

May 15, 2004

NRC 2004-0053  
10 CFR 50.55a(a)(3)(i)  
10 CFR 50.55a(g)(5)(iii)

U.S. Nuclear Regulatory Commission  
ATTN: Document Control Desk  
Washington, DC 20555

Point Beach Nuclear Plant, Units 1 and 2  
Dockets 50-266  
License Nos. DPR-24

Supplement 1 to Reactor Vessel Closure Head Penetration Repair and Flaw  
Characterization Relief Requests MR 02-018-1, Revision 1 and MR 02-018-2,  
Revision 1

Reference: (1) Letter from NMC to NRC dated May 13, 2004 (NRC 2004-0051)  
(2) NRC Safety Evaluation dated September 10, 2003  
(3) NRC Safety Evaluation dated September 24, 2003

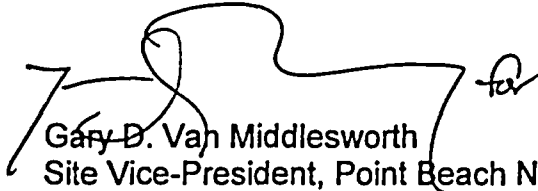
In reference 1, Nuclear Management Company (NMC) LLC, licensee for Point Beach Nuclear Plant (PBNP), requested revision to the relief, granted in references 2 and 3, pertaining to reactor vessel closure head (RVCH) penetration repair and flaw characterization.

During a conference call between NRC staff and NMC personnel on May 15, 2004, the staff requested additional information in support of their review of Reference 1, regarding crack growth rates in addition to those documented in EPRI MRP-55, "Materials Reliability Program (MRP) Crack Growth Rates for Evaluating Primary Water Stress Corrosion Cracking (PWSCC) of Thick-Wall Alloy 600 Material." Enclosure 1 to this letter provides the additional information requested by the staff.

This submittal provides revised primary water stress corrosion cracking (PWSCC) crack growth correlations and fatigue crack growth calculations, for the repair and flaw characterization, where portions of the new pressure boundary weld overlap onto portions of the remnant J-groove weld. These correlations and calculations address hypothetical growth in Alloy 82 material as a conservative representation for Alloy 52.

The conclusion of the revised calculation shows that, even with the very conservative assumption of using Alloy 82 crack growth rates for Alloy 52 weld material, a hypothetical remnant weld crack will not grow through the repair weld ligament for 1.4 effective full power years (EFPY) of operation. Therefore, the hypothetical flaw could not progress sufficiently to go through the pressure boundary during the next Unit 1 operating cycle.

This submittal contains no new or revised regulatory commitments.

A handwritten signature in black ink, appearing to read "Gary D. Van Middlesworth", is written over the typed name. The signature is stylized and includes a large loop at the end.

Gary D. Van Middlesworth  
Site Vice-President, Point Beach Nuclear Plant  
Nuclear Management Company, LLC

Enclosure: 1 - Structural Integrity Associates Calculation PBCH-09Q-302,  
Revision 2, Dated May 15, 2004

cc: Project Manager, Point Beach Nuclear Plant, NRR, USNRC  
Regional Administrator, Region III, USNRC  
NRC Resident Inspector - Point Beach Nuclear Plant  
PSCW

**ENCLOSURE I**

**STRUCTURAL INTEGRITY ASSOCIATES CALCULATION PBCH-09Q-302, REVISION 2,  
DATED MAY 15, 2004**

**PWSCC CRACK GROWTH CORRELATIONS AND FATIGUE CRACK GROWTH  
CALCULATIONS FOR POINT BEACH UNIT 1**

**POINT BEACH NUCLEAR PLANT, UNIT 1**



**STRUCTURAL  
INTEGRITY  
Associates, Inc.**

**CALCULATION  
PACKAGE**

FILE No.: PBCH-09Q-302

PROJECT No.: PBCH-09Q

PROJECT NAME: Point Beach Unit 1 CRDM Top Head Analysis

CLIENT: NMC Point Beach Nuclear Plant

CALCULATION TITLE: PWSCC Crack Growth Correlations and Fatigue Crack Growth Calculations for Point Beach Unit 1

Document Revision	Affected Pages	Revision Description	Project Mgr. Approval Signature & Date	Preparer(s) & Checker(s) Signatures & Date
0	1-7 A1 - A19	Original Issue	H. L. GUSTIN  2/17/04	H. L. GUSTIN 2/17/04  G. L. STEVENS 2/17/04
1	1-7 A1-A19	Incorporates actual overlap measurements for nozzle 26. Appendix A is not affected.	H. L. GUSTIN <i>H. L. Gustin</i> 5/12/04	H. L. GUSTIN <i>H. L. Gustin</i> 5/12/04  MING QIN <i>Ming Qin</i> 5/12/04
2	1-8 A1-A19	Addresses hypothetical growth in Alloy 82 material, as a conservative representation for Alloy 52	H. L. GUSTIN <i>H. L. Gustin</i> 5/15/04	H. L. GUSTIN <i>H. L. Gustin</i> 5/15/04  <i>P. C. Riccardella</i> P. C. RICCARDELLA 5/15/04

## 1.0 STATEMENT OF PROBLEM

Point Beach Unit 1 is proceeding with repair of RPV top head CRDM Nozzle 26 during the current, Spring 2004 refueling outage. Because of the steepness of this nozzle, and the relatively small head diameter and thickness, the standard Framatome repair process will result in a portion of the new attachment weld overlapping the original Alloy-82/182 weld over a portion of the circumference (see Figure 1).

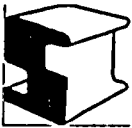
In order to evaluate repair options for the Point Beach Unit 1 Top Head CRDM penetrations, this calculation evaluates the growth of hypothetical flaws in the original alloy 82/182 weld through the weld repair fusion line with the low alloy steel base material. Earlier revisions of this calculation assumed a crack growth rate applicable to Alloy-600 base metal. To respond to NRC comments received on the earlier calculation, the calculation is revised herein to incorporate crack growth rates applicable to Alloy 82 weld metal.

Note that the repair weld through which the hypothetical crack is assumed to be propagating is Alloy-52, which has generally been shown to be highly resistant to PWSCC cracking and crack growth. The only potential crack growth region is at the fusion line between the low alloy steel nozzle and the Alloy-52 weld metal, in which some dilution of the weld metal may occur. Both the Alloy-600 and Alloy-82 crack growth curves are believed to be conservative approximations of the expected crack growth rate in this dilution zone.

## 2.0 METHODOLOGY

Stress intensity factors at the interface of the new, Alloy-52 repair weld and the original, Alloy-82/182 J-groove weld have been computed in Ref [5] assuming the entire original J-groove weld to be cracked. These K-levels are based on operating plus residual stresses resulting from the original J-groove weld plus the new repair weld, at normal operating conditions. The result K-levels are assumed to remain constant for the small amount of crack extension through the interface region, since the cracking will be confined to a narrow region of diluted material.

The resulting K-levels are then inserted into a stress corrosion crack growth law (see section 3.0 below) to determine the rate of crack propagation versus time, and to predict the time necessary for the assumed initial crack to grow through the new repair weld diluted zone and thus cause potential leakage during the upcoming fuel cycle.

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### 3.0 MATERIAL CRACK GROWTH RATE

The industry has established a panel of experts on stress corrosion cracking to review available data on PWSCC growth in components such as the CRDM penetration tubes and associated nickel-based weld metals. The panel is comprised of international experts, including representatives from NRC research and its contractors. This panel has established a recommended crack growth law for Alloy-600 base material [1], and more recently a recommended crack growth curves for Alloy 82 and 182 weld metals [2]. The correlation of available crack growth data from [2] is shown in Figure 2, normalized to a service temperature of 617 °F. The reported top head temperature for Point Beach Unit 1 is 592°F [7]. The crack growth rate is a strong function of temperature, and so to represent the Point Beach condition, it is necessary to adjust the Alloy-82 crack growth correlation for the lower temperature. References 1 and 2 also provide an activation energy equation for temperature adjustment of the crack growth curves.

For Alloy-82 weld material the PWSCC crack growth correlation reported in [2], adjusted to the Point Beach head temperature of 592°F is

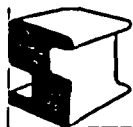
$$da/dt = 5.12 \times 10^{-08} (K - K_{th})^{1.6}$$

where:

- da/dt = crack growth rate at temperature T in in/hr
- K = crack tip stress intensity factor (ksi√in)
- K<sub>th</sub> = crack tip stress intensity factor threshold = 0 (ksi√in)

This correlation is applicable to evaluating the growth of ID connected flaws in Alloy 82 GTAW weld material. Since the diluted zone being evaluated in this calculation is Alloy-52, also a GTAW welding process, the Alloy-82 curve is conservatively applied.

As noted above, the repair material is Alloy 52. Since chromium content has been shown to be a key contributor to nickel-based alloy PWSCC resistance, this material (Alloy 52, with a chromium content of 28-31%) will have significantly higher PWSCC resistance than will Alloy 600 (chromium content 14-17%) or its associated weld materials Alloy 182 (chromium content 13-17%) or Alloy 82 (chromium content 18-22 %). The lower chromium content of the Alloy -82 material is deemed sufficient to account for the potential effects of dilution of the Alloy-52 material in the interface region with the low alloy steel head.



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#### 4.0 CRACK GROWTH CALCULATIONS

The objective of the calculation is to determine the time that would be required for a crack at the interface of the Alloy 52 repair material, the low alloy steel head material, and the underlying J-groove material to propagate parallel to the repair weld by a PWSCC mechanism through a distance defined by the repair weld ligament. If the time for such propagation is greater than the remaining service life of the head, no penetration of the pressure boundary due to such a crack would be predicted.

The above crack growth correlation was used with the SI program pc-CRACK [3] to perform PWSCC crack growth calculations. A hypothetical flaw was considered, which represents the bounds on geometries that may be encountered. This hypothetical flaw was a flaw in the axial-radial plane, across the entire remaining J-groove + butter. Such a flaw would be opened by hoop stresses, resulting in a tunnel crack under the repair weld.

PWSCC is driven by both applied and weld residual stresses. Based on analyses performed by Dominion Engineering [3], as summarized in another SI calculation [5], the normal operating stresses plus the weld residual stresses in the hoop direction can reasonably be represented by a constant through-wall stress intensity factor of 57 ksi $\sqrt{\text{in}}$ , at the junction of the Alloy-52 repair weld and the low alloy steel head material.

The analysis assumed that the entire original J-groove weld material was degraded (cracked), so no credit was taken for any flaw initiation or growth time in the remaining J-groove material. Because a constant applied K is assumed, starting flaw size has no effect on crack growth rate.

The flaw located in the axial-radial plane (opened by hoop stresses) was determined to be the governing flaw case, since the applied plus residual stresses in the hoop direction are greater than those in the radial direction by a factor of two to four at the location of the postulated crack, based upon review of Dominion Engineering results [3] for nodes in this location. As a result, crack growth in a radial-circumferential plane would be slower by a comparable factor.

Nozzle 26 is being repaired during the Spring 2004 outage. The repair of this nozzle has a minimum remaining ligament of 0.5 inch [6]. The repair may also contain a weld root defect of 0.1 inch based on Framatome analyses. Both cases (with and without a postulated root defect) are considered here, with pc-CRACK results contained in Appendix A.

This analysis took no credit for the portion of the repair weld that overlapped the Alloy 182 material, and so as a result the repair weld ligament was considered to be reduced in length from the design value. The repair weld is Alloy 52 weld material applied by a GTAW process.



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#### 4.1 Fatigue crack growth


Fatigue crack growth is driven by cyclic stresses. For the present case, the stress state for the assumed flaws is dominated by weld residual stresses (conservatively estimated as a constant 60 ksi) which are steady state secondary stresses. These residual stresses will not vary with heat-up/cooldown and other plant cycles, and will therefore have only a limited effect on fatigue crack growth (that is, they will have some effect on R-ratio, but none on delta K values due to cyclic plant operation. For the limited period of remaining plant operation with the current vessel head (estimated at less than 100 heat-up/cooldown cycles, producing a cyclic stress of 20 ksi), propagation of the hypothetical cracks considered herein by a fatigue mechanism is estimated at approximately 0.0002 inch, and is therefore considered negligible compared to PWSCC propagation discussed above. The pc-CRACK fatigue crack growth results are also included in Appendix A.

#### 5.0 RESULTS

The above analysis produces the following results. These results assume that an initial radial-axial flaw is present in the original J-groove weld, equal to the entire size of that weld. The growth is then calculated for the indicated remaining ligament length of potentially diluted Alloy-52 weld metal in the repair weld..

For the nozzle 26 repair (remaining ligament = 0.5 inch without an assumed root defect, or 0.4 inch with an assumed root defect), the time required for the assumed flaw to propagate through the remaining ligament is 1.73 EFPY (15200 EFPH) for the no root defect case, and 1.39 EFPY (12200 EFPH) for the root defect case. A crack would have to propagate through this remaining ligament before leakage and possible wastage of the vessel head material could occur.

The conclusion of this calculation is that, even with the very conservative assumption of using Alloy 82 crack growth rates for Alloy 52 weld material, a hypothetical remnant weld crack will not grow through the repair weld ligament for essentially all of the remaining cycle of operation before the reactor vessel head is replaced during the next scheduled refueling outage.

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## 6.0 REFERENCES

1. Materials Reliability Program, "Crack Growth Rates for Evaluating Primary Water Stress Corrosion Cracking (PWSCC) of Thick-Wall Alloy 600 Material," MRP-55, Revision 1, November 2002. EPRI Proprietary
2. Minutes of EPRI-MRP PWSCC Crack Growth Expert Panel Meeting, October 3, 2003 – Gaithersburg, Maryland, EPRI Letter PWR-MRP 2003-38 by John Hickling, October 20, 2003. MRP Proprietary.
3. Dominion Engineering, "Point Beach Unit 1 CRDM Nozzle Repair Weld Analysis" Calculation C-4430-00-2, Revision 1, SI File PBCH-09Q-204.
4. Structural Integrity Associates, pc-CRACK<sup>tm</sup> for Windows, version 3.1-98348.
5. Calculation, "Fracture Mechanics Evaluation of Point Beach Unit 1 Top Head CRDM 43.5 Degree Azimuth Penetration Weld Repair," PBCH-09Q-301, Revision 0.
6. E-mail from Brian Kemp (NMC) to Hal Gustin (SI) 5/12/04
7. Materials Reliability Program, "Interim Alloy 600 Safety Assessments for US PWR Plants, Part 2: Reactor Vessel Top Head penetrations," MRP-44, EPRI Report No. TP-1001491, Part 2, May 2001


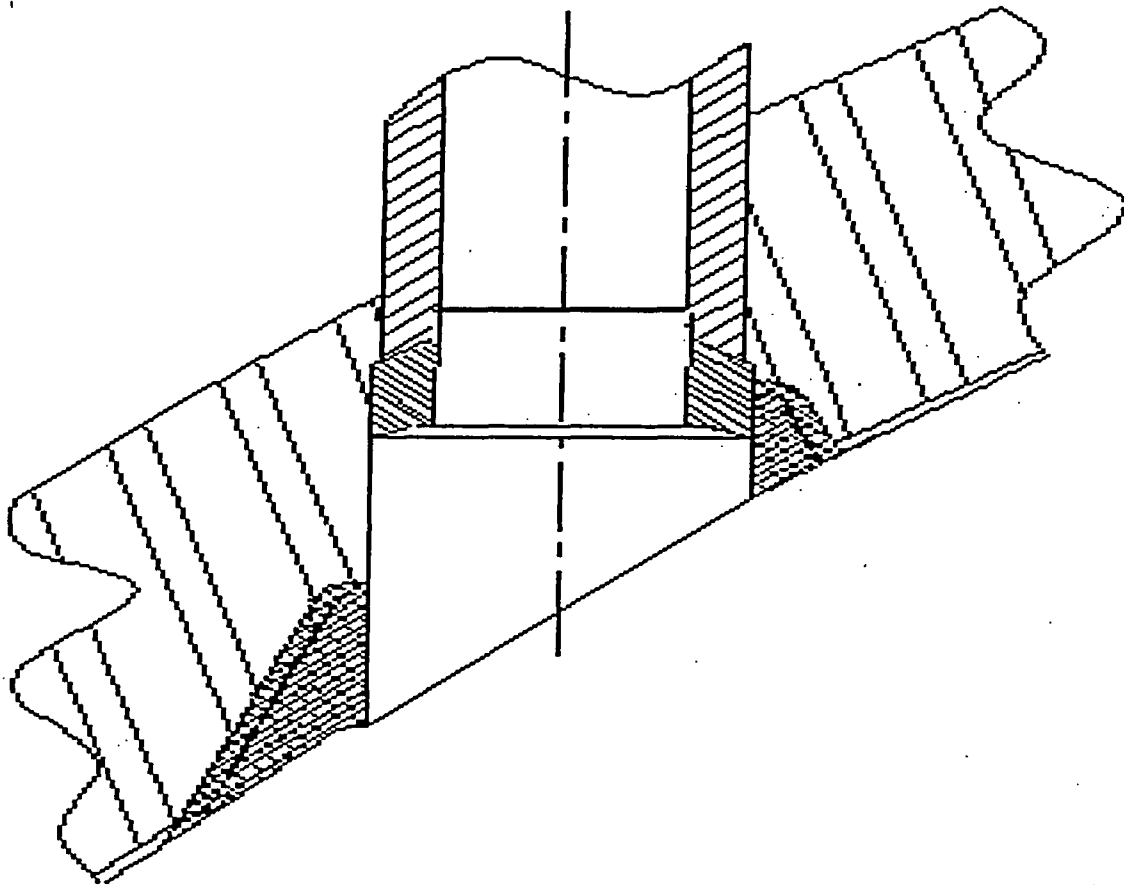
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Figure 1 – Illustration of Nozzle 26 Repair and Associated Overlap Region

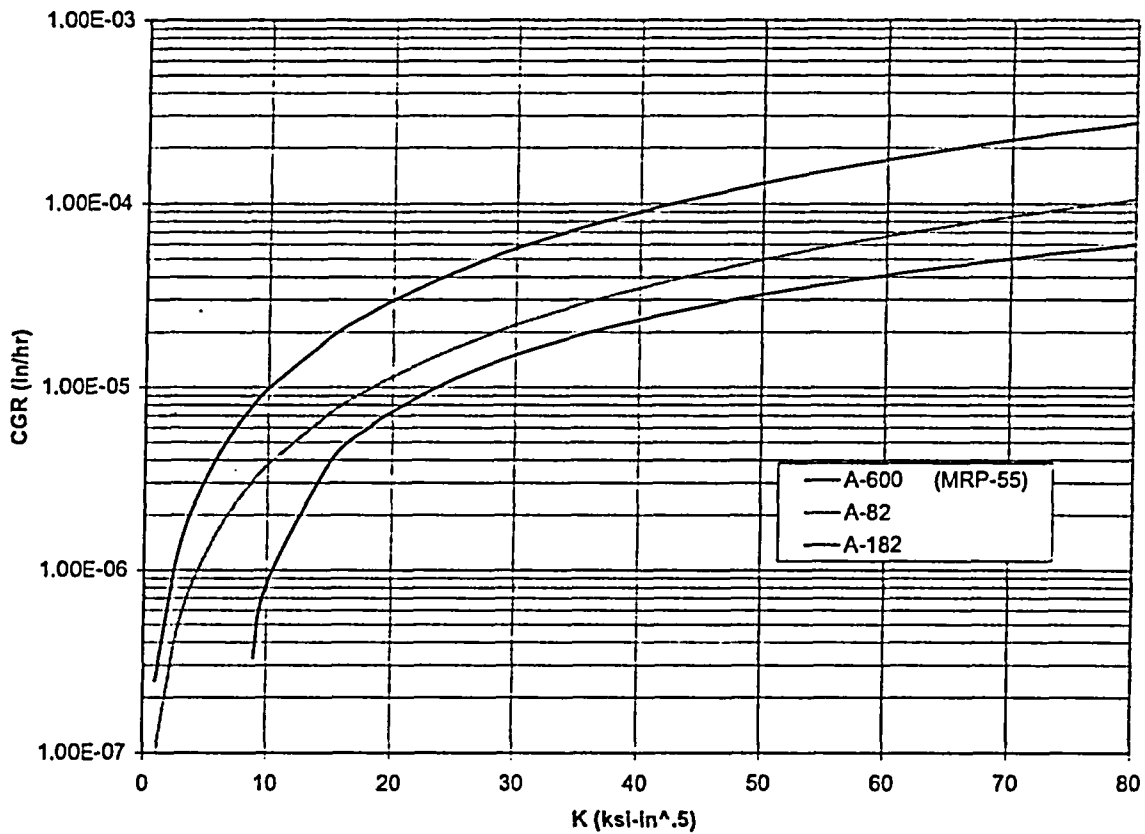


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Figure 2 – Alloy-82 and -182 Crack Growth Rate Correlations at 617 °F, from Reference [2]



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APPENDIX A  
 FLAW GROWTH CALCULATIONS: PC-CRACK OUTPUT



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tm  
 pc-CRACK for Windows  
 Version 3.1-98348  
 (C) Copyright '84 - '98  
 Structural Integrity Associates, Inc.  
 3315 Almaden Expressway, Suite 24  
 San Jose, CA 95118-1557  
 Voice: 408-978-8200  
 Fax: 408-978-8964  
 E-mail: pccrack@structint.com

Linear Elastic Fracture Mechanics

Date: Thu May 13 15:05:22 2004  
 Input Data and Results File: ALLOY82.LFM

Title: PBCH-09Q: PWSCC Calculation using Alloy 82

Load Cases:

Case ID: PWSCC --- K vs a


Depth      K

0.0000	57.0000
0.5000	57.0000
2.0000	57.0000

Case ID	Stress Coefficients				Type
	C0	C1	C2	C3	
PWSCC	0	0	0	0	K vs a

Crack Model: User Input K Versus Crack Size

Crack Parameters:  
 Max. crack size: 1.0000

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-----Stress Intensity Factor-----

Crack Case  
Size PWSCC

---

0.0200	57
0.0400	57
0.0600	57
0.0800	57
0.1000	57
0.1200	57
0.1400	57
0.1600	57
0.1800	57
0.2000	57
0.2200	57
0.2400	57
0.2600	57
0.2800	57
0.3000	57
0.3200	57
0.3400	57
0.3600	57
0.3800	57
0.4000	57
0.4200	57
0.4400	57
0.4600	57
0.4800	57
0.5000	57
0.5200	57
0.5400	57
0.5600	57
0.5800	57
0.6000	57
0.6200	57
0.6400	57
0.6600	57
0.6800	57



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0.7000 57  
 0.7200 57  
 0.7400 57  
 0.7600 57  
 0.7800 57  
 0.8000 57  
 0.8200 57  
 0.8400 57  
 0.8600 57  
 0.8800 57  
 0.9000 57  
 0.9200 57  
 0.9400 57  
 0.9600 57  
 0.9800 57  
 1.0000 57

Crack Growth Laws:

Law ID: Alloy 82  
 Type: Corrosion  
 Model: Paris


$da/dN = c * (dK)^n$   
 where  
 $dK = K_{max} - K_{min}$   
 $dK > K_{thres}$   
 $K_{max} < K_{Ic}$

Material parameters:  
 $c = 5.1200e-008$   
 $n = 1.6000$   
 $K_{thres} = 0.0000$

Material Fracture Toughness  $K_{Ic}$ :

Material ID: Alloy 52

Depth  $K_{Ic}$

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0.0000 200.0000  
 0.5000 200.0000  
 2.0000 200.0000

Initial crack size= 0.0100  
 Max. crack size= 1.0000

Number of blocks= 1  
 Print increment of block= 1

Subblock	Cycles /Time	Calc. incre.	Print incre.	Crk. Law	Grw. Alloy	Mat. K1c
PWSCC	40000	100	100	Alloy 82		Alloy 52

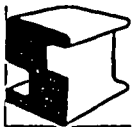
Subblock	Case ID	Kmax Scale Factor	Kmin Case ID	Scale Factor
PWSCC	PWSCC		1.0000	

Crack growth results:

/Time	/Time	Total Subblock				DaDn		
		Cycles Kmax	Cycles Kmin	DeltaK	R	/DaDt	Da	a a/thk

Block: 1

100	100	4.03e+001	0.00e+000	4.03e+001	0.00	1.90e-005	1.90e-003	0.0119	0.00
200	200	4.40e+001	0.00e+000	4.40e+001	0.00	2.18e-005	2.18e-003	0.01407	-
247674372620288.00									
300	300	4.78e+001	0.00e+000	4.78e+001	0.00	2.49e-005	2.49e-003	0.01657	593.04
400	400	5.19e+001	0.00e+000	5.19e+001	0.00	2.84e-005	2.84e-003	0.01941	-0.00
500	500	5.61e+001	0.00e+000	5.61e+001	0.00	3.22e-005	3.22e-003	0.02263	-0.00
600	600	5.70e+001	0.00e+000	5.70e+001	0.00	3.30e-005	3.30e-003	0.02593	0.00
700	700	5.70e+001	0.00e+000	5.70e+001	0.00	3.30e-005	3.30e-003	0.02923	0.00



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800 800 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.03253 0.00  
900 900 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.03583 0.00  
1000 1000 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.03913 0.00  
1100 1100 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.04244 0.00  
1200 1200 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.04574 0.00  
1300 1300 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.04904 0.00  
1400 1400 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.05234 0.00  
1500 1500 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.05564 0.00  
1600 1600 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.05894 0.00  
1700 1700 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.06224 0.00  
1800 1800 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.06554 0.00  
1900 1900 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.06885 0.00  
2000 2000 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.07215 0.00  
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2400 2400 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.08535 0.00  
2500 2500 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.08865 0.00  
2600 2600 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.09195 0.00  
2700 2700 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.09525 0.00  
2800 2800 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.09856 0.00  
2900 2900 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.1019 0.00  
3000 3000 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.1052 0.00  
3100 3100 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.1085 0.00  
3200 3200 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.1118 0.00  
3300 3300 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.1151 0.00  
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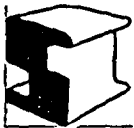
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Preparer/Date	HLG 2/17/04	HLG 5/12/04	HLG 5/15/04	
Checker/Date	GLS 2/17/04	MQ 5/12/04	PCR 5/15/04	
File No.	PBCH-09Q-302		Page A6 of A19	

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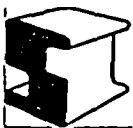
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Preparer/Date	HLG 2/17/04	HLG 5/12/04	HLG 5/15/04	
Checker/Date	GLS 2/17/04	MQ 5/12/04	PCR 5/15/04	
File No.	PBCH-09Q-302		Page A7 of A19	

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Revision	0	1	2	
Preparer/Date	HLG 2/17/04	HLG 5/12/04	HLG 5/15/04	
Checker/Date	GLS 2/17/04	MQ 5/12/04	PCR 5/15/04	
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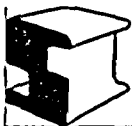
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Preparer/Date	HLG 2/17/04	HLG 5/12/04	HLG 5/15/04	
Checker/Date	GLS 2/17/04	MQ 5/12/04	PCR 5/15/04	
File No.	PBCH-09Q-302			Page A9 of A19

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 20100 20100 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.6697 0.00  
 20200 20200 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.673 0.00  
 20300 20300 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.6763 0.00  
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 20500 20500 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.6829 0.00  
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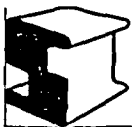
Revision	0	1	2	
Preparer/Date	HLG 2/17/04	HLG 5/12/04	HLG 5/15/04	
Checker/Date	GLS 2/17/04	MQ 5/12/04	PCR 5/15/04	
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21300 21300 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.7093 0.00  
 21400 21400 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.7126 0.00  
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 21600 21600 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.7192 0.00  
 21700 21700 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.7225 0.00  
 21800 21800 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.7258 0.00  
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 22000 22000 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.7324 0.00  
 22100 22100 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.7357 0.00  
 22200 22200 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.739 0.00  
 22300 22300 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.7423 0.00  
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 22500 22500 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.7489 0.00  
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 22800 22800 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.7588 0.00  
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Revision	0	1	2	
Preparer/Date	HLG 2/17/04	HLG 5/12/04	HLG 5/15/04	
Checker/Date	GLS 2/17/04	MQ 5/12/04	PCR 5/15/04	
File No.	PBCH-09Q-302			Page All of A19

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 29300 29300 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 0.9734 0.00  
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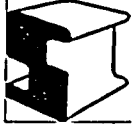


Revision	0	1	2	
Preparer/Date	HLG 2/17/04	HLG 5/12/04	HLG 5/15/04	
Checker/Date	GLS 2/17/04	MQ 5/12/04	PCR 5/15/04	
File No.	PBCH-09Q-302		Page A12 of A19	

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 30200 30200 5.70e+001 0.00e+000 5.70e+001 0.00 3.30e-005 3.30e-003 1.003 0.00

Crack size exceeded 1.0000 at cycle/time 30200

End of pc-CRACK Output

	Revision	0	1	2	
	Preparer/Date	HLG 2/17/04	HLG 5/12/04	HLG 5/15/04	
	Checker/Date	GLS 2/17/04	MQ 5/12/04	PCR 5/15/04	
	File No.	PBCH-09Q-302			Page A13 of A19



tm  
 pc-CRACK for Windows  
 Version 3.1-98348  
 (C) Copyright '84 - '98  
 Structural Integrity Associates, Inc.  
 3315 Almaden Expressway, Suite 24  
 San Jose, CA 95118-1557

Linear Elastic Fracture Mechanics

Date: Mon Feb 09 10:59:19 2004  
 Input Data and Results File: PB1FCG.LFM

Title: PBCH-09Q-302: Point Beach Unit 1 Fatigue Crack Growth

Load Cases:

Case ID	Stress Coefficients				Type
	C0	C1	C2	C3	
Residual	60	0	0	0	Coeff
Operating	20	0	0	0	Coeff

-----Through Wall Stresses for Load Cases With Stress Coeff-----

Wall Depth	Case Residual	Case Operating
0.0000	60	20
0.1000	60	20
0.2000	60	20
0.3000	60	20
0.4000	60	20
0.5000	60	20
0.6000	60	20
0.7000	60	20
0.8000	60	20
0.9000	60	20
1.0000	60	20

Crack Model: Single Edge Cracked Plate

Crack Parameters:

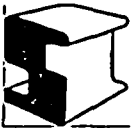
	Revision	0	1	2	
	Preparer/Date	HLG 2/17/04	HLG 5/12/04	HLG 5/15/04	
	Checker/Date	GLS 2/17/04	MQ 5/12/04	PCR 5/15/04	
	File No.	PBCH-09Q-302			Page A14 of A19

Plate width: 2.0000  
 Max. crack size: 1.0000

-----Stress Intensity Factor-----

Crack Size	Case Residual	Case Operating
0.0200	16.2806	5.42685
0.0400	23.1837	7.7279
0.0600	28.5895	9.52983
0.0800	33.2379	11.0793
0.1000	37.4133	12.4711
0.1200	41.2605	13.7535
0.1400	44.8649	14.955
0.1600	48.2816	16.0939
0.1800	51.5488	17.1829
0.2000	54.6939	18.2313
0.2200	58.4858	19.4953
0.2400	62.2586	20.7529
0.2600	66.021	22.007
0.2800	69.7794	23.2598
0.3000	73.5391	24.513
0.3200	77.3044	25.7681
0.3400	81.0788	27.0263
0.3600	84.8651	28.2884
0.3800	88.6656	29.5552
0.4000	92.4824	30.8275
0.4200	97.0061	32.3354
0.4400	101.582	33.8605
0.4600	106.209	35.4029
0.4800	110.888	36.9626
0.5000	115.618	38.5394
0.5200	120.4	40.1334
0.5400	125.234	41.7446
0.5600	130.118	43.3727
0.5800	135.054	45.0179
0.6000	140.04	46.6799
0.6200	146.332	48.7773
0.6400	152.715	50.9049
0.6600	159.186	53.0621
0.6800	165.746	55.2486
0.7000	172.392	57.464
0.7200	179.124	59.7079
0.7400	185.94	61.98
0.7600	192.84	64.2799
0.7800	199.822	66.6073
0.8000	206.886	68.9619



Revision	0	1	2	
Preparer/Date	HLG 2/17/04	HLG 5/12/04	HLG 5/15/04	
Checker/Date	GLS 2/17/04	MQ 5/12/04	PCR 5/15/04	
File No.	PBCH-09Q-302			Page A15 of A19

0.8200	216.919	72.3064
0.8400	227.102	75.7008
0.8600	237.433	79.1444
0.8800	247.91	82.6366
0.9000	258.53	86.1767
0.9200	269.292	89.7641
0.9400	280.195	93.3982
0.9600	291.235	97.0783
0.9800	302.412	100.804
1.0000	313.724	104.575

Crack Growth Laws:

Law ID: Alloy 52  
 Model: ASME Section XI - austenitic stainless steel in air environment

$$da/dN = C * 10^F * S * dK^{3.3}$$

where

$S = 1.0$  for  $R < 0$   
 $= 1.0 + 1.8 * R$  for  $0 < R < 0.79$   
 $= -43.5 + 57.97 * R$  for  $0.79 < R < 1$   
 F = code specified function of temperature  
 $dK = K_{max} - K_{min}$   
 $R = K_{min} / K_{max}$

where:

$C * 10^F = 1.9352e-010$   
 is for the currently selected units of:  
 force: kip  
 length: inch  
 temperature: 592.0000 Fahrenheit

Material Fracture Toughness K<sub>Ic</sub>:

Material ID: Alloy 52

Depth	K <sub>Ic</sub>
0.0000	200.0000
0.5000	200.0000
2.0000	200.0000

Initial crack size= 0.1000  
 Max. crack size= 1.0000



Revision	0	1	2	
Preparer/Date	HLG 2/17/04	HLG 5/12/04	HLG 5/15/04	
Checker/Date	GLS 2/17/04	MQ 5/12/04	PCR 5/15/04	
File No.	PBCH-09Q-302		Page A16 of A19	

Number of blocks= 1  
 Print increment of block= 1

Subblock	Cycles /Time	Calc. incre.	Print incre.	Crk. Law	Grw.	Mat. K1c
FCG	1000	10	10	Alloy 52		Alloy 52

Subblock	Kmax Case ID	Scale Factor	Kmin Case ID	Scale Factor
FCG	Residual	1.0000	Residual	1.0000
	Operating	1.0000		

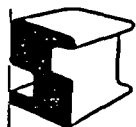
Crack growth results:

Total Subblock

Cycles Cycles DaDn  
 /Time /Time Kmax Kmin DeltaK R /DaDt Da a a/thk

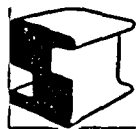
Block: 1

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20	20	4.99e+001	3.74e+001	1.25e+001	0.75	1.88e-006	1.88e-005	0.1	0.05
30	30	4.99e+001	3.74e+001	1.25e+001	0.75	1.88e-006	1.88e-005	0.1001	0.05
40	40	4.99e+001	3.74e+001	1.25e+001	0.75	1.88e-006	1.88e-005	0.1001	0.05
50	50	4.99e+001	3.74e+001	1.25e+001	0.75	1.88e-006	1.88e-005	0.1001	0.05
60	60	4.99e+001	3.74e+001	1.25e+001	0.75	1.88e-006	1.88e-005	0.1001	0.05
70	70	4.99e+001	3.74e+001	1.25e+001	0.75	1.88e-006	1.88e-005	0.1001	0.05
80	80	4.99e+001	3.74e+001	1.25e+001	0.75	1.88e-006	1.88e-005	0.1002	0.05
90	90	4.99e+001	3.74e+001	1.25e+001	0.75	1.89e-006	1.89e-005	0.1002	0.05
100	100	4.99e+001	3.74e+001	1.25e+001	0.75	1.89e-006	1.89e-005	0.1002	0.05
110	110	4.99e+001	3.74e+001	1.25e+001	0.75	1.89e-006	1.89e-005	0.1002	0.05
120	120	4.99e+001	3.75e+001	1.25e+001	0.75	1.89e-006	1.89e-005	0.1002	0.05
130	130	4.99e+001	3.75e+001	1.25e+001	0.75	1.89e-006	1.89e-005	0.1002	0.05
140	140	4.99e+001	3.75e+001	1.25e+001	0.75	1.89e-006	1.89e-005	0.1003	0.05
150	150	5.00e+001	3.75e+001	1.25e+001	0.75	1.89e-006	1.89e-005	0.1003	0.05
160	160	5.00e+001	3.75e+001	1.25e+001	0.75	1.89e-006	1.89e-005	0.1003	0.05
170	170	5.00e+001	3.75e+001	1.25e+001	0.75	1.89e-006	1.89e-005	0.1003	0.05
180	180	5.00e+001	3.75e+001	1.25e+001	0.75	1.89e-006	1.89e-005	0.1003	0.05
190	190	5.00e+001	3.75e+001	1.25e+001	0.75	1.89e-006	1.89e-005	0.1004	0.05
200	200	5.00e+001	3.75e+001	1.25e+001	0.75	1.89e-006	1.89e-005	0.1004	0.05
210	210	5.00e+001	3.75e+001	1.25e+001	0.75	1.89e-006	1.89e-005	0.1004	0.05
220	220	5.00e+001	3.75e+001	1.25e+001	0.75	1.89e-006	1.89e-005	0.1004	0.05
230	230	5.00e+001	3.75e+001	1.25e+001	0.75	1.89e-006	1.89e-005	0.1004	0.05
240	240	5.00e+001	3.75e+001	1.25e+001	0.75	1.89e-006	1.89e-005	0.1005	0.05
250	250	5.00e+001	3.75e+001	1.25e+001	0.75	1.90e-006	1.90e-005	0.1005	0.05



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260 260 5.00e+001 3.75e+001 1.25e+001 0.75 1.90e-006 1.90e-005 0.1005 0.05  
 270 270 5.00e+001 3.75e+001 1.25e+001 0.75 1.90e-006 1.90e-005 0.1005 0.05  
 280 280 5.00e+001 3.75e+001 1.25e+001 0.75 1.90e-006 1.90e-005 0.1005 0.05  
 290 290 5.00e+001 3.75e+001 1.25e+001 0.75 1.90e-006 1.90e-005 0.1005 0.05  
 300 300 5.00e+001 3.75e+001 1.25e+001 0.75 1.90e-006 1.90e-005 0.1006 0.05  
 310 310 5.00e+001 3.75e+001 1.25e+001 0.75 1.90e-006 1.90e-005 0.1006 0.05  
 320 320 5.00e+001 3.75e+001 1.25e+001 0.75 1.90e-006 1.90e-005 0.1006 0.05  
 330 330 5.00e+001 3.75e+001 1.25e+001 0.75 1.90e-006 1.90e-005 0.1006 0.05  
 340 340 5.00e+001 3.75e+001 1.25e+001 0.75 1.90e-006 1.90e-005 0.1006 0.05  
 350 350 5.00e+001 3.75e+001 1.25e+001 0.75 1.90e-006 1.90e-005 0.1007 0.05  
 360 360 5.01e+001 3.75e+001 1.25e+001 0.75 1.90e-006 1.90e-005 0.1007 0.05  
 370 370 5.01e+001 3.75e+001 1.25e+001 0.75 1.90e-006 1.90e-005 0.1007 0.05  
 380 380 5.01e+001 3.75e+001 1.25e+001 0.75 1.90e-006 1.90e-005 0.1007 0.05  
 390 390 5.01e+001 3.76e+001 1.25e+001 0.75 1.90e-006 1.90e-005 0.1007 0.05  
 400 400 5.01e+001 3.76e+001 1.25e+001 0.75 1.90e-006 1.90e-005 0.1008 0.05  
 410 410 5.01e+001 3.76e+001 1.25e+001 0.75 1.90e-006 1.90e-005 0.1008 0.05  
 420 420 5.01e+001 3.76e+001 1.25e+001 0.75 1.91e-006 1.91e-005 0.1008 0.05  
 430 430 5.01e+001 3.76e+001 1.25e+001 0.75 1.91e-006 1.91e-005 0.1008 0.05  
 440 440 5.01e+001 3.76e+001 1.25e+001 0.75 1.91e-006 1.91e-005 0.1008 0.05  
 450 450 5.01e+001 3.76e+001 1.25e+001 0.75 1.91e-006 1.91e-005 0.1009 0.05  
 460 460 5.01e+001 3.76e+001 1.25e+001 0.75 1.91e-006 1.91e-005 0.1009 0.05  
 470 470 5.01e+001 3.76e+001 1.25e+001 0.75 1.91e-006 1.91e-005 0.1009 0.05  
 480 480 5.01e+001 3.76e+001 1.25e+001 0.75 1.91e-006 1.91e-005 0.1009 0.05  
 490 490 5.01e+001 3.76e+001 1.25e+001 0.75 1.91e-006 1.91e-005 0.1009 0.05  
 500 500 5.01e+001 3.76e+001 1.25e+001 0.75 1.91e-006 1.91e-005 0.1009 0.05  
 510 510 5.01e+001 3.76e+001 1.25e+001 0.75 1.91e-006 1.91e-005 0.101 0.05  
 520 520 5.01e+001 3.76e+001 1.25e+001 0.75 1.91e-006 1.91e-005 0.101 0.05  
 530 530 5.01e+001 3.76e+001 1.25e+001 0.75 1.91e-006 1.91e-005 0.101 0.05  
 540 540 5.01e+001 3.76e+001 1.25e+001 0.75 1.91e-006 1.91e-005 0.101 0.05  
 550 550 5.01e+001 3.76e+001 1.25e+001 0.75 1.91e-006 1.91e-005 0.101 0.05  
 560 560 5.02e+001 3.76e+001 1.25e+001 0.75 1.91e-006 1.91e-005 0.1011 0.05  
 570 570 5.02e+001 3.76e+001 1.25e+001 0.75 1.91e-006 1.91e-005 0.1011 0.05  
 580 580 5.02e+001 3.76e+001 1.25e+001 0.75 1.92e-006 1.92e-005 0.1011 0.05  
 590 590 5.02e+001 3.76e+001 1.25e+001 0.75 1.92e-006 1.92e-005 0.1011 0.05  
 600 600 5.02e+001 3.76e+001 1.25e+001 0.75 1.92e-006 1.92e-005 0.1011 0.05  
 610 610 5.02e+001 3.76e+001 1.25e+001 0.75 1.92e-006 1.92e-005 0.1012 0.05  
 620 620 5.02e+001 3.76e+001 1.25e+001 0.75 1.92e-006 1.92e-005 0.1012 0.05  
 630 630 5.02e+001 3.76e+001 1.25e+001 0.75 1.92e-006 1.92e-005 0.1012 0.05  
 640 640 5.02e+001 3.76e+001 1.25e+001 0.75 1.92e-006 1.92e-005 0.1012 0.05  
 650 650 5.02e+001 3.76e+001 1.25e+001 0.75 1.92e-006 1.92e-005 0.1012 0.05  
 660 660 5.02e+001 3.77e+001 1.26e+001 0.75 1.92e-006 1.92e-005 0.1013 0.05  
 670 670 5.02e+001 3.77e+001 1.26e+001 0.75 1.92e-006 1.92e-005 0.1013 0.05  
 680 680 5.02e+001 3.77e+001 1.26e+001 0.75 1.92e-006 1.92e-005 0.1013 0.05  
 690 690 5.02e+001 3.77e+001 1.26e+001 0.75 1.92e-006 1.92e-005 0.1013 0.05  
 700 700 5.02e+001 3.77e+001 1.26e+001 0.75 1.92e-006 1.92e-005 0.1013 0.05  
 710 710 5.02e+001 3.77e+001 1.26e+001 0.75 1.92e-006 1.92e-005 0.1014 0.05  
 720 720 5.02e+001 3.77e+001 1.26e+001 0.75 1.92e-006 1.92e-005 0.1014 0.05  
 730 730 5.02e+001 3.77e+001 1.26e+001 0.75 1.92e-006 1.92e-005 0.1014 0.05  
 740 740 5.02e+001 3.77e+001 1.26e+001 0.75 1.93e-006 1.93e-005 0.1014 0.05



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750 750 5.02e+001 3.77e+001 1.26e+001 0.75 1.93e-006 1.93e-005 0.1014 0.05  
760 760 5.03e+001 3.77e+001 1.26e+001 0.75 1.93e-006 1.93e-005 0.1014 0.05  
770 770 5.03e+001 3.77e+001 1.26e+001 0.75 1.93e-006 1.93e-005 0.1015 0.05  
780 780 5.03e+001 3.77e+001 1.26e+001 0.75 1.93e-006 1.93e-005 0.1015 0.05  
790 790 5.03e+001 3.77e+001 1.26e+001 0.75 1.93e-006 1.93e-005 0.1015 0.05  
800 800 5.03e+001 3.77e+001 1.26e+001 0.75 1.93e-006 1.93e-005 0.1015 0.05  
810 810 5.03e+001 3.77e+001 1.26e+001 0.75 1.93e-006 1.93e-005 0.1015 0.05  
820 820 5.03e+001 3.77e+001 1.26e+001 0.75 1.93e-006 1.93e-005 0.1016 0.05  
830 830 5.03e+001 3.77e+001 1.26e+001 0.75 1.93e-006 1.93e-005 0.1016 0.05  
840 840 5.03e+001 3.77e+001 1.26e+001 0.75 1.93e-006 1.93e-005 0.1016 0.05  
850 850 5.03e+001 3.77e+001 1.26e+001 0.75 1.93e-006 1.93e-005 0.1016 0.05  
860 860 5.03e+001 3.77e+001 1.26e+001 0.75 1.93e-006 1.93e-005 0.1016 0.05  
870 870 5.03e+001 3.77e+001 1.26e+001 0.75 1.93e-006 1.93e-005 0.1017 0.05  
880 880 5.03e+001 3.77e+001 1.26e+001 0.75 1.93e-006 1.93e-005 0.1017 0.05  
890 890 5.03e+001 3.77e+001 1.26e+001 0.75 1.93e-006 1.93e-005 0.1017 0.05  
900 900 5.03e+001 3.77e+001 1.26e+001 0.75 1.94e-006 1.94e-005 0.1017 0.05  
910 910 5.03e+001 3.77e+001 1.26e+001 0.75 1.94e-006 1.94e-005 0.1017 0.05  
920 920 5.03e+001 3.77e+001 1.26e+001 0.75 1.94e-006 1.94e-005 0.1018 0.05  
930 930 5.03e+001 3.78e+001 1.26e+001 0.75 1.94e-006 1.94e-005 0.1018 0.05  
940 940 5.03e+001 3.78e+001 1.26e+001 0.75 1.94e-006 1.94e-005 0.1018 0.05  
950 950 5.03e+001 3.78e+001 1.26e+001 0.75 1.94e-006 1.94e-005 0.1018 0.05  
960 960 5.03e+001 3.78e+001 1.26e+001 0.75 1.94e-006 1.94e-005 0.1018 0.05  
970 970 5.04e+001 3.78e+001 1.26e+001 0.75 1.94e-006 1.94e-005 0.1019 0.05  
980 980 5.04e+001 3.78e+001 1.26e+001 0.75 1.94e-006 1.94e-005 0.1019 0.05  
990 990 5.04e+001 3.78e+001 1.26e+001 0.75 1.94e-006 1.94e-005 0.1019 0.05  
1000 1000 5.04e+001 3.78e+001 1.26e+001 0.75 1.94e-006 1.94e-005 0.1019 0.05

End of pc-CRACK Output



Revision	0	1	2	
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