

**Attachment B**

**COLR**

**for**

**Dresden Unit 2 Cycle 19**

**Revision 1**

**GNF-A Proprietary Version**

**Core Operating Limits Report**

for

**Dresden Unit 2 Cycle 19**

## **Proprietary Information Notice**

This document is the GNF non-proprietary version of the GNF proprietary report. From the GNF proprietary version, the information denoted as GNF proprietary (enclosed in double brackets) was deleted to generate this version.

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## Terms and Definitions

APLHGR	Average planar linear heat generation rate
APRM	Average power range monitor
ATRIUM-9B	ATRIUM-9B fuel
BOC	Beginning of cycle
DLO	Dual loop operation
EOC	End of cycle
EOOS	Equipment out of service
EOR	End of rated conditions (i.e cycle exposure at 100% power, 100% flow, all-rods-out)
FWHOOS	Feedwater heater out of service
FW	Feedwater
GE14	GE14C fuel
GNF	Global Nuclear Fuel
ICF	Increased core flow
LHGR	Linear heat generation rate
LHGRFAC <sub>F</sub>	Flow dependent LHGR multiplier
LHGRFAC <sub>P</sub>	Power dependent LHGR multiplier
LPRM	Local power range monitor
MAPLHGR	Maximum average planar linear heat generation rate
MCPR	Minimum critical power ratio
MCPR <sub>F</sub>	Flow dependent MCPR
MCPR <sub>P</sub>	Power dependent MCPR
OLMCPR	Operating limit minimum critical power ratio
PLUOOS	Power load unbalance out of service
PROOS	Pressure regulator out of service
RBM	Rod block monitor
SLMCPR	Safety limit minimum critical power ratio
SLO	Single reactor recirculation loop operation
SPC	Siemens Power Corporation
SRVOOS	Safety-relief valve out of service
TBPOOS	Turbine bypass valve out of service
TCV	Turbine control valve
TIP	Traversing Incore Probe
TSV	Turbine Stop Valve

1. **Average Planar Linear Heat Generation Rate**

1.1 Technical Specification Reference:

Sections 3.2.1 and 3.4.1.

1.2 Description:

Tables 1-1 and 1-2 are used to determine the maximum average planar linear heat generation rate (MAPLHGR) limit for each fuel type. Limits listed in Tables 1-1 and 1-2 are for Dual Reactor Recirculation Loop Operation.

For Single Reactor Recirculation Loop Operation (SLO), the MAPLHGR limits given in Tables 1-1 and 1-2 must be multiplied by a SLO MAPLHGR multiplier. The SLO MAPLHGR multiplier for SPC fuel is 0.84 (Reference 3 Section 16). The SLO MAPLHGR multiplier for GE14 fuel is 0.77 (Reference 3 Section 16).

**Table 1-1**  
**Maximum Average Planar Linear Heat**  
**Generation Rate (MAPLHGR) for all ATRIUM-9B Fuel**  
 ATRM9-P9HATB371-13GZ-SPC100T-9WR-144-T6-3912  
 ATRM9-P9HATB371-13GZ-SPC100T-9WR-144-T6-3914  
 (Bundles 3912 and 3914 - bundle types 6 and 7)  
 (Reference 3 Section 16 )

Planar Average Exposure (GWd/MTU)	MAPLHGR (kW/ft)
0.00	13.52
17.25	13.52
44.09	10.73
70.00	7.84

**Table 1-2**  
**Maximum Average Planar Linear Heat**  
**Generation Rate (MAPLHGR) for all GE14 Fuel**  
 GE14-P10HNAB408-16GZ-100T-145-T6-2483  
 GE14-P10HNAB411-4G7.0/9G6.0-100T-145-T6-2484  
 GE14-P10DNAB418-16GZ-100T-145-T6-2646  
 GE14-P10DNAB389-18GZ-100T-145-T6-2650  
 (Bundles 2483, 2484, 2646 and 2650,  
 bundle types 16, 17, 19, 20, 28, 29, 31, 32, 38, 39, 41, 42 and 47)  
 (Reference 3 Section 16)

Planar Average Exposure (GWd/MTU)	MAPLHGR (kW/ft)
0.00	11.68
16.00	11.68
55.12	8.02
63.50	6.97
70.00	4.36

**2. Minimum Critical Power Ratio**

**2.1 Technical Specification Reference:**

Sections 3.2.2, 3.4.1 and 3.7.7.

**2.2 Description:**

The various MCPR limits are described below.

**2.2.1 Manual Flow Control MCPR Limits**

The Operating Limit MCPR (OLMCPR) is determined from either section 2.2.1.1 or 2.2.1.2, whichever is greater at any given power and flow condition.

**2.2.1.1 Power-Dependent MCPR**

For operation at less than 38.5% core thermal power, the OLMCPR as a function of core thermal power is shown in Table 2-3. For operation at greater than 38.5% core thermal power, the OLMCPR as a function of core thermal power is determined by multiplying the applicable EOOS condition limit shown in Table 2-1 or 2-2 by the applicable MCPR multiplier  $K_F$  given in Table 2-3. For operation at exactly 38.5% core thermal power, the OLMCPR as a function of core thermal power is the higher of either of the two aforementioned methods evaluated at exactly 38.5% core thermal power.

**2.2.1.2 Flow-Dependent MCPR**

Tables 2-4 and 2-5 provide the  $MCPR_F$  limit as a function of flow. The  $MCPR_F$  limit determined from these tables is the flow dependent OLMCPR.

**2.2.2 Automatic Flow Control MCPR Limits**

Automatic Flow Control MCPR Limits are not provided.

**2.2.3 Option A and Option B**

Option A and Option B refer to scram speeds.

Option A scram speed is the Improved Technical Specification scram speed. The core average scram speed insertion time for 20% insertion must be less than or equal to the Technical Specification Scram Speed to utilize Option A MCPR limits. Reload analyses performed by Global Nuclear Fuel (GNF) for Cycle 19 Option A MCPR limits utilized a 20% core average insertion time of 0.900 seconds (Reference 7).

To utilize the MCPR limits for the Option B scram speed, the core average scram insertion time for 20% insertion must be less than or equal to 0.694 seconds (Reference 7). If the core average scram insertion time does not meet the Option B criteria, but is within the Option A criteria, the appropriate MCPR value may be determined from a linear

interpolation between the Option A and B limits with standard mathematical rounding to two decimal places. When performing a linear interpolation to determine MCPR limits, ensure that the time used for Option A is 0.900 seconds, which is the 20% insertion time utilized by GNF in the reload analysis.

#### 2.2.4 Recirculation Pump Motor Generator Settings

Cycle 19 was analyzed with a maximum core flow runout of 110%; therefore the Recirculation Pump Motor Generator scoop tube mechanical and electrical stops must be set to maintain core flow less than 110% (107.8 Mlb/hr) for all runout events (Reference 13 Section 15). This value is consistent with the analyses of Reference 5.

**Table 2-1**  
**M CPR Option A Based Operating Limits**  
 (Reference 3)

EOOS Combination	Fuel Type	Cycle Exposure	
		<EOR <sup>1</sup> - 1385 MWd/MT	≥ EOR <sup>1</sup> - 1385 MWd/MT
Base Case	GE14	1.58	1.68
	ATRIUM-9B	1.54	1.64
Base Case SLO	GE14	1.59	1.69
	ATRIUM-9B	1.55	1.65
TBPOOS	GE14	1.75	1.77
	ATRIUM-9B	1.69	1.71
TBPOOS SLO	GE14	1.76	1.78
	ATRIUM-9B	1.70	1.72
TCV Slow Closure	GE14	1.60	1.68
	ATRIUM-9B	1.54	1.64
TCV Slow Closure SLO	GE14	1.61	1.69
	ATRIUM-9B	1.55	1.65
PLUOOS	GE14	1.64	1.68
	ATRIUM-9B	1.59	1.64
PLUOOS SLO	GE14	1.65	1.69
	ATRIUM-9B	1.60	1.65
TCV Stuck Closed	GE14	1.58	1.68
	ATRIUM-9B	1.54	1.64
TCV Stuck Closed SLO	GE14	1.59	1.69
	ATRIUM-9B	1.55	1.65

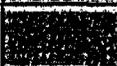
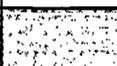
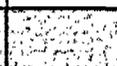
1. EOR refers to the end of rated power (i.e., 100% power/100% flow operation with all rods out)

**Table 2-2**  
**MCPR Option B Based Operating Limits**  
 (Reference 3)

EOOS Combination	Fuel Type	Cycle Exposure	
		<EOR <sup>1</sup> - 1385 MWd/MT	≥ EOR <sup>1</sup> - 1385 MWd/MT
Base Case	GE14	1.47	1.51
	ATRIUM-9B	1.45	1.47
Base Case SLO	GE14	1.48	1.52
	ATRIUM-9B	1.46	1.48
TBPOOS	GE14	1.58	1.60
	ATRIUM-9B	1.52	1.54
TBPOOS SLO	GE14	1.59	1.61
	ATRIUM-9B	1.53	1.55
TCV Slow Closure	GE14	1.47	1.51
	ATRIUM-9B	1.45	1.47
TCV Slow Closure SLO	GE14	1.48	1.52
	ATRIUM-9B	1.46	1.48
PLUOOS	GE14	1.47	1.51
	ATRIUM-9B	1.45	1.47
PLUOOS SLO	GE14	1.48	1.52
	ATRIUM-9B	1.46	1.48
TCV Stuck Closed	GE14	1.47	1.51
	ATRIUM-9B	1.45	1.47
TCV Stuck Closed SLO	GE14	1.48	1.52
	ATRIUM-9B	1.46	1.48

1. EOR refers to the end of rated power (i.e., 100% power/100% flow operation with all rods out)

Table 2-3  
 MCPR<sub>p</sub> for GE and SPC Fuel  
 (Reference 5 and 18)

EOOS Combination	Core Flow (% of rated)	Core Thermal Power (% of rated)								
		0	25	38.5	38.5	45	60	70	70	100
		Operating Limit MCPR			Operating Limit MCPR Multiplier, K <sub>p</sub>					
Base Case	≤ 60	3.19	2.61	2.29	1.32	1.28	1.15			1.00
	> 60	3.81	3.01	2.59						
Base Case SLO	≤ 60	3.20	2.62	2.30	1.32	1.28	1.15			1.00
	> 60	3.82	3.02	2.60						
TBPOOS	≤ 60	5.60	3.81	2.84	1.37	1.28	1.15			1.00
	> 60	6.85	4.66	3.48						
TBPOOS SLO	≤ 60	5.61	3.82	2.85	1.37	1.28	1.15			1.00
	> 60	6.86	4.67	3.49						
TCV Slow Closure	≤ 60	5.60	3.81	2.84	1.64		1.45	1.26	1.11	1.00
	> 60	6.85	4.66	3.48						
TCV Slow Closure SLO	≤ 60	5.61	3.82	2.85	1.64		1.45	1.26	1.11	1.00
	> 60	6.86	4.67	3.49						
PLUOOS	≤ 60	5.60	3.81	2.84	1.64		1.45	1.26	1.11	1.00
	> 60	6.85	4.66	3.48						
PLUOOS SLO	≤ 60	5.61	3.82	2.85	1.64		1.45	1.26	1.11	1.00
	> 60	6.86	4.67	3.49						
TCV Stuck Closed	≤ 60	3.19	2.61	2.29	1.32	1.28	1.15			1.00
	> 60	3.81	3.01	2.59						
TCV Stuck Closed SLO	≤ 60	3.20	2.62	2.30	1.32	1.28	1.15			1.00
	> 60	3.82	3.02	2.60						

Notes for Table 2-3:

- Values are interpolated between relevant power levels.
- For thermal limit monitoring at greater than 100% core thermal power, the 100% core thermal power multiplier, K<sub>p</sub>, should be applied.
- Allowable EOOS conditions are listed in Section 5.
- MCPR<sub>p</sub> limits are independent of scram speed.

**Table 2-4**  
**MCP<sub>F</sub> limits for all fuel types and all operating conditions**  
**except TCV Stuck Closed**

(Reference 10)

Flow (% rated)	MCP <sub>F</sub>
110.0	1.22
100.0	1.22
0.0	1.86

Notes for Table 2-4:

- Values are interpolated between relevant flow values.
- Rated flow is 98 Mlb/hr.
- MCP<sub>F</sub> limit is independent of scram speed.
- This table is not applicable to TCV Stuck Closed operating conditions.

**Table 2-5**  
**MCP<sub>F</sub> limits for all fuel types with a TCV Stuck Closed**

(Reference 10)

Flow (% rated)	MCP <sub>F</sub>
110.0	1.27
108.9	1.27
0.0	1.97

Notes for Table 2-5:

- Values are interpolated between relevant flow values.
- Rated flow is 98 Mlb/hr.
- MCP<sub>F</sub> limit is independent of scram speed.
- This table is only applicable to TCV Stuck Closed operating conditions.







Table 3-7  
 LHGRFAC<sub>p</sub> for all fuel types  
 (Reference 5)

EOOS Combination	Core Flow (% of rated)	Core Thermal Power (% of rated)							
		0	25	38.5	38.5	70	70	80	100
		LHGRFAC <sub>p</sub> multiplier							
Base Case	≤ 60	0.50	0.56	0.59	0.68			0.86	1.00
	> 60								
Base Case SLO	≤ 60	0.50	0.56	0.59	0.68			0.86	1.00
	> 60								
TBPOOS	≤ 60	0.22	0.39	0.48	0.54				1.00
	> 60	0.33		0.42					
TBPOOS SLO	≤ 60	0.22	0.39	0.48	0.54				1.00
	> 60	0.33		0.42					
TCV Slow Closure	≤ 60	0.22	0.39	0.48	0.54	0.73	0.78		1.00
	> 60	0.33		0.42					
TCV Slow Closure SLO	≤ 60	0.22	0.39	0.48	0.54	0.73	0.78		1.00
	> 60	0.33		0.42					
PLUOOS	≤ 60	0.22	0.39	0.48	0.54	0.73	0.78		1.00
	> 60	0.33		0.42					
PLUOOS SLO	≤ 60	0.22	0.39	0.48	0.54	0.73	0.78		1.00
	> 60	0.33		0.42					
TCV Stuck Closed	≤ 60	0.50	0.56	0.59	0.68			0.86	1.00
	> 60								
TCV Stuck Closed SLO	≤ 60	0.50	0.56	0.59	0.68			0.86	1.00
	> 60								

Notes for Table 3-7:

- Values are interpolated between relevant power levels.
- For thermal limit monitoring at greater than 100% core thermal power, the 100% core thermal power LHGRFAC<sub>p</sub> multiplier should be applied.
- Allowable EOOS conditions are listed in Section 5.
- LHGRFAC<sub>p</sub> multiplier is independent of scram speed.
- The LHGR multiplier for any core power/flow condition is the limiting of the LHGRFAC<sub>p</sub>, LHGRFAC<sub>F</sub>, and SLO Multiplier (if applicable)

**Table 3-8**  
**LHGRFAC<sub>F</sub> multipliers**  
 (Reference 5)

Flow (% rated)	LHGRFAC <sub>F</sub>
0	0.28
30	0.55
40	0.64
50	0.77
80	1.00
100	1.00
110	1.00

**Table 3-9**  
**LHGRFAC<sub>F</sub> multipliers for**  
**Turbine Control Valve Stuck Closed**  
 (Reference 5)

Flow (% rated)	LHGRFAC <sub>F</sub>
0	0.14
30	0.41
40	0.50
50	0.63
80	0.86
98.3	1.00
100	1.00
110	1.00

Notes for Tables 3-8 and 3-9:

- Values are interpolated between relevant flow values.
- 98 Mlb/hr is rated flow.
- For thermal limit monitoring above 100% rated core flow, utilize the 100% rated core flow LHGRFAC<sub>F</sub> multiplier.
- LHGRFAC<sub>F</sub> multipliers are applicable to all fuel types.
- Table 3-8 is valid for all operating conditions for all EOOS scenarios except TCV stuck closed.
- Table 3-9 is valid for all operating conditions with a TCV stuck closed.
- LHGRFAC<sub>F</sub> multipliers are independent of scram speed.
- The LHGR multiplier for any core power/flow condition is the limiting of the LHGRFAC<sub>P</sub>, LHGRFAC<sub>F</sub>, and SLO Multiplier (if applicable).

**Table 3-10**  
**LHGR SLO Multipliers for All Fuel Types**

(Reference 3, 15 and 16)

<b>Fuel Product Line</b>	<b>SLO LHGR Multiplier</b>
ATRIUM-9B	0.84
GE-14	0.77

Note for Table 3-10:

- The LHGR multiplier for any core power/flow condition is the limiting of the LHGRFAC<sub>P</sub>, LHGRFAC<sub>F</sub>, and SLO Multiplier (if applicable).

#### 4. Control Rod Withdrawal Block Instrumentation

##### 4.1 Technical Specification Reference:

Table 3.3.2.1-1

##### 4.2 Description:

The Rod Block Monitor Upscale Instrumentation Setpoints are determined from the relationships shown below (Reference 6):

ROD BLOCK MONITOR UPSCALE TRIP FUNCTION	ALLOWABLE VALUE
Two Recirculation Loop Operation	$0.65 W_d + 55\%$
Single Recirculation Loop Operation	$0.65 W_d + 51\%$

The setpoint may be lower/higher and will still comply with the Rod Withdrawal Event (RWE) Analysis because RWE is analyzed unblocked.

$W_d$  – percent of drive flow required to produce a rated core flow of 98 Mib/hr.

## 5. Allowed Modes of Operation (B 3.2.2, B 3.2.3)

The Allowed Modes of Operation with combinations of Equipment Out-of-Service are as described below:

Equipment Out of Service Options <sup>1,2,3,7,8</sup>	OPERATING REGION		
	Standard	MELLLA	Coastdown <sup>4</sup>
Base Case, Option A or B	Yes	Yes	Yes
Base Case SLO, Option A or B	Yes	Yes	Yes
TBPOOS, Option A or B	Yes	Yes	Yes
TBPOOS SLO, Option A or B	Yes	Yes	Yes
TCV Slow Closure <sup>5</sup> , Option A or B	Yes	Yes	Yes
TCV Slow Closure SLO <sup>5</sup> , Option A or B	Yes	Yes	Yes
PLUOOS, Option A or B	Yes	Yes	Yes
PLUOOS SLO, Option A or B	Yes	Yes	Yes
TCV Stuck Closed <sup>6</sup> , Option A or B	Yes	Yes	Yes
TCV Stuck Closed SLO <sup>6</sup> , Option A or B	Yes	Yes	Yes

<sup>1</sup> Each OOS Option may be combined with up to 18 TIP channels OOS (provided the requirements for utilizing SUBTIP methodology are met) with all TIPS available at startup from a refuel outage and up to 50% of the LPRMs OOS with an LPRM calibration frequency of 2500 Effective Full Power Hours (EFPH) (2000 EFPH +25%).

<sup>2</sup> Additionally, a single MSIV may be taken OOS (shut) under any and all OOS Options, so long as core thermal power is maintained  $\leq 75\%$  of 2957 MWt (Reference 12).

<sup>3</sup> Each EOOS Option except TBPOOS requires the opening profile for the Turbine Bypass Valves provided in Reference 7 to be met. These conditions also support 1 Turbine Bypass Valve OOS (TBPOOS) if the assumed opening profile (Reference 7) for the remaining 8 Turbine Bypass Valves is met. If the opening profile is not met with 8 or 9 operating Turbine Bypass Valves, or if two Turbine Bypass Valves are OOS, utilize the TBPOOS condition. For operation with three or more Turbine Bypass Valves OOS, utilize the TBPOOS Condition for operation above 42% rated power and the PLUOOS Condition for operation at or below 42% rated power. (References 25 and 26)

<sup>4</sup> Coastdown operation is defined as any cycle exposure beyond the full power, all rods out condition with plant power slowly lowering to a lesser value while core flow is held constant (Reference 11 Section 4.3.1.2.8). Up to a 15% overpower is analyzed per Reference 5.

<sup>5</sup> For operation with a pressure regulator out-of-service (PROOS), the TCV Slow Closure limits should be applied (Reference 17) and the operational notes from Reference 17 reviewed. PROOS and TCV Slow

Closure is not an analyzed out-of-service combination.

<sup>6</sup> Operation with one TSV OOS is allowed as evaluated in Reference 23. Combination of one TCV OOS and one TSV OOS is not allowed.

<sup>7</sup> The cycle specific stability analysis may impose restrictions on the Power-to-flow map and/or restrict the applicable temperature for feedwater temperature reduction (FWTR).

<sup>8</sup> Each EOOS option allows operation with up to a 10°F reduction in feedwater temperature (Final Feedwater Temperature Reduction or Feedwater Heaters OOS) throughout the cycle. For operation with reduced feedwater temperature greater than 10°F and less than or equal to 120°F, the penalties from Reference 27 shall be applied.

## 6. Methodology (5.6.5)

The analytical methods used to determine the core operating limits shall be those previously reviewed and approved by the NRC, specifically those described in the following documents:

1. ANF-1125 (P)(A) and Supplements 1 and 2, "Critical Power Correlation – ANFB," April 1990.
2. ANF-524 (P)(A) Revision 2 and Supplements 1 and 2, "ANF Critical Power Methodology for Boiling Water Reactors," November 1990.
3. XN-NF-79-71 (P)(A) Revision 2 and Supplements 1, 2 & 3, "Exxon Nuclear Plant Transient Methodology for Boiling Water Reactors," March 1986.
4. XN-NF-80-19 (P)(A) Volume 1 Supplements 1 and 2, "Exxon Nuclear Methodology for Boiling Water Reactors – Neutronic Methods for Design and Analysis," March 1993.
5. XN-NF-80-19 (P)(A) Volume 1 Supplement 3, Supplement 3 Appendix F, and Supplement 4, "Exxon Nuclear Methodology for Boiling Water Reactors," November 1990.
6. XN-NF-80-19 (P)(A) Volumes 2, 2A, 2B and 2C, "Exxon Nuclear Methodology for Boiling Water Reactors: EXEM BWR ECCS Evaluation Model," September 1982.
7. XN-NF-80-19 (P)(A) Volume 3 Revision 2, "Exxon Nuclear Methodology for Boiling Water Reactors, THERMEX: Thermal Limits Methodology Summary Description," January 1987.
8. XN-NF-80-19 (P)(A) Volume 4 Revision 1, "Exxon Nuclear Methodology for Boiling Water Reactors: Application of the ENC Methodology to BWR Reloads," June 1986.
9. XN-NF-85-67 (P)(A) Revision 1, "Generic Mechanical Design for Exxon Nuclear Jet Pump BWR Reload Fuel," September 1986.
10. ANF-913 (P)(A) Volume 1 Revision 1, and Volume 1 Supplements 2, 3, 4, "COTRANSA2: A Computer Program for Boiling Water Reactor Transients Analysis," August 1990.
11. XN-NF-82-06- (P)(A) Revision 1 and Supplements 2, 4 and 5, "Qualification of Exxon Nuclear Fuel for Extended Burnup," October 1986.
12. XN-NF-82-06- (P)(A) Supplement 1 Revision 2, "Qualification of Exxon Nuclear Fuel for Extended Burnup Supplement 1 Extended Burnup Qualification of ENC 9x9 BWR Fuel," May 1988.
13. ANF-89-14(P)(A) Revision 1 and Supplements 1 & 2, "Advanced Nuclear Fuels Corporation Generic Mechanical Design for Advanced Nuclear Fuels Corporation 9X9 – IX and 9x9 – 9X BWR Reload Fuel," October 1991.
14. ANF-89-14(P), "Advanced Nuclear Fuels Corporation Generic Mechanical Design for Advanced Nuclear Fuels Corporation 9X9 – IX and 9x9 – 9X BWR Reload Fuel," May 1989.
15. ANF-89-98 (P)(A), "Generic Mechanical Design Criteria for BWR Fuel Designs," Revision 1 and Revision 1 Supplement 1, May 1995.
16. ANF-91-048 (P)(A), "Advanced Nuclear Fuels Corporation Methodology for Boiling Water Reactors EXEM BWR ECCS Evaluation Model," January 1993.
17. Commonwealth Edison Company Topical Report NFSR-0091, "Benchmark of CASMO/MICROBURN BWR Nuclear Design Methods," Revision 0 and Supplements on Neutronics Licensing Analysis

(Supplement 1) and La Salle County Unit 2 benchmarking (Supplement 2), December 1991, March 1992, and May 1992, respectively.

18. EMF-85-74 (P) Revision 0 and Supplement 1(P)(A) and Supplement 2(P)(A), "RODEX2A (BWR) Fuel Rod Thermal-Mechanical Evaluation Model," February 1998.
19. NEDE-24011-P-A-14 Revision 14, "General Electric Standard Application for Reactor Fuel (GESTAR)," June 2000.
20. NEDC-32981P Revision 0, "GEXL96 Correlation for ATRIUM-9B Fuel", September 2000.
21. ANF-1125(P)(A), Supplement 1 Appendix E, "ANFB Critical Power Correlation Determination of ATRIUM-9B Additive Constant uncertainties," September 1998.
22. ANF-91-048(P)(A), Supplements 1 and 2, "BWR Jet Pump Model Revision for RELAX," October 1997.