

**PWR Secondary Water Chemistry Guidelines
Revision 6**

Non - Proprietary Version

Pressurized Water Reactor Secondary Water Chemistry Guidelines - Revision 6

Technical Report

Pressurized Water Reactor Secondary Water Chemistry Guidelines – Revision 6

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EPRI Project Manager
K. Fruzzetti

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ORGANIZATION(S) THAT PREPARED THIS DOCUMENT

PWR Secondary Water Chemistry Guidelines Revision 6 Committee

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CITATIONS

This report was prepared by

PWR Secondary Water Chemistry Guidelines Revision 6 Committee

AmerenUE J. Howard	Entergy B. Burke, D. Wilson	Pacific Gas & Electric J. Correa
AmerGen R. Walton	EPRI K. Fruzzetti, Chairman	Progress Energy R. Thompson
American Electric Power T. Andert, W. Hart	EPRI Consultant R. Litman	PSEG Nuclear J. Clancy, R. Dolan, S. Harvey
Arizona Public Service D. Raught	Exelon H. Hannoun, S. Kerr	Ringhals AB P.-O. Andersson
AECL C. Turner	First Energy G. Gillespie, S. Slosnerick	Rochester Gas & Electric B. Dahl, F. Mis
Babcock & Wilcox J. Jevec, J. Sarver	Florida Power & Light J. Berg, S. Jaster, R. Lieder	South Carolina Electric & Gas F. Bacon
British Energy E. Thornton	Framatome ANP W. Allmon	Southern California Edison O. Flores
COG S. McKay (OPG) M. Upton (Bruce Power)	INPO C. Halbfoster, L. Johnson C. Ware	Southern Nuclear F. Hundley
Constellation Energy J. Bills	iSagacity J. Bates, P. Millett	STPNOC S. Daniel
Dominion Engineering J. Gorman, C. Marks – Tech. Secretary & Consultant	Laborelec E. Girasa, M. De Wispelaere	Tennessee Valley Authority J. Barker, D. Bodine, M. King, R. Ritchie, K. Riggle
Dominion Resources L. Miller	Nuclear Management Company D. Schuelke, R. Slakes	TXU Electric G. Nichols, J. Stevens
Duke Energy R. Eaker, L. Wilson	NWT S. Sawochka	WCNOC D. Helm
Electricité de France F. Nordmann	Omaha Public Power District B. Shubert	Westinghouse J. Barkich

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REPORT SUMMARY

State-of-the-art water chemistry programs reduce equipment corrosion and enhance steam generator reliability. A committee of industry experts prepared these revised *PWR Secondary Water Chemistry Guidelines* to incorporate the latest field and laboratory data on secondary system corrosion and performance issues. PWR operators can use these guidelines to update their secondary water chemistry programs.

Background

EPRI updates industry water chemistry guidelines periodically as new information becomes available. Previous versions of these *PWR Secondary Water Chemistry Guidelines* identified a detailed water chemistry program deemed consistent with the then-current understanding of research and field information. Each revision discussed the impact of these guidelines on plant operation, noting that utilities may wish to revise the presented program following a plant-specific evaluation for implementation. Utility feedback since publication of Revision 5 in May 2000 revealed that some utility chemistry personnel required further details regarding how to best integrate these guidelines into plant-specific optimization process while still ensuring compliance with NEI 97-06 and NEI 03-08.

Objective

To update the *PWR Secondary Water Chemistry Guidelines—Revision 5*.

Approach

A committee of industry experts, including utility specialists, nuclear steam supply system vendor representatives, Institute of Nuclear Power Operations representatives, consultants, and EPRI staff, collaborated to review the available data on secondary water chemistry and secondary cycle corrosion. From these data, the committee generated water chemistry guidelines that utilities should adopt at all PWR nuclear plants. Recognizing that each nuclear plant owner has a unique set of design, operating, and corporate concerns, the guidelines committee developed a methodology for plant-specific optimization.

Results

Revision 6 of the *PWR Secondary Water Chemistry Guidelines* provides recommendations for PWR secondary systems of all manufacture and design, and includes the following chapters:

- Chapter 1 contains a list of management responsibilities and addresses secondary water chemistry program requirements for compliance with NEI 97-06 (SG Program Guidelines). It also identifies the parts of these Guidelines that are mandatory, “shall” requirements, and recommendations, consistent with NEI 03-08.

- Chapter 2 presents a compilation of corrosion data for steam generator tubing and, to a lesser extent, balance-of-plant materials. This information serves as the technical basis for the specific parameters and programs detailed in the document.
- Chapter 3 discusses the role of the concentration processes in local regions of the steam generator and the chemistry programs available for minimizing the impact of impurity concentration. It briefly identifies the supporting aspects and considerations in adopting these chemistry regimes.
- Chapter 4 presents a detailed method for performing plant-specific optimization, including development of a modified chemistry program.
- Chapters 5 and 6 present water chemistry programs for the recirculating steam generator (RSG) and once-through steam generator (OTSG). These are the chapters most frequently referred to by chemistry personnel. The tables in these chapters provide the boundaries for the plant-specific optimization procedures described in Chapter 4.
- Chapter 7 provides information on data collection, evaluation, and management. This chapter describes methods of using EPRI chemWORKS™ modules for evaluating plant data and predicting high-temperature chemistry environments throughout the cycle.
- Appendix A provides examples of methodologies for implementing integrated exposure programs.
- Appendix B provides the results of a recent review of PWR steam chemistry considerations.

EPRI Perspective

This sixth revision of the *PWR Secondary Water Chemistry Guidelines*, endorsed by the utility executives of the EPRI Steam Generator Management Program, represents another step in maintaining proactive chemistry programs to limit or control steam generator degradation, with consideration given to corporate resources and plant-specific design/operating concerns. Each utility should examine its plant-specific situation to determine which recommendations to implement.

Keywords

PWR

Water chemistry

Corrosion protection

Nuclear steam generators

Secondary coolant circuits

EPRI FORWARD

Industry water chemistry guidelines are updated periodically as new information becomes available. Previous revisions of these guidelines have identified a detailed water chemistry program that was deemed to be consistent with the then current understanding of research and field information. Each revision, however, has recognized the impact of these *Guidelines* on plant operation and has noted that utilities should optimize their program based on a plant-specific evaluation prior to implementation. To assist in such plant-specific evaluations, Revisions 4 and 5, issued in 1996 and 2000, respectively, provided an increased depth of detail regarding the corrosion mechanisms affecting steam generators and the balance of plant, and provided additional guidance on how to integrate these and other concerns into the plant-specific optimization process. Revision 6 retains the format of Revisions 4 and 5, and adds to the detailed information contained in these revisions. The chapters of Revision 6 cover the following:

- Chapter 1 identifies Management Responsibilities. It also describes which elements of the *Guidelines* are mandatory and “shall” requirements under NEI 03-08, Guideline for the Management of Materials Issues, (consistent with NEI 97-06) and which are recommendations.
- Chapter 2 presents a compilation of corrosion data for steam generator tubing and, to a lesser extent, balance-of-plant materials. It is not intended to relate operational bulk water chemistry to the corrosion phenomena, which is covered in Chapter 3. The corrosion data presented in Chapter 2 serve as the technical bases for each of the specific parameters and programs detailed in the balance of the document.
- Chapter 3 discusses the role of the concentration processes in the various locations of the steam generator and the chemistry “tools” available for modifying the resulting chemistry within these concentrating regions. It briefly identifies the supporting aspects of and the considerations for adopting these chemistry regimes. It refers the reader to more detailed documents for application of the chemistry strategies.
- Chapter 4 presents a detailed methodology for performing the plant-specific optimization that can be used to develop a modified chemistry program that satisfies site-specific concerns. Chapter 4 also presents example startup and operating chemistry parameters and limits that can be used as a starting point for site-specific evaluations.
- Chapters 5 and 6 present water chemistry programs for RSGs and OTSGs, respectively. These are the chapters most frequently referred to by chemistry personnel. The tables contained within these chapters provide boundaries of the envelope within which plant-specific optimization should occur.
- Chapter 7 provides information on data collection, evaluation, and management. This chapter covers use of EPRI chemWORKS™ modules for evaluating plant data and predicting high-temperature chemistry environments throughout the cycle.

-
- Appendix A provides detailed guidance with regard to use of the integrated exposure concept.
 - Appendix B provides a review of PWR steam chemistry considerations.

These *Guidelines* were produced by the Committee with support from an industry Technical Review Team and the technical committees of the Steam Generator Management Program. Key technical changes in this revision include:

Keith Fruzzetti
Chairman

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Don Adams	Tennessee Valley Authority
Chip Bach	Progress Energy
Johnny Barker	Tennessee Valley Authority
Stephen Barshay	Westinghouse
Alan Beebe	Omaha Public Power District
Mohamad Behraves	EPRI
Johan Blok	EPRI
Dennis Bostic	Dominion Resources
Michael Brett	COG (Ontario Power Generation)
Guy Bucci	Arizona Public Service
Dudley Carter	Southern Nuclear
Martin Cubitt	British Energy Generation
Robert Cullen	Entergy North
Nikki Delse	EPRI
Dave Evans	COG (Ontario Power Generation)
Lou Faltus	South Carolina Electric & Gas
Elio Fracalanza	COG (Ontario Power Generation)
Paul Frattini	EPRI
Ed Frese	Dominion Resources
Jeff Gardner	Pacific Gas & Electric
Gail Gary	AmerenUE
Tina Gaudreau	EPRI
Jeff Goldstein	Entergy
Dave Goode	COG (Ontario Power Generation)

Norma Gordon	Exelon
Jeff Heinold	Florida Power & Light
Rusty Hitch	Progress Energy
Peter King	Babcock & Wilcox Canada
Larry Lamanna	Framatome ANP
Victor Linnenbom, Jr.	First Energy
Tony Livingston	Southern Nuclear Operating Company
Joel McElrath	Nuclear Management Company
Al McIlree	EPRI
Brian Mervak	South Carolina Electric & Gas
Colin Morano	COG/Bruce Power
Curt Palmer	Wolf Creek Nuclear Operating Company
Mickey Perry	Southern Nuclear Operating Company
Frank Puzzuoli	COG/Ontario Power Generation
Graham Quirk	British Energy Generation
Robbe Robinson	Dominion Resources
John Rotchford, Jr.	Dominion Resources
Jerry Seager	Florida Power Corporation
Gary L. Ward	Duke Energy
Chris Wood	EPRI

CONTENTS

1 INTRODUCTION AND MANAGEMENT RESPONSIBILITIES	1-1
1.1 Introduction and Objectives.....	1-1
1.2 Water Chemistry Management Philosophy	1-2
1.3 Generic Management Considerations.....	1-3
1.3.1 Policies	1-3
1.4 Training and Qualification.....	1-5
1.5 Summary.....	1-5
1.6 References	1-6
 2 TECHNICAL BASIS FOR WATER CHEMISTRY CONTROL.....	2-1
2.1 Summary.....	2-1
2.2 Introduction	2-2
2.3 Corrosion of Steam Generator Tubing Alloys – Scientific Aspects	2-2
2.3.1 Role of Protective Oxide Films	2-3
2.3.2 Potential – pH (Pourbaix) Diagrams	2-3
2.3.3 Effects of Potential on Corrosion, and Protectiveness of Oxide Films	2-7
2.3.4 Effects of Specific Species	2-11
2.3.4.1 Known Deleterious Species.....	2-12
2.3.4.2 Possibly Deleterious Species.....	2-15
2.3.4.3 Possibly Beneficial Species	2-16
2.3.5 Modes of Corrosion Affecting Alloys 600, 800 and 690.....	2-16
2.3.6 SCC and IGA Growth Rates.....	2-19
2.4 Corrosion of Tubing Alloys – Engineering Aspects	2-21
2.4.1 Susceptibility in a Variety of Possible Environments	2-22
2.4.2 Effects of Material Condition and Type on Susceptibility to Corrosion	2-23
2.4.3 Elevated (Anodic or Oxidizing) Electrochemical Potentials	2-25
2.4.4 Depressed (Cathodic) Electrochemical Potentials	2-27
2.4.5 High Temperature, High Stress, and Local Cold Work.....	2-28

2.4.6 Denting	2-28
2.4.7 Effects of Lead.....	2-30
2.4.8 Pitting.....	2-30
2.4.9 Contaminated Steam and Internal Oxidation.....	2-31
2.4.10 Thermal Performance Issues	2-32
2.4.11 Considerations Regarding Use of Inhibitors	2-36
2.4.12 Considerations Regarding Wet Layup of Steam Generators	2-38
2.5 Balance of Plant Considerations	2-40
2.5.1 General Corrosion and Flow-Accelerated Corrosion (FAC) of Piping and Components, Including Steam Generators	2-40
2.5.2 BOP Layup Considerations	2-48
2.5.3 Startup and Cleanup Considerations.....	2-48
2.5.4 Turbines.....	2-48
2.5.5 Secondary System Heat Exchangers.....	2-49
2.6 Once-Through Steam Generators (OTSGs)	2-49
2.7 References.....	2-50
3 WATER CHEMISTRY CONTROL STRATEGIES.....	3-1
3.1 Introduction	3-1
3.2 Role of Concentration Processes.....	3-1
3.2.1 Concentration on Clean Tube Surfaces and Shallow Tube Scales.....	3-2
3.2.2 Concentration in Flow-Occluded Regions of RSGs.....	3-4
3.2.3 Conclusions	3-10
3.3 pH and ORP Optimization to Minimize Iron Transport	3-10
3.3.1 pH Control	3-11
3.3.1.1 Supporting Aspects of Alternate Amine Treatment.....	3-11
3.3.1.2 Considerations for Implementing Advanced Amine Treatment.....	3-11
3.3.2 Targeted pH Control by Tailored Injection of Amines	3-12
3.3.3 ORP Control	3-12
3.4 Control or Adjusting Water Chemistry or Power Level to Minimize the Formation of Aggressive Water Chemistry Environments in Flow-Occluded Regions.....	3-13
3.4.1 ALARA Chemistry.....	3-13
3.4.2 Molar Ratio Control (For Recirculating Steam Generators).....	3-14
3.4.2.1 Supporting Aspects of Molar Ratio Control.....	3-14
3.4.2.2 Considerations for Implementing Molar Ratio Control	3-15

3.4.3 Low Power Soaks.....	3-15
3.4.3.1 Supporting Aspects of Low Power Soaks	3-16
3.4.3.2 Considerations for Implementing Low Power Soaks	3-16
3.5 Controlling the ECP in Localized Regions of the Steam Generator	3-16
3.5.1 Elevated Hydrazine Operation.....	3-16
3.5.1.1 Supporting Aspects of Elevated Hydrazine.....	3-18
3.5.1.2 Considerations for Implementing Elevated Hydrazine Chemistry.....	3-18
3.5.2 Effects of Interruptions in Hydrazine Addition.....	3-19
3.5.3 Startup Oxidant Control	3-20
3.6 Minimizing Other Corrosion Accelerants	3-20
3.6.1 Lead.....	3-20
3.6.1.1 Supporting Aspects of Lead Minimization.....	3-20
3.6.1.2 Considerations for Lead Minimization.....	3-21
3.6.2 Copper.....	3-21
3.6.2.1 Supporting Aspects of Copper Minimization	3-21
3.6.2.2 Considerations for Copper Minimization	3-21
3.7 Adding Chemicals to Inhibit Corrosion	3-22
3.7.1 Boric Acid Treatment	3-22
3.7.1.1 Plant Trip with Recovery of Power – No Cooldown	3-23
3.7.1.2 Plant Trip, Hot Standby Maintained for More than Two Days.....	3-23
3.7.1.3 Heatup with High Boric Acid for Chemically Cleaned Steam Generators.....	3-23
3.7.1.4 Supporting Aspects of BAT	3-23
3.7.1.5 Considerations for Implementing BAT	3-24
3.7.2 Use of Corrosion Inhibitors	3-24
3.7.2.1 Supporting Aspects of Chemical Inhibitors	3-25
3.7.2.2 Considerations for Using Chemical Inhibitors	3-25
3.8 Management of Steam Generator Deposits.....	3-25
3.8.1 Chemical Cleaning	3-26
3.8.1.1 Supporting Aspects of Chemical Cleaning.....	3-27
3.8.1.2 Considerations for Chemical Cleaning.....	3-27
3.8.2 Top of Tubesheet Sludge Removal	3-28
3.8.2.1 Supporting Aspects of Top of Tubesheet Sludge Removal	3-28
3.8.2.2 Considerations for Top of Tubesheet Sludge Removal	3-28
3.8.2.3 Sludge Lancing.....	3-28

3.8.2.4 In-bundle Sludge Lancing	3-29
3.8.2.5 Ultrasonic Energy Cleaning	3-29
3.8.3 Tube Bundle Sludge Removal Technologies	3-29
3.8.3.1 High Volume Bundle Flushing.....	3-29
3.8.3.2 Upper Bundle Hydraulic Cleaning.....	3-30
3.8.3.3 Scale Conditioning Agents.....	3-30
3.9 References	3-30
4 METHODOLOGY FOR PLANT-SPECIFIC OPTIMIZATION	4-1
4.1 Introduction	4-1
4.2 Definition of Component/System Conditions and Design Features	4-2
4.2.1 Summary of Approach.....	4-2
4.2.2 Component Susceptibility	4-3
4.2.3 Component Reliability.....	4-3
4.3 Prioritization of Components/Systems	4-4
4.4 Selection of Chemistry Control Programs	4-5
4.4.1 General Considerations.....	4-5
4.4.2 ALARA Chemistry.....	4-6
4.4.3 Molar Ratio Control (RSGs).....	4-7
4.4.4 Integrated Exposure (RSGs)	4-7
4.4.5 Boric Acid Treatment and Injection of Corrosion Inhibitors	4-9
4.4.6 Minimization of Steam Generator Oxidant Exposure	4-9
4.4.6.1 Elevated Hydrazine.....	4-9
4.4.6.2 Limiting Exposure to Startup Oxidants.....	4-11
4.4.7 Secondary System pH Control	4-11
4.4.8 Steam Generator Deposit Management.....	4-12
4.4.9 NEI Commitments Regarding Chemistry Control – Strategic Water Chemistry Control Plan.....	4-12
4.4.10 Documenting Exceptions to Diagnostic Parameters	4-13
4.5 Final Optimization of Secondary Chemistry Program	4-15
4.6 References	4-18
5 WATER CHEMISTRY GUIDELINES RECIRCULATING STEAM GENERATORS	5-1
5.1 Introduction	5-1
5.2 Control and Diagnostic Parameters	5-2

5.3 Action Levels	5-3
5.3.1 Action Level 1	5-3
5.3.2 Action Level 2	5-4
5.3.3 Action Level 3	5-4
5.4 Corrective Actions	5-5
5.5 Specific Guidelines and Technical Justifications	5-5
5.5.1 Cold Shutdown/Wet Layup	5-5
5.5.1.1 Guidelines	5-5
5.5.1.2 Discussion	5-5
5.5.1.3 Justification for Parameters and Values	5-7
5.5.1.3.1 Steam Generator	5-7
5.5.1.3.2 Fill Source/Steam Generator	5-8
5.5.1.4 Corrective Action Guidelines	5-8
5.5.2 Heatup/Hot Shutdown (RCS >200°F, <30% Reactor Power)	5-9
5.5.2.1 Guidelines	5-9
5.5.2.2 Discussion	5-9
5.5.2.3 Justification for Parameters and Values	5-12
5.5.2.4 Corrective Action Guidelines – Heatup	5-13
5.5.3 Power Operation	5-14
5.5.3.1 Guidelines	5-14
5.5.3.2 Discussion	5-14
5.5.3.3 Justification for Parameters and Values	5-17
5.5.3.4 Corrective Action Guidelines – Power Operation	5-20
5.6 References	5-21
6 WATER CHEMISTRY GUIDELINES ONCE-THROUGH STEAM GENERATORS	6-1
6.1 Introduction	6-1
6.2 Control and Diagnostic Parameters	6-2
6.3 Action Responses	6-3
6.3.1 Action Level 1	6-3
6.3.2 Action Level 2	6-3

6.3.3 Action Level 3	6-4
6.4 Status Modes	6-4
6.5 Guidelines	6-5
6.5.1 Cooldown/Hot Soaks	6-5
6.5.2 Cold Shutdown/Wet Layup	6-6
6.5.2.1 Guidelines/Technical Justifications	6-6
6.5.2.2 Parameter Justifications.....	6-8
6.5.2.3 Corrective Actions.....	6-9
6.5.3 Startup, Hot Standby, and Reactor Critical at <15% Reactor Power (RCS >200°F, <15% Reactor Power) – Modes 1, 2, 3 and 4 of STS.....	6-9
6.5.3.1 Guidelines/Technical Justifications	6-9
6.5.3.2 Parameter Justifications.....	6-11
6.5.3.2.1 Feedwater	6-11
6.5.3.2.2 Steam Generator Bulk Water	6-12
6.5.3.3 Corrective Actions.....	6-13
6.5.4 Power Operation (≥15% Reactor Power)	6-14
6.5.4.1 Guidelines/Technical Justifications	6-14
6.5.4.2 Parameter Justifications.....	6-16
6.5.4.3 Corrective Action Guidelines – Power Operation.....	6-19
6.6 References	6-20
7 DATA: COLLECTION, EVALUATION, AND MANAGEMENT	7-1
7.1 Introduction	7-1
7.2 QA/QC Considerations.....	7-3
7.2.1 Basis for Generating Chemistry Data of Known Quality	7-3
7.2.2 Data Management	7-3
7.2.3 QC Considerations for Secondary Chemistry Control	7-3
7.3 Sampling Considerations	7-4
7.3.1 General Considerations.....	7-4
7.3.2 Special Sampling Considerations.....	7-6
7.3.3 Sampling for Lead	7-10
7.4 Data Collection.....	7-10
7.5 Data Evaluation Tools	7-10

7.5.1 Introduction.....	7-10
7.5.2 EPRI chemWORKS™ Software	7-11
7.5.3 Calculated Cation Conductivity.....	7-13
7.5.4 Steam Generator Corrosion Evaluations	7-15
7.5.4.1 Source Term Evaluation	7-16
7.5.4.2 Source Term Contribution from Total Organic Carbon	7-17
7.5.4.3 Integrated Exposure Evaluation (for Recirculating Steam Generators)	7-20
7.5.4.3.1 Integrated Exposure Method A: (ppb*days)	7-20
7.5.4.3.2 Integrated Exposure Method B: Tube Exposure Factor	7-23
7.5.4.3.3 Integrated Exposure Method C: CREV-SIM.....	7-29
7.5.4.4 Hideout Return Evaluations	7-29
7.5.4.5 Deposit Chemistry Evaluation.....	7-30
7.5.4.6 Sludge Analysis and Monitoring.....	7-30
7.6 Balance of Plant Corrosion Concerns	7-32
7.6.1 pH Control and Corrosion Product Transport	7-32
7.6.2 Integrated Corrosion Product Loading.....	7-33
7.7 Technical Assessments.....	7-34
7.7.1 Contaminant Ingress Control (Ionic Contaminants).....	7-35
7.7.2 Contaminant Ingress Monitoring (Oxidants)	7-35
7.7.3 Corrosion Product Transport	7-35
7.7.4 Steam Generator Corrosion	7-35
7.7.5 System/Component Observations.....	7-35
7.7.6 Demineralizer/Filter Performance	7-36
7.7.7 Process Instrument Performance and Reliability.....	7-36
7.7.8 Hideout Return	7-36
7.8 References	7-36
A INTEGRATED EXPOSURE EVALUATIONS	A-1
A.1 Introduction	A-1
A.2 Integrated Exposure Example 1.....	A-1
A.2.1 PWR Secondary Chemistry Operating Guideline	A-1
A.2.1.1 Introduction.....	A-1
A.2.1.2 Purpose	A-1
A.2.1.3 Operating Philosophy	A-2
A.2.1.4 Basis.....	A-3

A.2.1.5 Operating Methodology	A-5
A.3 Integrated Exposure Example 2.....	A-7
A.3.1 Utilization of Integrated Exposure Limits to Control Molar Ratio	A-7
A.4 Integrated Exposure Example 3.....	A-8
A.5 References.....	A-9
B PWR STEAM CHEMISTRY CONSIDERATIONS.....	B-1
B.1 Introduction	B-1
B.2 PWR Steam Chemistry Considerations -	B-1
B.2.1 Introduction to Paper.....	B-1
B.2.2 Recommendations	B-2
B.2.3 Discussion.....	B-2
B.2.4 Deposition Processes in Turbines.....	B-3
B.2.5 Steam Chemistry Guidelines.....	B-5
B.2.5.1 Acceptability of this Approach to Setting PWR Guidelines.....	B-6
B.2.5.2 Alternative Approach	B-6
B.3 References.....	B-7

LIST OF FIGURES

Figure 2-1 Potential – pH (Pourbaix) Diagram for Nickel-Water System at 288°C (Dissolved Species Activities of 10^{-3}) [2].....	2-4
Figure 2-2 Potential – pH (Pourbaix) Diagram for Chromium-Water System at 288°C (Dissolved Species Activities of 10^{-3}) [2].....	2-5
Figure 2-3 Potential – pH (Pourbaix) Diagram for Iron-Water System at 288°C (Dissolved Species Activities of 10^{-3}) [2]	2-6
Figure 2-4 Schematic Diagram of an Anodic Polarization Curve of an Active/Passive Alloy (Adapted from Figure 10-16 in [6])	2-7
Figure 2-5 Polarization Curve for Alloy 600 in Caustic at 300°C (Adapted from [7])	2-8
Figure 2-6 Polarization Curve for 600MA and 600SR in Complex Acid Environment [7].....	2-9
Figure 2-7 Polarization and Pitting Behavior of Alloy 800NG in Acid Chlorides [8].....	2-10
Figure 2-8 Polarization Curve for Alloy 600MA in Near Neutral Concentrated Sodium Chloride [7].....	2-11
Figure 2-9 Cracking Time in Sodium Tetrathionate for Alloy 600 C-Rings with Two Different Heat Treatments [16].....	2-14
Figure 2-10 Alloy 600 Corrosion Mode Diagram (T–300°C) (Adapted from Staehle, [48]).....	2-17
Figure 2-11 Corrosion Mode Diagram for Alloys 600MA, 600TT and 690TT (Based on CERT Tests at 300°C) (from [56])	2-19
Figure 2-12 IGA Growth Rate vs. pH at 315°C for 600MA (Adapted from [64])	2-20
Figure 2-13 SCC Growth Rate vs. pH at 315°C for 600MA (Adapted from [64])	2-21
Figure 2-14 Re-Creation of Berge/Donati Summary Curve for SCC in Deaerated NaOH at 350°C with C-Rings Stressed to About Yield [83]	2-24
Figure 2-15 Relationship between Inside and Outside of Crevice Compared with Open Circuit Conditions for Crevices which are Alkaline or Acid [91].....	2-25
Figure 2-16 Maximum Crack Depth vs. Specimen Potential for 600MA and 600TT Exposed to 10% NaOH at 315°C (Adapted from 92)	2-26
Figure 2-17 Corrosion Potentials of Type 304 Stainless Steel as a Function of Hydrazine Concentration at 100, 200, 250 and 288°C in High Purity Water [97].....	2-28
Figure 2-18 The Influence of pH and Electrode Potential on the Radius Change of Carbon Steel and Type 405 Stainless Steel at 280°C [101]	2-29
Figure 2-19 Steam Pressure Deviation from Design	2-33
Figure 2-20 Scale Thickness as a Function of Operating Time [120]	2-34
Figure 2-21 Equilibrium Corrosion Product Release Rate from Alloy 706 (90/10 Copper Nickel) [151]	2-41

Figure 2-22 Effect of pH on Iron Concentration at the Economizer Inlet [154]	2-42
Figure 2-23 Relative FAC Rate (Ratio to FAC Rate without Hydrazine and Oxygen) Measured in a Single-Phase Flow at 180°C and 235°C Using Ammonia ($\text{pH}_{25^\circ\text{C}}=9.0$) with Different Amounts of Hydrazine and Oxygen [159].....	2-46
Figure 2-24 Relative FAC Rate of a Carbon Steel with 0.009% Cr as a Function of Hydrazine Concentration in Water Conditioned with NH_3 , $\text{pH}_{25^\circ\text{C}}$ of 9, Test Temperature of 235° C [172].....	2-46
Figure 2-25 Relative FAC Rate (Ratio to FAC Rate without Hydrazine and Oxygen) versus Hydrazine Concentration for Tubular Carbon Steel Specimens (0.009% Cr) Exposed to a Single-Phase Flow at 180°C Using Ammonia ($\text{pH}_{25^\circ\text{C}}=9.0$) and With Oxygen Maintained Less Than or Equal to 0.5 ppb [159]	2-47
Figure 3-1 Concentration Factors vs. Heat Flux for 1 mil Deposit [2]	3-2
Figure 3-2 Schematic of a Kinetically-Limited Concentration Process [4].....	3-3
Figure 3-3 Crevice pH as a Function of Concentration Factor (MULTEQ Options: Static, Precipitates Retained, Vapor Removed).....	3-4
Figure 3-4 Crevice pH as a Function of Concentration Factor for $\text{Na} = 3 \times \text{Cl}$ (MULTEQ Options: Static, Precipitates Retained)	3-5
Figure 3-5 Crevice pH as a Function of Concentration Factor for $\text{Na} = \text{Cl}$ (MULTEQ Options: Static, Precipitates Retained)	3-6
Figure 3-6 Crevice pH as a Function of Concentration Factor for $\text{Cl} = 3 \times \text{Na}$ (MULTEQ Options: Static, Precipitates Retained)	3-6
Figure 3-7 Crevice pH as a Function of Concentration Factor for Sulfate Solutions (MULTEQ Options: Static, Precipitates Retained, Vapor Removed)	3-7
Figure 3-8 Conceptual Design of Heated Crevice Device Showing the Autoclave Heated Tube and Simulated Support Plate [7]	3-8
Figure 3-9 Amount of Accumulated Sodium as a Function of Exposure to Sodium in the Feedwater [6]	3-9
Figure 3-10 Feedwater and Steam Generator ECP Measurements as a Function of FW Hydrazine (ppb)/CPD O_2 (ppb) [23]	3-17
Figure 3-11 Percent of Iron as Magnetite in Steam Generator Blowdown as a Function of FW Hydrazine (ppb)/CPD O_2 (ppb) [23]	3-17
Figure 4-1 Feedwater Mossbauer Results at Plant X (Blowdown Data Shown as Solid Circles)	4-10
Figure 7-1 Example of Feedwater Sample Line Configuration for Oxygen Sampling.....	7-7
Figure 7-2 Example of Feedwater Sample Line Configuration for Metal Oxide Sampling.....	7-7
Figure 7-3 Suggested Feedwater Sample Line Configuration for Oxygen and Metal Oxide Sampling.....	7-8
Figure 7-4 Example of a Sample Tee Configuration.....	7-8
Figure 7-5 Spreadsheet Used to Calculate IE by Simple Integration Method.....	7-21
Figure 7-6 Sample Sodium IE Calculation for Plant with High Impurity Exposures During Startup.....	7-22
Figure 7-7 Plant Exposure at Normal Operation vs. Reference Plant Exposure	7-23

Figure 7-8 Three Cases with Similar Cumulative Mass Accumulation Over the Cycle Length	7-24
Figure 7-9 Relative Tube Surface Area Wetted for Three Different Cases where Cumulative Mass Accumulation at the End of the Cycle is the Same.....	7-24
Figure 7-10 Drilled Hole Crevice Geometry	7-25
Figure 7-11 Relationship between Surface Area Wetted vs. Volume Filled for an Eccentric Crevice	7-26
Figure 7-12 Relative Tube Exposure Factor Illustrating Differences in Exposure for Cases where Total Cumulative Mass Accumulation Over the Cycle Length is the Same	7-27
Figure 7-13 Sample Spreadsheet Used to Calculate Tube Exposure Factors	7-27
Figure 7-14 Example Relative Tube Exposure Factor for an Actual Operating Cycle Showing the Effect of the Startup Transient.....	7-28
Figure B-1 Location of Salt Concentration in LP Turbines	B-4
Figure B-2 Steam Expansion Path for Fossil and Nuclear Steam Cycles	B-7

LIST OF TABLES

Table 2-1 Relative Corrosion Behavior* of Alloys 600, 690, 800, and Stainless Steel [66]	2-13
Table 2-2 Stress Corrosion Cracking Results for C-Rings in 50% Caustic Solutions at 320°C. The Reference Environment is 50% NaOH + 1% Na ₂ CO ₃ . Exposure Times Were 2 Days in the Reference Solution and with the Boric Acid Additive; All Others Were 1 Week [41]	2-38
Table 3-1 Chemistry Input for Determining Effects of Localized Concentration.....	3-4
Table 4-1 Corrosion Susceptibility of Major Components/Systems	4-4
Table 4-2 Component/System Reliability	4-4
Table 4-3 Relative Impact of Components/Systems on Establishing an Optimized Chemistry Program	4-5
Table 4-4 Examples of Secondary Chemistry Initiative Evaluations	4-14
Table 4-5 Flowchart for Site-Specific Chemistry Optimization	4-16
Table 4-6 Examples of Plant Specific Chemistry Targets for RSGs	4-18
Table 4-7 Examples of Plant Specific Feedwater Chemistry Target Values for OTSG Plants (Power Operation)	4-18
Table 5-1 Full Wet Layup (RCS ≤200°F) Steam Generator Sample	5-6
Table 5-2 Recirculating Steam Generator Heatup/Hot Shutdown and Startup (RCS >200°F to <30% Reactor Power) Feedwater Sample (from Steam Generator Feed Source).....	5-10
Table 5-3 Recirculating Steam Generator Heatup/Hot Shutdown and Startup (RCS >200°F to <30% Reactor Power) Blowdown Sample.....	5-11
Table 5-4 Recirculating Steam Generator Power Operation (≥30% Reactor Power) Feedwater Sample	5-15
Table 5-5 Recirculating Steam Generator Power Operation (≥30% Reactor Power) Blowdown Sample.....	5-16
Table 5-6 Power Operation (>5% Reactor Power) Condensate Sample	5-16
Table 6-1 Full Wet Layup (RCS ≤200°F) (Technical Specification Modes 5 and 6) Steam Generator Sample	6-7
Table 6-2 Once-Through Steam Generator Fill Water	6-8
Table 6-3 Once-Through Steam Generator Startup/Hot Standby/Reactor Critical at <15% Reactor Power (Technical Specification Modes 1, 2, 3 and 4) Feedwater Sample	6-10
Table 6-4 Once-Through Steam Generator Startup/Hot Standby/Reactor Critical at <15% Reactor Power (Technical Specification Modes 1, 2 and 3 and Mode 4 During Startup) Blowdown Sample*	6-11

Table 6-5 Once-Through Steam Generator Power Operation ($\geq 15\%$ Reactor Power)	
Feedwater Sample	6-15
Table 6-6 Once-Through Steam Generator Power Operation ($> 15\%$ Reactor Power)	
Condensate Sample	6-16
Table 6-7 Once-Through Steam Generator Power Operation ($> 15\%$ Reactor Power)	
Mode 1 of Standard Technical Specifications Moisture Separator Drain Sample	6-16
Table 7-1 Continuous Instrumentation Suggestions for Recirculating Steam Generators	7-2
Table 7-2 Continuous Instrumentation Suggestions for Once-Through Steam Generators	7-2
Table 7-3 Example Calculation of Oxygen Reduction in a Feedwater Sample Line	7-9
Table 7-4 Equivalent Conductivities for Some Ions: [Ref MULTEQ Database]	7-15
Table 7-5 Typical Source and Removal Terms in PWR Secondary Systems	7-16
Table 7-6 Source and Removal Term Percentages	7-17
Table 7-7 pH Control Program Data Trends	7-32
Table 7-8 Example Calculation for Iron and Copper Transport	7-33
Table 7-9 Example Data on Steam Generator Deposit Loading	7-34
Table B-1 Reheat Steam Limits in Drum Units	B-5

1

INTRODUCTION AND MANAGEMENT RESPONSIBILITIES

1.1 Introduction and Objectives

The objective of this document is to provide guidance on determining and implementing a set of plant-specific water chemistry requirements for the secondary cycle of PWRs. Accordingly, this document presents the corrosion data that provide the technical bases for water chemistry control (Chapter 2), the various water chemistry control strategies that are available (Chapter 3), a recommended methodology for plant-specific optimization (Chapter 4), generic water chemistry guidelines for RSGs and OTSGs (Chapters 5 and 6, respectively), and suggested data collection, evaluation, and management techniques (Chapter 7).

In addition, the U.S. nuclear power industry established a framework for increasing the reliability of steam generators by adopting NEI 97-06, *Steam Generator Program Guidelines* [1, 2]. This initiative references EPRI's Water Chemistry Guidelines, including this document, as the basis for an industry consensus approach to chemistry programs. Specifically, the initiative requires that U.S. utilities meet the intent of the *EPRI PWR Secondary Water Chemistry Guidelines*. The focus of the NEI initiative is steam generator integrity. These *Guidelines* are a support document under NEI 97-06. These *Guidelines* include control parameters and monitoring requirements which must be incorporated into a plant's water chemistry program in order to meet the intent of these *Guidelines*.

1.2 Water Chemistry Management Philosophy

1.3 Generic Management Considerations

This section lists and discusses the considerations which are common to most utilities, including the elements of organizations which are needed to carry out the water chemistry program effectively. Actions are identified without specifying responsibility for completing them. Utility-specific implementation policies and procedures should assign the responsibilities to specific positions within the organization. One major element of these *Guidelines* is the need for every level of management to understand the importance of the action levels presented in Chapters 5 and 6 and their potential impact on, and benefits to, the utility company. In addition, there is a need for management to support a data collection, evaluation, and management system similar to the approach discussed in Chapter 7.

1.3.1 Policies

Introduction and Management Responsibilities

1.4 Training and Qualification

1.5 Summary

1.6 References

2

TECHNICAL BASIS FOR WATER CHEMISTRY CONTROL

2.1 Summary

Corrosion of steam generator tubes has been the major issue affecting selection of secondary water chemistry parameters. However, corrosion and flow-accelerated corrosion (FAC) of steam generator internals and other secondary system components are also important concerns. The objective of this chapter is to review the causes of this corrosion and FAC and to provide the technical bases for measures to control these concerns.

2.2 Introduction

This chapter of the secondary water chemistry guidelines discusses corrosion issues affecting PWR steam generators and balance of plant components, with the objective of providing bases for selecting secondary water chemistry parameters that minimize problems due to corrosion.

The objective of secondary side water chemistry control is to minimize corrosion damage and performance losses for all secondary system components and to thereby maximize the reliability and economic performance of the secondary system. To achieve this objective, the water chemistry has to be compatible with all parts of the system including steam generators, turbines, condensers, feedwater heaters, moisture separator reheaters (MSRs), and piping. The variety of materials used in the many components in typical secondary systems, and the range of temperatures, pressures, phases, and velocities place constraints on the selection of water chemistries for secondary systems.

2.3 Corrosion of Steam Generator Tubing Alloys – Scientific Aspects

2.3.1 Role of Protective Oxide Films

2.3.2 Potential – pH (Pourbaix) Diagrams

Figure 2-1
Potential – pH (Pourbaix) Diagram for Nickel-Water System at 288°C
(Dissolved Species Activities of 10^{-3}) [2]

Figure 2-2
Potential – pH (Pourbaix) Diagram for Chromium-Water System at 288°C
(Dissolved Species Activities of 10^{-3}) [2]

Figure 2-3
Potential – pH (Pourbaix) Diagram for Iron-Water System at 288°C
(Dissolved Species Activities of 10^{-3}) [2]

2.3.3 Effects of Potential on Corrosion, and Protectiveness of Oxide Films

Figure 2-4
Schematic Diagram of an Anodic Polarization Curve of an Active/Passive Alloy
(Adapted from Figure 10-16 in [6])

- As potential is raised further, the passive region is fully entered. The passive region is believed to be the result of increased stability of protective oxide films at the higher potentials. In the passive region of the polarization plot, no significant corrosion is observed. As potential is raised still further, general corrosion or wastage occurs.

Figure 2-5
Polarization Curve for Alloy 600 in Caustic at 300°C (Adapted from [7])

Figure 2-6
Polarization Curve for 600MA and 600SR in Complex Acid Environment [7]

Figure 2-7
Polarization and Pitting Behavior of Alloy 800NG in Acid Chlorides [8]

Figure 2-8
Polarization Curve for Alloy 600MA in Near Neutral Concentrated Sodium Chloride [7]

2.3.4 Effects of Specific Species

2.3.4.1 Known Deleterious Species

Table 2-1
Relative Corrosion Behavior* of Alloys 600, 690, 800, and Stainless Steel [66]

Figure 2-9
Cracking Time in Sodium Tetrathionate for Alloy 600 C-Rings with Two Different Heat
Treatments [16]

2.3.4.2 Possibly Deleterious Species

2.3.4.3 Possibly Beneficial Species

2.3.5 Modes of Corrosion Affecting Alloys 600, 800 and 690

Figure 2-10
Alloy 600 Corrosion Mode Diagram (T~300°C) (Adapted from Staehle, [48])

Figure 2-11
Corrosion Mode Diagram for Alloys 600MA, 600TT and 690TT (Based on CERT Tests at 300°C) (from [56])

2.3.6 SCC and IGA Growth Rates

Figure 2-13
SCC Growth Rate vs. pH at 315°C for 600MA (Adapted from [64])

2.4 Corrosion of Tubing Alloys – Engineering Aspects

2.4.1 Susceptibility in a Variety of Possible Environments

2.4.2 Effects of Material Condition and Type on Susceptibility to Corrosion

Figure 2-14
Re-Creation of Berge/Donati Summary Curve for SCC in Deaerated NaOH at 350°C
with C-Rings Stressed to About Yield [83]

2.4.3 Elevated (Anodic or Oxidizing) Electrochemical Potentials

Figure 2-15
Relationship between Inside and Outside of Crevice Compared with Open Circuit
Conditions for Crevices which are Alkaline or Acid [91]

Figure 2-16
Maximum Crack Depth vs. Specimen Potential for 600MA and 600TT Exposed to 10% NaOH at 315°C (Adapted from 92)

2.4.4 Depressed (Cathodic) Electrochemical Potentials

Figure 2-17
Corrosion Potentials of Type 304 Stainless Steel as a Function of Hydrazine Concentration
at 100, 200, 250 and 288°C in High Purity Water [97]

2.4.5 High Temperature, High Stress, and Local Cold Work

2.4.6 Denting

Figure 2-18
The Influence of pH and Electrode Potential on the Radius Change of Carbon Steel and
Type 405 Stainless Steel at 280°C [101]

2.4.7 Effects of Lead

2.4.8 Pitting

2.4.9 Contaminated Steam and Internal Oxidation

2.4.10 Thermal Performance Issues

Figure 2-19
Steam Pressure Deviation from Design

Figure 2-20
Scale Thickness as a Function of Operating Time [120]

2.4.11 Considerations Regarding Use of Inhibitors

Table 2-2

Stress Corrosion Cracking Results for C-Rings in 50% Caustic Solutions at 320°C. The Reference Environment is 50% NaOH + 1% Na₂CO₃. Exposure Times Were 2 Days in the Reference Solution and with the Boric Acid Additive; All Others Were 1 Week [41]

2.4.12 Considerations Regarding Wet Layup of Steam Generators

2.5 Balance of Plant Considerations

2.5.1 General Corrosion and Flow-Accelerated Corrosion (FAC) of Piping and Components, Including Steam Generators

Figure 2-21
Equilibrium Corrosion Product Release Rate from Alloy 706 (90/10 Copper Nickel) [151]

Figure 2-22
Effect of pH on Iron Concentration at the Economizer Inlet

Figure 2-23
Relative FAC Rate (Ratio to FAC Rate without Hydrazine and Oxygen) Measured
in a Single-Phase Flow at 180°C and 235°C Using Ammonia ($\text{pH}_{25^\circ\text{C}}=9.0$) with
Different Amounts of Hydrazine and Oxygen [159]

Figure 2-24
Relative FAC Rate of a Carbon Steel with 0.009% Cr as a Function of Hydrazine
Concentration in Water Conditioned with NH_3 , $\text{pH}_{25^\circ\text{C}}$ of 9, Test Temperature of 235° C [172]

Figure 2-25
Relative FAC Rate (Ratio to FAC Rate without Hydrazine and Oxygen) versus Hydrazine Concentration for Tubular Carbon Steel Specimens (0.009% Cr) Exposed to a Single-Phase Flow at 180°C Using Ammonia ($\text{pH}_{\text{25}^\circ\text{C}}=9.0$) and With Oxygen Maintained Less Than or Equal to 0.5 ppb [159]

2.5.2 BOP Layup Considerations

2.5.3 Startup and Cleanup Considerations

2.5.4 Turbines

2.5.5 Secondary System Heat Exchangers

2.6 Once-Through Steam Generators (OTSGs)

2.7 References

3

WATER CHEMISTRY CONTROL STRATEGIES

3.1 Introduction

Chapter 2 discussed the corrosion mechanisms that can lead to degradation of steam generator tubing, with specific emphasis on the corrosion of Alloy 600MA. Chapter 2 also noted that Alloys 600SR, 600TT, 800NG, and 690TT are subject to the same corrosion mechanisms as Alloy 600MA, though somewhat more resistant. This chapter presents a variety of chemistry control strategies that can be used to adjust those parameters that were shown to accelerate corrosion of steam generator tubing materials. Included in this chapter are:

3.2 Role of Concentration Processes

3.2.1 Concentration on Clean Tube Surfaces and Shallow Tube Scales

Figure 3-1
Concentration Factors vs. Heat Flux for 1 mil Deposit [2]

Figure 3-2
Schematic of a Kinetically-Limited Concentration Process [4]

Figure 3-3
Crevice pH as a Function of Concentration Factor (MULTEQ Options: Static, Precipitates Retained, Vapor Removed)

Table 3-1
Chemistry Input for Determining Effects of Localized Concentration

3.2.2 Concentration in Flow-Occluded Regions of RSGs

Figure 3-4
Crevice pH as a Function of Concentration Factor for Na = 3 X Cl
(MULTEQ Options: Static, Precipitates Retained)

Figure 3-5
Crevice pH as a Function of Concentration Factor for Na = Cl
(MULTEQ Options: Static, Precipitates Retained)

Figure 3-6
Crevice pH as a Function of Concentration Factor for Cl = 3 X Na
(MULTEQ Options: Static, Precipitates Retained)

Figure 3-7
Crevice pH as a Function of Concentration Factor for Sulfate Solutions
(MULTEQ Options: Static, Precipitates Retained, Vapor Removed)

Figure 3-8
Conceptual Design of Heated Crevice Device Showing the Autoclave Heated Tube and
Simulated Support Plate [7]

Figure 3-9
Amount of Accumulated Sodium as a Function of Exposure to Sodium in the Feedwater [6]

3.2.3 Conclusions

∴

3.3 pH and ORP Optimization to Minimize Iron Transport

3.3.1 pH Control

3.3.1.1 Supporting Aspects of Alternate Amine Treatment

3.3.1.2 Considerations for Implementing Advanced Amine Treatment

3.3.2 Targeted pH Control by Tailored Injection of Amines

3.3.3 ORP Control

3.4 Control or Adjusting Water Chemistry or Power Level to Minimize the Formation of Aggressive Water Chemistry Environments in Flow-Occluded Regions

3.4.1 ALARA Chemistry

3.4.2 Molar Ratio Control (For Recirculating Steam Generators)

3.4.2.1 Supporting Aspects of Molar Ratio Control

3.4.2.2 Considerations for Implementing Molar Ratio Control

3.4.3 Low Power Soaks

3.4.3.1 Supporting Aspects of Low Power Soaks

3.4.3.2 Considerations for Implementing Low Power Soaks

3.5 Controlling the ECP in Localized Regions of the Steam Generator

3.5.1 Elevated Hydrazine Operation

Figure 3-10
Feedwater and Steam Generator ECP Measurements as a Function of FW Hydrazine
(ppb)/CPD O₂ (ppb) [23]

Figure 3-11
Percent of Iron as Magnetite in Steam Generator Blowdown as a Function of FW Hydrazine
(ppb)/CPD O₂ (ppb) [23]

3.5.1.1 Supporting Aspects of Elevated Hydrazine

3.5.1.2 Considerations for Implementing Elevated Hydrazine Chemistry

3.5.2 Effects of Interruptions in Hydrazine Addition

3.5.3 Startup Oxidant Control

3.6 Minimizing Other Corrosion Accelerants

3.6.1 Lead

3.6.1.1 Supporting Aspects of Lead Minimization

3.6.1.2 Considerations for Lead Minimization

3.6.2 Copper

3.6.2.1 Supporting Aspects of Copper Minimization

3.6.2.2 Considerations for Copper Minimization

3.7 Adding Chemicals to Inhibit Corrosion

3.7.1 Boric Acid Treatment

3.7.1.1 Plant Trip with Recovery of Power – No Cooldown

3.7.1.2 Plant Trip, Hot Standby Maintained for More than Two Days

3.7.1.3 Heatup with High Boric Acid for Chemically Cleaned Steam Generators

3.7.1.4 Supporting Aspects of BAT

3.7.1.5 Considerations for Implementing BAT

3.7.2 Use of Corrosion Inhibitors

3.7.2.1 Supporting Aspects of Chemical Inhibitors

3.7.2.2 Considerations for Using Chemical Inhibitors

3.8 Management of Steam Generator Deposits

Water Chemistry Control Strategies

Corrosion Product Transport Control

Steam Generator Deposit Removal

3.8.1 Chemical Cleaning

3.8.1.1 Supporting Aspects of Chemical Cleaning

3.8.1.2 Considerations for Chemical Cleaning

3.8.2 Top of Tubesheet Sludge Removal

3.8.2.1 Supporting Aspects of Top of Tubesheet Sludge Removal

3.8.2.2 Considerations for Top of Tubesheet Sludge Removal

3.8.2.3 Sludge Lancing

3.8.2.4 In-bundle Sludge Lancing

3.8.2.5 Ultrasonic Energy Cleaning

3.8.3 Tube Bundle Sludge Removal Technologies

3.8.3.1 High Volume Bundle Flushing

3.8.3.2 Upper Bundle Hydraulic Cleaning

3.8.3.3 Scale Conditioning Agents

3.9 References

4

METHODOLOGY FOR PLANT-SPECIFIC OPTIMIZATION

4.1 Introduction

Due to the wide range of conditions and materials of construction in the secondary system, no single optimum water chemistry program can be specified for all PWRs. As such, a site-specific optimized water chemistry program requires development. This program should consider factors such as steam generator and BOP component design and operating history and use of condensate and/or blowdown demineralizers. The overall objective of the optimization is to maximize the total avoided costs from corrosion and other performance related issues while minimizing operating costs. Since a cost/benefit analysis for the secondary system cannot be completed with great certainty, the approach presented here considers the relative risks/benefits of various chemistry programs on a component-by-component basis. It is recognized that tradeoffs exist whereby optimization of the water chemistry program for one component (e.g., steam generators) could negatively impact costs of operating other components (e.g., demineralizers). The relative importance of individual components should be evaluated based on utility and plant-specific considerations. The goal of this chapter of the guidelines is to provide a basis for establishing an optimized secondary water chemistry program, not to prescribe the program in detail.

4.2 Definition of Component/System Conditions and Design Features

4.2.1 Summary of Approach

4.2.2 Component Susceptibility

4.2.3 Component Reliability

Table 4-1
Corrosion Susceptibility of Major Components/Systems

Table 4-2
Component/System Reliability

4.3 Prioritization of Components/Systems

Table 4-3
Relative Impact of Components/Systems on Establishing an Optimized Chemistry Program

4.4 Selection of Chemistry Control Programs

4.4.1 General Considerations

4.4.2 ALARA Chemistry

4.4.3 Molar Ratio Control (RSGs)

4.4.4 Integrated Exposure (RSGs)

4.4.5 Boric Acid Treatment and Injection of Corrosion Inhibitors

4.4.6 Minimization of Steam Generator Oxidant Exposure

4.4.6.1 Elevated Hydrazine

Figure 4-1
Feedwater Mossbauer Results at Plant X (Blowdown Data Shown as Solid Circles)

4.4.6.2 Limiting Exposure to Startup Oxidants

4.4.7 Secondary System pH Control

4.4.8 Steam Generator Deposit Management

4.4.9 NEI Commitments Regarding Chemistry Control – Strategic Water Chemistry Control Plan

4.4.10 Documenting Exceptions to Diagnostic Parameters

Table 4-4
Examples of Secondary Chemistry Initiative Evaluations

4.5 Final Optimization of Secondary Chemistry Program

Table 4-5
Flowchart for Site-Specific Chemistry Optimization

Table 4-5
Flowchart for Site-Specific Chemistry Optimization (Continued)

Table 4-6
Examples of Plant Specific Chemistry Targets for RSGs

—

Table 4-7
Examples of Plant Specific Feedwater Chemistry Target Values for OTSG Plants
(Power Operation)

4.6 References

5

WATER CHEMISTRY GUIDELINES RECIRCULATING STEAM GENERATORS

5.1 Introduction

These guidelines reflect current understanding of the role of chemical transport, impurity concentrations, material selection, corrosion behavior, chemical analysis methods, and industry practices on the operation and integrity of steam generator systems.

The guidelines included in this chapter represent a condensation of the technical bases from Chapter 2, chemical control strategies from Chapter 3, and optimization issues from Chapter 4 into a generic program for recirculating steam generators (RSG).

5.2 Control and Diagnostic Parameters

5.3 Action Levels

5.3.1 Action Level 1

5.3.1.1 "Shall" Requirement Actions

5.3.2 Action Level 2

5.3.3 Action Level 3

5.4 Corrective Actions

Typical corrective actions for various plant status modes are also presented. These corrective actions are not meant to be all-inclusive or universally applicable but should be considered. It should be noted that impurities may originate from within the system (weld repair, plant modification, component replacement, etc.) or from without (condenser cooling water leak, makeup water contamination, etc.). Corrective actions vary accordingly.

5.5 Specific Guidelines and Technical Justifications

5.5.1 Cold Shutdown/Wet Layup

5.5.1.1 Guidelines

5.5.1.2 Discussion

Table 5-1
Full Wet Layup (RCS $\leq 200^{\circ}\text{F}$) Steam Generator Sample

5.5.1.3 Justification for Parameters and Values

5.5.1.3.1 Steam Generator

5.5.1.3.2 Fill Source/Steam Generator

5.5.1.4 Corrective Action Guidelines

5.5.2 Heatup/Hot Shutdown (RCS >200°F, <30% Reactor Power)

5.5.2.1 Guidelines

5.5.2.2 Discussion

Table 5-2
Recirculating Steam Generator Heatup/Hot Shutdown and Startup (RCS >200°F to <30%
Reactor Power) Feedwater Sample (from Steam Generator Feed Source)

Table 5-3
Recirculating Steam Generator Heatup/Hot Shutdown and Startup (RCS >200°F to <30%
Reactor Power) Blowdown Sample

5.5.2.3 Justification for Parameters and Values

5.5.2.4 Corrective Action Guidelines – Heatup

5.5.3 Power Operation

5.5.3.1 Guidelines

5.5.3.2 Discussion

Table 5-4
Recirculating Steam Generator Power Operation ($\geq 30\%$ Reactor Power) Feedwater Sample

Table 5-5
Recirculating Steam Generator Power Operation ($\geq 30\%$ Reactor Power) Blowdown Sample

5.5.3.3 Justification for Parameters and Values

5.5.3.4 Corrective Action Guidelines – Power Operation

5.6 References

6

WATER CHEMISTRY GUIDELINES ONCE-THROUGH STEAM GENERATORS

6.1 Introduction

The guidelines presented in this chapter reflect the current understanding of the roles of chemical transport, impurity concentrations, and materials on the operation and integrity of once-through steam generator (OTSG) systems. They also reflect the technical bases of Chapter 2, the chemical control strategies of Chapter 3 and the optimization issues of Chapter 4.

6.2 Control and Diagnostic Parameters

6.3 Action Responses

6.3.1 Action Level 1

6.3.2 Action Level 2

6.3.2.1 "Shall" Requirement Actions

6.3.3 Action Level 3

6.4 Status Modes

6.5 Guidelines

6.5.1 Cooldown/Hot Soaks

6.5.2 Cold Shutdown/Wet Layup

6.5.2.1 Guidelines/Technical Justifications

Table 6-1
Full Wet Layup (RCS $\leq 200^{\circ}\text{F}$) (Technical Specification Modes 5 and 6) Steam Generator
Sample

Table 6-2
Once-Through Steam Generator Fill Water

6.5.2.2 Parameter Justifications

6.5.2.3 Corrective Actions

6.5.3 Startup, Hot Standby, and Reactor Critical at <15% Reactor Power (RCS >200°F, <15% Reactor Power) – Modes 1, 2, 3 and 4 of STS

6.5.3.1 Guidelines/Technical Justifications

Table 6-3
Once-Through Steam Generator Startup/Hot Standby/Reactor Critical at <15% Reactor
Power (Technical Specification Modes 1, 2, 3 and 4) Feedwater Sample

Table 6-4
Once-Through Steam Generator Startup/Hot Standby/Reactor Critical at <15% Reactor
Power (Technical Specification Modes 1, 2 and 3 and Mode 4 During Startup)
Blowdown Sample*

6.5.3.2 Parameter Justifications

6.5.3.2.1 Feedwater

6.5.3.2.2 Steam Generator Bulk Water

6.5.3.3 Corrective Actions

After verification that a parameter is not within normal limits, the following corrective actions should be considered:

6.5.4 Power Operation ($\geq 15\%$ Reactor Power)

6.5.4.1 Guidelines/Technical Justifications

Feedwater chemistry guidelines for power operation are given in Table 6-5. Chemistry guidelines for condensate samples are given in Table 6-6. For normal operation, these values represent limits below which little impurity-related corrosion of steam generator or turbines has been noted by the industry. Out-of-guideline conditions should be corrected to normal values within the time specified. Higher water quality should be maintained whenever possible.

Table 6-5
Once-Through Steam Generator Power Operation ($\geq 15\%$ Reactor Power)
Feedwater Sample

Table 6-6
Once-Through Steam Generator Power Operation (>15% Reactor Power)
Condensate Sample

6.5.4.2 Parameter Justifications

6.5.4.3 Corrective Action Guidelines – Power Operation

After verification that a parameter is out-of-guidelines, the following corrective actions should be considered:

6.6 References

7

DATA: COLLECTION, EVALUATION, AND MANAGEMENT

7.1 Introduction

Table 7-1
Continuous Instrumentation Suggestions for Recirculating Steam Generators

7.2 QA/QC Considerations

7.2.1 Basis for Generating Chemistry Data of Known Quality

7.2.2 Data Management

7.2.3 QC Considerations for Secondary Chemistry Control

7.3 Sampling Considerations

7.3.1 General Considerations

7.3.2 Special Sampling Considerations

Figure 7-2
Example of Feedwater Sample Line Configuration for Metal Oxide Sampling

Figure 7-4
Example of a Sample Tee Configuration

Table 7-3
Example Calculation of Oxygen Reduction in a Feedwater Sample Line

7.3.3 Sampling for Lead

7.4 Data Collection

7.5 Data Evaluation Tools

7.5.1 Introduction

7.5.2 EPRI chemWORKS™ Software

7.5.3 Calculated Cation Conductivity

7.5.4 Steam Generator Corrosion Evaluations

7.5.4.1 Source Term Evaluation

Table 7-5
Typical Source and Removal Terms in PWR Secondary Systems

Table 7-6
Source and Removal Term Percentages

7.5.4.2 Source Term Contribution from Total Organic Carbon

7.5.4.3 Integrated Exposure Evaluation (for Recirculating Steam Generators)

*7.5.4.3.1 Integrated Exposure Method A: (ppb*days)*

Figure 7-5
Spreadsheet Used to Calculate IE by Simple Integration Method

Figure 7-6
Sample Sodium IE Calculation for Plant with High Impurity Exposures During Startup

Figure 7-7
Plant Exposure at Normal Operation vs. Reference Plant Exposure

7.5.4.3.2 Integrated Exposure Method B: Tube Exposure Factor

Figure 7-8
Three Cases with Similar Cumulative Mass Accumulation Over the Cycle Length

Figure 7-9
Relative Tube Surface Area Wetted for Three Different Cases where Cumulative Mass Accumulation at the End of the Cycle is the Same

Figure 7-10
Drilled Hole Crevice Geometry

Figure 7-11
Relationship between Surface Area Wetted vs. Volume Filled for an Eccentric Crevice

The spreadsheet used to calculate the tube exposure factors is also easy to setup.

Figure 7-13 depicts a sample spreadsheet.

Figure 7-12
Relative Tube Exposure Factor Illustrating Differences in Exposure for Cases where Total Cumulative Mass Accumulation Over the Cycle Length is the Same

Figure 7-13
Sample Spreadsheet Used to Calculate Tube Exposure Factors

Figure 7-14
Example Relative Tube Exposure Factor for an Actual Operating Cycle Showing the Effect
of the Startup Transient

7.5.4.3.3 Integrated Exposure Method C: CREV-SIM

7.5.4.4 Hideout Return Evaluations

7.5.4.6 Sludge Analysis and Monitoring

7.6.2 Integrated Corrosion Product Loading

7.7.4 Steam Generator Corrosion

7.7.5 System/Component Observations

7.7.7 Process Instrument Performance and Reliability

7.7.8 Hideout Return

7.8 References

A

INTEGRATED EXPOSURE EVALUATIONS

A.1 Introduction

This appendix was created to demonstrate how some plants use integrated exposure in practice. Three plant documents (or summaries of plant documents) are presented, which describe different methodologies for use of integrated exposure.

A.2 Integrated Exposure Example 1

A.2.1 PWR Secondary Chemistry Operating Guideline

A.2.1.1 Introduction

A.2.1.2 Purpose

A.2.1.3 Operating Philosophy.

A.2.1.4 Basis

Integrated Exposure Evaluations

A.2.1.5 Operating Methodology

A.3 Integrated Exposure Example 2

A.3.1 Utilization of Integrated Exposure Limits to Control Molar Ratio

A.4 Integrated Exposure Example 3

A.5 References

B

PWR STEAM CHEMISTRY CONSIDERATIONS

B.1 Introduction

B.2 PWR Steam Chemistry Considerations

B.2.1 Introduction to Paper

This paper reviews the key issues associated with steam chemistry in PWR's. Over the past several years, EPRI and other international organizations have sponsored a research program focused on steam chemistry within power plant steam cycles.

B.2.2 Recommendations

B.2.3 Discussion

B.2.4 Deposition Processes in Turbines

PWR Steam Chemistry Considerations

Figure B-1
Location of Salt Concentration in LP Turbines

B.2.5 Steam Chemistry Guidelines

Table B-1
Reheat Steam Limits in Drum Units

B.2.5.1 Acceptability of this Approach to Setting PWR Guidelines

B.2.5.2 Alternative Approach

Figure B-2
Steam Expansion Path for Fossil and Nuclear Steam Cycles

B.3 References

7

About EPRI

EPRI creates science and technology solutions for the global energy and energy services industry. U.S. electric utilities established the Electric Power Research Institute in 1973 as a nonprofit research consortium for the benefit of utility members, their customers, and society. Now known simply as EPRI, the company provides a wide range of innovative products and services to more than 1000 energy-related organizations in 40 countries. EPRI's multidisciplinary team of scientists and engineers draws on a worldwide network of technical and business expertise to help solve today's toughest energy and environmental problems.

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