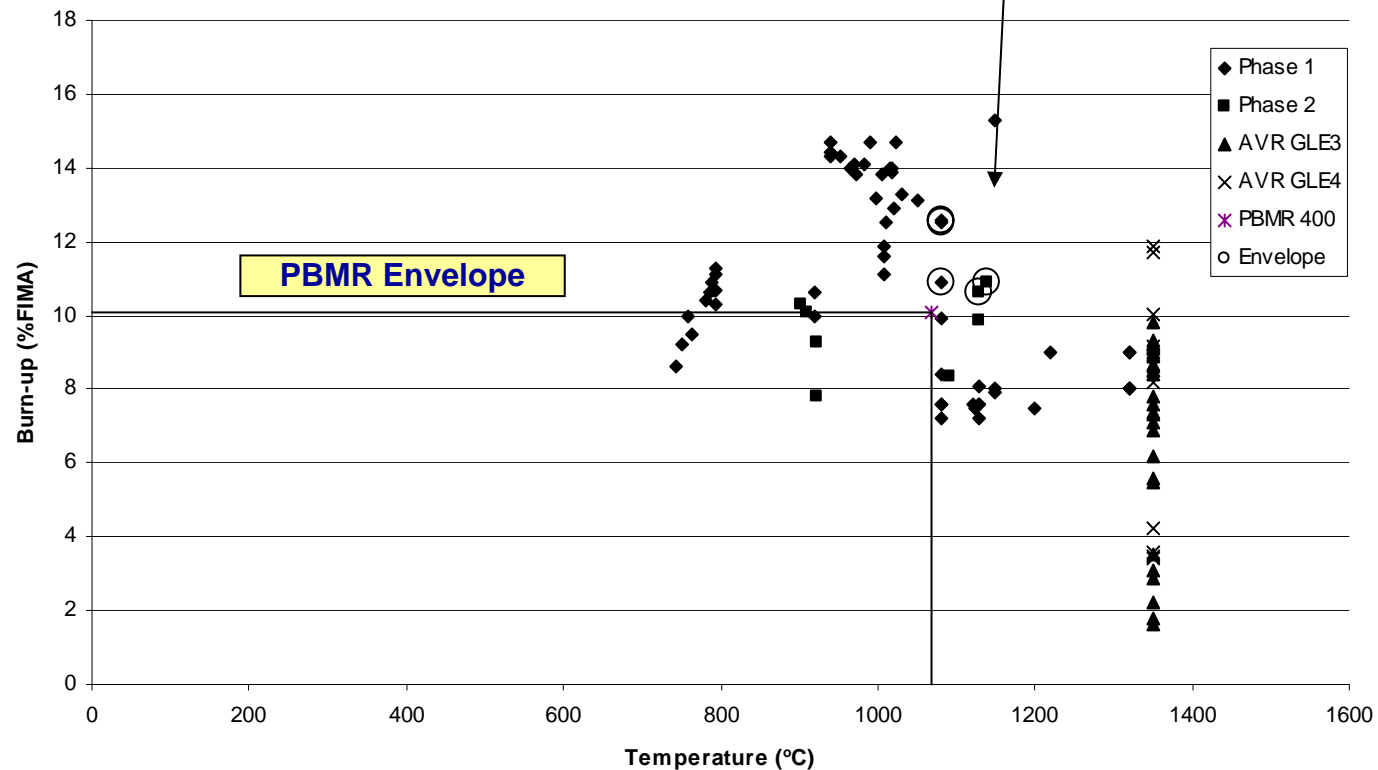
## ***PBMR Nominal Operation Envelope***

- **Temperature 1068°C**
- **Burn-up 10.1% FIMA (maximum)**
- **Fast Neutron Dose  $2.72 \times 10^{21} \text{ cm}^{-2}$**
- **Fuel Sphere Power 2.76 kW**

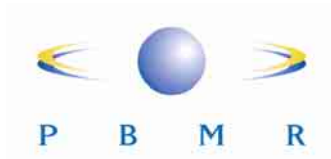
**Data may change slightly as analyses are finalized.**

# Operating Envelope Comparison

Circled data envelope PBMR conditions simultaneously.

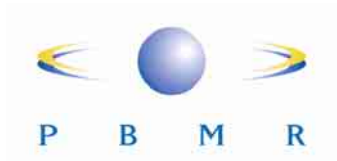






## ***Empirical Correlation***

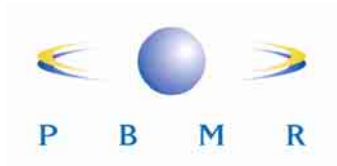
- **Fuel failure fraction vs. temperature**
- **Full range of temperatures:**
  - Normal operation (800°C – 1200°C)
  - Transients and accidents (1200°C – 1800°C)
- **The number of “failed” particles is not counted/measured directly during a test**
  - Number of “failed” coated particles is deduced from the release-to-birth ratio observed for a nuclide during tests
- **Correlation covers releases during**
  - Normal operation irradiation



# ***Sources of Radioactivity Releases***

- **Normal operation**

- Fission product release from coated particles damaged during manufacture
- Fission reactions in enriched uranium contamination on surface of OPyC layer
- Fission reactions in trace uranium and thorium contamination in natural graphite matrix material
- Migration of fission products through coated particle layers



## ***Sources of Radioactivity Releases ...***

- **Transients and accident heat-ups**

- Fission product release from coated particles damaged during manufacture
- Fission product release from coated particles that fail (e.g., opening of a crack) due to higher temperatures
- Migration of fission products through coated particle layers due to higher temperatures



## ***German Irradiation Data Representative of PBMR Conditions***

<b>Test</b>	<b>Sample Number</b>	<b>Irradiation Time (efpd)</b>	<b>Centre Temperature (°C)</b>	<b>Burn-up (%FIMA)</b>	<b>Fast Neutron Dose E&gt;0.1 MeV (x 10<sup>25</sup> m<sup>-2</sup>)</b>	<b>Number of Coated Particles</b>
HFR-P4	3	351	1010-1082	9.9-14.7	5.5-8.0	19 572
HFR-K3	4	359	1220	9.0	4.9	16 400
HFR-K6	2		1130	10.64	4.6	14 580
	3		1140	10.88	4.8	14 580
	4		1130	9.89	4.5	14 580
<b>Total Number of Coated Particles in selected MTR Tests</b>						<b>79712</b>

**No failures observed during irradiation**



## ***Prediction of Normal Operation “Failures”***

- **One-sided, binomial statistical analysis performed for “no observed failures”**

<b>Confidence Level</b>	<b>Failure Fraction</b>
50%	$8.70 \times 10^{-6}$
95%	$3.76 \times 10^{-5}$

- **Core contains a mix of new and irradiated fuel**
- **Therefore, failure fraction for core-average burn-up is taken conservatively as 50% of that for the fully irradiated fuel spheres**



## ***Total Failure Fraction for Normal Operation***

- **Total is combination of “failures” due to manufacturing and irradiation.**

<b>Confidence Level</b>	<b>Failure Fraction Due to Manufacturing Deficiencies</b>	<b>Core Average Failure Fraction Due to Irradiation</b>	<b>Total Failure Fraction During Irradiation</b>
<b>Nominal</b>	<b>1.0E-05</b>	<b>4.35E-06</b>	<b>1.44E-05</b>
<b>95%</b>	<b>3.0E-05</b>	<b>1.88E-05</b>	<b>4.88E-05</b>

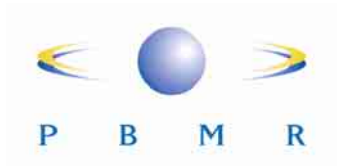
50% of values on previous slide



## ***Design Failure Fraction Specification for Normal Operations***

- For conservatism, the German fuel specification imposed a “free” uranium fraction of  $6 \times 10^{-5}$  as a design limit on fuel sphere manufacturing lots. The same lot limit is used by PBMR.
- For the “design” failure fraction, the predicted core-average failure fraction was based on a conservative 97.5% confidence level for fully irradiated fuel.

<b>Confidence Level</b>	<b>Failure Fraction Due to Irradiation of Manufacturing Deficiencies</b>	<b>Average Core Failure Fraction Due to Irradiation</b>	<b>Total Failure Fraction During Irradiation</b>
<b>Design</b>	<b>6.0E-05</b>	<b>4.63E-05</b>	<b>1.06E-04</b>

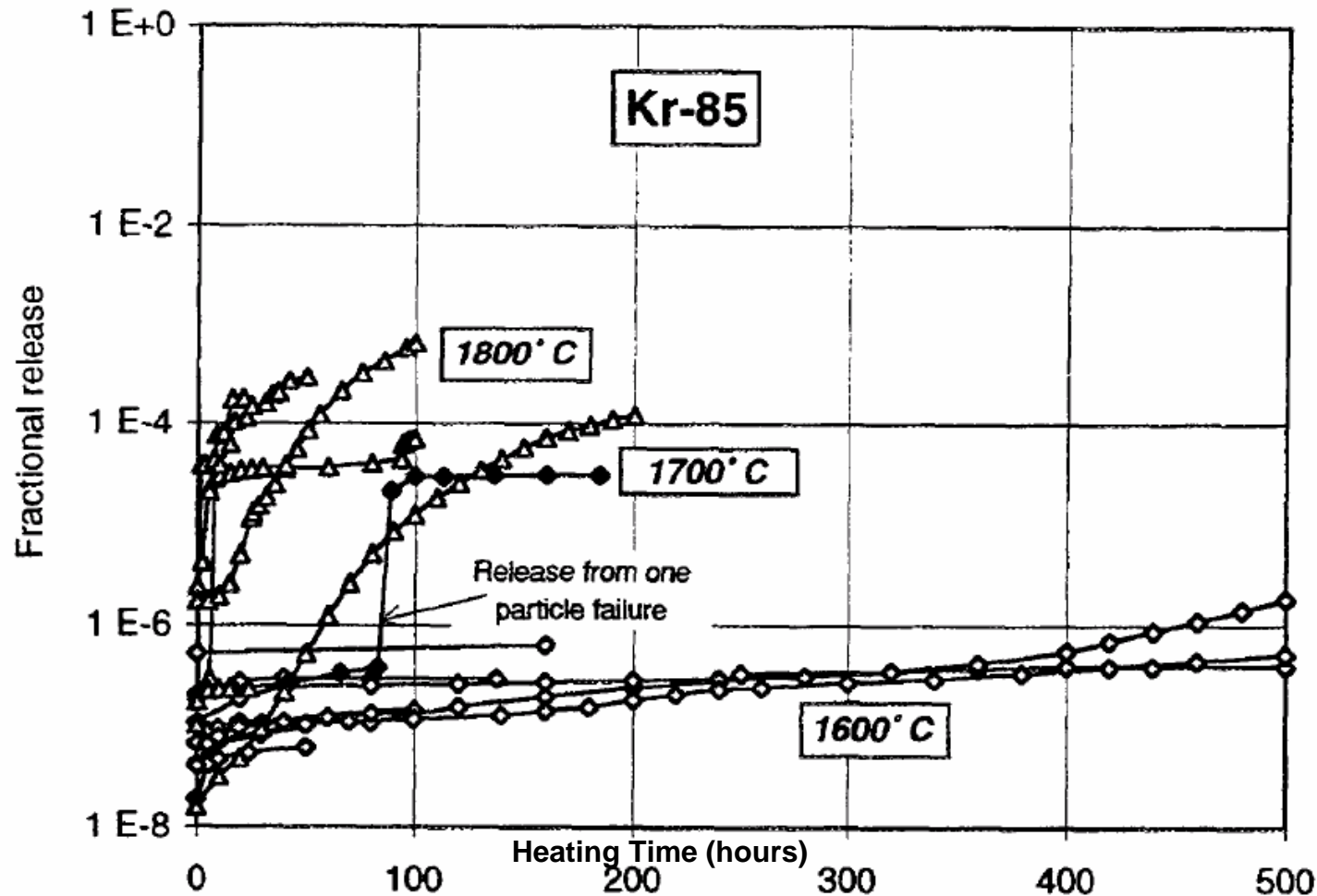


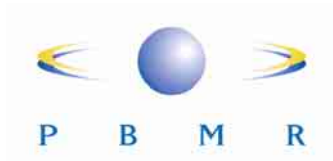
## ***Failures During Transients and Accidents***

- **Total failure fraction is sum of components from**
  - Normal operation
  - Transient and accident heat-up
- **Heat-up “failures” are based on German data**
  - Releases occur over many hours
  - Release rate depends on the test temperature



# Time-at-Temperature Coated Particle Performance for Different Heat-up Tests





## *German Heat-up Data Used for PBMR*

Phase	Temperature (°C)	Burn-up (%FIMA)	Fast Neutron Dose $E > 0.1$ MeV ( $\times 10^{25} \text{ m}^{-2}$ )
MTR	794/1120	7.6/13.9	0.2/7.5
AVR	Cycles < 1400	1.6/9.8	0.4/2.9

**Irradiated Particles Subsequently Heated to Simulate DBA Heat-up:**

**MTRs: 42,586 particles**

**AVR: 213,200 particles**

**Total: 255,786 particles**

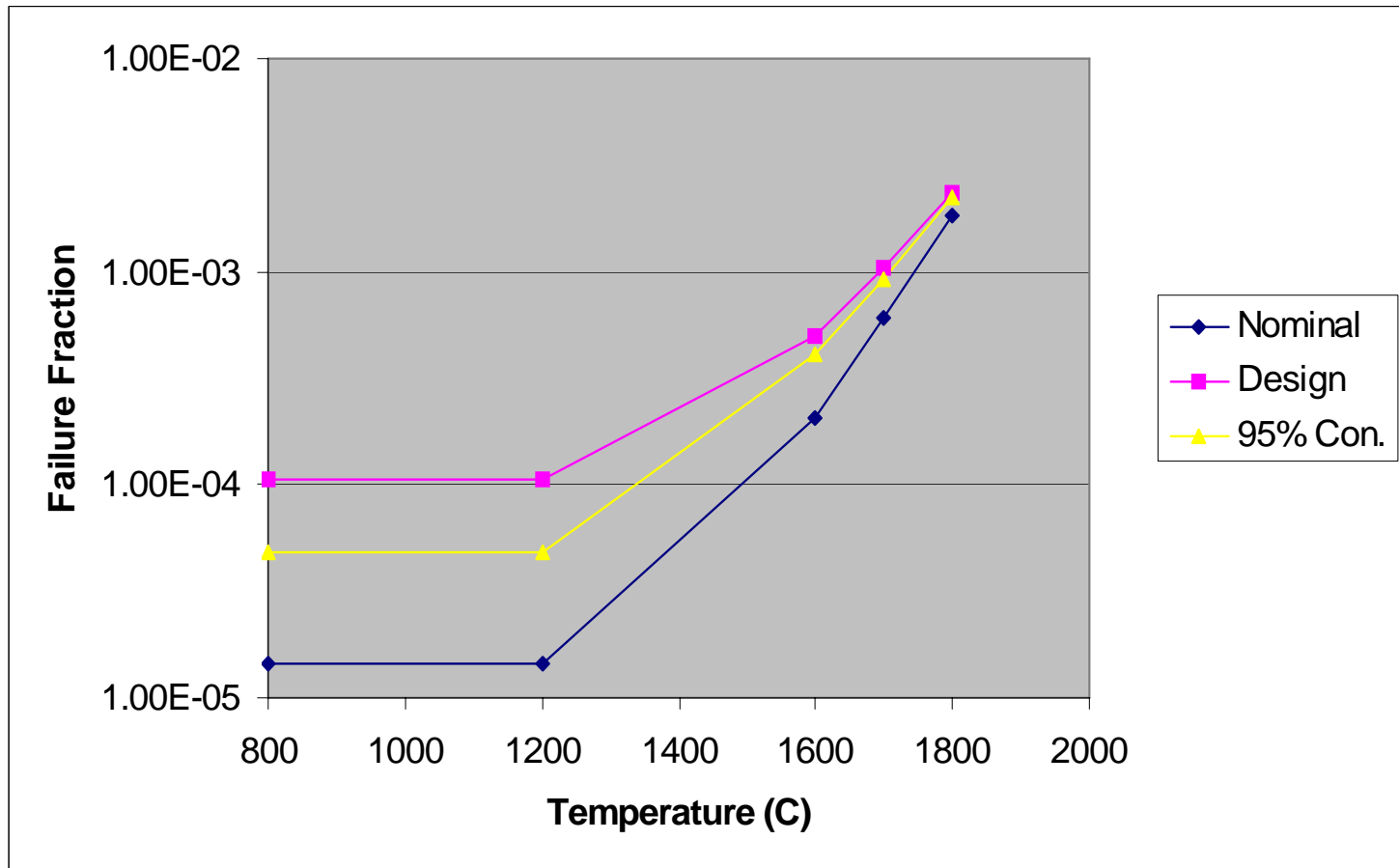
## Summary of Heat-up Test Results

Heating Temperature (°C)	Number of Coated Particles	Number of Failed Coated Particles	Expected Failure Fraction (Average)	95% One-sided Upper Confidence Limit	Design Limit
1 600	86 893	7	$8.06 \times 10^{-5}$	$1.51 \times 10^{-4}$	$1.66 \times 10^{-4}$
1 700	36 062	20	$5.55 \times 10^{-4}$	$8.06 \times 10^{-4}$	$8.56 \times 10^{-4}$
1 800	132 831	108	$8.13 \times 10^{-4}$	$9.54 \times 10^{-4}$	$9.82 \times 10^{-4}$

- **Failure fractions at each confidence level were assumed to be an exponential function of temperature**
  - Based on the statistical distribution of material properties as a function of load on the SiC coating layer
- **The above data were fitted to an exponential correlation**
  - A factor of 2 was added to ensure that the resulting correlation would bound the above data

<b>Temperature (°C)</b>	<b>Nominal Failure Fraction</b>	<b>95% Confidence Failure Fraction</b>	<b>Design Failure Fraction</b>
800	$1.44 \times 10^{-5}$	$4.88 \times 10^{-5}$	$1.06 \times 10^{-4}$
1200	$1.44 \times 10^{-5}$	$4.88 \times 10^{-5}$	$1.06 \times 10^{-4}$
1600	$2.08 \times 10^{-4}$	$4.11 \times 10^{-4}$	$5.04 \times 10^{-4}$
1700	$6.12 \times 10^{-4}$	$9.31 \times 10^{-4}$	$1.04 \times 10^{-3}$
1800	$1.85 \times 10^{-3}$	$2.21 \times 10^{-3}$	$2.33 \times 10^{-3}$

# Representative Empirical Correlation of Failure Fraction vs. Temperature

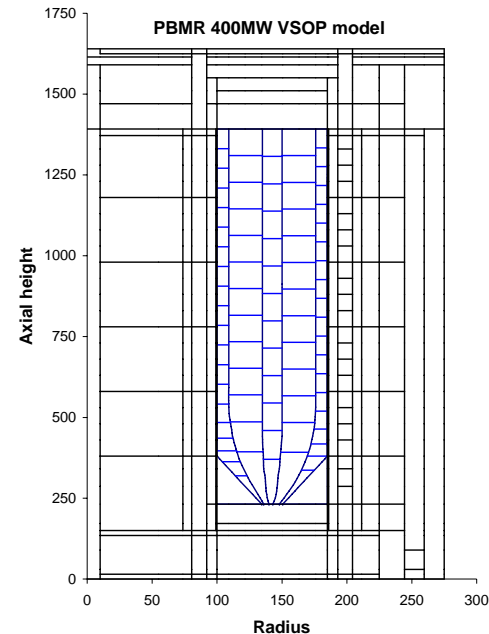


# ***Overview of Use of Release of Fission Products From the Fuel in Accident Analysis***



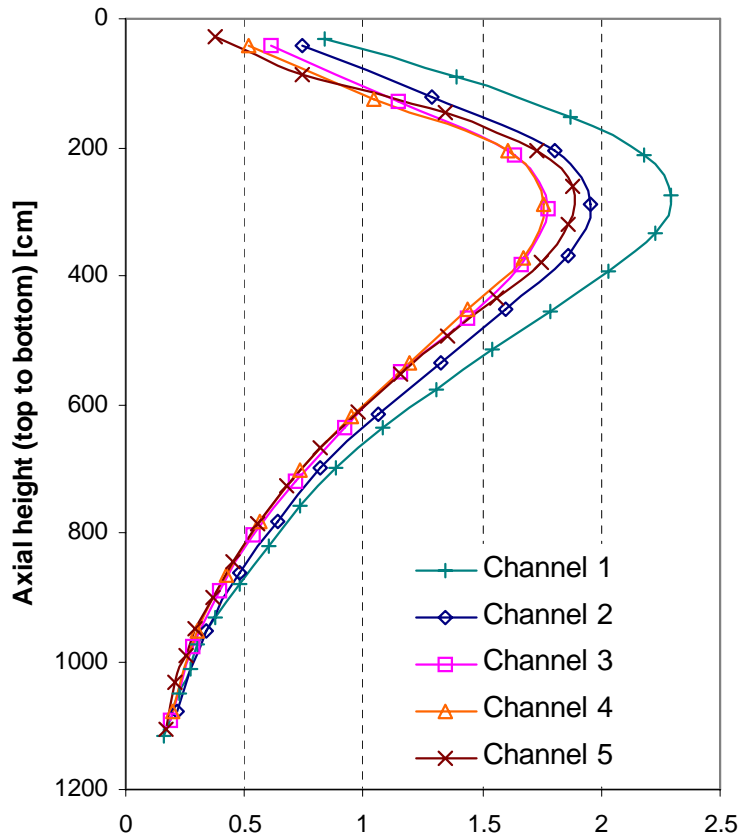
# Release Process Overview

- Fission product content of coated particles is based on burn-up accrued during normal operation
  - Flow of spheres through core
  - Steady-state fuel power, burn-up, and temperatures
  - Core divided into radial channels and vertical layers
- TINTE used to predict fuel temperatures during transients
- Temperatures used with the “failure fraction vs. temperature” correlation to predict quantity of failed particles throughout the core
- Mechanistic code is used to predict releases from the fuel spheres

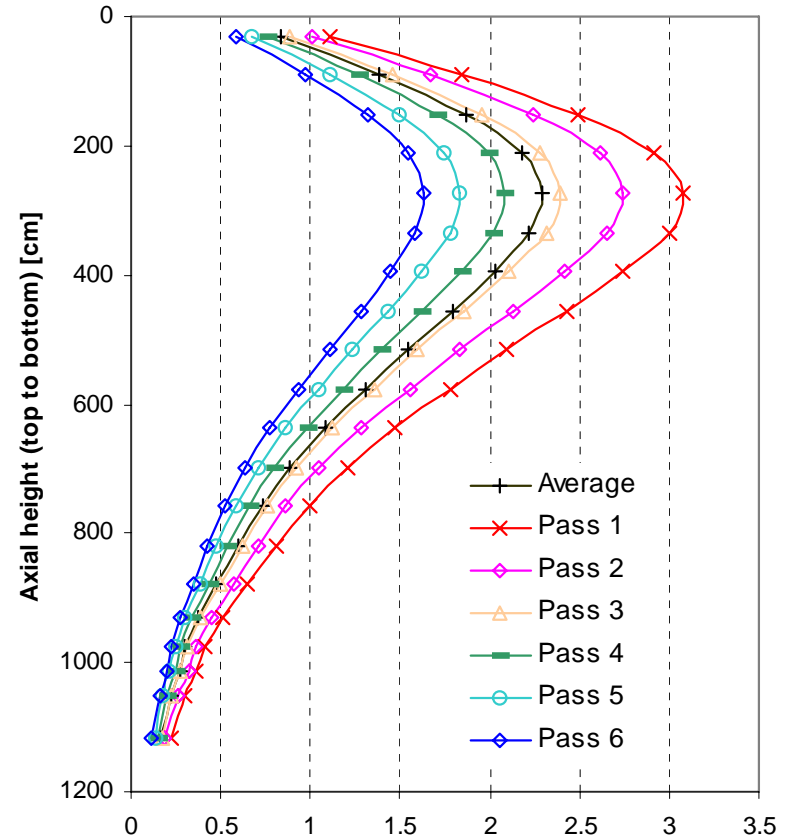




# Typical Axial Power Profiles (Normal Operations)



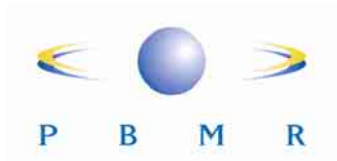
Average power (kW) per sphere for axial position



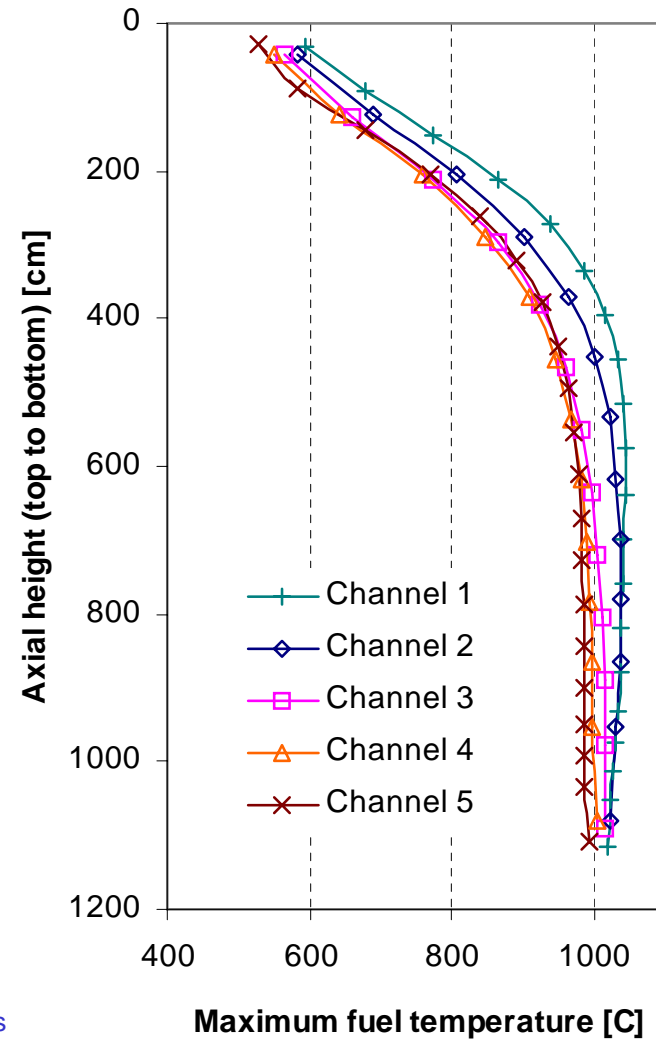
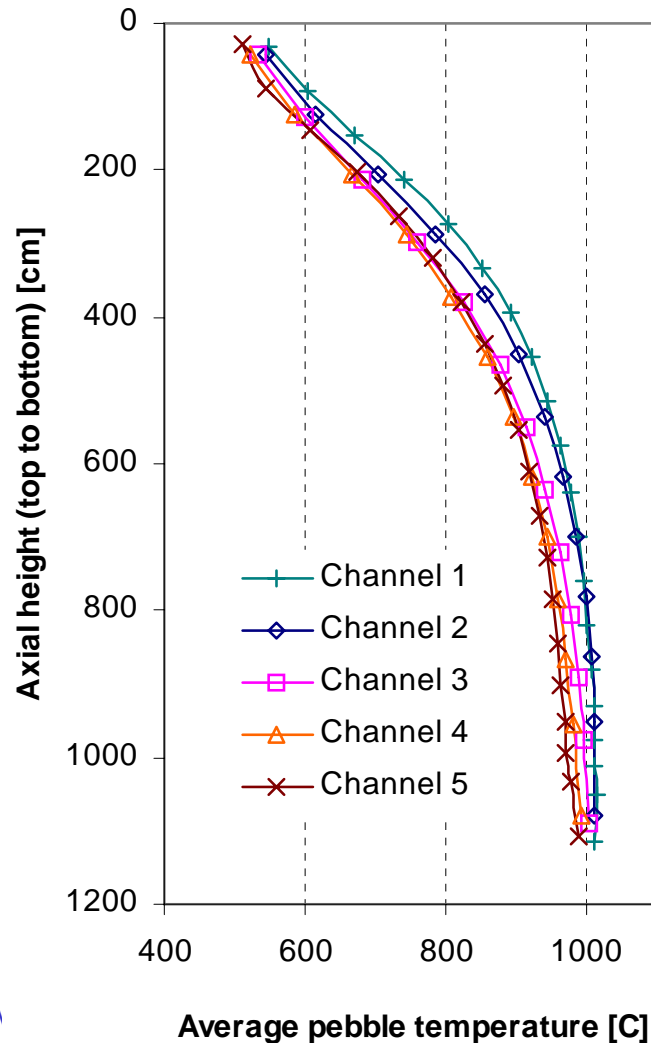
Channel 1- Average power (kW) per sphere for axial position

Core average: 0.88 kW/sphere



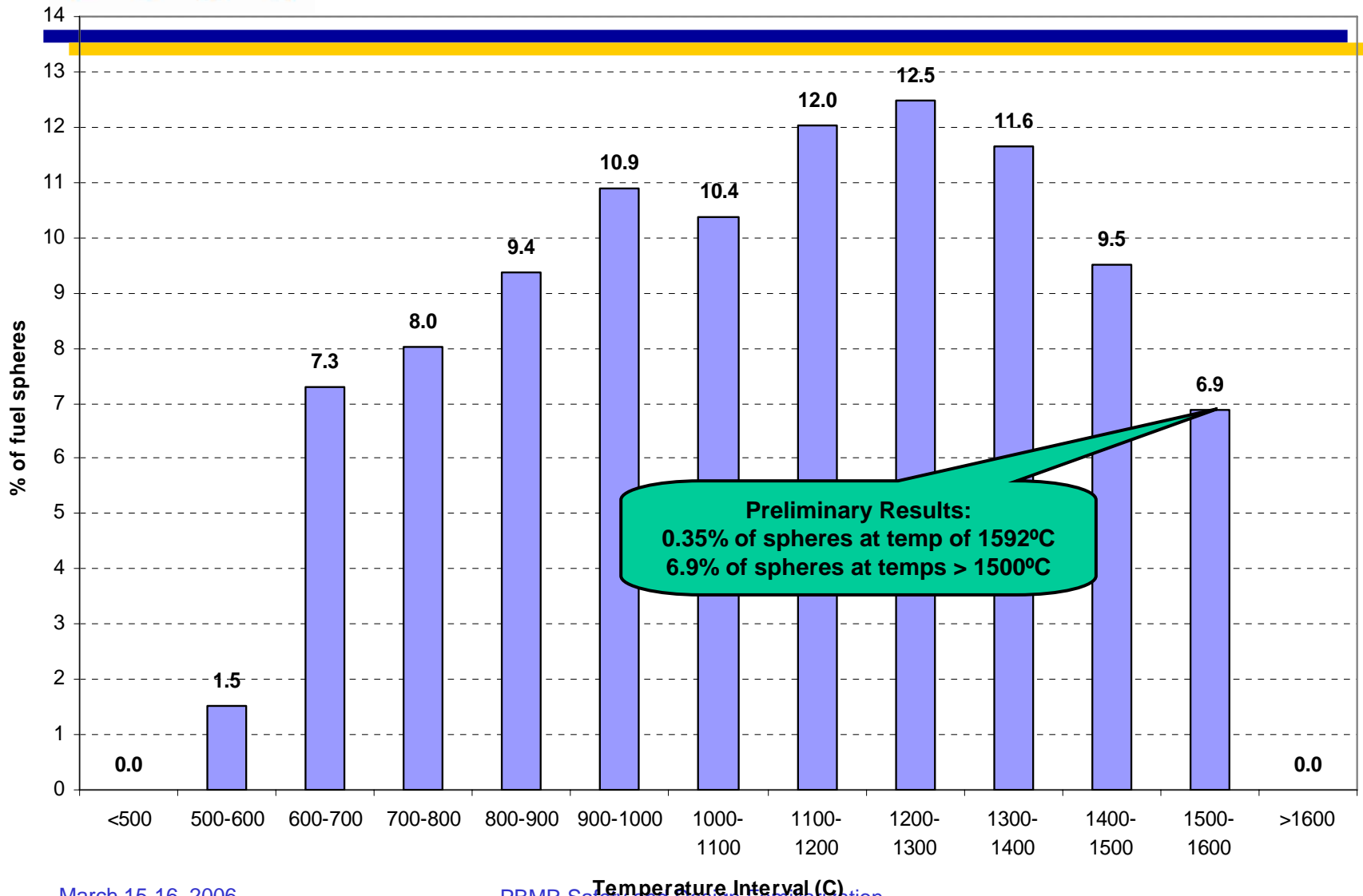


# Typical Fuel Temperature Distributions (Normal Operations)



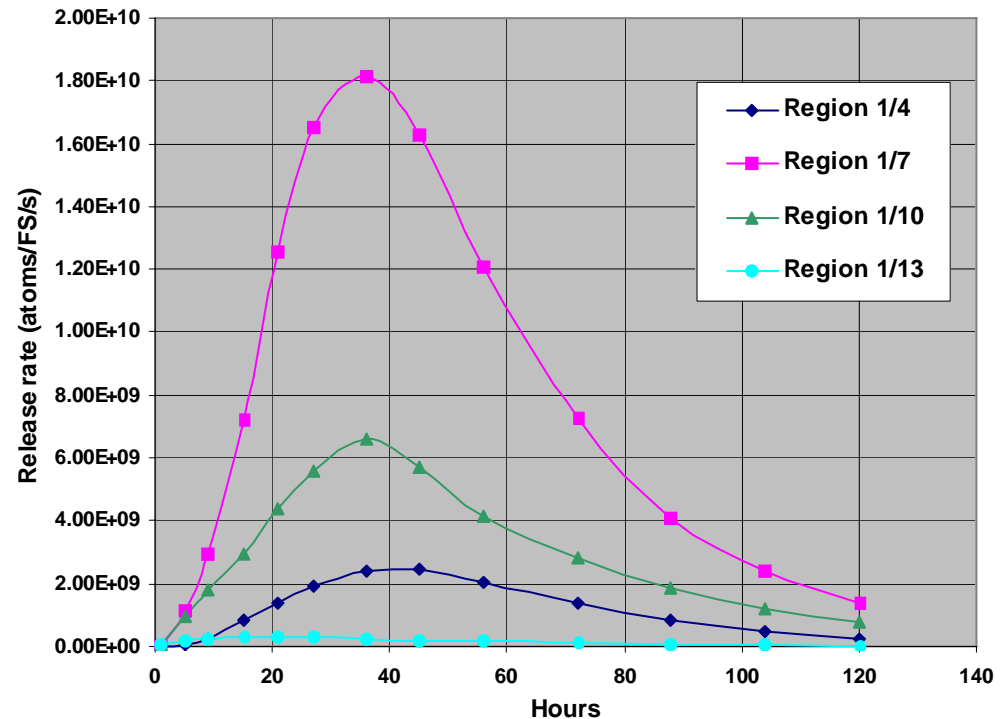


## Typical DLOFC Fuel Temperature Histogram at Time of Peak Fuel Temperature



# Activity Release From Fuel Spheres

- Inputs: normal operation burn-up, transient fuel temperatures, and failure-fraction correlation
- Mechanistic code is used to predict the number of failed particles over the core and the diffusion of fission products to the surface of the fuel spheres



Cs137 – higher release rate only in limited fraction of core volume



## ***Summary – Activity Release Method***

- **Failure fraction as a function of temperature based on manufacturing failures, normal operation irradiation and heat-up test data**
- **Core-wide fuel temperatures during transients used to calculate the fraction of equivalent failed particles in a sphere for the range of burn-ups in the core**
- **Mechanistic model used to predict fission product releases from the spheres**