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May 4, 2005  
BW050041

U.S. Nuclear Regulatory Commission  
ATTN: Document Control Desk  
Washington, DC 20555-0001

Braidwood Station, Unit 2  
Facility Operating License No. NPF-77  
NRC Docket No. STN 50-457

Subject:      Core Operating Limits Report, Braidwood Unit 2 Cycle 12

The purpose of this letter is to transmit the Core Operating Limits Report (COLR) for Braidwood Unit 2 Cycle 12, in accordance with Technical Specification 5.6.5, "Core Operating Limits Report (COLR)." This revision of the COLR was recently implemented in support of a reload cycle.

If you have any questions regarding this matter, please contact Mr. Dale Ambler, Regulatory Assurance Manager, at (815) 417-2800.

Sincerely,



Keith J. Polson  
Site Vice President  
Braidwood Station

Attachment:    Core Operating Limits Report, Braidwood Unit 2 Cycle 12

cc:      Regional Administrator – NRC Region III  
          NRC Senior Resident Inspector – Braidwood Station

A001

**ATTACHMENT 1**

**Core Operating Limits Report**

**Braidwood Unit 2, Cycle 12**

## CORE OPERATING LIMITS REPORT (COLR) for BRAIDWOOD UNIT 2 CYCLE 12

1.0 CORE OPERATING LIMITS REPORT

This Core Operating Limits Report (COLR) for Braidwood Station Unit 2 Cycle 12 has been prepared in accordance with the requirements of Technical Specification 5.6.5 (ITS).

The Technical Specifications affected by this report are listed below:

- SL 2.1.1 Reactor Core Safety Limits (SLs)
- LCO 3.1.1 SHUTDOWN MARGIN (SDM)
- LCO 3.1.3 Moderator Temperature Coefficient (MTC)
- LCO 3.1.4 Rod Group Alignment Limits
- LCO 3.1.5 Shutdown Bank Insertion Limits
- LCO 3.1.6 Control Bank Insertion Limits
- LCO 3.1.8 PHYSICS TESTS Exceptions – MODE 2
- LCO 3.2.1 Heat Flux Hot Channel Factor ( $F_Q(Z)$ )
- LCO 3.2.2 Nuclear Enthalpy Rise Hot Channel Factor ( $F_{\Delta H}^N$ )
- LCO 3.2.3 AXIAL FLUX DIFFERENCE (AFD)
- LCO 3.2.5 Departure from Nucleate Boiling Ratio (DNBR)
- LCO 3.3.1 Reactor Trip System (RTS) Instrumentation
- LCO 3.3.9 Boron Dilution Protection System (BDPS)
- LCO 3.4.1 Reactor Coolant System (RCS) Pressure, Temperature, and Flow Departure from Nucleate Boiling (DNB) Limits
- LCO 3.9.1 Boron Concentration

The portions of the Technical Requirements Manual affected by this report are listed below:

- TRM TLCO 3.1.b Boration Flow Paths – Operating
- TRM TLCO 3.1.d Charging Pumps – Operating
- TRM TLCO 3.1.f Borated Water Sources – Operating
- TRM TLCO 3.1.g Position Indication System – Shutdown
- TRM TLCO 3.1.h Shutdown Margin (SDM) – MODE 1 and MODE 2 with  $k_{eff} \geq 1.0$
- TRM TLCO 3.1.i Shutdown Margin (SDM) – MODE 5
- TRM TLCO 3.1.j Shutdown and Control Rods
- TRM TLCO 3.1.k Position Indication System – Shutdown (Special Test Exception)

## CORE OPERATING LIMITS REPORT (COLR) for BRAIDWOOD UNIT 2 CYCLE 12

## 2.0 OPERATING LIMITS

The cycle-specific parameter limits for the specifications listed in Section 1.0 are presented in the following subsections. These limits are applicable for the entire cycle unless otherwise identified. These limits have been developed using the NRC-approved methodologies specified in Technical Specification 5.6.5.

## 2.1 Reactor Core Safety Limits (SLs) (SL 2.1.1)

2.1.1 In MODES 1 and 2, the combination of Thermal Power, Reactor Coolant System (RCS) highest loop average temperature, and pressurizer pressure shall not exceed the limits specified in Figure 2.1.1.

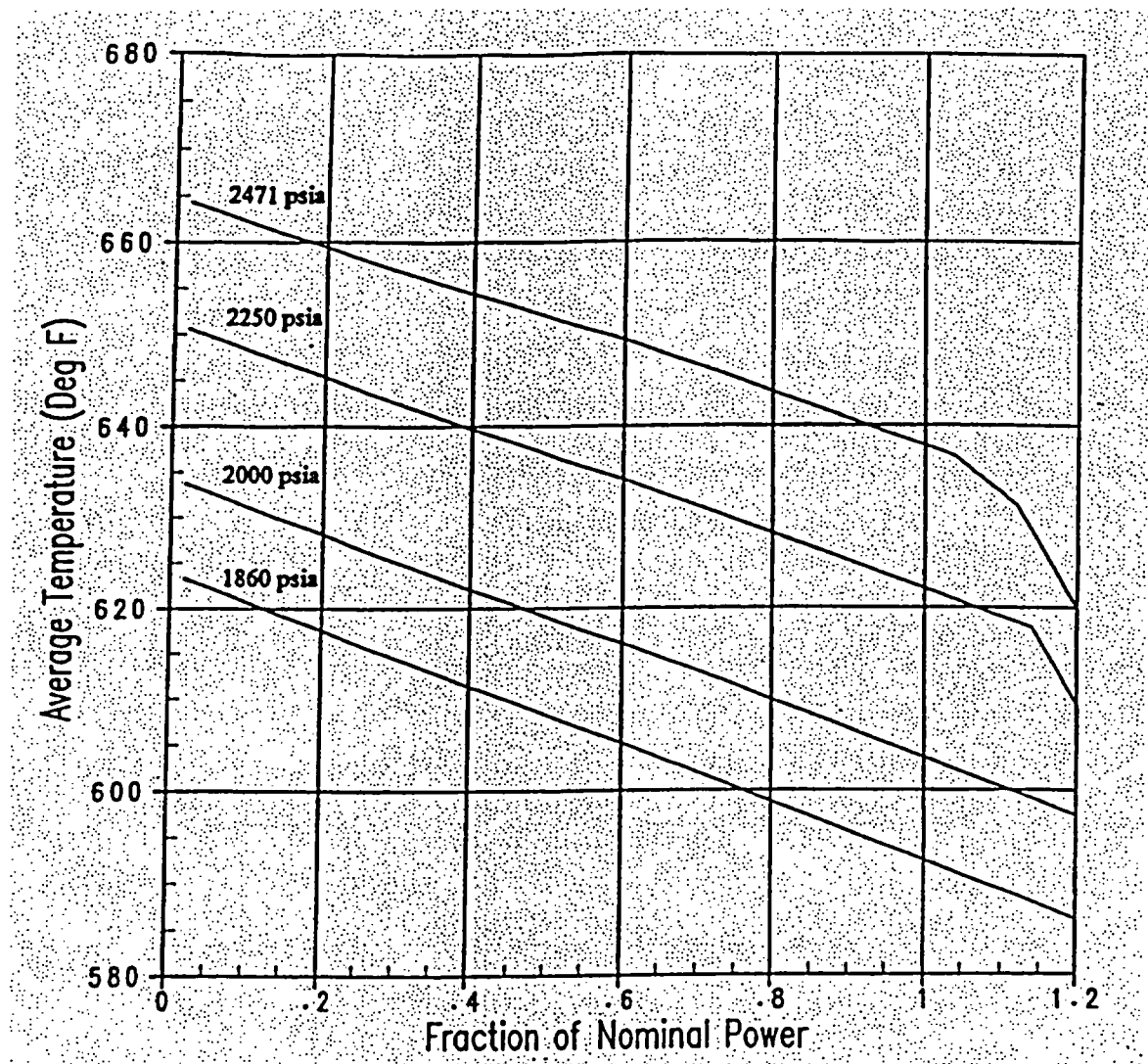


Figure 2.1.1: Reactor Core Limits

## CORE OPERATING LIMITS REPORT (COLR) for BRAIDWOOD UNIT 2 CYCLE 12

**2.2 SHUTDOWN MARGIN (SDM)**

The SDM limit for MODES 1, 2, 3, and 4 is:

2.2.1 The SDM shall be greater than or equal to 1.3%  $\Delta k/k$  (LCOs 3.1.1, 3.1.4, 3.1.5, 3.1.6, 3.1.8, 3.3.9; TRM TLCOs 3.1.b, 3.1.d, 3.1.f, 3.1.h, and 3.1.j).

The SDM limit for MODE 5 is:

2.2.2 SDM shall be greater than or equal to 1.3%  $\Delta k/k$  (LCO 3.1.1, LCO 3.3.9; TRM TLCOs 3.1.i and 3.1.j).

**2.3 Moderator Temperature Coefficient (MTC) (LCO 3.1.3)**

The Moderator Temperature Coefficient (MTC) limits are:

2.3.1 The BOL/ARO/HZP-MTC upper limit shall be  $+1.28 \times 10^{-5} \Delta k/k^{\circ}F$ .

2.3.2 The EOL/ARO/HFP-MTC lower limit shall be  $-4.6 \times 10^{-4} \Delta k/k^{\circ}F$ .

2.3.3 The EOL/ARO/HFP-MTC Surveillance limit at 300 ppm shall be  $-3.7 \times 10^{-4} \Delta k/k^{\circ}F$ .

2.3.4 The EOL/ARO/HFP-MTC Surveillance limit at 60 ppm shall be  $-4.3 \times 10^{-4} \Delta k/k^{\circ}F$ .

where: BOL stands for Beginning of Cycle Life  
 ARO stands for All Rods Out  
 HZP stands for Hot Zero Thermal Power  
 EOL stands for End of Cycle Life  
 HFP stands for Hot Full Thermal Power

**2.4 Shutdown Bank Insertion Limits (LCO 3.1.5)**

2.4.1 All shutdown banks shall be fully withdrawn to at least 224 steps.

**2.5 Control Bank Insertion Limits (LCO 3.1.6)**

2.5.1 The control banks, with Bank A greater than or equal to 224 steps, shall be limited in physical insertion as shown in Figure 2.5.1.

2.5.2 Each control bank shall be considered fully withdrawn from the core at greater than or equal to 224 steps.

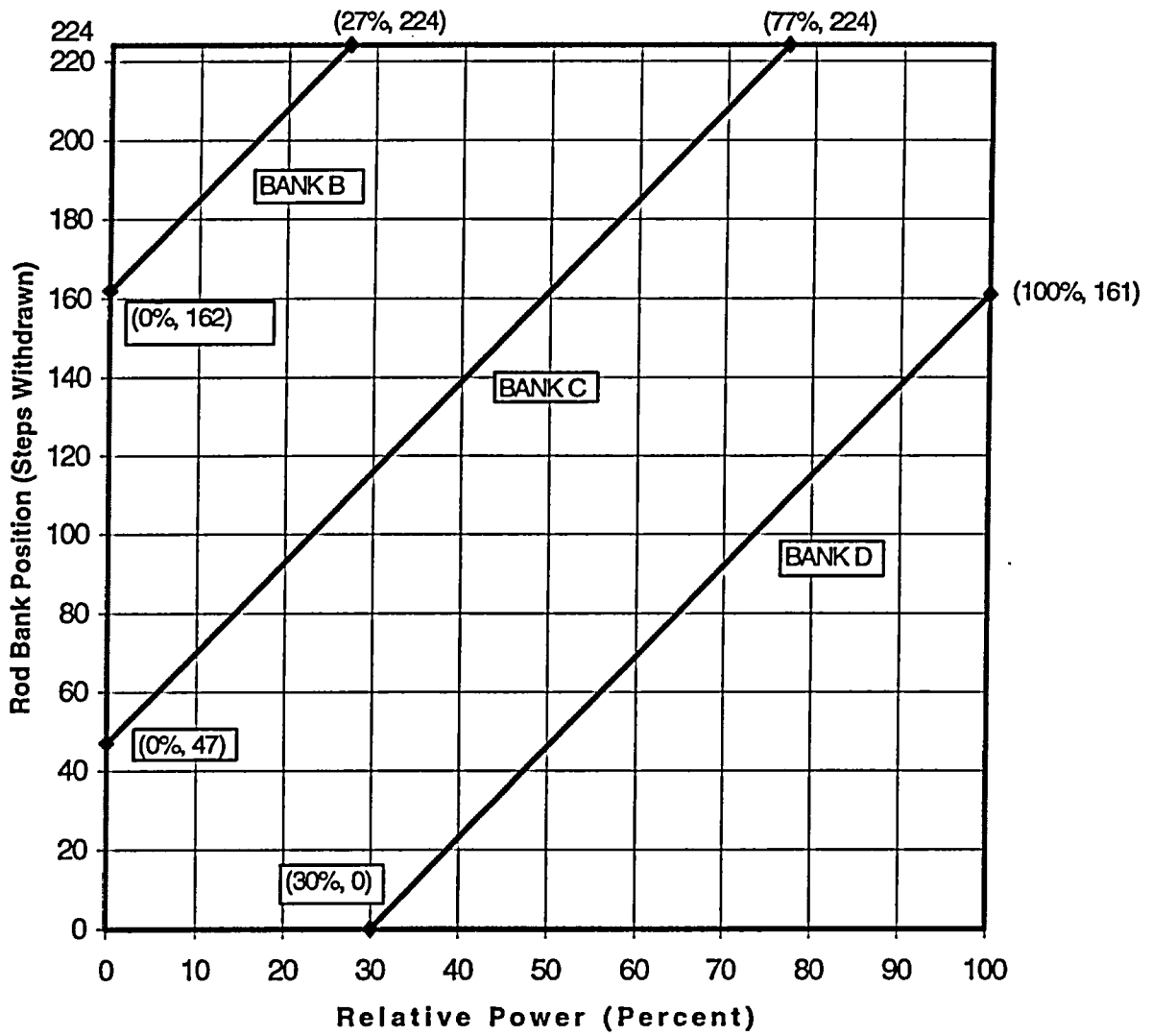
2.5.3 The control banks shall be operated in sequence by withdrawal of Bank A, Bank B, Bank C and Bank D. The control banks shall be sequenced in reverse order upon insertion.

2.5.4 Each control bank not fully withdrawn from the core shall be operated with the following overlap limits as a function of park position:

Park Position (step)	Overlap Limit (step)
225	110
226	111
227	112
228	113
229	114

CORE OPERATING LIMITS REPORT (COLR) for BRAIDWOOD UNIT 2 CYCLE 12

Figure 2.5.1:  
Control Bank Insertion Limits Versus Percent Rated Thermal Power



## CORE OPERATING LIMITS REPORT (COLR) for BRAIDWOOD UNIT 2 CYCLE 12

2.6 Heat Flux Hot Channel Factor ( $F_Q(Z)$ ) (LCO 3.2.1)

## 2.6.1 Total Peaking Factor:

$$F_Q(Z) \leq \frac{F_Q^{RTP}}{0.5} \times K(Z) \text{ for } P \leq 0.5$$

$$F_Q(Z) \leq \frac{F_Q^{RTP}}{P} \times K(Z) \text{ for } P > 0.5$$

where: P = the ratio of THERMAL POWER to RATED THERMAL POWER

$$F_Q^{RTP} = 2.60$$

K(Z) is provided in Figure 2.6.1.

## 2.6.2 W(Z) Values:

a) When PDMS is OPERABLE, W(Z) = 1.00000 for all axial points.

b) When PDMS is inoperable, W(Z) is provided in Figures 2.6.2.a through 2.6.2.d.

The normal operation W(Z) values have been determined at burnups of 150, 6000, 14000, and 20000 MWD/MTU.

Table 2.6.2 shows the  $F_Q^C(z)$  penalty factors that are greater than 2% per 31 Effective Full Power Days (EFPD). These values shall be used to increase the  $F_Q^W(z)$  as per Surveillance Requirement 3.2.1.2. A 2% penalty factor shall be used at all cycle burnups that are outside the range of Table 2.6.2.

## 2.6.3 Uncertainty:

The uncertainty,  $U_{FQ}$ , to be applied to the Heat Flux Hot Channel Factor  $F_Q(Z)$  shall be calculated by the following formula

$$U_{FQ} = U_{qu} \cdot U_e$$

where:

$U_{qu}$  = Base  $F_Q$  measurement uncertainty = 1.05 when PDMS is inoperable  
( $U_{qu}$  is defined by PDMS when OPERABLE.)

$U_e$  = Engineering uncertainty factor = 1.03

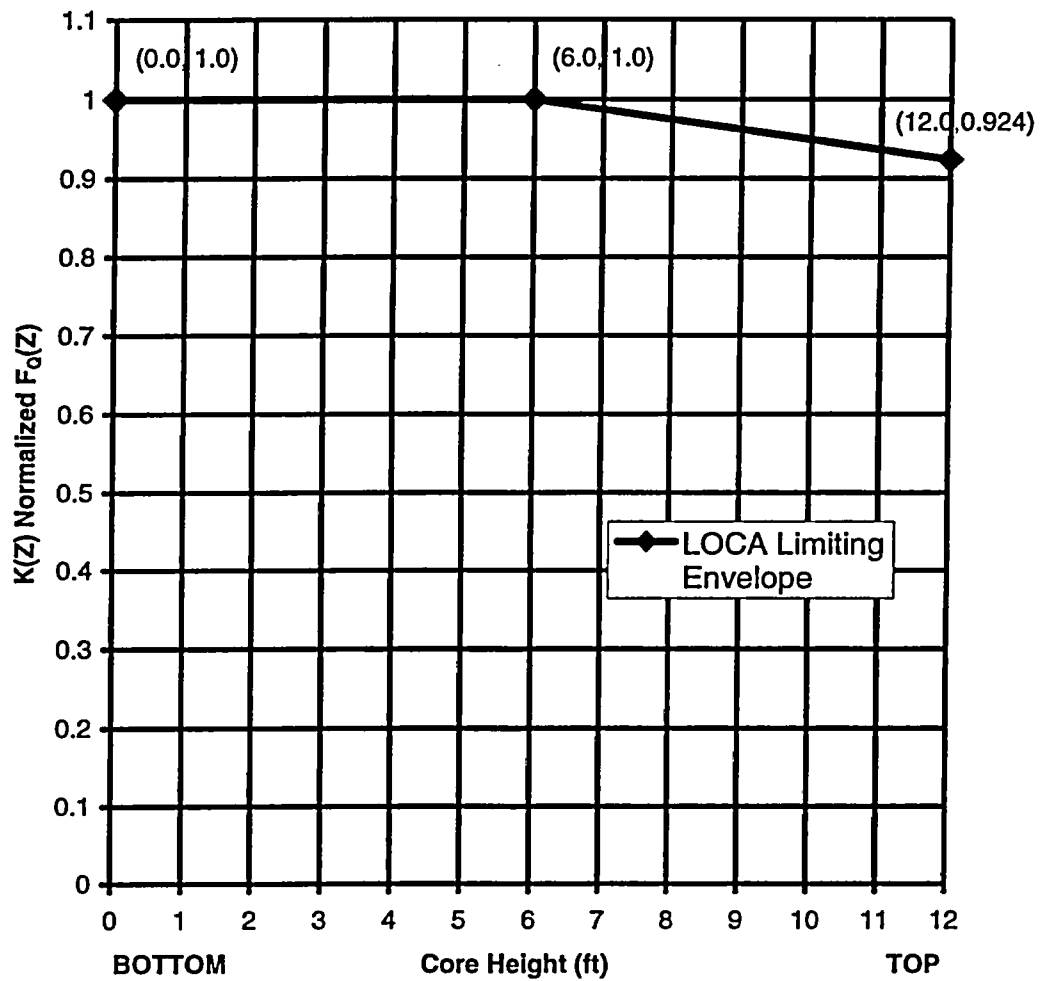
## 2.6.4 PDMS Alarms:

$F_Q(Z)$  Warning Setpoint  $\geq 2\%$  of  $F_Q(Z)$  Margin

$F_Q(Z)$  Alarm Setpoint  $\geq 0\%$  of  $F_Q(Z)$  Margin

CORE OPERATING LIMITS REPORT (COLR) for BRAIDWOOD UNIT 2 CYCLE 12

**Figure 2.6.1**  
**K(Z) - Normalized  $F_0(Z)$  as a Function of Core Height**





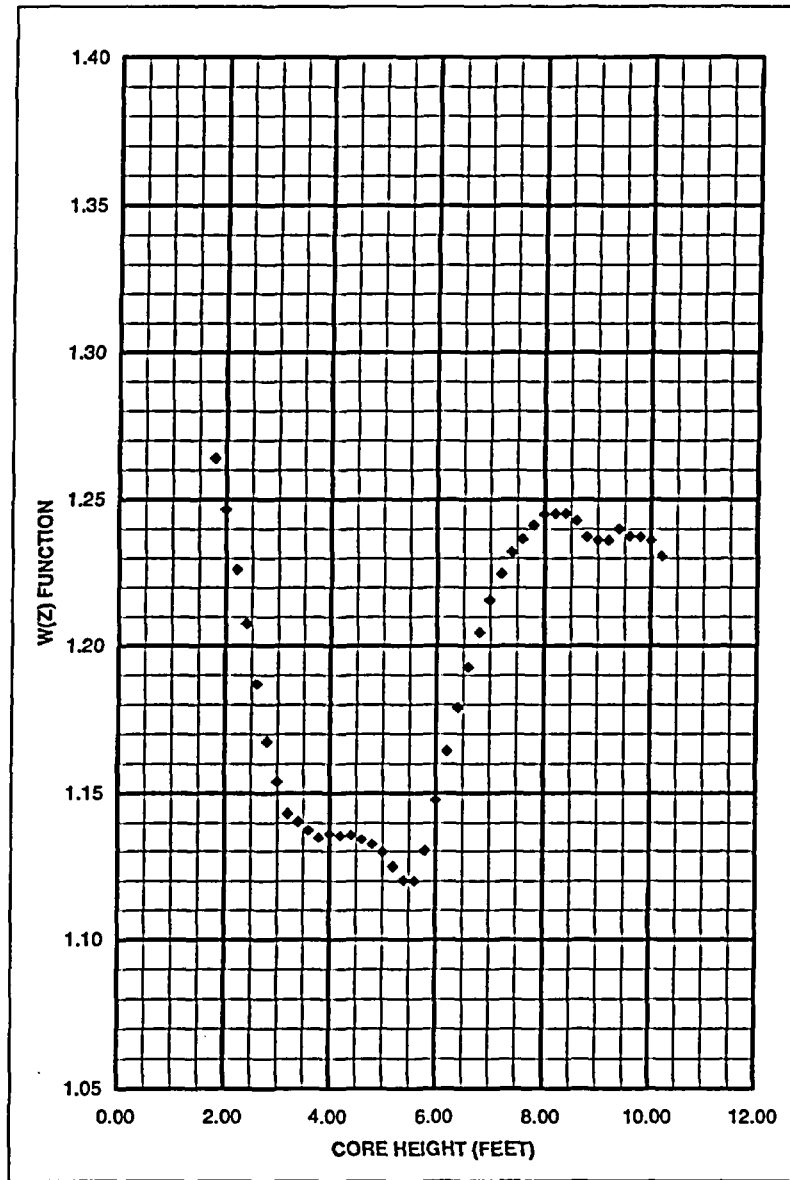
CORE OPERATING LIMITS REPORT (COLR) for BRAIDWOOD UNIT 2 CYCLE 12

Height Feet	MAX W(Z)
0.00	1.0000
0.20	1.0000
0.40	1.0000
0.60	1.0000
0.80	1.0000
1.00	1.0000
1.20	1.0000
1.40	1.0000
1.60	1.0000
1.80	1.2639
2.00	1.2467
2.20	1.2262
2.40	1.2077
2.60	1.1870
2.80	1.1675
3.00	1.1540
3.20	1.1432
3.40	1.1405
3.60	1.1376
3.80	1.1348
4.00	1.1362
4.20	1.1355
4.40	1.1357
4.60	1.1342
4.80	1.1324
5.00	1.1297
5.20	1.1248
5.40	1.1201
5.60	1.1199
5.80	1.1301
6.00	1.1477
6.20	1.1643
6.40	1.1790
6.60	1.1927
6.80	1.2046
7.00	1.2157
7.20	1.2247
7.40	1.2321
7.60	1.2366
7.80	1.2413
8.00	1.2450
8.20	1.2452
8.40	1.2453
8.60	1.2428
8.80	1.2373
9.00	1.2363
9.20	1.2362
9.40	1.2400
9.60	1.2376
9.80	1.2374
10.00	1.2361
10.20	1.2307
10.40	1.0000
10.60	1.0000
10.80	1.0000
11.00	1.0000
11.20	1.0000
11.40	1.0000
11.60	1.0000
11.80	1.0000
12.00	1.0000

Briadwood Unit 2 Cycle 12

Figure 2.6.2.a

Summary of W(Z) Function at 150 MWD/MTU  
(Top and Bottom 15% Excluded per WCAP-10216)



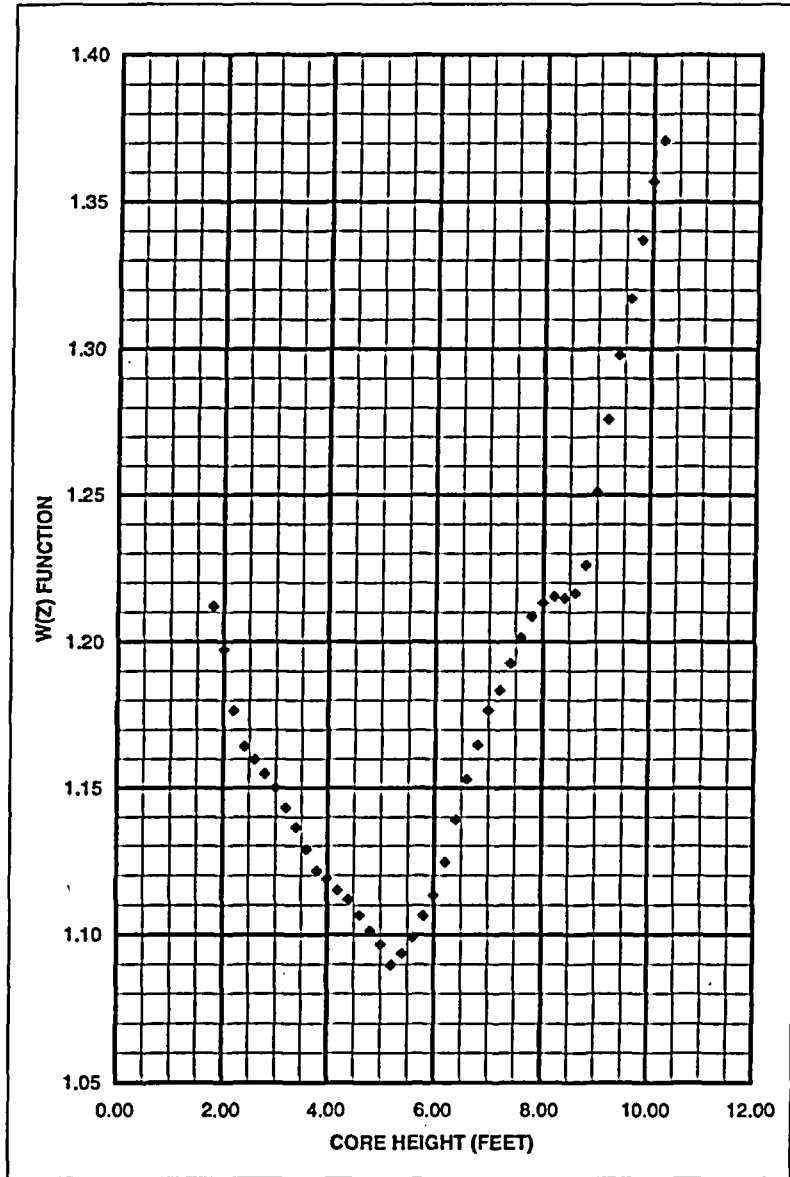
CORE OPERATING LIMITS REPORT (COLR) for BRAIDWOOD UNIT 2 CYCLE 12

Height Feet	MAX W(Z)
0.00	1.0000
0.20	1.0000
0.40	1.0000
0.60	1.0000
0.80	1.0000
1.00	1.0000
1.20	1.0000
1.40	1.0000
1.60	1.0000
1.80	1.2119
2.00	1.1973
2.20	1.1764
2.40	1.1642
2.60	1.1598
2.80	1.1549
3.00	1.1501
3.20	1.1433
3.40	1.1365
3.60	1.1287
3.80	1.1215
4.00	1.1188
4.20	1.1149
4.40	1.1117
4.60	1.1065
4.80	1.1013
5.00	1.0966
5.20	1.0898
5.40	1.0937
5.60	1.0990
5.80	1.1064
6.00	1.1132
6.20	1.1244
6.40	1.1392
6.60	1.1529
6.80	1.1647
7.00	1.1766
7.20	1.1835
7.40	1.1926
7.60	1.2014
7.80	1.2086
8.00	1.2132
8.20	1.2153
8.40	1.2147
8.60	1.2165
8.80	1.2260
9.00	1.2510
9.20	1.2760
9.40	1.2980
9.60	1.3170
9.80	1.3370
10.00	1.3570
10.20	1.3710
10.40	1.0000
10.60	1.0000
10.80	1.0000
11.00	1.0000
11.20	1.0000
11.40	1.0000
11.60	1.0000
11.80	1.0000
12.00	1.0000

Braidwood Unit 2 Cycle 12

Figure 2.6.2.b

Summary of W(Z) Function at 6000 MWD/MTU  
(Top and Bottom 15% Excluded per WCAP-10216)



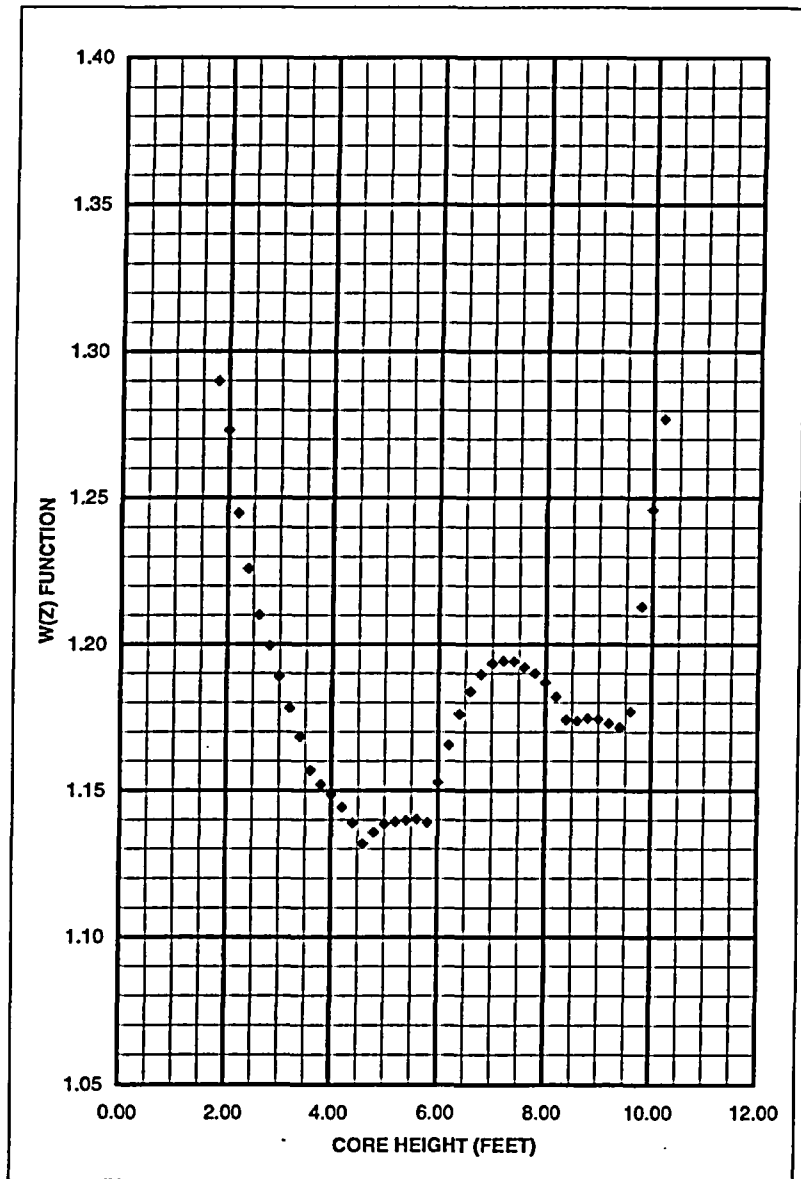
CORE OPERATING LIMITS REPORT (COLR) for BRAIDWOOD UNIT 2 CYCLE 12

Height Feet	MAX W(Z)
0.00	1.0000
0.20	1.0000
0.40	1.0000
0.60	1.0000
0.80	1.0000
1.00	1.0000
1.20	1.0000
1.40	1.0000
1.60	1.0000
1.80	1.2899
2.00	1.2730
2.20	1.2447
2.40	1.2258
2.60	1.2100
2.80	1.1995
3.00	1.1890
3.20	1.1782
3.40	1.1684
3.60	1.1568
3.80	1.1520
4.00	1.1486
4.20	1.1443
4.40	1.1390
4.60	1.1318
4.80	1.1358
5.00	1.1386
5.20	1.1394
5.40	1.1398
5.60	1.1403
5.80	1.1392
6.00	1.1528
6.20	1.1655
6.40	1.1761
6.60	1.1838
6.80	1.1896
7.00	1.1934
7.20	1.1943
7.40	1.1941
7.60	1.1921
7.80	1.1900
8.00	1.1869
8.20	1.1820
8.40	1.1741
8.60	1.1737
8.80	1.1746
9.00	1.1743
9.20	1.1728
9.40	1.1715
9.60	1.1770
9.80	1.2130
10.00	1.2460
10.20	1.2770
10.40	1.0000
10.60	1.0000
10.80	1.0000
11.00	1.0000
11.20	1.0000
11.40	1.0000
11.60	1.0000
11.80	1.0000
12.00	1.0000

Braidwood Unit 2 Cycle 12

Figure 2.6.2.c

Summary of W(Z) Function at 14000 MWD/MTU  
(Top and Bottom 15% Excluded per WCAP-10216)



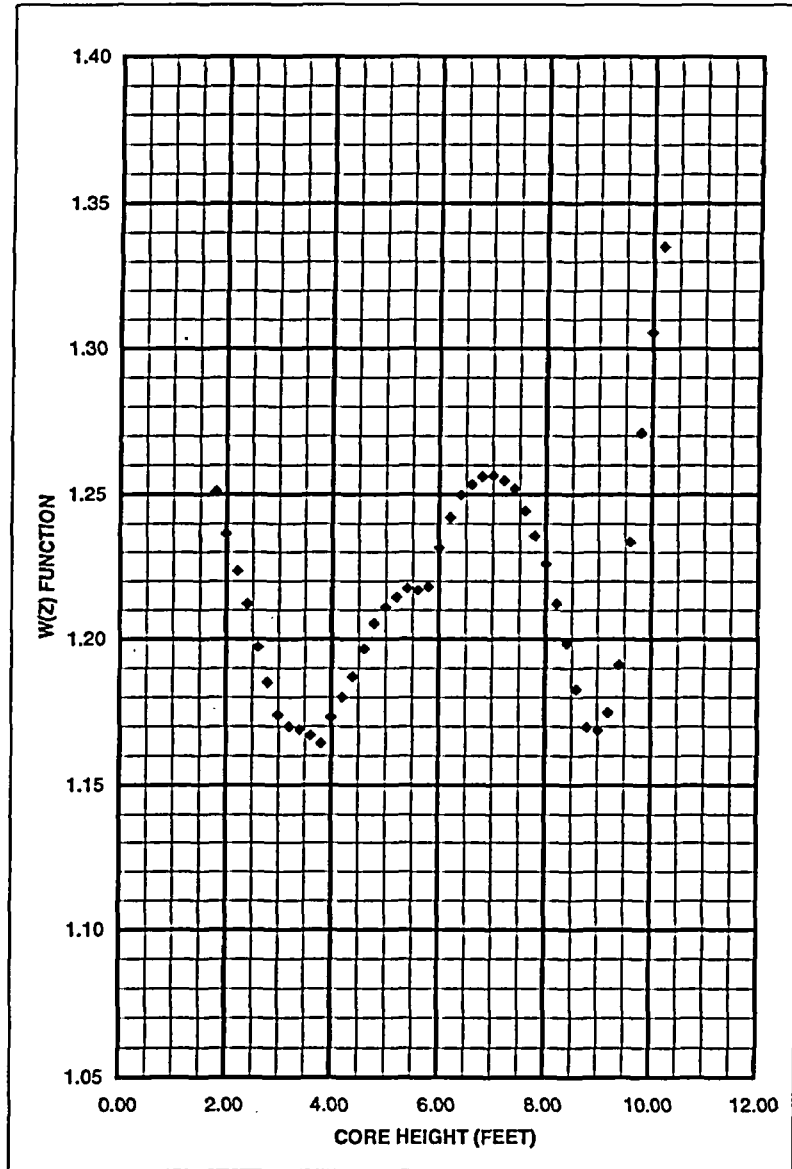
CORE OPERATING LIMITS REPORT (COLR) for BRAIDWOOD UNIT 2 CYCLE 12

Height Feet	MAX W(Z)
0.00	1.0000
0.20	1.0000
0.40	1.0000
0.60	1.0000
0.80	1.0000
1.00	1.0000
1.20	1.0000
1.40	1.0000
1.60	1.0000
1.80	1.2510
2.00	1.2365
2.20	1.2236
2.40	1.2122
2.60	1.1974
2.80	1.1851
3.00	1.1740
3.20	1.1700
3.40	1.1690
3.60	1.1670
3.80	1.1643
4.00	1.1732
4.20	1.1800
4.40	1.1871
4.60	1.1967
4.80	1.2054
5.00	1.2110
5.20	1.2145
5.40	1.2175
5.60	1.2170
5.80	1.2181
6.00	1.2316
6.20	1.2421
6.40	1.2498
6.60	1.2534
6.80	1.2561
7.00	1.2564
7.20	1.2548
7.40	1.2519
7.60	1.2443
7.80	1.2357
8.00	1.2260
8.20	1.2122
8.40	1.1985
8.60	1.1827
8.80	1.1697
9.00	1.1687
9.20	1.1748
9.40	1.1911
9.60	1.2336
9.80	1.2711
10.00	1.3056
10.20	1.3353
10.40	1.0000
10.60	1.0000
10.80	1.0000
11.00	1.0000
11.20	1.0000
11.40	1.0000
11.60	1.0000
11.80	1.0000
12.00	1.0000

Braidwood Unit 2 Cycle 12

Figure 2.6.2.d

Summary of W(Z) Function at 20000 MWD/MTU  
(Top and Bottom 15% Excluded per WCAP-10216)



## CORE OPERATING LIMITS REPORT (COLR) for BRAIDWOOD UNIT 2 CYCLE 12

Table 2.6.2 Penalty Factors In Excess of 2% per 31 EFPD	
Cycle Burnup (MWD/MTU)	Penalty Factor $F_o^c(z)$
13080	1.0200
13252	1.0216
13424	1.0203
13597	1.0200

## Notes:

Linear interpolation is adequate for intermediate cycle burnups.

All cycle burnups outside the range of the table shall use a 2% penalty factor for compliance with the 3.2.1.2 Surveillance Requirements.

## CORE OPERATING LIMITS REPORT (COLR) for BRAIDWOOD UNIT 2 CYCLE 12

2.7 Nuclear Enthalpy Rise Hot Channel Factor ( $F_{\Delta H}^N$ ) (LCO 3.2.2)

$$2.7.1 \quad F_{\Delta H}^N \leq F_{\Delta H}^{\text{RTP}} [1.0 + PF_{\Delta H}(1.0 - P)]$$

where: P = the ratio of THERMAL POWER to RATED THERMAL POWER

$$F_{\Delta H}^{\text{RTP}} = 1.70$$

$$PF_{\Delta H} = 0.3$$

## 2.7.2 Uncertainty when PDMS is Inoperable

The uncertainty,  $U_{F_{\Delta H}}$ , to be applied to the Nuclear Enthalpy Rise Hot Channel Factor  $F_{\Delta H}^N$  shall be calculated by the following formula:

$$U_{F_{\Delta H}} = U_{F_{\Delta Hm}}$$

where:

$$U_{F_{\Delta Hm}} = \text{Base } F_{\Delta H}^N \text{ measurement uncertainty} = 1.04$$

## 2.7.3 PDMS Alarms:

$F_{\Delta H}^N$  Warning Setpoint  $\geq 2\%$  of  $F_{\Delta H}^N$  Margin

$F_{\Delta H}^N$  Alarm Setpoint  $\geq 0\%$  of  $F_{\Delta H}^N$  Margin

2.8 AXIAL FLUX DIFFERENCE (AFD) (LCO 3.2.3)

2.8.1 When PDMS is Inoperable, the AXIAL FLUX DIFFERENCE (AFD) Acceptable Operation Limits are provided in Figure 2.8.1 or the latest valid PDMS Surveillance Report, whichever is more conservative.

2.8.2 When PDMS is OPERABLE, no AFD Acceptable Operation Limits are applicable.

2.9 Departure from Nucleate Boiling Ratio (DNBR) (LCO 3.2.5)

$$2.9.1 \quad \text{DNBR}_{\text{APSL}} \geq 1.536$$

The Axial Power Shape Limiting DNBR ( $\text{DNBR}_{\text{APSL}}$ ) is applicable with THERMAL POWER  $\geq 50\%$  RTP when PDMS is OPERABLE.

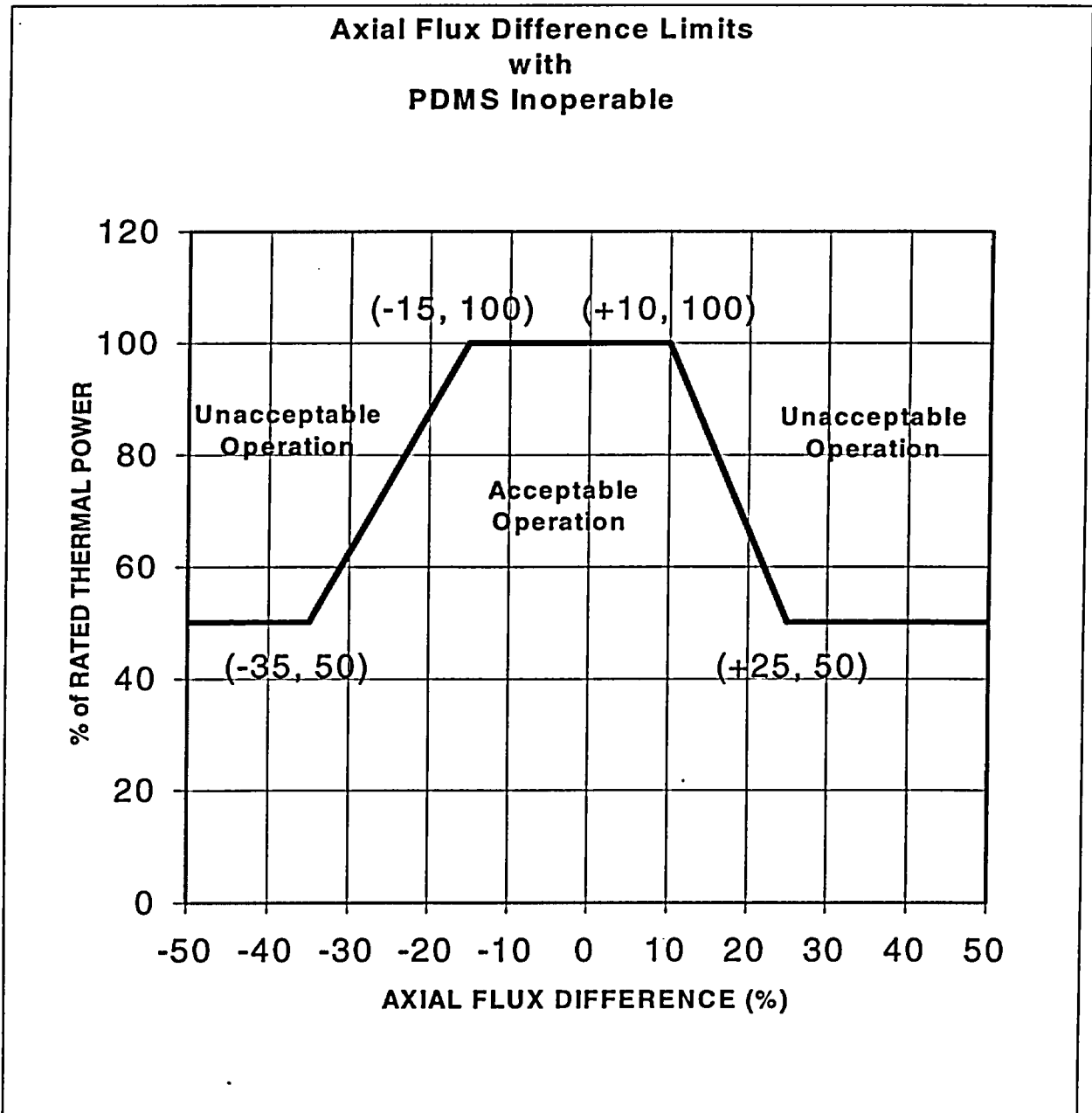
## 2.9.2 PDMS Alarms:

DNBR Warning Setpoint  $\geq 2\%$  of DNBR Margin

DNBR Alarm Setpoint  $\geq 0\%$  of DNBR Margin

CORE OPERATING LIMITS REPORT (COLR) for BRAIDWOOD UNIT 2 CYCLE 12

Figure 2.8.1 Axial Flux Difference Limits as a Function of Rated Thermal Power



## CORE OPERATING LIMITS REPORT (COLR) for BRAIDWOOD UNIT 2 CYCLE 12

2.10 Reactor Trip System (RTS) Instrumentation (LCO 3.3.1) - Overtemperature  $\Delta T$  Setpoint Parameter Values

- 2.10.1 The Overtemperature  $\Delta T$  reactor trip setpoint  $K_1$  shall be equal to 1.325.
- 2.10.2 The Overtemperature  $\Delta T$  reactor trip setpoint  $T_{avg}$  coefficient  $K_2$  shall be equal to 0.0297 / °F.
- 2.10.3 The Overtemperature  $\Delta T$  reactor trip setpoint pressure coefficient  $K_3$  shall be equal to 0.00181 / psi.
- 2.10.4 The nominal  $T_{avg}$  at RTP (indicated)  $T'$  shall be less than or equal to 588.0 °F.
- 2.10.5 The nominal RCS operating pressure (indicated)  $P'$  shall be equal to 2235 psig.
- 2.10.6 The measured reactor vessel  $\Delta T$  lead/lag time constant  $\tau_1$  shall be equal to 8 sec.
- 2.10.7 The measured reactor vessel  $\Delta T$  lead/lag time constant  $\tau_2$  shall be equal to 3 sec.
- 2.10.8 The measured reactor vessel  $\Delta T$  lag time constant  $\tau_3$  shall be less than or equal to 2 sec.
- 2.10.9 The measured reactor vessel average temperature lead/lag time constant  $\tau_4$  shall be equal to 33 sec.
- 2.10.10 The measured reactor vessel average temperature lead/lag time constant  $\tau_5$  shall be equal to 4 sec.
- 2.10.11 The measured reactor vessel average temperature lag time constant  $\tau_6$  shall be less than or equal to 2 sec.
- 2.10.12 The  $f_1(\Delta I)$  "positive" breakpoint shall be +10%  $\Delta I$ .
- 2.10.13 The  $f_1(\Delta I)$  "negative" breakpoint shall be -18%  $\Delta I$ .
- 2.10.14 The  $f_1(\Delta I)$  "positive" slope shall be +3.47% / %  $\Delta I$ .
- 2.10.15 The  $f_1(\Delta I)$  "negative" slope shall be -2.61% / %  $\Delta I$ .



## CORE OPERATING LIMITS REPORT (COLR) for BRAIDWOOD UNIT 2 CYCLE 12

- 2.11 Reactor Trip System (RTS) Instrumentation (LCO 3.3.1) - Overpower  $\Delta T$  Setpoint Parameter Values
- 2.11.1 The Overpower  $\Delta T$  reactor trip setpoint  $K_4$  shall be equal to 1.072.
  - 2.11.2 The Overpower  $\Delta T$  reactor trip setpoint  $T_{avg}$  rate/lag coefficient  $K_5$  shall be equal to 0.02 / °F for increasing  $T_{avg}$ .
  - 2.11.3 The Overpower  $\Delta T$  reactor trip setpoint  $T_{avg}$  rate/lag coefficient  $K_5$  shall be equal to 0 / °F for decreasing  $T_{avg}$ .
  - 2.11.4 The Overpower  $\Delta T$  reactor trip setpoint  $T_{avg}$  heatup coefficient  $K_6$  shall be equal to 0.00245 / °F when  $T > T''$ .
  - 2.11.5 The Overpower  $\Delta T$  reactor trip setpoint  $T_{avg}$  heatup coefficient  $K_6$  shall be equal to 0 / °F when  $T \leq T''$ .
  - 2.11.6 The nominal  $T_{avg}$  at RTP (indicated)  $T''$  shall be less than or equal to 588.0 °F
  - 2.11.7 The measured reactor vessel  $\Delta T$  lead/lag time constant  $\tau_1$  shall be equal to 8 sec.
  - 2.11.8 The measured reactor vessel  $\Delta T$  lead/lag time constant  $\tau_2$  shall be equal to 3 sec.
  - 2.11.9 The measured reactor vessel  $\Delta T$  lag time constant  $\tau_3$  shall be less than or equal to 2 sec.
  - 2.11.10 The measured reactor vessel average temperature lag time constant  $\tau_6$  shall be less than or equal to 2 sec.
  - 2.11.11 The measured reactor vessel average temperature rate/lag time constant  $\tau_7$  shall be equal to 10 sec.
  - 2.11.12 The  $f_2(\Delta I)$  "positive" breakpoint shall be 0 for all  $\Delta I$ .
  - 2.11.13 The  $f_2(\Delta I)$  "negative" breakpoint shall be 0 for all  $\Delta I$ .
  - 2.11.14 The  $f_2(\Delta I)$  "positive" slope shall be 0 for all  $\Delta I$ .
  - 2.11.15 The  $f_2(\Delta I)$  "negative" slope shall be 0 for all  $\Delta I$ .

## CORE OPERATING LIMITS REPORT (COLR) for BRAIDWOOD UNIT 2 CYCLE 12

**2.12 Reactor Coolant System (RCS) Pressure, Temperature, and Flow Departure from Nucleate Boiling (DNB) Limits (LCO 3.4.1)**

2.12.1 The pressurizer pressure shall be greater than or equal to 2209 psig.

2.12.2 The RCS average temperature ( $T_{avg}$ ) shall be less than or equal to 593.1 °F.

2.12.3 The RCS total flow rate shall be greater than or equal to 386,000 gpm.

**2.13 Boron Concentration**

2.13.1 The refueling boron concentration shall be greater than or equal to the value given in the Table below (LCO 3.9.1). The reported value also bounds the end-of-cycle requirements for the previous cycle.

2.13.2 To maintain  $keff \leq 0.987$  with all shutdown and control rods fully withdrawn in MODES 3, 4, or 5 (TRM TLCO 3.1.g Required Action B.2 and TRM TLCO 3.1.k.2), the Reactor Coolant System boron concentration shall be greater than or equal to the values given in the Table below.

COLR Section	Conditions	Boron Concentration (ppm)
2.13.1	Refueling	1750
2.13.2	a) prior to initial criticality	1838
2.13.2	b) all other times in core life	1966