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1.0 OBJECTIVE

1.1 Background

With the eventual implementation of the Alternative Source Term (AST), 10 CFR 50.67, the Standby Liquid Control (SBLC) System is being considered for preventing re-evolution of iodine from the suppression pool in the event of a Design Basis Accident (DBA-LOCA). Specifically, NRC Regulatory Guide 1.183 states that the radiological consequence analysis should consider iodine re-evolution if the suppression pool liquid pH is not maintained greater than 7. Maintaining the suppression pool liquid pH greater than 7.0 can be accomplished by the buffering action of boron released to the suppression pool from the SBLC System (see calculation EC-059-1041).

1.2 Statement of Problem

It is proposed to inject boron to the suppression pool via the SBLC System to maintain basic pH in the suppression pool in order to minimize re-evolution of iodine from the suppression pool in the event of a Loss of Coolant Accident (LOCA). However, the system fails to meet all the requirements of a safety-related system in that SBLC is not designed for the single active component failure criteria. Therefore, a failure of a critical component would prevent the system from controlling suppression pool liquid pH by using the buffering action of boron injected to the suppression pool from the SBLC system (via the reactor vessel). The success of the SBLC system is necessary in order to take credit for this pH control function and prevention of iodine re-evolution. The NRC has provided review guidelines for the SBLC system that do not meet single failure criteria or that are not of the expected quality (safety related). This calculation will specifically demonstrate compliance with the requirements identified in the NRC review guideline document.

The evaluation will be accomplished in four steps, as follows:

- a) Provide overall assurance the SBLC System meets the quality guidelines
 (a)-(e) regarding the reliability, redundancy presented in Sections 1.4 and 1.5 below.
- b) Identify all active and passive components of the SBLC System under consideration.

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c) Screen for (and identify) critical components subject to single failure criteria. (Details are discussed starting in Section 4.3)

d) Substantiate a low risk failure probability for the identified components.

1.3 <u>System Overview</u>

The SBLC System is an independent and diverse backup system to the Control Rod Drive (CRD) System. SBLC shuts down the reactor by injecting a neutron absorbing solution into the reactor coolant, which is circulated through the core. The neutron absorber used in SBLC is an aqueous solution of sodium pentaborate decahydrate, $Na_2B_{10}O_{16}$ *10H₂O. Sufficient solution is injected to bring the reactor from maximum rated power conditions to cold subcritical over the entire reactor temperature range, from maximum operating to cold shutdown conditions. SBLC is not required to scram the reactor, or to serve as a backup scram system. There is no requirement for SBLC to be capable of operation when the reactor is shut down by the CRD System.

The SBLC System is listed as a Nuclear Steam Supply System. Based on Regulatory Guide 1.70, the SBLC is identified as a safe shutdown system having a safety-related classification. Safety-related systems provide the actions necessary to assure safe shutdown of the reactor, to protect the integrity of radioactive material barriers, and/or to prevent the release of radioactive material in excess of allowable dose limits. Safe shutdown of the reactor is classified as a nuclear safety function, and thus, the SBLC is classified as having a safetyrelated function.

The SBLC System consists of two 100% capacity positive displacement triplex type (3-piston) injection pumps which when operating together are capable of delivering sodium pentaborate to the reactor vessel to meet 10CFR50.62 requirements, two 100% capacity explosive actuated injection valves, one storage tank, one test tank, and the piping, valves, instrumentation and controls necessary to inject the solution into the reactor and to test the SBLCS. All equipment in the SBLCS which comes in contact with the neutron absorbing solution is stainless steel for corrosion protection.

1.4 Quality Guidance In Support of AST

To demonstrate that the SBLC System is able to perform its AST (10 CFR 50.67) function (injection of sodium pentaborate into the suppression pool), the System should satisfy, as a minimum, the recommended guidelines listed below (NRC

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	es). Meeting these criteria, de the SSES SBLC System. Th		

b) The SLC system should be seismically qualified in accordance with Regulatory Guide 1.29 and Appendix A to 10 CFR Part 100.

c) The SLC system should be incorporated into the plant's ASME Code ISI and IST Programs based upon the plant's code of record (10 CFR 50.55a).

d) The SLC system should be incorporated into the plant's Maintenance Rule program consistent with 10 CFR 50.65.

e) The SLC system should meet 10 CFR 50.49 and Appendix A (GDC 4) to 10 CFR 50.

Therefore, meeting the intent of these guidelines should provide reasonable assurance of the System's ability to support the pH controlling function. Each specific guideline, as it impacts and is supported by the SSES SBLC System, is addressed in detail in Section 4.1 of this evaluation.

1.5 Reliability Requirements in Support of AST

In addition to meeting the quality requirements of the NRC review guidelines, the SBLC system must also meet reliability requirements. The following criteria are provided in the NRC review guidelines if the SBLC system can not perform its AST function due to a single failure of an active component.

Acceptable quality and reliability of the non-redundant active components and/or compensatory actions in the event of failure of the non-redundant active components.

Under this approach, the licensee should provide the following information in justifying the lack of redundancy of active components in the SLC system:

(a) The licensee should identify the non-redundant active components in the SLC system and provide their make, manufacturer and model number. The staff

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reviewer will compare this information with performance data for the component from industry data bases and other sources.

(b) The licensee should provide the design-basis conditions for the component and the environmental and seismic conditions under which the component may be required to operate during a design basis event. Environmental conditions include design basis pressure, temperature, relative humidity and radiation fields. The staff reviewer will compare the environmental conditions associated with the design basis accident to conditions for which the component was designed to determine whether the component is capable of performing its intended function.

(c) The licensee should indicate whether the component was purchased in accordance with Appendix B to 10 CFR Part 50. If the component was not purchased in accordance with Appendix B, the licensee should provide information on the quality standards under which it was purchased. For the latter situation, information in the component would be reviewed by the appropriate technical review branch responsible for the component, as requested by the lead SPSB reviewer.

(d) The licensee should provide the performance history of the component both at the licensee's facility and in industry databases such as EPIX and NPRDS. The staff reviewer will use this information to evaluate the reliability of the component relative to other components used in safety-related applications.

(e) The licensee should provide a description if its inspection and testing program including standards, frequency and acceptance criteria. The staff reviewer will use this information to evaluate the licensee's activities to monitor the component's performance at the facility. The information on the component would be reviewed by the appropriate technical review branch responsible for the component, as requested by the lead SPSB reviewer.

(f) The licensee should also indicate the potential compensating actions that could be taken within an acceptable time period to address the failure of the component. An example of a compensating action might be the ability to jumper a switch in the control room to overcome its failure. The staff reviewer will consider the availability of compensating actions and the likelihood of successful injection of the sodium pentaborate where non-redundant active components fail to perform their intended functions.

Each Reliability Requirement, as it impacts and is supported by the SSES SBLC System, is addressed in detail in Section 4.2 of this evaluation.

System, is addressed in detail in Section 4.2 of this evaluation.

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2.0 CONCLUSIONS & RECOMMENDATIONS

The results of this calculation show that the use of the SBLC System for preventing re-evolution of iodine from the suppression pool in the event of a Design Basis Accident (DBA-LOCA) meets all of the NRC Guidelines for that application.

3.0 ASSUMPTIONS/DESIGN INPUTS

The following general input data was used in this evaluation:

- 3.1 SBLC System component data was obtained from References 6.2 through 6.16.
- 3.2 Performance history of critical components was obtained from References 6.16 through 6.18.
- 3.3 Other input data as referenced in the respective section(s), or when used.

4.0 <u>METHODOLOGY</u>

By means of the approach presented in Section 1.2, the details of substantiation of using the SBLC System for this application follow.

4.1 Quality Guidance of the SBLC System in Support of 10 CFR 50.67:

As suggested by the "Guidance on the Assessment of a BWR SLC System for pH Control", guideline items (a) through (e) present details of demonstrating reasonable assurance regarding the quality of the SSES SBLC System. These are presented in the same order as listed in Section 1.4 above.

a) <u>The SLC system should be provided with standby AC power</u> supplemented by the emergency diesel generators.

The SBLC pumps, storage tank heaters and instrumentation and controls are powered from or connectable to the standby AC power supply. The pump,

powered from or connectable to the standby AC power supply. The pump,

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explosive actuated valve, and instrumentation and controls for loop "A" are powered from load group 1C and those components in loop "B" are powered from load group 1A. All components in the SBLC System are connected to Division I power, but the use of two load groups per electrical division provides for electrical separation for the SBLC System.

Reference 6.24 (Drawing E-166, Sheets 1, 2, 5, and 6) show that each SBLC pump and associated equipment is powered from an independent 4.16 kV bus through the preferred AC electrical power to all Class 1E loads. This is shown on Single Line Diagram for the station, Reference 6.8 (E-1, Sheet 1). It shows that the normal power supply for Division I, Channel A and Division I, Channel C is from Engineered Safeguard Transformer 101 (0X201). However, Division I can also be fed by Engineered Safeguard Transformer 103 (0X203). In the event of total loss of offsite power sources, onsite <u>Independent diesel generators</u> provide the standby safety features loads.

The A pump, 1(2)P208A, (along with power to open squib valve 1(2)48-F004A, and control power for the A instrumentation and controls) is from Division I, Channel C, MCC 1(2)B236, which can be supplied from the <u>C Diesel</u>, if offsite power is unavailable.

The B pump, 1(2)P208B (along with power to open squib valve 248-F004B and control power for the B instrumentation and controls) is from Division I, Channel A, MCC 1(2)B217, which can be supplied from the <u>A Diesel</u> if offsite power is unavailable. The power to open the squib valve 148-F004B, is from 1B216.

Valves HV-1(2)48-F006 are powered from 1E 480V, MCC 1(2)B236

Both of the SLC storage tank heaters (heater A - 1(2)E219, and heater B - 1(2)E220) are powered from 1E 480V, MCC 1(2)B236.

b) <u>The SLC system should be seismically qualified in accordance with</u> <u>Regulatory Guide 1.29 and Appendix A to 10 CFR Part 100.</u>

Mechanical Components:

The SBLC System is designed to meet the intent of **Regulatory Guide 1.29**, "Seismic Design Classification", Revision 2, 2/76

General Design Criterion 2, "Design Basis for Protection Against Natural Phenomena" (GDC 2), requires that structures, systems, and components

Phenomena" (GDC 2), requires that structures, systems, and components

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important to safety be designed to withstand the effects of natural phenomena such as earthquakes without loss of capability to perform their safety functions. The guidance in **Regulatory Guide 1.29** provides an acceptable method of determining seismic classification and applicability. Because the SBLC System forms part of the RCPB, and can be used for reactor shutdown, it is classified by Regulatory Guide 1.29 as **Seismic Category I**. The NRC Safety Evaluation Report, NUREG-0776 Section 9.3.2, lists compliance with Regulatory Guide 1.29 as one of the reasons that the SBLC design is acceptable.

SBLC System Seismic Category I structures and components are analyzed under the loading conditions of the SSE and OBE. Since the two earthquakes vary in intensity, the design of Seismic Category I structures, components, and equipment to resist each earthquake and other loads are based on levels of material stress or load factors, whichever is applicable. Piping and equipment, including support structures, are designed to Seismic Class I earthquake requirements. FSAR Table 3.2-1 contains a detailed breakdown of the SBLC System and the seismic classification.

Electrical Equipment and Instrumentation:

The SBLC Seismic Category 1 electrical and instrumentation and control equipment is designed to meet the intent of IEEE Standard 344-1971, "IEEE Recommended Practices for Seismic Qualification of Class 1E Equipment for Nuclear Power Generating Stations". (FSAR Section 3.10a.2).

All SBLC electrical and instrumentation and control equipment designated as Seismic Category 1 are designed to resist and withstand the effects of the postulated earthquakes. Seismic Category 1 instrumentation and electrical equipment is designed to withstand the effects of the safe shutdown earthquake (SSE) defined in FSAR Subsection 3.7.1, and to withstand the effects of hydrodynamic loads without functional impairment. The Class 1E equipment is capable of performing all safety-related functions during; (I) normal plant operation, (2) anticipated transients, (3) design basis accidents, and (4) postaccident operation, while being subjected to, and after the cessation of, the accelerations resulting from the SSE at the point of attachment of the equipment to the building or supporting structure.

c) <u>The SLC system should be incorporated into the plant's ASME Code ISI</u> and IST Programs based upon the plant's code of record (10 CFR 50.55a).

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The SBLC is designed to meet the design intent of the requirements of the ASME Boiler and Pressure Vessel Code, Section XI, "Rules for Inservice Inspection of Nuclear Power Plant Components".

10CFR50.55a, "Codes and Standards, requires that an inservice inspection program be developed in accordance with ASME Section XI. NUREG-0800, "Standard Review Plan for the Review of Safety Analysis Reports for Nuclear Plants", requires a test program to ensure that all ASME Code Class 1, 2, and 3 pumps and valves will be in a state of operational readiness to perform necessary safety functions throughout the life of the plant. The ASME Boiler and Pressure Vessel Code, Section XI, "Rules for Inservice Inspection of Nuclear Power Plant Components," describes an acceptable method of complying with the requirements of **10CFR50.55a** and NUREG-0800 for a test program to test ASME Code Class 1, 2, and 3 pumps and valves.

Where practical, all ASME Section III Class 1, 2, and 3 pumps are in-service tested in accordance with Subsection IWP of ASME Section XI in order to establish and detect changes in the hydraulic and mechanical reference parameters. The pump test program meets, to the extent practical, the requirements for establishing reference values of IWP-3000 of ASME Section XI. The allowable ranges of in-service test quantities, corrective actions, and bearing temperature tests are in accordance with IWP-3200 and IWP-4300 of ASME Section XI.

SSES Procedure NDAP-QA-0423, commits the plant to ASME IST pump and valve testing as required by Technical Specification 5.5.6, "Inservice Testing Program". This Specification provides controls for inservice testing of ASME Code Class 1, 2, and 3 components. The program includes testing frequencies specified in Section XI of the ASME Boiler and Pressure Vessel Code and applicable Addenda.

Functional Testing:

Functional testing of the SBLC System is performed by (1) circulating demineralized water with the explosive valves closed and (2) pumping demineralized water from the test tank through the explosive valves into the reactor.

System testing enhances the reliability of the system and demonstrates system

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also provides the capability to verify system pumping capability to the reactor when the plant is shut down.

d) <u>The SLC system should be incorporated into the plant's Maintenance Rule</u> program consistent with 10 CFR 50.65.

The SBLC System is designed to meet the intent of the requirements of **10CFR50.65**, "Requirements for Monitoring the Effectiveness of Maintenance at Nuclear Power Plants". The SBLC Ssystem has been incorporated into the plant's Maintenance Rule Program.

The Commission's determination as stated in Regulatory Guide 1.160, Rev. 1, was that the decision that a maintenance rule was needed arose from the conclusion that proper maintenance is essential to plant safety. PPL has not committed to a particular revision of this regulatory guide.

However, the SBLC System is designed such that periodic surveillance testing and maintenance can be performed on system components. PPL Procedure NDAP-QA-0413, "SSES Maintenance Rule Program," implements the SSES program for compliance with 10CFR50.65.

The following table summarizes PP&L's commitment to the SBLC System Maintenance Rule functions. The data for SBLC System is maintained (or viewed) at the following SSES Information System sites:

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FUNCTION NUMBER	FUNCTION	MAINTENANCE RULE FAILURE FUNCTION (MRFF) GUIDANCE
	STANDBY LIQUIE	CONTROL SYSTEM # 53
01A	Pump A injects sodium pentaborate solution into the reactor as an alternate means of shutting down the reactor independent of the CRD system	Component failures resulting in the loss of capability to inject sodium pentaborate into the reactor vessel.



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FUNCTION NUMBER	FUNCTION	MAINTENANCE RULE FAILURE FUNCTION (MRFF) GUIDANCE
01B	Pump B injects sodium pentaborate solution into the reactor as an alternate means of shutting down the reactor independent of the CRD system	Component failures resulting in the loss of capability to inject sodium pentaborate into the reactor vessel.
02	Provide containment isolation	Failure of 1(2)48F007 and HV1(2)48F006 to close on demand. LLRT is monitored with the overall containment integrity function in system 59.
03	Components of this system are required to maintain integrity of the reactor coolant pressure boundary	Leakage through a visible indication (i.e. through wall leakage) resulting in loss of reactor coolant fluid from the reactor coolant system boundary.
04	Maintain SLC piping and tank at sufficiently high temperature to keep sodium pentaborate above saturation temperature	Component failures resulting in loss of capability to maintain SLC fluid within the required limits for fluid temperature. Failure of the heat tracing, including failure of the associated breaker 1(2)B236063 (A heater) or 1(2)B236111 (B heater), may cause a MRFF. Reference TS Table 3.1.7-2.
05	Provide SBLC flow and storage tank level indication to the control room	Failures that result in the inability to determine SBLC flow or storage tank level indication (indication is available from 1(2)C601 and the plant computer). Blockage of a bubbler tube may be a MRFF.
06	Provide input to RWCU Isolation logic on SBLC actuation	SBLC logic system component failures resulting in the inability to isolate the RWCU outboard isolation valve, HV1(2)44F004.
07	Provide Containment Isolation valve position indication signal for control room display	Failure that results in the inability to determine the position of HV1(2)48F006 from the control room. Light bulb failures are not considered a MRFF IAW NDAP-QA-0413.
	Provide an alternate means of reactor vessel makeup via the SLC Boron Tank or demin water cross- tie	Component failures resulting in loss of capability to makeup to the reactor vessel via the SBLC.

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e)

The SLC system should meet 10 CFR 50.49 and Appendix A (GDC 4) to 10 CFR 50.

The SBLC System is designed to accommodate the effects of and to be compatible with the environmental conditions associated with normal operation (not accident), maintenance, and testing. (GDC 4)

Table A-1 of licensing topical report NEDE-31096-P, "Anticipated Transients Without Scram; Response to NRC ATWS Rule, 10CFR50.62" notes that NRC guidance for EQ for a new SLC System would be to design for anticipated operational occurrences only, not for accidents. A review of the reactor building post-LOCA temperature response calculation (EC-LOCA-0500) determined that the area in which the SBLC system is located only increases a few degrees during the first few hours post-LOCA. Additionally, the SBLC equipment will not experience significant radiation damage given the short duty time of the SBLC system and the early initiation time for the design basis scenario. The relative humidity and area pressures should remain relatively unchanged. Given that SBLC initiation will occur within the first few hours post-LOCA and the demand time is low, the environment that the SBLC system electrical equipment will experience bost-LOCA is not significantly different than the environment that it experiences during normal operation and will be able to successfully fulfill its design basis function.

The SBLC is appropriately protected against dynamic effects, including the effects of missiles that may result from equipment failures and from events and conditions inside the plant. Runs of system piping in the secondary containment which are subject to damage due to possible failure of nearby piping or components of other systems are protected by structural steel or reinforced concrete, or spatial separation (FSAR Sect. 9.3.5, 7.4.1.2).

FSAR Section 3.11 discusses the normal and accident environmental conditions relative to temperature, pressure, humidity, and integrated radiation exposure under which systems and components required for safe shutdown are required to remain functional. Reference 6.2 lists harsh environments of various plant areas, including those where the SBLC is located, and the normal and anticipated accident environmental conditions in these areas. Safety-related equipment is installed in accordance with mechanical and electrical separation requirements. It is also designed and qualified to function properly in the environments listed.

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Tornado-generated missiles are the only natural phenomena missiles considered. Protection consists of tornado-resistant buildings with structures and barriers designed to protect against the postulated missiles listed in FSAR Table 3.5-4.

The SBLC is designed to meet the intent of Regulatory Guide 1.46, "Protection Against Pipe Whip Inside Containment", 5/73. (FSAR Section 3.6.2.1.4.5)

General Design Criterion 4, "Environmental and Missile Design Basis" (GDC 4), requires that structures, systems, and components important to safety be appropriately protected against dynamic effects that may result from equipment failures, including the effects of pipe break. Regulatory Guide 1.46 describes an acceptable basis for selecting the design locations and orientations of postulated pipe breaks in designing the SBLC System piping within the reactor containment and for determining the measures that should be taken for restraint against pipe whipping that may result from such breaks.

Pipe whip is an unrestrained pipe movement of either end of the ruptured pipe in any direction about a plastic hinge formed at the nearest pipe whip restraint. Pressurized components in the SBLC System where service temperature exceeds 200°F or service pressure exceeds 275 psig were evaluated as to the potential for pipe whip. Pipe whip restraints are provided for the SBLC injection line inside the primary containment. The plant has been designed in accordance with the criteria of Branch Technical Position ASB 3-1, "Protection Against Postulated Piping Failures in Fluid Systems Outside Containment" and is documented in Section 3.6 of NUREG-0776, "Safety Evaluation Report Related to the Operation of SSES Units 1 and 2".

4.2 Reliability Requirements in Support of AST

(a) The licensee should identify the non-redundant active components in the SLC system and provide their make, manufacturer and model number.

Through a thorough review of the SBLC System components (Attachment 1) and the system P&IDs (Reference 6.6) single components with no backup or redundant component with a singe power source (SBLC tank heaters) were identified and documented as the single failure candidates (Table 4.4.2).

Characteristics of each non-redundant active component are presented in detail in the respective section where the component is individually discussed.

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However, Table 4.2.1 below identifies the non-redundant components and their design characteristics.

Component Name	Component Function	Component System Number (Unit)	Component Model Number	Component Manufacturer
SBLC Manual initiation	Initiate system boron	HS14804 (U1) HS24804	CR 2940	General Electric
switch	injection. Closes contacts that	(U2)	(Reference 6.24, Sh. 1)	(Reference 6.24, Sh. 1)
	energize the A and B Pumps			
SBLC Outboard motor operated	Normally CLOSED. Acts as an isolation	HV148F006 (U1) HV248F006 (U2)	1 ½ "Yarway Welbond Valve with Limitorque Electric Motor	Yarway Corp. Blue Bell, PA
stop check valve	check valve in the injection line when in the OPEN		Actuator. Globe stop-check valve. (Reference 6.21,	(Reference 6.21, Sh. 1)
SBLC	position. Check valve	148F007	Sh. 1) 1 ½ " Y-Type	Borg Warner
inside dryweli check	for the SBLC injection line.	(U1) 248F007 (112)	Check Valve Part No. 74730	Nuclear Valve Division
valve.		(U2)	(Reference 6.10, Sh. 1)	Van Nuys, CA
				(Reference 6.10, Sh. 1)
Locked open manual	Stays open to allow boron	148F008 (U1) 248F008	1 ½ " Gate Valve, Cres.	Borg Warner Nuclear Valve
injection	injection.	(U2)	Part No. 74680	Division

Table 4.2.1 - Component Characteristics

injection

injection. (U2)

| Part No. 74680

| Division

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	vaive	Down stream of the above check valve.		(Reference 6.20, Sh. 1)	Van Nuys, CA (Reference 6.20, Sh. 1)
	SBLC Storage tank heater "A" (10 kW)	Operates to automatically maintain solution temperature above the precipitation	1E219 (U1) 2E219 (U2)	Part No. 2D433G0022 Part No. 2D433G0022	General Electric General Electric (Reference 6.31)
	SBLC Storage tank heater	point Used to elevate the mixture	1E220 (U1)	(Reference 6.31) Part No. 166B7320P001	General Electric
	"B" (40 kW)	temperature during chemical addition	2E220 (U2)	Part No.: 2D507G140 (Reference 6.31)	Weliman Co. (Reference 6.31)

Additional information on SBLC operation and redundancy is provided below.

Operation of the SBLC pumps and the explosive actuated valves that inject the solution into the reactor are controlled from the control room panel by a single manual control switch on panel 1C601 keylocked in the "STOP" position. This is shown on drawing J-802 Sheet 2 (Reference 6.25). The key is removable in the left "STOP" position. The SBLC is initiated by turning the keylock switch to the "START" position. Placing the key switch in the "START" position initiates both "A" and "B" trains of the SBLC. When the SBLC is initiated, both explosive-actuated valves fire. Simultaneously, both SBLC pumps are started and parallel solution injection begins. This is shown on elementary diagram M1-C41-36 Sheets 1, 2, and 3 (Reference 6.26) and M1-C41-31 (Reference 6.27). Concurrently with initiation of the SBLC, a signal is sent to the Reactor Water Cleanup (RWCU) System to isolate the RWCU System from the reactor to prevent the removal and dilution of the neutron absorbing solution. The SBLC pumps may be operated locally for system testing, but actuation of the explosive actuated valves may only be accomplished from the control room.

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Redundancy has been designed into the electric power system supporting SBLC System components, controls and instrumentation. Justification in support of this statement follows.

Redundancy of SBLC System Components:

The on-site electric power system includes four load groups. The load groups are redundant in that three load groups are capable of ensuring vital functions are maintained in the event of postulated accident. Sufficient independence is provided between redundant load groups to ensure that postulated single failures affect only a single load group and are limited to the extent of total loss of that load group. The remaining redundant load groups remain intact to provide for the containment integrity.

The SBLC pumps, storage tank heaters and instrumentation and controls are powered from or connectable to the standby AC power supply. The pump, explosive actuated valve, and instrumentation and controls for loop "A" are powered from load group 1C and those components in loop "B" are powered from load group 1A. All components in the SBLC are connected to Division I power, but the use of two load groups per electrical division provides for electrical separation for the SBLC System. The only exception is the storage tank heaters which are powered from a common bus for each respective unit.

The SBLC pump circuit is protected or separated from the explosive valve ignition circuit. Protection or separation between these two circuits is required so that a short in the ignition circuit will not affect operation of the pumps.

The ignition circuit for each explosive actuated valve squib is fused to prevent disabling any pump with a short in any squib valve. The fuses are shown on M1-C41-36 (Reference 6.27). Each firing circuit (two per valve) contains a single fuse (C41-F2, F3, F5, F6) which are sized at 2 amps. An electrical short in the ignition circuitry will cause the fuse to fail, isolating the shorted circuit from the balance of the control system.

SBLC System Control:

Controls are provided, in the control room, from which actions can be taken to operate the SBLC System safely under normal conditions. (GDC 19)

Controls for normal operation, monitoring, and testing the SBLC are placed in the main control room. Information is furnished to the operator through meters,

main control room. Information is furnished to the operator through meters,

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annunciators, gauges, and indicating lights as to the standby and operational status of the SBLC. Operation of the SBLC from the control room is entirely a manual operation to prevent inadvertent initiation of the system.

Instrumentation and Control:

Criterion XIV of Appendix B to 10CFR50 "Quality Assurance Criteria for Nuclear Power Plants and Fuel Reprocessing Plants", requires that measures be established for indicating the operating status of structures, systems and components of the nuclear power plant, such as by tagging valves and switches, to prevent inadvertent operation. Section 50.55a of 10CFR50, "Codes and Standards", requires in Paragraph (h) that protection systems meet the requirements set forth in IEEE 279-1971, "IEEE Standard Criteria for Protection Systems for Nuclear Power Generating Stations".

The continuity of the explosive valve circuit is continuously monitored and is annunciated in the control room if the continuity is broken (current flow is interrupted). The level and temperature of the storage tank solution are continuously monitored with the high and low levels and high and low temperature conditions annunciated in the control room. The removal of all other equipment for servicing is manually annunciated and is administratively controlled.

The SBLC System is designed to meet the intent of **Regulatory Guide 1.97**, "Instrumentation for Light-Water-Cooled Nuclear Power Plants To Assess Plant and Environs Conditions During and Following an Accident", Revision 2, 12/80.

General Design Criterion 13, "Instrumentation and Control" (GDC 13), requires that instrumentation be provided to monitor variables and systems over their anticipated ranges for accident conditions as appropriate to ensure adequate safety. General Design Criterion 19, "Control Room" (GDC 19), requires that equipment, including the necessary instrumentation, at appropriate locations outside the control room be provided with the design capability for prompt hot shutdown of the reactor. **Regulatory Guide 1.97** provides an acceptable method for designing the SBLC instrumentation to conform to the requirements of General Design Criteria 13 and 19.

Jaculaton: Cuido 1.07 requires CBI C control ream flow indication of 0 to 1100/

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level instrumentation LI/FI-1(2)4806 (including LE-1(2)4812 and LT-C41-1(2)N001) has a detection range of 0 to 126 inches and 0 to 5000 gallons. The tank size is 5711 gallons (Reference 6.38). Per Reference 6.4 the setpoint volume for High Alarm is at 4897 gallons and Low Alarm at 4587 gallons (which is also the Technical Specification 3.1.7 limit). LE-1(2)4812 and LT-C41-1(2)N001 are not 1E qualified but are fed from a vital UPS bus, 1(2)D666, which meets the requirement that instrumentation be powered from a reliable source. The instrument readouts are real time and continuous. The instrumentation is required to be of Regulatory Guide 1.97 Type D, Category 2, design and qualification criteria. Additionally, the instrumentation should be energized from a high reliability power source, but not necessarily standby power, and should be backed up by batteries where momentary interruption is not tolerable. PLA-2222 (Reference 6.28), "Susquehanna Steam Electric Station Conformance to Regulatory Guide 1.97, Rev. 2", describes in Section 4.0 that the SBLC flow and level indication exceeds the range and meets the environmental gualification and power supply requirements for Type D, Category 2 instrumentation. The instrumentation is not required to be seismically qualified, per Regulatory Guide 1.97 Position 1.4.

(b) The licensee should provide the design-basis conditions for the component and the environmental and seismic conditions under which the component may be required to operate during a design basis accident. Environmental conditions include design-basis pressure, temperature, relative humidity and radiation fields. The staff reviewer will compare the environmental and seismic conditions associated with the design-basis accident to the conditions for which the component was designed to determine whether the component is capable of performing its intended function.

Environmental conditions, including design basis pressure, temperature, relative humidity and radiation fields are presented in Table 4.2.2 below. To provide a clear distinction of environmental conditions, the Normal Operation and DBA Columns have been split into a) conditions internal to the system and b) conditions external to the system. The seismic qualification for each component is discussed in Section 4.5.

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Table 4.2.2 - Component Design/Environmental Operating Conditions

Component	Location where Component Resides	Design Basis of Component (Conditions of Component as Part of the System)	Normal Operating Mode of Component (Conditions of Component during System Operation)	DBA Conditions of Component Operation
	•			
HS14804 (U1) HS24804 (U2) (Manual initiation switch)	Control Room (Not a harsh environment designation)	P = 14.7psia T = 75 F RH = 50% Rad = ≤ .5 mR/hr	P = 14.7psia T = 75 F RH = 50% Rad = ≤ .5 mR/hr	P = 14.7psia T = 75 F RH = 50% Rad = ≤ .5 mR/hr
1997 - 1997 -	Reference (6.29, 6.30)	Reference (6.29, 6.30)	Reference (6.29, 6.30)	Reference (6.29, 6.30, FSAR Sect. 6.4.4.1)
HV148F006 (U1)	Reactor Building EL 752'	P = 1203 psi T = 570 F	Injection time frame	Injection time frame
HV148F006 (U2)	Rooms I-506, II- 506	RH = N/A (water) Rad = ≥ 100 mR/hr	INSIDE SYSTEM P = Reactor static head to1203 psi	<u>INSIDE SYSTEM</u> P ≤56 psia
(First isolation	Reference (6.31,	Reference (6.31,	T = 70/570 F	T ≤340 F

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		Component	Location where Component Resides	Design Basis of Component (Conditions of Component as Part of the System)	Normal Operating Mode of Component (Conditions of Component during System Operation)	DBA Conditions of Component Opera	
		check valve)	6.32)	6.32, Sht. 9)	RH = N/A (water) Rad ≥ 100 mR/hr	RH = N/A (water) Rad ≥ 100 mR/hr	
	- -				EXTERNAL ENV. P ~ 14.7 psia T = 60/110 F RH = 20/80%	EXTERNAL ENV. P ~ 14.7 psia T = to 133 F RH = 100%	
					Rad = 10 R/hr	Rad = 6.2×10^4 R/	/hr
					Reference (6.31, 6.32, FSAR Table 9.3-11)	Reference (6.31, 6 FSAR Table 9.3-1	
		148F007 (U1) 248F007 (U2)	Drywell EL 739' Rooms I-400, II-	P = 1203 psi T = 570 F RH = N/A (water)	Injection time frame	Injection time fram	le
		(Check valve)	400 Reference (6. 33,	$Rad = \ge 100 \text{ mR/hr}$	P = Reactor static head to1203 psi	$P \le 56 \text{ psia}$ T = 340 F	
					· · · ·		

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· I	Component	Location where Component Resides	Design Basis of Component (Conditions of Component as Part of the System)	Normal Operating Mode of Component (Conditions of Component during System Operation)	DBA Conditions of Component Operation	
		34)	Reference (6.31, 6.32, Sht. 9)	T = 70/570 F RH = N/A (water) Rad = ≥ 100 mR/hr <u>EXTERNAL ENV.</u> P = 0.1-1.5 psig T = 90/150 F	RH = N/A (water) Rad = ≥ 100 mR/h EXTERNAL ENV. P ≤ 56 psia T ≤ to 340 F RH = 100%	
				RH = 20/90 % Rad = 26.25 R/hr	Rad = 7.1×10^6 R/hr	
				Reference (6.31, 6.33, FSAR Table 9.3-11, 6.40)	Reference (6. 33, FSAR Table 9.3-11)	
	148F008 (U1) 248F008 (U2)	Drywell EL 738' Rooms I-400, II- 400	P = 1203 psi T = 570 F RH = N/A (water) Rad = ≥ 100 mR/hr	Injection time frame INSIDE SYSTEM P = Reactor static	Injection time frame INSIDE SYSTEM P = to 56 psia	
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	Component	Location where Component Resides	Design Basis of Component (Conditions of Component as Part of the System)	Normal Operating Mode of Component (Conditions of Component during System Operation)	DBA Conditions of Component Opera
	(locked open gate valve)	Reference (6. 33, 34)	Reference (6.31, 6.32, Sht. 9)	head to1203 psi T = 70/570 F RH = N/A (water)	T = 85/95 F RH = N/A (water) Rad = ≥ 100 mR/r
				Rad = ≥ 100 mR/hr EXTERNAL ENV. P = 0.1-1.5 psig T = 90/150 F RH = 20/90 % Rad = 26.25 R/hr	$\frac{\text{EXTERNAL ENV.}}{\text{P} \le 56 \text{ psia}}$ $T \le \text{to 340 F}$ $\text{RH} = 100\%$ $\text{Rad} = 7.1 \times 10^6 \text{ R}$
				Reference (6.31, 6.33, FSAR Table 9.3-11, 6.40)	Reference (6. 33, FSAR Table 9.3-1
	1E219 (U1)	Reactor building	Tank Conditions	Tank Conditions	Tank Conditions
	2E219 (U2)	EL 749'		1	

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	Component	Location where Component	Design Basis of Component	Normal Operating Mode of	DBA Conditions of Component Operation
		Resides	(Conditions of	Component	
·			Component as Part of the System)	(Conditions of Component during System Operation)	
		· · · · · · · · · · · · · · · · · · ·			
· . ·	(10 kW heater		P = approx 10' water T = 85/95 F	P = approx 10' water	P = approx 10' wate T = 85/95 F
. •	inside SBLC tank)	Reference (6.32)	RH = N/A (water) Rad = 0.1 mR/hr	T = 85/95 F RH = N/A (water) Rad = 0.1 mR/hr	RH = N/A (water) Rad = 0.1 mR/hr
			OUTSIDE TANK P =25 inwg	OUTSIDE TANK	OUTSIDE TANK P ~ 14.7 psia
•					
			T = 60/100 F RH = 20/80%	P ~ 14.7 psia T = 60/100 F	T = 113 F RH = 100%
			RH = 20/80% Rad = 0.1 mR/hr		RH = 100% Rad = 100 R/hr
			RH = 20/80%	T = 60/100 F RH = 20/80%	RH = 100% Rad = 100 R/hr
	1E220(U1) 2E220(U2)	Reactor building EL 749' I-513, II-513	RH = 20/80% Rad = 0.1 mR/hr	T = 60/100 F RH = 20/80% Rad = 0.1 mR/hr Reference (6. 4,	RH = 100%

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	Component	Location where	Design Basis of	Normal Operating	DBA Conditions of
		Component Resides	Component	Mode of Component	Component Operation
		1,00,000	(Conditions of	Component	
			Component as Part of	(Conditions of	
			the System)	Component during System Operation)	
				•	
	(40 kW heater		T = 85/95 F	water	T = 85/95 F
	inside SBLC tank)	Reference (6.32)	RH = N/A (water) Rad = 0.1 mR/hr	T = 85/95 F RH = N/A (water)	RH = N/A (water) Rad = 0.1 mR/hr
		· · · · · · · · · · · ·		Bad = 0.1 mR/hr	
	· · · · · · · · · · · · · · · · · · ·		OUTSIDE TANK		OUTSIDE TANK
			P =25 inwg	OUTSIDE TANK	P ~ 14.7 psia
			T = 60/100 F	P ~ 14.7 psia	T = 113 F
			RH = 20/80%	T = 60/100 F	RH = 100%
			Rad = 0.1 mR/hr	RH = 20/80% Rad = 0.1 mR/hr	Rad = 100 R/hr
			Deference (6. 4. 6.22)		Reference (6. 4, 6.3
	·		Reference (6. 4, 6.32)	Reference (6. 4,	

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(c) The licensee should indicate whether the component was purchased in accordance with Appendix B to 10 CFR Part 50. If the component was not purchased in accordance with Appendix B, the licensee should provide information on the quality standards under which it was purchased. For the latter situation, information on the component would be reviewed by appropriate technical review branch responsible for the compo0nent, as requested by the lead SPSB reviewer.

Table 4.2.3 affirms the purchase requirement of the components under 10CFR50, Appendix B criteria and points to the reference where this is confirmed.

Component	Classification	Purchased in accordance with 10CFR 50, App. B	Where referenced
HS14804 (U1) HS24804 (U2)	Q	Yes	Reference (6.15, 6.34)
HV148F006 (U1) HV248F006 (U2)	Q	Yes	Purchase Spec. P-14A and Reference (6.15, 6.35)
148F007 (U1) 248F007 (U2)	Q	Yes	Purchase Spec. P-14BC and Reference (6.15, 6.36)

Table 4.2.3 – 10CFR50, Appendix B Requirement

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	148F008 (U1) 248F008 (U2)	Q	Yes	Purcha Spec. F and		
				Referer (6.15, 6		
	1E219 (U1) 2E219 (U2)	Q	Yes	Referer (6.15, 6		

(d) The licensee should provide the performance history of the component both at the licensee's facility and in industry databases such as EPIX and NPRDS. The staff reviewer will use this information to evaluate the reliability of the component relative to other components used in safety-related applications.

Yes

Reference

(6.15, 6.34)

Q

1E220 (U1)

2E220 (U2)

Information has been included in Attachments 2 and 3 of this calculation. The data in Attachment 2 is an extensive search of the EPIX and NPRDS data bases. Attachment 3 contains confirmation of Susquehanna's component operating history.

Other than routine maintenance on the Susquehanna specific components no failures have occurred. Similar results were obtained from the extensive search of EPIX and NPRDS data bases. Therefore, the equipment is reliable.

(e) The licensee should provide a description if its inspection and testing program including standards, frequency and acceptance criteria. The staff reviewer will use this information to evaluate the licensee's activities to monitor the component's performance at the facility. The information on the component would be reviewed by appropriate technical review branch responsible for the component, as requested by the lead SPSB reviewer.

In response to the above, Table 4.2.4 below summarizes the inspection and testing program for the SBLC System and components

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	Table	4.2.4 - Component Test	ing and Ins	pection Program	
					
r	r <u> </u>		T	Assessment Criteri	
Test/Inspection Procedure	Title	Purpose		Acceptance Criteri	a
Procedure				an a	
	1				
NO.					
NO.					
NO.					
NO. SUS-ISTPLN-	Pump and Valve	Unit 1&2 IST Pump a		As noted in Test	
	Inservice Inspection	Program establishes	testing	As noted in Test Requirements	
SUS-ISTPLN- 100.0		Program establishes requirements to asse	testing ess the		
SUS-ISTPLN- 100.0 SUS-ISTPLN-	Inservice Inspection	Program establishes requirements to asse operational readines	e testing ess the is of		
SUS-ISTPLN- 100.0	Inservice Inspection	Program establishes requirements to asso operational readines certain ASME Safety	e testing ess the s of y Class 1,		
SUS-ISTPLN- 100.0 SUS-ISTPLN-	Inservice Inspection	Program establishes requirements to asse operational readines certain ASME Safety 2, and 3 pumps and	e testing ess the s of y Class 1,		
SUS-ISTPLN- 100.0 SUS-ISTPLN-	Inservice Inspection	Program establishes requirements to asso operational readines certain ASME Safety	e testing ess the s of y Class 1, valves		
SUS-ISTPLN- 100.0 SUS-ISTPLN-	Inservice Inspection	Program establishes requirements to asse operational readines certain ASME Safety 2, and 3 pumps and that are required to: a. Shut down the to the safe shutdown	e testing ess the s of y Class 1, valves e reactor		
SUS-ISTPLN- 100.0 SUS-ISTPLN-	Inservice Inspection	Program establishes requirements to asse operational readines certain ASME Safety 2, and 3 pumps and that are required to: a. Shut down the to the safe shutdown condition,	e testing ess the s of y Class 1, valves e reactor		
SUS-ISTPLN- 100.0 SUS-ISTPLN-	Inservice Inspection	Program establishes requirements to asse operational readines certain ASME Safety 2, and 3 pumps and that are required to: a. Shut down the to the safe shutdown condition, b. Maintain the r	e testing ess the s of y Class 1, valves e reactor n reactor in		
SUS-ISTPLN- 100.0 SUS-ISTPLN-	Inservice Inspection	Program establishes requirements to asse operational readines certain ASME Safety 2, and 3 pumps and that are required to: a. Shut down the to the safe shutdown condition, b. Maintain the r the safe shutdown c	e testing ess the s of y Class 1, valves e reactor n reactor in		
SUS-ISTPLN- 100.0 SUS-ISTPLN-	Inservice Inspection	Program establishes requirements to asse operational readines certain ASME Safety 2, and 3 pumps and that are required to: a. Shut down the to the safe shutdown condition, b. Maintain the r	e testing ess the s of y Class 1, valves e reactor n reactor in		

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	Test/Inspection Procedure	Title		Purpose	Acceptance Criteria	U	n
	NO.						
			·	- <u>1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999</u>			
				Valves:			
				HV1(2)48F006:			
				Full Stroke Open – Once Every 92 d			
				Stroke Time Open - Once Every 92 d			
				Full Stroke Closed - Once Every 92 d			
				Stroke Time Closed - Once Every 92 d			
				Seat leakage test required 10 CFR 50 Appendix J –In accordance with owners program. Remote Position Indication Once every two years			·

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Da Da	ept ate esigned By G.Ko hecked By	wal	PROJECT Assessment of SE System for Suppre Pool pH Control		Calc. No. Rev. No. Sh. No.	EC-053- 		
T	Test/Inspection Procedure	Title		Purpose	· · · ·		Acceptance Criteria	Unit
	NO.							
							L	
ł				1(2)48F	007:			
				Full Stro Every 92	ke Open – (2 d	Dnce		
				Every 92	ke Closed - 2 d			
		•	. ·	Seat lea	kage test re 50 Appendi	quired by x J –In		
				accorda program	nce with ow	ners		
		· ·		1(2)48F		I*		
					Position Inc rery two yea		n an an Arrange ann a Arrange ann an Arrange	
	SO-153-003	24 - N Opera	Nonthly SBLC		enstrate all h unblocked		All heat traced piping demonstrated unblocked by	#1 v
	SO-253-003		~~		g from storag		pumping from storage tank	

Dept Date Designed By G.Kov Checked By	PROJECT Assessment of SB Aal_ System for Suppre		
Test/Inspection Procedure	Title	Purpose	Acceptance Criteria
NO.			
00.150.004		of SBLCI Systems pumps to individually provide required flow at a specific discharge pressure and fulfilling requirements of Station In- Service Test (IST) Program Plan quarterly testing 2) demonstrate proper opening and closing of SBLC Injection HV-148F006 3) demonstrate proper opening of Injection Check 148F007	Pump A/B Minimum Flow is ≥ 41.2 gpm with a Discharge Pressure of ≥ 1395 psig SBLC Pump A/B Flow within 41.2 and 44.3 gpm with Discharge Pressure within 1395 and 1405 psig
SO-153-004 SO-253-004	Quarterly SBLC Flow Verification	Demonstrate capability of Standby Liquid Control System pumps to individually	Pump A/B Minimum Flow is ≥ 41.2 gpm with a Discharge Pressure of ≥ 1395 psig
		provide required flow at a specified discharge pressure, fulfilling requirements of Station Inservice Test (IST)	SBLC Pump A/B Flow within 41.2 and 45gpm with Discharge Pressure within

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		PP&L CAL	CULATION SHEET		
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les Prot	Test/Inspection Procedure	Title	Purpose	Acceptance Criteria	Unit
10.	NO.				
				<u> </u>	
·			Program Plan quarterly testing and TS 3.1.7.	1395 and 1405 psig	
30-	SO-153-015	Two Year SBLC RPI Checks	Demonstrate proper operation of Remote Position Indicators	HV-148-F006 RPI CLOSED indication acceptable	#1
30-	SO-253-015		(RPI's) used in valve exercising testing as required once per two years by Station Inservice Testing (IST) Program Plan	Yes/No HV-148-F006 RPI INTERMEDIATE indication acceptable Yes/No HV-148-F006 RPI OPEN indication acceptable Yes/No	#2
				HV-148-F008 RPI CLOSED indication acceptable Yes/No HV-148-F008 RPI INTERMEDIATE indication acceptable Yes/No HV-148-F008 RPI OPEN indication acceptable	

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	PP&L CAL	CULATION SHEET		
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Test/Inspection Procedure	Title	Purpose	Acceptance Criteria	Uni
NO.				
			Yes/No	
SE-159-047	LLRT OF STANDBY	This procedure describes how	A Combined leak rate of less	#1
SE-159-047 SE-259-047	LIQUID CONTROL PENETRATION	This procedure describes how to perform the LLRT for the Standby Liquid Control	than or equal to 3.3 gpm (12,492 ccm) for all	#1
	NUMBER X-42 AND CHECK VALVE OPERABILITY TESTS	Penetration Number X-42. NDAP-QA-0412 outlines the frequency. Additionally, this	containment isolation valves in hydrostatically tested lines which penetrate the Primary	
		procedure covers 24 month check valve operability testing required by the ASME code per TS 5.5.6.	Containment, when tested at 1.10 P_a , 49.5 psig.	
		Confirm that check valve HV148F006 closes by		
		observing essentially restricted flow through HV148F006 to vent 148005.		
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1.2 				

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(f) The licensee should also indicate the potential compensating actions that could be taken within an acceptable time period to address the failure of the component. An example of a compensating action might be the ability to jumper a switch in the control room to overcome this failure. The staff reviewer will consider the availability of compensating actions and the likelihood of successful injection of the sodium pentaborate where non-redundant active components fail to perform their intended functions.

Compensating actions are discussed in the specific sections for the Hand Switch (HS 1(2)4804), Section 4.5.2, and replacement of the heating element in the Borated Water Storage Tank, Section 4.5.4.

4.3 All Active and Passive Components of the SBLC System

To obtain a complete listing of the SBLC System equipment and components, the SSES's Nuclear Information Management System (NIMS) (Reference 6.16) was queried. Out of a database of <u>381,572</u> pieces of equipment and components the search was narrowed to **373** components for the SBLC System. A copy of this data listing is included as Attachment No. 1. This data set was then reviewed in conjunction with the System P&ID (Reference 6.6) for components critical to the SBLC System function. These results are discussed in the subsequent Section 4.4.

4.4 Critical Components Subject to Single Failure Criteria

From the data listed in Attachment No. 1 and the System P&ID nineteen components in each unit's SBLC System were identified as being contributing to (or resulting) in potential single failure. These components are summarized in the following Table 4.4.1. A further assessment

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Keu Dy				Ontrol	SII. NO.	30- Ui	100
			· · · · · · · · · · · · · · · · · · ·			· · · ·	····
				TABLE	4.4.1		
		· · ·					
	SBLC	SYSTEM CO	MPONEN'	TS LIST CONTRIBUT	ING TO, OR RE	SULTING IN S	INGLE FAILURE
	_	·					
	N						SINGLE FAILUR
	0	COMP. ID.	SYST.	COMPONENT NAM	E / FUNCTION		CRITERIA
	 		NO.				COMPONENT
	·				TT 1		
					· · · · · · · · · · · · · · · · · · ·	· · · ·	· · · · ·
	1	148011	153A	SBLC INJECTION PUN			NO
	2	148F001	153A	SELC INJECTION PUN		K SUPPLY VLV	NÖ
	3	148F002A	153A	SELC INJECTION PUN			NO
	4	148F002B	153A	SBLC INJECTION PUN			NO
	5	148F003A 148F003B	153A 153A	SBLC INJECTION PUN			NO
	6	148F004A	153A	SBLC INJECTION PUN	ip b dischange vi	.v	NO NO
	8	148F004A	153A	SQUIB VALVE B			NO
· · ·	9	148F007	153A	CHECK VALVE			YES
	10	148F008	153A	STANDBY LIQUID COI	TROL INLISO VALV	/F	YES
	11	148F033A	153A	CHECK VALVE	THOE INDIGO TAL	<u></u>	NO
	12	148F033B	153A	CHECK VALVE			NO
	13	1E219	153A	SBLC STORAGE TANK	ELECTRIC HEATEL	AF	YES
	14	1E220	153A	SBLC STORAGE TANK			YES
	15	1P208A	153A	STANDBY LIQ CONTR			NO
	16	1P208B	153A	STANDBY LIQ CONTR	OL PUMP 'B'		NO
	17	1T204	153A	STANDBY LIQUID COI		ANK	NO (PASSIVE)
	18	HS14804	153A	SBLC MANUAL INITIA	TON SWITCH		YES
	19	HV148F006	153A	SBLC OB INJECTION	ALVE		YES
		· · · · · · · · · · · · · · · · · · ·	·	TR.	IT 2		
	1	248011	253A	SBLC INJECTION PUN			NO
	2	248F001	253A	SBLC INJECTION PUN		< SUPPLY VLV	NO
	3	248F002A	253A	SBLC INJECTION PUN			NO
	4	248F002B	253A 253A	SBLC INJECTION PUN		N	NO
	5	248F003A 248F003B	253A 253A	SBLC INJECTION PUN			NO
•	6	248F003B	253A 253A	EXPLOSIVE ACTUATE		v	NO NO
	8	248F004B	253A	EXPLOSIVE ACTUATE	ومريا المسجو المستحد والمراجع المتقاد المتقاد المتحاد والم		NO
	9	248F007	253A	CHECK VALVE		·····	YES
	10	248F008	253A	STANDBY LIQUID COM	TROL IN USO VALV	E	YES
	11	248F033A	253A	CHECK VALVE		-	NO
	12	248F033B	253A	SBLC PUMP 2P208B D	SCHARGE CKV		NO
	13	2E219	253A	SBLC STORAGE TANK	the second s	A	YES
	14	2E220	253A	SELC STORAGE TANK			YES
	15	2P208A	253A	STANDBY LIQ CONTR		·	NO
	16	2P208B	253A	STANDBY LIQ CONTR			NO
	17	27204	253A	STANDBY LIQUID COM		· · · · · · · · · · · · · · · · · · ·	NO (PASSIVE)
				SBLC MANUAL INITIAT		····	YES
	18	HS24804	253A	1 ODLO MAINUAL INITIAT			163

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of components in this table with respect to design attributes such as redundancy, single power source, interlocks and hand operation results in a further reduction to **six** potential single failure components for each unit. A summary Table 4.4.2 of these components is shown below, with the corresponding identification number from Table 4.1 above.

TABLE 4.4.2

Single Failure Criteria Components

N O	COMP. ID.	SYST. NO.	COMPONENT NAME / FUNCTION	SINGLE FAILURE CRITERIA COMPONENT/ ACTIVE (PASSIVE)
			UNIT 1	
	·····			
9	148F007	153A	CHECK VALVE	YES / ACTIVE
10	148F008	153A	STANDBY LIQUID CONTROL INJ ISO VALVE	YES PASSIVE
13	1E219	153A	SELC STORAGE TANK ELECTRIC HEATER A	YES / ACTIVE
14	1E220	153A	SELC STORAGE TANK ELECTRIC HEATER B	YES / ACTIVE
18	HS14804	153A	SELC MANUAL INITIATION SWITCH	YES / ACTIVE
19	HV148F006	153A	SBLC OB INJECTION VALVE	YES / ACTIVE
	· · · · · · · · · · · · · · · · · · ·			
			UNIT 2	
				· · · · · · · · · · · · · · · · · · ·
9	248F007	253A	CHECK VALVE	YES / ACTIVE
10	248F008	253A	STANDBY LIQUID CONTROL INJ ISO VALVE	YES / PASSIVE
13	2E219	253A	SBLC STORAGE TANK ELECTRIC HEATER A	YES / ACTIVEE
14	2E220	253A	SBLC STORAGE TANK ELECTRIC HEATER B	YES / ACTIVE
18	HS24804	253A	SBLC MANUAL INITIATION SWITCH	YES / ACTIVE
19	HV248F006	253A	SBLC OB INJECTION VALVE	YES / ACTIVE

The components shown in Table 4.4.2 fall under the definition of single failure criteria i.e., "an occurrence that results in the loss of capability of a component to perform its intended safety function." In order to take credit for the application of the SBLC System to the suppression pool pH function these components must be evaluated for their low risk failure probability and judged acceptable. This is done for each component including the guidelines (a)-(e) discussed in Section 4.1 above as well as, the following evaluation criteria:

- a) component's design (seismic, ASME, etc.), inspection and procurement program
- b) testing and maintenance program
- c) industry historical performance of these components
- d) SSES plant experience with these components
- e) power source

The argument and justification for the low risk of failure of each component is presented in detail in the following Section 4.5.

The arrument and inclification for the low rick of failure of each component is presented in

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4.5 Justification for Low Risk Failure Probability

The argument and justification for the low risk of failure of each component identified in Table 4.4.2 follows.

4.5.1 CHECK VALVE - 1(2)48F007⁽¹⁾

The possibility of SBLC System Isolation Check Valve 1(2)48- F007 having a single failure (fails closed-preventing flow) when called to service of system injection into the Reactor Vessel is evaluated consequently. The valve is a high reliability component whose potential failure is very low and this premise is justified below.

The objective argument against a single failure (fails closed) probability of the SBLC Injection check valve is based on the in-place safeguards and the quality applied to the valve's operation. First, the valve has been procured as ASME, Section III, Class 1 safety-related component, is periodically tested and inspected, and has demonstrated historical performance with no failures. Second, an extensive search of INPO (EPIX, NPRDS – Attachment No. 2) and Susquehanna (NIMS) databases revealed no failures (to open or close) of this and similar valves. The INPO, EPIX and NPRDS databases were searched on all BWR (including Susquehanna) plants on key words such as: Standby Liquid Control (SBLC), Maintenance Rule applicability and for the particular valve (by function, type and manufacturer). All records reviewed show only requirement for routine maintenance and minor correction to leak rate. The Susquehanna site system engineer likewise confirmed this result through in-plant performance history (Attachment No. 3).

The results of this evaluation show the potential for failure of the valve is very low based on the quality as established by the component's procurement as an ASME, Section III, Class 1 safety-related valve, its periodic testing and inspection (References 6.13 and 6.14), and historical performance of the component (NIMS Data Base Maintenance Record, INPO EPIX, NPRDS).

Table 4.5.1 further summarizes the important attributes, which serve as additional testimony of the valve's reliability against a potential single failure occurrence.

Terminology is used throughout to designate Unit #1 and #2 valves and components.

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TABLE 4.51

Valve Component Data Sheet

VALVE NO	1/0/48 5007	REFERENCES
ATTRIBUTE	1(2)48-F007	HEFERENCES
TYPE	Litte Obeel 11/ inch M Turne	
TYPE	Lift Check – 1 ½ inch Y Type	6.10
MANUFACTURER NORMAL OPERATION	Borg - Wamer Valve in closed position. Ultrasonic flow unit FE-1(2)4806 would indicate if valve fails closed on system start.	6.10 6.2, 6.3, 6.6, 6.13, 6.14
QUALITY ASSURANCE REQUIREMENT	YES 10CFR50, APPENDIX B	6.15, 6.16
Q CLASS	YES Quality Group A, per RG 1.26	6.15, 6.16
SAFETY CLASSIFICATION	1 - Per ANSI, N212	6.15, 6.16
ASME	ASME Section III, Class 1	6.15, 6.16
ASEC	III, NB	6.15, 6.16
MAINTENANCE RULE	YES	6.15, 6.16
SEISMIC CATEGORY	CATEGORY I, SSE	6.15, 6.16

Although, acknowledging that a single failure possibility exists to open the injection check valve, the above arguments accentuate that the potential for <u>failure is very low</u>. This is based on the quality as established by the valve's procurement as a safety-related valve, its testing and inspection and historical performance.

4.5.2 SBLC MANUAL INITIATION SWITCH, HS1(2)4804

As mentioned above, one of the two components identified, the main control room selector switch HS1(2)4804 is also considered for the single failure criteria. Similar to the check valve, the hand switch is likewise a high reliability component whose potential for failure is very low.

In the event that system operation is required, the operator must place Keylock Hand Switch HS-14804, SBLC MANUAL INITIATION on Panel 1C601 to the START position. This switch is of the maintained contact type, and in the START position, acts to close contacts that energize

In the quant that quatern energian is required, the energias must place Kaulook Hand Quitab

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both the "A" and "B" SBLC Pump start relays and the K2 and K6 relays. The pumps will continue to run until stopped by the Control Room operator.

The Hand Switch is a high reliability component at a very accessible location and whose failure is very unlikely. This switch is of the maintained contact type (passive) and is turned on manually. In case of remote possibility of failure of this switch, an available option allows access to the back panel where it could be easily replaced (or bypassed) in enough time to start system initiation.

Table 4.5.2 lists some important attributes, which serve as additional testimony of the switch's reliability against a potential single failure occurrence.

TABLE 4.5.2

Key Locked Hand Switch Component Data Sheet

VALVE NO ATTRIBUTE	HS1(2)4804	REFERENCES
TYPE	Key Locked Hand Switch	6.6, 6.16
MANUFACTURER	General Electric	6.7
NORMAL OPERATION	Maintained contact type switch. Operator must place switch on Panel 1(2)C601 to the START position to energize relays to start pumps.	6.2, 6.3, 6.16
EQ	NO	6.15, 6.16
QUALITY ASSURANCE REQUIREMENT	YES 10CFR50, APPENDIX B	6.15, 6.16
Q CLASS	YES Quality Group A, per RG 1.26	6.15, 6.16
SAFETY CLASSIFICATION	1 - Per ANSI, N212	6.15, 6.16
ASME	No	6.15, 6.16
ASEC	No	6.15, 6.16
MAINTENANCE RULE	YES	6.15, 6.16
SEISMIC CATEGORY	CATEGORY I, SSE	6.15, 6.16

The results show the Hand Switch HS 1(2)4804 is a high reliability component, at a very accessible location and whose failure is very improbable and would not prevent the SBLC System from performing its intended function.

The results show the Hand Switch HS 1(2)4804 is a high reliability component, at a very

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4.5.3 <u>STANDBY LIQUID CONTROL INJ ISO VALVE - 1(2)48F008;</u> <u>SBLC OB INJECTION VALVE</u> <u>HV1(2)F006</u>

The possibility of SBLC System Isolation Valves HV 1(2)48-F006 and 1(2)48-F008 experiencing a single failure (fail closed) when called to service is evaluated consequently. Even though the single failure criteria applies to the containment isolation valves, the valves are very high reliability components whose potential failure is very small.

The objective argument against a single failure (fails closed) probability of the SBLC Injection valves is based on the in-place safeguards and the quality applied to the valves' operation. First, the valves have been procured as ASME, Section III, Class 1 safety-related, are periodically tested and inspected, and have demonstrated historical performance of their reliability. Second, from safety consideration, valve HV-1(2)48F006 has a keylock switch and will annunciate on Control Panel C601 if the switch is in CLOSE position or if the valve is NOT FULLY OPEN. Similarly, valve 1(2)48-F008 is LOCKED OPEN and its' position indication is shown on Control Panel C601.

A detailed search of the NIMS Data Base shows only routine maintenance requirement of the valves and minor corrections to instrumentation. There has not been an incident where either valve closed spuriously or had a false indication of being open or closed.

The results of this evaluation show the potential for failure of the valve is very low based on the quality as established by the component's procurement as an ASME, Section III, Class 1 safety-related valve, its periodic testing and inspection (References 6.13, 6.14), and historical *performance* of the component (NIMS Data Base Maintenance Record and INPO - EPIX, NPRDS).

Table 4.5 further summarizes the important attributes, which are additional proof of the valves' reliability and safety against a single failure occurrence.

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)esigned Checked		system for Suppression ool pH Control	Sh. No. 42- of	13 8 —
		TABLE	4.5.3	· · · · · · · · · · · · · · · · · · ·
	VALVE NO ATTRIBUTE	HV 1(2)48-F006	1(2)48-F008	REFERENCES
	ТҮРЕ	YARWAY- 1 1/2" MOV	Borg-Warner - 1 1/2* GT	6.7, 6.20, 6.21
	NORMAL OPERATION	Position Switch ZS-12. Alarm if valve not fully open (AR-107-D03). Displayed on 1(2)C601 Powered by 1(2)B236.	Locked open manual injection. Position indication displayed on 1(2)C601. Powered by 1(2)Y216.	6.4, 6.6, 6.7, 6.11, 6.12
	QUALITY ASSURANCE REQUIREMENT	YES 10CFR50, APPENDIX B	YES 10CFR50, APPENDIX B	6.15, 6.16
	Q CLASS	YES Quality Group A, per RG 1.26	YES Quality Group A, per RG 1.26	6.15, 6.16
	SAFETY CLASSIFICATION	1 - Per ANSI, N212	1 - Per ANSI, N212	6.15, 6.16
	ASME	ASME Section III, Class 1	ASME Section III, Class 1	6.15, 6.16
	ASEC	III, NB	III, NB	6.15, 6.16
	MAINTENANCE RULE	YES	YES	6.15, 6.16
	SEISMIC	CATEGORY I, SSE	CATEGORY I, SSE	6.15, 6.16

Acknowledging the possibility of a single failure to close one of the two SBLC injection valves, the above argument accentuates that the potential for fallure is very low. This is based on the quality as established by the valves' procurement as safety-related valves, their testing and inspection, and their historical performance.

4.5.4 SBLC STORAGE TANK ELECTRIC HEATERS A, B - 1(2)E219, 1(2)E220

Table 4.4.2 also lists SBLC Storage Tank Heater A (1(2)E219) and Heater B (1(2)E220) as potential components for single failure. Their function is maintaining a minimum storage tank temperature to prevent the sodium pentaborate solution from precipitating out of solution; thereby, rendering the system incapable of performing its design functions. The heaters are active components and are somewhat redundant which is best explained by their respective function. Storage tank heater "A" is a 10 kW heater powered from 480 VAC MCC 1(2)B236. This heater operates to automatically maintain solution temperature above the precipitation point, and can be removed for maintenance/replacement without draining the storage tank. active components and are somewhat redundant which is best explained by their respective

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Storage Tank Heater "B" is used to elevate the temperature during chemical addition to increase the solubility of the sodium pentaborate in water. This is necessary because the mixing of sodium pentaborate and water is an endothermic reaction, which draws heat from the system. This heater is a 40 kW heater powered from 480 VAC MCC 1(2)B236.

As is evident above, the single failure criteria impacts the heaters since they are powered from the same power source i.e., 480 VAC MCC 1(2)B236.

Since regulatory criteria dictate that SBLC System initiation post LOCA is completed by 24 hours, an option is available for supplying power to the heaters from Diesel Generator A or C (References 6.8 and 6.9) on loss of the AC Bus. However, should backup power not be available for the first 24 hours, the need for maintaining the minimum storage tank temperature is still necessary to prevent sodium pentaborate from precipitating out of solution; thereby rendering the system not applicable of performing the AST function. Therefore, a calculation was performed to determine the transient cool-down rate of the tank's inventory over a 24 hour period with the heaters off. The solution temperature at 24 hours confirmed it is still within design limits.

The stepped approach of the Calculation is presented as follows:

Assumptions/Input:

Input data for the Storage Tank's normal operating temperature limits were obtained from References 6.2 through 6.5. These were used in setting the initial conditions.

- With the heater control switch in AUTO, the 'A' heater is controlled by a temperature indicating controller to maintain tank temperature between <u>85°F and 95°F</u>.
- The high temperature alarm activates at a tank temperature of 110°F, increasing and the low temperature alarm activates at 80°F, decreasing. The low temperature alarm set at 80°F ensures action can be taken prior to tank temperature decreasing below the saturation temperature of the solution.
- Technical Specification 3.1.7 requires a minimum sodium pentaborate concentration of 18.
 6 weight percent limit. From Figure 3.1.7.2 of the Technical Specification at that concentration an acceptable operating range temperature of 66°F is required.

The SBLC Storage Tank geometry and dimensions were obtained from Reference 6.22.

It was determined a standard electrical analogy method for transient conduction is applicable for this situation. Equations and parameters used were obtained from Reference 6.23, Sections 34 and 35.

The tank's sodium pentaborate solution was assumed to have properties of ordinary water.

Sections 34 and 35.

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		······		
Methodology:				
	e input and assumptions, con			
	perature decay (cool-down) in loss of both heaters.	the Standby Li	quid Control S	System Storage 1
in the event of	USS OF DUIT HEATERS.			
	etry and dimensions of the tar		analysis is illu	strated in the ske
below: Data is	obtained from References 6.2	2 and 6.41.		
		······································		
		· · · ·	Took	ID = 9 ft
	9.0	•	•••	OD = 9.03 ft
	ζ	•	•	
· · ·				thickness = $3/16^{\circ}$
	•			r level = 4587 ga
				5.6" = 9.63 ft (low)
-		12.0'		r level = 4897 ga
		·		3.5" = 10.3 ft (high
			Tank	insulation = 1"
		· [Calcium silicate
	-SBLC STORAGE TANK		•- ;	
		••••••••••••••••••••••••••••••••••••••	*. • .	
Second the an	proach referenced for transien	t conduction is	obtained from	n Reference 6 23
	w. The method used to deten			
	ped Parameter Electrical Anal			
	peu Falamele: Liecuical Ana		ILTIS UBSCIL	
tank is the Lum				
		AAV METUA	`	
	AMETER ELECTRICAL ANAL	OGY METHOD	<u>)</u>	
LUMPED PAR	-	OGY METHO	<u>)</u>	
LUMPED PAR	AMETER ELECTRICAL ANAL (OGY METHOD	<u>)</u>	(1)
$\frac{\text{LUMPED PAR}}{T_t = T_{\bullet} + (T_o - T_o)}$	「₌) exp (-t/C _e R _e)	<u>OGY METHOI</u>	<u>2</u>	(1)
$\frac{\text{LUMPED PAR}}{T_t = T_{\bullet} + (T_o - T_o)}$	-	<u>OGY METHOI</u>	<u>2</u>	(1)

 $R_e = 1 / hA_s$

 T_t = medium temperature at time ~t, °F T_o = initial medium temperature, °F

 T_∞ = bulk outside ambient temperature, °F

 T_t = medium temperature at time ~t, °F

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<u></u>		·		
	$T_s = surface temperature k = thermal conductivity,$	•		
	t =time, hr ρ = mass density, lb/ft3	= 62.3	·	
	C_p = specific heat, Btu/lb L_c = characteristic length V = volume, ft ³		A _s)	
	$A_s = surface area, ft^2$	- #2 OF	• • • •	
	h = film coefficient, Btu/($l = 0.29{(T_s - T_s)/L_c}^{0.2}$ for GrPr = 10 ⁴ to 10 ⁹)		Il cylinder geo	metry), (applicable
	nation of the Rayleigh Numbe I the cylinder film coefficient.	er (GrPr produc	t) has to be m	ade in order to

The Prandtl Number is defined as follows:

 $Pr = c_p \mu/k$

Where $\mu = viscosity$, lb/hr-ft

And the Grashof Number is,

 $\begin{aligned} Gr &= (L_c^3 g \beta \rho^2 \ (T_s - T_\infty)) / \mu^2 \\ \text{Where } g &= \text{gravitational acceleration, ft/hr}^2 \\ \beta &= \text{volumetric coefficient of expansion, 1/ °R} \end{aligned}$

Assuming conservative conditions for $T_s = 95^{\circ}F$ and $T_w = 60^{\circ}F$, the Grashot Number is conservatively determined using T_w (60°F), (Reference 6.23, Appendix 35.C)

Pr = 0.72 $g\beta\rho^2/\mu^2 = 2.58 \times 10^6$ (interpolated) $L_c^3 = (V/A_s)^3 = (\pi r^2 h/2\pi rh)^3 = (r/2)^3 = ((9.03 \text{ ft}/2)/2)^3 = 11.5 \text{ feet}^3$

Note that the surface area of the top and bottom of the tank are neglected. The bottom of the tank is connected to concrete and will insulate the tank from heat loss. Additionally, the water does not go to the top of the tank therefore the inside lid of the tank will be exposed to air. The heat transfer through the lid will be very small and is neglected.

Therefore, the Rayleigh Number (GrPr product) is,

 $GrPr = 11.5x(2.58 \times 10^{6})x(95 - 60)x 0.72 = 7.48 E+08$

Therefore, the Rayleigh Number (GrPr product) is,

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	n to confirming the Rayleigh numbe irmation is performed below.	r, Reference 6.	23 states that $d/L \ge 35/(Gr$) ^{0.25}
9.03/2.26	$\geq 35/(1.04 \times 10^9)^{0.25}$ OR $4.0 \geq 0.25$	2		
Which sa	tisfies the criteria of using the above	film coefficien	l: 0.29{(T₅ - T₅)/L _c } ^{0.25}	
	Equation 1 above i.e., $T_t = T_m + (T_o - t_c)$ ic study of the tank temperature with			t, a
From abc	we.	· .		
$C_e = c_p \rho V$ $R_e = 1 /hA$				
The follow	ing range of values were used in the	analysis,		
= ra	itial medium (sodium pentaborate) t ange of 95°F to 80°F (95°F taken co mperature)			ıg
	ulk outside ambient temperature, °F ange of 80°F to 60°F (assumed)			
V = mi = 6	nimum volume, ft ³ = 4587 gal x 0.13 13 ft ³	1368 ft ³ /gal (see	above calculation and ske	ətch
Note the to be c	ne minimum tank volume was conse ooled.	ervatively used	since it lowers the amount	of r
	urface area, ft ² = 6.28x4.515′x9.633 73 ft ²	(see above o	alculation and sketch abo	ve)
(the r	$29{(T_s - T_s)/L_c)}^{0.25}$ (Var nedium temperature is assumed to a constant heat transfer coefficient	be the surface	• •	1e ci
Therefore	, substituting values			
$C_e = c_p \rho V$	= (0.999) (62.3) (613) = 38,151			
I neretore	, substituting values	•		

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Or	/ (0.29{(T _s - T _*)/L _c)} ^{0.25}) (273) s - T _*)/2.26) ²⁵ = 1/64.6(T _s - T _* 51)(0.0155(T _s - T _*) ^{-0.25}) = 591		- T _*)/ L _c)] ^{0.25} T _s - T _*) ^{-0.25}	
$\mathbf{U}_{\mathbf{g}} \times \mathbf{n}_{\mathbf{g}} = (30, 1)$	$51/(0.0155(1_8 - 1_8)) = 551$.∪(s ⁻ <i>n)</i>		
Substituting the	above parameters into Equation	on 1,		
$T_t = T_{\infty} + (T_o - T_{o})$	-) exp (-t/C _e R _e)			
= T₌ + (T₀ - 1) exp (-t / (591.3 / (T _s - T) ^{0.4}	²⁵)		
= T _⊷ + (T _o - T	·•) exp (-t(.00169({(T₅ - T∞)} ^{0.2}	⁵)))		(2)
Equation (2) ab the transient filr	ove was used to produce the n coefficient.	transient result	is of temperat	ure in the tank using
	cases the tank insulation was ature decrease.	s conservatively	y neglected si	nce the insulation wil

4.5.4.1 Constant Heat Transfer Coefficient Analysis:

Given the uncertainty of the air flow patterns around the tank a case was run with a constant heat transfer coefficient. A value of 6.0 Btu/hr ft² °F was chosen since it is representative of a heat transfer coefficient for a 15 mph wind speed. This value will obviously bound any conditions that would exist in the reactor building.

The calculation was performed in a manner similar to the methodology described above except the value of Re simply became

 $R_e = 1/hA_s = 1/(6)(273) = 6.105 \times 10^{-4}$

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A number of parametric runs were performed for the variable input values discussed in Section 4.5.4 above. The results were generated using an EXCEL spreadsheet and are presented below in Table 4.5.4. The spreadsheet results are included as Attachment 5. Table 4.5.4 results use the variable (h) and a constant (h) = 6.0 Btu/hr-ft². Only the two most challenging cases are presented.

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TABLE 4.5.4 -Cool-down Temperatures Using a Variable and Constant(h)

TIME	Variable (h)	Constant (h)
in∧⊑ (hr)	80 Inside ,	(h = 6.0) 80 Inside ,
(in)	60 Outside	60 Outside
		60 Outside
0	80	80
0.5	79.96429	79.57518
1	79.92868	79.15938
1.5	79.89316	78.75241
2	79.85774	78.35409
2.5	79.82242	77.96422
3	79.78718	77.58264
3.5	79.75204	77.20917
4	79.717	76.84363
4.5	79.68205	76.48585
5	79.64719	76.13567
5.5	79.61242	75.79293
6	79.57774	75.45747
6.5	79.54316	75.12913
7	79.50867	74.80777
7.5	79.47427	74.49324
8	79.43996	74.18539
8.5	79.40574	73.88407
9	79.37161	73.58916
9.5	79.33757	73.30051
10	79.30362	73.01799
11	79.23566	72.47083
12	79.16836	71.94667
13	79.10141	71.44453
14	79.03481	70.96351
15	78.96855	70.5027
16	78.90264	70.06126
17	78.83707	69.63837
18	78.77184	69.23326
19	78.70695	68.84518
20	78.6424	68.4734
21	78.57817	68.11726
22	78.51428	67.77608
23	78.45072	67.44924
24	78.38748	67.13614

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5.0	rapid cool down Technical Specif RESULTS Acknowledging	ve that the initial and outside ten occurs with the assumption of a lication limit (66 ^o F) is not excer that a single failure of one o bove arguments accentuate t	a constant film con eded over the enti f the component	efficient (h = 6. re 24 hours wi ts listed in Tal	0). However, the th either coefficient. ble 4.4.2 is remote	
	based on the q their testing an	uality as established by the o d inspection, their historical p edundant power sources.	components' pro	curement as	safety-related valv	
	based on the q their testing an	uality as established by the o d inspection, their historical p	components' pro	curement as	safety-related valv	

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			<u> </u>		
6.0	REFERENCES				:
6.1		native Radiological Source Te		ating Design Bas	is Accidents at
		Reactors", Regulatory Guide,			
6.2		"Standby Liquid Control", Sys		Student Text, Ho	ev. U3, 4/25/02.
6.3		dby Liquid Control System", R			_
6.4		RD, SLC, DRYWELL SUMPS		Inclator Procedur	е.
6.5		andby Liquid Control System		and BA	
6.6		18, "Unit 1 P&ID, Standby Liqu			
6.7	17	5, Sht.3, 4, 7, 8, Schematic D			
6.8	30.	50, Sht. 1, Susquehanna S.E.		- · · ·	
6.9	Drawing D10715 Systems*, Unit 1	59, Sht. 1, "Single Line Meter 6 & 2,Rev. 23.	& Relay Diagr	am , 125VDC, 25	0VDC & 120V/
6.10		70, Sh. 1001, "Valve Assemb	ly lift Check -	1 1/2 inch Y Type	e." Borg - Warn
	Corp.				•
U .11		3-0011, "Standby Liquid Cont	rol System". E	lectrical, Rev. 7.	
6.12		3-0013, "Standby Liquid Cont			
6.13		Month SBLC Operability", Re			•••••
6.14		uarterly SBLC Flow Verification		· · · · ·	÷
6.15		tation FSAR Table 3.2-1.	,		
6.16		tation Nuclear Information Ma	nagement Sv	stem (NIMS).	
6.17		tation Site Performance & Ma			gineer Ian C.
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6.19	Deleted.				
6.20		FF110470), "Valve Assembly	- 1 1/z inch Ga	ate. Cres." Borg -	Warner Corp.
6.21		40, Sht. 1001,"1 1/2" Yarway			
		heck Design." Rev. 8.	· · ·		
6.22		10, Sh. 2801, 2802, Standby	Liquid Contro	Storage Tank. G	ieneral Electric
÷.	Co.	······································		. .	
6.23		el R., "Mechanical Engineering	Reference Ma	anual for the PE E	xam".
		Professional Publications. Inc.			
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6.25		5, Sht. 2, "Emerg. Core Clg. I			, .
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6.27		-31, "FCOStandby Liquid Co			
28		formance to Regulatory Guide			
0.29		30-1007, "Transient Temper			
LJ	Accident Condit	· · · ·			
6.30		"Shielding and Radiation Zoni	na Drawina	Control Building	L 729'-1"
<u> </u>	NIMS Data Base	•	ng bioming, C	Since Building, B	
9 .31	Calculation FC-	,)30-1007, "Transient Temper	ature Respon	se of CS with HV	AC - Normal a
. 29	valculation EU-L	Nou-Tour, Transient Temper	aiure nespon		

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6.32	•	5, Sheet 9, "SSES Unit 1& 2 F	Reactor Buildin	g Equipment	Qualification Harsh
0.00	Environment Zor		Drimon Contair	ment Caulor	east Qualification
6.33	Harsh Environm	5, Sheet 1, "SSES Unit 1& 2 F nent Zones	mary Contair	iment Equipri	nent Qualification
6.34	General Electric	's "Nuclear Products Quality	Assurance Mai	nual".	
6.35	Yarway's "Nucle	ar Products Quality Assuran	ce Manual"		
6.37	Borg-Warner's "	Nuclear Products Quality Ass	surance Manua	f ^o	
1 St. 1997	Drawing J-653.	Sheet 53, Rev. 7, "SBLC Sto	rage Teek		
6.38			rage rank.		
6.38 6.39	Email from Ian M			n and measur	ement of the
6.38 6.39		Aissien (site engineer) based		n and measur	ement of the
6.39	insulation thickn	Aissien (site engineer) based ess.	on a walkdowr		
	insulation thickn Calculation EC-	Aissien (site engineer) based	on a walkdowr alification Radi	ation Doses f	or Selected Zones

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ATTACHMENT NO. 1

SBLC UNIT 1 AND UNIT2 COMPONENT LIST

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SLC STANDBY LIQUID CONTROL COMPONENT LIST

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COMPONENT	SYST NO.	SÝSTEM	UNIT NO
NXL01-U1	153	SLC STANDBY LIQUID CONTROL	
FO14813	153	SLC STANDBY LIQUID CONTROL	
FO14814	153	SLC STANDBY LIQUID CONTROL	
FV14814	153	SLC STANDBY LIQUID CONTROL	
NXF01-U1	153	SLC STANDBY LIQUID CONTROL	
148013	153	SLC STANDBY LIQUID CONTROL	
SPDCB101H23	153A	ISLC STANDBY LIQUID CONTROL	
148F002A	153A	SLC STANDBY LIQUID CONTROL	
	153A		
148F014			
FI14814	153A	SLC STANDBY LIQUID CONTROL	
HSS14802	153A	SLC STANDBY LIQUID CONTROL	
JBD-178	153A	SLC STANDBY LIQUID CONTROL	_
LIC411R601	153A	SLC STANDBY LIQUID CONTROL	
PIC411R003	153A	SLC STANDBY LIQUID CONTROL	
SPJCD107H9	153A	SLC STANDBY LIQUID CONTROL	· · · ·
SPDCB101H2015	153A	SLC STANDBY LIQUID CONTROL	
SPHCB105H2001	153A	SLC STANDBY LIQUID CONTROL	
1T207A	153A	SLC STANDBY LIQUID CONTROL	
SPDCA106H19	153A	SLC STANDBY LIQUID CONTROL	
PI148R003-R2	153A	SLC STANDBY LIQUID CONTROL	
1T207B	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H17	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H2010	153A	SLC STANDBY LIQUID CONTROL	
148F002B	153A	SLC STANDBY LIQUID CONTROL	
148F003B	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H2	153A	SLC STANDBY LIQUID CONTROL	
HCB105H9	153A	SLC STANDBY LIQUID CONTROL	1
148015	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H31	153A	SLC STANDBY LIQUID CONTROL	
SPHCD131H3	153A	SLC STANDBY LIQUID CONTROL	
		SLC STANDBY LIQUID CONTROL	
SPJBD1045H2000	153A		
SPJCD107H10	153A		
C-PI148207B-	153A	SLC STANDBY LIQUID CONTROL	
148005	153A		
HCB105H2	153A	SLC STANDBY LIQUID CONTROL	
DCA-106	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H29	153A		
.G14803	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H14	153A		
<u>S14806</u>	153A	SLC STANDBY LIQUID CONTROL	
AHL14810	153A	SLC STANDBY LIQUID CONTROL	
SPHBD101H2008	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H6	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H36	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H2050	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H2012	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H20	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H16	153A	SLC STANDBY LIQUID CONTROL	
ISHL14812	153A	SLC STANDBY LIQUID CONTROL	
DCB-101	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H44	153A	SLC STANDBY LIQUID CONTROL	
ICB105H8	153A	SLC STANDBY LIQUID CONTROL	
IS14808B	153A	SLC STANDBY LIQUID CONTROL	
10148F006/ACT	153A	SLC STANDBY LIQUID CONTROL	

 HS14808B
 153A
 ISLC STANDBY LIQUID CONTROL

 HV148F006/ACT
 153A
 ISLC STANDBY LIQUID CONTROL

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PI148R003-R1	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H1	153A	SLC STANDBY LIQUID CONTROL	······································
HCB105H1	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H34	153A	SLC STANDBY LIQUID CONTROL	
FI14806	153A	SLC STANDBY LIQUID CONTROL	
SPJBD1045H2001	153A	SLC STANDBY LIQUID CONTROL	
XY14806	153A	SLC STANDBY LIQUID CONTROL	
148010	153A	SLC STANDBY LIQUID CONTROL	
148F031	153A	SLC STANDBY LIQUID CONTROL	
1E219	153A	SLC STANDBY LIQUID CONTROL	
DCA-206	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H32	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H24	153A	SLC STANDBY LIQUID CONTROL	······
1P208B	153A	SLC STANDBY LIQUID CONTROL	
148F017	1153A	SLC STANDBY LIQUID CONTROL	
148F015	153A	SLC STANDBY LIQUID CONTROL	
TSHLC411N003	153A	SLC STANDBY LIQUID CONTROL	
TEC411N006	153A	SLC STANDBY LIQUID CONTROL	. 4
SPHCD131H1	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H4	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H33	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H11	153A	SLC STANDBY LIQUID CONTROL	
SPDCA106H8	153A	SLC STANDBY LIQUID CONTROL	-
SPDCA106H17	153A	SLC STANDBY LIQUID CONTROL	
148016	153A	SLC STANDBY LIQUID CONTROL	1
TSHL14810	153A	SLC STANDBY LIQUID CONTROL	1
SPDCB101H7	153A	SLC STANDBY LIQUID CONTROL	
	153A	SLC STANDBY LIQUID CONTROL	
HS14806 SPDCB101H21	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H2016	153A	SLC STANDBY LIQUID CONTROL	1
SPDCB101H2016		SLC STANDBY LIQUID CONTROL	
	153A 153A	SLC STANDBY LIQUID CONTROL	
PI148207A			
JBD181H1	153A		1
JBD-1045	153A		
HS14804	153A	SLC STANDBY LIQUID CONTROL	1
HCB105H4	153A	SLC STANDBY LIQUID CONTROL	1
FT14806	153A	SLC STANDBY LIQUID CONTROL	1
DCB-201	153A	SLC STANDBY LIQUID CONTROL	1
1T203	153A	SLC STANDBY LIQUID CONTROL	1
1 <u>E220</u> 148F033A	153A 153A	SLC STANDBY LIQUID CONTROL	1
XYC411M600A		SLC STANDBY LIQUID CONTROL	
	153A	SLC STANDBY LIQUID CONTROL	1
148012	153A	SLC STANDBY LIQUID CONTROL	1
HV148F006	153A	SLC STANDBY LIQUID CONTROL	1
FICC411R004	153A	SLC STANDBY LIQUID CONTROL	1
148F003A	153A	SLC STANDBY LIQUID CONTROL	1
148F001	153A	SLC STANDBY LIQUID CONTROL	1
148009	153A	SLC STANDBY LIQUID CONTROL	1
48008	153A	SLC STANDBY LIQUID CONTROL	1
148002	153A	SLC STANDBY LIQUID CONTROL	1
ricc411R002	153A	SLC STANDBY LIQUID CONTROL	1
E14810	153A	SLC STANDBY LIQUID CONTROL	1
SPHCD131H2	153A	SLC STANDBY LIQUID CONTROL	. 1
SPHCB105H4	153A	SLC STANDBY LIQUID CONTROL	1
	153A	SLC STANDBY LIQUID CONTROL	<u>t</u>
SPDCB101H2008	153A	SLC STANDBY LIQUID CONTROL	1
HS14808A	153A	SLC STANDBY LIQUID CONTROL	1



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PI148207B	153A	SLC STANDBY LIQUID CONTROL	
SPDCA106H2005	153A	SLC STANDBY LIQUID CONTROL	
SPHCB105H3	153A	SLC STANDBY LIQUID CONTROL	
PSV148F029A	153A	SLC STANDBY LIQUID CONTROL	
ZS14808L	153A	SLC STANDBY LIQUID CONTROL	· ·
148003	153A	SLC STANDBY LIQUID CONTROL	
SPDCA106H14	153A	SLC STANDBY LIQUID CONTROL	
148F004B	153A	SLC STANDBY LIQUID CONTROL	
148F024	153A	SLC STANDBY LIQUID CONTROL	
SPDCA106H35	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H10	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H22	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H5	153A	SLC STANDBY LIQUID CONTROL	
C-PI148207A-	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H2013	153A	SLC STANDBY LIQUID CONTROL	
148018	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H15	153A	SLC STANDBY LIQUID CONTROL	
148F012	153A	SLC STANDBY LIQUID CONTROL	
E14806	153A	SLC STANDBY LIQUID CONTROL	
48F033B	153A	SLC STANDBY LIQUID CONTROL	
48F021	153A	SLC STANDBY LIQUID CONTROL	
48F018	153A	SLC STANDBY LIQUID CONTROL	
48017	153A	SLC STANDBY LIQUID CONTROL	
KA14804	153A	SLC STANDBY LIQUID CONTROL	
PCV14811B	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H18	153A	SLC STANDBY LIQUID CONTROL	
PIC411R600	153A	SLC STANDBY LIQUID CONTROL	
SPDCA106H2006	153A	SLC STANDBY LIQUID CONTROL	
PT148N004-R2	153A	SLC STANDBY LIQUID CONTROL	
PT148N004-R1	153A	SLC STANDBY LIQUID CONTROL	
AHL14801	153A	SLC STANDBY LIQUID CONTROL	
P208A	153A	SLC STANDBY LIQUID CONTROL	
148F026	153A	SLC STANDBY LIQUID CONTROL	
148F025	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H8	153A	SLC STANDBY LIQUID CONTROL	
IC411R001	153A	SLC STANDBY LIQUID CONTROL	
SV148F029B	153A	SLC STANDBY LIQUID CONTROL	
48004	153A	SLC STANDBY LIQUID CONTROL	
PCV14811C	153A	SLC STANDBY LIQUID CONTROL	
AHL14803	153A	SLC STANDBY LIQUID CONTROL	
SPHCB105H2	153A	SLC STANDBY LIQUID CONTROL	
SPHCB105H1	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H28	153A	SLC STANDBY LIQUID CONTROL	
PCV14811A	153A	SLC STANDBY LIQUID CONTROL	
SPDCA106H10	153A	SLC STANDBY LIQUID CONTROL	
T204	153A	SLC STANDBY LIQUID CONTROL	· ·
E14812	153A	SLC STANDBY LIQUID CONTROL	
BD-181	153A	SLC STANDBY LIQUID CONTROL	
ICB105H11	153A	SLC STANDBY LIQUID CONTROL	
48F016	153A	SLC STANDBY LIQUID CONTROL	
48F011	153A	SLC STANDBY LIQUID CONTROL	
48F008	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H19	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H19	153A	SLC STANDBY LIQUID CONTROL	
SPHCB105H2002	153A	SLC STANDBY LIQUID CONTROL	
SHLC411N600	153A	SLC STANDBY LIQUID CONTROL	
ICD-131	153A	SLC STANDBY LIQUID CONTROL	· · ·

HCD-131 153A SLC STANDBY LIQUID CONTROL

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HCB105H7 SPDCB101H9	153A 153A	SLC STANDBY LIQUID CONTROL	<u> </u>
HCB-105	153A	SLC STANDBY LIQUID CONTROL	
		SLC STANDBY LIQUID CONTROL	
LI/FI14806	153A 153A		
148019 SPDCA106H16	153A	SLC STANDBY LIQUID CONTROL	·
and the second			
XYC411M600B	153A	SLC STANDBY LIQUID CONTROL	
HCB105H3	153A	SLC STANDBY LIQUID CONTROL	····
SPHCB105H2000	153A	SLC STANDBY LIQUID CONTROL	·
SPDCB101H40	153A	SLC STANDBY LIQUID CONTROL	· · · · · · · · · · · · · · · · · · ·
SPDCB101H3	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H2014	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H2002	153A	SLC STANDBY LIQUID CONTROL	·
SPDCB101H1000	153A	SLC STANDBY LIQUID CONTROL	
PTC411N004	153A	SLC STANDBY LIQUID CONTROL	
148011	153A	SLC STANDBY LIQUID CONTROL	
JBD178H1	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H43	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H37	153A	SLC STANDBY LIQUID CONTROL	
148F027	153A	SLC STANDBY LIQUID CONTROL	
TC411N001	153A	SLC STANDBY LIQUID CONTROL	
SPDCA106H42	153A	SLC STANDBY LIQUID CONTROL	
ESC411K600	153A	SLC STANDBY LIQUID CONTROL	
IC011	153A	SLC STANDBY LIQUID CONTROL	
48F007	153A	SLC STANDBY LIQUID CONTROL	
48007	153A	SLC STANDBY LIQUID CONTROL	•
48006	153A	SLC STANDBY LIQUID CONTROL	
48001	153A	SLC STANDBY LIQUID CONTROL	
S14808U	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H45	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H39	153A	SLC STANDBY LIQUID CONTROL	
48F004A	153A	SLC STANDBY LIQUID CONTROL	
SPDCB101H2009	153A	SLC STANDBY LIQUID CONTROL	
XF01-U2	253	SLC STANDBY LIQUID CONTROL	
48013	253	SLC STANDBY LIQUID CONTROL	· · · · · · · · · · · · · · · · · · ·
V24814	253	SLC STANDBY LIQUID CONTROL	· · · · · · · · · · · · · · · · · · ·
CB253	253	SLC STANDBY LIQUID CONTROL	<u></u>
CB254	253	SLC STANDBY LIQUID CONTROL	
024814	253	SLC STANDBY LIQUID CONTROL	
024813	253	SLC STANDBY LIQUID CONTROL	·····
IXL01-U2	253	SLC STANDBY LIQUID CONTROL	
48F025	253A	SLC STANDBY LIQUID CONTROL	
T203	253A	SLC STANDBY LIQUID CONTROL	
PDCB201H5026	253A	SLC STANDBY LIQUID CONTROL	
48004	253A	SLC STANDBY LIQUID CONTROL	
PJCD207H1	253A	SLC STANDBY LIQUID CONTROL	
SHLC412N600	253A	SLC STANDBY LIQUID CONTROL	
PDCB201H5022	253A	SLC STANDBY LIQUID CONTROL	
ICB205H52	253A	SLC STANDBY LIQUID CONTROL	
PHCB205H56	253A	SLC STANDBY LIQUID CONTROL	
PHCD231H4	253A	SLC STANDBY LIQUID CONTROL	
PJCD207H2	253A	SLC STANDBY LIQUID CONTROL	
48F033A	253A	SLC STANDBY LIQUID CONTROL	
	253A	SLC STANDBY LIQUID CONTROL	
PHCB205H54	253A	SLC STANDBY LIQUID CONTROL	
124814	253A	SLC STANDBY LIQUID CONTROL	
T207B	253A	SLC STANDBY LIQUID CONTROL	

2T207B 253A SLC STANDBY LIQUID CONTROL



HCB205H54	253A	SLC STANDBY LIQUID CONTROL	
ZS24806	253A	SLC STANDBY LIQUID CONTROL	
SPDCB201H5	253A	SLC STANDBY LIQUID CONTROL	
2T204	253A	SLC STANDBY LIQUID CONTROL	
LE24812	253A	SLC STANDBY LIQUID CONTROL	
248003	253A	SLC STANDBY LIQUID CONTROL	
248017	253A	SLC STANDBY LIQUID CONTROL	
248F017	253A	SLC STANDBY LIQUID CONTROL	
2E219	253A	SLC STANDBY LIQUID CONTROL	
HSS24802	253A	SLC STANDBY LIQUID CONTROL	
TSHLC412N003	253A	SLC STANDBY LIQUID CONTROL	
LI/FI24806	253A	SLC STANDBY LIQUID CONTROL	
PI248207A	253A	SLC STANDBY LIQUID CONTROL	
SPHBD6010H9004	253A	SLC STANDBY LIQUID CONTROL	
SPHBD6010H9004	253A	SLC STANDBY LIQUID CONTROL	
SPHCD231H2	253A	SLC STANDBY LIQUID CONTROL	
2P208B	253A 253A	SLC STANDBY LIQUID CONTROL	
248001			
248F021	253A		
248F024	253A	SLC STANDBY LIQUID CONTROL	
SPDCA206H2604	253A		
SPDCB201H61	253A	SLC STANDBY LIQUID CONTROL	
	253A	SLC STANDBY LIQUID CONTROL	
PTC412N004	253A	SLC STANDBY LIQUID CONTROL	
248005	253A	SLC STANDBY LIQUID CONTROL	
SPHCD231H1	253A	SLC STANDBY LIQUID CONTROL	
TEC412N006	253A	SLC STANDBY LIQUID CONTROL	
ZS24808U	253A	SLC STANDBY LIQUID CONTROL	
TAHL24803	253A	SLC STANDBY LIQUID CONTROL	
248006	253A	SLC STANDBY LIQUID CONTROL	
248F007	253A	SLC STANDBY LIQUID CONTROL	2
ESC412K600	253A	SLC STANDBY LIQUID CONTROL	
SPDCA206H2611	253A	SLC STANDBY LIQUID CONTROL	2
HS24808A	253A	SLC STANDBY LIQUID CONTROL	
PIC412R600	253A	SLC STANDBY LIQUID CONTROL	
SPDCA206H2618	253A	SLC STANDBY LIQUID CONTROL	
SPDCA206H2620	253A	SLC STANDBY LIQUID CONTROL	2
SPDCB201H58	253A	SLC STANDBY LIQUID CONTROL	
SPDCB201H9001	253A	SLC STANDBY LIQUID CONTROL	
	253A	SLC STANDBY LIQUID CONTROL	
SPJCD207H9004	253A	SLC STANDBY LIQUID CONTROL	
SPJCD207H9006	253A	SLC STANDBY LIQUID CONTROL	
248019	253A	SLC STANDBY LIQUID CONTROL	
-BD-6010	253A	SLC STANDBY LIQUID CONTROL	
T24806	253A	SLC STANDBY LIQUID CONTROL	
	253A	SLC STANDBY LIQUID CONTROL	
	253A	SLC STANDBY LIQUID CONTROL	
SPDCB201H60	253A	SLC STANDBY LIQUID CONTROL	
ICC412R002	253A	SLC STANDBY LIQUID CONTROL	
SHL24810	253A	SLC STANDBY LIQUID CONTROL	
(A24804	253A	SLC STANDBY LIQUID CONTROL	
	253A	SLC STANDBY LIQUID CONTROL	
	253A	SLC STANDBY LIQUID CONTROL	
	253A	SLC STANDBY LIQUID CONTROL	
	253A	SLC STANDBY LIQUID CONTROL	
E24806 CV24811A	253A	SLC STANDBY LIQUID CONTROL	
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HCB205H53 253A SLC STANDBY LIQUID CONTROL 2



1S24808B	253A	SLC STANDBY LIQUID CONTROL	
PIC412R003	253A	SLC STANDBY LIQUID CONTROL	
248F012	253A	SLC STANDBY LIQUID CONTROL	
48F027	253A	SLC STANDBY LIQUID CONTROL	
46F027 4CB205H51	253A	SLC STANDBY LIQUID CONTROL	
		SLC STANDBY LIQUID CONTROL	
IBD281H1	253A		
.G24803	253A	SLC STANDBY LIQUID CONTROL	
248F001	253A	SLC STANDBY LIQUID CONTROL	
2E220	253A	SLC STANDBY LIQUID CONTROL	
48F004B	253A	SLC STANDBY LIQUID CONTROL	
BD-278	253A	SLC STANDBY LIQUID CONTROL	
2SV248F029B	253A	SLC STANDBY LIQUID CONTROL	
27248N004-R1	253A	SLC STANDBY LIQUID CONTROL	2
SPDCA206H2602	253A	SLC STANDBY LIQUID CONTROL	2
SPHCD231H3	253A	SLC STANDBY LIQUID CONTROL	2
48002	253A	SLC STANDBY LIQUID CONTROL	2
48008	253A	SLC STANDBY LIQUID CONTROL	2
48F002A	253A	SLC STANDBY LIQUID CONTROL	2
PHBD6010H9002		SLC STANDBY LIQUID CONTROL	2
ICB-205	253A	SLC STANDBY LIQUID CONTROL	2
IV248F006	253A	SLC STANDBY LIQUID CONTROL	2
IV248F006/ACT	253A	SLC STANDBY LIQUID CONTROL	2
BD-2045	253A	SLC STANDBY LIQUID CONTROL	2
PDCA206H2608	253A	SLC STANDBY LIQUID CONTROL	2
PDCB201H19	253A	SLC STANDBY LIQUID CONTROL	2
PHCB205H58	253A	SLC STANDBY LIQUID CONTROL	2
ICB205H4	253A	SLC STANDBY LIQUID CONTROL	2
48016	253A	SLC STANDBY LIQUID CONTROL	2 2 2 2 2 2 2 2 2 2 2 2
48F004A	253A	SLC STANDBY LIQUID CONTROL	2
SPDCB201H5020	253A	SLC STANDBY LIQUID CONTROL	
48007	253A	SLC STANDBY LIQUID CONTROL	
48F026	253A	SLC STANDBY LIQUID CONTROL	2
IS24804	253A	SLC STANDBY LIQUID CONTROL	
IS24804	253A	SLC STANDBY LIQUID CONTROL	2
SV248F029A	253A	SLC STANDBY LIQUID CONTROL	
SPDCA206H2601	253A	SLC STANDBY LIQUID CONTROL	2
	253A	SLC STANDBY LIQUID CONTROL	2
PJBD2045H9001	253A	SLC STANDBY LIQUID CONTROL	2
PCV24811C	and the second data was not seen as a second data was not seen as a second data was not second data was not se		
P208A	253A 253A	SLC STANDBY LIQUID CONTROL	2
48F031	253A	SLC STANDBY LIQUID CONTROL	2
C011	253A	SLC STANDBY LIQUID CONTROL	2
ICC412R004	253A		2
ICD-231	253A		2
BD278H1	253A	SLC STANDBY LIQUID CONTROL	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
IC412R001	253A	SLC STANDBY LIQUID CONTROL	2
PDCB201H5003	253A	SLC STANDBY LIQUID CONTROL	2
48010	253A	SLC STANDBY LIQUID CONTROL	2
AHL24810	253A	SLC STANDBY LIQUID CONTROL	2
PDCA206H2619	253A	SLC STANDBY LIQUID CONTROL	2
PJCD207H9003	253A	SLC STANDBY LIQUID CONTROL	2
48012	253A	SLC STANDBY LIQUID CONTROL	2
48F011	253A	SLC STANDBY LIQUID CONTROL	2
48F018	253A	SLC STANDBY LIQUID CONTROL	2
CB205H3	253A	SLC STANDBY LIQUID CONTROL	2
AHL24801	253A	SLC STANDBY LIQUID CONTROL	2
1248207B	253A	SLC STANDBY LIQUID CONTROL	



253A

SLC STANDET LIQUID CONTROL

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SPJBD2045H9000	253A	SLC STANDBY LIQUID CONTROL	
PT248N004-R2	253A	SLC STANDBY LIQUID CONTROL	2
248011	253A	SLC STANDBY LIQUID CONTROL	2
SPDCB201H5023	253A	SLC STANDBY LIQUID CONTROL	2
SPDCB201H5024	253A	SLC STANDBY LIQUID CONTROL	2
248018	253A	SLC STANDBY LIQUID CONTROL	2
248F002B	253A	SLC STANDBY LIQUID CONTROL	2
248F003B	253A	SLC STANDBY LIQUID CONTROL	2
248F033B	253A	SLC STANDBY LIQUID CONTROL	2
JBD-281	253A	SLC STANDBY LIQUID CONTROL	2
LTC412N001	253A	SLC STANDBY LIQUID CONTROL	2
PI248R003-R2	253A	SLC STANDBY LIQUID CONTROL	
IC-PI248207A-	253A	SLC STANDBY LIQUID CONTROL	2
248015	253A	SLC STANDBY LIQUID CONTROL	2
248F003A	253A	SLC STANDBY LIQUID CONTROL	2
248F015	253A	SLC STANDBY LIQUID CONTROL	2
248F016	253A	SLC STANDBY LIQUID CONTROL	2
DCD-220	253A	SLC STANDBY LIQUID CONTROL	2
HCB205H1	253A	SLC STANDBY LIQUID CONTROL	22 22 22 22 22 22 22 22 22 22 22 22 22
PCV24811B	253A	SLC STANDBY LIQUID CONTROL	2
SPDCB201H2600	253A	SLC STANDBY LIQUID CONTROL	2
SPDCB201H56	1253A	SLC STANDBY LIQUID CONTROL	2
XYC412M600A	253A	SLC STANDBY LIQUID CONTROL	2
SPDCA206H2606	253A	SLC STANDBY LIQUID CONTROL	2
IC-PI248207B-	253A	SLC STANDBY LIQUID CONTROL	2
248F008	253A	SLC STANDBY LIQUID CONTROL	2
PI248R003-R1	253A	SLC STANDBY LIQUID CONTROL	2
SPDCA206H2607	253A	SLC STANDBY LIQUID CONTROL	2
SPDCB201H5025	253A	SLC STANDBY LIQUID CONTROL	2
XY24806	253A	SLC STANDBY LIQUID CONTROL	2
ZS24808L	253A	SLC STANDBY LIQUID CONTROL	2
SPDCB201H57	253A	SLC STANDBY LIQUID CONTROL	2
SPHCB205H60	253A	SLC STANDBY LIQUID CONTROL	222
SPDCD220H1	253A	SLC STANDBY LIQUID CONTROL	2

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PP&L CALCULATION SHEET					
Dept-	PROJECT	Calc. No.	EC-053-1012		
Designed By C Keyyol	Assessment of SBLC	Rev. No.	0		
Designed By G.Kowal Checked By		Sh. No.	44 of 44		

ATTACHMENT NO. 2

EPIX, NPRDS VALVE DATA

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Equipment Performance and Information Exchange 4.0 Failure Summary Report

Generation Date 3/17/2005

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EPIX 4.0 Failure Summary Report

Key Specific Model: 3243-26-1 Direct Cause or Contributor General Cause: mechanical process

Equipment Details

Next

Failure Number : 306 Susquehanna 2

Bookmarks:

Abstract

Contact

Abstract

Susquehanna 2- Failure Number :306

02/09/1997 2:35:00 AM - No plant effect, from power operation. No generation capability was lost. A Rosemount Controls Systems model 1151DP4E22T0002PB (1151DP4E22T0002PB), failure caused the event. SLC STANDBY LIQUID CONTROL accumulators, tanks, air receivers, 2T204- unaffected by failure; transmitters, detectors, elements, LTC412N001- high output, but available; indicators, recorders, gauges, LI/FI24806- high output/indication.

Contact

Key:

DORN*JERRY G

System Engineer

570-542-3443 3443 jgdom@pplweb.com

Equipment Details

Components Affected:

SLC STANDBY LIQUID CONTROL System Accumulators, tanks, air receivers 2T204 unaffected by failure After 4701 days in service Site Common Name: STANDBY LIQUID CONTROL STORAGE TA Manufacturer: Alpha Tank & Metals Mfg. Model: 3243-26-1 Generic Model: 3243-26-1 **Application :Boron Injection Tank** Type (Parts List) :Liquid, Unpressurized SLC STANDBY LIQUID CONTROL System Indicators, recorders, gauges LI/FI24806 high output/indication After 187 days in service Site Common Name: SBLC TANK LEVEL AND FLOW Manufacturer: International Instruments Div/ Sigma Model: 9270-D1N-0-2-VB Generic Model: 9270-D1N-0-2-VB Parameter Measured/Input Signal :Flow Type (Primary Function) (Parts List) : Indicator

Supporting :

Component Causing Failure: Supporting :

SLC STANDBY LIQUID CONTROL

Transmitters, detectors, elements LTC412N001 high output, but available After 4701 days in service

high output, but available



Site Common Name: SBLC STORAGE TANK LEVEL TRANSMITTER Manufacturer: Rosemount Controls Systems Model: 1151DP4E22T0002PB Generic Model: 1151DP4E22T0002PB Parameter Measured/Input Signal : Level Principle of Operation (Parts List) : Positive Displacement Type (Primary Function) : Transmitter LTC412N001 tube sblc storage tank level transmitter - bubbler tube clogged/blocked - inservice since 3/28/84 Due to: mechanical process, clogged / blocked

Causes of Component Failure:

> Function restored by: operator actions taken restored normal lineup **Recurrence Prevented by:** preventive maintenance interval changed preventive maintenance program revised

Associated Maintenance:

None

Top |Prev |Next

Susquehanna 2 <u>Failure Number : 307</u>

Bookmarks: Abstract Abstract

Contact

Equipment Details

Susquehanna 2- Failure Number :307

02/22/1997 12:00:00 PM - No plant effect, from power operation. No generation capability was lost. A Rosemount Controls Systems model 1151DP4E22T0002PB (1151DP4E22T0002PB), failure caused the event. SLC STANDBY LIQUID CONTROL accumulators, tanks, air receivers, 2T204- unaffected by failure; transmitters, detectors, elements, LTC412N001- high output, but available; indicators, recorders, gauges, LI/FI24806- high output/indication.

Contact

DORN*JERRY G

System Engineer

570-542-3443

3443

jgdorn@pplweb.com

Equipment Details

Components Affected:	SLC STANDBY LIQUID CONTROL System
Key:	Accumulators, tanks, air receivers 2T204
•	unaffected by failure
	After 4714 days in service
· ·	Site Common Name: STANDBY LIQUID CONTROL STORAGE TA
	Manufacturer: Alpha Tank & Metals Mig.
	Model: 3243-26-1
	Generic Model: 3243-26-1
	Application :Boron Injection Tank
$\gamma = 1$	Type (Parts List) : Liquid, Unpressurized
· · · ·	SLC STANDBY LIQUID CONTROL System
Supporting :	Indicators, recorders, gauges LI/FI24806

SLC STANDBY LIQUID CONTROL System

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high output/indication After 200 days in service Site Common Name: SBLC TANK LEVEL AND FLOW Manufacturer: International Instruments Div/ Sigma Model: 9270-D1N-0-2-VB Generic Model: 9270-D1N-0-2-VB Parameter Measured/Input Signal :Flow Type (Primary Function) (Parts List) Indicator

Component Causing Failure: Supporting :

SLC STANDBY LIQUID CONTROL

Transmitters, detectors, elements LTC412N001 high output, but available After 4714 days in service Site Common Name: SBLC STORAGE TANK LEVEL TRANSMITTER Manufacturer: Rosemount Controls Systems Model: 1151DP4E22T0002PB Generic Model: 1151DP4E22T0002PB Parameter Measured/Input Signal : Level Principle of Operation (Parts List) : Positive Displacement Type (Primary Function) : Transmitter LTC412N001 tube sblc storage tank level transmitter - bubbler tube clogged/blocked - inservice since 3/28/84 Due to: mechanical process, clogged / blocked

Causes of Component Failure:



Function restored by: operator actions taken restored normal lineup **Recurrence Prevented by:** preventive maintenance interval changed preventive maintenance program revised

Associated Maintenance:

None

Top Prev Next

Failure Number : 308

Bookmarks:

Abstract

Contact

Equipment Details

Abstract

Susquehanna 2- Failure Number :308

03/08/1997 1:30:00 AM - No plant effect, from power operation. No generation capability was lost. A Rosemount Controls Systems model 1151DP4E22T0002PB (1151DP4E22T0002PB), failure caused the event, SLC STANDBY LIQUID CONTROL accumulators, tanks, air receivers, 2T204- unaffected by failure; transmitters, detectors, elements, LTC412N001- high output, but available; indicators, recorders. gauges, LI/FI24806- high output/indication.

Contact

DORN*JERRY G

System Engineer

570-542-3443

3443

igdorn@pplweb.com



Susquehanna 2

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Equipment Details

	-	Affected
•		
		Components Key :

Supporting :

Component Causing Failure: Supporting :

Causes of Component Failure:

Function restored by: operator actions taken restored normal lineup Recurrence Prevented by: preventive maintenance interval changed

Due to:

Associated Maintenance:

None

Top Prev Next

Susquehanna 2 Failure Number : 309

Bookmarks: Abstract

Bookmarks:

Abstract

Contact

SLC STANDBY LIQUID CONTROL System Accumulators, tanks, air receivers 2T204

Manufacturer: Alpha Tank & Metals Mfg.

Site Common Name: SBLC TANK LEVEL AND FLOW Manufacturer: International Instruments Div/ Sigma

Site Common Name: STANDBY LIQUID CONTROL STORAGE TA

unaffected by failure After 4728 days in service

Model: 3243-26-1

Generic Model: 3243-26-1 Application :Boron Injection Tank Type (Parts List) :Liquid, Unpressurized SLC STANDBY LIQUID CONTROL System Indicators, recorders, gauges LI/FI24806

high output/indication After 214 days in service

Model: 9270-D1N-0-2-VB

high output, but available After 4728 days in service

Model: 1151DP4E22T0002PB

Generic Model: 9270-D1N-0-2-VB Parameter Measured/Input Signal :Flow Type (Primary Function) (Parts List) :Indicator

SLC STANDBY LIQUID CONTROL

Transmitters, detectors, elements LTC412N001

Manufacturer: Rosemount Controls Systems

Principle of Operation (Parts List) : Positive Displacement

Generic Model: 1151DP4E22T0002PB Parameter Measured/Input Signal : Level

Type (Primary Function) : Transmitter

clogged/blocked - inservice since 3/28/84

preventive maintenance program revised

mechanical process, clogged / blocked

Site Common Name: SBLC STORAGE TANK LEVEL TRANSMITTER

LTC412N001 tube sblc storage tank level transmitter - bubbler tube -

Equipment Details

Abstract

<u>Contact</u>

Equipment Details

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Susquehanna 2- Failure Number :309

02/09/1997 2:00:00 PM - No plant effect, from power operation. No generation capability was lost. A Rosemount Controls Systems model 1151DP4E22T0002PB (1151DP4E22T0002PB), failure caused the event. SLC STANDBY LIQUID CONTROL accumulators, tanks, air receivers, 2T204- unaffected by failure; transmitters, detectors, elements, LTC412N001- high output, but available; indicators, recorders, gauges, LI/FI24806- high output/indication.

Contact

Key:

DORN*JERRY G

System Engineer

570-542-3443

3443

jgdom@ppiweb.com

Equipment Details

Components Affected: SLC STANDBY LIQUID CONTROL System Accumulators, tanks, air receivers 2T204 unaffected by failure After 4701 days in service Site Common Name: STANDBY LIQUID CONTROL STORAGE TA Manufacturer: Alpha Tank & Metals Mfg. Model: 3243-26-1 Generic Model: 3243-26-1 **Application :Boron Injection Tank** Type (Parts List) :Liquid, Unpressurized SLC STANDBY LIQUID CONTROL System Indicators, recorders, gauges LI/FI24806 high output/indication After 187 days in service Site Common Name: SBLC TANK LEVEL AND FLOW Manufacturer: International Instruments Div/ Sigma Model: 9270-D1N-0-2-VB Generic Model: 9270-D1N-0-2-VB Parameter Measured/Input Signal :Flow Type (Primary Function) (Parts List) : Indicator

Supporting :

Component Causing Failure: Supporting :

Causes of Component Failure:

SLC STANDBY LIQUID CONTROL

Transmitters, detectors, elements LTC412N001 high output, but available After 4701 days in service Site Common Name: SBLC STORAGE TANK LEVEL TRANSMITTER Manufacturer: Rosemount Controls Systems Model: 1151DP4E22T0002PB Generic Model: 1151DP4E22T0002PB Parameter Measured/Input Signal : Level Principle of Operation (Parts List) : Positive Displacement Type (Primary Function) : Transmitter LTC412N001 tube sblc storage tank level transmitter - bubbler tube clogged/blocked - inservice since 3/28/84 Due to:

mechanical process, clogged / blocked

Function restored by: operator actions taken

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restored normal lineup **Recurrence Prevented by:** preventive maintenance interval changed preventive maintenance program revised

Associated Maintenance:

None

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Failure Number : 310

Bookmarks:

Abstract

Contact

Equipment Details

Abstract

Susquehanna 2- Failure Number :310

04/12/1997 12:00:00 PM - No plant effect, from power operation. No generation capability was lost. A Rosemount Controls Systems model 1151DP4E22T0002PB (1151DP4E22T0002PB), failure caused the event. SLC STANDBY LIQUID CONTROL accumulators, tanks, air receivers, 2T204- unaffected by failure; transmitters, detectors, elements, LTC412N001- high output, but available; indicators, recorders, gauges, LI/FI24806- high output/indication.

Contact

Key:

DORN*JERRY G

System Engineer

3443 570-542-3443

jgdorn@pplweb.com

Equipment Details

Components Affected: SLC STANDBY LIQUID CONTROL System Accumulators, tanks, air receivers 2T204 unaffected by failure After 4763 days in service Site Common Name: STANDBY LIQUID CONTROL STORAGE TA Manufacturer: Alpha Tank & Metals Mfg. Model: 3243-26-1 Generic Model: 3243-26-1 Application :Boron Injection Tank Type (Parts List) :Liquid, Unpressurized SLC STANDBY LIQUID CONTROL System Indicators, recorders, gauges LI/FI24806 high output/indication After 249 days in service Site Common Name: SBLC TANK LEVEL AND FLOW Manufacturer: International Instruments Div/ Sigma Model: 9270-D1N-0-2-VB Generic Model: 9270-D1N-0-2-VB Parameter Measured/Input Signal :Flow Type (Primary Function) (Parts List) : Indicator

Supporting :

Component Causing Failure: Supporting :

SLC STANDBY LIQUID CONTROL

Transmitters, detectors, elements LTC412N001 high output, but available After 4763 days in service

high output, but available

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Site Common Name: SBLC STORAGE TANK LEVEL TRANSMITTER Manufacturer: Rosemount Controls Systems Model: 1151DP4E22T0002PB Generic Model: 1151DP4E22T0002PB Parameter Measured/Input Signal : Level Principle of Operation (Parts List) : Positive Displacement Type (Primary Function) : Transmitter LTC412N001 tube sbic storage tank level transmitter - bubbler tube clogged/blocked - inservice since 3/28/84 Due to: mechanical process, clogged / blocked

Causes of Component Failure:

> Function restored by: operator actions taken restored normal lineup **Recurrence Prevented by:** preventive maintenance interval changed preventive maintenance program revised

Associated Maintenance:

None

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Susquehanna 2 Failure Number : 311

Bookmarks: Abstract

Abstract

Contact

Equipment Details

Susquehanna 2- Failure Number :311

05/01/1997 4:54:00 PM - No plant effect, from power operation. No generation capability was lost. A Rosemount Controls Systems model 1151DP4E22T0002PB (1151DP4E22T0002PB), failure caused the event. SLC STANDBY LIQUID CONTROL accumulators, tanks, air receivers, 2T204- unaffected by failure: transmitters, detectors, elements, LTC412N001- high output, but available; indicators, recorders, gauges, LI/FI24806- high output/indication.

Contact

DORN*JERRY G

System Engineer

570-542-3443

3443

jgdom@pplweb.com

Equipment Details

Components Affected:	SLC STANDBY LIQUID CONTROL System
Key:	Accumulators, tanks, air receivers 2T204
	unaffected by failure
	After 4782 days in service
	Site Common Name: STANDBY LIQUID CONTROL STORAGE TA
	Manufacturer: Alpha Tank & Metals Mfg.
	Model: 3243-26-1
	Generic Model: 3243-26-1
	Application :Boron Injection Tank
	Type (Parts List) :Liquid, Unpressurized
	SLC STANDBY LIQUID CONTROL System
Supporting :	Indicators, recorders, gauges LI/FI24806

Type (Parts List) :Liquid, Unpressunzed SLC STANDBY HOUID CONTROL System

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high output/indication After 268 days in service Site Common Name: SBLC TANK LEVEL AND FLOW Manufacturer: International Instruments Div/ Sigma Model: 9270-D1N-0-2-VB Generic Model: 9270-D1N-0-2-VB Parameter Measured/Input Signal :Flow Type (Primary Function) (Parts List) : Indicator

Component Causing Failure: Supporting :

SLC STANDBY LIQUID CONTROL

Transmitters, detectors, elements LTC412N001 high output, but available After 4782 days in service Site Common Name: SBLC STORAGE TANK LEVEL TRANSMITTER Manufacturer: Rosemount Controls Systems Model: 1151DP4E22T0002PB Generic Model: 1151DP4E22T0002PB Parameter Measured/Input Signal : Level Principle of Operation (Parts List) : Positive Displacement Type (Primary Function) : Transmitter LTC412N001 tube sbic storage tank level transmitter - bubbler tube clogged/blocked - inservice since 3/28/84 Due to: mechanical process, clogged / blocked

Causes of Component Failure:

> Function restored by: operator actions taken restored normal lineup **Recurrence Prevented by:** preventive maintenance interval changed preventive maintenance program revised

Associated Maintenance:

None

Susquehanna 2

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Failure Number : 312

Bookmarks:

Abstract

Contact

Equipment Details

Abstract

Susquehanna 2- Failure Number :312

05/17/1997 3:30:00 PM - No plant effect, from power operation. No generation capability was lost. A Rosemount Controls Systems model 1151DP4E22T0002PB (1151DP4E22T0002PB), failure caused the event. SLC STANDBY LIQUID CONTROL accumulators, tanks, air receivers, 2T204- unaffected by failure: transmitters, detectors, elements, LTC412N001- high output, but available; indicators, recorders, gauges, LI/FI24806- high output/indication.

Contact

DORN*JERRY G

System Engineer

570-542-3443

3443

jgdorn@pplweb.com

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Equipment Detalls

Components Affected:	SLC STANDBY LIQUID CONTROL System	
Key:	Accumulators, tanks, air receivers 2T204	
	unaffected by failure	
	After 4798 days in service	

Manufacturer: Alpha Tank & Metals Mfg.

Indicators, recorders, gauges LI/FI24806

Site Common Name: SBLC TANK LEVEL AND FLOW Manufacturer: International Instruments Div/ Sigma

Model: 3243-26-1

Generic Model: 3243-26-1 Application :Boron Injection Tank Type (Parts List) :Liquid, Unpressurized SLC STANDBY LIQUID CONTROL System

high output/indication After 284 days in service

Model: 9270-D1N-0-2-VB

Site Common Name: STANDBY LIQUID CONTROL STORAGE TA

Supporting :

Component Causing Failure: Supporting :

Causes of Component Failure:

> mechanical process, clogged / blocked Function restored by: operator actions taken restored normal lineup Recurrence Prevented by: preventive maintenance interval changed preventive maintenance program revised

Associated Maintenance:

None

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Susquehanna 2 Failure Number : 313

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Equipment Details

T

Bookmarks:

Abstract

Contact

Equipment Details

Generic Model: 9270-D1N-0-2-VB Parameter Measured/Input Signal :Flow Type (Primary Function) (Parts List) :Indicator SLC STANDBY LIQUID CONTROL Transmitters, detectors, elements LTC412N001 biob output but available

high output, but available After 4798 days in service Site Common Name: SBLC STORAGE TANK LEVEL TRANSMITTER Manufacturer: Rosemount Controls Systems Model: 1151DP4E22T0002PB Generic Model: 1151DP4E22T0002PB Parameter Measured/Input Signal : Level Principle of Operation (Parts List) : Positive Displacement Type (Primary Function) : Transmitter LTC412N001 tube sblc storage tank level transmitter - bubbler tube clogged/blocked - inservice since 3/28/84 Due to: mechanical process, clogged / blocked

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Susquehanna 2- Failure Number :313

06/03/1997 9:00:00 PM - No plant effect, from power operation. No generation capability was lost. A Rosemount Controls Systems model 1151DP4E22T0002PB (1151DP4E22T0002PB), failure caused the event. SLC STANDBY LIQUID CONTROL accumulators, tanks, air receivers, 2T204- unaffected by failure; transmitters, detectors, elements, LTC412N001- high output, but available; indicators, recorders, gauges, LI/FI24806- high output/indication.

Contact

DORN*JERRY G

r G System

System Engineer

570-542-3443 3443

jgdom@pplweb.com

Equipment Details

Components Affected: SLC STANDBY LIQUID CONTROL System Key: Accumulators, tanks, air receivers 2T204 unaffected by failure After 4815 days in service Site Common Name: STANDBY LIQUID CONTROL STORAGE TA Manufacturer: Alpha Tank & Metals Mfg. Model: 3243-26-1 Generic Model: 3243-26-1 Application :Boron Injection Tank Type (Parts List) :Liquid, Unpressurized SLC STANDBY LIQUID CONTROL System Supporting : Indicators, recorders, gauges LI/FI24806 high output/indication After 301 days in service Site Common Name: SBLC TANK LEVEL AND FLOW Manufacturer: International Instruments Div/ Sigma Model: 9270-D1N-0-2-VB Generic Model: 9270-D1N-0-2-VB Parameter Measured/Input Signal :Flow Type (Primary Function) (Parts List) : Indicator Component Causing SLC STANDBY LIQUID CONTROL Failure: Transmitters, detectors, elements LTC412N001 Supporting : high output, but available After 4815 days in service Site Common Name: SBLC STORAGE TANK LEVEL TRANSMITTER Manufacturer: Rosemount Controls Systems Model: 1151DP4E22T0002PB Generic Model: 1151DP4E22T0002PB Parameter Measured/Input Signal : Level Principle of Operation (Parts List) : Positive Displacement Type (Primary Function) : Transmitter **Causes of Component** LTC412N001 tube sblc storage tank level transmitter - bubbler tube -Failure: clogged/blocked - inservice since 3/28/84 Due to:

mechanical process, clogged / blocked

Function restored by: operator actions taken

Eunation restored his

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restored normal lineup **Recurrence Prevented by:** preventive maintenance interval changed preventive maintenance program revised

Associated Maintenance:

None

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Susquehanna 2 Failure Number : 314

Bookmarks:

Abstract

Contact

Equipment Details

Abstract

Susquehanna 2- Failure Number :314

06/30/1997 12:00:00 PM - No plant effect, from power operation. No generation capability was lost. A Rosemount Controls Systems model 1151DP4E22T0002PB (1151DP4E22T0002PB), tailure caused the event. SLC STANDBY LIQUID CONTROL accumulators, tanks, air receivers, 2T204- unaffected by failure; transmitters, detectors, elements, LTC412N001- high output, but available; indicators, recorders, gauges, LI/FI24806- high output/indication.

Contact

Key:

DORN*JERRY G

System Engineer 570-542-3443

3443

jgdom@pplweb.com

Equipment Details

Components Affected: SLC STANDBY LIQUID CONTROL System Accumulators, tanks, air receivers 2T204 unaffected by failure After 4842 days in service Site Common Name: STANDBY LIQUID CONTROL STORAGE TA Manufacturer: Alpha Tank & Metals Mfg. Model: 3243-26-1 Generic Model: 3243-26-1 Application :Boron Injection Tank Type (Parts List) : Liquid, Unpressurized SLC STANDBY LIQUID CONTROL System Indicators, recorders, gauges LI/FI24806 high output/indication After 328 days in service Site Common Name: SBLC TANK LEVEL AND FLOW Manufacturer: International Instruments Div/ Sigma Model: 9270-D1N-0-2-VB Generic Model: 9270-D1N-0-2-VB Parameter Measured/Input Signal :Flow Type (Primary Function) (Parts List) :Indicator

Supporting :

Component Causing Failure: Supporting :

SLC STANDBY LIQUID CONTROL

Transmitters, detectors, elements LTC412N001 high output, but available After 4842 days in service

high output, but available Affar ADAD dava in non-in-

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Site Common Name: SBLC STORAGE TANK LEVEL TRANSMITTER Manufacturer: Rosemount Controls Systems Model: 1151DP4E22T0002PB Generic Model: 1151DP4E22T0002PB Parameter Measured/Input Signal : Level Principle of Operation (Parts List) : Positive Displacement Type (Primary Function) : Transmitter LTC412N001 tube sblc storage tank level transmitter - bubbler tube clogged/blocked - inservice since 3/28/84 Due to:

Causes of Component Failure:

mechanical process, clogged / blocked

Function restored by: operator actions taken restored normal lineup Recurrence Prevented by: preventive maintenance interval changed preventive maintenance program revised

Associated Maintenance:

None

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Susquehanna 2 Failure Number : 315

Bookmarks: Abstract Abstract

Contact

Equipment Details

Susquehanna 2- Failure Number :315

07/31/1997 11:29:00 PM - No plant effect, from power operation. No generation capability was lost. A Rosemount Controls Systems model 1151DP4E22T0002PB (1151DP4E22T0002PB), failure caused the event. SLC STANDBY LIQUID CONTROL accumulators, tanks, air receivers, 2T204- unaffected by failure; transmitters, detectors, elements, LTC412N001- high output, but available; indicators, recorders, gauges, LI/FI24806- high output/indication.

Contact

DORN*JERRY G

System Engineer

570-542-3443

3443

jgdom@pplweb.com

Equipment Details

Components Affected:	SLC STANDBY LIQUID CONTROL System
Key:	Accumulators, tanks, air receivers 2T204
	unaffected by failure
	After 4873 days in service
	Site Common Name: STANDBY LIQUID CONTROL STORAGE TA
	Manufacturer: Alpha Tank & Metals Mig.
· · ·	Model: 3243-26-1
· .	Generic Model: 3243-26-1
	Application :Boron Injection Tank
	Type (Parts List) :Liquid, Unpressurized
	SLC STANDBY LIQUID CONTROL System
Supporting :	Indicators, recorders, gauges LI/FI24806

Type (Parts List) :Liquid, Unpressunzed SI C STANDRY I IOUID CONTROL System



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high output/indication After 359 days in service Site Common Name: SBLC TANK LEVEL AND FLOW Manufacturer: International Instruments Div/ Sigma Model: 9270-D1N-0-2-VB Generic Model: 9270-D1N-0-2-VB Parameter Measured/Input Signal :Flow Type (Primary Function) (Parts List) : Indicator

Component Causing Fallure: Supporting :

SLC STANDBY LIQUID CONTROL

Transmitters, detectors, elements LTC412N001 high output, but available After 4873 days in service Site Common Name: SBLC STORAGE TANK LEVEL TRANSMITTER Manufacturer: Rosemount Controls Systems Model: 1151DP4E22T0002PB Generic Model: 1151DP4E22T0002PB Parameter Measured/Input Signal : Level Principle of Operation (Parts List) : Positive Displacement Type (Primary Function) : Transmitter LTC412N001 tube sblc storage tank level transmitter - bubbler tube clogged/blocked - inservice since 3/28/84 Due to: mechanical process, clogged / blocked

Causes of Component Failure:

Associated Maintenance:

None

Function restored by: operator actions taken restored normal lineup **Recurrence Prevented by:**

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Failure Number: 316

Bookmarks:

Abstract

Susquehanna 2

Contact

preventive maintenance interval changed preventive maintenance program revised

Equipment Details

Abstract

Susquehanna 2- Failure Number :316

09/02/1997 12:00:00 PM - No plant effect, from power operation. No generation capability was lost. A Rosemount Controls Systems model 1151DP4E22T0002PB (1151DP4E22T0002PB), failure caused the event. SLC STANDBY LIQUID CONTROL accumulators, tanks, air receivers, 2T204- unaffected by failure; transmitters, detectors, elements, LTC412N001- high output, but available; indicators, recorders, gauges, LI/FI24806- high output/indication.

Contact

DORN'JERRY G

System Engineer

570-542-3443

3443

jgdorn@pplweb.com

Equipment Details

Components Affected:	SLC STANDBY LIQUID CONTROL System
Key:	Accumulators, tanks, air receivers 2T204
	unaffected by failure
	After 4906 days in service
	Site Common Name: STANDBY LIQUID CONTROL STORAGE TA
	Manufacturer: Alpha Tank & Metals Mfg.

Model: 3243-26-1

high output/indication After 392 days in service

Model: 9270-D1N-0-2-VB

high output, but available *After* 4906 days in service

- inservice since 3/28/84

Model: 1151DP4E22T0002PB

Generic Model: 9270-D1N-0-2-VB Parameter Measured/Input Signal :Flow Type (Primary Function) (Parts List) :Indicator

SLC STANDBY LIQUID CONTROL

Transmitters, detectors, elements LTC412N001

Manufacturer: Rosemount Controls Systems

Principle of Operation (Parts List) : Positive Displacement

Generic Model: 1151DP4E22T0002PB Parameter Measured/Input Signal : Level

Type (Primary Function) : Transmitter

Site Common Name: SBLC STORAGE TANK LEVEL TRANSMITTER

LTC412N001 tube sblc storage tank level transmitter - bubbler tube - blocked tube

Generic Model: 3243-26-1 Application :Boron Injection Tank

Type (Parts List) :Liquid, Unpressurized

SLC STANDBY LIQUID CONTROL System Indicators, recorders, gauges LI/FI24806

Site Common Name: SBLC TANK LEVEL AND FLOW Manufacturer: International Instruments Div/ Sigma

Supporting :

Component Causing Failure: Supporting :

Causes of Component Failure:

Function restored by: operator actions taken restored normal lineup Recurrence Prevented by: preventive maintenance interval changed preventive maintenance program revised

mechanical process, clogged / blocked

Associated Maintenance:

None

Due to:

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Susquehanna 2 Failure Number : 317

Bookmarks: Abstract

Abstract

<u>Contact</u>

Equipment Details

Bookmarks:

Abstract

Contact

Equipment Details

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Susquehanna 2- Failure Number :317

11/24/1997 10:00:00 AM - No plant effect, from power operation. No generation capability was lost. A Rosemount Controls Systems model 1151DP4E22T0002PB (1151DP4E22T0002PB), failure caused the event. SLC STANDBY LIQUID CONTROL accumulators, tanks, air receivers, 2T204- unaffected by failure; transmitters, detectors, elements, LTC412N001- high output, but available; indicators, recorders, gauges, LI/FI24806- high output/indication.

Contact

Key:

DORN*JERRY G

System Engineer

570-542-3443

3443

jgdorn@pplweb.com

Equipment Details

Components Affected: SLC STANDBY LIQUID CONTROL System Accumulators, tanks, air receivers 2T204 unaffected by failure After 4989 days in service Site Common Name: STANDBY LIQUID CONTROL STORAGE TA Manufacturer: Alpha Tank & Metals Mfg. Model: 3243-26-1 Generic Model: 3243-26-1 **Application :Boron Injection Tank** Type (Parts List) :Liquid, Unpressurized SLC STANDBY LIQUID CONTROL System Indicators, recorders, gauges LI/FI24806 high output/indication After 475 days in service Site Common Name: SBLC TANK LEVEL AND FLOW Manufacturer: International Instruments Div/ Sigma Model: 9270-D1N-0-2-VB Generic Model: 9270-D1N-0-2-VB Parameter Measured/Input Signal :Flow Type (Primary Function) (Parts List) :Indicator SLC STANDBY LIQUID CONTROL

Supporting :

Component Causing Fallure: Supporting :

Causes of Component Failure:

high output, but available After 4989 days in service

Transmitters, detectors, elements LTC412N001

Site Common Name: SBLC STORAGE TANK LEVEL TRANSMITTER Manufacturer: Rosemount Controls Systems

Model: 1151DP4E22T0002PB

Generic Model: 1151DP4E22T0002PB

Parameter Measured/Input Signal : Level

Principle of Operation (Parts List) : Positive Displacement

Type (Primary Function) : Transmitter

LTC412N001 tube sblc storage tank level transmitter - bubbler tube - blocked tube - inservice since 3/28/84

Due to:

mechanical process, clogged / blocked

Function restored by: operator actions taken

Function restored by:

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restored normal lineup Recurrence Prevented by: preventive maintenance interval changed preventive maintenance program revised

Contact

Associated Maintenance:

None

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Failure Number: 820

Bookmarks:

Abstract

System Engineer

Equipment Details

Abstract

Susquehanna 2- Failure Number :820

05/20/1999 - No plant effect, from power operation. No generation capability was lost. A Rosemount Controls Systems model 1151DP4E22T0002PB (1151DP4E22T0002PB), failure caused the event. SLC STANDBY LIQUID CONTROL accumulators, tanks, air receivers, 2T204- unaffected by failure; transmitters, detectors, elements, LTC412N001- high output, but available; indicators, recorders, gauges, LI/FI24806- high output/indication.

Contact

MISSIEN*IAN C

570-542-3396

3396

icmissien@pplweb.com

Equipment Details

Components Affected: SLC STANDBY LIQUID CONTROL System Accumulators, tanks, air receivers 2T204 Key:

unaffected by failure After 5531 days in service Site Common Name: STANDBY LIQUID CONTROL STORAGE TA Manufacturer: Alpha Tank & Metals Mfg. Model: 3243-26-1 Generic Model: 3243-26-1 **Application :Boron Injection Tank** Type (Parts List) :Liquid, Unpressurized SLC STANDBY LIQUID CONTROL System Indicators, recorders, gauges LI/FI24806 high output/indication After 1017 days in service Site Common Name: SBLC TANK LEVEL AND FLOW Manufacturer: International Instruments Div/ Sigma Model: 9270-D1N-0-2-VB Generic Model: 9270-D1N-0-2-VB Parameter Measured/Input Signal :Flow Type (Primary Function) (Parts List) :Indicator

Supporting :

Component Causing Failure: Supporting :

SLC STANDBY LIQUID CONTROL

Transmitters, detectors, elements LTC412N001 high output, but available After 5531 days in service

high output, but available An Frid dama in an da

Revision 0 Page 78 of 138

Site Common Name: SBLC STORAGE TANK LEVEL TRANSMITTER Manufacturer: Rosemount Controls Systems Model: 1151DP4E22T0002PB Generic Model: 1151DP4E22T0002PB Parameter Measured/Input Signal : Level Principle of Operation (Parts List) : Positive Displacement Type (Primary Function) : Transmitter LTC412N001 tube sblc storage tank level transmitter - bubbler tube - blocked tube - inservice since 3/28/84 Due to: mechanical process, clogged / blocked

Causes of Component Failure:

> Function restored by: operator actions taken restored normal lineup Recurrence Prevented by: preventive maintenance interval changed preventive maintenance program revised

None

Associated Maintenance:

INPO

Equipment Performance and Information Exchange 4.0

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 ${rak M}$ Warning: Do not use the Browser Back, Forward, Stop, Refresh or Home buttons on this page. **EPIX/NPRDS General Text Search** In NPRDS Go Look for "SBLC" AND "ISOLATION CHECK VALVE" Search Tips Documents 1 to 2 of 2 matching the query ""SBLC" AND "ISOLATION CHECK VALVE"". 1. 92~QUAD CITIES 1~Valves, dampers Abstract: *SBLCS Cntmnt Isol Check Valve~1-1101-16~Internal Leakage~Standby Liquid Control-GE~System Function/Operation Unaffected~Resulted in No Significant Effect~Crane Co~3888-XU http://www.inpo.org/databases/nprds/185/cweqad1185708.htm - size 6333 bytes -11/13/1992 5:00:00 PM GMT 2. <u>92~HOPE CREEK 1~Valves, dampers</u> Abstract: *SBLCS Cntmnt Isol Check Valve~1BHV-029~Internal Leakage~Standby Liquid Control-GE~System Function/Operation Unaffected~Resulted in No Significant Effect~Rockwell Int/ Flow Control Div~1.5-36274T1 http://www.inpo.org/databases/nprds/164/peghcs1164209.htm - size 5909 bytes -10/7/1992 5:00:00 PM GMT Page 1 of 1





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Equipment Performance and Information Exchange 4.0 Failure Summary Report

Generation Date 3/17/2005

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EPIX 4.0 Failure Summary Report

Key Component Type: Valves, dampers Direct Cause or Contributor Component Type: Valves, dampers

Nine Mile Point 2 Failure Number : 351

Bookmarks:

Abstract

Contact

Equipment Details

Abstract

Nine Mile Point 2- Failure Number :351

03/07/2000 3:20:00 PM - Outage impacted, from refueling. No generation capability was lost. A Velan Inc model B303-6W14MS (B303-6W14MS), failure caused the event. Standby Liquid Control System valves, dampers, 2SLS*V10- internal leakage when fully seated.

Contact

Tanguay, Thomas

System Engineer 315

315-349-4428

TanguayT@nimo.com

Equipment Details

Component Causing Failure: Key :

Causes of Component Failure:

Standby Liquid Control System Valves, dampers 2SLS*V10 internal leakage when fully seated After 4906 days in service Industry Common Name: *SBLCS Cntmnt Isol Check Valve Manufacturer: Velan Inc. Model: B303-6W14MS Generic Model: B303-6W14MS Body Material : Austenitic Stainless STL-316 Function/Application : One-Way Flow Nominal Inlet Size (Range) : 2 to 3.99 IN **Operator : None** Type (Parts List) : Check 2SLS*V10 none identified by investigation Due to: mechanical process, foreign material

Function restored by: operator actions taken repaired device (beyond recalibration) Recurrence Prevented by: actions to prevent recurrence not needed None

Associated Maintenance:

INPO

INPO

Equipment Performance and Information Exchange 4.0

Production Read Only

Equipment Performance and Information

Production Read Only

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Equipment Performance and Information Exchange 4.0 Failure Summary Report

Generation Date 3/17/2005

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EPIX 4.0 Failure Summary Report

Manufacturer: Crane Co	Generic Model Number: 3888
Unit: Dresden 2	MR System: Standby Liquid Control

Dresden 2

Failure Number : 245

Bookmarks:

[Next]

Abstract

Contact

Equipment Details

Abstract

Dresden 2- Failure Number :245

03/09/1998 10:30:00 AM - No plant effect, from refueling. No generation capability was lost. A Crane Co model 3888XU (3888), failure caused the event. Standby Liquid Control valves, dampers, 2-1101-15- internal leakage when fully seated.

Contact

Daniel Oakley LLRT System Engineer 815 942-2920 3708 daniel.oakley@ucm.com

Equipment Details

Component Causing Failure:	Standby Liquid Control	
Key:	Valves, dampers 2-1101-15	
	internal leakage when fully se	ated
	After 10288 days in service	
	Industry Common Name: *SE	BLCS Cntmnt Isol Check Valve
	Manufacturer: Crane Co	
	Model: 3888XU	
	Generic Model: 3888	
	Body Material : Austenitic Sta	inless STL-Other
	Function/Application : One-W	•
	Nominal Inlet Size (Range) :	1/2 to 1.99 IN
	Operator : None	
·	Type (Parts List) : Check	
Causes of Component Failure:	2-1101-15 none identified by	investigation
	Due to: equipment age - invalid c invalid cause after 09/01/200	ause after 09/01/2001, normal, expected aging -
	Function restored by: replaced device	
	Recurrence Prevented by: actions to prevent recurrence	not needed
Associated Maintenance	•	
Manufacturer: Rockwell	Int/ Flow Control Div	Generic Model Number: 36274
Unit: Hatch 1		MR System: SBLC

Manufacturer: Rockwell Int/ Flow Control Div

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Failure Number : 60

Contact

Bookmarks: Abstract

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Hatch 1

Equipment Details

Hatch 1- Failure Number :60

03/13/1999 12:00:00 PM - No plant effect, from cold shutdown. No generation capability was lost. A Rockwell Int/ Flow Control Div model 36274 (36274), failure caused the event. SBLC valves, dampers, 1C41-F006internal leakage when fully seated.

Contact

TROUNG, THI SYS ENG 912 537 1395 2468

Abstract

Equipment Details

Component Causing Failure:	SBLC	
Key:	Valves, dampers 1C41-F006	
	internal leakage when fully seated	
	Advard 470 di alevan lan animala a	

After 4781 days in service Industry Common Name: *SBLCS Cntmnt Isol Check Valve Manufacturer: Rockwell Int/ Flow Control Div Model: 36274 Generic Model: 36274 Body Material : Austenitic Stainless STL-316 Function/Application : One-Way Flow Nominal Inlet Size (Range) : 1/2 to 1.99 IN **Operator : None** Type (Parts List) : Check

Causes of Component Fallure:

1C41-F006 spring(s) loss of compression - inservice since 2/8/86

Due to:

equipment age - invalid cause after 09/01/2001, normal, expected aging invalid cause after 09/01/2001

Function restored by: repaired device (beyond recalibration) replaced piece part **Recurrence Prevented by:** actions to prevent recurrence not needed

Associated Maintenance: None

Manufacturer: Velan Inc Unit: Nine Mile Point 2

Generic Model Number: B303-6W14MS MR System: Standby Liquid Control System



Top| Prev| Next Nine Mile Point 2 Failure Number : 351

Nine Mile Point 2 Failure Number : 351

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Bookmarks:

Abstract

Contact

Equipment Details

Abstract

Nine Mile Point 2- Failure Number :351

03/07/2000 3:20:00 PM - Outage impacted, from refueling. No generation capability was lost. A Velan Inc model B303-6W14MS (B303-6W14MS), failure caused the event. Standby Liquid Control System valves, dampers, 2SLS*V10- internal leakage when fully seated.

Contact

Tanguay, Thomas

System Engineer

315-349-4428

TanguayT@nimo.com

Equipment Details

Component Causing Failure: Key:

Causes of Component Failure:

Standby Liquid Control System Valves, dampers 2SLS*V10 internal leakage when fully seated After 4906 days in service Industry Common Name: *SBLCS Cntmnt Isol Check Valve Manufacturer: Velan Inc Model: B303-6W14MS Generic Model: B303-6W14MS Body Material : Austenitic Stainless STL-316 Function/Application : One-Way Flow Nominal Inlet Size (Range) : 2 to 3.99 IN **Operator : None** Type (Parts List) : Check 2SLS*V10 none identified by investigation Due to: mechanical process, foreign material

Function restored by: operator actions taken repaired device (beyond recalibration) **Recurrence Prevented by:** actions to prevent recurrence not needed None

Associated Maintenance:

Manufacturer: Velan Inc **Unit: Browns Ferry 3**

Generic Model Number: W7234B13MS MR System: Standby Liquid Control-GE

Topi Prev Next

Browns Ferry 3

Failure Number : 200

Bookmarks:

Abstract

Contact

Equipment Details

Abstract

Browns Ferry 3- Failure Number :200

03/26/2002 - No plant effect, from refueling. No generation capability was lost. A Hancock Mfg Co Inc model 5580 (5580), Velan Inc model W7234B13MS (W7234B13MS), Atwood & Morrill Co. Inc./Xomox model 11462 (11462), Velan Valve Corp model B107144B02AA (B107144B02AA), Anchor/Darling Valve Co. model 900/w9223821a (900/W9223821A), Anchor / Darling Co. model 900/W9223821A (900/W9223821A), failure

5580 (5580), Velan Inc model W7234B13MS (W7234B13MS), Atwood & Morrill Co. Inc./Xomox model 11462 111460 \ Volon Volos Co



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caused the event. High Pressure Coolant Injection-GE valves, dampers, 3-CKV-073-0609- internal leakage when fully seated; Standby Liquid Control-GE valves, dampers, 3-CKV-063-0526- internal leakage when fully seated; Feedwater-GE valves, dampers, 3-CKV-003-0554- internal leakage when fully seated; Main Steam-GE valves, dampers, 3-FCV-001-0056- internal leakage when fully seated; Reactor Water Cleanup-GE valves, dampers, 3-CKV-069-0629- internal leakage when fully seated; valves, dampers, 3-CKV-069-0629- internal leakage when fully seated; valves, dampers, 3-CKV-069-0629- internal leakage when fully seated; valves, dampers, 3-CKV-069-0628- internal leakage when fully seated.

Contact

Fredrick Nilsen

LLRT Component Engineer

256-729-2958

2958

fjnilsen@tva.gov

Equipment Details

Component Causing Failure: Key :

Causes of Component Failure:

Component Causing Failure: Key :

Causes of Component Failure:

Feedwater-GE Valves, dampers 3-CKV-003-0554 internal leakage when fully seated After 9156 days in service Industry Common Name: *Fdwtr Cntmnt Check Valve Manufacturer: Atwood & Morrill Co. Inc./Xomox Model: 11462 Generic Model: 11462 **Body Material : Carbon Steel** Function/Application : Flow Control (incl temp control) Nominal Inlet Size (Range) : 20 to 39.99 IN **Operator: None** Type (Parts List) : Check 3-CKV-003-0554 none identified by investigation Due to: mechanical process, leakage Function restored by: repaired device (beyond recalibration) **Recurrence Prevented by:** supplemental testing performed High Pressure Coolant Injection-GE Valves, dampers 3-CKV-073-0609 internal leakage when fully seated After 9156 days in service Industry Common Name: Primary Cntmnt Isol Valve Manufacturer: Hancock Mfg Co Inc. Model: 5580 Generic Model: 5580 Body Material : Carbon Steel Function/Application : One-Way Flow Nominal Inlet Size (Range) : 2 to 3.99 IN **Operator : None** Type (Parts List) : Check 3-CKV-073-0609 none identified by investigation Due to: mechanical process, leakage Function restored by: repaired device (beyond recalibration) **Recurrence Prevented by:** supplemental testing performed

repaired device (beyond recalibration)

Component Causing Failure: Key :

Causes of Component Failure:

Component Causing Failure: Key :

Causes of Component Fallure:

Component Causing Failure: Key :

Valves, dampers 3-FCV-001-0056 internal leakage when fully seated After 2375 days in service Industry Common Name: Primary Cntmnt Isol Valve Manufacturer: Velan Valve Corp Model: B107144B02AA Generic Model: B107144B02AA Body Material : Carbon Steel Function/Application : Shutoff/Isolation/Stop Nominal Inlet Size (Range) : 2 to 3.99 IN Operator : Electric Motor/Servo (MOV) Type (Parts List) : Gate 3-FCV-001-0056 none identified by investigation 3-FCV-001-0056 seat Due to: mechanical process, leakage Function restored by: tested and restored to service **Recurrence Prevented by:** engineering analysis performed **Reactor Water Cleanup-GE** Valves, dampers 3-CKV-069-0628 internal leakage when fully seated After 840 days in service Site Common Name: Primary Cntmnt Isol Valve Manufacturer: Anchor / Darling Co. Model: 900/W9223821A Generic Model: 900/W9223821A Function/Application : One-Way Flow Nominal Inlet Size (Range) : 4 to 11.99 IN **Operator : None** Program : Appendix J LLRT program SubType : Check-Swing Type (Parts List) : Check 3-CKV-069-0628 seat Due to: mechanical process, leakage Function restored by: replaced piece part **Recurrence Prevented by:** supplemental testing performed **Reactor Water Cleanup-GE** Valves, dampers 3-CKV-069-0629 internal leakage when fully seated After 840 days in service Site Common Name: Primary Critmit Isol Valve Manufacturer: Anchor/Darling Valve Co. Model: 900/w9223821a Generic Model: 900/W9223821A Function/Application : One-Way Flow Nominal Inlet Size (Range) : 4 to 11.99 IN **Operator : None**

Main Steam-GE

Nominal Inlet Size (Hange) : 4 to 11.99 IN Oberator : None

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Causes of Component Failure:

Component Causing Failure: Key:

Causes of Component Fallure:

Associated Maintenance:

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Browns Ferry 3 Bookmarks:

Abstract

Contact

Equipment Details

Failure Number : 272

Abstract

Browns Ferry 3- Failure Number :272

03/01/2004 - No plant effect, from refueling. No generation capability was lost. A Crane Valve Prod/Crane Co Fr Chapman model CD-06005-8-06 (CD-06005-8-06), Velan Inc model W7234B13MS (W7234B13MS), Velan Valve Corp model B107144B02AA (B107144B02AA), Anchor/Darling Valve Co. model 900/w9223821a (900/W9223821A), Anchor / Darling Co. model 900/W9223821A (900/W9223821A), Pittsburgh - Des Moines Steel Co (PDM) model A (A), General Electric Company model F01 (F01), failure caused the event. High Pressure Coolant Injection-GE valves, dampers, 3-FCV-073-0026- internal leakage when fully seated; Standby Liquid Control-GE valves, dampers, 3-CKV-063-0526- internal leakage when fully seated; Radwaste-GE valves, dampers, 3-FCV-077-0002A- internal leakage when fully seated; Main Steam-GE valves, dampers, 3-FCV-001-0056- internal leakage when fully seated; Reactor Water Cleanup-GE valves. dampers. 3-CKV-069-0629- internal leakage when fully seated; valves, dampers, 3-CKV-069-0628- internal leakage when fully seated; Primary Containment-GE containment penetrations, air locks, hatches, 3-STRU-303-DW/HEAD- loss of pressure boundary function; containment penetrations, air locks, hatches, 3-EPEN-100-0101C- loss of pressure boundary function.

Program : Appendix J LLRT program

mechanical process, leakage

Use : System, line, or component isolation check

Industry Common Name: *SBLCS Cntmnt Isol Check Valve

Service : Clean water SubType : Check-Swing Type (Parts List) ; Check

3-CKV-069-0629 seat

Function restored by: replaced piece part

Recurrence Prevented by: supplemental testing performed

Standby Liquid Control-GE

After 9156 days in service

Manufacturer: Velan Inc Model: W7234B13MS

Type (Parts List) : Check

Function restored by: recalibrated/adjusted device **Recurrence Prevented by:** supplemental testing performed

Operator : None

Due to:

Unplanned

Generic Model: W7234B13MS Body Material : Carbon Steel

Function/Application : One-Way Flow Nominal Inlet Size (Range) : 1/2 to 1.99 IN

mechanical process, leakage

3-CKV-063-0526 none identified by investigation

Valves, dampers 3-CKV-063-0526 internal leakage when fully seated

Due to:

leakage when fully seated; Primary Containment-GE containment penetrations, air locks, hatches, 3-STRU-202 DIMINIEAD loce of proceeding houndary function. containment panetrations air locks hatches 3-FDENL

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Contact

Frederick Nilsen 2958

Containment Leak Rate Program Engineer fjnilsen@tva.gov

256-729-

Equipment Details

Key:

Component Causing Fallure: High Pressure Coolant Injection-GE Valves, dampers 3-FCV-073-0026 internal leakage when fully seated After 9862 days in service Industry Common Name: *HPCI Suct From Supp Pool Isol Valve Manufacturer: Crane Valve Prod/Crane Co Fr Chapman Model: CD-06005-8-06 Generic Model: CD-06005-8-06 **Body Material : Carbon Steel** Function/Application : Shutoff/Isolation/Stop Nominal Inlet Size (Range) : 12 to 19.99 IN Operator : Electric Motor/Servo (MOV) Type (Parts List) : Gate

Causes of Component Failure:

Component Causing Failure: Key:

Causes of Component Failure:

3-FCV-073-0026 wedge Due to:

management, delayed implementation of corrective actions resource management, resources not available or insufficient Function restored by: repaired device (beyond recalibration) **Recurrence Prevented by:** overhauled or refurbished equipment Main Steam-GE Valves, dampers 3-FCV-001-0056 internal leakage when fully seated After 3081 days in service Industry Common Name: Primary Cntmnt Isol Valve Manufacturer: Velan Valve Corp Model: B107144B02AA Generic Model: B107144B02AA **Body Material : Carbon Steel** Function/Application : Shutoff/Isolation/Stop Nominal Inlet Size (Range) : 2 to 3.99 IN Operator : Electric Motor/Servo (MOV) Type (Parts List) : Gate

3-FCV-001-0056 disc

3-FCV-001-0056 mechanical stop(s)

3-FCV-001-0056 seat

Due to:

design, inadequate original design

management, delayed implementation of corrective actions resource management, resources not available or insufficient

incufficient

resource management, resources not available or

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Component Causing Failure: Key :

Causes of Component

Component Causing Failure: Key :

Causes of Component Fallure:

Component Causing Failure: Key :

Function restored by: repaired device (beyond recalibration) tested and restored to service **Recurrence Prevented by:** administrative controls applied or evaluated established plan for replacement of components **Primary Containment-GE** Containment penetrations, air locks, hatches 3-EPEN-100-0101C loss of pressure boundary function After 11596 days in service Site Common Name: Recirc Pump Power Electrical Penetration Manufacturer: General Electric Company Model: F01 Generic Model: F01 Subcategory (Parts List) : Electrical 3-EPEN-100-0101C sealant Due to: equipment aging - nonmetallic parts, abnormal or accelerated wear Function restored by: tested and restored to service **Recurrence Prevented by:** engineering analysis performed **Primary Containment-GE** Containment penetrations, air locks, hatches 3-STRU-303-DW/HEAD loss of pressure boundary function After 11596 days in service Site Common Name: Drywell Head Manufacturer: Pittsburgh - Des Moines Steel Co (PDM) Model: A Generic Model: A Subcategory (Parts List) : Other 3-STRU-303-DW/HEAD gasket/seal/o-ring(s) Due to: equipment aging - metallic parts, normal wear Function restored by: installed temporary alternative to device function **Recurrence Prevented by:** engineering analysis performed written instructions or documents revised Radwaste-GE

Valves, dampers 3-FCV-077-0002A internal leakage when fully seated *After* 9862 days in service *Site Common Name:* Primary Cntmnt Isol Valve *Manufacturer:* Velan Inc *Model:* B10-064B-2TS *Generic Model:* 0064B Body Material : Carbon Steel Function/Application : Shutoff/Isolation/Stop Nominal Inlet Size (Range) : 2 to 3.99 IN Operator : Pneumatic (Diaphragm or Cylinder) (AOV)

Nominal Inlet Size (Range) : 2 to 3.99 (N Operator : Becumptic (Disphragm or Outinder) (AQV)

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Causes of Component Failure:

Component Causing Fallure: Key :

Causes of Component Failure:

Component Causing Failure: Key :

Causes of Component Failure: Type (Parts List) : Gate

3-FCV-077-0002A disc

3-FCV-077-0002A seat

Due to: equipment aging - metallic parts, normal wear Function restored by: modified the design **Recurrence Prevented by:** design changes implemented **Reactor Water Cleanup-GE** Valves, dampers 3-CKV-069-0628 internal leakage when fully seated After 1546 days in service Site Common Name: Primary Cntmnt Isol Valve Manufacturer: Anchor / Darling Co. Model: 900/W9223821A Generic Model: 900/W9223821A Function/Application : One-Way Flow Nominal Inlet Size (Range) : 4 to 11.99 IN **Operator : None** Program : Appendix J LLRT program SubType : Check-Swing Type (Parts List) : Check

3-CKV-069-0628 bonnet

Due to:

installation, improper assembly installation, inadequate assembly or installation instructions

Function restored by: recalibrated/adjusted device tested and restored to service **Recurrence Prevented by:** supplemental checks or inspections performed **Reactor Water Cleanup-GE** Valves, dampers 3-CKV-069-0629 internal leakage when fully seated After 1546 days in service Site Common Name: Primary Cntmnt Isol Valve Manufacturer: Anchor/Darling Valve Co. Model: 900/w9223821a Generic Model: 900/W9223821A Function/Application : One-Way Flow Nominal Inlet Size (Range) : 4 to 11.99 IN **Operator** : None Program : Appendix J LLRT program Service : Clean water SubType : Check-Swing Type (Parts List) : Check Use : System, line, or component isolation check

3-CKV-069-0629 seat insert

Due to:

J-UNV-UDY-UDZY Seat Insert





Component Causing Failure: Key :

Function restored by: repaired device (beyond recalibration) **Recurrence Prevented by:** overhauled or refurbished equipment Standby Liquid Control-GE Valves, dampers 3-CKV-063-0526 internal leakage when fully seated After 9862 days in service Industry Common Name: *SBLCS Cntmnt Isol Check Valve Manufacturer: Velan inc Model: W7234B13MS Generic Model: W7234B13MS **Body Material : Carbon Steel** Function/Application : One-Way Flow Nominal Inlet Size (Range) : 1/2 to 1.99 IN **Operator : None** Type (Parts List) : Check 3-CKV-063-0526 disc 3-CKV-063-0526 spring(s)

equipment aging - nonmetallic parts, abnormal or accelerated wear

Causes of Component Failure:

•

Associated Maintenance:

Manufacturer: Velan Valve Corp Unit: Duane Arnold 1 Generic Model Number: P122ON4 MR System: Standby Liquid Control

management, delayed implementation of corrective actions

Top |Prev|

Duane Arnold 1

Failure Number : 167

Bookmarks: Abstract

Abstract

Contact

Due to:

Planned

Function restored by:

Recurrence Prevented by:

repaired device (beyond recalibration)

overhauled or refurbished equipment

Equipment Details

Duane Arnold 1- Failure Number :167

11/03/1999 - No plant effect, from cold shutdown. No generation capability was lost. A Velan Valve Corp model P122ON4 (P122ON4), failure caused the event. Standby Liquid Control valves, dampers, V26-0008internal leakage when fully seated.

Contact

Bowman, Bob

Project Engineering, Mechanical

319-851-7729

n/a

Equipment Details

Component Causing Failure: Key : Standby Liquid Control Valves, dampers V26-0008

Component Causing Failure:

Standby Liquid Control

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internal leakage when fully seated After 9380 days in service Industry Common Name: *SBLCS Cntmnt Isol Check Valve Manufacturer: Velan Valve Corp Model: P122ON4 Generic Model: P122ON4 Body Material : Austenitic Stainless STL-316 Function/Application : One-Way Flow Nominal Inlet Size (Range) : 1/2 to 1.99 IN Operator : Mechanical (Differential-Press Open/Spring-Force Close) Type (Parts List) : Check V26-0008 Not yet determined Due to: equipment aging - metallic parts, normal wear mechanical process, leakage Function restored by: repaired device (beyond recalibration) **Recurrence Prevented by:** actions to prevent recurrence not needed Planned

Causes of Component Failure:

Associated Maintenance:

INPO

Equipment Performance and Information Exchange 4.0

Production Read Only

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=NPRDS=

Failure Report with Unit Information

Go to: System Information || Component Information || Failure Information || Failure Narrative

G. Size (Inlet):	
Unit Information	
Utility:	Commonwealth Edison Company
Unit:	DRESDEN 3
NSSS:	General Electric
System Information	Return to Top
System:	Standby Liquid Control-GE
Utility System:	1100
Component Information	Return to Top
Component:	Valves, dampers
Utility Component ID:	3-1101-15
Application:	*SBLCS Cntmnt Isol Check Valve
Data Start Date:	07/01/1974
In-Service Date:	10/05/1971
Out-of-Service Date:	
Manufacturer:	Crane Co
Mfr Model ID:	3888
Mfr Model No:	3888XU
Mfr Serial No.	
Drawing No.	PID-M-364
Safety Class	S
Engineering Characteristics	
A. Type:	Check
B. Operator:	None
C. Function/Application:	One-Way Flow
D. Body Material:	Austenitic Stnls Stl-Other
F. Nominal Inlet Size (Range):	1/2 to 1.99 IN
1.500 IN	
H. Maximum Design Pressure:	1500.000 PSIG
J. Maximum Design	575.000 DEGF
Temperature:	
User Data/Comments	
Data/Comments 1:	G , M

User Data/Comments

91~DRESDEN 3~Valves, dampers

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Data/Comments 2:	C, G
Data/Comments 3:	USAS B16.5
Data/Comments 4:	G0
Data/Comments 5:	3-1101-15

Return to Top
02/19/1991
12:00
12/12/1991
G - Resulted in No Significant Effect
PCA - Standby Liquid Control-GE
D - Degraded Train/Channel
K - Degraded
IL - Internal Leakage
B - Maintenance/Test
J - Other Devices
AB - Foreign Material/Substance (incld AJ before 4/94) BG - Corrosion
AG - Repair Component/Part
N - Other Documents or Records are Not Available

Failure Narrative

Return to Top

UNIT WAS IN A REFUELING OUTAGE WITH THE STANDBY LIQUID CONTROL (SBLC) TRAIN IN TEST. THE SBLC INBOARD INJECTION CHECK VALVE WAS BEING LOCAL LEAK RATE TESTED (LLRT) AND FAILED AT 40 SCFH. THIS WAS NOT LLRT TESTED THE LAST REFUELING OUTAGE AND HAD TO BE TESTED DURING THIS CURRENT OUTAGE. THE TRAIN WAS DEGRADED BUT THE FAILURE HAD NO EFFECT ON THE UNIT.

THE FAILURE WAS DUE TO A BUILD UP OF CORROSION AND MATERIAL ON THE VALVE SEAT .

THE VALVE WAS DISASSEMBLED AND CLEANED AND WAS THEN SUCCESSFULLY RETESTED . (WR D96746)

Contact at Time of Failure John Reid Return to Top 815-942-2920 x2380

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=NPRDS=

Failure Report with Unit Information

Go to: System Information || Component Information || Failure Information || Failure Narrative

G. Size (Inlet): Unit Information Utility: Unit: NSSS:

System Information System: Utility System:

Component Information Component: Utility Component ID:

Application:

Data Start Date: In-Service Date: **Out-of-Service** Date: Manufacturer: Mfr Model ID: Mfr Model No: Mfr Serial No. Drawing No. Safety Class **Engineering Characteristics** A. Type: B. Operator: C. Function/Application: D. Body Material: F. Nominal Inlet Size (Range): 1.500 IN H. Maximum Design Pressure: J. Maximum Design Temperature:

Commonwealth Edison Company QUAD CITIES 1 General Electric

Return to Top Standby Liquid Control-GE 1100

Return to Top Valves, dampers 1-1101-16 *SBLCS Cntmnt Isol Check Valve Primary Cntmnt Isol Valve 07/01/1974 10/07/1971

Crane Co 3888 3888-XU

M-40 S

Check None One-Way Flow Austenitic Stnls Stl-316 1/2 to 1.99 IN

900.000 PSIG

1125.000 DEGF



Temperature:

User Data/Comments

1125.000 DEGF

92-QUAD CITIES 1-Valves, dampers

A, B, F F. 4

LLRT

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Data/Comments	1:
Data/Comments	2:
Data/Comments	3:
	Data/Comments

Failure Information

Discovery Date:

Discovery Time:

System Affected:

System Effect:

Severity Level: Failure Mode:

Failure Detection:

Corrective Action:

Documentation: LER Report Number:

Failure Cause Category:

Failure Cause Description:

End Date:

Plant Effect:

Return to Top 11/13/1992 12:00 06/10/1994 G - Resulted in No Significant Effect PCA - Standby Liquid Control-GE E - System Function/Operation Unaffected K - Degraded IL - Internal Leakage B - Maintenance/Test K - Unknown (included Code X prior to 4/94) AD - Normal Wear (included AH before 4/94) AK - Valve Seat Condition (code added 4/94) AH - Replace Part(s) N - Other Documents or Records are Not Available

Failure Narrative

Return to Top

UNIT SHUTDOWN FOR REFUELING . DURING LOCAL LEAK RATE TEST , STANDBY LIQUID CONTROL (SBLC) OUTBOARD ISOLATION VALVE (1 OF 2) FAILED TO MAINTAIN REQUIRED LEAK RATE INTEGRITY . VALVE LEAKED BY AT 16.0 SCFH . REQUIRED ACTION LIMIT IS 10.0 SCFH . THESE CHECK VALVES ARE DESIGNED TO ISOLATE THE REACTOR FROM ANY LINE BREAK IN THE SBLC SYSTEM TO PREVENT LOSS OF VESSEL INVENTORY WHILE THE VESSEL IS AT PRESSURE . DUE TO SATISFACTORY INTEGRITY OF THE INBOARD ISOLATION CHECK VALVE , LEAKAGE DEGRADED ONLY ABILITY OF THIS CHECK VALVE TO ISOLATE THE VESSEL , THE ISOLATION CAPABILITY OF THE LINE WAS NOT DEGRADED . UNIT WAS NOT AFFECTED BECAUSE A SAFETY EVALUATION WAS PERFORMED WHICH ALLOWED CONTINUED OPERATION AT THE MEASURED LEAK RATE OF 16.0 SCFH UNTIL THE NEXT SCHEDULED OUTAGE .

ON DISASSEMBLY THE DISC WAS FOUND NOT SEATING PROPERLY AND THE DISC WAS SCORED WHERE IT CONTACTED THE SEAT . ROOT CAUSE IS UNKNOWN . SUSPECTED CAUSES INCLUDE NORMAL WEAR AND EROSION .

THE IN-BODY SEATS WERE LAPPED . THE DISC AND DISC GUIDE WERE REPLACED . THE VALVE WAS REASSEMBLED AND INSTALLED . A LOCAL LEAK RATE TEST WAS PERFORMED AND PASSED AT 2 . 9 SCFH . (Q04090)

Contact at Time of Failure Kristal Moore <u>Return to Top</u> 309-654-2241 x3070

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=NPRDS=

Failure Report with Unit Information

Go to: System Information || Component Information || Failure Information || Failure Narrative

G. Size (Inlet): Unit Information Utility: Unit: NSSS:

System Information System: Utility System:

Component Information Component: Utility Component ID: Application: Data Start Date: In-Service Date: **Out-of-Service** Date: Manufacturer: Mfr Model ID: Mfr Model No: Mfr Serial No. Drawing No. Safety Class **Engineering Characteristics** A. Type: **B.** Operator: C. Function/Application: D. Body Material: F. Nominal Inlet Size (Range): 1.500 IN H. Maximum Design Pressure: J. Maximum Design Temperature: **User Data/Comments** Data/Comments 1:

Public Service Electric and Gas Company HOPE CREEK 1 General Electric

Return to Top Standby Liquid Control-GE BH

Return to Top Valves, dampers 1BHV-029 *SBLCS Cntmnt Isol Check Valve 12/20/1986 06/28/1986

Rockwell Int/ Flow Control Div 36274 1.5-36274T1

P&ID M-48-1 S

Check None One-Way Flow Austenitic Stnls Stl-316 1/2 to 1.99 IN

1525.000 PSIG 575.000 DEGF

S

User Data/Comments

92-HOPE CREEK 1-Valves, dampers

Page	2	of	2

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Data/Comments 2:	A, F
Data/Comments 3:	ASME III
Data/Comments 4:	R3

Failure Information Discovery Date: Discovery Time: End Date: Plant Effect: System Affected: System Effect: Seventy Level: Failure Mode: Failure Detection: Failure Cause Category: Failure Cause Description: Corrective Action: Documentation: LER Report Number: Return to Top 10/07/1992 12:00 10/18/1992 G - Resulted in No Significant Effect PCA - Standby Liquid Control-GE E - System Function/Operation Unaffected K - Degraded IL - Internal Leakage B - Maintenance/Test H - Age/Normal Usage AD - Normal Wear (included AH before 4/94) AG - Repair Component/Part N - Other Documents or Records are Not Available

Failure Narrative

Return to Top

THE PLANT WAS IN MODE 5, REFUELING OUTAGE 4, WHEN THE INSERVICE TEST GROUP REPORTED THE STANDBY LIQUID CONTROL (SBLC) SYSTEM INBOARD CONTAINMENT ISOLATION CHECK VALVE, 1 OF 2, FAILED THE LOCAL LEAK RATE TEST (LLRT) DEGRADING THE CONTAINMENT FUNCTION OF THE VALVE. THERE WAS NO SIGNIFICANT AFFECT ON THE OPERATION OF THE SYSTEM OR PLANT. THE VALVE INTERNALS HAD LIGHT DEPOSITS OF DIRT THAT PREVENTED PROPER VALVE SEATING. THE DIRT WAS ATTRIBUTED TO NORMAL WEAR. THE SEAL WELD WAS CUT, THE VALVE DISASSEMBLED, INSPECTED, CLEANED INTERNALS, PERFORMED BLUE CHECK, INSTALLED INTERNALS AND REWELDED PER CODE JOB PACKAGE, SATISFACTORILY TESTED AND RETURNED TO SERVICE. (92-09-42); WO-921007215

Contact at Time of Failure Benjamin Tashjian

Return to Top 609-339-5582

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=NPRDS=

Failure Report with Unit Information

Go to: System Information || Component Information || Failure Information || Failure Narrative

G. Size (Inlet):	· · · · ·		
Unit Information			
Utility:	Commonwealth Edison Comp	any	
Unit:	DRESDEN 2	· .	
NSSS:	General Electric		
System Information	Return to Top		
System:	Standby Liquid Control-GE		
Utility System:	1100		
Component Information	Return to Top		
Component:	Valves, dampers		
Utility Component ID:	2-1101-4		
Data Start Date:	07/01/1974		
In-Service Date:	01/07/1970		
Out-of-Service Date:	03/15/1994		
Manufacturer:	Crane Co		
Mfr Model ID:	47-1/2		
Mfr Model No:	47.5U		
Mfr Serial No.		· · .	
Drawing No.	PID-M-33		
Safety Class	S		
Engineering Characteristics			
A. Type:	Globe		
B. Operator:	Manual	·	
C. Function/Application:	Shutoff/Isolation/Stop		
D. Body Material:	Carbon Steel		
F. Nominal Inlet Size (Range):	2 to 3.99 IN		
2.500 IN			
H. Maximum Design Pressure:	150.000 PSIG		
J. Maximum Design			
Temperature:	500.000 DEGF		
User Data/Comments		·.	
Data/Comments 1:	F, N	•	· .
Data/Comments 2:	A, F		
 USEI LARA COMMENS			
User Data/Comments			

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Data/Comments 4:	S0
Data/Comments 5:	1101-4

Failure Information	Return to Top
Discovery Date:	10/07/1990
Discovery Time:	12:00
End Date:	12/17/1990
Plant Effect:	G - Resulted in No Significant Effect
System Affected:	PCA - Standby Liquid Control-GE
System Effect:	C - Loss of One or More Train/Channel Functions
Severity Level:	J - Complete
Failure Mode:	FC - Failed to Close
Failure Detection:	B - Maintenance/Test
Failure Cause Category:	J - Other Devices
Failure Cause Description:	BF - Flow Obstruction (included BM before 4/94) BE - Dirty
Corrective Action:	AG - Repair Component/Part
Documentation:	N - Other Documents or Records are Not Available
LER Report Number:	

Failure Narrative

Return to Top

UNIT WAS IN COLD SHUTDOWN WITH STANBBY LIQUID CONTROL (SBLC) TRAIN IN TEST. MAINTENANCE AND OPERATIONS PERSONNEL WERE PERFORMING AN OPERABILITY TEST, WHEN SBLC VALVE 1101-4, WHICH IS NORMALLY OPEN WOULD NOT GO CLOSED. THE VALVE WAS TRIED A SECOND TIME WITH NO SUCCESS. THE TRAIN ISOLATION FUNCTION WAS LOST BUT THERE WAS NO PLANT AFFECT. THE FAILURE TO THE VALVE WAS DUE TO BUILD UP OF BORON IN THE INTERNAL PARTS OF THE VALVE. THIS BUILD UP OF BORON PREVENTED THE VALVE FROM OPERATING AS INTENDED.

THE VALVE WAS REMOVED, CLEANED AND WHILE THE VALVE WAS DISASSEMBLED THE PACKING WAS ALSO REPLACED. THE VALVE WAS REINSTALLED AND SUCCESSFULLY TESTED FOR OPERABILITY. THE VALVE WAS THEN RETURNED TO SERVICE. (WR 88244)

Contact at Time of Failure John Reid Return to Top 815-942-2920 x2380

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=NPRDS=

Failure Report with Unit Information

Go to: System Information || Component Information || Failure Information || Failure Narrative

G. Size (Inlet): Unit Information Utility: Unit: NSSS:

System Information System: Utility System:

Component Information Component: Utility Component ID: Data Start Date: In-Service Date: Out-of-Service Date: Manufacturer: Mfr Model ID: Mfr Model No: Mfr Serial No. Drawing No. Safety Class **Engineering Characteristics** A. Type: **B.** Operator: C. Function/Application: D. Body Material: F. Nominal Inlet Size (Range): 3.000 IN H. Maximum Design Pressure: J. Maximum Design Temperature: **User Data/Comments** Data/Comments 1: Data/Comments 2:

User Data/Comments 1.

PP&L, Inc. SUSQUEHANNA 1 General Electric

Return to Top Standby Liquid Control-GE 153A

<u>Return to Top</u> Valves, dampers 148F031 06/08/1983 06/08/1983 03/15/1994 Aloyco Div./Walworth Co.

N-226-SP

P&ID-M-148 S

Gate Manual Shutoff/Isolation/Stop Austenitic Stnls Stl-316 2 to 3.99 IN

100.000 PSIG 150.000 DEGF

X F, 4

x

86~SUSQUEHANNA 1~Valves, dampers

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Data/Comments 3:ASME-SEC.IIIData/Comments 4:W0Data/Comments 5:C41-1F031

Failure Information

Discovery Date: Discovery Time: End Date: Plant Effect: System Affected: System Effect: Severity Level: Failure Mode: Failure Detection: Failure Cause Category:

Failure Cause Description:

Corrective Action: Documentation: LER Report Number:

Failure Narrative

Return to Top 08/12/1986 12:00 09/10/1986 G - Resulted in No Significant Effect PCA - Standby Liquid Control-GE D - Degraded Train/Channel K - Degraded FC - Failed to Close B - Maintenance/Test K - Unknown (included Code X prior to 4/94) BB - Mechanical Damage (included BK before 4/94) BC - Out of Mechanical Adjustment AG - Repair Component/Part N - Other Documents or Records are Not Available

A

Return to Top

ON AUGUST 12, 1986, THERE WAS SODIUM PENTABORATE SOLUTION LEAKING FROM THE STANBY LIQUID CONTROL (SBLC) STORAGE TANK INTO THE SBLC TEST TANK. TEST TANK OUTLET VALVE 148F031 WAS FOUND TO BE LEAKING THROUGH ALLOWING SBLC TANK LEVEL TO RISE.

AFTER INVESTIGATION IT WAS DETERMINED THE CAUSE OF THIS EVENT WAS DUE TO THE BOTTOM SIDE OF THE VALVE DISC MAKING CONTACT WITH THE BOTTOM OF THE VALVE BODY. ACTUAL ROOT CAUSE UNKNOWN.

GROUND THE VALVE DISC AND PERFORMED BLUE CHECK ON VALVE BODY UNTIL NO CONTACT WAS NOTED . STROKED VALVE AND VERIFIED NO BONNET GASKET LEAK AT SYSTEM OPERATING PRESSURE VALVE RETURNED TO SERVICE .

Contact at Time of Failure Terry Constance Return to Top 610-774-7608



EC-	053-1	012
Re	ivisio	n 0
Page	104 (of 138

1

	PP&L CALCULATI				
Dept	PROJECT	Calc. No.	EC-053-1012		
Date	Assessment of SBLC	Rev. No.	0		
Designed By G.Kowal Checked By	System for Suppression Pool pH Control	Sh. No.	1 — of	14	
		QII. 140.	Ui	1-1	

ATTACHMENT NO. 3

Susquehanna - Valve Operating Experience

Kowal, George M

From: Sent: To: Cc: Subject: Missien, Ian C Monday, March 21, 2005 3:59 PM Kowal, George M Vazquies, Ronald Allen; Maertz, Gerald G Standby Liquid Control (SLC) Outboard Containment Isolation Valve, 1(2)48F007

Mr. Kowal,

The SLC O/B Containment Isolation Valves, 1(2)48F007 have performed very well for PPL Susquehanna, LLC. A review of work history on these valves shows no failures. Typically, the leakage rates for these valves is nil (0-10 cc/min). Reference SE-1(2)59-047 (LLRT of Penetration X-42) and the work history in NIMS via the CMPINFO screen.

lan C. Missien 254-3396

Component Data Sheet

EC-053-1012 CRH2vision ORCPECDA1 Page 106 of 138

19203A	·····	STADDI LIO G	DNITROL FU	E 020		
Parent ID:				Unit :	1	Fail Code: 2B
бува	153A			Area ;	29	Maint Rule: 1
Manufacturer:	UNION PMP	ASME :	Y	Elev :	749	Criticality: 1
Model Nc.;	2X3 TD-60 TRIPLEX	ASEC	III	Act. Elev:	750.5	Duty Cycle:
Part No.:	TBD	Q:	Q	Room :	I-513	Environment
Serial No.:	284222	EQ:	N	Bldg :	RX	
Install Date:	26-JAN-1996	Comp. Type:	PUMP	Col/Line :	7526.5/4WT	
		Design Status:	ASELT	Azimuth :		
Locz						

Description:

Relationsh	ip ID			Name			Component	- Turne	
		· · · · · · · · · · · · · · · · · · ·	·		· ·			туре	
IS BLOCKED	BY 18:	236081			CONTROL INJECTIO	N PUMP	SUBPNL	•	
IS POWERED	BY 1B:	236081		A 19208A BKR STANDBY LIQUID A 19208A BKR	CONTROL INJECTIO	N PUMP	SUBPNL		
			Deed	T Characteria	ieles			· · · · · · · · · · · · · · · · · · ·	
ategory	Nane	<u></u>		Value		Unit			
OM	MOTOR SPEED			NULL		Revol	utions		
IOM	POWER RATING			40		hp			
IOM	SCAFFOLDING HEIG	GHT		0.0		foot			
IOM	VOLTAGE			460		volt	AC		
			Physi	ool Charactori	Jettes				
ategory	Name			Value		Unit			
/A	MOTOR TYPE			NULL		n/a			
/A	MANUFACTURER			NULL		n/a			
/A	MODEL NUMBER			NULL		n/a		•	
/A	SERIAL NUMBER			NULL		n/a			
/A	MOTOR FRAME			NULL		n/a			
/A	ORIENTATION			NULL		n/a			
OM	STATOR FULL LOAD	AMPS		NULL		Апр			
	MOTOR LOCKED ROT	for Amps		NULL	· · · · ·	Атр	- 1 - E - E - E - E - E - E - E - E - E		
	MOTOR PHASE			NULL	÷ .	n/a		:	
/A />	STATOR INSUL THE	,		NULL		n/a			
_	MOTOR ENCLOSURE			NULL		n/a	•		
_	MOTOR SERVICE FA			NULL		n/a			
	MOTOR TEMPERATUR			NULL		n/a			
	MOTOR SPACE HEAT OIL COOLING COIL			NULL NULL		n/a n/a			
_	UPPER OR OB BEAR			NULL		n/a n/a			
	LOWER OR IB BEAR			NULL		n/a			
	UPPER OR OB BEAR			NULL		n/a			
	LOWER OR IB BEAR			NULL		n/a			
	UPPER OR OB BEAR			NULL		n/a			
	LOWER OR IB BEAR			NULL		n/a			
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	DC MOTOR WINDING			NULL		Алр	i		
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BEARINGS	MOTOR	ALVANIA			0000935656		?		
PAC	GR	HARMONY	68 AW ((DRUM)	0091202198		7		
age 1 0	f 2 f 2	ment caraton	Naurs		Catalog no. Re	port D	ate: 23-	MAR-200	5
PADINCO	MOTOR	AIJVANIA			0000935656		~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~		

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106179		5	26	Y	M-29-5	1	26	PLANT DESIGN DRAWING	REACTOR BLDG AREA 29
106253		1	27	N	M-148	1	27	PLID STANDBY LIQUID	CONTROL
IOM5		1	2	N	M1-C41-21	1	2	TRIPLEX POWER PUMPS	TD-60 OR STANDBY LIQU
. [1961			Groups			
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PP&I NIMS		Compon	ent Data	a Sheet	EC-053-1012 Revision 0 Page 108 of 138	CFX -	RCPECDA1
1485007		8					
Parent ID:				Unit :	ì	Fail Code:	1B
Sys:	153A		•	Area :	26	Maint Rule:	1
Manufacturer:	BORG WAR	ASME:	Υ	Elev :	739	Criticality:	1
Model No.:	?	ASEC:	III,NB	Act. Elev:	739	Duty Cycle:	÷
Part No.:	TBD	· · · · · · · · · · · · · · · · · · ·	Q	Room :	I-400	Environment:	
Serial No.:		EQ:	N	Bldg :	CNTMI		
Install Date:	08-MAR-1996	Comp. Type:	СК	Col/Line :			
Loc:		Design Status:	ASBLT	Azimuth :	15 170		

Description:

Category	Name	Value	Unit	
N/A	PIPE CLASS	DCA	n/a	
N/A	PIPE LINE 1D	106,	n/a	
NORM	PRESSURE	1005	psi	
N/A	PIPE SCHEDULE	805	n/a	• .
n/a	BONNET ATTACHMENT	SLNLD	n/a	
NOM	SCAFFOLDING HEIGHT	7.0	foot	
NOM	SIZE	1.50	inch	
NORM	TEMPERATURE	547	deg F	
N/A	VALVE TO PIPE ATTACHMENT	SOCKET WELD	n/a	
N/A	VALVE CLASS	CCA	n/a	
N/A	VALVE OPERATOR TYPE	SPRING OPERATED	n/a	

Category	Name	Value	Unit
N/A	VALVE BODY MATERIAL	SA182-F316	n/a
N/A	VALVE TRIM MATERIAL	STELL	n/a
NOM	STEM OUTSIDE DIAMETER	0	inch
NOM	STUFFING BOX INSIDE DIAMETER	0	inch
NOM	STUFFING BOX DEPTH	NULL	inch
NOM	LEAKOFF PORT DEPTH	NULL	inch
N/A	LEAKOFF ACTIVE	NULL	n/a
NOM	LANTERN RING HEIGHT	NULL	inch
NOM	STUD OUTSIDE DIAMETER	NULL	inch
NOM	NUT SIZE	NULL	inch
NOM	CRANE "B" FACTOR	NULL	n/a
MOM	GLAND LENGTH	NULL	inch
\$/A	NUMBER OF STUDS	NULL	n/a
NOM	LOWER BUSHING HEIGHT	NULL	inch
NOM	UPPER BUSHING HEIGHT	NULL	inch
NOM	PACKING SET HEIGHT (REPACK)	0	inch
MON	NUMBER OF WASHERS/STUD	NULL	n/a
N/A	VALVE PACKING TYPE (REPACK)	NULL	n/a
JOM	PACKING STRESS	1	lbs
K/A	PACKING CONFIGURATION (REPACK)	NULL	n/a
I/A	TRANSFER RATIO (REPACK)	0	n/a
V/A	PACKING COEFFICIENT OF PRICTION (REPACK)	0	n/a
1/A	LOWER BUSHING CAT #	NULL	n/a
1/A	UPPER BUSHING CAT #	NULL	n/a
/A	PRIMARY PACKING CAT #	NULL	n/a
I/A	FLAT WASHER CAT #	NULL	n/a
	of 2		Report Date: 14-MAR-2005
/A	UPPER BUSHING CAT #	NULL	n/a

NULL

n/a

N/A N/A PRIMARY PACKING CAT #

Divgloci Characterizitien Unit Category Mame Unit N/A Live LOAD WASHER CAT # NULL n/A NMA LATERN RING CAT # NULL n/A NOM PACHING SET HETGAT (RETORQUE) 0 JAC NMA PARTIC (RETORQUE) 0 JAC N/A TRANSFER RATIO (RETORQUE) 0 JAC Labe Location Lube Component Catalog Name Catalog No. Classical 1 27 PALHES No. Labe Location Lube Component Retor A Ember A Ender <							ompor.	ent Dat		E Pao	e 109 of 138	CPI		RCPECI
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Source Type Level JEAK RATE TESTING REQUIRED (LLRT/ILRT) LEAK RATE TESTING LEAK RATE TESTING Design ZON9 Associations ZON9 Associations Jone Name Status Type Zone Use Comment RAD IN Design: Physical: 148F007 Manufacturer:	SURV V	VALVE I	SI			CATA	GORIES	A and C ap	ply					
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Physical: 148F007 Manufacturer:	Desimi		••••••••			·			*******					
Manufacturer:	-	. 14	8F007											
	-		• •					•				•		
sng. Notes:														
	ang. Not	65:			• •									

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PP&L - NIMS

Component Data Sheet

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Page 110 of 130	

CPX - RCPECDA1

1437000	······································	STANDER DIQUE	CONTROL	EN EN		
Parent ID:				Unit :	1	Fail Code: 1B
Sys:	153A			Area :	26	Maint Rule: 1
Manufacturer:	BORG WAR	ASME:	Y	Elev :	738	Criticality: 1
Model No.:	P/N 74680	ASEC:	III,NB	Act. Blev:	742	Duty Cycle:
Part No.:	TBD	Q:	Q	Room :	1-400	Environment:
Serial No.:	17977	EQ:	N	Bldg :	CNIMT	
Install Date:	26-JAN-1996	Comp. Type:	GT	Col/Line :		
·	·	Design Status:	ASBLT	Azimuth :	15 175	

Loc:

1

Description: STANDBY LIQUID CONTROL INJ ISO

1		Dasign Characteristics		
Category	Name	Value	Unit	······································
N/A	PIPE CLASS	DCA	n/a	
N/A	PIPE LINE ID	106	n/a	
NORM	PRESSURE	1005	psi	
N/A	PIPE SCHEDULE	805	n/a	
N/A	BONNET ATTACHMENT	SLWLD	n/a	
NOM	SCAFFOLDING HEIGHT	0.0	foot	
NOM	SIZE	1.50	inch	
NORM	TEMPERATURE	547	deg F	
N/A	VALVE TO PIPE ATTACHMENT	SOCKET WELD	n/a	
N/A	VALVE CLASS	CCA	n/a	
N/A	VALVE OPERATOR TYPE	HAND OPERATED	n/a	

Category	Name	Value	Unit	
N/A	VALVE BODY MATERIAL	SA182-F316	n/a	
NOM	SUGGESTED NUT TORQUE	85.0	ft-lbs	
N/A	VALVE STEM MATERIAL	SA564~630	n/a	
N/A	VALVE TRIM MATERIAL	STELL	n/a	
NOM	STEM OUTSIDE DIAMETER	0.875	inch	
NOM	STUFFING BOX INSIDE DIAMETER	1.375	inch	
NOM	STUFFING BOX DEPTH	1.625	inch	
NOM	LEAKOFF PORT DEPTH	NULL	inch	
N/A	LEAKOFF ACTIVE	NULL	n/a	
NOM	LANTERN RING HEIGHT	NULL	inch	
MOM	STUD OUTSIDE DIAMETER	0.000	inch	
NOM	NUT SIZE	1.25	inch	
IOM	CRANE "B" FACTOR	NULL	n/a	
tom	GLAND LENGTH	NULL	inch	
:/A	NUMBER OF STUDS	C	n/a	
IOM	LOWER BUSHING HEIGHT	0.312	inch	
MON	UPPER BUSHING HEIGHT	NULL	inch	
IOM	PACKING SET HEIGHT (REPACK)	1.25	inch	
MOM	NUMBER OF WASHERS/STUD	NULL	n/a	
I/A	VALVE PACKING TYPE (REPACK)	COMPOSITE	n/a	
OM	PACKING STRESS	4000	lbs	
/A	PACKING CONFIGURATION (REPACK)	52	n/a	÷.,
/A	TRANSFER RATIO (REPACK)	.85	n/a	
/A	PACKING COEFFICIENT OF FRICTION (REPACK)	. 05	n/a	
/A	LOWER BUSHING CAT #	NULL	n/a	
/A	UPPER BUSHING CAT #	NULL	n/a	,

Page 1 of 2

&/A

(REPACK) LOWER BUSHING CAT #

NULL

Report Date: 14-MAR-2005

n/a

Component Data Sheet

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CPX - RCPECDA1

	Physical Phy	stel chasecoristics		
Category	Name	Value	Unit	
N/A	PRIMARY PACKING CAT #	00910218476	n/a	
N/A	FLAT WASHER CAT #	NULL	n/a	
N/A	LIVE LOAD WASHER CAT #	NULL	n/a	
N/A	LANTERN RING CAT #	NULL	n/a	
NOM	PACKING SET HEIGHT (RETORQUE)	0 · · · · · · · · · · · · · · · · · · ·	inch	
NOM	PACKING STRESS (RETORQUE)	1	psi	÷
N/A	TRANSFER RATIO (RETORQUE)	0	n/a	
N/A	PACKING COEFFICIENT OF FRICTION (RETORQUE)	0	n/a	

					Budg Dour	163			
Lube Location	Lube	Componer	t Cat	alog Name		Cat	alog No.	Quantity	ט/א
				ទ	ealge Docu				
			Latest						
ID	Sheet	Rev.	Rev.	AE No.	AE Sheet	AE Rev.	Descri	ption	1
·····						•			
E106253	1	27	N	M-148	1	27	P&ID STAN	DBY LIQUID C	CONTROL
IOM216	1	8	N	P14B-58	1	8	1 & 1 1/2	4 2 INCH ST	AINLESS GATE & Y TYPE
FF110470	801	13	¥	P14B-8	1	13	ASSEMBLY	1 1/2 INCH G	ATE VALVE

		BGEOGE			
Туре	Name	Description			
COND	ENVIRONMENTAL CONDITION GROUP 6	100 - 140 DEGREES F/HIGH HUMIDITY			·
COND	RADIOLOGICAL CONDITION ZONE 5 GROUP	DOSE RATE >100 mrem/hr.			
nsefeg	UNIT 1 SLC SYS FEG		•	 •	· .

			ZODC	Associat	SLODE	-		
Zone	Name	Status	Туре	Zone Use	Comment		·	
RAD5	RADIATION ZONE V		RAD	IN				
			•	Commentes				

Design: BUSHING INCLUDED IN PACKING SET

Physical: BUSHING INCLUDED IN PACKING SET

Manufacturer:

Eng. Notes:

		Addisional C		· · · · · · · · · · · · · · · · · · ·
Туре	Comment Text			
OPS LOCATIO OPERATIONS	LOC1: AZ175 R742' (FC)	:		

EL - NI	MS	Compon	ent Da	ata Sheet		-053-1012 Revision 0	. CPX -	RCPECDA
1/1/137/00/3		SELC OB ENTES	PION VIA	7				
arent ID:				Unit :	1		Fail Code:	18
ys:	153A	•		Area :	29		Maint Rule:	1
lanufactur	er: YARWAY CORP	ASME :	Y	Elev 1	749		Criticality:	
lodel No.:			III,NB		752		Duty Cycle:	
	•••••••				. –			
art No.:	N/A	Qı	7	Room :	1-506		Environment:	· · · · ·
erial No.		EQ:	•••	Bldg :	RX		•	•
nstall Da	ta: 08-MAR-1996	Comp. Type:	MOV	Col/Line :	1S25/14WT			
_		Design Status:	ASBLT	Azimuth :				
Loci								
escriptio	n: SLC ISO VLV							
							•	
		Rey	କରି କ	mponents				
elationsh	lip ID		Name				Component in	
erectonar		1	Nellite				Component Typ	12
S BLOCKED	BV 18236664			THIROPTON W	IRI_1488000	020	SUBPNL	
S POWERED				INJECTION VLV				
3 FORSKED	BY 18236064			INJECTION VLV	NV-148F006	BKK	SUBPNL	
		Dessign	d Ghar	reterristics				
tegory	Name	1	/alue			Unit	1	
		·					·	
M	MOTOR SPEED	1	(ULL			Revolu	tions	
/A	PIPE CLASS		CA			r/a		
/A	PIPE LINE ID			· .				
			106	1		n/a		
ORM	PRESSURE		1005			psi	1	
A	PIPE SCHEDULE	8	10S			n/a		
/A	BONNET ATTACHMENT	5	SLWLD			n/a		
м	SIZB	. 3	. 50			inch		
DRM	TEMPERATURE	-	547			deg F		
				81 D				
/A /2	VALVE TO PIPE ATTACHMENT		SOCKET WI	للا		n/a		
/A	VALVE CLASS		:CA			n/a	•	
/A	VALVE OPERATOR TYPE	M	IOTOR OPI	ERATED	·	n/a		
		Bazala	ນ ຜີກາ	netorriotion				· · · · ·
	Name		alue			Unit	·····	
/A	ACTUATOR ORDER NO.		A4681A			n/a		
/A	ACTUATOR SIZE		MB-000			n/a	1. 1. A.	
`A .	VALVE BODY MATERIAL		A182-F31	16		n/a n/a		
A ·	REMAINING GLAND TAKE-UP		3125			inch		
Ά	FLAT WASHER INSTALLED (Y/N		•			n/a	•	. *
'A	LIVE LOADED (Y/N)	· Y				n/a n/a		
'A	MOTOR TYPE		ULL			n/a n/a		
'А	MANUFACTURER		ULL	1		n/a n/a		
А 'А	MODEL NUMBER					n/a n/a		
A A	SERIAL NUMBER		ຫມະ ຫມະ	· · · ·		n/a n/a		
А 'А	MOTOR FRAME			· · · · ·		n/a n/a		
A A	ORIENTATION		ULL ULL			n/a n/a		
M								
m M	STATOR FULL LOAD AMPS MOTOR LOCKED ROTOR AMPS		ULL ULT			Amp		
	Motor Ducked Rotor Amps Motor Phase		ULL			Amp n/a		
A.			ULL			n/a n/a		
	STATOR INSUL THERMAL CLASS	,	ULL			n/a n/a		•••
	MOTOR ENCLOSURE TYPE					n/a n/a	• •	
	MOTOR SERVICE FACTOR	•	ULL		· · ·			
	MOTOR TEMPERATURE RISE		ULL			n/a n/a	· .	
	MOTOR SPACE HEATERS (Y/N) OIL COOLING COILS		ULL			n/a n/a		
8	ALL CONTRACTING	N1			• •	/ G	<u>1977 - 1977 - 1977 - 1977 - 1977 - 1977 - 1977 - 1977 - 1977 - 1977 - 1977 - 1977 - 1977 - 1977 - 1977 - 1977</u>	
A								_ جي المجمع الذي المحمد التي
	f 4				Rer	ort Da	te: 14-MAD	-2005
age 1 o	f 4 MOTOR TEMPERATURE RISE	N	UEL		Rep	oort Da n/a	ate: 14-MAR	-2005

Component Data Sheet

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	Phys	eal Characteristics	
Category	Name	Value	Unit
<u> </u>		NULL	n/a
n/a	UPPER OR OB BEARING TYPE.		n/a
N/A	LOWER OR IB BEARING TYPE	NULL	n/a
N/A	UPPER OR OB BEARING NO.	NULL	n/a
1/A	LOWER OR IB BEARING NO.	NULL	n/a
/A	UPPER OR OB BEARING CAPACITY.	NULL	n/a
/A	LOWER OR IB BEARING CAPACITY	NULL	Amp
MOM	DC MOTOR FIELD AMPS	NULL	Алр
iom .	DC MOTOR WINDING AMPS	NULL	volt
NOM	MOTOR VOLTAGE	460	
MOM	Motor Horsepower	.17	hp Se lba
VOM	MOTOR START TORQUE	5	ft-lbs
NOM	MOTOR RUN TORQUE	1	ft-lbs
MOM	MOTOR SPEED	850	rpm
NOM	MOTOR DUTY RATING	15M	n/a
NOM	MOTOR INSUL TYPE/CLASS	B ·	n/a
NOM	MOTOR FRAME	M46	n/a
NOM	MOTOR FULL LOAD AMPS	1	Anp
NOM	MOTOR LOCKED ROTOR AMPS	2	qnA
NOM	MOTOR TEMPERATURE	40	deg C
NOM	SUGGESTED NUT TORQUE	59.0	ft-lbs
NOM	POWER RATING	0.17	hp
MIN	LOWEST ALLOWED TORQUE SWITCH SETTING	1.5	n/a
MAX	HIGHEST ALLOWED TORQUE SWITCH SETTING	2.5	n/a
	SPRING PACK GAP	.305	inch
NOM	SPRING PACK NUMBER OF WASHERS	17	n/a
NOM	VALVE STEM MATBRIAL		n/a
K/A	SPRING PACK WASHER THICKNESS	.065	n/a
NOM		STELL	n/a
N/A	VALVE TRIM MATERIAL	1.5	n/a
NOM	TORQUE SWITCH ACTUAL OPEN SETTINGS	1.5	n/a
NOM	TORQUE SWITCH ACTUAL CLOSE SETTINGS	•	n/a
NOM	MOTOR PINION TEETH	22	n/a
Nom	WORM GEAR TEETH	23	n/a
Nom	MTR PINION TO WSG RATIO	1.04	volt AC
KOM	VOLTAGE	460	inch
Nom	STEM OUTSIDE DIAMETER	0.937	
Nom	STUFFING BOX INSIDE DIAMETER	2.062	inch
Nom	STUFFING BOX DEPTH	2.125	inch
NOM	LEAKOFF PORT DEPTH	N/A	inch
n/a	LEAKOFF ACTIVE	N/A	n/a
Nom	LANTERN RING HEIGHT	N/A	inch
NOM	STUD OUTSIDE DIAMETER	0.75	inch
NOM	NUT SIZE	1.25	inch
NOM	CRANE "B" FACTOR	91	n/a
NOM	GLAND LENGTH	NEED	inch
N/A	NUMBER OF STUDS	2	n/a
NOM	LOWER BUSHING HEIGHT	.437	inch
NOM	UPPER BUSHING HEIGHT	N/A	inch
NOM	PACKING SET HEIGHT (REPACK)	1.25	inch
	NUMBER OF WASHERS/STUD	3	n/a
NOM NAN	VALVE PACKING TYPE (REPACK)	Composite	n/a
N/A		4000	lbs
NOM	PACKING STRESS	37	n/a
N/A	PACKING CONFIGURATION (REPACK)		n/a
N/A	TRANSFER RATIO (REPACK)	.85	n/a
N/A	PACKING COEFFICIENT OF FRICTION	.05	u) e
m / m	(REPACK) Lower Bushing Cat #	0091219152	D/a
N/A		N/A	n/a
N/A	UPPER BUSHING CAT #	0091218662	n/a
n/a	PRIMARY PACKING CAT #	~~3797000%	
Page 2		0001710157	Report Date: 14-MAR-2005 n/a
N/A	LOWER BUSHING CAT #	0091219152 N/D	n/a

- LOWER BUSHING CAT # N/A
- 11/2 _

n/a n/a

N/A

Component Data Sheet

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CPX - RCPECDA1

•	Rhysical Characteristas								
Category	Name	Value	Unit						
N/A	FLAT WASHER CAT #	0091219132	n/a						
N/A	LIVE LOAD WASHER CAT #	0091217318	n/a						
N/A	LANTERN RING CAT #	N/A	n/a						
N/A	GRAPHITE WASHER CAT #	N/A, NEEDS CUT	n/a	. *					
NOM	PACKING SET HEIGHT (RETORQUE)	1.25	inch						
NOM	PACKING STRESS (RETORQUE)	4000	psi						
N/A	TRANSFER RATIO (RETORQUE)	.85	n/a						
N/A	PACKING COEFFICIENT OF FRICTION (RETORQUE)	.05	n/a						

Lube Location	Lube Cor	ponent	Catalog	Nans		Cat	alog Nc.	Quantity	U/M	-
	- <u> </u>			Der	den Doen	100 <u>6</u> 0				
ID	Sheet R	Lat lev. Rev		No.	AE Sheet	AE Rev.	Descri	ption		
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D107315 14 E-166 4 N 14 SCHEMATIC DIAGRAM STANDBY LIQUID CONTROL S 4 E106253 1 27 N M-148 27 1 PLID STANDBY LIQUID CONTROL IOM270-1 1 2 N P14A-32 2 5500 SERIES MOTORIZED VALVES FOR STANDBY L 1 FF110140 1001 8 ¥ P14A-10 1 1/2 INCH YARWAY WELBOND VALVE WITH LIMIT 1 8 FF121010 3602 14 N M1-C41-36 2 14 ELEMENTARY DIAGRAM STANDBY LIQUID CONTROL

		BGEOEED	
Туре	Name	Description	
IST	IST PROGRAM GROUP	. *	
NSEFEG	1B236 ·		1 - 1
nsefeg	Primary Containment Isolation Valves		
NSEFEG	UNIT 1 SLC SYS FEG		
REPORT	NPRDS REPORTABLE GROUP		
SURV	LOCAL LEAK RATE TESTING GROUP	Pre & Post LLRT required	IAW NDAP-QA-0412
SURV	VALVE ISI	CATAGORIES A and C apply	· ·

	Require	1909 (1909)	·····	
Requirement	Source	Туре	Level	·····
10.1 LIMITORQUE SMB AND SB MOV ACTUATOR INSTALLATION	EQ PROGRAM	EQAR-084	Design	
10.1 T&B CRIMPED WIRE JOINT INSTALLATION	EQ PROGRAM	EQAR-091	Design	
10.1 TERMINAL BLOCK INSTALLATION	EQ PROGRAM	EQAR-089	Design	· .
10.2 TEB CRIMPED WIRE JOINT MAINTENANCE	BQ PROGRAM	EQAR-091	Design	
10.2 TERMINAL BLOCK MAINTENANCE	EQ PROGRAM	EQAR-089	Design	•
10.2.1 LIMITORQUE SMB AND SE MOV ACTUATOR MAINTENANCE	EQ PROGRAM	EQAR-084	Design	
10.3 TAB CRIMPED WIRE JOINT CONFIGURATION	EQ PROGRAM	EQAR-091	Design	·
10.3 TERMINAL BLOCK CONFIGURATION	EQ PROGRAM	EQAR-089	Design	
10.3.1 LIMITORQUE SME, SE 460VAC MOV ACTUATOR CONFIGURATION	EQ PROGRAM	EQAR-084	Design	
10.7 LIMITORQUE SMB AND SB MOV ACTUATOR PROCUREMENT	EQ PROGRAM	EQAR-084	Design	
10.7 TEB CRIMPED WIRE JOINT PROCUREMENT	EQ PROGRAM	EQAR-091	Design	
10.7 TERMINAL BLOCK PROCUREMENT	EQ PROGRAM	EQAR-089	Design	
LEAK RATE TESTING REQUIRED (LLRT/ILRT)	LEAK RATE TESTING PROGRAM	LEAK RATE TESTING	Design	
			· · · · · · · · · · · · · · · · · · ·	

Report Date: 14-MAR-2005

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PP&L - NIMS		Component Data Sheet	Revision 0 CPX - RCPECDA1 Page 115 of 138
•		Dasign Documentes	
		CommenCes	
Designa	SLC ISO VLV		
Physical:	LAST REPACKED 3/28/04 CRR NEED CUT. A NEW STEM WAS	CHW TORQUED TO 58 FT/LBS. ALL RINGS AR INSTALLED U1-13RIO.	E .3125" TALL. GRAPHITE WASHER WILL
		Additional Companys	
Type Eng. Notes:	Comment Text		
OPERATIONS	(FC) SUBHEADING: SBLC		
OPS LOCATIO	LOC1: I-506 R752'		
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Report Date: 14-MAR-2005

și - NI	MS		Сопро	nent Dat	a Sheet	:	EC-053-1012 Revision 0 Page 116 of 138	CPX'-	RCPECI
1514803			SHE MANUAL	INNERVICION					
arent ID:	: 1C601				Unit	: 1	F	ail Code:	18
ys:	153A				Area			int Rule:	1
anufactur	cer: ?		ASM	B: N	Elev			ticality:	1
odel No.	•		ASE	C:	Act. Elev	732.5	Du	ty Cycle:	
art No.:	?		· (2= 0	Room	: C-409	Env	ironment:	
erial No.				אים	Bldg	1 CONT			
nstall Da	ate: 18-0CT-20	00	Comp. Type	** S	Col/Line	:		k.	
		I	esign Statu	S: ASBLT	Azimuth	:			
Loc:						_	-153-	- coll	
escriptic	3112			·		64	-15)-		
	maan gewin 19								
		· · · · · · · · · · · · · · · · · · ·	Dest	on Onara	<u>erisida</u>	3		<u> </u>	
Category	Name			Value			Unit		
1/8		N 1 6 2 ADDR3	TONG		· · · · ·			· ·	
1/A (AX	DEVICE RANGE	N 1 & 2 OPERAT	TÁNQ	NULL			n/a TBD		
	DEVICE RANGE I			NULL			TBD		
IN IOM	DEVICE RANGE	· - · · ·	•	NULL			TBD		•
iom (Ax	PROCESS RANGE								·
				NULL			TBD		
IN	PROCESS RANGE			NULL			TBD		
юь(+)	PROCESS RANGE			NULL			TBD		
OL (-)	PROCESS RANGE			NULL	,		TED		
	PROCESS SETPO			NULL			TBD	1 1	
OL(+)	PROCESS SETPOI			NULL			Ted Ted		
юц(-) //а	PROCESS SETPOI SETPOINT REVIS			NULL					
OL(-)	DEVICE SETPOIN		(-) TO	NULL			n/a TED		
OL(+)	DEVICE SETPOIN		-	NULL			TBD		
				Buba Pola	1 2 -3				£
Lube Loca	ation Lube Co	mponent Ca	talog Name		Cat	alog No.	Quantity	ע/ע	
		Latest	Ð	reed Topic	nen 68		······································		· · · · · · · · · · · · · · · · · · ·
D .	Sheet 1	Rev. Rev.	AE No.	AE Sheet	AE Rev.	Descri	ption		
107315	1 1	19 N	E-166	1	19	SCHEMATIC	DIAGRAM STAN	BY LIQUID	CONTROL
107315	1 2	20 Y	E-166	1	20		DIAGRAM STAND	-	CONTROL
106253		27 N	M-148	1	27		DBY LIQUID CON		
162128	2 1	15 N	J-802	2	15	LAYOUT EN	ERGENCY CORE C	OOLING BEN	ICHBOARD
				କ୍ଟୋଡ୍ସେଡି					
ype Na		·	Descriptio	on H					
	NT 1 SLC SYS FE	EG			· · ·				
sepeg un				Comment	Ø				
Sepeg un									:
SEPEG UN Design:							i i i		
	HS14804	•						7	
Design: Physical:	HS14804	d created to s		lordier our					

Page 1 of 2

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Comment Text

Report Date: 14-MAR-2005

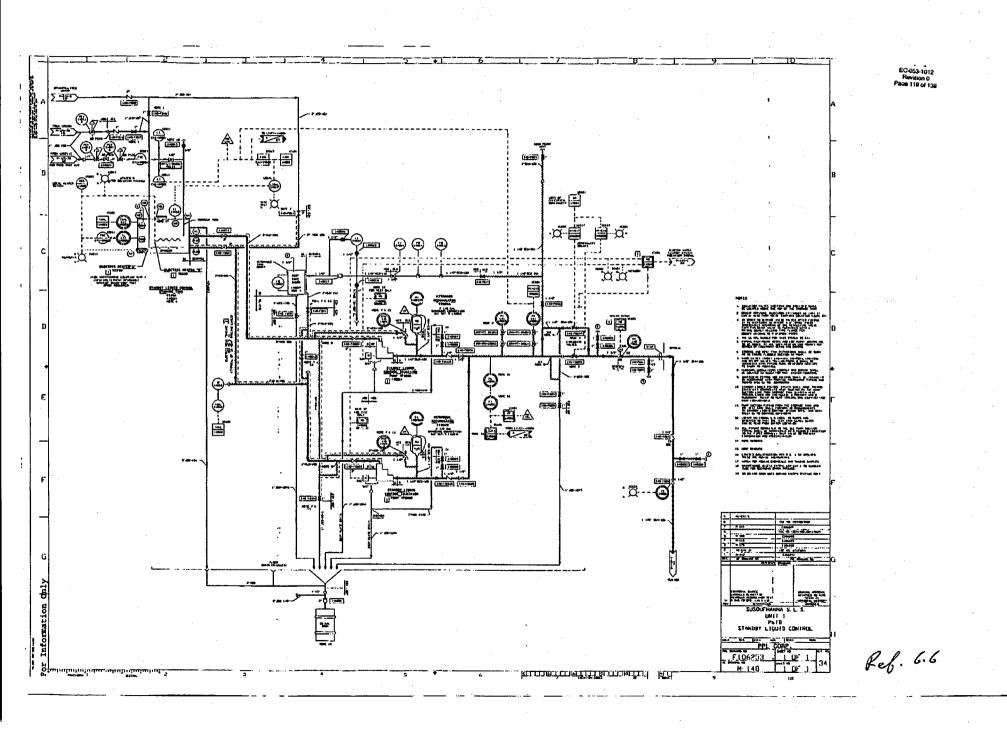
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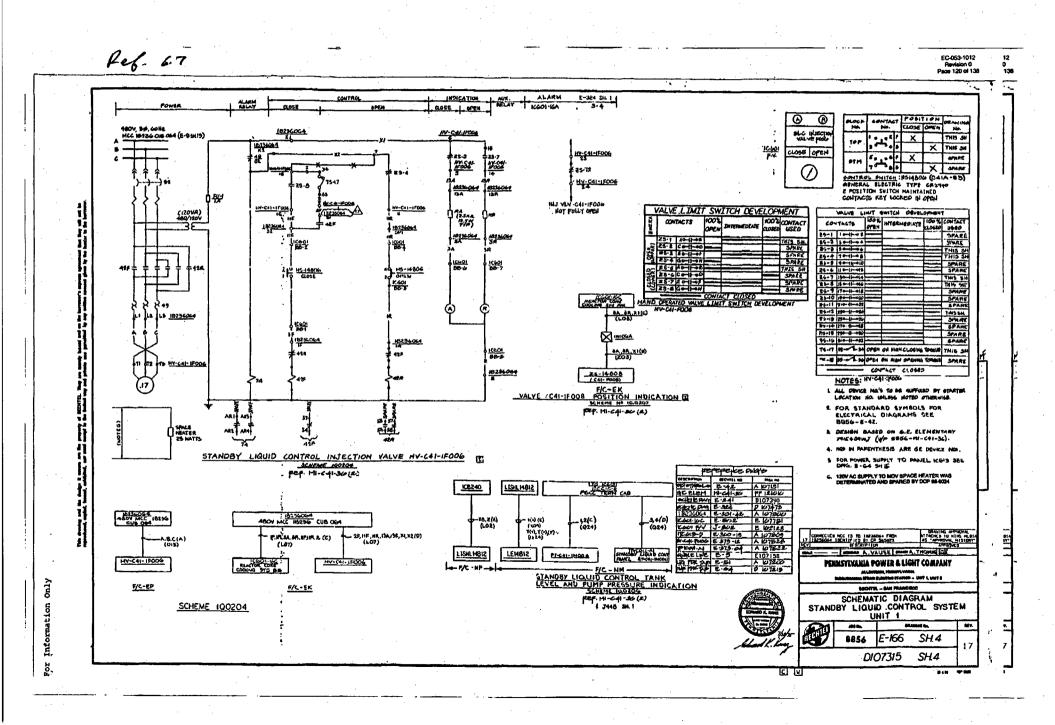
P	PEL - NIMS			Component	Data	Sheet	EC-053-1012 Revision 0 Page 117 of 138	CPX -	RCPECDAL
1				Destge	Dogu	99 6 9			
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		Comment Text		Addisio	<u>1991</u> (1997)	mento			
	Type			·····					
	OPS LOCATIO	POCI: TCEOI		•					
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-	Page 2 of 1		· · · · · · · · · · · · · · · · · · ·	· · ·		<u> </u>			
	Page 2 of 2	£	·			•	Report Date	:: 14-MAR	-2005
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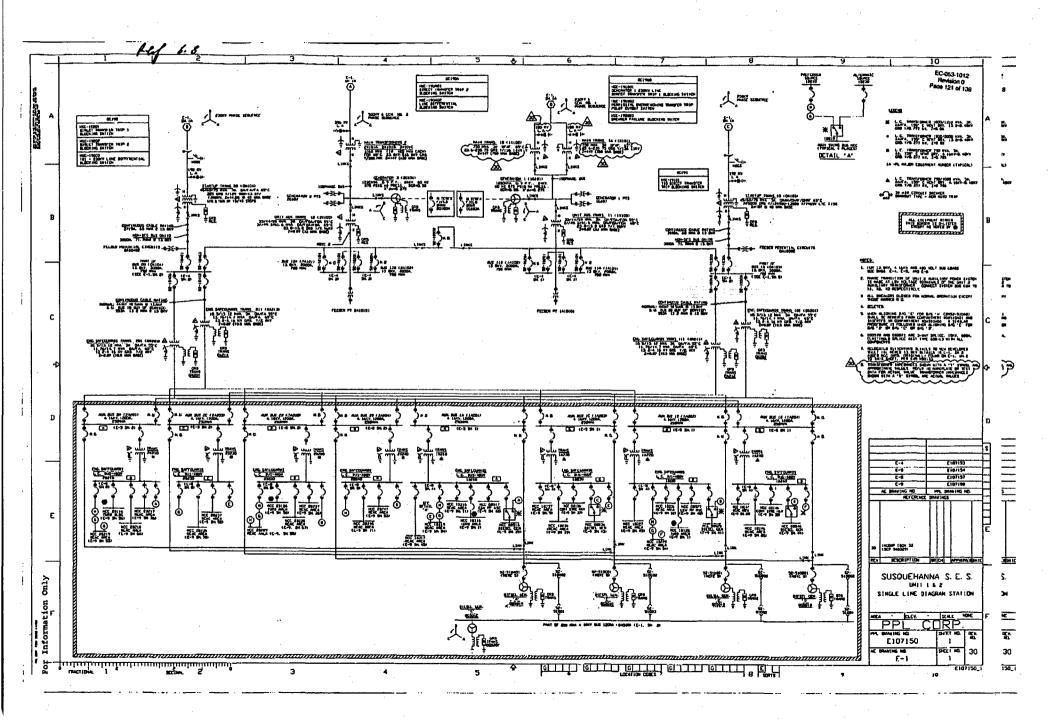
			· · · ·	EC-053-1012 Revision 0 Page 118 of 138	•.
	PP&L CALCULAT	ION SHEET		•	
Dept	PROJECT Assessment of SBLC	Calc. No. Rev. No.	EC-053-1012 0		-
Designed By G.Kowal Checked By	System for Suppression Pool pH Control	Sh. No.	1 of	1 8 —	

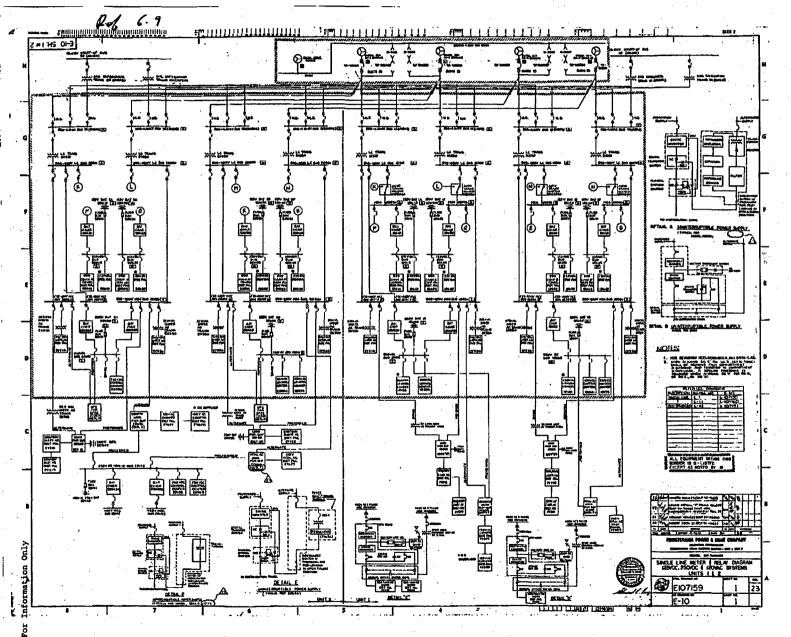
ATTACHMENT NO. 4

Input Data - Drawings

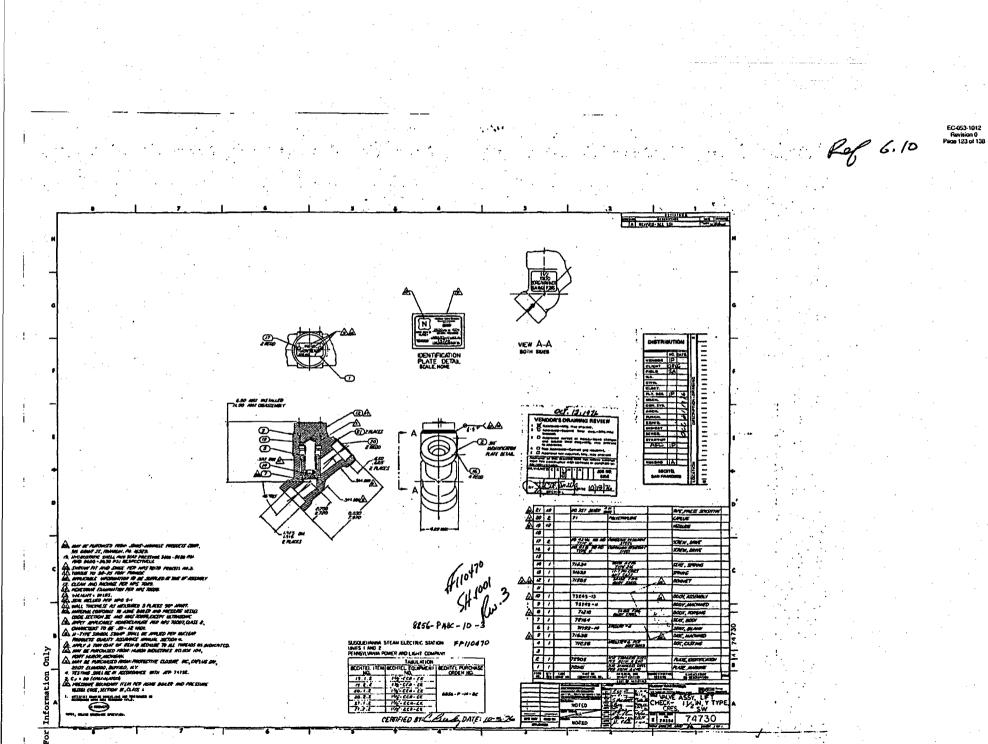








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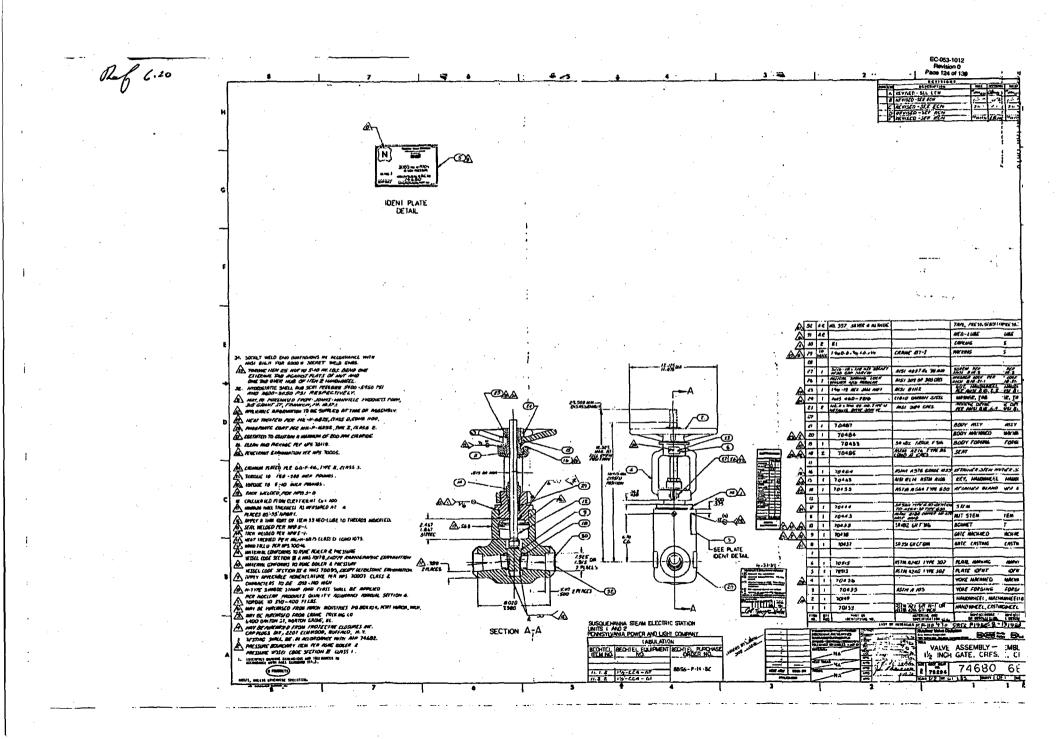


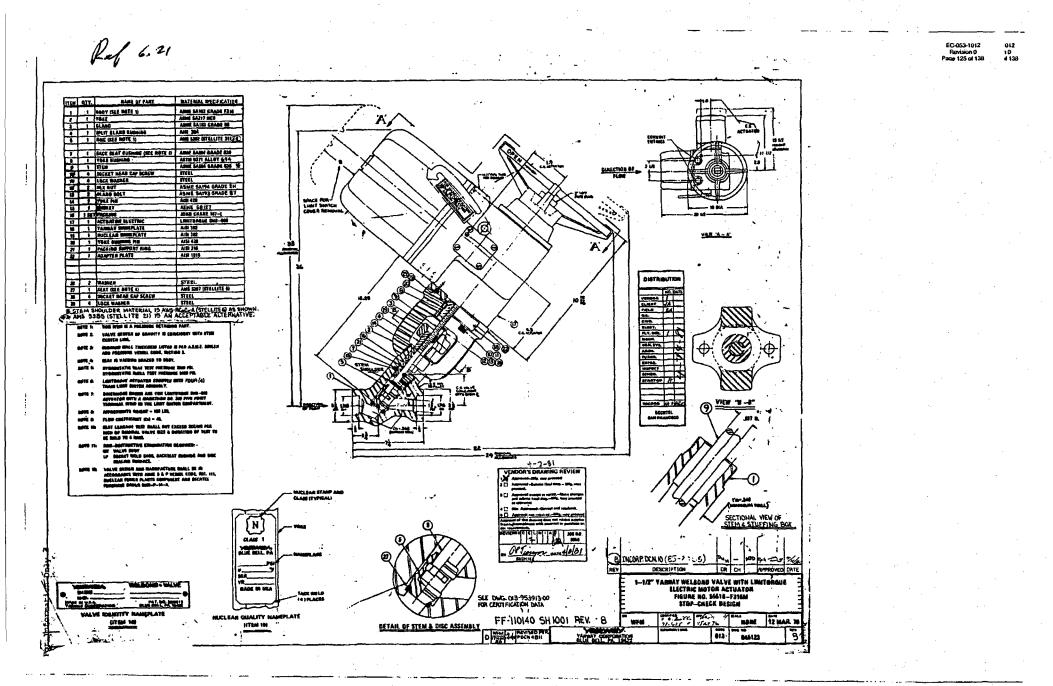
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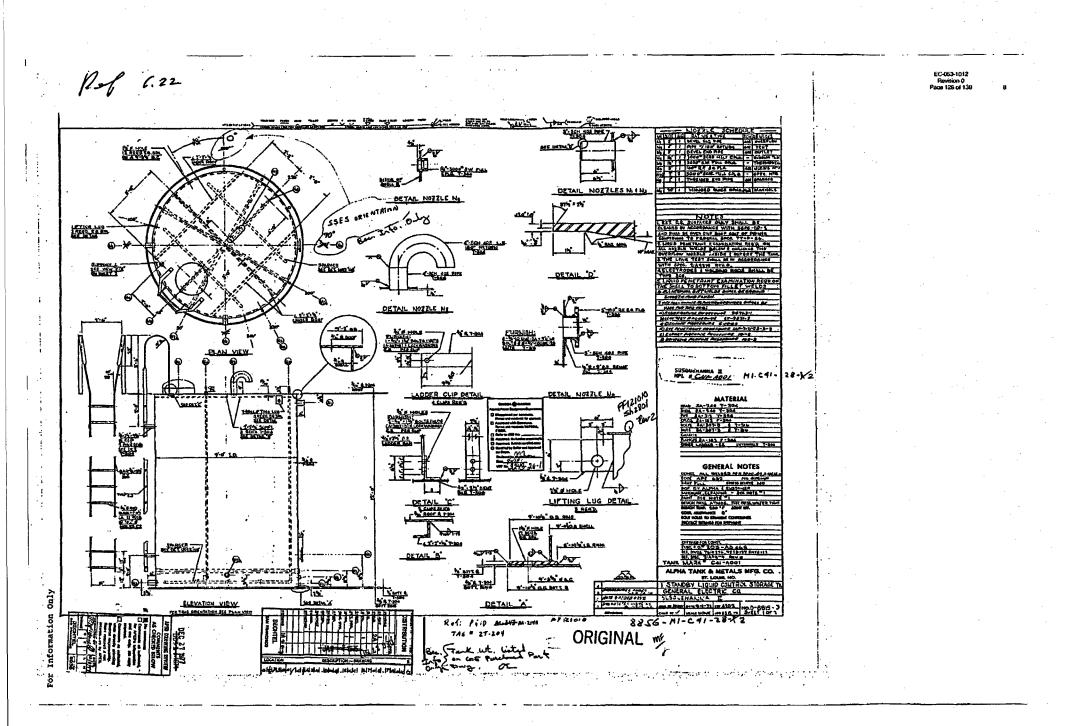
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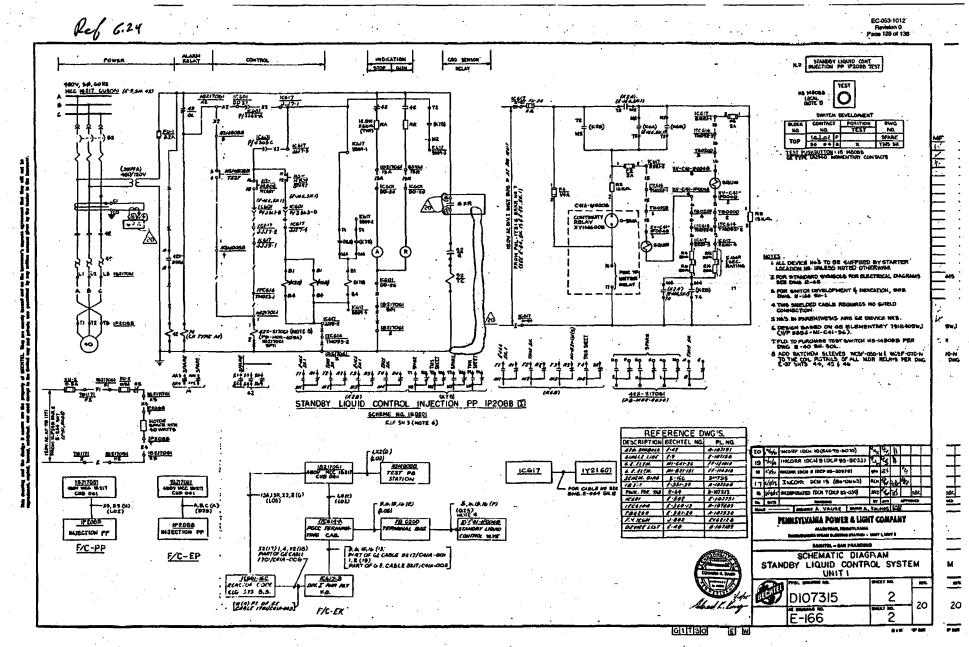
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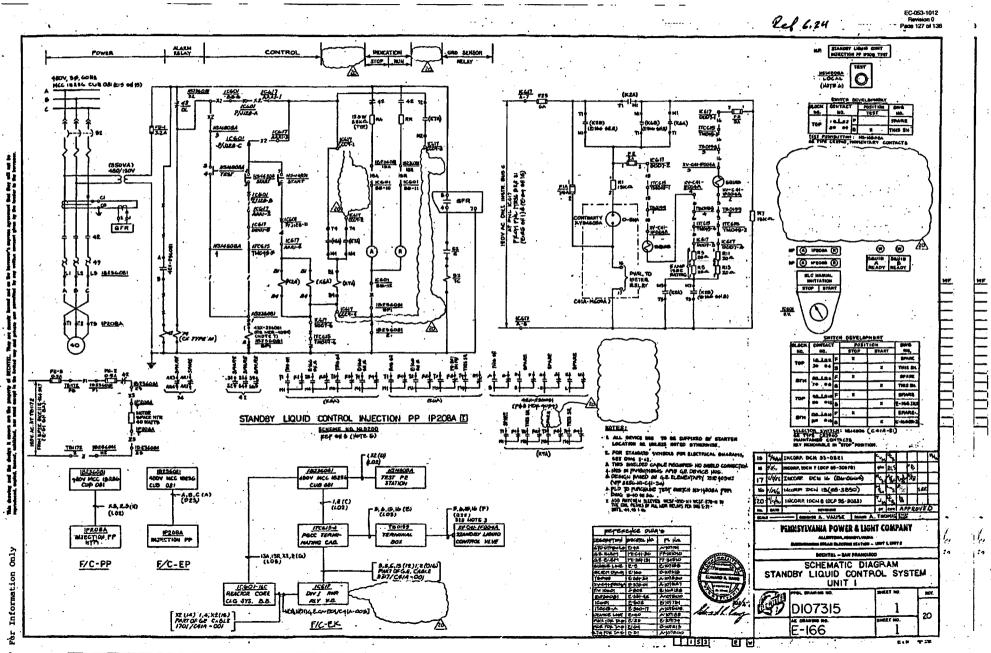


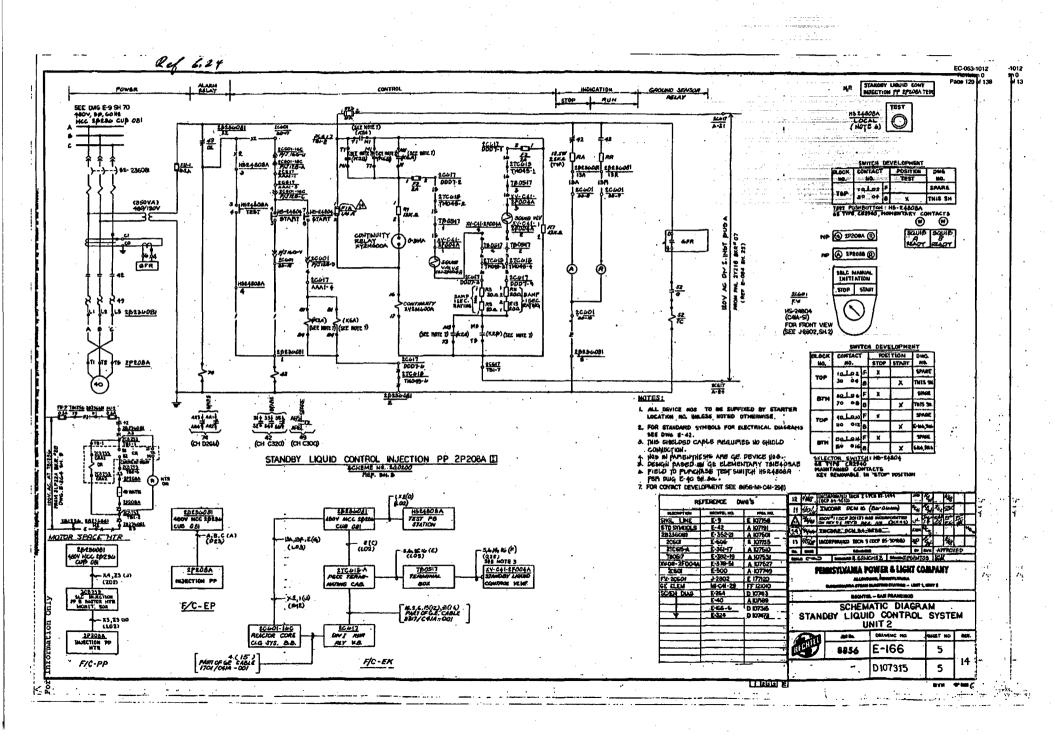


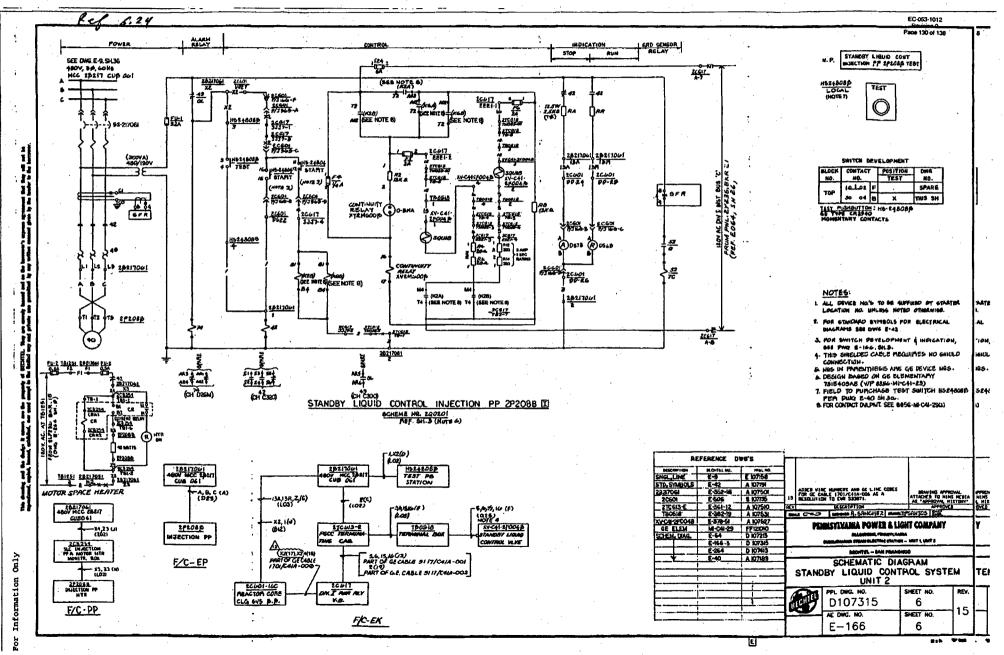
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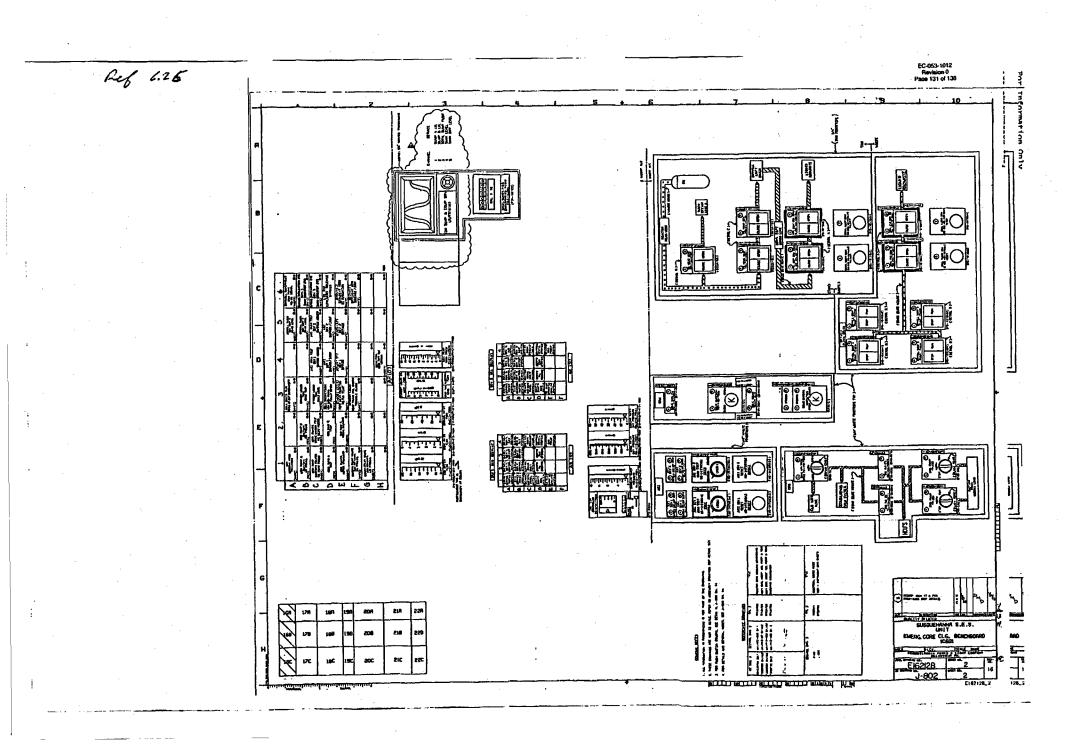


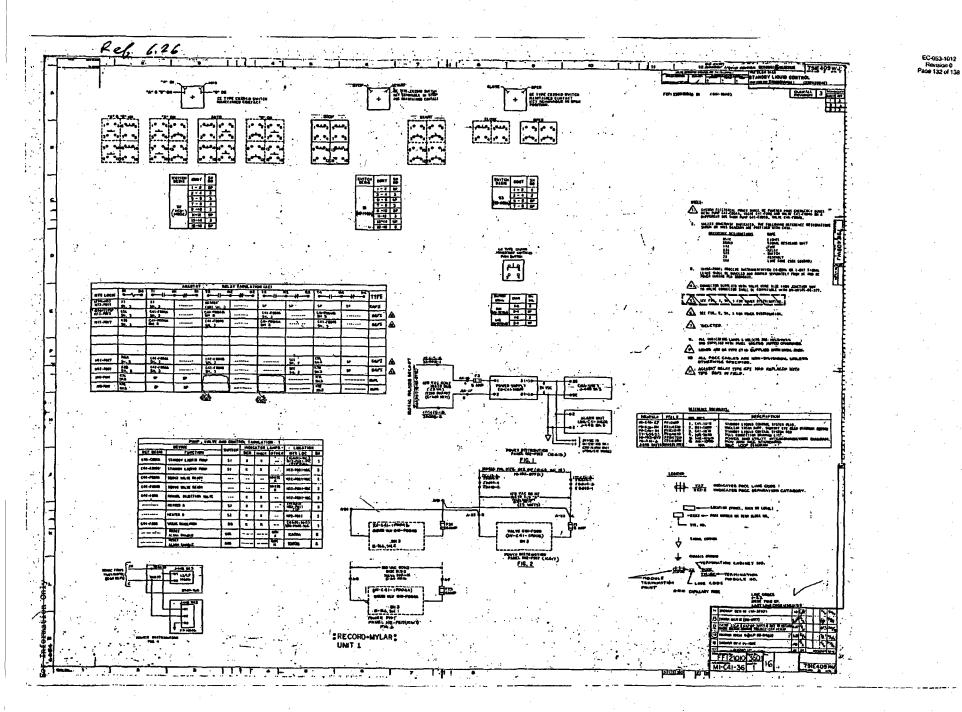


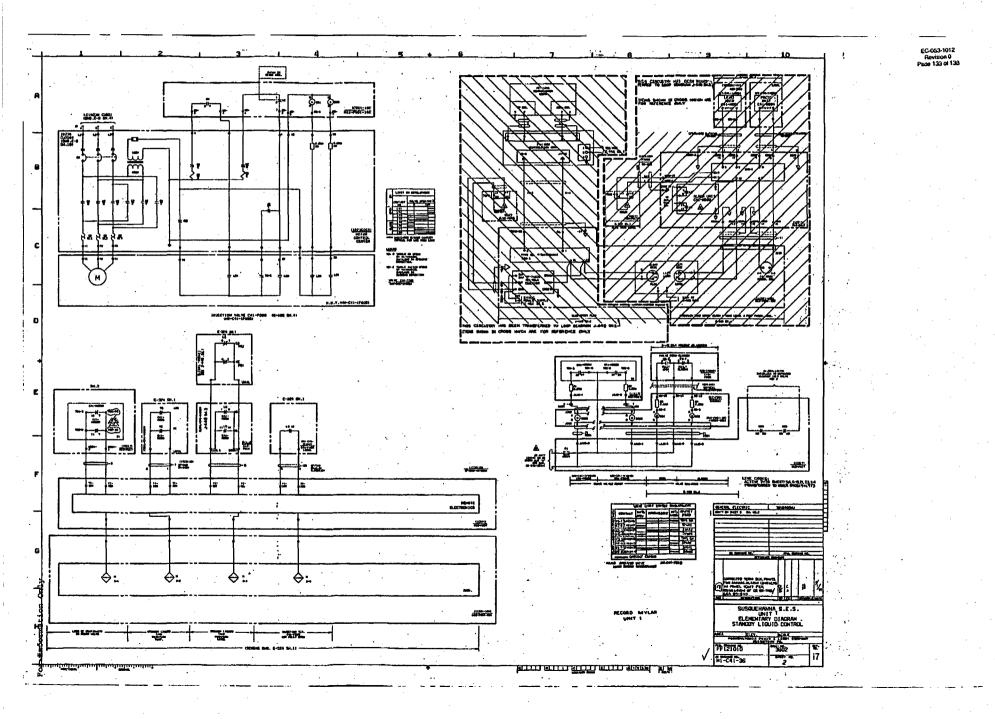


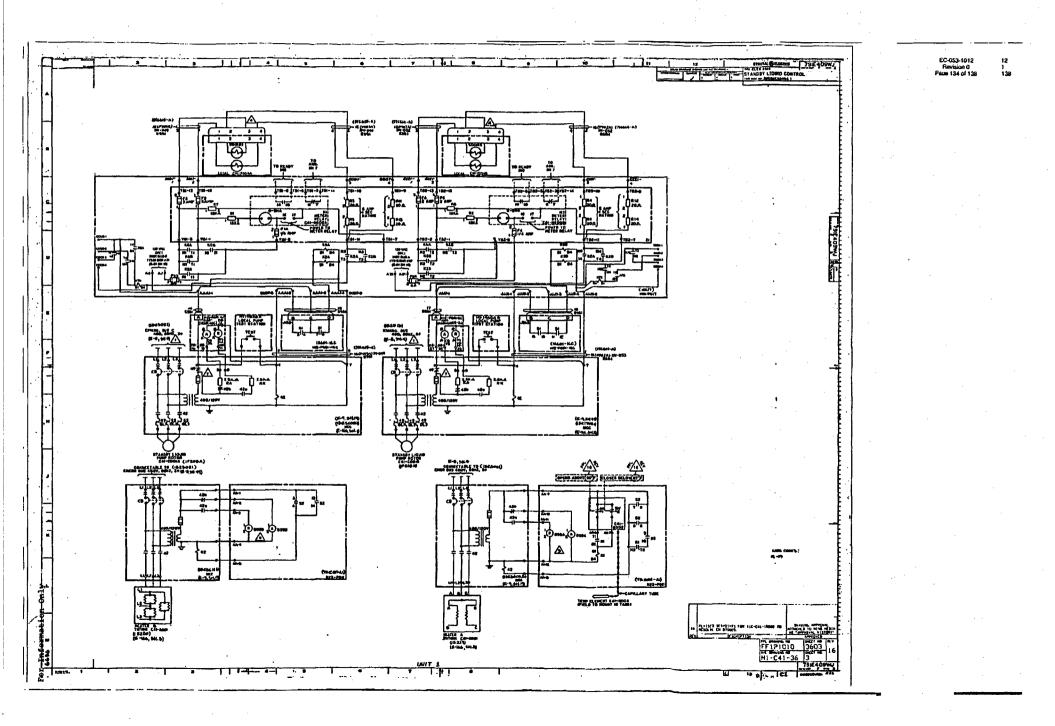
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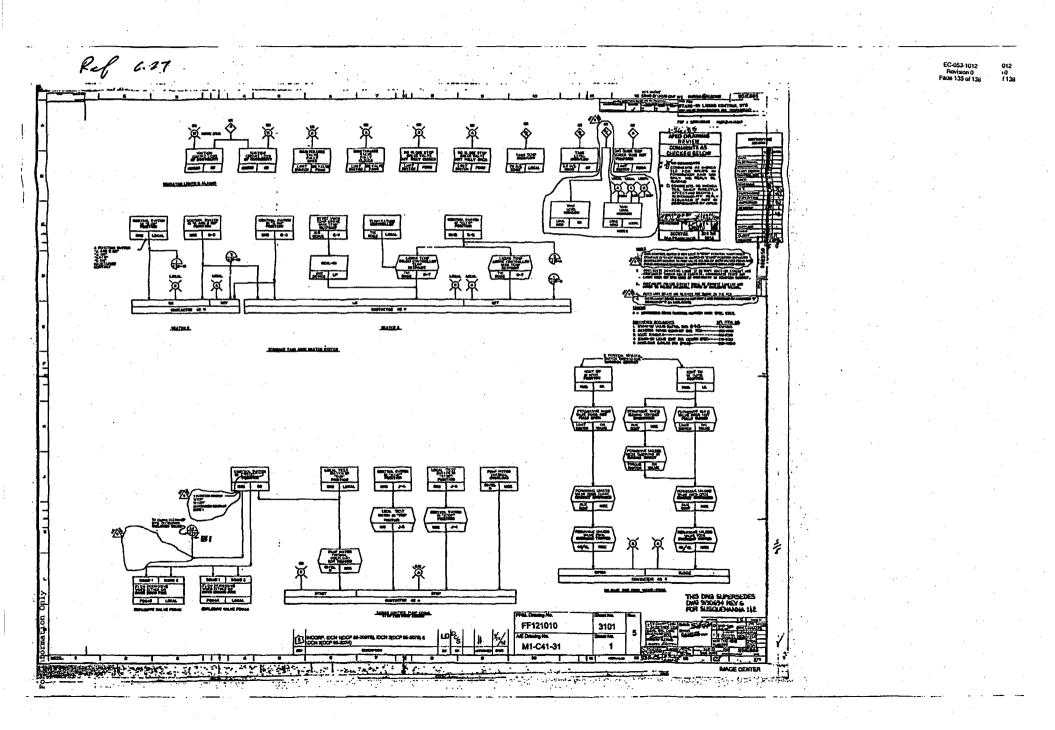
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PP&L CALCULATION SHEET								
Dept	PROJECT Assessment of SBLC	Calc. No. Rev. No.	EC-053-10120	· · · · · · · · · · · · · · · · · · ·				
Designed By G.Kowal Checked By	System for Suppression	Sh. No.	1 of	3				

ATTACHMENT NO. 5

EXCEL Spreadsheet Results

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					PP	&L CALCUL	ATION SH	IEET		
ent-				PR	OJECT		Ca	ic. No.	EC-053-10	12
				Assessment of SBLC			Re	v. No.	0	
Designed By G.Kowal			val			Suppressior	1			
heck					ol pH Co			No.	2 — of	3
							•			
					· · · · · · · · · · · · · · · · · · ·					
								.*		
RES	SULTS	S OF COC			WATER TI LE film co	EMPERATUR	E AT 80F AN	ID AMBIEN	IT AT 60F	
		·		0		(Ts -		EXP(-		
t		∏ ∞	То		To - T∞	T∞)^.25	.00169*E4	tF4)	Tt	
•						,				
	0	60		80	20	2.114743	0.003574	1	80	· ·
	0.5	60		80	20	2.114743	0.003574	0.998215	79.96429	
	1	60		80	20	2.113798	0.003572	0.996434	79.92868	
	1.5	60		80	20	2.112855	0.003571	0.994658	79.89316	•
	2	60		80	20	2.111913	0.003569	0.992887	79.85774	
	2.5	60		80	20	2.110972	0.003568	0.991121	79.82242	
	3	60		80	20	2.110033	0.003566	0.989359	79.78718	
	3.5	60		80	20	2.109094	0.003564	0.987602	79.75204	
,	4	60		80	20	2.108157	0.003563	0.98585	79.717	
	4.5	60		80	20	2.107222	0.003561	0.984102	79.68205	•
	5	60		80	20	2.106287	0.00356	0.982359	79.64719	
1.1	5.5	60		80	20	2.105354	0.003558	0.980621	79.61242	
	6	60		80	20	2.104422	0.003556	0.978887	79.57774	•
	6.5	60		80	20	2.103491	0.003555	0.977158	79.54316	
	7	60	Ŧ	80	20	2.102561	0.003553	0.975433		
	7.5	60		80	20	2.101633	0.003552	0.973713	79.47427	
	8	60		80	20	2.100706	0.00355	0.971998		
	8.5	60		80	20	2.09978	0.003549	0.970287		
	9	60		80	20	2.098856	0.003547	0.968581	79.37161	
х 	9.5	60		80	20	2.097932	0.003546	0.966879		
	10	60		80	20	2.09701	0.003544	0.965181	79.30362	
	11	60		80	20	2.096089	0.003542	0.961783		
	12	60		80	20	2.094242	0.003539	0.958418	79.16836	
	13	60		80	20	2.092407	0.003536	0.95507		
	14	60		80	20	2.090578	0.003533	0.95174		
	15	60		80	20	2.088753	0.00353	0.948428		
	16	60		80	20	2.086933	0.003527	0.945132		
	17	60		80	20	2.085118	0.003524	0.941854		
	18	60		80	. 20	2.083307	0.003521	0.938592		
	19	60		80	20	2.081502	0.003518	0.935348		,
	20	60		80	20	2.0797	0.003515	0.93212		
	21	60	•	80	20	2.077904	0.003512	0.928909	78.57817	
	22	60		80	20	2.076112	0.003509	0.925714	78.51428	
	23	60		80	20	2.074325	0.003506	0.922536	78.45072	
	24	60		80	20	2.072542	0.003503	0.919374		

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				PP&	L CALCUL	ATION SH	IEET		
Dept-			- PR	OJECT			Ic. No.	EC-053-10	12
r B				essment	of SBLC		v. No.	0	
Desin	ined F	By G. Kowa			uppression			•	
Chec			· · · · · ·	ol pH Cont	••		. No.	3 of	9
Checi	reu p	y		n pri com		GI	. NU.	UI	
				·· <u></u> ····					
					•				
RE	SULT	S OF COOLI	NG FOR V	NATER TEI	MPERATUR	E AT 80F AN	ND AMBIEN	NT AT 60F	
			(CONST	ANT film co	efficient)				
			_		<u> </u>		EXP(-		
1		T∞	To	To-Te	(Ts - T∞)	.04294*E4	tF4)	Tt	
·						-			
	0	60	80		20	0	1		
	0.5	60	80		20	0.02147	0.978759		and the second second
	1	60	80			0.04294	0.957969		
	1.5	60	80		19.15938	0.06441	0.93762		
	2	60	80		18.75241	0.08588	0.917704		· .
	2.5	60	80		18.35409	0.10735	0.898211		
	3	60	80		17.96422	0.12882	0.879132		•
	3.5	60	80		17.58264	0.15029			
•	4	60	80		17.20917	0.17176	0.842181		· ·
	4.5	60	80	20	16.84363	0.19323	0.824292	76.48585	
	5	60	80	20	16.48585	0.2147	0.806783	76.13567	· · · · · ·
	5.5	60	80	20	16.13567	0.23617	0.789646	75.79293	
	6	60	80	20	15. 79 293	0.25764	0.772873	75.45747	
	6.5	60	80	20	15.45747	0.27911	0.756457	75.12913	1
	7	60	08	20	15.12913	0.30058	0.740389	74.80777	
	7.5	60	80	20	14.80777	0.32205	0.724662	74.49324	
	8	60	80	20	14.49324	0.34352	0.709269	74.18539	
	8.5	60	80	20	14.18539	0.36499	0.694204	73.88407	
	9	60	60	20	13.88407	0.38646	0.679458	73.58916	
	9.5	60	80	20	13.58916	0.40793	0.665025	73.30051	
	10	60	80	20	13.30051	0.4294	0.6509		
	11	60	80	20	13.01799	0.47234	0.623541	72.47083	•
	12	60	-80	20	12.47083	0.51528	0.597333		
	13	60	80	20	11.94667	0.55822	0.572227		
÷	- 14	60	80	20	11.44453	0.60116	0.548175	70.96351	
	15	60	80	20	10.96351	0.6441	0.525135	70.5027	
	16	60	80	20	10.5027	0.68704	0.503063	70.06126	
	17	60	80	20	10.06126	0.72998	0.481919		
	18	60	80	20	9.638373	0.77292	0.461663		
	19	60	80	20	9.233261	0.81586	0.442259		
	20	60	80	20	8.845176	0.8588	0.42367		
	21	60	80	20	8.473404	0.90174	0.405863		
	22	60	80	20	8.117257	0.94468	0.388804		·
	23	60	80	20	7.776079	0.98762	0.372462		
	24	60	80	20	7.449242	1.03056	0.356807	67.13614	·.
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